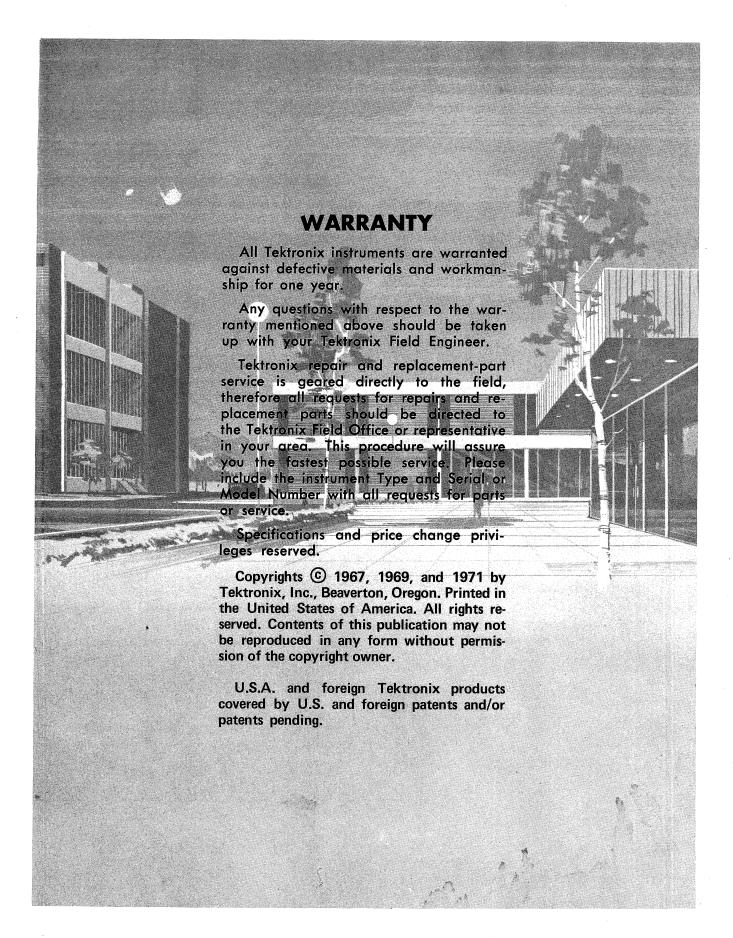
# MANUAL

Serial Number \_\_\_\_\_

TYPE Chris Wingrup

520/R520

NTSC VECTORSCOPE



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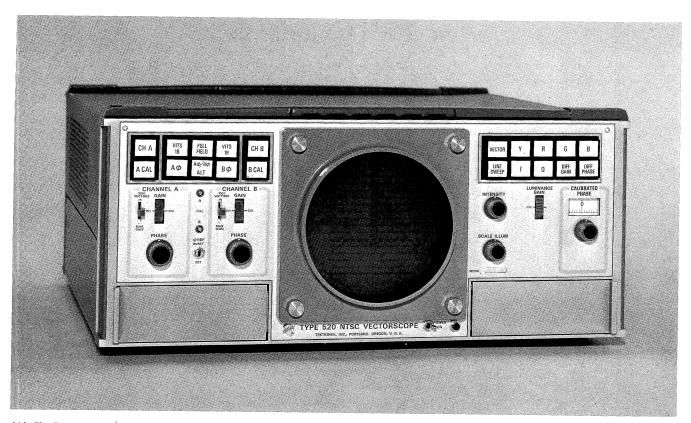
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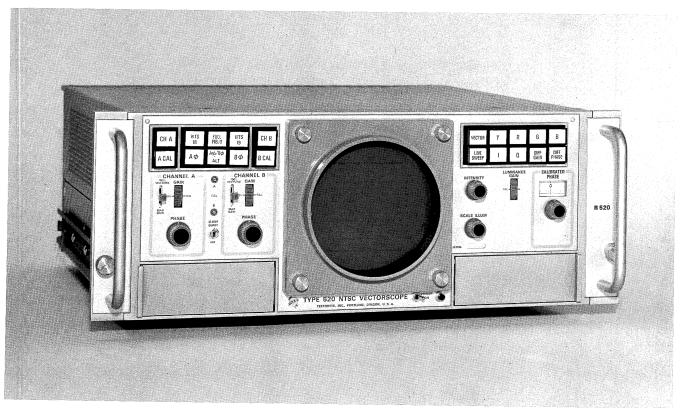
Section 10 Rackmounting

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Abbreviations and symbols used in this manual are based on, or taken directly from, IEEE Standard 260 "Standard Symbols for Units", MIL-STD-12B and other standards of the electronics industry. Change information, if any, is located at the rear of the manual.



(A) The Type 520 NTSC Vectorscope (bench model).



(B) The Type R520 NTSC Vectorscope (rackmount model).

Fig. 1-1. Both models of the Vectorscope are electrically identical. Mechanical parts are available from Tektronix, Inc. to permit easy field conversion from one type of Vectorscope to the other (see Section 10 in this manual).

# SECTION 1 TYPE 520/R520 NTSC SPECIFICATION

Change information, if any, affecting this section will be found at the rear of the manual.

#### **General Information**

The Tektronix Type 520 or R520 NTSC Vectorscope<sup>1</sup> is designed to measure luminance, hue and saturation of the NTSC<sup>2</sup> composite color television signal. This instrument uses silicon solid-state circuitry for low-wattage power consumption and cool operation. No fan is required; hence, instrument operation is quiet. The Type R520 is intended for continuous monitoring of the signal. Self-canceling pushbutton switches permit rapid selection of displays for quick analysis of the television signal characteristics, and to check the Vectorscope calibration.

The luminance channel in the Type R520 separates and displays the luminance (Y) component of the composite color signal. The Y component is combined with the output of the chrominance demodulators for R, G and B modes which are displayed at a line rate. The chrominance channel demodulates the chrominance signal to obtain color information from the composite video signal in VECTOR, LINE SWEEP, R, G, B, I, Q, DIFF GAIN and DIFF PHASE displays.

Horizontal displacement is a function of time in all modes except VECTOR. In the VECTOR mode a polar plot is displayed. The radius of a polar plot is a function of the peak-to-peak amplitude of the chrominance signal; the angular (phase) displacement is relative to the phase of the reference vector (burst).

Two inputs are provided which can be operated independently or on a time-sharing basis. Each channel can be checked for chrominance-channel gain calibration and luminance-channel gain calibration accuracy with an internal test signal. A digital line selector allows the display of a single line Vertical Interval Test Signal (VITS) from a selected line of either field 1 or field 2.

#### **ELECTRICAL CHARACTERISTICS**

The following performance requirements are valid over the stated environmental range for instruments calibrated at an ambient temperature of  $+20^{\circ}\text{C}$  to  $+30^{\circ}\text{C}$ . A 20 minute warmup is required for rated accuracies.

TABLE 1-1
CHROMINANCE ELECTRICAL CHARACTERISTICS

Characteristic	Performance Requirement
Frequency Response Chrominance Bandwidth:	
	3.579545 MHz

<sup>&</sup>lt;sup>1</sup>Since both models of the Vectorscope are electrically identical, the Type R520 is used for the text and illustrations in this manual unless noted otherwise.

Upper —3dB Point	F <sub>sc</sub> +500 kHz, ±100 kHz
Lower —3 dB Point	F <sub>sc</sub> −500 kHz, ±100 kHz
Vector	
Phase Accuracy	1° or less error between marker and graticule.
Incremental Phase Accuracy	0.5° or less error in any 10° segment on vector graticule.
QUAD PHASE Adjustment Range	$+2^{\circ}$ to $-2^{\circ}$ , total of $4^{\circ}$ .
Test Circle Amplitude	Within 1% of 707 mV.
Color Decoding Accuracy in R, G and B Modes	Within 3% amplitude of Red, Green or Blue component.
I	Demodulation axis 57° from burst within 2° when burst axis has been aligned with vector graticule.
Q	Demodulation axis 147° from burst within 2° when burst axis has been aligned with vector graticule.
DIFF GAIN Deflection Factor	SN B150100 and up: 5% change deflects trace 5% (25 IRE units, 0.5 inches) within 5% (VITEAC Modulated Stairstep Signal, chrominance +3 dB, —6 dB of 143 mV).  Below SN B150100: With variable GAIN control set to CAL, 5% change of a 143-mV signal deflects trace 5% (25 IRE units, 0.5 inches) within 5%.
Differential Gain: (50% APL)	1% or less last 90% of trace.
Dynamic Gain (10% to 90% APL)	1% or less last 90% of trace.
DIFF PHASE Resolution	0.1° of differential phase will produce at least 1 IRE unit of deflection on a normal staircase test signal 143 mV P-P subcarrier.
Burst φ REF: (50% APL)	0.3° of differential phase last 80% of trace.
Dynamic Phase (10% to 90% APL)	0.3° of differential phase last 80% of trace.

<sup>&</sup>lt;sup>2</sup>National Television System Committee.

TABLE 1-1 (cont)
CHROMINANCE ELECTRICAL CHARACTERISTICS

Performance Requirement
0.15° or less of differential phase last 90% of trace.
0.15° or less of differential phase last 90% of trace.
+15° to $-15$ °, total 30°.
Within 10% per 2° increment. Total incremental error 0.5° or less between +14° and -14°.
1° or less.
Trace will shift <0.2° in 10 s.
Within 15 Hz of 3.579545 MHz.
15 s or less with $F_{sc}$ within 15 Hz.
3 minutes, subcarrier within
15 Hz.
1.5 V to 2.5 V.

TABLE 1-2
LUMINANCE ELECTRICAL CHARACTERISTICS

Characteristic	Performance Requirement
Luminance Bandwidth —3 dB Rolloff Frequency	700 kHz to 1.1 MHz.
Luminance Gain	140 IRE units within 1% per volt in the 75% CAL.
LUMINANCE GAIN Range	0.7:1 to 1.4:1 ( $+3  dB$ to $-3  dB$ ).

TABLE 1-3
INPUT ELECTRICAL CHARACTERISTICS

Characteristic	Performance Requirement
Input Amplitude Range	0.7 V to 1.4 V video (sync tip to peak white).
Maximum DC Level	+20 V, -20 V.
Gain Stability With Time, Temperature and Line Volts	Within 1% (except in DIFF PHASE and DIFF GAIN) with line voltage. Within 5% with temperature.
Time Sharing Switching Rate	One fourth H rate. Locked to H sync.
Input Horiz Sync Input Range 50% APL	0.7 V to 1.4 V.
Dynamic (10% to 90% APL)	0.8 V to 1.4 V.
Ext Horiz Sync Input Range 50% APL Composite Video	0.7 V to 1.4 V.
Dynamic (10% to 90% APL) Composite Video	0.7 V to 1.4 V.
Composite Sync	3.5 V to 7.5 V.
	1

Channel A GAIN and Chan- nel B GAIN Range (Vari- able)	0.5:1 to 1.4:1 (+3 dB, -6 dB).
Input Attenuator 100% VECTOR (Chromi- nance and Luminance)	Within 2% of 0.75 times gain in 75% CAL.
75% (Chrominance and Luminance)	Within 1% of 140 IRE units per volt.
Maximum GAIN (Chrominance only)	SN B150100 and up: Internally adjustable to 5 times gain in 75% CAL. Below SN B150100: Within 5% of 3.5 times gain in 75% CAL.
Return Loss (terminated in 75 ohms, Input in Use or Not in Use, Instrument On or Off). Input A	Greater than 40 dB (DC to 5 MHz).
Input B	Greater than 40 dB (DC to 5 MHz).
Ext φ Reference	Greater than 40 dB at 3.58 MHz.
Ext Sync for 4 V Composite Sync (Factory Connected)	Greater than 46 dB (DC to 5 MHz).
1 V Composite Video (Optional Connection)	Greater than 40 dB (DC to 5 MHz).

## TABLE 1-4 VERTICAL & HORIZONTAL AMPLIFIER ELECTRICAL CHARACTERISTICS

Characteristic	Performance Requirement
Clamp Stability With Temperature and Line Voltage	1 minor div or less.
VECTOR With Rotation of A PHASE, B PHASE Con- trol	2 minor div or less X and Y axis. 3.58 MHz component on synctips 2 mV or less.
Y (Luminance) Display Shift	1 minor div or less with dynamic shift (10% to 90% APL).
Display Shift with Operation of LINE SWEEP, I, Q and DIFF PHASE	3 IRE units or less.

## TABLE 1-5 POWER SOURCE ELECTRICAL CHARACTERISTICS

Characteristic	Performance Requirement
Line Voltage Ranges	
	90 VAC to 110 VAC
	104 VAC to 126 VAC
	112 VAC to 136 VAC
	180 VAC to 220 VAC
	208 VAC to 252 VAC
	224 VAC to 272 VAC
Maximum Power Consumption at 115 VAC, 60 Hz.	100 watts
Maximum Amperes at 115 VAC, 60 Hz.	1.1 A
Line Frequency	47 Hz to 63 Hz

TABLE 1-6
CRT DISPLAY ELECTRICAL CHARACTERISTICS

Characteristic	Performance Requirement
Type T5201	
Horizontal Resolution	At least 12 lines/cm
Vertical Resolution	At least 10 lines/cm
Usable Scanning Radius	5.5 cm
Geometry	0.05 cm or less
Orthogonality	Within 1°
Trace Rotation	At least $+3^{\circ}$ to $-3^{\circ}$ , total of 6°.

TABLE 1-7
PHYSICAL CHARACTERISTICS

Characteristic	Information
Finish	Anodized aluminum front panel. Blue vinyl painted cabinet.
Overall Dimensions (measured at maximum points)	
Type 520	7 inches high, 16% inches wide and 19% inches long. 17.8 cm high, 42.9 cm wide and 48.7 cm long.
Type R520	7 inches high, 19 inches wide and 193/4 inches long.
	17.8 cm high, 48.3 cm wide and 50.2 cm long.

### ENVIRONMENTAL CHARACTERISTICS (see Table 1-8)

The following environmental test limits apply when tested in accordance with the recommended test procedure. This instrument will meet the electrical performance requirements given in this section following an environmental test. Complete details on environmental test procedures, including failure criteria, etc., may be obtained from Tektronix, Inc. Contact your local Tektronix Field Office or representative.

**TABLE 1-8** 

Characteristic	Information
Temperature Non-operating	—40° C to +65° C
Operating	0° C to +50° C
Altitude Non-operating Operating	To 50,000 feet. To 15,000 feet.
Transportation	Qualified under National Safe Transit Committee procedure 1A, Category I (18-inch drop), when properly packaged (see Section 4 of this manual for repackaging in- structions).

#### **ACCESSORIES**

Standard accessories supplied with this instrument can be found on the last page of the Mechanical Parts List Illustrations in this manual. For additional accessories, see the current Tektronix, Inc. catalog.

### NOTES

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# SECTION 2 OPERATING INSTRUCTIONS

Change information, if any, affecting this section will be found at the rear of the manual.

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FIRST-TIME OPERATION	2-12	To convert a rackmount Vectorscope (Type R5: bench model (Type 520), or vice versa, refer to	
GENERAL OPERATING INFORMATION		in this manual.	
Pushbutton Switches	2-20		
Internal Triggering Source	2-20	Operating Voltage	
Opening the Access Doors	2-20	The Vectorscope may be operated from either a 230-V line voltage source. Quick-change li	a 115-V or ne-voltage
Positioning the Right Recessed Control Subchassis	2-22	selector plugs, located under the fuse cover or panel, change the transformer primary connection instrument can operate from one line voltage or	n the rear ons so the
Graticule Illumination	2-22	(115 V or 230 V). In addition, the plugs permit on	ie of three
Burst Brightening	2-22	line voltage operating ranges to be selected. Tab all the voltage ranges that enable the instrument	
Vector Displays	2-22	supplies to regulate properly.	- •
Linear Sweep Displays	2-22	To convert to a different line voltage, proceed	as follows:
Dual Displays	2-22	1. Disconnect the Vectorscope from the power	source.

TABLE 2-1

115/230 Voltage Selector Plug Position	Range Selector Plug Position	Nominal Line (center) Voltage	Line Voltage Operating Range <sup>1</sup>
	LO (Low)	100 VAC	90 to 110 VAC
115	M (Medium)	115 VAC	104 to 126 VAC
	HI (High)	124 VAC	112 to 136 VAC
	LO (Low)	200 VAC	180 to 220 VAC
230	M (Medium)	230 VAC	208 to 252 VAC
	HI (High)	248 VAC	224 to 272 VAC

- 2. Unscrew the two captive screws which hold the fuse cover. Remove the cover with attached fuses.
- 3. To convert to a different line voltage (115 V or 230 V), pull out the 115/230 Voltage Selector plug (see Fig. 2-1). Rotate the plug 180° and insert it into the opposite set of holes. The 115/230 Voltage Selector plug is located in the upper position for 115-V operation and in the lower position for 230-V operation.
- 4. To change the line-voltage operating range (LO, M or HI), pull out the Range Selector plug (see Fig. 2-1) and insert it in the desired hole locations. Select a range which has a center voltage (see column 3 in Table 2-1) that closely corresponds to the line voltage that will be applied when completing this procedure.

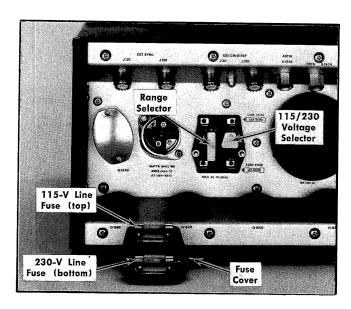


Fig. 2-1. Location of Range and Voltage Selector plugs with fuse cover removed. The plugs as shown are set for 115-V medium range operation.

5. Re-install the cover with the two captive screws and fuses. Be sure the cover fits firmly against the rear panel. This indicates that the line fuses are seated properly in the fuse clips.

6. Before applying power to the instrument, check that the indicating tabs on the selector plugs protrude through the proper holes in the cover for the correct line voltage and the proper operating range.

#### CAUTION

The Vectorscope should not be operated when the 115/230 Voltage Selector and/or Range Selector plugs are not in the correct position for the line voltage to be applied. Operation of the instrument with either plug in the wrong position may cause incorrect operation or damage to the instrument.

#### **BASIC INFORMATION**

In color television the visual sensation of color is described in terms of three quantities; luminance, hue and saturation. Fig. 2-2A shows a conical representation of these concepts.

Luminance is brightness as perceived by the eye. As the eye is most sensitive to green and least to blue light of equal energy, green is a bright color, blue is a dark color as conveyed by the luminance signal to monochrome TV receivers. Color TV receivers utilize the luminance signal to produce both monochrome and color pictures.

Chrominance consists of two additional quantities: hue and saturation. Hue is the attribute of color perception that determines whether the color is red, blue, green or the like. White, black and grey are not considered hues. Hue is presented on the Vectorscope CRT as a phase angle and not in terms of wavelength. For example, red, having a wavelength of 610 millimicrons is indicated as 104° on the standard color phase vector diagram (see Fig. 2-2B) and the Type R520 vector graticule (see Fig. 2-2C).

Saturation is the degree to which a color (or hue) is diluted by white light in order to distinguish between vivid and weak shades of the same hue. For example, vivid red is highly saturated and pastel red has little saturation. Using the Vectorscope, saturation is the radial distance from the center (where zero saturation exists) to the end of the color vector where 75% or 100% saturation exists for a particular color. If burst vector amplitude corresponds to the 75% marking, (see Fig. 2-2C) the colors are 75% saturated. If the burst vector amplitude corresponds to the 100% marking, the colors are 100% saturated.

#### NOTE

At the time of the preparation of this Instruction Manual, a portion of publication RS-189 is being amended to use the 7.5% black-level setup instead of the 10% setup formerly used. (RETMA Engineering Committee TR-4 on Television Transmitters prepared publication RS-189.)

In an NTSC color television transmission system, the hue and saturation information are carried on a single color subcarrier, 3.579545 MHz. These signals, in modulated subcarrier form, are called chrominance. The hue information is carried by the subcarrier phase; the saturation information is carried by means of amplitude modulation with the subcarrier suppressed. A subcarrier which supplies phase information is required for demodulation. No chrominance signals are present during the horizontal blanking interval, and a sample of the subcarrier is provided within this interval and is called burst.

Applicable when the line contains less than 2% total distortion.

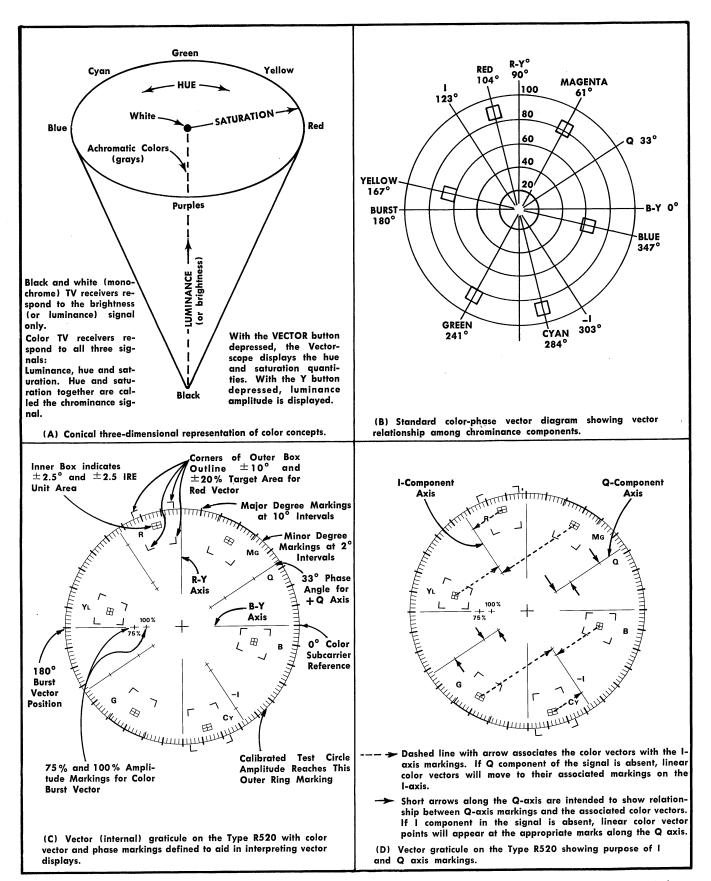


Fig. 2-2. Illustrations showing relationships between basic color concepts, standard color-phase vector diagram and the vector graticule on the Type R520.

#### Operating Instructions—Type 520/R520 NTSC

To recover the hue information, phase demodulators are employed in the Vectorscope. The phase reference is the color subcarrier which is regenerated by an oscillator in the instrument. The oscillator is locked in both phase and frequency to the color burst signal. When the VECTOR button is pressed, the Vectorscope displays the relative phase and amplitude of chrominance signal on polar coordinates. To identify these coordinates the vector graticule (see Fig. 2-2C) has points which correspond to the proper phase and amplitude of the three primary colors: R (Red), B (Blue) and G (Green). In addition, the complements of the primary colors are indicated as follows: C<sub>Y</sub> (Cyan), Y<sub>L</sub> (Yellow) and M<sub>G</sub> (Magenta).

Any errors in the color encoding, video tape recording or transmission processes which change these phase and/or amplitude relationships cause color errors on the television receiver picture. The polar coordinate type of display such as that obtained on the Type R520 CRT has proved to be the best method for portraying these errors.

The polar display permits measurement of hue in terms of relative phase of the chrominance signal with respect to the color burst. Relative amplitude of chrominance to burst is expressed in terms of the displacement from center (radial dimension of amplitude) towards the color point which corresponds to 75% (or 100%) saturation of the particular color being measured.

The outer boxes around the color points correspond to phase and amplitude error limits per FCC requirements ( $\pm 10^{\circ}$ ,  $\pm 20\%$ ). The inner boxes indicate  $\pm 2.5^{\circ}$  and 2.5 IRE units. These limits correspond to phase and amplitude error limits per EIA specification RS-189, amended for 7.5% setup.

Fig. 2-2D shows the purpose of the small marks that intersect the I and Q axis. The topic "Color Encoder" provided later in this section describes the distortions that may occur in a signal when an improper display is obtained.

The vector graticule inscribed inside the Type R520 CRT permits accurate amplitude measurements of color and burst vectors to be made when a 7.5% color setup signal is applied to the instrument. Fig. 2-3 illustrates the details of a standard encoded color bar test signal using the 7.5% setup. Color signals having 10% setup can also be measured just as accurately if the slight differences between the two setups are considered. The following paragraph describes the differences.

Table 2-2 provides a side-by-side comparison of the 10% and 7.5% setup color bar amplitudes. To use the Type R520 for 10% setup vector measurements, apply the 10% setup color test signal to the instrument. Obtain the vector display in the usual manner. Set the channel GAIN control to position the color vectors within the inner box marking on the vector graticule. When this is accomplished, the 10% setup burst vector will be slightly less than 1/32 inch (or less than 1/32 inch (or less than 1/32 inch (or less than 1/32 inch use 1/32 inch difference can be considered to be negligible. The 1/32 inch difference is derived from these distances: The distance from the center of the vector graticule to the 1/32 mark is 1/32 inch for 1/32 setup. Using a 1/320% setup color signal, the distance of the burst vector is 1/3228 inch or a difference of only 1/3238 inch.

The two major distortions to which the chrominance signal is subject are differential gain and differential phase. Both

can be measured on the Type R520 Vectorscope. Differential gain is a change in color subcarrier amplitude due to a change in the luminance signal while hue and saturation of the original signal are held constant. In the reproduced picture, the saturation will be distorted in the areas between the light and dark portions of the scene.

Differential phase is a phase change of the chrominance signal by the luminance signal while the original chrominance signal is held constant. In the reproduced picture, the hue will vary with scene brightness. Differential gain and differential phase may occur separately or together. The causes of these distortions are chrominance nonlinearities caused by luminance amplitude variations. To measure differential phase using the Type R520 no graticule is needed. Instead, the trace overlay and slide-back technique using the CALIBRATED PHASE control provides the means for performing the measurement.

The IRE graticule (see Fig. 2-4) is used primarily for measuring differential gain and video signal amplitude. To measure video signal amplitude, the IRE graticule is marked in IRE units. In standard TV practice, 140 IRE units equal 1 volt. Hence, with the aid of the IRE graticule, the composite video signal will be exactly 1 volt in amplitude when the equipment is adjusted to obtain a display amplitude of exactly 140 IRE units. Next, the IRE graticule is used as a guide for checking and adjusting the composite video signal for the following typical proportions:

- 1. The white level should correspond to the +100 IRE unit graticule marking.
- 2. The reference black level should correspond to the 7.5% setup marking.
- 3. The blanking level of the video signal should coincide with the 0 IRE graticule line.
- 4. The sync pulse amplitude should correspond to the —40 IRE unit graticule line.

Fig. 2-5 shows a modulated stairstep (or staircase) Vertical Interval Test Signal that is inserted in line 19 of field two to provide in-service trouble diagnosis. This signal has ten equal steps going from black level to white level with a burst of 3.58 MHz sine waves on each step. This signal is used for checking differential gain and differential phase. Differential gain is checked on the Type R520 by amplitude-demodulating the signal and presenting a magnified display of the successive stairstep segments. The IRE graticule has a Diff Gain scale to facilitate differential gain measurements in percent of signal gain or loss. The measurement technique is described later in step 22 of the First-Time Operation procedure.

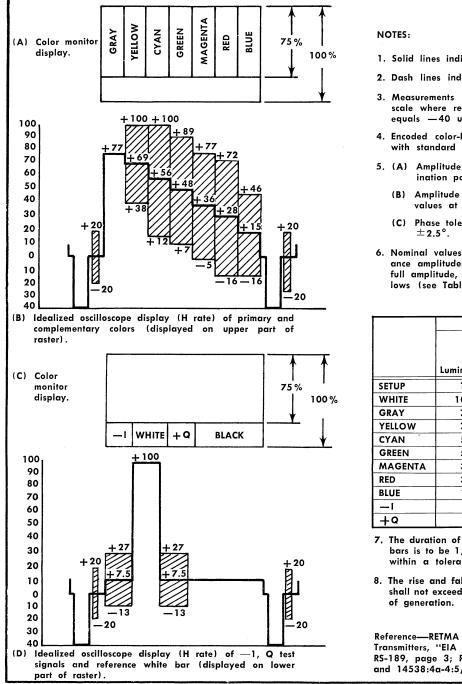
#### **CONTROLS AND CONNECTORS**

#### Introduction

A brief description of the function or operation of the Type R520 front- and rear-panel controls, adjustments and connectors is provided here (see Fig. 2-6).

#### NOTE

Some photographs of the Type R520 may show the instrument having a snap-in graticule cover and pushbuttons labeled dA and  $d\phi$ . These are pictures of an earlier instrument (below SN B150100). For later instruments (SN B150100 and up), the graticule cover is held in place with four thumb screws, dA, is changed to DIFF GAIN, and  $d\phi$  is changed to DIFF PHASE.



- 1. Solid lines indicate luminance signal levels.
- 2. Dash lines indicate color subcarrier envelope levels.
- 3. Measurements are made by using a standard IRE unit scale where reference white equals 100 units and sync equals -40 units.
- 4. Encoded color-bar signal levels shall be in accordance with standard video transmission levels.
- 5. (A) Amplitude tolerance of all luminance values at origination point equals  $\pm$  2.5 IRE units.
  - (B) Amplitude tolerance of all peak-to-peak subcarrier values at origination point equals  $\pm 2.5$  IRE units.
  - (C) Phase tolerance of colors at origination point equals  $\pm$  2.5°.
- 6. Nominal values of luminance and peak-to-peak chrominance amplitudes for fully saturated color bars, 75% of full amplitude, using 10% and 7.5% setup, are as follows (see Table 2-2):

TABLE 2-2

	10%	Setup	7.5 % Setup	
ļ		Peak-to-		Peak-to-
	1	Peak		Peak
		Chromi-		Chromi-
	Luminance	nance	Luminance	nance
SETUP	10		7,5	
WHITE	100		100	
GRAY	77		77	
YELLOW	70	60	69	62
CYAN	57	86	56	88
GREEN	50	80	48	82
MAGENTA	38	80	36	82
RED	30	86	28	88
BLUE	17	60	15	62
<b>-</b> I	10	40	7.5	40
+Q	10	40	7.5	40

- 7. The duration of each of the primary (and complementary) bars is to be 1/7 of the active portion of a scanning line within a tolerance of  $\pm 10\%$ .
- The rise and fall times of the luminance signal component shall not exceed 0.2 microseconds as measured at the point of generation.

Reference—RETMA Engineering Committee TR-4 on Television Transmitters, "EIA Standard for Encoded Color Bar Signals": RS-189, page 3; Revised RS-189, pages 14538: 3a-4:5/66 and 14538:4a-4:5/66.

Fig. 2-3. Illustrations with notes showing the characteristics of a standard encoded color bar signal using a 7.5% setup. Table 2-2 compares the amplitude of the color bars for 10% and 7.5% setup.

#### **Main Front-Panel Controls**

Signal Selector Switch Contains ten pushbuttons but consists of four separate self-canceling switches to select the following signals:

First Switch: Selects channel A signal source.

CH A: Channel A signal applied to CH A connector.

A CAL: 1-V luminance amplitude calibration test signal is applied internally

to Channel A in Y, R, G and B modes. A test circle display is obtained in the VECTOR mode for amplitude calibration and QUAD PHASE alignment.

Second Switch: Unblanks the CRT to display the selected line(s).

<sup>2</sup>VITS 18: Vertical Interval Test Signal on line 18 in either field.

FULL FIELD: Total signal for one picture (all lines).

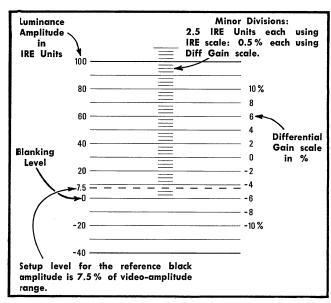


Fig. 2-4. The Type R520 IRE (external) graticule, Illuminated when

<sup>2</sup>VITS 19: Vertical Interval Test Signal on line 19 in either field.

Third Switch: Turns on the PHASE and CALIBRATED PHASE controls.

 $A\phi$ : Places A PHASE and CALIBRATED PHASE controls in operation. Operates with CH A or CH B, depending on which button is pressed.

 $A\phi/B\phi$  ALT: Enables A and B PHASE controls to operate on a time-shared basis. Used in conjunction with CH A and/or CH B pushbuttons for dual-display mode of operation. Also, used in conjunction with the CALIBRATED PHASE control.

<sup>2</sup>The circuits controlled by these buttons can be changed to display other lines as described later in this section. These buttons are used

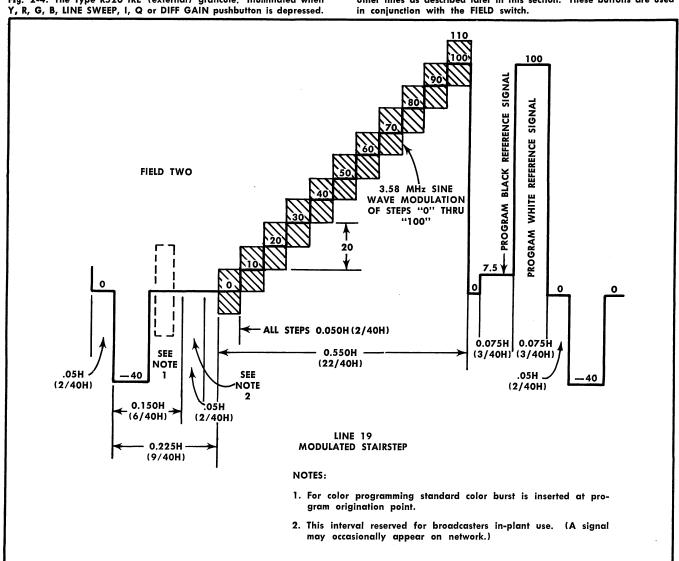


Fig. 2-5. Details of ten-step linearity test signal. Reproduced from a paper by S. C. Jenkins, Transmission Engineer, Long Lines Dept., American Telephone and Telegraph Co., "Vertical Interval Test Signals", April 8, 1964, Figure 4.

In CH A and CH B dual-display mode of operation, the A PHASE control operates with CH A and the B PHASE controls operates with CH B.

 $B\phi$ : Places B PHASE and CALIBRATED PHASE controls in operation. Operates with CH A or CH B, depending on which button is pressed.

Fourth Switch: Selects Channel B signal source.

CH B: Channel B signal applied to the CH B connector.

B CAL: 1-V luminance amplitude calibration test signal is applied internally to Channel B in Y, R, G and B modes. A test circle display is obtained in the VECTOR mode for amplitude calibration and QUAD PHASE alignment.

Channel A and B 100%-75%-MAX GAIN

Three-position lever switch. Two positions provide a calibrated gain change for observing either 100% or 75% amplitude color bar signals per EIA Spec RS-189, corrected for 7.5% setup. These percentages are International Standards. The third position is MAX GAIN for maximum calibrated gain in the DIFF GAIN mode; maximum uncalibrated gain in the other modes.

GAIN

Thumbwheel control to vary the amplitude of the input composite video signal. The control has a CAL (calibrated) detent position.

A CAL

A screwdriver adjustment which provides a means for calibrating the gain of Channel A amplifier when CH A GAIN and LUMINANCE GAIN controls are set to CAL.

**B CAL** 

A screwdriver adjustment which provides a means for calibrating the gain of Channel B amplifier when CH B GAIN and LU-MINANCE GAIN controls are set to CAL.

PHASE

Provides for continuously uncalibrated control of phase. Range is 360°.

 $\phi$  REF

Two-position lever switch to provide for selection of internal or external CW source.

BURST: Internal 3.58 MHz CW from an automatic phase and frequency controlled oscillator.

EXT: External CW source obtained via the EXT CW  $\phi$  REF connectors.

Display Selector Switch A 10-position self-canceling pushbutton switch that selects the displays that follow.

#### NOTE

In all Display Selector pushbutton modes except VECTOR, the displays are presented at the line rate on a linear time base. In the VECTOR mode, a polar plot display is presented. VECTOR: Presents a test circle display when A CAL (or B CAL), FULL FIELD and  $A\phi$  ( $A\phi/B\phi$  ALT or  $B\phi$ ) buttons are pressed. Presents a color-vector display when CH A (or CH B), FULL FIELD or VITS and  $A\phi$  ( $A\phi/B\phi$  ALT or  $B\phi$ ) buttons are pressed.

Y: Presents a luminance calibration display when A CAL (or B CAL), FULL FIELD and  $A\phi$  ( $A\phi/B\phi$  ALT or  $B\phi$ ) buttons are pressed.

Presents the luminance portion of the color signal with chrominance removed when CH A (or CH B), FULL FIELD and  $A\phi$  ( $A\phi/B\phi$  ALT or  $B\phi$ ) buttons are pressed.

#### NOTE

In the Y and DIFF GAIN modes the  $A\phi$  ( $A\phi/B\phi$  ALT or  $B\phi$ ) but tons need not be depressed to obtain a useful display. In the R, G, B, LINE SWEEP, I, Q and DIFF PHASE modes, the  $A\phi$  ( $A\phi/B\phi$  ALT or  $B\phi$ ) button must be depressed with the CH A (or CH B) and FULL FIELD buttons to obtain a useful display of the applied signal.

- R: Presents the output signal from the red camera or the red portion of the signal supplied to a color kinescope.
- G: Presents the output signal from the green camera or the green portion of the signal supplied to a color kinescope.
- B: Presents the output signal from the blue camera or the blue portion of the signal supplied to a color kinescope.

LINE SWEEP: Presents the R-Y component of the color signal when burst is aligned at 180°. Indicates time relationship of the chrominance portion of the signal; that is, the sequence in which the color vectors will be portrayed by the CRT beam when the VECTOR mode is used.

The LINE SWEEP mode is also used as the calibration mode for the Type R520. When the CH A (or CH B), FULL FIELD and  $A\phi$  ( $A\phi/B\phi$  ALT or  $B\phi$ ) buttons are depressed, the burst portion of the waveform is brightened to facilitate proper adjustment of the BURST FLAG TIMING control. When the A CAL (or B CAL), FULL FIELD and  $A\phi$  ( $A\phi/B\phi$  ALT or  $B\phi$ ) buttons are depressed, a horizontal trace for checking the BEAM ROTATE control is presented.

- I: Presents the portion of the color signal demodulated along the I axis.
- Q: Presents the portion of the color signal demodulated along the Q axis.

DIFF GAIN: Presents a magnified display of the peak amplitude of the 3.58 MHz component in the color signal for use in checking differential gain.

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DIFF PHASE: Phase-demodulates a modulated signal and presents the display greatly magnified and inverted on alternate lines allowing the use of the slideback method to overlay the two traces when measuring small phase changes. The CALIBRATED PHASE control is used for direct readout of differential phase in degrees.

INTENSITY

Controls brightness of the display by varying the CRT beam current.

SCALE ILLUM

Controls graticule illumination by varying the edge-light intensity.

LUMINANCE GAIN

Thumbwheel control for varying the gain in the luminance channel without affecting the chrominance gain. The control has a CAL (calibrated) detent position. The control varies the amplitude of the display in Y, R, G and B modes only.

CALIBRATED **PHASE** 

Provides for accurate incremental phase measurements, with a  $\pm 15^{\circ}$  total range using a metal tape dial for readout.

**POWER** 

Switch: Toggle switch to apply power to the instrument.

Light: Indicates that the POWER switch is on and the instrument is connected to a line source.

#### Recessed Front-Panel Operational Controls (right door)

**FOCUS** 

Permits adjustment of CRT beam for optimum display resolution.

**FIELD** 

Two-position slide switch to select Field 1 or Field 2 when used in conjunction with the VITS 18 and VITS 19 pushbuttons.

VERT POSITION Positions the display vertically on the CRT in Y, R, G, B and DIFF GAIN pushbutton modes only.

**BURST FLAG** TIMING

Adjusts sync circuits to compensate for variation in time between the leading edge of the sync pulse and the burst flag of the composite video signal. Adjusted when CH A (or CH B), FULL FIELD,  $A\phi$  (or  $B\phi$ ) and LINE SWEEP buttons are depressed.

#### **IMPORTANT**

If an unstable display is obtained on the Type R520 CRT, always check the positions of the  $\phi$  REF and SYNC switches first and then check that the BURST FLAG TIM-ING adjustment is properly adjusted. The BURST FLAG TIMING adjustment varies the burst sampling point by varying the start of the sweep generator. This, in turn, varies the action of the various clamps in the Type R520 circuitry and also the lock-in stability of the sweep generator. Misadjustment of the BURST FLAG TIMING control varies the stability of the subcarrier regenerator, affects the gain of the luminance channel, and may cause the horizontal sweep to drop out of sync. Hence, if an unstable display or improper luminance display amplitude is obtained, check that the BURST FLAG TIMING adjustment is adjusted properly as described in steps 8 and 9 in the First-Time Operation procedure.

SYNC

Two-position slide switch to select INT (internal) or EXT (external) sync signal source.

INT: Channel A or B amplifier is the internal sync source when CH A or CH B pushbuttons respectively are used. Channel A amplifier is the internal sync source when both CH A and CH B pushbuttons are depressed.

EXT: External sync source is obtained via the EXT SYNC input connector.

HORIZ **POSITION** 

Positions the display horizontally on the CRT in all Display Selector pushbutton modes except VECTOR.

#### Recessed Front-Panel Maintenance Adjustments (left door)

QUAD PHASE

Screwdriver adjustment to provide for fine adjustment of the 90° phase difference between the R-Y and B-Y demodulators. adjusted for optimum overlay of two test circles. Adjusted when A CAL (or B CAL), FULL FIELD,  $A\phi$  (or  $B\phi$ ) and VECTOR buttons are depressed.

GAIN BAL

Screwdriver adjustment for controlling B-Y demodulator gain. Rounds out the two merged test ellipses so a circle is obtained. Adjusted when A CAL (or B CAL), FULL FIELD,  $A\phi$  (or  $B\phi$ ) and VECTOR button are depressed.

**HORIZ POSITION** CLAMP

Screwdriver adjustment that controls the horizontal clamp level of the display in all modes.

BEAM ROTATE

Screwdriver adjustment that rotates the beam so the vertical trace can be aligned with the graticule 90°-to-270° vector graticule line. Adjusted when A CAL (or  $\ddot{B}$  CAL), FULL FIELD,  $A\phi$  (or  $B\phi$ ) and VEC-TOR buttons are depressed; blue-on-white wire to pin AB on Driver Amplifier board is disconnected. An alternate procedure is given in step 11 of the First-Time Operation procedure.

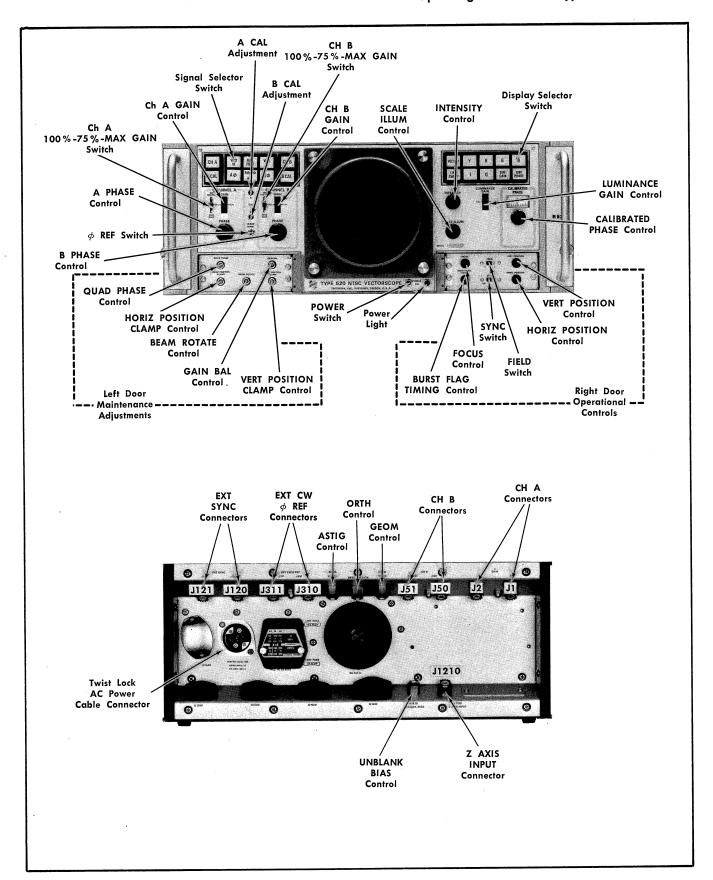


Fig. 2-6. Front- and rear-panel controls and connectors on the Type R520 Vectorscope.

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**YERT POSITION CLAMP** 

Screwdriver adjustment for controlling the vertical clamp level of the display in all modes.

#### Rear-Panel Adjustments

**ASTIG** (R1476)

Screwdriver adjustment used in conjunction with the FOCUS control to adjust the beam for optimum display resolution.

ORTH (R1474)

Screwdriver adjustment for aligning the horizontal trace parallel with nearest luminance graticule line. Adjusted when the A CAL (or B CAL), FULL FIELD,  $A\phi$  (or  $B\phi$ ) and VECTOR buttons are depressed; green-on-white wire to pin AD on Driver Amplifier board is disconnected.

GEOM (R1472)

Screwdriver adjustment for minimizing any bowing of vertical and horizontal lines. Proper adjustment is obtained when the voltage at the center arm of the GEOM control equals the voltage at the upper vertical-deflection plate (blue lead to CRT neck pin). Adjusted when FULL FIELD, Ap (or B $\phi$ ) and VECTOR buttons are depressed.

**UNBLANK BIAS** (R1478)

Screwdriver adjustment for obtaining a uniform brightness test circle. Adjusted when A CAL (or B CAL), FULL FIELD,  $A\phi$ (or  $B\phi$ ) and VECTOR buttons are depress-.

#### **Rear-Panel Connectors**

EXT SYNC

BNC connectors permit loop-through (or (J120 and J121) terminated into 75 ohms) external synchronization on composite video or sync signals.

EXT CW  $\phi$  REF BNC connectors for loop-through (or termi-(J310 and J311) nated into 75 ohms) external 3.58 MHz CW signal.

CH A (J1 and J2) and CH B (J50 and J51)

Dual-input BNC connectors. Permits loopthrough (or terminated into 75 ohms) operation for each channel with a bridging resistance of  $\approx$ 14 k $\Omega$  and a bridging

capacitance of  $\approx$ 16 pF.

Z Axis INPUT (J1210)

BNC connector permits Z-axis modulation of CRT display.

#### SIGNAL CONNECTIONS

#### Introduction

All signal connections to the Vectorscope are made through BNC coaxial connectors on the rear panel of the instrument (see Fig. 2-6). Two connectors for each input (except Z AXIS input) provide high-impedance loop-through connections so that the Vectorscope may be connected into any part of a system.

When the Vectorscope is connected to the output of a system (loop-through connections not required), a 75-ohm terminating resistor should be connected to the unused input connector to properly terminate the system.

#### **Chrominance Signal Inputs**

The signal (or signals) from the system under test is applied to the CH A input and/or CH B input connector. This may be either a composite color signal with negative-going sync pulses, or a chrominance signal only without the sync pulses. If a chrominance signal only is applied and synchronization of the sweep and unblanking is desired, separate sync pulses and usually an external subcarrier signal must be applied as described in the Sync Input and External Subcarrier Input topics that follow.

#### Sync Input

The EXT SYNC input connector accepts external signals for synchronizing the Vectorscope sweep and unblanking circuitry. This input is connected to the synchronizing circuit when the SYNC switch (located behind the right side frontpanel door) is set to the EXT position. Sync-negative composite video, about  $0.7\,\mathrm{V}$  to  $1.4\,\mathrm{V}$ , peak to peak, or negative-going composite sync, about 3.5 V to 7.5 V, can be used. A choice of pin connections on the Sync board permits either amplitude signal to be used.

The Type R520 is normally connected at the factory for use with a  $3.5\,\mathrm{V}$  to  $7.5\,\mathrm{V}$  peak-to-peak negative composite sync external signal. To accomplish this, the black-red-onwhite wire is connected to pin E on the Input Sync board as shown in Fig. 2-7. The Input Sync board is located on the top right rear of the chassis. If a 0.7 V to 1.4 V peak-to-peak negative-going composite video signal is applied to the EXT SYNC connector, the black-red-on-white wire should be connected to pin D.

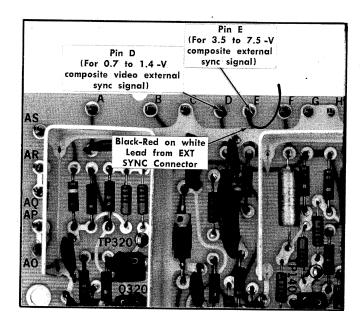


Fig. 2-7. Selecting the external sync pin connection on the Input Sync board. Pin E is the normal connection.

#### NOTE

The SYNC switch should not be placed in the EXT position unless an external sync signal is applied to the EXT SYNC input connectors; otherwise, unstable displays will be obtained. When using the Type R520 to observe non-composite video, a 1-V sync-negative composite video should be applied to EXT SYNC connector, pin E on the Sync board should be used and the SYNC switch should be set to EXT.

Horizontal drive pulses may also be used to synchronize the Vectorscope; however, with this type of synchronization it is not possible to view vertical interval test signals. Also, if the internal Subcarrier Regenerator ( $\phi$  REF switch is set to BURST) is used when horizontal drive pulses are applied to EXT SYNC connector, it will be necessary to readjust the BURST FLAG TIMING control to obtain synchronized operation. This control is located behind the right front-panel door. Then, it will be necessary to readjust the control again when returning to the use of horizontal sync pulses. This is because the leading edge of a horizontal drive pulse occurs some time before the leading edge of the corresponding horizontal sync pulse.

It is important to note that the sweep circuits in the Vectorscope will free run and not be locked if the synchronizing pulses are not present. However, it is possible to present, without synchronizing pulses, a vector display of a chrominance signal only, using an external subcarrier signal.

#### **External Subcarrier Input**

The EXT CW  $\phi$  REF subcarrier input connector accepts an external 3.579545-MHz subcarrier necessary for demodulating the input chrominance signal. The external subcarrier signal must have a peak to peak amplitude of 1.5 V to 2.5 V. This signal is connected to the subcarrier processing circuits of

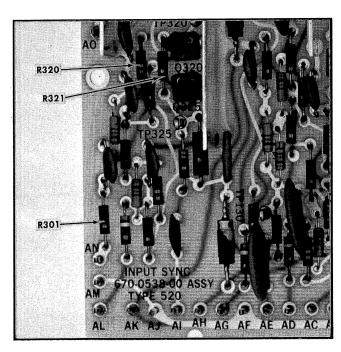


Fig. 2-8. Location of the resistors on the Input Sync board.

the Vectorscope when the  $\phi$  REF switch is set to the EXT position

If the external subcarrier signal is 1 volt peak to peak in amplitude, the instrument can be modified to accommodate this signal by changing the values of R301, R320, and R321. These resistors are located on the Input Sync board (see Fig. 2-8) and the resistance values are given in Table 2-3.

TABLE 2-3

Resistor Circuit		Tektronix Part		
Number	Resistance	Wattage	Tolerance	Number
R301	15 kΩ	1/4	5%	315-0153-00
R320	7.5 kΩ	1/4	5%	315-0752-00
R321	10 kΩ	1/4	5%	315-0103-00

If a subcarrier is not conveniently available, it can be generated within the Vectorscope by placing the  $\phi$  REF switch to the INT position. This switch position applies the color-burst portion of the applied chrominance signal to the internal Subcarrier Regenerator circuit. The Subcarrier Regenerator then generates a 3.579545-MHz signal of the proper phase relationship to burst to be used throughout the Vectorscope in place of the external subcarrier.

## Trace Intensification Input SN B150100 and up.

As shipped from the factory, the Z-axis input lead connects internally from the Z AXIS INPUT connector J1210 on the rear panel to pin BO (see Fig. 2-9) on the Sweep board. This board is located on the bottom side, center-rear portion, of the chassis.

Depending on the intended use of the Type R520, the Z axis input lead may be connected to either pin BO or BQ. Pin BO is the normal connection. The purpose of this connection is intended for use with short-term trace intensific-

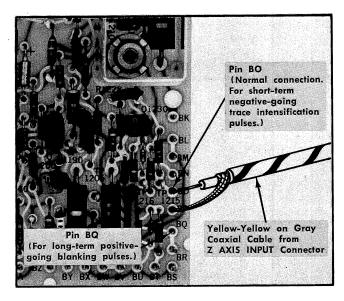


Fig. 2-9. Selecting the Z axis input pin connection on the Sweep board.

#### Operating Instructions—Type 520/R520 NTSC

ation pulses; for example, to identify a television line or a portion thereof. This connection is AC coupled into the grid of the CRT and a negative-going signal of about 5 volts will cause noticeable brightening of the trace. The pulses should not exceed 15 volts in amplitude.

To view several lines, connect the Z-axis input lead to pin BQ. When using this connection, the deflection blanking feature of the CRT is employed rather than the AC-coupled connection to the CRT grid that was previously described. Pin BQ connection requires a positive-going signal of about one volt in amplitude to blank the CRT. This signal should not exceed 5 volts in amplitude. Since this connection is direct coupled, any number of lines can be blanked (or left unblanked). For example, if an appropriate switching signal were available, it would be possible to use this signal to display a selected group of 17 lines while the undesired lines were blanked.

#### Below SNB150100

Circuit operation is the same (as above), except that pin BO is pin AP, and pin BQ is pin AW.

#### FIRST-TIME OPERATION

The following procedure is a suggested method for becoming familiar with the basic operation of the Type R520. In addition, this procedure is a quick check for the front-panel adjustments, including the rear-panel ASTIG and UNBLANK BIAS adjustments. Exception: The BEAM ROTATE adjustment procedure in step 11 will normally be a satisfactory method for general operating use, but a precise method is given in the Calibration Procedure, Section 6, in this manual.

#### NOTE

The GEOM and ORTH adjustments are not included in the First-Time Operation procedure. The Calibration Procedure in Section 6 should be used when performing these adjustments.

Only two signals are required for this procedure; (1) A 75%-amplitude encoded color-bar test signal, and (2) a ten-step linearity test signal. Fig. 2-10 shows the waveforms as photographed using a Waveform Monitor. These particular signals have a 7.5% setup level. The First-Time Operation procedure is as follows:

- 1. Set the INTENSITY control fully counterclockwise.
- 2. Connect a 75%-amplitude encoded color-bar signal to the CH A input connector.

#### NOTE

If the Type R520 is connected to the output of a test-signal distribution system, connect a 75-ohm terminating resistor to the other unused CH A input connector.

- 3. Connect a ten-step linearity test signal to the CH B input connector. If the other CH B input connector is not used, connect a 75-ohm terminating resistor to the unused connector as directed in step 2 NOTE.
- 4. Connect the instrument to a suitable power source and turn on the POWER switch.

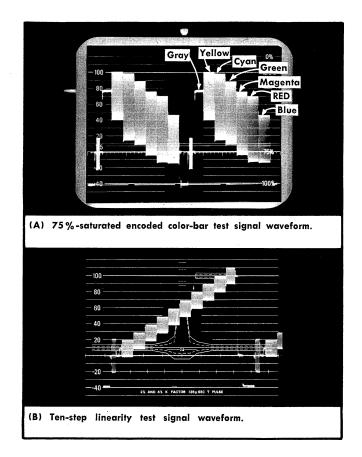


Fig. 2-10. Signals required for performing the First-Time Operation procedure. A waveform monitor was used to obtain the displays.

5. While the instrument is warming up (at least 20 minutes), set the Type R520 front-panel controls to these positions:

me Type K320 mom-paner	controls to mese position
Signal Selector	FULL FIELD $A\phi^3$ (CH A & A CAL: Off) (CH B & B CAL: Off)
Ch A 100%-75%- MAX GAIN	75%
Ch A GAIN	CAL
A PHASE	As is
Ch B 100%-75%- MAX GAIN	75%
Ch B GAIN	CAL
B PHASE	As is
$\phi$ REF	BURST
Display Selector	VECTOR
LUMINANCE GAIN	CAL
CALIBRATED PHASE	0°
SCALE ILLUM	As desired
FOCUS	Fully CCW
FIELD	1
SYNC	INT
VERT POSITION	Midrange
HORIZ POSITION	Midrange

 $^3 \rm Either$  the A $\phi$  or B $\phi$  button can be depressed to make the corresponding A PHASE or B PHASE control operable. In this procedure the A $\phi$  button was arbitrarily used.

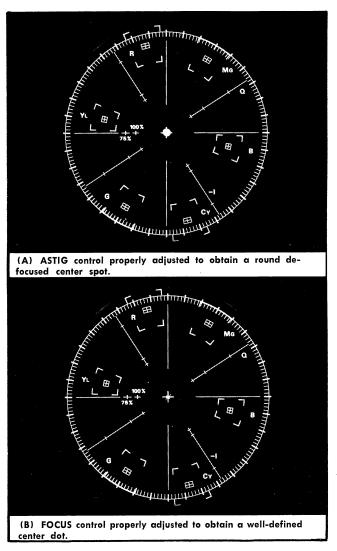


Fig. 2-11. Adjusting the ASTIG and FOCUS controls. Pushbuttons depressed: FULL FIELD,  ${\bf A}\phi$  and VECTOR.

- 6. Rotate the INTENSITY control clockwise until the center dot is the desired brightness. The dot will be out of focus (see Fig. 2-11A) until step 7 has been completed.
- 7. If the center dot does not have a round shape, adjust the rear-panel ASTIG control to obtain a round spot similar to the display shown in Fig. 2-11A. Next, adjust the FOCUS control to obtain a well-defined center dot (see Fig. 2-11B).

#### CAUTION

Avoid using excessive intensity when displaying the focused dot. Excessive intensity (a spot or dot having a bright halo around it) may burn the CRT phosphor.

- 8. Press the CH A and LINE SWEEP buttons. Leave the FULL FIELD and  ${\rm A}\phi$  buttons depressed.
- 9. Rotate the A PHASE control to obtain maximum burst amplitude (see Fig. 2-12A).

#### NOTE

Another method for obtaining maximum burst amplitude is to depress the VECTOR button, set

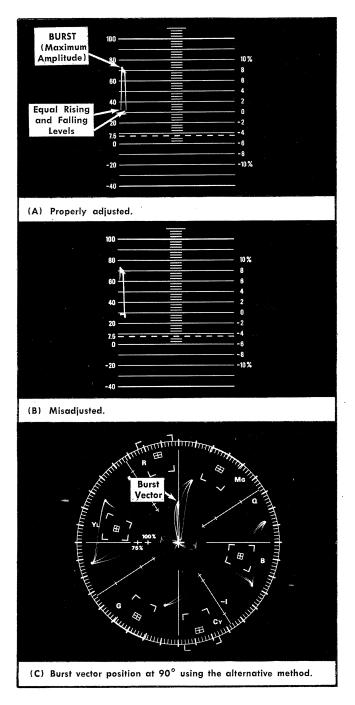


Fig. 2-12. Adjusting the BURST FLAG TIMING control. Pushbuttons pressed for (A) and (B): CH A, FULL FIELD, A $\phi$  and LINE SWEEP; for (C): CH A, FULL FIELD, A $\phi$  and VECTOR.

the A PHASE control so the burst vector coincides with the 90° position (see Fig. 2-12C) or 270° (produces a negative-going burst display in the LINE SWEEP mode). Then, press the LINE SWEEP button and continue with step 9 procedure.

Check that the intensified rising and falling portions of the burst waveform are equal. (Use the INTENSITY control to decrease the brightness of these portions for better viewing contrast.) If the rising and falling portions are not equal, adjust the BURST FLAG TIMING control to obtain the proper display as shown in Fig. 2-12A. Fig. 2-12B shows one effect obtained when the adjustment is incorrect.

- 10. Depress the A CAL button. Leave the FULL FIELD,  $A\phi$  and LINE SWEEP buttons depressed.
- 11. Check that the trace aligns with the 30 IRE unit graticule marking as shown in Fig. 2-13A. If not, adjust the BEAM ROTATE control to obtain proper alignment.

#### NOTE

If the trace is located above or below the 0°-180° vector graticule marking, preadjust the VERT POSITION CLAMP control to position the trace.

12. Depress the Y button. Leave the A CAL and FULL FIELD buttons depressed. Check that the display amplitude is 140 IRE units in the vertical center area of the graticule. Overlook the starting portion of the waveform. Use the VERT POSITION and HORIZ POSITION controls to position the display for best viewing (see Fig. 2-14). To minimize parallax viewing errors, use the pupil of the eye reflected from the —40 IRE unit graticule marking to align the bottom of the waveform with the graticule marking. Next, check the position of the top of the waveform with respect to the (+) 100 IRE graticule marking by reflecting the pupil of the eye from this graticule mark.

If the displayed amplitude is not 140 IRE units within  $\pm 1\%$  (1.4 IRE units), set the A CAL screwdriver adjustment to obtain the correct amplitude.

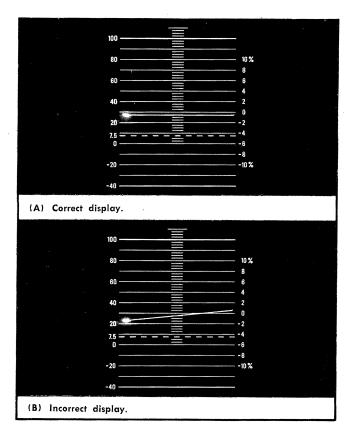


Fig. 2-13. Adjusting the BEAM ROTATE control. Pushbuttons depressed: A CAL, FULL FIELD,  ${\bf A}\phi$  and LINE SWEEP.

Press the B CAL button and cancel the A CAL button. Repeat the procedure for channel B. If necessary, adjust the B CAL screwdriver adjustment to obtain the same 140 IRE unit display amplitude as obtained for channel A.

13. Depress the A CAL and VECTOR buttons. Cancel the B CAL button. Check that the FULL FIELD and  $A\phi$  buttons are depressed. The test circle should match the guide circle inscribed on the vector graticule.

#### NOTE

If the test circle trace is too dim for a portion of its circumference, preset the rear-panel UNBLANK BIAS control as described in step 17 and then continue with step 13 and on.

If the test circle is out-of-round, or if the circles do not overlay properly (within 0.032 inch,  $\frac{1}{3}$  of a 2° phase mark length on the vector graticule), use Table 2-4 to obtain the proper display as shown in Fig. 2-15A. Repeat the adjustments, as necessary, to obtain optimum results. Figs. 2-15B and 2-15C show two examples where the adjustments are set incorrectly.

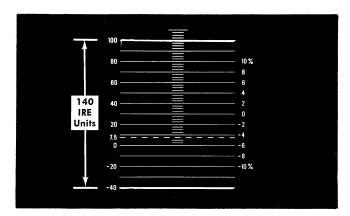


Fig. 2-14. Proper luminance calibrated test signal amplitude. Pushbuttons depressed: A CAL, FULL FIELD,  ${\bf A}\phi$  (not required) and Y.

TABLE 2-4

Adjustments	Effect on Test Circle Display
VERT POSITION CLAMP	Vertical positioning.
HORIZ POSITION CLAMP	Horizontal positioning.
QUAD PHASE	Merges the two ellipses to form a superimposed ellipse or circle.
GAIN BAL	Left and right portions.

After completing the adjustments, the test circles may not overlay perfectly, but they should be within the 0.032-inch radial separation limit. Accurate vector measurements can be made if the effects caused by a slight separation of the test circles are considered. In general, radial trace separation between the test circles is maximum at or near one or more of these points: 45°, 135°, 225° or 315°. The effect of this separation on a vector is as follows:

a. No phase error for a vector positioned at 90° or 270°.

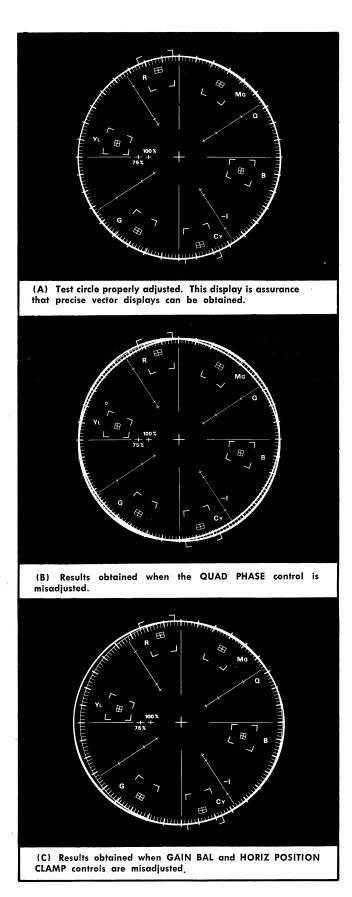


Fig. 2-15. Obtaining a properly adjusted test circle display. Pushbuttons depressed: A CAL, FULL FIELD,  $A\phi$  and VECTOR.

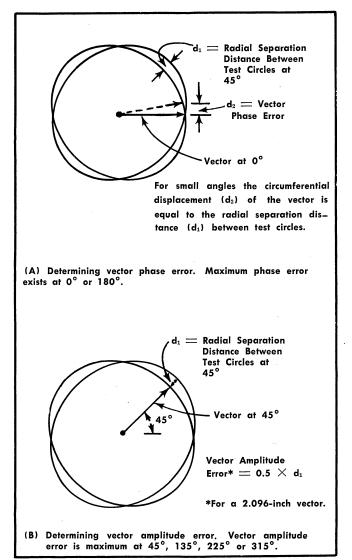


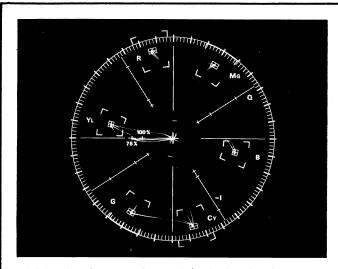
Fig. 2-16. Determining phase and amplitude errors of vectors when the test circles have maximum radial separation at  $45^{\circ}$ ,  $135^{\circ}$ ,  $225^{\circ}$  or  $315^{\circ}$ .

b. For a vector positioned at 0° or 180°, the phase error is equal to the radial separation distance between test circles (see Fig. 2-16A). For example, if the separation is 0.032 inch, the circumferential displacement of the vector is 0.032 inch or slightly less than 1° using this formula:

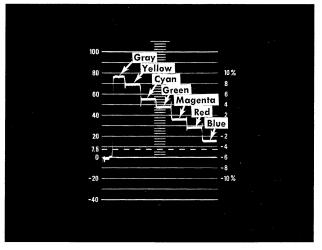
$$\phi = 2$$
 arc  $\sin \frac{d_1}{2p}$ 

where  $\phi$  is the vector phase error in degrees, d<sub>1</sub> is the radial separation between the test circles at 45° and R is the 2.096-inch radius of the inscribed test circle.

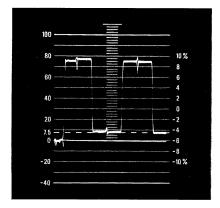
- c. No vector amplitude error for vectors positioned at 0°, 90°, 180° or 270°.
- d. For a vector positioned at 45°, 135°, 225° or 315°, the vector amplitude error for a 2.096-inch vector is 0.5 times the radial separation distance between test circles (see Fig. 2-16B). A 2.096-inch vector is used in the calculation because



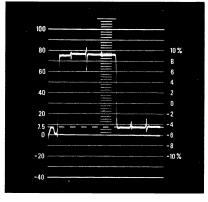
(A) VECTOR button is depressed to display the chrominance portion of the color-bar signal. Position of the dots within the smaller boxes indicate that the displayed color vectors are within  $\pm 2.5^\circ$  and  $\pm 2.5$  IRE units of the assigned hue (in degrees) and saturation (vector amplitude).



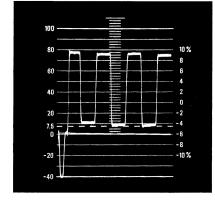
(B) Pushbutton Y is depressed to display the luminance amplitude of the color-bar signal. The vertical deflection is calibrated in IRE units as indicated by the left-hand scale.



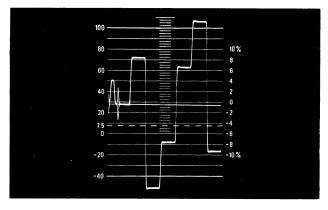
(C) Pushbutton R is depressed to display the red output waveform.



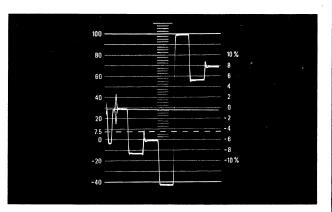
(D) Pushbutton G is depressed to display the green output waveform.



(E) Pushbutton B is depressed to display the blue output waveform.



(F) Pushbutton I is depressed to display the I component of the signal.



(G) Pushbutton  $\mathbf{Q}$  is depressed to display the  $\mathbf{Q}$  component of the signal.

Fig. 2-17 Typical waveforms obtained when displaying the chrominance and luminance portions of a color-bar test signal. Signal Selector pushbuttons depressed: CH A, FULL FIELD and  $A\phi$ . Display Selector pushbuttons depressed: See individual waveforms.

2-16

the radius of the inscribed graticule test circle is this distance. For example, if the separation distance between test circles is 0.032 inch, then 0.5 times 0.032 inch is 0.016 inch. The amplitude error for a 2.096-inch vector is 0.016 inch, or about 0.8% amplitude error for any vector positioned at 45°, 135°, 225° or 315°.

For most distortions in which the test circles overlay properly but deviate slightly from the inscribed circle at some point, the effect on the vector is as follows:

For small angles the circumferential displacement (phase error) of a 2.096-inch vector located about 45° from the point of maximum circle deviation will be equal to the distance between the test circle deviation and the graticule circle. For a 2.096-inch vector pointing toward the circle distortion area, the vector amplitude error is equal to the test circle deviation distance from the graticule circle.

- 14. Press the B CAL button and cancel the A CAL button. Leave the FULL FIELD,  $A\phi$  and VECTOR buttons depressed.
- 15. Check that a proper size (same size as obtained in step 13) test circle is obtained. The test circle should align with the vector graticule guide circle within the limits described in step 13.
- 16. Depress the A CAL button and cancel the B CAL button. Leave the FULL FIELD,  ${\rm A}\phi$  and VECTOR buttons depressed.
- 17. Set the INTENSITY control to obtain a dim circle under low-ambient light conditions. If trace intensity is not uniform, adjust the rear-panel UNBLANK BIAS control to obtain uniform intensity for the full circumference of the circle.
- 18. Reset the INTENSITY control to obtain a normal brightness display.
- 19. Press the CH A button. Leave the FULL FIELD,  $A\phi$  and VECTOR buttons depressed. Adjust the A PHASE control to align burst with the 180° position. The burst tip should coincide with the 75% mark on the vector graticule and all color vectors should appear in their respective inner boxes (see Fig. 2-17A). This indicates that the color-bar signal input is 1 V peak-to-peak, the colors are 75% saturated, burst amplitude is 286 mV peak to peak, and the color-vector phase and amplitude are within  $\pm 2.5$ ° and  $\pm 2.5$  IRE unit tolerance.
- 20. Using Table 2-5 and Figs. 2-17B through 2-17G as a guide, check the displays obtained when Y, R, G, B, I and Q buttons are depressed in the order just given.

TABLE 2-5

Display Selector Pushbutton	Typical Waveform
Υ	Fig. 2-17B
R	Fig. 2-17C
G	Fig. 2-17D
В	Fig. 2-17E
1	Fig. 2-17F
Q	Fig. 2-17G

21. With a staircase signal applied to the CH B input connector, press the following pushbuttons:

Signal Selector CH B
Display Selector Y

Cancel the CH A button. Check that the FULL FIELD and  $A\phi$  buttons are depressed. The waveform should be a staircase signal as shown in Fig. 2-18A.

#### SN B150100 and up

22. Differential Gain Measurements. The Diff Gain scale on the line sweep graticule can be used to make differential gain measurements within an accuracy of 1% if the test signal modulation is preset to a standard amplitude. The procedure that follows describes how to preset a test signal to a standard modulation amplitude before proceeding with the measurement.

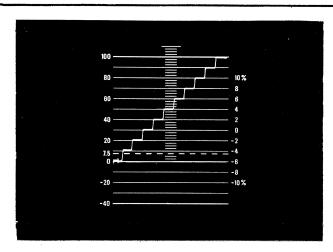
#### NOTE

As a test signal for differential gain measurements, it is possible to use any signal at the subcarrier frequency that retains a constant modulation amplitude (within a 70-mV to 196-mV range) throughout the line or portion being measured while the DC level of the signal varies. No burst or external subcarrier is required. However, the staircase vector display obtained in steps 22e and 22f will be free running and jittering will occur. A ramp with 100-mV peak-to-peak modulation and a staircase with 140-mV peak-to-peak modulation are examples of signals (see Fig. 2-18) that meet the stated test requirements.

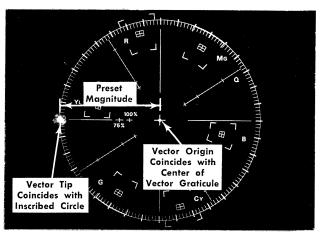
- a. Press the VECTOR button. Check that the CH B, FULL FIELD and  $A\phi$  buttons are depressed. Check that the Ch B 100%-75%-MAX GAIN switch is set to 75%.
- b. Use the A PHASE control to align the staircase vector at 0° or 180°. If burst is present disregard it in making this measuremnt.
- c. Set the Ch B 100%-75%-MAX GAIN switch to MAX GAIN. Check that the origin of the staircase vector coincides with the vector graticule center (see Fig. 2-18B). If it does not, adjust the VERT POSITION CLAMP and HORIZ POSI-3 TION CLAMP controls to center the vector origin.
- d. Check that the tip of the staircase vector (not the burst vector) coincides with the vector graticule inscribed circle. If it does not, adjust the CH B GAIN control for proper vector tip and inscribed circle coincidence (see Fig. 2-18B). Readjust, if necessary, the A PHASE control to position the staircase vector at 0° or 180°.

Up to this point in the procedure, the staircase vector has been preset to a standard magnitude for use in making the differential gain measurements that follow. In addition, the staircase vector has proper phase for performing the differential phase measurement.

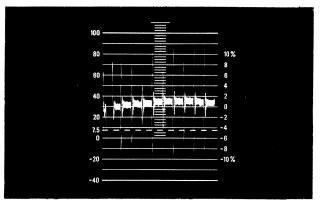
- e. Press the DIFF GAIN button. Check that the CH B, FULL FIELD and  $A\phi$  buttons are depressed and the Ch B 100%-75%-MAX GAIN switch is set to MAX GAIN.
- f. Adjust, if necessary, the VERT POSITION control to position the first step to the 0% Diff Gain graticule line as a reference. If there is no differential gain, all the stairstep



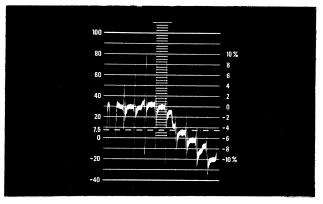
(A) 10–step linearity test signal. Buttons depressed: CH B, FULL FIELD,  ${\bf A}\phi$  and Y.



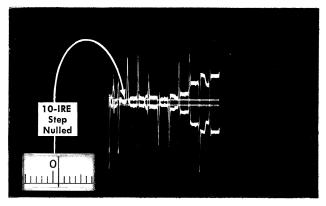
(B) Presetting the staircase vector to a standard magnitude before performing the differential gain measurement. Buttons depressed: CH B, FULL FIELD,  $\mathbf{A}\phi$  and VECTOR.



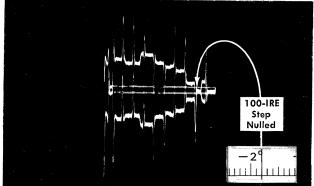
(C) Typical display obtained when test signal is linear within 1 %. If no distortion were present, the staircase segments would form a straight horizontal line. Buttons depressed: CH B, FULL FIELD,  ${\bf A}\phi$  and DIFF GAIN.



(D) Waveform illustrating presence of severe differential gain. The tenth stairstep shows a 10% loss in signal amplitude. Buttons depressed: Same as (B).



(E) Initial CALIBRATED PHASE dial setting when measuring differential phase. Buttons depressed: CH B, FULL FIELD,  ${\bf A}\phi$  and DIFF PHASE.



(F) Final CALIBRATED PHASE dial setting when measuring differential phase between the 10-IRE and 100-IRE steps on the waveform. Buttons depressed: Same as (E).

Fig. 2-18. Typical waveforms obtained when displaying a ten-step linearity test signal. Waveforms (B) through (F) were obtained with the CH B 100%-75%-MAX GAIN switch set to MAX GAIN.

2-18

segments will coincide with the 0% Diff Gain graticule line (see Fig. 2-18C). If a stairstep does not coincide with the 0% graticule line (for an example, see Fig. 2-18D), differential gain is present.

Table 2-6 is a conversion chart to equate the Diff Gain scale to percent of signal gain or loss, voltage ratio and dB. Using Fig. 2-18D display as an example, the sixth step has a signal loss of 2%, a voltage ratio of 0.98 and is 0.176 dB down.

#### **BELOW SN B150100**

Follow the above procedure, except for step d. The input signal must be 143 mV in amplitude in order to read differential gain in % directly from the graticule and TABLE 2-5. If the input signal is less than or greater than 143 mV, the readings obtained from the external graticule scale will decrease or increase by a direct ratio; for example, if the input signal is 157.3 mV (an increase of 10%), the readings from the graticule scale will increase by 10% and TABLE 2-6 will need revision.

#### TABLE 2-6

#### Differential Gain Conversion Chart

(Based on a staircase vector magnitude equal to the radius of the vector graticule inscribed circle as shown in Fig. 2-18B).

Line Sweep Graticule	100%-75%-MAX GAIN Switch Set to MAX GAIN			
Diff Gain Scale	% of Signal Gain or Loss	Voltage Ratio	dB	
10%	+10%	1.10	+0.828	
. 8	+8%	1.08	+0.668	
6	+6%	1.06	+0.506	
4	+4%	1.04	+0.341	
2	+2%	1.02	+0.172	
0	0%	1.00	+0.000	
2	-2%	0.98	<b>—0.176</b>	
<u>-4</u>	-4%	0.96	0.354	
<u>6</u>	<b>6%</b>	0.94	0.538	
8	<b>_8%</b>	0.92	0.724	
<b>—10%</b>	<b>—10%</b>	0.90	<u> </u>	

23. Differential Phase Measurements. Press the DIFF PHASE button. Check that the Ch B, FULL FIELD and  $A\phi$  buttons are depressed. Check that the Ch B 100%-75%-MAX GAIN switch is set to MAX GAIN, and the Ch B GAIN control is set to CAL.

a. Check that the CALIBRATED PHASE is set to "." Use the A PHASE control as a coarse adjustment to "ull the first step on the display (see Fig. 2-18).

#### NOTE

As an alternative method froughly nulling the first step in the display, control to position the ton and use the A PHO° or 0°. After properly staircase vector at case vector, press the DIFF positioning the staircase vector, press the DIFF PHASE button or

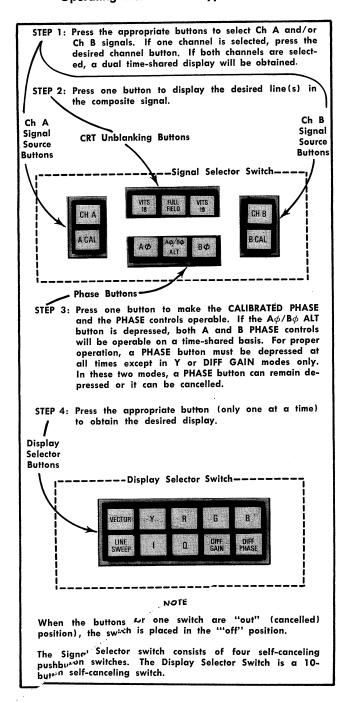


Fig. 2-19. Grouping of the pushbuttons for each switch. One button for each group, with exceptions as given in Steps 1 and 3, should be depressed to obtain a useful display.

b. Use the CALIBRATED PHASE control as a vernier adjustment for nulling the first step. Note the dial reading. For example, in Fig. 2-18E the dial reading is  $-0.1^{\circ}$ .

c. Set the CALIBRATED PHASE control so the last step is at null. Note the dial reading. Fig. 2-18F indicates a dial reading of  $-2.2^{\circ}$ .

d. Subtract the dial difference readings noted in steps 23b and 23c. The result should be the amount of differential

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phase between the first and last step in the 10-step linearity test signal. Using Figs. 2-18E and 2-18F as an example: —0.1° subtracted from —2.2° equals 2.1° differential phase. Since total differential phase is the point of interest, the algebraic sign of the resultant may be omitted.

#### NOTE

Using step 23 as a guide, differential phase between any two steps on the waveform can be measured if desired. Best accuracy is obtained when the CALIBRATED PHASE control is turned in one direction (without reversing direction) when nulling between steps on the waveform. Turning the dial in one direction eliminates any possible backlash as a source of error.

#### GENERAL OPERATING INFORMATION

#### **Pushbutton Switches**

The Signal Selector switch consists of four self-canceling switches arranged as shown in the upper part of Fig. 2-19. The Display Selector switch is a 10-button self-canceling switch as shown in the lower part of Fig. 2-19. For proper instrument operation and to produce useful displays, follow the procedure given in the illustration

#### NOTE

To cause a depressed button in any self-canceling switch button group to cancel so all buttons in that group are "out", apply slight finger pressure at a point on an "out" button that permits the finger to extend over the "in" (depressed) button. Let the "in" button release outward until it touches the finger. Then remove the finger so both buttons can spring to their "out" (canceled) positions. When all buttons for one group are "out", the self-canceling switch is in the "Off" position.

The First-Time Operation procedure provides one way to become familiar with the operation of the pushbuttons. Another source of information is the Pushbutton Logic topic provided in the Performing The Measurements portion of this Operating linstructions section.

#### **Internal Triggering Source**

Table 2-7 lists the internal triggering source for each possible combination of the CH A, A CAL, CH B and B CAL pushbutton positions. Use this information to check that a signal is applied to the proper rear-panel connector for the pushbutton combination to be used. This assures that optimum display stability will be obtained when operating the instrument. To obtain a stable dual-channel display (CH A and CH B), CH B input signal must be synchronous with CH A input signal, since the CH B display is triggered from the CH A input.

Note that for the A CAL/B CAL dual-display mode of operation, no signal to the CH A or CH B connectors is required, When A CAL, B CAL and VECTOR buttons are depressed,

the internal calibration signal originates from the 3.59-MHz Test Circle Oscillator located on the Input Amplifier board. (In the absence of a video sync source during the VECTOR mode of operation with the A CAL and/or B CAL buttons depressed, it may be necessary to adjust the BURST FLAG TIMING control to obtain a stable test circle display.)

When A CAL, B CAL and any Display Selector switch button except VECTOR is depressed, the internal calibration signal originates from the collector of Q570 located on the Demodulator board. Repetition rate of this sync signal is H/4.

#### **Opening the Access Doors**

The right door opens at the right side and can be slid into a slot located at the left side of the recessed area. The left door opens at the left side and can be slid into a slot located at the right side of the recessed area.

TABLE 2-7

Pushbutton Channel A	Combination Channel B	Internal	For Optimum Display	
		Sync Source	Stability	
CH A	Off		Apply signal	
CH A	СН В		to CH A In-	
CH A	B CAL	Channel A	put connec-	
Off	B CAL		tor.	
A CAL	Off		Apply signal	
A CAL	СН В	Change I D	to CH B in-	
Off	СН В	Channel B	put connec-	
Off	Off		tor.	
A CAL	B CAL	None required	No input sig- nal required.	

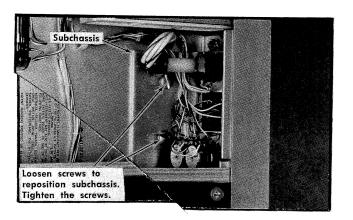


Fig. 2-20. Bottom right-front portion or location of the subchassis mounting screwige Type R520 showing

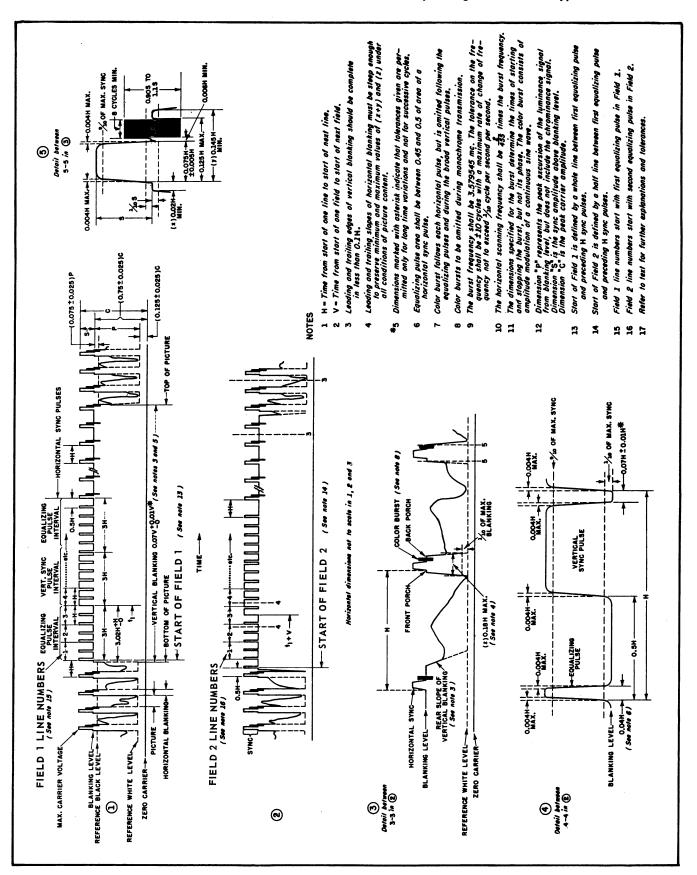


Fig. 2-21. Details of a television synchronizing waveform for color transmission. Similar to the illustration shown on page 265 of the FCC Rules and Regulations, Volume III, March 1968 edition.

#### Positioning the Right Recessed Control Subchassis

The FOCUS, BURST FLAG TIMING, VERT POSITION and HORIZ POSITION recessed controls are mounted on an adjustable position subchassis (see Fig. 2-20). The subchassis has slotted mounting holes to adjust the protrusion distance of these controls. With the subchassis positioned to its maximum inward position, the control knobs will protrude 1/8 inch or less from the recessed front panel. This position permits full closure of the right door. With the door opened, the controls can be adjusted by placing a screwdriver in the arrowed slot to turn the knob. The arrowed slot is a simple indicator for the relative rotational position of the knob.

If the subchassis is positioned to its maximum outward position, the knobs will protrude about 1/2 inch or more from the recessed front panel. This subchassis position enables the knobs to be easily turned by hand, so a screw-driver is not needed. If the subchassis is mounted in this position, the protruding control knobs will prevent the right door from closing; hence, the door should be left open and out of the way by sliding the door fully into its slot.

#### **Graticule Illumination**

When the VECTOR button is depressed, the SCALE ILLUM control varies the illumination of the vector graticule. When any Display Selector button except VECTOR and DIFF PHASE buttons are depressed, the SCALE ILLUM control varies the illumination of the IRE graticule. No graticule illumination occurs when the DIFF PHASE button is depressed.

#### **Burst Brightening**

Trace intensification occurs during the first 3 microseconds of the linear sweep, when the burst amplifier is keyed on and the CRT trace is brightened. This intensified portion provides positive identification of the burst signal. Burst brightening takes place in the LINE SWEEP mode only.

#### **Vector Displays**

The VECTOR presentation is a graphic display for operational measurements with color bars, modulated staircase waveform of the VITS, or other industry test signals. Carrier balance corrections can be made while on the air because the VECTOR display shows direction and magnitude of the required adjustments.

With a VECTOR display, phase measurements can be made within 1° and saturation measurements, within  $\pm 1\%$  on the graticule, and even closer when comparing two signals in dual-channel operation.

The internally generated test circle matched with the graticule circle verifies the accuracy of the VECTOR display.

#### **Linear Sweep Displays**

The color signals can be demodulated along any desired axis, I, Q, R-Y, B-Y, G-Y, etc. and displayed at the line rate on a linear time base. The various linear time base display modes permit a variety of useful operational tests and measurements to be made. This is accomplished by selecting the appropriate Display Selector modes: I, Q, R, B, G, DIFF GAIN, DIFF PHASE.

Calibrated phase shift using the trace overlay technique permits a slide-back type of phase measurement with a resolution of at least 0.1°.

#### **Dual Displays**

In dual-channel operation, successive samples of each channel are displayed on a time-shared basis. For example, the input signal to some location in the broadcast plant can be compared to the output signal to measure any phase and/or amplitude distortion caused at that location. Also, the outputs of any two areas of the broadcast plant can be compared. Video cable lengths can be accurately matched for time delay at color subcarrier frequency to less than 1° phase difference.

Using the VECTOR display, either channel can be turned off to provide a zero reference point for the other channel. The reference point is a sharply defined spot in the center of the display.

Using the linear-sweep displays, turning off one channel while the other remains in use provides a zero reference line against which signals can be nulled.

When using dual-channel operation and internal triggering, refer to Table 2-7 in this section of the manual. This table lists the internal triggering source for each pushbutton combination.

#### **Vertical Interval Testing**

The binary counters in the Type R520 Line Selector Matrix operate in conjunction with the Field Selector circuit to select lines in either field that may carry suitable test signals. These circuits enable the Vectorscope to be used for measuring differential gain and differential phase during color broadcasts on the test signals which may be transmitted during the vertical blanking interval. The topics, "VITS Line Selection" and "VITS Field Selection", that follow describe how to select any NTSC line from 7 through 22 in the same field or in opposite fields. BELOW SN B150100: Lines selected are from 7 through 21.

To aid in the identification of fields and lines, a television synchronizing waveform illustration is shown in Fig. 2-21 to accompany the following definitions:

- a. FIELD 1: The start of Field 1 is defined by a whole H line between the first equalizing pulse and the preceding H sync pulse.
- b. FIELD 2: The start of Field 2 is defined by a **half H line** between the first equalizing pulse and the preceding H sync pulse.
- c. Line numbering for Field 1: Field 1 line numbers start with the **first equalizing pulse** in Field 1.
- d. Line Numbering for Field 2: Field 2 line numbers start with the **second equalizing pulse** in Field 2.

#### VITS Line Selection

#### SN B150100 and up

The Type 520 is normally connected at the factory to permit selection of lines 18 and 19 in either television field by means of the VITS 18 and VITS 19 pushbuttons in conjunction with

the FIELD switch. Quick-disconnect jumper wires are used on the Sweep board to preselect the lines so that, if desired, any pair of NTSC lines (from 7 through 22) or the same lines in each field can be preselected. Intensity and focus are automatically adjusted for optimum viewing of VITS; that is, the front-panel INTENSITY and FOCUS controls do not need to be readjusted when switching from FULL FIELD to VITS 18 or VITS 19.

To preselect a pair of lines in a television field, use TABLE 2-8 and Fig. 2-22A as a guide for the VITS 18 pushbutton. Use TABLE 2-9 and Fig. 2-22A as a guide for the VITS 19 pushbutton. The connectors with jumpers are located on the Sweep board. The Sweep board is located on the bottom center-rear of the chassis. Five jumpers for each VITS pushbutton control the selection of lines.

#### NOTE

Whenever the jumper wires are connected to select lines other than 18 and 19, be sure to change the number on the button to match the new line number. Button numbers can be changed by covering the old number with a new number.

#### **BELOW SN B150100**

Line preselection is made by placement of jumpers between various pins located on the Sweep board. Any pair of lines (or the same lines) within a group of lines can be made selectable by the VITS 18 and VITS 19 pushbuttons. There are two groups of lines for preselection: Group 1 (lines 7 through 14) and Group 2 (lines 15 through 21).

To preselect a pair of lines within Group 1 (lines 7 through 14), in a television field, use Table 2-10 and Fig. 2-22B as a guide. To preselect a pair of lines within Group 2 (lines 15

**TABLE 2-8** 

SN B150100 and up
Line Preselection For VITS 18 Pushbutton

Lines to	to Jumper Wire Pin Connections						
be pre-	Pin	Pin	Pin	Pin	Pin		
selected	AA to	S to	M to	G to	A to		
7	AC	U					
8	AB	U	0				
9	AC	T					
10	AB	1		1			
11	AC	U		1			
12	AB		N				
13	AC	Т					
14	AB	1			С		
15	AC	U			C		
16	AB		0				
17	AC	Т					
18	AB	1					
19	AC	U	11		Н Н	п	
20	AB	U	N				
21	AC	Т	'*				
22	AB	•					

## TABLE 2-9 SN B150100 and up Line Preselection For VITS 19 Pushbutton

Lines to	Jum	per Wire	e Pin Co	nnection	ıs
be Pre-	Pin	Pin	Pin	Pin	Pin
selected	AG to	W to	Q to	K to	E to
7	AH	V			
8	AF	X	В		
9	AH	R	٧		
10	AF	<b>V</b>		L	F
11	AH				
12	AF	X	P		
13	AH	V	r		
14	AF	<b>'</b>			
15	AH	х			
16	AF	^	R		
17	AH	٧	N.		
18	AF	<b>Y</b>		J	
19	AH	Х		J	
20	AF	^	P		
21	AH	V			
22	AF	<b>'</b>			

## **TABLE 2-10**Below SN B150100

### Preselecting VITS Pushbutton Lines 7 through 14 (Group 1)

Push- buttons	Lines to be Prese- lected	Jum	per Wire	e Pin Co	onnections	
	7	U to T	O to N		- BM to C	
	8	U to V	0 10 14	I to H		
	9	U to T	O to P	1 10 11		
VITS 18	10	U to V	0 10 1			
VII 3 10	11	U to T	O to N			
	12	U to V	0/10/14	l to J		
	13	U to T	O to P	1 10 3		п .
	14	U to V	0 10 1			BO to
	7	R to S	L to M			BN
	8	R to Q	L IO M	F to G		
	9	R to S	L to K	1 10 0		
VITS 19	10	R to Q	LIOK		BL to B	
VII3 17	13 17 11	R to S	1 to 1/4		DL 10 B	
	12	R to Q	L to M	F to E		
	13	R to S	L to K	1 10 E		
	14	R to Q	LIOK			

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through 21), use Table 2-11 and Fig. 2-22B as a guide. The connector pins with jumpers are located on the bottom side, center-rear portion, of the chassis. Three of the jumpers control the selection of a group of lines, and three jumpers for each VITS push-button control the selection of lines within a group.

In general, it is not possible to use one VITS pushbutton to select a line in Group 1 and the other VITS pushbutton to select a line in Group 2. However, some overlap from Group 1 into the first few lines of Group 2 is possible. The amount of overlap depends on circuit tolerances and may vary from instrument to instrument. Usually it is possible to extend two or three lines from Group 1 into Group 2 by means of the BO and BN jumper connection. For example, to preselect line 10 with the VITS 18 button and line 16 with the VITS 19 button, refer to Table 2-12.

**TABLE 2-11**Below SN B150100

Preselecting VITS Pushbutton Lines 15 Through 21 (Group 2)

Push- buttons	Lines to be Prese- lected	Jum	per Wire	e Pin Co	onnections	
VITS 18	15	U to T	O to N	I to H	BM to D	BO to BP
	16	U to V				
	1 <i>7</i>	U to T	O to P			
	185	U to V				
	19	U to T	O to N	l to J		
	20	U to V				
	21	U to T	O to P			
VITS 19	15	R to S	L to M	F to G	BL to A	
	16	R to Q				
	17	R to S	L to K			
	18	R to Q				
	195	R to S	L to M L to K	F to E		
	20	R to Q				
	21	R to S				

 $^{5}\mathrm{Fig.}$  2-22B illustrates the connections for preselecting these lines (18 and 19).

**TABLE 2-12**Below SN B150100

Push- buttons	Lines to be Prese- lected	Jum	per Wire	e Pin Co	onnections	
VITS 18 VITS 19	10 16				BM to C	BO to BN

Note that for the example given in Table 2-12, the BO to BN connection keeps both buttons in Group 1. Then by connecting the VITS 19 group selector jumper wire between pins BL and A(see Table 2-11), the VITS 19 button can be set to

preselect one of the first few lines in Group 2. In the example just given, line 16 was preselected.

#### VITS Field Selection

As mentioned previously, the Type R520 is normally connected at the factory to permit selection of lines 18 and 19 in either field by means of the VITS 18 and VITS 19 push-buttons in conjunction with the FIELD switch. For example, if the FIELD switch is set to 2, line 18 or 19 in field 2 can be selected by depressing the VITS 18 or VITS 19 button, respectively.

Suppose, however, that the color test signals are being transmitted on line 19 in field 1 and on the same line (19) in field 2. Suppose further that the operator desires to select these signals by means of the VITS pushbuttons only (without opening the right-hand door to move the FIELD switch when selecting the pushbutton positions). This can be accomplished by first using Table 2-9 to change the VITS 18 button to select line 19. Next, leave the FIELD switch in the 2 position and preselect field one for the left-hand pushbutton by moving the VITS 18 field selector jumper to the proper connections (AK to AL) using the information provided in Table 2-13 and illustrated in Fig. 2-23. Note that the pushbutton field-selector jumper connections are located conveniently near the line-selector jumper connections.

TABLE 2-13
SN B150100 and up
Field Preselection For VITS Pushbuttons

Push- button	FIELD Switch Position	Field to be Preselected	Jumper Wire Pin Connections
	1	1	AK to AM
	2	2	(Normal connection)
VITS 18	1	2	AK to AL <sup>6</sup>
	2	1	
	1	1	AO to AN
VITS 19	2	2	(Normal connection)
	1	2	AO to AP6
	2	1	_

<sup>&</sup>lt;sup>6</sup>Note that these connections reverse the FIELD switch positions.

TABLE 2-14
Below SN B150100
Field Preselection For VITS Pushbuttons

Push- button	FIELD Switch Position	Field to be Preselected	Jumper Wire Pin Connections	
VITS 18	1	1	AA to Z	
	2	2	(Normal connection)	
	2	1	AA to AB <sup>7</sup>	
	1	2	AA 10 AB	
VITS 19	1	1	X to Y	
	2	2	(Normal connection)	
	2	1	X to W <sup>7</sup>	
	1	2	X 10 VV	

<sup>&</sup>lt;sup>7</sup>Note that these connections reverse the FIELD switch positions.

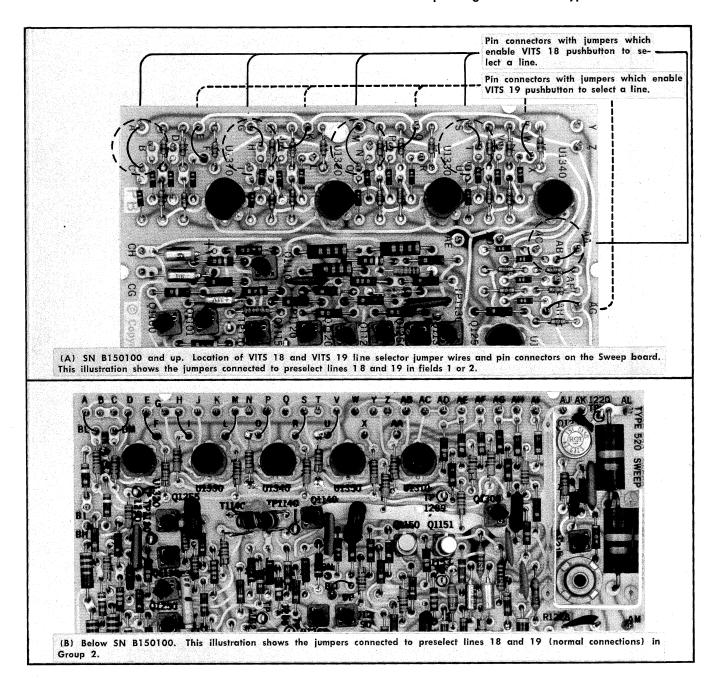


Fig. 2-22. Location of the line selector jumper wires on the Sweep board. These illustrations are examples to show how to preselect a pair of lines using the information given in Tables 2-8 and 2-9 (SN B150100 and up) or Tables 2-10 and 2-11 (below SN B150100).

#### NOTE

When preselecting VITS pushbutton lines and fields, be sure to indicate these changes on the front panel of the instrument for your information and to notify other operators. Using the latter example (line 19 in both fields); the left-hand button nomenclature should read: VITS 19, FIELD 1 and the FIELD switch nomenclature for the 2 position should read: LEAVE AT 2. The right-hand button should read: VITS 19, FIELD 2.

#### PERFORMING THE MEASUREMENTS

#### **Pushbutton Logic**

In Section 11 of this manual there is a table printed on three pullout pages entitled, "Operating Displays". This table provides a concise list of pushbutton combinations for check or measurement to be performed. Space at the end of the table has been provided for adding new data if desired. Note that for a single channel operation in this table, the signal is applied to the CH A input connector. Internal sync and burst signals are used. These assumed conditions simplify the table and setup procedure. In actual practice, either CH A or

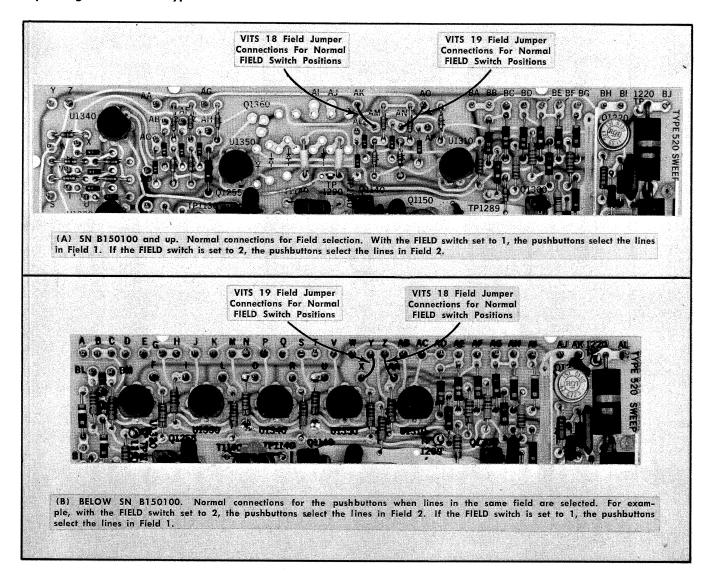


Fig. 2-23. Location of the field-selection jumper wires on the Sweep board. Note that the jumpers can be connected so the buttons select lines in the same field or opposite fields while the FIELD switch remains at a predetermined position.

CH B input connectors can be used. In addition, external sync and burst signals can be used if desired. The only requirement is that the pushbutton switches and controls associated with the channel to be displayed are set properly. If external sync and burst signals are applied to the Type R520, then the SYNC and  $\phi$  REF switches should be set to the EXT positions when the INT option is not desired.

#### Color Encoder

All necessary adjustments to the encoder can be made with the Type R520. Using the VECTOR mode, the I matrix may be checked for accuracy by turning off the Q channel and observing that all six dots align with the cross marks along the I axis of the vector graticule.

Check that the Type R520 100%-75%-MAX GAIN switch is set to 75% and the GAIN control for the channel is set to CAL. Set the I chroma gain on the encoder so that the largest amplitude (red and cyan) dots align with the I-axis

cross marks. All the other dots should align, too.

Some typical causes of I-axis dot misalignment may be due to incorrect matrixing from the R, G and B signals to the I signal, matrix resistor value changes, incorrect gain of an inverting amplifier associated with the matrix function, nonlinear amplification of the matrixed signals, or nonlinear amplification of the doubly-balanced I modulators.

The remarks given for the I channel apply equally to the Q channel.

Having established independently the correct operation of the I or Q channel, with the other channel temporarily disabled, the quadrature phasing between the I and Q channels is facilitated as follows:

- 1. Turn on both channels in the encoder.
- 2. Adjust the encoder quadrature phasing and the Type R520 A PHASE (or B PHASE) control so that all color dots lie within their respective inner boxes on the vector graticule.

- Burst phasing of the encoder may then be adjusted so that the burst vector is at exactly 180° on the vector graticule.
- 4. The amplitude of the burst vector may be set on the encoder.
- The luminance levels in the encoder can now be set to their correct amplitudes using the Y (luminance) mode of operation.

#### **Color Saturation**

The saturation of the displayed colors can be checked by using the 75% and 100% burst amplitude markings on the vector graticule and by noting the position of the 100%-75%-MAX GAIN switch. The general procedure for making this check is as follows:

- 1. While obtaining a normal VECTOR display, check that the GAIN control for the channel is set to CAL.
- 2. Set the 100%-75%-MAX GAIN switch to a position that causes the displayed color vectors to appear within the target areas. Note the location of the burst tip along the 180° axis on the vector graticule and the position of the 100%-75%-MAX GAIN switch. If both the burst tip location and the switch position indicate 75%, the colors are 75% saturated. If the burst tip location and the switch position indicate 100%, the colors are 100% saturated.

#### **Differential Gain**

In general, any differential gain present in the signal can be checked by using the DIFF GAIN mode of operation and by setting the 100%-75%-MAX GAIN switch to MAX GAIN. With a standard 10-step linearity staircase signal applied to the Type R520, any differential gain present will cause a variation in the segment levels as described in step 22 of the First-Time Operation procedure and illustrated in Fig. 2-18D.

The IRE graticule major divisions represent % of signal gain or loss when the displayed 100 IRE level coincides with the 0% graticule lines. Using the right-hand graticule marking for the scale in conjunction with the major and minor graticule markings, differential gain measurements can be made within an accuracy of 1%.

If the 10-step linearity staircase signal is transmitted as a VITS signal, the Type R520 can be used to monitor this test signal and perform differential gain measurements while the test signal is being broadcast with the regular program material. The VITS buttons can be set to preselect any line between 7 and 22 in either field as described in VITS Line Selection and VITS Field Selection topics presented previously in this section of the manual. BELOW SN B150100: lines that can be preselected are from 7 through 21.

#### NOTE

Any signal at the subcarrier frequency that retains constant amplitude throughout the line or portion being measured while the DC level of the signal varies can be used as a test signal for differential gain measurements.

#### **Differential Phase**

Any differential phase present can be detected by noting the dial settings of the CALIBRATED PHASE control when using the slideback method for overlaying two traces in DIFF PHASE mode of operation. As described previously in step 23 of the First-Time Operation procedure, no phase distortion is present if the traces are parallel.

If phase distortion is present, the phase demodulated lines of both traces will not be parallel; that is, the traces are farther apart at certain points as distortion increases, as shown in Figs. 2-18E and 2-18F. The two magnified presentations show the 10 IRE step nulled as compared to the 100 IRE step nulled. The difference in CALIBRATED PHASE dial settings required to null these two is the difference in phase which, in this instance, is 2.1°.

Using the standard linearity test signal, a differential phase error of 0.2° can be measured. The CALIBRATED PHASE dial provides excellent resolution since 1° of phase shift is represented by approximately one inch of dial tape movement.

#### NOTE

Any signal at the subcarrier frequency that retains constant phase throughout the line or portion being measured while the DC level of the signal varies can be used as a test signal for differential phase measurements.

#### Phase vs Time Delay

Time delay between two signals can be checked, because the phase difference at any particular frequency can be related to time difference. An example of this is the setup of two color cameras some distance apart. With the outputs of the cameras connected to the inputs on the Vectorscope, and the following pushbuttons depressed: CH A, CH B, FULL FIELD,  $A\phi$  and VECTOR, the two signals can be viewed together on a time-shared basis. Any time-delay difference between the two camera links will appear as a phase difference in the vectorial display.

This time-delay difference can be determined by noting that 360° on the graticule equals 280 nanoseconds of time. The difference can be minimized by adjusting the connecting cable lengths so that there will be no hue or phase difference from one camera to the other.

#### **OBTAINING WAVEFORM PHOTOGRAPHS**

Fig. 2-24 shows the Tektronix C27 camera setup that was used when photographing the vector displays and waveform for this manual. Polaroid<sup>8</sup> Land film pack Type 107 with an ASA rating of 3000 was used in the camera. Similar results can be obtained if roll film Type 47 with an ASA rating of 3000 is used in a Polaroid Land  $3\frac{1}{4} \times 4\frac{1}{4}$  Roll-Film Back Part No. 122-0603-00. If a Roll-Film Back is used, the part number for the focusing plate that should be used in steps 9 through 14 is 387-0460-00.

Fig. 2-25A shows the size of the image with respect to the recording area when the F1.9—1:0.5 lens is used. If a larger size image area is desired as shown in Fig. 2-25B, use a F1.9—1:0.7 lens (122-0547-00). However, this lens should be used with a pack-film back to obtain consistent alignment of the image within the recording area.

<sup>&</sup>lt;sup>8</sup>Registered Trade Mark, Polaroid Corporation.

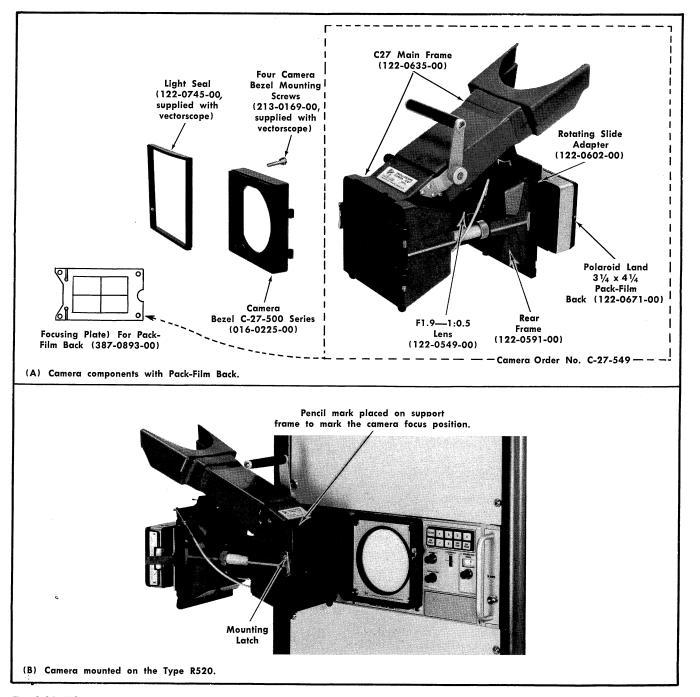


Fig. 2-24. Tektronix C27 camera setup used in obtaining the waveform photographs for the Instruction Manual. If a larger size image (see Fig. 2-25B) on the recording area is desired, use a 1.9-1:0.7 lens (122-0547-00).

Camera types other than those made by Tektronix, Inc. can be adapted to fit the Type R520 if the proper bezel is used. Contact your local Field Engineer or Field Office for more information about the availablity of other bezels.

To obtain the photographs for this section (Operating Instructions, Section 2) of the manual, the camera was set as follows: Shutter speed, 1/5 second; aperature selector, F5.6.

The following procedure is suggested for mounting the camera on the instrument and obtaining the pictures.

- 1. Remove the graticule cover with accompanying parts by removing four graticule thumb screws (see Fig. 2-26A). BELOW SN B150100. Loosen the graticule cover by pulling outward on the rim near the lower left-hand corner. Hold the unsnapped corner with one hand and use the other hand to pull outward on the opposite rim near the upper right-hand corner. Carefully remove the graticule cover with all accompanying parts.
- 2. Remove the light seal from the camera bezel and install the one supplied with the Type R520. Save the removed light seal, if desired.

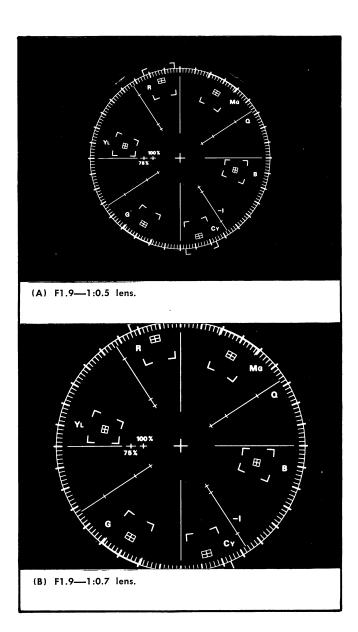


Fig. 2-25. Comparing the image size with respect to the recording area when using different object-to-image ratio lenses.

3. Place the IRE graticule, paper light shield and light guide (see Fig. 2-26B) in the camera bezel.

### NOTE

To obtain the highest quality vector waveform pictures for use in this section of the manual, the IRE graticule was removed. If utmost clarity is not important, good vector pictures can be obtained without removing the IRE graticule. In addition, the IRE graticule provides protection against marring the plastic face plate bonded to the face of the CRT.

4. Mount the camera bezel together with the graticule parts on the front of the Vectorscope CRT. Use the four thumb screws supplied with the Type R520. (The bezel moun-

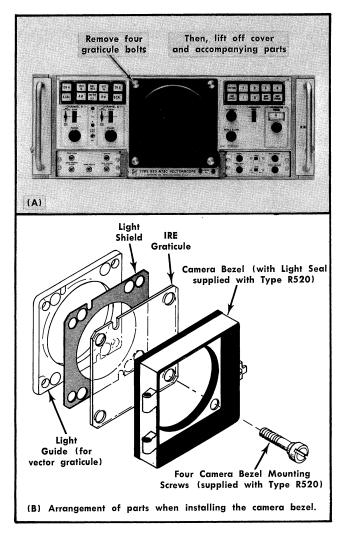


Fig. 2-26. Removing the graticule cover and installing the camera bezel.

ting nuts furnished with the camera are not used with the Type R520, but they can be used when mounting the bezel on oscilloscopes having the appropriate mounting studs.

- 5. Apply a color signal to the Vectorscope and set the controls to obtain a normal vector display.
- 6. Adjust the FOCUS and INTENSITY controls for well-defined vector dots with less than normal brightness. Set the SCALE ILLUM control to illuminate the vector graticule.
- 7. Attach the camera to the bezel hinge and secure the camera against the Vectorscope with the Mounting Latch (see Fig. 2-24B).
- 8. Open the camera back and install the focusing plate with frosted side towards the camera lens.
- 9. Set the camera Aperture selector to F1.9 and place the shutter Speed selector at "T". Press the Shutter Release control to open the shutter.
- 10. Carefully focus the camera on the vector display and illuminated vector graticule markings. Use low ambient light

# Operating Instructions—Type 520/R520 NTSC

conditions to facilitate accurate focusing. Place a pencil mark on the camera support frame (see Fig. 2-24B) as a reference for the focus position.

- 11. Check that the display is centered in the focusing plate area. If not, the rotating slide adapter can be adjusted to permit proper centering of the image within the film frame. Refer to the camera manual for further information.
- 12. IMPORTANT: Press the Shutter Release control to close the shutter before setting the following camera controls:

Shutter Speed

1/5 s

Aperture Selector

F5.6

#### NOTE

F-stops higher than F4 are used to obtain better depth of field.

- 13. Remove the focusing plate. Load the camera back with 3000 ASA rating film. Close the camera viewing door.
- 14. Press the Shutter Release control to photograph the vector display. Develop the picture. If the vector photograph is not satisfactory; i.e., display and/or graticule markings are not properly exposed, readjust the INTENSITY and SCALE ILLUM controls. Take another picture.

#### NOTE

Initially, several pictures will have to be taken in order to find the best control settings. Once these settings are known by mentally noting the display presentation or by logging the control settings, then it is possible to duplicate the picture with less experimentation when the camera is used the next time. For additional information con-

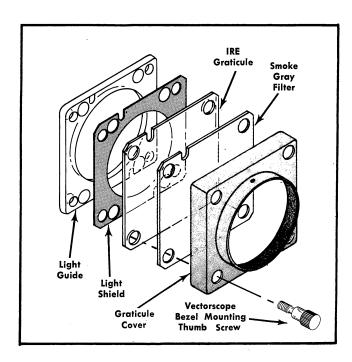


Fig. 2-27 Arrangement of parts when re-installing the graticule cover.

cerning the use of the camera, refer to the manual shipped with the C27 camera.

15. To obtain a double exposure photograph of two displays using a common graticule for both, proceeds as follows:

With the graticule illuminated and the desired display presented on the CRT, press the Shutter Release control to photograph the display. Set the Vectorscope controls to present the second display, turn down the SCALE ILLUM control so the graticule is not illuminated, and press the Shutter Release control. Develop the picture.

- 16. To obtain good photographs using the IRE (external) graticule, consider the following hints:
- (a) Check that the IRE graticule fits close to the CRT face. This position will minimize parallax. (The CRT face should protrude from the front panel the same distance as the thickness of the vector graticule light guide.)
- (b) Since another set of graticule lamps is turned on, readjust (if necessary) the SCALE ILLUM control to obtain proper graticule illumination.
- (c) Use the channel variable GAIN control to produce a slightly greater amplitude display to compensate for the parallax between the trace and IRE graticule as "seen" by the camera.
- (d) If the vector graticule appears on the photograph, remove the camera bezel. Position the IRE graticule lamp holders so the filaments are in line with the IRE graticule position. This will ensure that only the IRE graticule will receive proper edge lighting.
- 17. After completing the picture taking and the use of the camera, remove the camera and bezel. Re-install the graticule cover with all its associated parts (see Fig. 2-27) on the front of the Vectorscope CRT.

# **GLOSSARY OF TERMS**

CHROMINANCE: This term is used to indicate both hue and saturation of a color.

CHROMINANCE SIGNAL: In television, the sidebands of the modulated chrominance subcarrier which are added to the monochrome signal to convey color information. The chrominance signal components (I and Q signals NTSC) transmit the qualities of hue and saturation but do not include luminance or brightness.

COLOR BURST: In NTSC color, normally refers to a burst of approximately 8 cycles of 3.579545 MHz subcarrier on the back porch of the composite video signal. This serves as a color synchronizing signal to establish a frequency and phase reference for the chrominance signal.

COMPOSITE VIDEO SIGNAL: The complete video signal. For monochrome, it consists of the picture signal and the blanking and synchronizing signals. For color, additional color synchronizing signals and color picture information are added.

DIFFERENTIAL GAIN: The amplitude change, usually of the NTSC 3.579545 MHz color subcarrier, introduced by the

over-all circuit, measured in dB or per cent, as the picture signal on which it rides is varied from blanking to white level.

DIFFERENTIAL PHASE: The phase change of the 3.579545 MHz NTSC color subcarrier introduced by the over-all circuit, measured in degrees, as the picture signal on which it rides is varied from blanking to white level.

DYNAMIC: (When referred to a characteristic of the Type R520) Denotes the change of that characteristic with respect to a 10%-90% change in Average Picture Level (APL). Examples: Dynamic Phase, Dynamic Gain.

GEOMETRY: The degree to which a rectilinear display on a CRT screen is accurately reproduced. Generally associated with properties of a CRT.

H PULSE: Applicable only to the Type 520/R520. A pulse of approximately 6  $\mu$ s duration generated during horizontal blanking time and used as a timing pulse.

H RAMP: Applicable only to the Type 520/R520. A ramp voltage generated coincident with the H pulse and having the same time duration as the H pulse.

H RATE: The time for scanning one complete line, including trace and retrace, NTSC equals 1/15734 sec (color) or  $63.5~\mu s$ .

HUE: The attribute of color perception that determines whether an object is red, yellow, green, blue, purple, or the

like. White, black, and gray are not considered as being hues.

LUMINANCE: This indicates the amount of light intensity, which is perceived by the eye as brightness.

ORTHOGONALITY: The extent to which traces parallel to the vertical axis of a cathode-ray-tube display conform to a right angle with the horizontal axis.

SATURATION: This indicates how little a color is diluted by white light, distinguishing between vivid and weak shades of the same hue. The more a color differs from white the greater is its saturation. Saturation is also indicated by the terms purity and chroma. High purity and chroma correspond to high saturation and vivid color.

SCR: Subcarrier regenerator (applicable only to Type 520/R520).

COLOR SUBCARRIER: In NTSC color, the carrier whose modulation sidebands are added to the monochrome signal to convey color information, i.e. 3.579545 MHz.

VIDEO STRIPPING: The process of removing the video information from the composite video signal.

VITS: Vertical interval test signal.

9 LINE KEY-OUT: The period of time utilized by the equalizing pulses and the serrated vertical pulse, equal to the time duration of nine television lines during which burst is not present.

# **NOTES**

# SECTION 3 CIRCUIT DESCRIPTION

Change information, if any, affecting this section will be found at the rear of the manual.

#### Introduction

This section of the manual contains an electrical description of each circuit in the Type R520 Vectorscope. Block diagrams illustrating signal flow for six modes of operation are described prior to the detailed circuit description. A detailed block diagram of the complete instrument is included in the Diagrams section as an aid in troubleshooting. Complete schematics are also included in the Diagrams section. These diagrams should be referred to during the detailed circuit description. The electron convention of current flow is used in all references to current flow in the circuit description.

Proper understanding of the circuit description to follow will depend to some extent on the reader's understanding of typical electronic circuits. The list of references which follows provides an index of reference material relating to some of these typical circuits.

#### 1. Operational Amplifiers

Jacob Millman and Herbert Taub, "Pulse, Digital and Switching Waveforms", McGraw-Hill, New York, 1965, pp. 15-18.

#### 2. Field-Effect Transistors

Jacob Millman and Herbert Taub, "Pulse, Digital and Switching Waveforms", McGraw-Hill, New York, 1965, pp. 658-663.

#### 3. Miller Sweep Circuit

Jacob Millman and Herbert Taub, "Pulse, Digital and Switching Waveforms", McGraw-Hill, New York, 1965, pp. 536-538, 540-554.

#### 4. Regulated Power Supply

Phillip Cutler, "Semiconductor Circuit Analysis", McGraw-Hill, New York, 1964, pp. 559-625.

#### 5. Class "C" Oscillators

Frederick E. Terman, "Electronic and Radio Engineering", fourth edition, McGraw-Hill, New York, 1955, pp. 493.

# 6. Oscillators, Crystal

Frederick E. Terman, "Electronic and Radio Engineering", fourth edition, McGraw-Hill, New York, 1955, pp. 506-519.

#### 7. Synchronous Demodulators

A. Frederick E. Terman, "Electronic and Radio Engineering", fourth edition, McGraw-Hill, New York, 1955, pp. 1007.

B. Bernard Grob, "Basic Television Principles and Servicing", third edition, McGraw-Hill, New York, 1964, pp. 591, 602-607.

#### SIGNAL FLOW BLOCK DIAGRAMS

In the following description when a specific block has the same function in all modes of operation, only the initial description will be given. The switch selection for each mode of operation is specified on each block diagram.

Mode one (Fig. 3-1). Color bar signals are coupled into channel A and channel B Input Amplifiers of the Type R520. Channel A and B Input Amplifiers are operational amplifiers with a gain of one. The composite signal from the channel A amplifier is coupled to the Burst and Sync Amp, which has a gain of approximately two. The signal is then coupled to the Subcarrier Regenerator and to the Sweep circuit. The Sync Processing circuit removes the video from the composite signal and recovers the sync. This composite sync pulse is used as a timing reference for the regeneration of the sweep sawtooth and for the Field Selector circuit. The color burst is recovered from the composite signal that was coupled to the Subcarrier Regenerator and is used to phase and frequency-lock the internal oscillator that generates the reference subcarrier. The reference subcarrier is coupled into the Precision Phase Shifter, which is the front panel CALIBRATED PHASE control, to adjust the phase of the subcarrier up to  $\pm 15^{\circ}$ . The subcarrier is then coupled through the Subcarrier Amplifier to the A and B PHASE Goniometers. The A and B PHASE Goniometers are continuously variable and are controlled from the front panel. They can shift the phase of the reference subcarrier through 360°. The subcarrier is then coupled into the Subcarrier Switching circuit on the Demodulator board. The composite signals from the channel A and channel B Input Amplifiers are also coupled to the Demodulator board through the channel A and channel B Switching circuit.

The Subcarrier Switching circuit and channel A/channel B Switching circuits are controlled by a J-K flip flop with an output pulse at one quarter of the horizontal scanning frequency. Therefore the output of the channel A/channel B Switching circuit is a time-shared signal containing two lines of channel A information and two lines of channel B information. These signals are coincident with the timeshared A and B phase outputs of the Subcarrier Switching circuit. The reference subcarrier is coupled through a Subcarrier Amplifier to the Horizontal Demod Driver. The output of the Horizontal Demod Driver is coupled to the Horizontal Demodulator and to the Vertical Demod Driver. The reference subcarrier is shifted 90° in phase through the Vertical Demod Driver and coupled into the Vertical Demodulator. The composite signal from the channel A and B Switching circuit is coupled through a Composite Video Amplifier to a Chrominance Amplifier. The input to the chrominance amplifier is a high pass filter that removes all but the chrominance information from the signal. The output of the chrominance amplifier is coupled to the Vertical and Horizontal Demodulators.

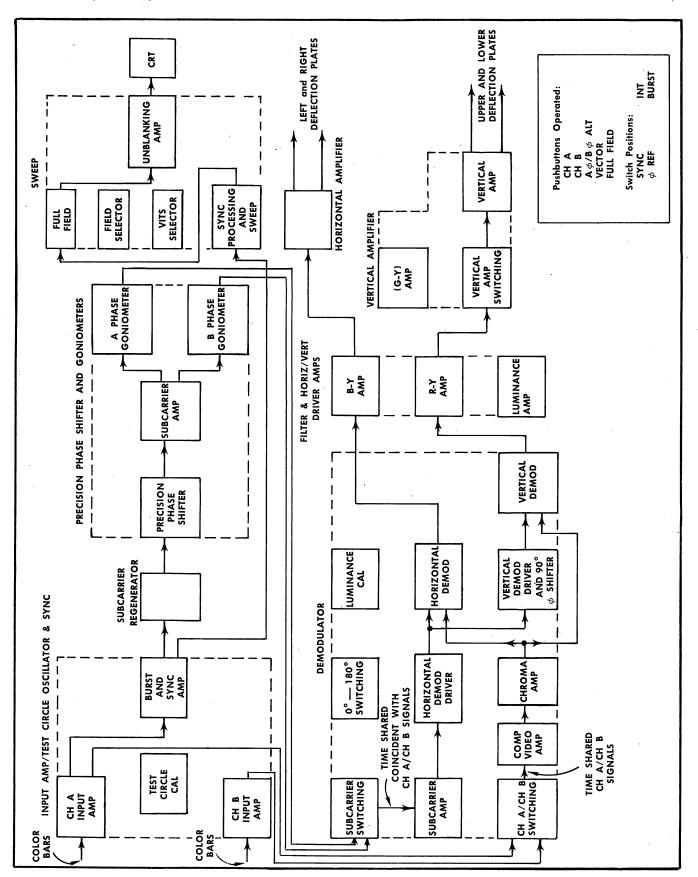


Fig. 3-1. Mode one, signal flow block diagram.

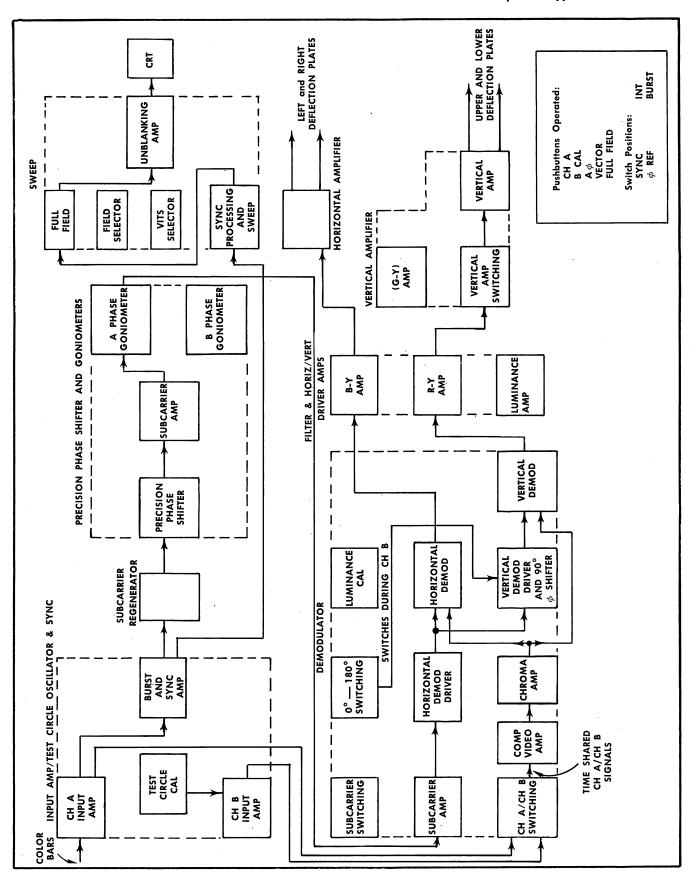


Fig. 3-2. Mode two, signal flow block diagram.

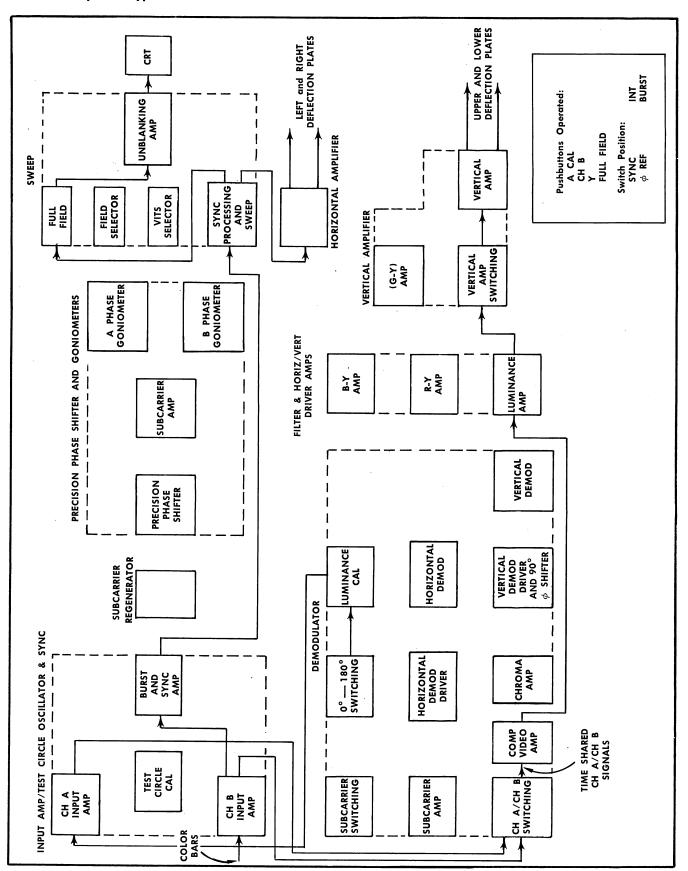


Fig. 3-3. Mode three, signal flow block diagram.

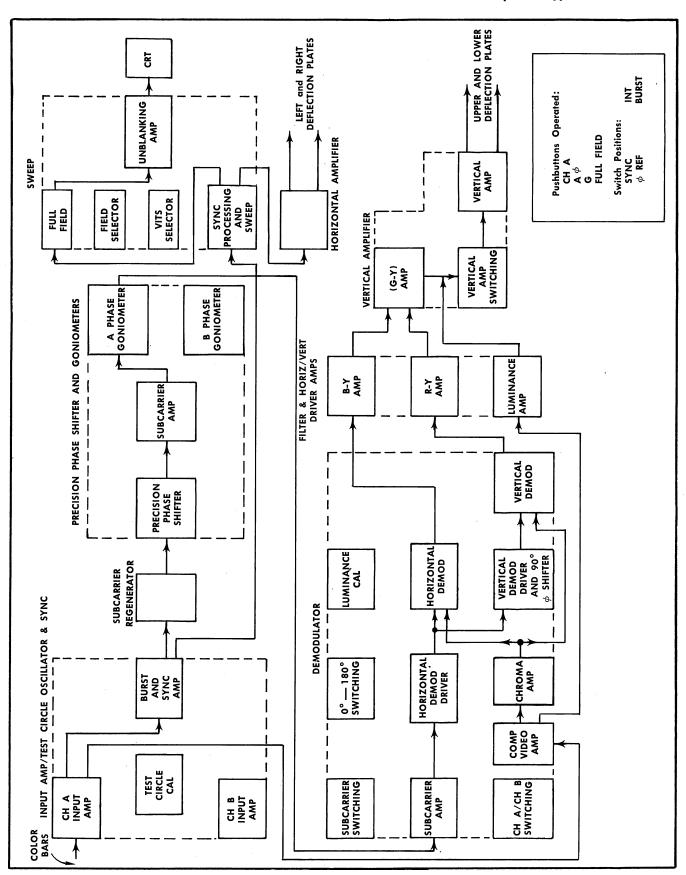


Fig. 3-4. Mode four, signal flow block diagram.

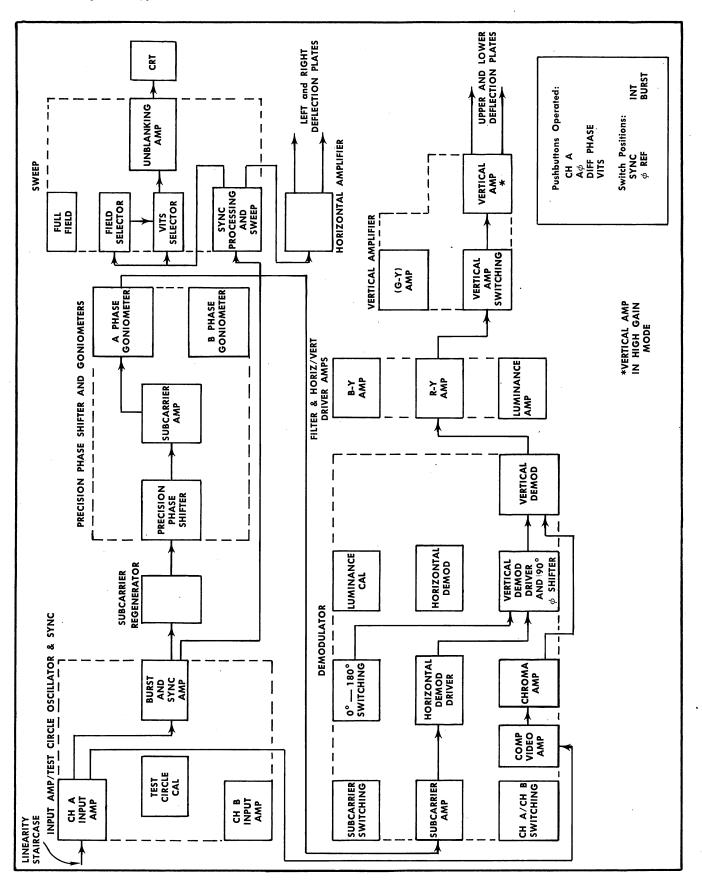


Fig. 3-5. Mode five, signal flow block digaram.

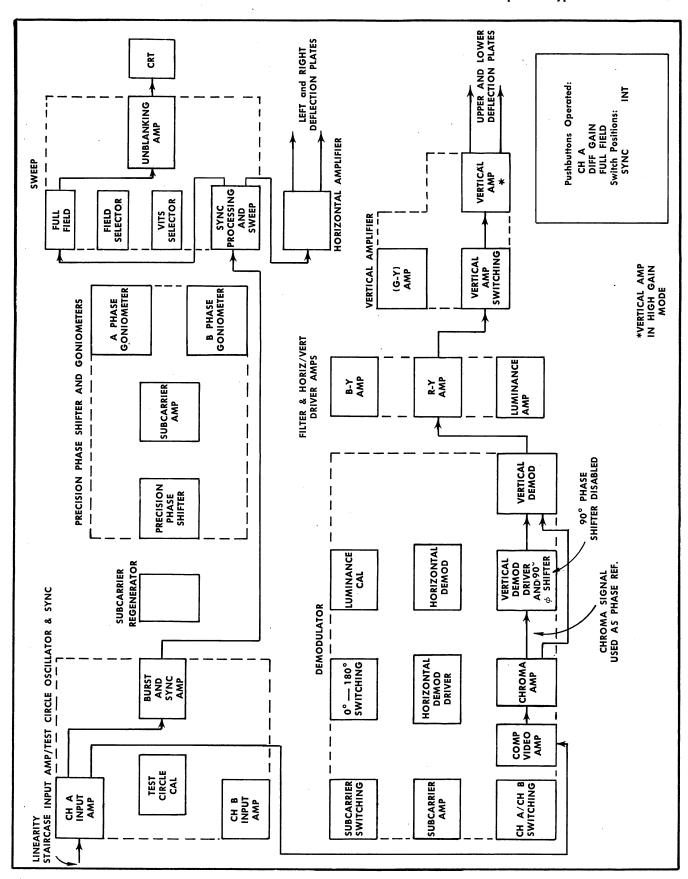


Fig. 3-6. Mode six, signal flow block diagram.

# Circuit Description—Type 520/R520 NTSC

The Vertical and Horizontal Demodulators are synchronous demodulators. The output of the demodulators corresponds to the amplitude of two components of the chrominance signal, with 90° phase difference between the Horizontal Demodulator and the Vertical Demodulator. The output of the Horizontal Demodulator is coupled through the B-Y Amplifier to the Horizontal Amplifier. The output of the Vertical Demodulator is coupled through the R-Y Amplifier to the Vertical Amplifier Switching circuit, which selects the signal to be coupled to the Vertical Amplifier. The output of the Vertical Amplifier. The Vertical and Horizontal Amplifiers are push-pull amplifiers driven paraphase. The outputs of the amplifiers are coupled to the deflection plates of the CRT where a display is obtained.

**Mode two (Fig. 3-2).** In this mode of operation, color bars are coupled into the channel A Input Amplifier only and channel B receives the signal from the Test Circle Oscillator. The Test Circle Oscillator is a crystal-controlled oscillator tuned to a frequency of 3.59 MHz. The test circle oscillator signal is coupled into the channel A/channel B Switching circuit and time shared with the signal from channel A input. Since  $A\phi$  is selected, the output of the A and B PHASE Goniometer is not time-shared, and only the A phase reference is coupled to the Subcarrier Amplifier.

In this mode of operation, since test circles are being displayed, the polarity of the reference subcarrier driving the Vertical Demodulator is inverted every television line. This is accomplished by the 0°-180° Switching circuit. The 0°-180° Switching circuit is controlled by the divide-by-two J-K flip flop. When QUAD PHASE is misadjusted, reversing the phase of the subcarrier driving the Vertical Demodulator every television line will produce two test circles, and a more accurate adjustment of the QUAD PHASE can be accomplished.

The remainder of the circuits used in this mode are as previously explained.

**Mode three (Fig. 3-3).** The Type R520 is being used to analyze the luminance component of this signal. Color bars are coupled into the B channel, and the cal signal for line sweep operation is coupled through the A channel. The square wave from the 0°-180° Switching circuit is used as the cal signal for line sweep displays. It provides a display of two horizontal traces adjusted for 140 IRE units of separation (1 volt peak-to-peak).

The luminance component is coupled from the Composite Video Amplifier through a filter to the Luminance Amplifier. The signal is then coupled to the Vertical Amplifier through the Vertical Amp Switching circuit. The sawtooth voltage from the Sweep circuit is coupled to the Horizontal Amplifier to provide the time base for the display.

**Mode four (Fig. 3-4).** This is another line sweep mode of operation used to measure the green signal. Color bars are coupled into channel A and the B channel is off.

The luminance component is coupled from the Composite Video Amplifier through the Luminance Amplifier to the Vertical Amplifier Switching circuit. The outputs of the Vertical and Horizontal Demodulators are coupled through the R-Y and B-Y Amplifiers respectively to the G-Y Amplifier. The R-Y and B-Y signals are added at the input of the G-Y Am-

plifier to form the G-Y signal. The amplifier inverts the signal and produces the G-Y signal. The G-Y signal is then added to the luminance signal to produce the green signal. The green signal is then coupled to the vertical amplifier.

**Mode five (Fig. 3-5).** The Type R520 is being used to make a differential phase measurement and the linearity staircase signal is coupled into channel A. Channel B is off and there is no cal signal.

The 0°-180° Switching circuit is operating in this mode of operation and the phase of the reference subcarrier in relation to the Vertical Demod Driver is being inverted every television line. This produces two horizontal traces on the CRT that can be adjusted to coincide by adjusting the phase of the reference subcarrier. The phase of the reference subcarrier is shifted by the Precision Phase Shifter and when the two traces coincide, the amount of differential phase can be read from the CALIBRATED PHASE shifter dial. The gain of the output from the Vertical Demodulator is changed to  $\times 5$  in the Vertical Amplifier Switching circuit for DIFF PHASE and DIFF GAIN measurements.

The recovered sync pulse is now coupled to the Field Selector and VITS Selector so an unblanking pulse is developed during the selected field and television line. This is another line sweep mode of operation.

Mode six (Fig. 3-6). A differential gain measurement is being made and the linearity staircase signal is coupled into channel A with channel B off. The reference subcarrier is not used when making this type of measurement. The chrominance signal from the Chrominance Amplifier is coupled to the Vertical Demod Driver and to the Vertical Demodulator. The 90° Phase Shifter in the Vertical Demod Driver is disabled in DIFF GAIN mode of operation. The chrominance signal is used as the phase reference in the Vertical Demodulator so that phase distortion will not influence the accuracy of differential gain measurements.

The previous modes of operation illustrate some of the uses of the Type R520 vectorscope. A detailed description of the circuits used is given in the following pages of this section.

# INPUT AMPLIFIERS AND TEST CIRCLE OSCILLATOR

This circuitry contains the Test Circle Oscillator and two input amplifier channels (A and B). Inputs to each amplifier can be selected from: composite video, the Test Circle Oscillator output for calibration of the vector display, or the Cal signal for calibration of the line sweep display. As an example, if channel A is selected for composite video, channel B might be selected for Test Circle Oscillator output. The channel that is selected for composite video has an output that is coupled to the Subcarrier Regenerator and if external sync is not used, the composite video signal is coupled to the Sweep circuit for triggering purposes and timing. Also, each channel has an output that is coupled to the Demodulator. Each amplifier is an operational amplifier with high input impedance. Therefore, the Type R520 does not present any appreciable loading effect to the signal under test, permitting the signal connections to remain in place when the Type R520 is not in operation.

# Input Amplifiers

The Input Amplifiers for both the A and B channels are the same; therefore, a description of the A channel will apply to both amplifiers.

Assume switch SW5 is in the A position. A negative 15 volts is applied to the cathode of D14, and D14 is forward biased. This causes the anode of D18 to be about negative 0.6 V (set by D16) and D18 is reverse biased. The output of the Test Circle Oscillator, therefore, cannot be coupled to the base of Q80. Composite video is connected to either J1 or J2. D8 is forward biased through the divider consisting of R3 and R4, so composite video is coupled to the base of Q80 through D8. Transistors Q80, Q81, and Q85 comprise the operational amplifier for the A channel, which has a gain of about one. D85 limits the collector of Q81 to about +10 V. Appearing on the collector of Q85 is the composite video signal, with about the same amplitude that is present at J1. Capacitor C2 is for frequency compensation.

The resistive networks containing D112 and D108 perform an AND function to either forward bias or reverse bias D116. If SW5 and SW55 are selected so —15 V is applied to R111 and R105, D112 and D108 are reverse biased. D114 is forward biased and D116 is reverse biased. Thus, any signal on the collector of Q85 cannot be coupled to the base of Q140. With the switches in this position, D100 in the B channel signal path is forward biased.

Since initially SW5 is assumed to be in the A position, R111 is not connected to —15 V, the voltage on the cathode end of D114 becomes positive and D114 is reverse biased. With D114 reverse biased, D116 becomes forward biased and the signal path from the collector of 85 to the base of Q140 is uninterrupted. With SW5 in the A position, —15 V is applied to the cathode of D102 which forward biases D102 and reverse biases D100.

The composite video that is present on the collector of Q85 is coupled through R88 to the Demodulator, and to the base of Q140 through D116. Q140 and Q141 form an operational amplifier with a gain of about two. (For Instruments SN B241650-up only. R141 and C143 provides the AC coupled feedback path from the collector of Q141 and to the base of Q140 to set this gain. In addition, R142, D142, R144, C144 and D144 provide sync-tip clamping at +4 volts. Clamping Q141's collector to this level insures the SCR output will not change with APL changes.) The composite video is coupled from the collector of Q141 through R149 to the Subcarrier Regenerator. Also, if Ext Sync is not used and SW130 is in the INT SYNC position, D134 is forward biased. Composite video is coupled to the Sweep Circuit through D134 and C136. If Ext Sync is used and SW130 is in the EXT position, D134 is reverse biased through D132. Ext Sync is coupled through D122, which is forward biased, to the Sweep circuit. Provisions are made so either 4 V or 1 V of Ext Sync can be used. R120 should be pin-connected to J120/J121 if 4 V of sync is used, and R121 should be connected if 1 V of Ext Sync is used.

#### **Test Circle Oscillator**

The Test Circle Oscillator supplies a calibrated 3.59 MHz sine wave to the input amplifier when a test circle display is desired for calibration purposes. The Test Circle Oscillator consists of a crystal oscillator Y40 and Q40, a feedback amplifier transistor Q30 and a transistor used to isolate the oscillator from the input amplifier, Q41.

When a vector display is selected, +10 V is removed from R33 and the base of Q30 goes negative. This turns Q30 on. As Q30 conducts, its collector goes in the positive direction, turning on oscillator transistor Q40. The oscillator output is taken off the collector of Q41 through a Pi filter which is resonant at 3.59 MHz, and coupled to the anode of D18 and D68. The oscillator output is fed back to the base of Q30 through D48. By controlling the amount of feedback to Q30, the amplitude of the output from the oscillator is controlled. Resistor R45 sets the DC level across D48. This determines at what point on the positive half cycle of the oscillator output D48 will become forward biased, which determines the amount of feedback to the base of Q30. Therefore, the oscillator output is maintained at a constant amplitude.

The primary and secondary windings of T45 act as RF chokes to decouple the oscillator output from the DC supply. Resistor R39 is used as a parasitic suppressor in the oscillator circuit. C18 and C66 are frequency compensating capacitors for the input amplifier.

#### SUBCARRIER REGENERATOR

The Subcarrier Regenerator (SCR) develops a continuous sine wave at the subcarrier frequency that can be used in place of an external subcarrier. The Internal Subcarrier Oscillator frequency is phase- and frequency-locked to the color burst, and is therefore locked to the chrominance signal. All the critical components of the oscillator and feedback amplifier are contained in a temperature controlled oven, and thus are free of any adverse affects caused by components. The burst intensification pulse for the unblanking amplifier is also developed in the SCR. Fig. 3-7 is a simplified block diagram of the SCR.

# **SCR Blocking Oscillator**

The SCR Blocking Oscillator includes Q205 and T205. The blocking oscillator is triggered by Q200. The back-swing of the blocking oscillator is used to switch the gain of a feedback amplifier during burst time and to develop the burst intensification pulse.

In the quiescent condition (no input signal) Q200 is off. D206 in the base circuit of Q205 is forward biased and Q205 is turned off. Since there is no current in the center-tapped secondary of T205, diodes D212 and D214 are off. D212 and D214 are matched diode units containing two diodes each. The two diodes in each unit develop sufficient voltage to provide adequate pulse amplitude for the burst intensification pulse.

The -H pulse is coupled to the base of Q200 through a differentiator consisting of C201 and R201. Q200 is forward biased by the positive spike of the differentiated waveform, causing the collector of Q200 to be pulled down. Through transformer coupling, the junction of the secondary of T205 and D206 goes positive and reverse biases D206. Q205 turns on and is driven into saturation. D212 and D214 remain off during the on time of Q205, since they are reverse biased by the secondary winding polarity of T205. As D206 is reverse biased, C208 starts to charge through R206. When C208 is charged to a voltage approximately 0.6 V more positive than the voltage on the base winding of T205, D206 starts conducting. The conduction of D206 causes the base of Q205 to be pulled down. The voltage drop in the base winding of T205 is coupled to the collector winding of T205, causing Q205 to be turned off very fast. During the backswing of T205, the polarity across the center-tapped second-

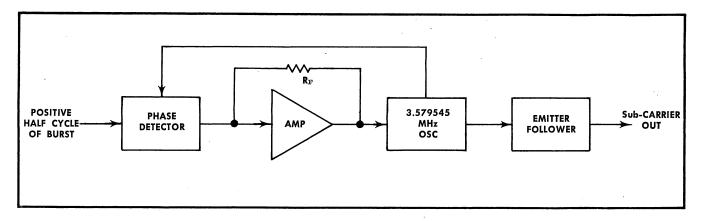


Fig. 3-7. Simplified block diagram of SCR.

ary reverses and forward biases D212 and D214. With D212 and D214 forward biased, the emitter resistance for Q220 becomes about 100 ohms (the parallel combination of D212 and D214 in series with R216).

The pulse developed by the blocking oscillator during back-swing is fed to the sweep board after going through a pulse shaping network, and is used to intensify the CRT trace during burst time.

Transistors Q220 and Q225 comprise a feedback amplifier that has its gain switched during burst time by the blocking oscillator.

The composite video signal is coupled through R220 to the 600 kHz band-pass filter consisting of L220, C220, L221 and C221, which removes the luminance component of the incoming signal and rejects any noise outside the pass-band. The chrominance component then appears at the base of Q220. The feedback amplifier normally has a gain of about one during burst time of the chrominance signal except when the back-swing of the blocking oscillator is occurring. Presence of burst causes the emitter resistance of Q220 to become about 100 ohms. The gain now becomes about 20, and burst is amplified approximately 20 times. D224 clamps the base of Q225 at approximately +10.6 V. The output of Q225 is coupled to the base of Q230 through C231.

#### SCR Limiter SN B251880 and up

The SCR Limiter consists of Q230, Q236 and Q238. Q238 provides constant current to either Q236 (normally on) or Q230. Q236 and Q230 are connected as a differential comparator.

With no burst applied to the base of Q230, the base is held at approximately -0.7 volts by divider R231 and R232. Q236 base is at approximately 0 volts; therefore, Q230 is off and Q236 is on. Under these conditions, any noise or residual chroma less than 0.6 volts appearing at the base of Q230 will not appear in the phase detector.

During burst time, the burst intensification pulse (discussed above) is applied to the base of Q236. The negative portion of this pulse drives the base negative and is clamped to about —0.6 volts by D235. Under these conditions, only the

positive portions of burst are of sufficient amplitude to switch the current from Q236 to Q230 to drive the phase detector. Driving the phase detector in this manner minimizes any natural ringing of the primary winding which would affect the oscillator frequency.

**Below SN B251880.** Q230 is a clamp and is biased so that it only turns on during the positive half cycle of burst. The emitter of Q230 is limited to  $-0.6\,\mathrm{V}$  by D234. A positive-going signal greater than 0.6 volt is required to turn on Q230; therefore, any noise or any residual chroma less than 0.6 V from the feedback amplifier will not turn Q230 on.

# **Phase Detector**

The Phase Detector is composed of C242, T235, C244, D242 and D244. The diodes are normally reverse-biased and the output of the Subcarrier Oscillator appears at the junction of D242 cathode and D244 anode. The potentiometer, R243<sup>1</sup>, is used to Balance the Phase Detector.

When Q230 is turned on during the positive half cycle of burst, its collector goes in the negative direction. This causes the upper end of T235 secondary to become positive and the lower end negative. D242 and D244 are now forward biased, and a sample is taken of the subcarrier oscillator frequency. If the feedback oscillator signal is of the correct frequency and shifted in phase exactly 90° from burst, the error signal at this time will be 0 volts. If the oscillator is off frequency, the error voltage will be either positive or negative, depending on whether the oscillator frequency is too high or too low. (Refer to Fig. 3-8). The RC time constant of the feedback circuit of the oscillator is sufficiently long that it requires the phase relationship to be incorrect for several television lines before a correction is made.

During the time D242 and D244 are forward biased, C242 and C244 are being charged to the burst amplitude. During the time when burst is absent, the capacitors discharge through R242, R243 and R244, keeping D242/D244 reverse biased. The discharge time of these capacitors is sufficiently long so the capacitors will only discharge a small amount during 9 line key-out.

<sup>&</sup>lt;sup>1</sup>R243 was added starting SN B150100.

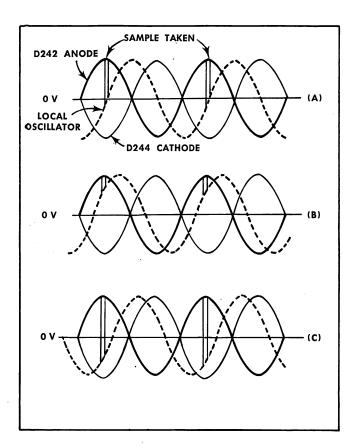


Fig. 3-8. Signals present in Phase Detector when D242 and D244 are forward biased and sample is taken. (A) Local oscillator same frequency as color burst. (B) Local oscillator at a higher frequency than color burst. (C) Local oscillator at a lower frequency than color burst.

#### **Oscillator Section**

The Subcarrier Oscillator is a crystal controlled oscillator contained in a constant temperature oven. The oscillator is not affected by heat dissipation of components or by environmental temperature changes.

The oscillator consists of Q260, Y260, and D260. Diode D260 is used as a voltage-variable capacitor across the crystal. By causing the voltage across the diode to change, the capacitance of the diode is changed and the crystal frequency is made to change. The voltage across D260 is controlled by the operational amplifier Q250 and Q255.

Q250 and Q255 are normally on. The gate of Q250 is referenced to 0 V DC and a signal voltage is present on the gate only during the time D242 and D244 are forward biased. The collector of Q255 is at a quiescent level which establishes the voltage across D260, and thus sets the crystal frequency. As D242 and D244 are forward biased, the error signal at their junction appears on the gate input of Q250. If the oscillator frequency and phase are correct the error voltage will be zero and the collector voltage of Q255 will remain at its quiescent level. If the oscillator frequency is high at the time the sample is taken, the error voltage appearing at the gate of Q250 will be positive. Q250 will turn on harder, causing Q255 to conduct more. Q255 collector goes in the negative direction, causing the cathode of D260 to become less positive. The capacitance of D260 increases and this returns the oscillator to the correct frequency.

The feedback network (low pass filter) for the feedback amplifier Q250 and Q255 consists of R254, C254, C255 and R255. R254 ( $R_1$ ) and the parallel combination of R242 and R244 ( $R_1$ ) set the DC gain for this amplifier. The amplifier has a gain of about 60 for the DC level change. The feedback path for the operational amplifier consists of a low pass filter to eliminate frequency components higher than 30 Hz, which stabilizes the oscillator.

Resistor R250 DC BAL, is provided to adjust the oscillator frequency. The adjustment of R250 changes the operating bias of Q250 and Q255, which sets the quiescent collector voltage of Q255. The collector voltage of Q255 establishes the voltage across D260, the voltage-variable capacitor.

The output of Q260 is coupled through Q270, which isolates the oscillator from the output, through a Pi filter designed to pass only the subcarrier frequency to the base of Q275. The output of the SCR is taken off the emitter of Q275 and the signal to the Phase Detector is taken off the collector of Q275. Therefore, the output of the SCR is isolated from the Phase Detector. The collector impedance of Q275 is approximately two times the emitter impedance of Q275 at the subcarrier frequency. The signal to the Phase Detector is 2× the subcarrier output to R301. The low DC resistance of the parallel combination R279 and L279 allows the feedback signal to be referenced at 0 volts DC.

#### SCR Oven

The critical components of the Subcarrier Regenerator oscillator are contained in an oven which is maintained at a constant temperature of about 85°C. A bridge consisting of two wire-wound nickel resistive elements and two wire-wound manganin resistive elements form the heating element and also the sensing element. The temperature coefficient for manganin is 0%/°C and for nickel it is +0.55%/°C. The resistors are designed so their resistances are equal at about 85°C. A comparator, Q280A and Q280B, is used to sense any unbalance across the bridge and to operate the current control transistor Q285.

When power is initially applied to the Type R520 the bridge is unbalanced, since the oven is not up to operating temperature. The resistances of R280B and R280D are less than those of R280A and R280C making the base of Q280A more negative than the base of Q280B. Thus, Q280A is on and Q280B is off. With Q280A on, its collector is pulled up and Q285 is turned on, conducting through the bridge. Q295, which controls the current through the quick-heater (R299), is on and the quick-heater is operating. This eliminates long warm up time. As the oven comes up to operating temperature, the resistance of R280B and R280D increases and Q280B turns on. Q280B conducts through the baseemitter junction of Q291 and turns Q291 on. As Q291 turns on, its collector goes negative and turns Q295 off. This turns the quick-heater off. Also as the oven approaches its operating temperature, the base of Q280A becomes more positive which decreases the conduction of Q280A. This causes the base of Q285 to becomes more negative, decreasing the conduction of Q285. When the oven is at its operating temperature, the voltage across the bridge is balanced. This balances the comparator and the current through Q285 is at a constant level. If the temperature of the oven either increases or decreases the resistance of R280B and R280D reacts in the same manner, unbalancing the bridge and causing either more or less current to flow

through Q285. Thus, the oven is returned to its operating temperature.

Any tendency of the circuit to oscillate due to common mode signals is eliminated by R287, which establishes the common mode gain as less than unity. "Hunting", sometimes experienced in this type of circuit when the oven reaches its operating temperature, is offset by R292. The heater circuitry is very stable and the oven temperature is maintained within about one degree of its operating point. A thermal cutout, TK280, is provided to disable the heater circuit by removing the +10 V supply if the oven temperature should ever exceed approximately 95°C.

# PRECISION PHASE SHIFTER AND GONIOMETERS

The purpose of the Precision Phase Shifter is to provide extremely accurate incremental phase measurements. The CALIBRATED PHASE control is capable of shifting the phase of the reference subcarrier + and  $-15^{\circ}$ . The Goniometers provide a non-calibrated means of shifting the phase of the reference subcarrier through 360°.

Either the internal reference subcarrier or an external reference subcarrier can be coupled into the Precision Phase Shifter circuit. Switch SW305 selects either of the two reference subcarriers. Assume that the internal subcarrier is selected, and SW305 is placed in the BURST position. A positive 10 volts is connected to R316, and D312 becomes forward biased. When D312 is forward biased, D311 is reverse biased and the external reference subcarrier is prevented from being coupled into the Precision Phase Shifter. C314 establishes AC ground on the anode of D312 and prevents any subcarrier from being coupled through the capacitance of D311. D302 is reverse biased through R304, and D301 is forward biased through R302 and R320. The internal reference subcarrier is coupled to the base of Q320. Q320 and Q325 form an operational amplifier with the output taken off the emitter of Q235. The reference subcarrier is coupled into the Precision Phase Shifter from the emitter of Q325. The Precision Phase Shifter consists of R331, R333, R335, R337, L331, L332, C332 and C335. L331 and L332 are used during the calibration of the instrument to tune the circuit to resonance. R335 is adjusted during calibration to obtain the correct dial reading. C335 (CALI-BRATED PHASE), is the front panel control, and as it is varied the capacitance to ground is changed. This causes the phase of the signal out of the Precision Phase Shifter to shift in increments between + and  $-15^{\circ}$ . The reference subcarrier is coupled from the Precision Phase Shifter through an operational amplifier consisting of Q340 and Q345 to the A and B PHASE Goniometers.

#### **Goniometers**

The A and B PHASE Goninometers are the same except for circuit numbers; therefore, only the A PHASE Goniometer will be described.

The Goniometer consists of two sets of primary coils at right angles to each other, and a secondary coil that can be rotated through 360°. R354 and C354 provide a fixed 90° phase shift in the horizontal coils, which is necessary for a rotating magnetic field when a sine wave is applied. R354 and C354 are designed so the circuit has a Q of one, so the current in the two sets of coils is equal. The entire circuit is resonant to the reference subcarrier frequency.

The secondary coil can be rotated manually and placed in any position relative to the primary coils. The magnetic lines of force formed by the currents in the primary coils induce a voltage into the secondary. The phase relationship of the output voltage to the input voltage will be determined by the physical position of the secondary coil in relationship to the primary coils. The output of the Goniometer is inductively coupled into the Demodulator circuit. The secondary coil is rotated by the PHASE control on the front panel.

# **DEMODULATORS**

The Vertical and Horizontal Demodulator circuits are both located on the Demodulator circuit board. The circuit operation of the Vertical and Horizontal Demodulators is the same except for a 90° phase difference between the demodulated chrominance signals out.

The 0° and 180° switching for test circle operation and differential phase measurements takes place on the Demodulator board, as does the 33° phase shift for demodulation along the I and Q axis.

Since the operation of the Horizontal and Vertical Demodulators is the same, only the operation of the Horizontal Demodulator will be described.

#### **Horizontal Demodulator**

The Horizontal Demodulator is composed of Q590A, Q590B, Q595A, Q595B, and T598. Transistors Q595A and Q595B are used as switches to alternately switch each end of T598 to ground at the subcarrier rate. The reference subcarrier is coupled to the bases of Q590A and Q590B. As Q590A and Q590B are alternately turned on and off they cause Q595A and Q595B to be turned on and off. Therefore, the polarity of the secondary of T598 is reversed at the reference subcarrier rate. Diodes D594 and D596 prevent Q595A from saturating. D594 is forward biased during the entire time power is applied to the Type R520. D596 becomes forward biased when the collector voltage of Q595A equals the base voltage, so the collector voltage can never become more negative than the base voltage, and Q595A is not allowed to saturate. The effects of transistor storage time are thus eliminated. In the same manner as just described, D598 and D599 prevent Q595B from saturating. Diodes D595 and D597 clamp the collectors of Q595A and Q595B at approximately .8 volt.

The chrominance signal (modulated subcarrier) is applied to the primary winding of T598. By switching the polarity of the secondary of T598 at the subcarrier rate an effect is produced as if the reference subcarrier were present in the secondary winding. There is a voltage developed at the secondary center-tap of T598 that is dependent upon the phase relationship of the modulated signal in the primary, and the rate at which the polarity of the secondary is switched. As the phase relationship changes, the amplitude of the voltage developed at the center-tap will also change. These voltage changes correspond to the modulating signal (or the difference frequency), so the demodulated chrominance signal is present on the center-tap of T598. The demodulated chrominance signal is essentially free of any subcarrier.

Fig. 3-9 is a simplified illustration of the action taking place in T598 as each end of the secondary is switched to ground through the transistor. The transistors are represented

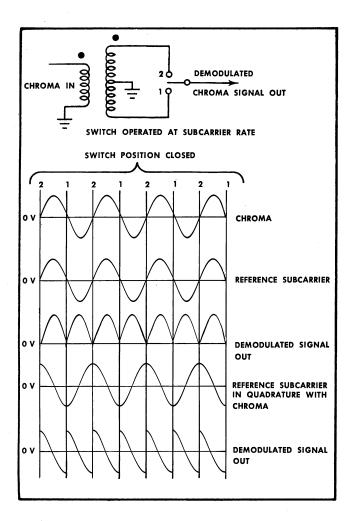


Fig. 3-9. Simplified illustration of Vertical/Horizontal Demodulators.

would have been disconnected. When it is desired that channel A and channel B inputs alternate, SW520 (A $\phi$ /B $\phi$ ALT) is depressed and -15 V is connected to the emitters of Q515 and Q516 through R519, D515 and D517. With SW520 depressed, Q515 and Q516 are connected in a common emitter configuration and driven in a paraphase manner by pins 5 and 7 of U511.

With channel A selected, D520 and D522 are forward biased and the reference subcarrier appears on the base of Q530. Q530 is an operational amplifier with the AC feedback path being C535, D532 and D533. Since the forward resistance of the diodes will change with any change in amplitude of the signal,  $R_{\rm f}$  is effectively variable (greater for small signals and less for larger signals). Thus, the peak amplitude of the signal is limited by the forward resistance of the diodes. The RC network consisting of R532, R533 and C532 sets the DC level of the signal on the collector of Q530 by a toggle switch and the waveforms for each position of the toggle switch are illustrated. C593 is a subcarrier bal-

ance capacitor to balance out any reference subcarrier from the Vertical Demodulator that is coupled into the Chrominance Amplifier, Q470/Q471. The reference subcarrier driving the Horizontal Demodulator is capacitively coupled through C593 and C594 to the Chrominance Amplifier. The subcarrier driving the Vertical Demodulator is shifted in phase 90° from the subcarrier driving the Horizontal Demodulator. The fed-back signal from the Horizontal Demodulator to the Chrominance Amplifier will appear 180° out of phase with any signal coupled into the Chrominance Amplifier from the Vertical Demodulator, thereby canceling the unwanted signal.

#### **Vertical Demodulator**

The Vertical Demodulator includes T508, Q500A, Q500B, Q505A and Q505B. The demodulator operates in the same manner as the Horizontal Demodulator and the components have the same function as their counter parts in the Horizontal Demod.

To display a vector presentation, a 90° phase shift between the vertical and horizontal signals driving the deflection circuits is required. The reference subcarrier is shifted 90° in the vertical circuit by C491, the feedback capacitor for the Vertical Demod Driver Q490/Q491.

R501 is a Subcarrier Balance to balance out any subcarrier from the Vertical Demodulator that is coupled into the chrominance signal that is being demodulated by the Vertical Demodulator. A portion of the subcarrier driving the Vertical Demodulator is coupled into the Chrominance Amplifier by the adjustment of R501. The fed-back signal appears 180° out of phase with the unwanted subcarrier that is coupled into the Chrominance Amplifier from the Vertical Demodulator, thereby canceling the unwanted signal. In line sweep operation if the unwanted subcarrier was not canceled out, the DC level of the demodulated signal out of the Vertical Demodulator would change and there would be a noticeable trace shift on the CRT when the instrument was operated in DIFF PHASE.

#### Reference Subcarrier Channel

The reference subcarrier for the Horizontal and Vertical Demodulators is received from the A and B PHASE Goniometers. The A channel input consists of D520, D521 and D522 The B channel input consists of D524, D525 and D526. Either channel may be selected by switching transistors Q515 and Q516. The switching transistors can also be operated in an alternate mode which displays two lines of channel A and then two lines of channel B. Of the three buttons,  $A\phi$ ,  $B\phi$ ,  $A\phi/B\phi$  ALT, only one can be depressed at a time. The selected channel is coupled into an operational amplifier Q530.

Integrated circuits U510 and U511 are J-K flip flops. Pins 5 and 7 are the output pins and pin 2 receives the trigger pulse. Each time a negative-going trigger is received on pin 2, the multi will flip and the output pins will change states. U510 is triggered by the —H pulse coupled through D511. Pin 5 of U510 is connected to pin 2 of U511, so each time pin 5 of U510 is down, U511 receives a trigger. With the integrated circuits connected in this manner U510 is a divide-by-two multi and U511 is a divide-by-four multi. The outputs of U511 operate the switching transistors for the A and B channels in the alternate mode and the output of U510 is used to do the 0° to 180° switching. Refer to Fig. 3-10 for U510 and U511 output pin logic.

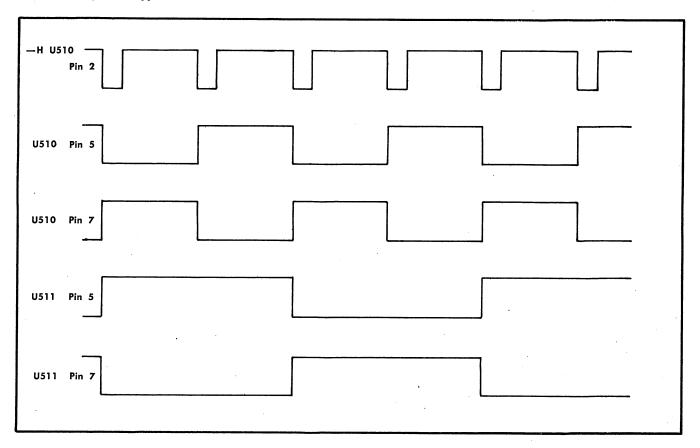


Fig. 3-10. Logic for output pins of U510 and U511.

Assume that it is desired to select channel A, and SW510 is placed in the  $A\phi$  position.  $-15\,\mathrm{V}$  is applied to the emitter of Q515 through R517. Q515 turns on and its collector is pulled down. With the collector of Q515 pulled in the negative direction D524 and D526 are reverse biased. D525 is forward biased, preventing the collector of Q515 from going below approximately  $+3.0\,\mathrm{V}$ .

Therefore, any signal appearing on the B channel is blocked by D524 and D526 and if any signal is fed through D524, it is shorted to ground by D525. SW515 and SW520 are off so the emitter circuit of Q576 is open and Q576 is off. D521 is reverse biased, D520 and D522 are forward biased through R521, and the reference subcarrier on the A channel is coupled through D520, D522 and C529 to the base of Q530. If channel B had been selected, Q516 would have been turned on and D520/D522 in the A input line through negative feedback. The output of Q530 is coupled to the base of Q540, another operational amplifier that is operated as a limiter. D543 in the emitter circuit of Q540 clamps the emitter at approximately -0.6 V. If the negative peak swing of the signal on the base of Q540 is greater than approximately -0.6 V, Q540 will cut off and limit the negative half of the signal. The current through Q540 when the base swings positive is limited by R543 to about 6 mA. Since the average current through Q540 is controlled by the feedback resistor, R545, both the amplitude and duty cycle of the collector current are relatively independent of input signal amplitude. The signal on the collector of Q540 is coupled through a Pi section filter to the base of Q560. Q560 and Q565 form an operational amplifier, with R556 as  $R_{\rm i}$  and R566 as  $R_{\rm f}$ , driving the primary of T590. The reference subcarrier is induced into the two seconary windings of T590 which drive the Horizontal Demodulator and Vertical Demod Driver.

The 33° phase shift for the I and Q signal is accomplished by C554, which swings the Pi section tank to the other side of resonance. When either the I or Q signal is selected, a positive voltage is removed from the base of Q550, which turns off Q550. This disconnects C554 from the low pass filter through Q550 and shifts the reference subcarrier by 33°.

The reference subcarrier from the center-tapped secondary of T590 is coupled through D488 to an operational amplifier consisting of Q490 and Q491. Q490 and Q491 are operated as an integrator with R586 as  $R_i$  and C491 as  $C_f$  providing the 90° phase shift required for the Vertical Demod. The collector load for Q491 is the primary of T500, whose secondary drives the Vertical Demodulator. Fig. 3-11 (A) illustrates phase relationship of  $E_{in}$  and  $E_{out}$  through Q490/Q491.

A QUAD PHASE control (R588) is provided so the phase of the reference subcarrier driving the Vertical Demodulator can be adjusted for exactly 90° phase difference between the Vertical and Horizontal Demodulators. When displaying test circles, if the phase difference is exactly 90°, a perfect circle will be displayed. If the phase difference between the outputs of the Vertical and Horizontal Demodulators is not exactly 90° two ellipses will be displayed. This adjustment will affect the vertical demodulation axis whether test circles are being displayed or not; therefore, it should only be adjusted when test circles are being displayed. The

adjustment of R588 changes the voltage on D586 which is a voltage-variable capacitor. As the voltage on D586 changes, the capacitance also changes, shifting the phase of the reference subcarrier.

When differential gain measurements are being made the reference subcarrier is disconnected from the Vertical Demodulator and the chrominance signal is coupled to the Vertical Demodulator. This is accomplished by Q480, D486, D487, and D488. With Q480 off, D488 is forward biased. When making a differential gain measurement, a positive voltage is applied to the base of Q480 through R484 and Q480 turns on. When Q480 turns on, D488 is reverse biased and D487 is forward biased. The chrominance signal is coupled to the Vertical Demodulator Driver through C474 in place of the reference subcarrier.

Since the  $Z_i$  to Q490/Q491 is now capacitive rather than resistive, the chrominance signal into the amplifier will undergo a phase inversion through the amplifier, but will not be shifted in phase 90° (as is the subcarrier in all other modes of operation). The signal applied to the bases of Q500A and Q500B is then in phase with the chrominance signal applied to T508. The output of the demod will then be proportional only to the amplitude of the incoming signal, and differential gain measurements will not be in-

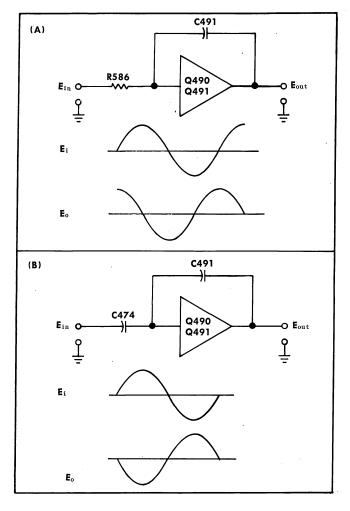


Fig. 3-11. Q490/Q491 configuration; (A) For all modes except DIFF GAIN,  $E_{\rm o}$  phase-inverted and phase-shifted 90° lagging in relation to  $E_{\rm i}$ . (B) For DIFF GAIN,  $E_{\rm o}$  phase-inverted in relation to  $E_{\rm i}$ .

fluenced by the presence of differential phase. Fig. 3-11 (A) Illustrates the configuration of Q490/Q491 and the phase relationship of  $E_{\rm in}$  to  $E_{\rm out}$  for all modes of operation other than DIFF GAIN. Fig. 3-11 (B), illustrates the DIFF GAIN configuration of Q490/Q491 and the phase relationship of  $E_{\rm in}$  to  $E_{\rm out}$ .

When making differential gain measurements, the output of the Vertical Demodulator is referenced at essentially 0 volts during H pulse time by the action of Q495. At the completion of the —H pulse the associated circuitry of Q495 provides an offset current to the summing junction of Q620/Q630, the Vert Driver Amps. The offset current allows the greatly magnified display in DIFF GAIN to be positioned on screen by the VERT POSITION control. Fig. 3-12 a partial diagram of the Vertical Demodulator.

When the DIFF GAIN switch is pressed, +10 volts is connected to R495 in the emitter circuit of Q495, turning off D496 and causing Q495 to conduct during the time the —H pulse is present on its base. The —H pulse also turns on D497, causing its anode to go in the negative direction to reverse bias D498. When Q495 conducts its collector goes in the positive direction, which turns off Q500A and Q500B. With Q500A and B turned off, the ends of the center-tapped secondary of T508 are clamped to ground by Q505A and Q505B. This establishes a reference for the clamping circuit in the Vertical Amplifier.

At the end of the —H pulse Q459 will turn off and the Vertical Demodulator will operate normally. The output of the demodulator will be negative with respect to the reference level, and will go more negative with increasing signal. However, D497 turns off at the completion of the —H pulse and the current that was flowing through it flows through D498 to the summing junction of Q620/Q630. This current is opposing the output of the demodulator and is used to provide an offset to position the magnified chrominance signal on screen.

When the DIFF GAIN switch is not pressed Q495 is off, and D496 is forward biased. The current that was flowing through D498 now flows through D496 and the offset current is disconnected from the summing junction of Q620/Q630.

The DIFF GAIN switch SW530 also applies a positive voltage to the base of Q530 through R528 and to Q540 through R541 to saturate the transistors and prevent any subcarrier from being coupled through to the demodulators.

#### Input Channel Switching

The A and B inputs to the chrominance channel are coupled in from the input amplifier. Each input contains a resistive network where the attenuation ratio can be changed by SW405 (A input) or SW415 (B input) to display the 100 per cent or 75 per cent color bar signals properly in the vector display. The 100% position on the GAIN switch permits the vector presentation of 100% bars to occupy the same display area (except for burst) as the 75% bars. The instrument is calibrated in IRE only in the 75% position. The third position of SW405 and SW415 is the MAX GAIN position, which provides maximum gain of the chrominance signal for DIFF GAIN and DIFF PHASE. When the MAX GAIN position of either SW405 or SW415 is selected, the luminance component of the signal is filtered out by either L401 or L411 respectively. (Below SN B150100, the filter is L402 or L412). This allows the signal to be analyzed very closely. The GAIN controls are R403 for the A channel and R413 for the B channel. The GAIN controls vary the attenua-

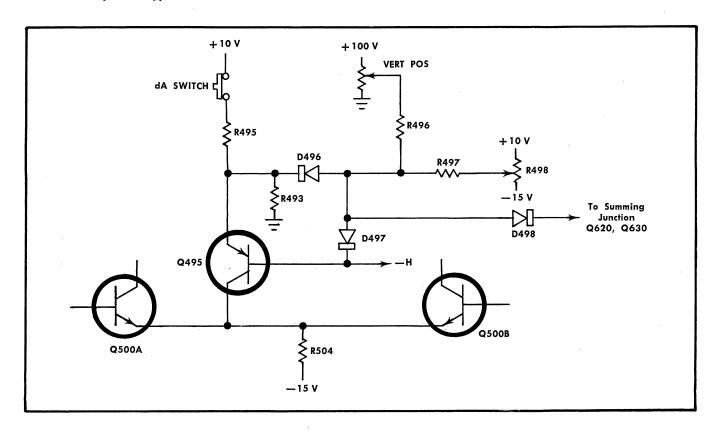


Fig. 3-12. Partial diagram of Vertical Demodulator.

tion of the divider which changes the amplitude of the signal into the demodulator. Both the A and B input lines have switching diodes—D407, D408, D409 and D429 for the A channel, and D417, D418, D419 and D424 for the B channel. These diodes select the desired channel for viewing. The diodes are controlled by switching transistors Q420 and Q425.

Assume that the demodulator is being used in the alternate mode of operation  $A\phi/B\phi ALT$ . In this mode of operation both the channel A switch (SW5) and the Channel B switch (SW55) are pressed and neither pin P nor pin S is connected to + 10 volts. Therefore, Q421 is turned off and the only source of emitter current for Q420 or Q425 is through R428 to +10 volts. Transistors Q420 and Q425 are alternately being turned on and off by the divide-by-four J-K flip-flop U511. Each transistor is on for two television lines and off for two lines. When pin 5 of U511 is down, Q420 is turned on and conducts through D421 and R428 to +10 V. With Q420 conducting, its collector is pulled up and D408/D429 are reverse biased. D407 is forward biased through R409 to +10 V. The signal appearing on the A input line is shorted to ground by D407 and blocked from the chrominance channel by D408 and D409. D409 clamps the collector of Q420 to  $\pm$ 0.6 V. When pin 5 of U511 is down, pin 7 is up and Q425 is off. With Q425 off, D418 and D424 are forward biased through R429 and D417 is reverse biased. The signal appearing on the B channel line is coupled through to the base of Q440. When U511 receives the next trigger from U510, pins 5 and 7 change states, Q420 turns off, and Q425 turns on. Now the A signal is coupled to the base of Q440 and the B signal is blocked.

Now assume that A channel is selected. SW5 (channel A) is pressed and the  $+10\,\mathrm{V}$  is removed from the emitter of Q420 through R421. Q420 turns off and D408/D429 are forward biased through R424, D407 and D409 are reverse biased. The signal on the A channel input line is coupled into the amplifier consisting of Q440, Q445 and Q450. Since SW55 (channel B) is not pressed, +10 V is connected to the emitter of Q425 through R426 and Q425 is on. With Q425 on, the diodes in the B input line are reverse biased and the signal is prevented from being coupled through to the chrominance channel. The  $+10 \,\mathrm{V}$  at the junction of R423 and R426 supplies base current to Q421 so Q421 is conducting. With Q421 conducting its collector is pulled down and D421/D427 are reverse biased. If either SW5 or SW55 is in the off position, the pulse from U511 is not sufficient to cause Q420 and Q425 to switch.

The composite signal is coupled through an operational amplifier consisting of Q440, Q445 and Q450. When the 100%, 75%, MAX GAIN switch (SW415/SW405) is placed in the MAX GAIN position, the gain of the amplifier is increased X5. This is accomplished by the feedback network located on the Feedback board which changes the amount of current fed back in the amplifier. The feedback circuit for both the A and B channels operate in the same manner, therefore only channel A will be discussed.

The feedback resistors are R433/R434, with the amount of current through R433 controlled by Q432. In the 100% or 75% position of SW405, the base of Q432 is connected to ground and the transistor is off. R437, in the collector of Q432, presents a high impedance to ground at the junc-

tion of R433/R434 and the majority of the feedback current flows through R433.

When SW405 is placed in the MAX GAIN position, the ground is removed from the base of Q432 and +10 volts is applied to the base through R438. The transistor now saturates and approximately 4/5 of the current that was flowing through R433 now flows through the transistor, thus reducing the amount of feedback current in the amplifier and increasing the gain to approximately X5. The gain of the amplifier is adjusted by C434, which changes the amount of current flowing through Q432, and the phase of the feedback current is adjusted by C430. If the A CAL pushbutton is pressed in during the time SW405 is in the MAX GAIN position, —15 volts is connected to the base of Q432 through R439, which turns the transistor off. This prevents an erroneous display of the CAL signal.

D450 limits the base of Q450 to about +10.6 V. The luminance component is coupled from the collector of Q450 through R452 to the luminance filter. The chrominance is coupled through R453 and R455, through a high-pass filter (L455, C455, L457 and C457) to the emitter of Q470. Transistors Q470 and Q471 form an operational amplifier with the output taken off the collector of Q471. The chrominance signal is coupled from the collector of Q471 to the Vertical and Horizontal Demodulators. The chrominance is also coupled through C474 to the anode of D487 and cathode of D486. D487 is reverse biased and D486 is conducting, except when differential gain measurements are being made.

The 3rd and 5th harmonics of the chrominance signal are prevented from being fed into the demodulators by traps in the collector circuit of Q450. L453 and C453 comprise the 5th harmonic trap, L454 and C454 comprise the 3rd harmonic trap.

During the horizontal blanking pulse time, the junction of C455 and C457 is effectively at AC ground. Any signal

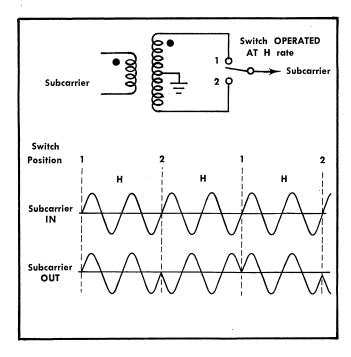


Fig. 3–13. Simplified illustration of the  $0^{\circ}$  to  $180^{\circ}$  switching action.

appearing at the junction is shorted to ground during this time. The clamps in the Vertical and Horizontal Amplifiers can now clamp to zero signal level during sync tip time. Q460 is normally off and is turned on by the —H pulse coupled through C461 to the base of Q460. When Q460 turns on, D463 and D465 are forward biased to effectively connect the base and collector of Q460 together. The collector of Q460 is at a very low impedance to ground, which effectively grounds any signal at the junction of C455 and C457.

# 0° and 180° Switching

During the time test circles are being displayed or differential phase measurements are being made, the phase relationship of the reference subcarrier to the Vertical Demodulator is switched between 0° and 180°. Transistors Q575 and Q576 alternately switch each end of the center tapped secondary of T590 to the signal ground. Therefore, the phase of the signal at the center-tap is alternately switched from 0° to 180°. The operation of the 0° to 180° switching is similar to the switching action of the demodulators except that a slower switching rate is used. Fig. 3-13 is a simplified illustration of the 0° to 180° switching action, in which Q575 and Q576 are represented by a toggle switch.

When no CAL signal is selected or differential phase measurements are not being made, the 0° and 180° switching circuit is not operating. The  $+10\,\mathrm{V}$  supply is connected to the base of Q571 through the divider consisting of R578, R576 and R577. D576 is reverse biased and Q571 is saturated. Q570 is off and the pulse from the divide-by-two flip flop U510 will not cause Q570 and Q571 to switch. The phase of the reference subcarrier at the center-tapped secondary of T590 is unchanged Now, assume that a differential phase measurement is to be made. The  $+10\,\mathrm{V}$ is removed from R578, and D576 becomes forward biased. Q571 is not conducting as hard, and the pulse from the divide-by-two flip flop will now cause Q570 and Q571 to switch. As Q570 and Q571 are switched, Q575 and Q576 are alternately turned on and off, causing each end of the center-tapped secondary of T590 to be alternately switched to signal ground. The switching square wave from pin 7 of U510 is occurring at an H/2 rate; therefore, the phase of the reference subcarrier at the center-tap of T590 secondary is being inverted every television line.

#### **Test Circles**

Test circles are provided as a CAL signal to insure an exact 90° phase relationship of the Horizontal and Vertical Demodulators, and correct gain adjustment of the Vertical and Horizontal circuits. This insures a true representation of the phase of the vectors displayed in vector operation.

When test circles are being displayed, the signal from the Test Circle Oscillator is coupling into either the A or B chrominance input of the demodulator. The signal is then coupled through the chrominance channel to the Vertical and Horizontal Demodulators. The reference subcarrier from either the A or B PHASE Goniometer is coupled through the reference subcarrier channel to the Horizontal and Vertical Demodulator. The reference subcarrier that is coupled to the Vertical Demodulator has its phase reversed 180° every television line by the 0° to 180° Switching circuit. This causes the output of the Vertical Demodulator to be inverted every other line. Without this inversion, a misadjustment of QUAD PHASE would have caused the test circle to look like an

ellipse. Now, with the vertical axis reversed, a misadjustment of QUAD PHASE appears as two crossed ellipses, allowing a more accurate adjustment of QUAD PHASE. The output of both the Horizontal and Vertical Demodulators is the difference frequency of the Test Circle Oscillator and the reference subcarrier. The output of the Vertical Demodulator

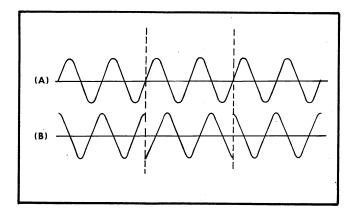


Fig. 3-14. Simplified illustration of demodulator outputs in test circle operation. (A) Horizontal output, (B) Vertical output.

on the CRT, but if there is exactly 90° phase difference between the vertical and horizontal circuits the circles will coincide and appear as one. If during calibration of the instrument the two circles do not coincide, a quadrature adjustment (R588) is provided to adjust the phase difference for exactly 90°.

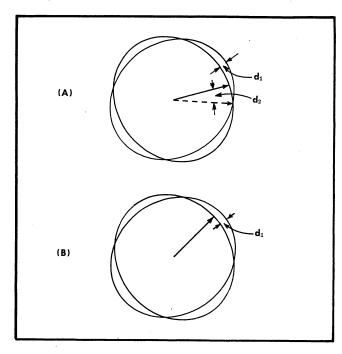


Fig. 3-15. Phase and Amplitude error of vectors when QUAD PHASE is misadjusted. Phase and Amplitude error may be positive or negative depending on whether phase shift between vertical and Horizontal Demodulators is greater or less than 90°.

- (A) Phase error when QUAD PHASE is misadjusted  $(d_1 = d_2)$ .
- (B) Amplitude error when QUAD PHASE is misadjusted. Amplitude error is 1/2 of  $d_1$  and is maximum for vectors along 45°, 135°, 225° and 315° axis.

The misadjustment of QUAD PHASE does not affect vectors lying on the vertical axis, but has its maximum effect on the horizontal axis. The amount of radial separation of the test circles is related to the angular displacement of a vector, lying on the horizontal axis and having an amplitude is shifted in phase 90° with respect to the Horizontal Demodulator output. Fig. 3-14 is a simplified illustration of the phase relationship of the outputs of the Vertical and Horizontal Demodulators in test circle operation. The outputs of the Horizontal and Vertical Demodulators are coupled to the deflection circuits and there will be two circles displayed equal to that of the test circle. The radial separation is equal to the displacement of the vector. Fig. 3-15 illustrates the test circle display when QUAD PHASE is misadjusted. As an example; one degree of error in a vector lying on the horizontal axis having an amplitude equal to the test circle means that the vector is 0.0366 inches (pertaining to Type R520) away from where it should be. If this error were due to a misadjustment of QUAD PHASE, the test circles would have a separation of 0.0366 inches. The angular error would be at a maximum for vectors measuring 0° and 180°. The maximum error in amplitude is one-half the separation of the circles, and would be most prominent for vectors at 45°, 135°, 225° and 315°. In this case, the maximum amplitude error would be 0.0183 inches or 0.9% since the radius of the test circle is 2.096 inches.

Assume that it is desired to display test circles on channel B. The B CAL switch SW55 is actuated and Q425 is turned off (refer to Chrominance Channel Switching for operation of Q420 and Q425). SW55 also connects —15 V to the emitter of Q430 through R432. Q420 is on, so its collector is pulled up which causes the base of Q430 to go positive and turns on Q430. Q430 turning on decreases the positive voltage at the cathode end of D576 and D576 becomes forward biased. The positive bias on Q571 is decreased and the 0° and 180° Switching operates as previously described in the 0° and 180° Switching description.

#### Cal Signal, Line Sweep

The CAL signal available in the LINE SWEEP mode of operation is two horizontal traces separated vertically by 140 IRE units. When either the A CAL or B CAL switch is operated the 0° and 180° switching circuit operates as previously described. The square wave that is developed on the collector of Q570 is coupled through Q580 to the input amplifier circuit. From the input amplifier, it is coupled back into the chrominance channel through either the A or B input line. The CAL signal is then taken off the collector of Q450 through R452 and coupled into the luminance input filter. The network consisting of D580 and C580 delays the turn-on of Q580 to allow the clamps in the Luminance Amplifier and the Vertical Amplifier to always sample the bottom of the CAL square wave. Resistor R583 LUMINANCE CAL in the collector circuit of Q580 is an adjustment used during calibration to adjust for 140 IRE units of vertical separation between the two horizontal traces.

#### FILTER AND HORIZ/VERT DRIVER AMPS

Since the operation of the Vertical and Horizontal Driver Amplifiers is essentially the same, only the operation of the Vertical circuit will be described.

# **Vertical Driver Amplifier**

The demodulated signal from the Vertical Demodulator is coupled into a low pass filter having a 600 kHz bandpass, consisting of L601, C601, L602 and C602. From the low pass filter, it is coupled through the terminating resistor R621 to the base of Q620. Q620 and Q630 form an operational amplifier with a gain of approximately 10. The signal is coupled from the emitter of Q630 to the Vertical Amplifier. An offset current is also coupled to the summing junction of Q620 and Q630 when differential gain measurements are being made. The gain of the Vertical Amplifier is increased during the time of differential gain measurements and the offset current at the base of Q620 maintains the display within the control limits of the deflection circuits. One of the feedback resistors R626 is variable (R-Y GAIN) so the gain of the operational amplifier can be adjusted during calibration. R624 establishes the operating point for Q620 and is adjusted for a 0 V DC output level at the emitter of Q630 during sync time with VECTOR button depressed. C632 is a frequency compensating capacitor.

The GAIN BAL adjustment in the feedback circuit of the Horizontal Driver permits slight adjustment of the horizontal gain from the front panel.

#### **Luminance Driver**

The luminance signal and the luminance CAL signal from the collector of Q450 in the Video Amp is coupled into a low pass filter consisting of L610-L618 and C610-C619. From the low pass filter the signal is coupled through emitter follower Q660 to the gate of FET, Q670. The signal is coupled through the operational amplifier, Q670 and Q680, through R688 to the Vertical Amplifier. R672 (LUM DC BAL) is adjusted during calibration to establish the operating point for Q680 during sync tips. D680 is a protection diode that prevents the base of Q680 from going more positive than +10.6 volts.

The gate of Q670 is referenced to ground during sync tip time by the action of the sync tip blocking oscillator, Q691. The blocking oscillator is triggered by the -H pulse. Assume a quiescent condition, no trigger in. Q690 and Q691 are off and D694 is forward biased through R694. The zener diodes D695 and D696 are conducting through R697 and R698. The voltage at the junction of D695 and R697 is +3 volts, and the voltage at the junction of D696 and R698 is -3 volts. Sampling diodes D697 and D698 are reverse biased.

The -H pulse is coupled to the emitter of Q690 through C690. Q690 is turned on by the leading edeg of the -H pulse. When Q690 turns on, the incoming pulse is clamped at -0.6 V by the base-emitter impedance. Thus, Q690 remains on for a short duration and triggers the blocking oscillator. The current from Q690 into the primary winding of T695 induces a positive voltage into the secondary winding at the junction of D694, and D694 is reverse biased. As D694 is reverse biased the base of Q691 goes positive and Q691 turns on. The center-tapped secondary of T695 is wound in such a manner that the polarity of the induced voltage is positive at the end of the center-tapped secondary connected to D695 during the time Q690 or Q691 is on. D697 and D698 remain reverse biased during the conduction time of Q691. When D694 is reverse biased C695 starts to charge in the positive direction. When the end of C695 that is connected to the anode of D694 becomes approximately 0.6 V more positive than the induced voltage into the secondary winding of T695, D694 is forward biased. When D694 is forward biased, Q691 is turned off. When Q691 turns off, the polarity of the voltage across the center-tapped secondary reverses and the junction of D695 and D697 goes negative. At the same time, the junction of D696 and D698 goes positive. Diodes D697 and D698 are forward biased by the back swing of the blocking oscillator and the gate of Q670 is clamped to ground during sync tip time.

A LUMINANCE GAIN control (R685) is provided as a front panel control. The gain of the luminance channel is adjusted during calibration with SW685 in the CAL or open position, and the luminance signal is coupled through R688. If the front panel GAIN control is operated, SW685 is closed and R688 is shunted. The luminance signal is then divided down through R685 and R687.

#### **VERTICAL AMPLIFIER**

The signals from the Horiz/Vert Driver Amps are coupled into the Vertical Amplifier board. The luminance, R-Y and B-Y signals are matrixed to form the G-Y, red, blue and green signals. The input signal to the Vertical Amplifier is selected by transistors operated as switches. The transistors are controlled by the buttons located on the front panel labeled, VECTOR, LINE SWEEP, Y, I, R, Q, G, DIFF GAIN, B and DIFF PHASE. The output of the Vertical Amplifier is a cascode amplifier which drives the upper and lower deflection plates.

# Signal Switching

The R-Y signal from the Vertical Demodulator is coupled to D716 through R718, to D746 through R745, and to D766 through R765. The B-Y signal from the Horizontal Demodulator is coupled through R728 to D726, and to D756 through R755. This signal is also connected from the input connector to the Horizontal Amplifier. The luminance signal is coupled to D706, D716, D726 and D736 through R705, R715, R725 and R735.

The R-Y and B-Y signals are coupled to the emitter of Q770 through R770 and R771. Q770 and Q780 form an operational amplifier.

The R-Y and B-Y signals are added together through R770 and R771 and coupled into the amplifier to form the G-Y signal on the collector of Q780. The G-Y signal is coupled through R786 to the cathode of D706. D780 in the base circuit of Q780 is a protection diode that clamps the base at  $\pm 10.6\,\mathrm{V}$  when the amplifier is overdriven. D775 sets the base of Q770 at  $\pm 0.6\,\mathrm{V}$  and is for temperature compensation.

Since the switching transistors (Q700, Q710, Q720, Q730, Q740, Q750 and Q760) and the switching diodes (D706, D716, D726, D736, D746, D756 and D766) all operate in the same manner, only the operation of Q710 and D716 will be described. The switching transistors are normally conducting, so the collectors are pulled up and the diodes (D706 - D766) are reversed biased. Assume it is desired to display the red signal. SW710 is pressed and a positive voltage is connected to the base of Q710 through R712, so Q710 is turned off. All of the other switching transistors will remain on. —15 V is connected to the cathode of D716 through R716 and D716 turns on. The R-Y signal is coupled through R718 to the cathode of D716 and the luminance signal is coupled through R715 to the cathode of D716. When the two signals are added algebraically (R-Y + Y) the red signal is produced and coupled through D716 to the vertical amplifier. The

amplitude of the R-Y signal at the input to the Vertical Amplifier board is equal to (R-Y) 2/1.14. To completely cancel out the Y component at the summing point (the cathode of D716), the R-Y signal must be attenuated. This is accomplished by the resistance ratio of R715 and R718.

The resistance values for R725 and R728 have been chosen to completely cancel the Y component when the blue signal is selected. The amplitude of the B-Y signal at the input of the Vertical Amplifier board is (B-Y) 2/2.03.

The amplitude of the G-Y signal on the collector of Q780 is equal to (G-Y) 2/0.71. Therefore, the resistance values for R786 and R705 have been selected to completely cancel the Y component when the green signal is selected.

The gain of the vertical amplifier is increased  $\times 5$  when DIFF GAIN or DIFF PHASE measurements are being made. When either DIFF GAIN or DIFF PHASE is selected, R765 becomes R<sub>i</sub> for the operational amplifier Q830/Q835 in the Vertical Amplifier. The resistance value for R765 is 953  $\Omega$ , while R<sub>i</sub> in the other modes of operation is 4.99 k $\Omega$ .

# **Vertical Amplification**

The signal selected by the switch transistors is coupled to the base of Q830. Q830 and Q835 form an operational amplifier that drives a paraphase amplifier. The vertical gain is adjusted by changing the R<sub>f</sub> of the operational amplifier  $(R_{\rm f}/R_{\rm i}=$  gain). The collector of Q835 drives Q836, which is one half of the paraphase amplifier. The signal on the emitter of Q835 is coupled to the emitter of Q855, which drives the other half of the paraphase amplifier, Q856. The signals appearing on the collectors of the paraphase are about equal in amplitude, but of opposite polarity. The output of Q836 is coupled to the upper deflection plate and the output of Q856 is coupled to the lower deflection plate. L838 and L858 are series peaking coils. Capacitor C848 is adjusted for high frequency response and resistor R849 is used to adjust damping, and is adjusted for the best transient response. Transistor Q840 provides a constant current source for the paraphase amplifier.

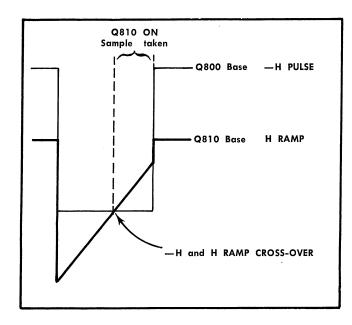


Fig. 3-16. Signals present on Q800 and Q810 bases when deflection plate voltage is sampled.

#### **Vertical Positioning**

During sync tip time, a sample of the output of the paraphase amplifier is taken. If there is any voltage difference, an error signal is coupled to the Vertical Amplifier to balance the outputs and position the CRT trace in the center of the CRT vertically. The front panel VERT POSITION control is in the circuit only when either Y, R, G, B or DIFF GAIN is selected.

The collector of Q856 is coupled to the base of Q870A through R876, and the collector of Q836 is coupled to the base of Q870B through R885. Q870A and Q870B form a differential amplifier with the common mode level of the bases set by R875 Vert Com Mode Lev. D875 and D876 clamp the difference of potential between the bases of Q870A and Q870B at 0.6 volts. Therefore Q870A and Q870B are prevented from being overdriven excessively. The bias on the base of Q870B is set by the adjustment of R880 VERT POSI-TION CLAMP. R880 is adjusted so the spot is in the center of the CRT in VECTOR operation with no input. Q860 is conducting unless either G, R, B, or Y is selected. With Q860 conducting, its collector is positive and D873 is reverse biased. D862 is reverse biased through R864 and D861. With D862 and D873 reverse biased, any voltage change produced by the VERT POSITION control is blocked from the bases of the differential amplifier, and the VERT POSITION control cannot set the position of the trace on the CRT.

The output of the differential amplifier is taken off the collector of Q870B and coupled to a four-diode gate consisting of D805A, B, C and D. Q800 is normally on and its collector is pulled down. Q810 is normally off, so its collector is positive. With Q800 on and Q810 off the charge across C807 and C817 is such that the four-diode gate is reverse biased and the signal from the differential amplifier is not coupled to the gate of Q820. During sync tip time, the -H pulse is coupled to the base of Q800 and the H ramp from the Sweep circuit is coupled to the base of Q810. The -H pulse and the H ramp are coincident with each other. Refer to Fig. 3-16 for the voltage and time relationship of the —H pulse and the H ramp. As the —H pulse and the H ramp step negative, Q800 continues to conduct and remains on during the time the ramp is running up to the cross-over point of the H ramp and the —H pulse. At the cross-over point, the base of Q810 becomes more positive than the base of Q800 and Q810 turns on. As Q810 turns on, its collector goes negative and the collector of Q800 goes positive. The charge then across C807 and C817 forward biases the four-diode gate and the error signal from the collector to Q870B is coupled to the gate of Q820. Q820 is a source follower and the error signal is coupled to the base of Q855. If there is a difference of potential between the upper and lower deflection plates during sample time the current in Q856 is either increased or decreased to balance the output of the paraphase amplifier. When the -H pulse and H ramp steps up, Q810 turns off and Q800 turns on. Thus the diode gate is closed until the next sync tip time.

If either G, R, B, or Y is selected, +10 V is connected to the junction of D861 and R865. D861 is reverse biased and Q860 is turned off. Since D861 is reverse biased, D862 is forward biased through R862; and with Q860 off, D873 is forward biased through R867. The bias on the bases of the differential amplifier can now be changed by the VERT POSITION control and the CRT trace can be positioned vertically.

Q890 is an emitter follower which develops the  $+3\,\mathrm{V}$  supply.

#### HORIZONTAL AMPLIFIER

The Horizontal Amplifier and horizontal positioning circuits operate essentially in the same manner as the vertical circuits. Therefore, the circuit description given for the Vertical Amplifier applies to the Horizontal Amplifier except for circuit numbers.

# Signal Switching

The sawtooth sweep from the Sweep circuit is coupled to the Horizontal Amplifier through D940 except during the VECTOR mode of operation. During VECTOR operation the horizontal video signal from the Horizontal Demodulator is coupled through D944 to the Horizontal Amplifier.

Signal switching is accomplished by Q930. Transistor Q930 is conducting except when SW30 (VECTOR) is actuated. With Q930 conducting, its collector is pulled up and D944 is reverse biased. D940 is forward biased through R934 and the sawtooth voltage is coupled to the Horizontal Amplifier. When SW30 is actuated,  $+10\,\mathrm{V}$  is connected to the junction of R930 and R936, which turns Q930 off. When Q930 turns off, D944 is forward biased through R939 and the horizontal video signal is coupled to the Horizontal Amplifier. The  $+10\,\mathrm{V}$  at the junction of R936 and R930 forward biases D932, and D940 is reverse biased which disconnects the sawtooth voltage from the Horizontal Amplifier.

The HORIZ POSITION control operates in all switch positions except VECTOR. When SW30 is actuated,  $+10\,\mathrm{V}$  is connected to the base of Q1010 through R1016 and Q1010 turns on. When Q1010 turns on, its collector goes negative and D993 is reverse biased.  $+10\,\mathrm{V}$  is also connected to the cathode of D983 through D982, and D983 is reverse biased. With D983 and D993 reverse biased, the HORIZ POSITION control cannot change the bias on the bases of the differential amplifier.

The adjustment for setting the DC level of the -H pulse is in the base circuit of Q900. The adjustment of R905 sets the bias on Q900 and Q800 which determines where the crossover of the -H pulse and the H ramp will occur and the sample of the error signal will be taken.

#### **SWEEP**

#### Sync Separator

The Sync Separator circuit (Q1100, Q1101, Q1110, Q1115) removes the video information from the composite video signal, leaving sync with sync tips clamped at a certain voltage level. This circuit is an operational amplifier that has three possible feedback paths:

- 1. From the collector of Q1101 through Q1115 baseemitter junction, D1110, Q1110 base-emitter junction, and R1101 to the base of Q1100. This is the primary feedback path under no-signal quiescent conditions.
- 2. From the collector of Q1101 through R1116, R1114, Q1110 base-emitter junction, R1102 and C1102 to the base

of Q1100. This path is shunted by R1108. This parallel circuit is the primary feedback path when the signal is applied to the base of Q1100. During sync pulse transitions (leading and trailing edges), the dominant feedback path is through R1108 which gives maximum circuit gain.

3. From the collector of Q1101 through D1106 and D1105 to the emitter of Q1100. Although these diodes are primarily anti-saturation diodes, they can be considered as a local feedback path when both diodes are on and the signal is not at the sync tip level.

To understand the circuit operation, first assume a quiescent condition with no input signal. All the transistors are conducting and the voltage at the emitter of Q1100 is about  $+0.6\,\text{V}$ . With Q1101 on, the voltage at the collector of Q1101 is about  $+3.4\,\text{V}$ . Thus, D1105 is forward biased; D1106 reverse biased. The voltage at the base of Q1100 is about 0 V and about 150  $\mu\text{A}$  of current is flowing through R1103 and the parallel combination of R1101 and R1108. This sets the emitter voltage of Q1110 at about  $+3.2\,\text{V}$  and the base voltage is at  $+3.8\,\text{V}$ . C1114 charges to the positive DC level at the base of Q1110. With Q1115 on and its base at the same voltage as Q1101 collector, the emitter voltage of Q1115 is at  $+4.1\,\text{V}$ . This voltage enables D1110 to be slightly forward biased to maintain the charge on C1114.

Assume that a sync-negative composite video signal has been applied to the base of Q1100. Under this condition, D1110 is reverse biased between sync pulses. As the leading edge of the sync pulse goes in the negative direction, the emitter of Q1100 tends to go negative, causing the collector of Q1101 to go in the positive direction. D1110 becomes forward biased to provide a charge path for C1114. The feedback path is from the collector of Q1101 through R1116, R1114, Q1110 base-emitter junction, R1102 and C1102 to the base of Q1100. This path is shunted by R1108. This parallel-connected feedback path establishes the sync tip clamp level by providing the DC operating level for Q1100. This operating level shifts with the average picture level and is controlled by the charge of C1114.

As the trailing edge of the negative-going sync pulse at the base of Q1100 starts going in the positive direction, the collector of Q1101 starts in the negative direction. When the collector voltage of Q1101 goes slightly more negative than the charge of C1114, D1110 becomes reverse biased.

When the collector and base voltage of Q1101 become equal, D1106 is forward biased. This diode prevents Q1101 from saturating and returns the collector of Q1101 to approximately +0.7 V between sync pulses when the signal is not at the sync tip level. Only a small fraction of the positive-going video at the base of Q1100 will appear at the output of Q1101 (at TP1101). Thus, the output signal will be positive-going sync pulses approximately 3.5 volts peak to peak in amplitude, with the video greatly attenuated. Because of the state of D1110 during the sync pulse transitions, R1108 is the dominant feedback path during these intervals and the circuit has high gain.

DC restoration is accomplished by the RC combination of C1114 R1114, C1116 and R1116 with diode D1110. Also, any hum content of the incoming signal will always go through the feedback path consisting of R1101, C1114, R1114, C1116 and R1116. Any hum appearing at the input is thus greatly reduced on the restored output. Noise with a peak-

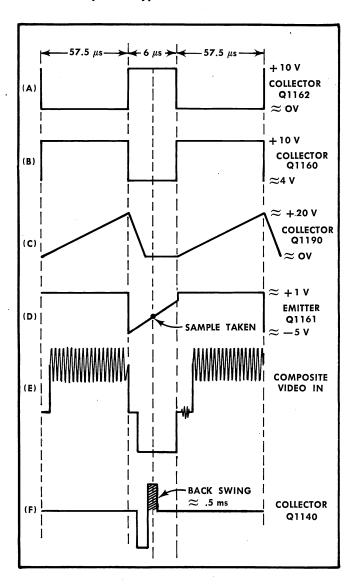


Fig. 3-17. Time relationship of signals present in Miller sawtooth generator.

to-peak amplitude slightly less than the amplitude of the incoming sync will not influence the operation of the circuit. Sharp transients greater in amplitude than sync will not affect the operation of the circuit because of the action of Q1115.

The video stripped sync pulse is applied to the base of the Sync Comparator circuit consisting of Q1120 and Q1121. Q1121 has its base set at —2 V by divider resistors R1128 and R1129. Q1121 is normally conducting, and the level shift across R1118 and R1120 during the video portion of the incoming signal is not sufficient to cause Q1120 to conduct. As the positive-going sync pulse at the collector of Q1101 is applied to the base of Q1120 through the level shifting divider consisting of R1118 and R1120, Q1120 turns on when the level reaches —2 V. This corresponds to a level midway between sync tip and blanking level. Then the signal appearing on the collector of Q1120 is a clean (noise free) sync pulse 0 to —1.6 V in amplitude. The use of this pulse will be discussed in the Miller Integrator description for the Field Selector circuit.

#### Miller Sawtooth Generator

The purpose of the Miller sawtooth generator is to generate a continuous chain of H rate pulses and a sweep at the television horizontal rate (63.5  $\mu$ s in the NTSC). The H rate pulses are used as clock pulses to trigger other circuits in the Type R520. The Miller sawtooth generator is free running in the absence of incoming sync.

The complete Miller sawtooth generator is composed of the following circuits: Multivibrator, Miller runup, blocking oscillator, and a comparator circuit. During the following circuit description, constant reference to Fig. 3-17 will aid in understanding the sequence of events.

Transistors Q1160, Q1161, and Q1162 are the active devices of the multivibrator. The timing capacitor and resistor for the multi are C1164 and R1165.

Assume that there is no sync input and the Miller circuit is in its free running state. Q1162 begins to conduct and Q1160 turns off with its base clamped at —0.6 volts by D1160. The negative-going signal on the collector of Q1162 is coupled through the gating emitter-follower Q1180 to the anodes of D1190 and D1192, the disconnect diodes for the Miller runup generator Q1190.

The timing capacitor and resistor for the Miller circuit are C1190 and R1190. To understand Miller Runup operation, assume no current through R1152. When a negative-going signal from the collector of Q1162 is applied to the anodes of D1190 and D1192 through Q1180, the diodes become reverse biased and C1190 charges through R1190. This produces a positive-going ramp at the collector of Q1190, which is fed back through a resistive divider (R1160/R1161) to the base of Q1160 in the multivibrator. When the ramp at the collector of Q1190 reaches about +20 volts, Q1160 turns on and its collector goes from  $+10\,\mathrm{V}$  to about  $+4\,\mathrm{V}$ . This negative-going signal forward biases D1164 and the signal is coupled through Q1161, turning Q1162 off so that its collector goes positive. This positive-going signal is coupled through emitter-follower Q1180 to the anodes of D1190 and D1192, forward biasing D1192. With D1192 forward biased, C1190 begins to discharge and the runup of the ramp is terminated. When the collector voltage of Q1190 approaches the voltage on the base end of C1190, diode D1190 turns on and clamps the collector of Q1190 to its base. In this free running state (no incoming sync) the time duration of the runup will be about 61  $\mu$ s.

The ramp will not run up again until Q1162 turns on, and Q1162 is controlled by the time constant of C1164 and R1165. When the collector of Q1160 goes negative, this produces a negative-going step on the end of C1164 connected to D1166, which reverse biases D1166. With D1166 reverse biased, C1164 charges through R1165. Since R1165 is connected to  $+100\,\mathrm{V}$ , the positive-going ramp produced by C1164 is essentially linear. When the potential at the base of Q1161 approaches about 0 volts, Q1162 is turned on through Q1161. This turns off Q1160, and as the collector of Q1160 starts positive, D1164 is reverse biased. D1166 clamps the base of Q1161 to about  $+1\,V$ . With D1164 reverse biased, C1164 is disconnected from the collector of Q1160. The collector voltage of Q1160 steps quickly to +10volts, since C1164 does not have to discharge through R1163. The time duration of the positive-going step waveform on the collector of Q1162 is 6 µs, which determines the rundown and clamp time of the Miller (67  $\mu s$  in the free running state).

A +H pulse is available at the collector of Q1162, a -H pulse at the collector of Q1160, and a -H ramp at the emitter of Q1161. The +H pulse is coupled to other circuits through emitter follower Q1170. The -H pulse is coupled through emitter follower Q1200 to other circuits in the Type R520.

An AFC circuit is used to establish the frequency of the sweep from the Miller circuit at the television line frequency. The AFC circuit times the sweep to start at the beginning of each television line.

The circuit consists of coincident emitter follower Q1130, a blocking oscillator Q1140, which generates a gate to sample a portion of the —H ramp created by C1164 in the Gating Multi, and a Comparator circuit that increases or decrease the charging current of C1190 in the Miller circuit. As the charging current of C1190 is changed, the positive-going ramp will either speed up or slow down in time.

During the time a +H pulse is not present on the emitter of Q1170, D1178 is forward biased through R1174 and R1127 to ground. Q1130 is normally conducting slightly, with its base held at ground (or slightly negative) by R1127 and D1178. Any positive-going signal appearing on the base of Q1130 during the absence of the +H pulse will be coupled through D1178, and will not trigger the blocking oscillator. This action rejects most noise signals and greatly improves noise pulse immunity. Also, if a +H pulse occurs in the absence of a sync pulse, D1178 is reverse biased and the blocking oscillator is not triggered. Now, assume a sync pulse is present at the base of Q1120 coincident with the +H pulse on the emitter of Q1170. This turns Q1120 on and Q1121 off. When Q1121 turns off, a positive pulse is developed on its collector which is differentiated by C1126 and R1127. Since D1178 is reverse biased by the +H pulse, the positive spike is coupled through Q1130 and triggers the blocking oscillator which is normally non-conducting.

The waveform appearing on the collector of Q1140 is transformer-coupled to the center-tapped secondary of T1140. Zener diodes D1142 and D1144 keep D1143 and D1145 reverse biased, so there is normally no current flow in D1143 and D1145. During the time the blocking oscillator is conducting, the initial negative portion of the waveform increases the reverse bias on D1143 and D1145 and the loop remains open. During the backswing of the oscillator, the polarity of the voltage across the center-tapped secondary reverses to forward bias D1143/D1145 and the loop is closed. Also coupled in through the center tap of the secondary is the negative-going ramp generated in the multi. Refer to Fig. 3-17. During the backswing a narrow sample is taken which charges the memory capacitor C1150 to the value of the ramp voltage appearing at the center-tap during sample time. At the completion of the backswing of the blocking oscillator, D1143 and D1145 are again reverse biased by D1142 and D1144. There is no signal current flowing in the base circuit of Q1140 during the backswing of the oscillator, as the backswing reverse biases D1135 and disconnects the base of Q1140.

The Comparator circuit consisting of dual FET Q1150 is supplying a small percentage of timing current to C1190. With the sweep running at the correct rate (63.5  $\mu$ s), the sample of the ramp taken by the blocking oscillator will ap-

pear at the same voltage level each time, and the memory capacitor C1150 will acquire a charge representing the ramp level attained at the time of the sample. The Comparator then will supply its specified amount of timing current. Now, assume that the sweep from the Miller is running too fast. This will cause the sample of the ramp from C1164 to be taken later, at a more positive level. The gate of Q1150 and the charge on C1150 will go in the positive direction, turning Q1.150A on harder. Increased conduction of Q1150A decreases the conduction of Q1150B, which decreases the timing current to C1190 and causes the sweep to slow down, returning to 63.5  $\mu$ s.

The DC gain of the comparator loop is quite high to combat drift, while the AC signal gain is less than unity to prevent oscillatory action of the AFC circuit. The AC signal gain is reduced by R1153 and C1153 forming a signal current divider with R1152. For a 1  $\mu s$  error in sweep frequency, approximately 6  $\mu A$  of error current from the Comparator is required to restore the sweep to the correct frequency. The Burst Flag Timing control R1158 sets the voltage level on the gate of Q1150B and, in turn, the voltage level of the negative ramp at which the sample is taken. This adjustment determines the time relationship between the H pulse and incoming sync.

The Miller Sawtooth Generator has generated a positive H pulse, a negative H pulse, a negative H ramp, and a sweep, each with a rate of  $63.5 \,\mu\text{s}$ , with the start of each referenced by the incoming sync pulse. Refer to Fig. 3-17 for a time relationship of the Miller sawtooth generator signals.

# Miller Integrator

The Miller Integrator is designed to integrate the vertical sync pulse and produce (at the collector of Q1255) an integrated sawtooth which starts at 0 V and rises in amplitude to about positive 20 volts. The timing resistor and capacitor for the Miller Integrator are R1254 and C1252.

The negative-going sync pulse from the collector of Q1120 is coupled through a current transfer transistor Q1250 to the anodes of D1252 and D1253. The negative-going pulse on the collector of Q1250 reverse biases D1252 and D1253, and C1252 charges through R1254. The time duration of the horizontal sync pulse is not sufficient to allow the charge of C1252 to attain any appreciable level. During the vertical sync group, D1252 and D1253 are reverse biased for a sufficient duration so that C1252 attains the desired charge. During the vertical serration time, C1252 will discharge only a slight amount through R1253. At the end of vertical sync time the signal at the collector of Q1255 is a positivegoing ramp whose peak corresponds to the end of the vertical sync group. After the collector of Q1250 has gone positive and sync pulse ends, D1253 will be forward biased, discharging C1252 through R1253. The recovery of the sawtooth voltage is disconnected from the sync circuit by Q1250. As the charge on both sides of the capacitor becomes equal, D1252 will be forward biased. This stops the rundown. The capacitor will remain essentially in this condition until the next vertical sync pulse.

The sawtooth voltage at the collector of Q1255 is applied to a peak detector consisting of D1256, C1259, R1259, R1270, D1270 and the base-emitter junction of Q1270.

When the Type R520 is turned on, C1259 acquires an initial charge, with the end connected to the cathode of

#### Circuit Description—Type 520/R520 NTSC

D1256 being positive. As the ramp developed on the collector of Q1255 goes in the positive direction, diode D1256 becomes forward biased when its anode voltage exceeds the charge of C1259. When D1256 becomes forward biased, some of the current that was flowing through R1270 is used to charge C1259. As the sawtooth voltage starts in the negative direction and the charge on C1259 exceeds the anode voltage of D1256, the diode becomes reverse biased and C1259 can no longer charge. The signal developed on the base of Q1260 is a positive-going signal whose amplitude is determined by the current change through R1270, corresponding in time to the peak of the integrated waveform on the collector of Q1255. The time constant of R1259 and C1259 is sufficiently long that C1259 can discharge only a slight amount before the next vertical sync group. The DC level at the end of the capacitor connected to Q1260 is approximately 0 volts.

This level remains constant because of temperature compensating diode D1270 and the base-emitter junction of Q1270.

# Field Rate Multivibrator

The Field Rate Multi, Q1260 and Q1265, generates a pulse to preset the Line Selector J-K flip flops and to trigger the Field J-K flip flop. The duration of the pulse from the multi extends for approximately 27 television lines. Below SN B150100, the pulse duration is approximately 20 lines.

The Field Rate Multivibrator is a monostable multi, and Q1265 is normally conducting. The timing resistor and capacitor for the multi are R1265 and C1263. With Q1265 conducting, the end of the capacitor connected to Q1260 is at +10 V and the end connected to the base of Q1265 is at 0 V. The base voltage of Q1265 is clamped by D1265 and D1266, which are also temperature-compensating diodes.

When the positive-going pulse from the peak detector is applied to the base of Q1260, the multi switches states and Q1260 turns on. This causes its collector to go in the negative direction to approximately +3.5 volts. This negative-going signal is coupled to the base of Q1265, turning Q1265 off. With Q1260 conducting and Q1265 off, the capacitor charges through R1265. When the charge on C1263 increases enough to overcome the bias on Q1265, the multi switches states, turning Q1265 on and Q1260 off. The multi remains in this condition until the arrival of the next positive-going pulse at the base of Q1260. The signal at the collector of Q1260 is a negative-going pulse whose leading edge is approximately coincident with the ending of the vertical sync group, and whose duration is equivalent to 27 horizontal lines of either field. Below SN B150100, the pulse duration is 20 lines.

This negative-going pulse is coupled (and has its level shifted) through emitter follower Q1290 to pin 6 of U1320, U1330, U1340, U1350, and U1370, the preset input of the Line Selector J-K flip flops. The pulse is also coupled to pin 2 of U1310, the trigger input of the Field J-K flip flop. Below SN B150100, omit U1370.

#### Field One Multivibrator

The Field One Multi consists of Q1280 and Q1285, with Q1285 normally conducting. The multi develops a positive-going pulse on each even field. This pulse is used to turn on either Q1300 in the Field Selector circuit, or to preset the Field J-K flip flop. Q1270 is an AND gate or coincidence amplifier whose output is used to trigger Field One Multi.

The positive-going integrated waveform that was developed and peak-detected from the vertical sync group is available at the base of Q1260. This signal is coupled through D1270 to the emitter of Q1270. The +H pulse is coupled from emitter follower Q1170 through R1176 to the emitter of Q1270. Q1270 is biased so that it requires coincidence of the +H pulse and the peak-detected signal to turn it on. Since the odd field (field two) starts with  $\frac{1}{2}H$  and the even field (field one) starts with a full H, coincidence will only occur on the even field.

When Q1270 is turned on, its collector goes positive, turning on Q1280. As Q1280 is turned on, the multi changes states and Q1285 is turned off. The collector of Q1285 goes positive. With Q1280 conducting the base end of C1283, the timing capacitor for the multi, charges through R1285 in a positive direction. When the charge on C1283 becomes sufficiently positive to overcome the bias on Q1285, transistor Q1285 turns on and the multi is returned to its stable state. The resulting signal on the collector of Q1285 is a positive-going pulse whose duration is equivalent to line 6 through approximately line 22, occurring only on the even field. Below SN 150100, the pulse duration is equivalent to line 7 through approximately line 17.

The multi is clamped and temperature-compensated by diodes D1285 and D1286. D1275 clamps the base of Q1280 to about  $-0.6\,\mathrm{V}$  when there is not coincidence between the  $+\mathrm{H}$  pulse and the peak-detected signal from the vertical sync group.

#### Field Selector

The Field Selector circuit is composed of Q1300, U1310 (a J-K flip flop), and diodes D1310, D1312, D1314, D1316, and D1318. D1310 and D1314 are each connected to one of the VITS Line Selectors, and operates in conjunction with the Line Selector diodes in determining when the CRT will be unblanked. By an arrangement of pin connectors, either VITS line can be connected to the same field. To unblank the CRT for either VITS line, all the diodes connected to that line must be reverse biased. Below SN B150100, omit D1312, D1316 and D1318.

The J-K flip flop used in the Field Selector is the same type as the ones in the VITS Line Selector. Pins 5 and 7 are the output pins, pin 2 receives the trigger pulse and requires a negative going trigger. The preset pin is pin 6 and it must be low to enable the multi to change states when a trigger pulse is applied. In the preset condition if pin 6 has a high applied, pin 7 is low.

Assume the Field Switch SW1305 is in the 2 position, and —15 volts is now applied through R1302 to the base of Q1300, which is sufficient to reverse bias Q1300. This negative voltage is also applied to pin 6 of U1310 through the voltage divider, and the multi is released to change states if it receives a negative-going trigger on pin 2.

The positive-going pulse from the collector of Q1285 in the Field One Multi is applied to pin 6 of U1310 through R1307, which causes pin 7 to go low and pin 5 high. Simultaneously, the negative-going pulse from the Field Multi is coupled through Q1290 to pin 2 of U1310. Thus, pin 7 is low on the even field. The positive-going pulse from Q1285 is also applied to the base of Q1300, but is not of sufficient amplitude to forward bias Q1300. As the next field pulse from Q1290 is applied to pin 2 of U1310, the multi changes states and pin 7 goes high. The positive-going pulse from Q1285 is absent at this time, as the field pulse is occurring on an odd field or field two. From the foregoing sequence of events, it can be determined that the even field pulse insures pin 7 is low on each even field.

# SN B150100 and up.

The diodes in the output lines of U1310 can be pin connected to either VITS 18 or VITS 19. When either VITS button is pressed, —15 volts is connected to that line and the diodes connected to the selected line are forward biased through R1319 to +10 volts. When a low occurs on either output pin of U1310, this puts an effective ground on that pin. If the diodes in the output line are forward biased, then the effective ground is coupled through the diodes, through D1359 (which is forward biased unless the FULL FIELD switch is pressed), to the base of the Unblanking Amplifier, Q1220. This turns Q1220 off and the CRT is blanked. When a high occurs on the selected output pin of U1310, Q1220 is turned on and the CRT is unblanked.

#### **BELOW SN B150100**

If either D1310 or D1314 is connected to pin 5, the diode is reverse biased at this time and the associated VITS line is selected on field one. If either of the diodes is connected to pin 7 it is reverse biased on the odd field and its associated VITS line is selected.

By changing SW1305 to the 1 position, the reverse bias on Q1300 is decreased and pin 6 of U1310 is pulled farther in the negative direction. Now, as the even field pulse from Q1285 occurs it is sufficiently positive to forward bias Q1300, but is not sufficient to overcome the negative voltage on pin 6 of U1310. On each even field pulse, Q1300 turns on and pin 5 of U1310 is pulled low. The multi will operate as previously explained, except now each time an even field pulse occurs, pin 5 of U1310 is low and pin 7 is high. Table 3-1 shows the condition of pins 5 and 7 as related to field one and two with SW1305 in position 1 and 2.

TABLE 3-1

(A) SW1305		
Position 2	Field 1	Field 2
Pin 5/U1310	Н	L
Pin 7/U1310	L	Н
(B) SW1305 Position 1	Field 1	Field 2
Pin 5/U1310	L	Н
Pin 7/U1310	Н	L

# **Line Selector Matrix**

#### SN B150100 and up.

The Line Selector Matrix is composed of J-K flip flop integrated circuits U1320, U1330, U1340, and U1370 with their associated diodes. The integrated circuits are used as binary counters to supply either a high or low through the gating diodes to the base of the Unblanking Amplifier (Q1220). The diodes are connected in such a manner that any line from line 7 through line 22 of either field can be selected. The line pre-selection is accomplished by an arrangement of pin connector jumpers on the Sweep board and by front-panel pushbuttons.

The J-K flip flops used in the Line Selector are connected in such a manner that pins 5 and 7 are the output, pin 6 is the preset and pin 2 receives the clock pulse or the trigger. Pin 2 requires a negative-going clock pulse to flip the counter from one state to the other. A high on pin 6 presets pin 7 low, and the counter is locked in this condition. If pin 2 receives a clock pulse at this time, the counter will not change states. When pin 6 is changed to a low, the counter is released to change states but will not flip until pin 2 receives a clock pulse.

The negative preset pulse from the emitter of Q1290 is coupled to pin 6 of the counters, and pin 7 is low. The low on pin 6 of the counters releases them to change states, but they will not do so until pin 2 of each counter receives a negative-going clock pulse.

The —H pulse, which is occurring at the television line rate, is coupled through Q1200 to pin 2 of the ÷2 counter (U1350). Upon the arrival of the first —H pulse after the counters are released, U1350 will change states. When U1350 flips, pin 5 goes high. This applies a high to pin 2 of U1340 and since the flip flops require a negative-going clock pulse, the multi will not change states and the remaining counters will stay in their preset condition. When the next —H pulse arrives at pin 2 of U1350, the multi changes states and pin 5 goes low. A negative-going clock pulse is now applied to pin 2 of U1340 and the ÷4 counter changes states, which causes pin 5 to go low. The signal (low) on pin 5 of U1340 is coupled to pin 2 of the  $\div$ 8 counter (U1330) which changes states, pulling pin 5 low. The low on pin 5 of U1330 is coupled to pin 2 of the  $\div$  16 counter (U1320), causing it to flip and changing pin 5 of U1320 to the low state. This, in turn, is coupled to the  $\div$  32 counter (U1370) which changes states and results in a low on pin 5 of U1370.

By referring to Table 3-2, a truth table for the  $\div$ 2 (U1350),  $\div$ 4 (U1340),  $\div$ 8 (U1330),  $\div$ 16 (U1320),  $\div$ 32 (U1370) counters, the condition of the output pins can be readily determined as each successive —H pulse is applied to pin 2 of U1350. When the Field Rate Multi changes states again (after approximately 27 television lines) the collector of Q1260 goes in the positive direction and the counters are restored to their preset condition.

The diodes connected to the output pins of the line counters can be pin-connected to either VITS 18 or VITS 19, to pre-select a television line to be displayed when either VITS button is pressed. When a VITS button is pressed, —15 volts is connected to the output of the counters that are pin-connected to that VITS line. The diodes connected

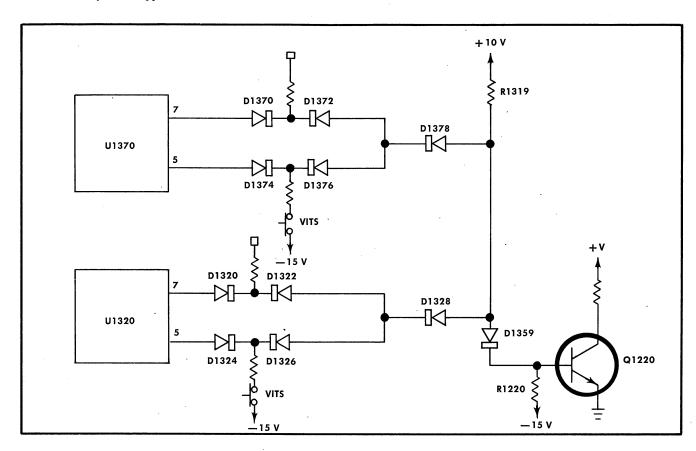


Fig. 3-18. Simplified drawing of the Line Selector circuit.

to the output pins of the counters are then forwarded biased through R1319 to +10 volts. D1359 is foward biased at all times unless the FULL FIELD switch is pressed in.

Fig. 3-18 is a simplified drawing of the Line Selector circuit illustrating the operation with only two counters.

Referring to Fig. 3-18, assume pins 5 of U1320 and U1370 are pin-connected to a VITS line. Diodes D1374, D1376, D1378 of U1370 and diodes D1324, D1326, D1328 of U1320 become forward biased. D1370/D1372 and D1320/D1322 are reverse biased since they are not connected to a VITS line. D1359 is forward biased. First, assume pin 5 of U1320 is low and pin 5 of U1370 is high. When a low occurs on the output pin of a counter, an effective ground is established on that pin. Since D1324, D1326, D1328, and D1359 are forward biased, the ground appearing on pin 5 of U1320 also appears at the base of the Unblanking Amplifier, Q1220. Therefore the transistor is off, its collecter is up and the CRT trace is blanked. Now, assume U1320 receives a clock pulse and the counter multi switches states; this causes pin 5 to go high and pin 7 low. U1370 does not receive a clock pulse, therefore the counter does not flip. Since pins 5 of both U1320 and U1370 are high, a high is coupled through the diodes to the base of the Unblanking Amplifier, which turns the transistor on. The collector of Q1220 is pulled down and a negative-going pulse is coupled to the CRT, which unblanks the trace. The CRT will remain unblanked until the next clock pulse causes the counters to change states. The remaining counters in the Line Selector circuit operate in the same manner as just described for U1320/ U1370. A high is required on all the output pins that are connected to the selected VITS line before the Unblanking Amplifier will turn on and unblank the CRT trace.

By referring to Table 2-8 and Table 2-9 in Operating Instructions, television lines 7 through 22 can be preselected to be displayed on either VITS 18 or VITS 19.

When the FULL FIELD switch (SW1314) is pressed, +10 volts is connected to the base of Q1220 through R1209, which turns the transistor on and also reverse biases D1259. The transistor is turned off during sweep retrace time by the —H pulse which is coupled to its base through C1204.

# Line Selector Matrix BELOW SN B150100

The Line Selector Matrix is composed of J-K flip flop integrated circuits U1320, U1330, U1340, U1350 with diodes D1320, D1324, D1330, D1334, D1340, D1344, D1350, D1354 and D1360/D1362. The integrated circuits are used as binary counters to either forward or reverse bias the diodes, which in turn control the Unblanking Amplifier, Q1220. The diodes are connected so that any line from line 7 through line 14 or line 15 through line 21 of either television field can be pre-selected. Refer to Tables 2-10 and 2-11 in Section 2 of this manual. The pre-selected line selection is accomplished by an arrangement of pin connectors on the Sweep board and by front panel pushbuttons.

**TABLE 3-2**SN B150100 and up

		VI	TS I	line	Sele	ctor	Tru	h T	able	for	Pin	5							
No. of —H												,							
Pulses	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19
÷2 (U1350)	L	Н	L	Н	L	Н	L	Η	L	Н	L	Н	L	Н	L	Н	L	Н	L
÷4 (U1340)	L	L	Η	Н	L	L	Н	Τ	L	L	Н	Н	L	L	Н	Н	L	L	Н
÷8 (U1330)	L	L	L	L	Н	Н	Н	Τ	L	L	L	L	Ĥ	Н	Н	Н	L	L	L
÷16 (U1320)	L	L	L	L	L	L	·L	L	Н	Н	Н	Н	Н	Н	Н	Н	L	L	L
÷32 (U1370)	L	L	L	L	L	L	L	L	L	L	L	L	L	L	L	L	Н	Н	Н
TV Line	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25

The J-K flip flops used in the Line Selector are connected in such a manner that pins 5 and 7 are the output, pin 6 is the preset and pin 2 receives the clock pulse or the trigger. Pin 2 requires a negative-going clock pulse to flip the counter from one state to the other. A high on pin 6 presets pin 7 low, and the counter is locked in this condition. If pin 2 receives a clock pulse at this time the counter will not change states. When pin 6 is changed to a low, the counter is released to change states but will not flip until pin 2 receives a clock pulse.

The anodes of D1324, D1334, D1344 and D1354 are connected together to control one VITS Line Selector, and D1320, D1330, D1340 and D1350 control the other VITS Line Selector. When all the diodes in the selected line are reverse biased, a positive voltage forward biases either D1360 or D1362, causing the base of Q1220 to go in the positive direction. This turns on the Unblanking Amplifier, which unblanks the CRT.

By referring to Table 3-3 which is a truth table for the  $\div 2$  (U1350),  $\div 4$  (U1340),  $\div 8$  (U1330) and  $\div 16$  (U1320) counters, the Line Selector circuit can be more easily understood.

For the following sequence of events assume D1324, D1344 and D1354 are pin-connected to pin 5 of their respective counters and D1334 is connected to pin 7 of U1330. Switch SW1310 is in the on position, which applies +10 V to one end of R1310. (With D1324, D1334, D1344 and D1354 connected in this manner television line 18 is to be selected.) Assume D1314 is reverse biased.

The negative-going pulse from the collector of Q1260 in the Field Multi is coupled through emitter follower Q1290 to pin 6 of the Line Selector J-K flip flops. The counters are released to change states during the entire duration of the pulse which is from line 7 through line 27 or line 7 through 19 of the television field. The -H pulse from Q1160 in the Gating Multi is coupled through emitter follower Q1200 to pin 2 of U1350. With a negative-going clock pulse at pin 2, U1350 changes states and pin 5 goes low. The output of pin 5 is connected to D1354 and pin 2 of U1340. A low on pin 2 of U1340 causes it to flip, so pin 5 of U1340 goes low. Pin 5 of U1340 is connected to D1344 and to pin 2 of U1330. A low on pin 2 of U1330 causes it to change states and pin 5 to go low, which causes U1320 to flip. This puts a low on pin 5 of U1320. A low on the output pin of U1320, U1330, U1340 or U1350 puts an effective ground at the cathode end of the diode connected to that pin. Since SW1310 is on, there is +10 volts through R1310 to the anodes of D1324, D1334, D1344 and D1354. With an effective ground at the cathodes of D1324, D1344 and D1354 they are forward biased. This establishes an effective ground at their anodes which reverse biases D1360. This keeps Q1220 turned off and prevents the CRT from being unblanked. D1334 is connected to pin 7 of U1330 and pin 7 is high at this time; therefore, D1334 is reverse biased. When the second —H pulse appears at pin 2 of U1350, the multi flips and pin 5 goes high. Since the J-K's require a negative trigger, the ÷4 counter can not change states and the ÷8 and ÷16 counters do not receive a trigger. By referring to Table 3-2, the condition of the output pins of U1320, U1330, U1340, and U1350 can be readily determined as each successive —H pulse is applied to pin 2 of U1350.

Continuing through the sequence of -H pulses to the twelfth one after the J-K flip flops were released, (which corresponds to television line 18) it is found that the cathodes of D1324, D1334, D1344 and D1354 all have a high applied to them. Therefore, the diodes are reverse biased and  $+10\,\mathrm{V}$  is applied through R1310 and D1360 to the base of Q1220, forward biasing Q1220. The collector of Q1220 is pulled down and the CRT is unblanked. Q1220 remains on

TABLE 3-3 BELOW SN B150100

VITS Line Selector Truth Table for Pin 5															
No. of —H															
Pulses	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
÷2	L	Н	L	Н	L	Н	L	Н	L	Н	L	Н	L	Н	L
÷4	L	L	Н	Н	L	L	Н	Н	L	L	Н	Н	L	L	H <sub>.</sub>
÷8	L	L	L	L	Н	Н	Н	Н	L	L	L	L	Н	Н	Н
÷16	L	L	L	L	L	L	L	L	Н	Н	Н	Н	Н	Н	Н
TV															
Line	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
	Pin Combination														
÷2	7	5	7	5	7	5	7	5	7	5	7	5	7	5	7
÷4	7	7	5	5	7	7	5	5	7	7	5	5	7	7	5
÷8	7	7	7	7	5	5	5	5	7	7	7	7	5	5	5
÷16	7	7	7	7	7	7	7	7	5	5	5	5	5	5	5

until the arrival of the next —H pulse from Q1200 which forward biases D1208 and turns Q1220 off, blanking the CRT during the retrace time of the sweep.

The usable lines that can be selected are limited by the duration of the negative pulse applied to pin 6 of the multis, which releases the J-K's to change states from line 7 through line 27, or line 7 through line 19. Therefore, the usable lines are 7through 14 or 15 through 21.

# **Unblanking Amplifier**

The Unblanking Amplifier is composed of Q1220 and Q1230. A negative-going unblanking pulse from the collector of Q1220 is applied to the unblanking plates of the CRT. Q1230 applies a positive-going signal to the CRT grid during the unblanking time.

Q1220 is forward biased by either the VITS Line Selectors or the FULL FIELD Switch (SW1314), and is reverse biased by the -H pulse during sweep retrace time. The collector of Q1220 is limited to +100 volts by D1225. D1220 and D1222 prevent Q1220 from saturating, thereby eliminating the storage time effects of a saturated transistor.

The negative-going unblanking pulse from the collector of Q1220 is AC coupled to the base of Q1230, an operational amplifier. For full field operation, the average level at the base of Q1230 during each television line holds the collector of Q1230 at a given level. During VITS the change in duty cycle of the unblanking waveform at the collector of Q1220 produces a large negative pulse at the base of Q1230. This produces a positive pulse on the collector of Q1230 which is AC coupled to the CRT grid as a VITS intensifying pulse. Diodes D1235 and D1239 limit the swing of Q1230's collector from about  $-0.6\,\mathrm{V}$  to  $+40\,\mathrm{V}$ . R1233 and C1233 compensate for the time constants in the CRT grid circuit.

A negative-going burst intensification pulse is coupled to the base of Q1230 through R1216 during burst time, which causes the collector of Q1230 to become more positive during burst, thus intensifying burst. A Z axis input to the base of Q1230 is available to externally intensify any portion of the sweep. Because the grid of the CRT is AC coupled, this input should be used for short duration pulses only.

Q1210 provides a DC coupled input to the Unblanking Amplifier Q1220, and is used to blank (or unblank) the CRT for extended time periods.

# **CRT CIRCUIT**

The CRT Circuit provides the high voltage necessary for operation of the cathode ray tube (CRT). The control circuits for controlling the electron beam and the power supply for the integrated circuits are contained in the CRT circuit.

#### High Voltage Oscillator

Q1420 with its associated circuitry is operated as a class C oscillator to produce the drive for the high voltage transformer T1450. The amplitude of the high voltage oscillations is controlled by a sensing circuit consisting of Q1400, Q1410, and the sensing winding (center-tapped primary) of T1450.

As the equipment is turned on, a negative voltage is applied to the base of Q1400 through R1402, and Q1400 satur-

ates. The collector of Q1400 is pulled up near ground and Q1410 saturates, allowing R1414 to supply base drive to Q1420. This turns on the High Voltage Oscillator. D1414 is reversed biased as the oscillator is turning on. As the amplitude of the oscillations fed back from the collector winding to the base winding of T1450 increases, the collector of Q1410 becomes more negative until D1414 is forward biased. When D1414 becomes forward biased, the available base drive to Q1420 increases. As the amplitude of the oscillations increases, a voltage is induced into the sensing winding of T1450. The induced voltage is coupled through C1438 to a voltage doubler circuit consisting of D1432, D1436, C1433 and C1436. The voltage developed across C1433 at the cathode end of D1432 is coupled to the base of Q1400. The signal is coupled through Q1400 to emitter follower Q1410. The emitter of Q1410 is coupled to the base of Q1420 to control the amplitude of the high voltage oscillations. The frequency response of the feedback loop is compensated by R1430 and C1430.

R1404 to ground and the return for the high voltage form a current feedback loop for the CRT cathode current. Any change in cathode current causes a corresponding change in current through R1404. As the cathode current changes, the voltage developed across R1404 produces an apparent shift of the reference voltage for the supply. For an increase in CRT cathode current, the output of the supply will increase slightly, thus making the output resistance of the supply lower than it would be without the feedback. The frequency of the High Voltage Oscillator is approximately 30-50 kHz.

Diodes D1404 and D1405 provide overload protection for Q1400. L1422, C1422, and C1423 form a decoupling network to decouple the high voltage oscillations from the  $\pm$ 10 V and  $\pm$ 15 V power supplies. Switching transients are filtered out by L1426, R1426, R1420 and L1420.

The center-tapped primary of T1450 is also used in conjunction with D1440 and D1442 to form a full-wave rectifier. The rectifier has a choke input filter (L1440) and is the  $\pm 3.6$  volt supply for the integrated circuits.

The high voltage transformer T1450 has two secondary windings. One secondary winding supplies the filament voltage for the cathode ray tube. The other secondary winding in conjunction with the voltage doubler (D1452, D1453, C1452 and C1453) provides the high voltage, (approximately negative 3.875 kV), for the cathode ray tube elements. The filtered high voltage at the junction of R1453 and C1454 is connected to a divider consisting of R1469, the most negative point in the divider, through R1462, the most positive point in the divider. D1468 provides a constant 100 V drop across R1468 and R1469, thus allowing sufficient negative grid bias to turn off the CRT.

Resistor R1460 is switched in and out of the divider by SW1314, the FULL FIELD switch. There is a positive-going signal from the Sweep circuit coupled into the CRT control grid through C1490 and C1480 to intensify the sweep (or portions thereof) during burst time, in VITS operation, or if there is a signal connected to the Z AXIS INPUT jack. To prevent any de-focusing that might occur because of the increased beam current, the focusing anode voltage is made correspondingly more negative by adding R1460 to the divider. This is done by opening SW1314 in either of the VITS modes. During full field operation, R1460 is shorted out by SW1314.

#### **CRT Control Circuits**

Focus of the CRT display is controlled by the FOCUS control, R1465. The voltage applied to the focus grid is more positive (less negative) than the voltage on either the control grid or the CRT cathode. The ASTIG adjustment, R1476, which is used in conjunction with the FOCUS control to provide a well-defined display, varies the positive level on the astigmatism grid.

The GEOMETRY adjustment, R1472, varies the positive level on the horizontal deflection plate shields and the CRT screen to control the overall geometry of the display.

Two adjustments control the trace alignment by varying the magnetic field around the CRT. The ORTH adjustment, R1474 controls the current through L1474, which rotates the beam before the vertical deflection has been accomplished, insuring that the vertical and horizontal deflections are truly at right angles to each other. The BEAM ROTATE adjustment, R1470 controls the current through L1470, which rotates the beam after both the vertical and horizontal deflection plates, in order to align the trace and graticule.

The UNBLANK BIAS adjustment changes the difference of potential between the unblanking plates and is adjusted for uniform intensity on the CRT.

The INTENSITY control adjusts the DC potential of the control grid, thus controlling the quantity of electrons in the electron beam.

#### LOW VOLTAGE POWER SUPPLY

The Low Voltage Power Supply circuit provides the operating power for this instrument from four regulated supplies. Electronic regulation is used to provide stable, low ripple

output voltages. Each regulated supply, except the  $\pm 10\,\mathrm{V}$  supply which is current limited, is fused to prevent instrument damage if a supply is inadvertently shorted to ground. The power input stage includes the Voltage Selector Assembly. This assembly allows selection of the operating voltage range and regulating range for the instrument.

### Power Input

Power is applied to the primary of transformer T1501 through the 115 volt line fuse F1500, POWER switch SW1500, Range Selector SW1503, and Voltage Selector SW1502. The Range Selector SW1503 connects the split primaries of T1501 in parallel for 115 volt range of operation, or in series for 230 volt range of operation. A second line fuse, F1501, is connected in the circuit when the Range Selector switch is set to the 230 volt position to provide the correct protection for 230 V operation (F1501 current rating is one-half of F1500).

The Voltage Selector switch SW1502 allows the instrument to regulate correctly on higher or lower than normal line voltages. Each half of the primary has taps above and below the 115 volt (230 V) point. As the Voltage Selector switch is switched from LO to M to HI, more turns are added to the primary winding. Therefore, whether the primary voltage has increased or decreased, the secondary voltage can be maintained at a nearly constant level (Es = Ep x Ns/Np).

# —15 Volt Supply

The -15 volt supply provides the reference voltage for the remaining supplies. The reference for the -15 V supply is a 9 volt zener (D1570) that is contained in an oven and

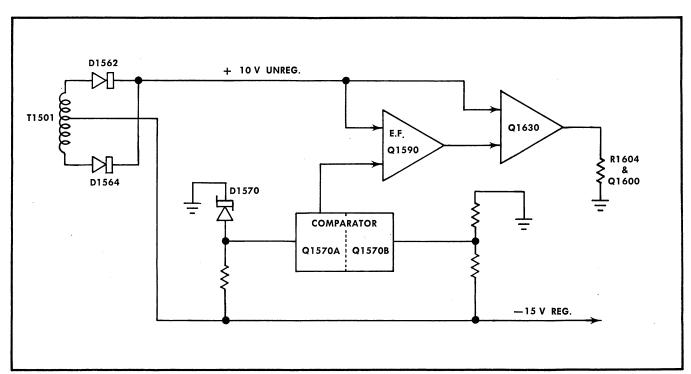


Fig. 3-19. Simplified block diagram of regulated -15 volt supply.

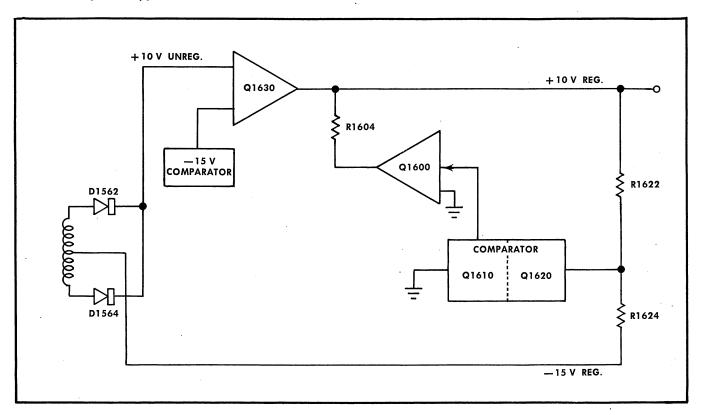


Fig. 3-20. Simplified block diagram of regulated +10 volt supply.

maintained at a constant temperature. The output from the secondary of T1501 is rectified by a full wave rectifier, D1562 and D1564, and then applied to the —15 V Series Regulator stage Q1630, to provide a stable output voltage. The Series Regulator can be compared to a variable resistance which is changed to control the output current, thus controlling the output voltage. The Series Regulator stage is controlled by the Error Amplifier, Q1570A and Q1570B.

The Error Amplifier is connected as a comparator. The base of Q1570A is referenced to —9 V by zener diode D1570. The voltage on the base of Q1570B is determined by the divider consisting of R1584, R1585, R1587 and R1588. R1588 adjusts the base voltage of Q1570B so the output voltage of this supply is —15 volts. The collector current of Q1570A is amplified by Q1590, an emitter follower, to control the Series Regulator Q1630.

Assume that the —15 volt supply tries to go in the positive direction. The base of Q1570B goes positive, turning Q1570B on harder. This decreases the conduction of Q1570A. The collector of Q1570A goes positive, causing Q1590 to increase conduction. The emitter of Q1590 becomes more positive and Q1630 turns on harder, which increases the current through the load and returns the supply to —15 volts. Fig. 3-19 is a simplified block diagram of the —15 V supply. R1600 and C1600 are for frequency compensation.

# +10 Volt Supply

Since the current through the  $-15\,\mathrm{V}$  supply to ground exceeds the current through the  $+10\,\mathrm{V}$  supply is shunt regulated and derived from the

—15 V supply. The current through the shunt regulator Q1600 is controlled by the Comparator consisting of Q1610 and Q1620. The current through the Comparator is determined by the voltage developed across R1622 and R1624. If the +10 V supply tries to go more positive, the base of Q1620 becomes more positive. This increases the conduction of Q1620 and decreases the conduction of Q1610. The collector of Q1610 goes positive, turning Q1600 on harder. As Q1600 increases conduction, the current through R1622 and R1624 is reduced and the +10 V supply returns to +10 volts. Q1600 effectively reduces the impedance of the +10 V supply. Fig. 3-20 is a simplified diagram of the +10 volt supply.

If the differential current between the  $+10\,\mathrm{V}$  supply and the  $-15\,\mathrm{V}$  supply exceeds approximately 206 mA, the  $+10\,\mathrm{V}$  supply will go out of regulation. With the  $-15\,\mathrm{V}$  supply drawing an excessive amount of current, the voltage at the junction of R1604 and Q1600 will decrease sufficiently to begin to saturate Q1600. When Q1600 starts to saturate, D1590 turns on and prevents the  $+10\,\mathrm{V}$  volt supply from going below approximately 9.8 volts.

# +100 Volt Supply

Rectified voltage for the  $\pm 100\,\mathrm{V}$  supply is provided by the bridge rectifier consisting of D1532A-D. The rectified voltage is connected to Series Regulator, Q1550. Reference voltage for this supply is provided by voltage divider R1552 and R1554 connected between the  $\pm 15\,\mathrm{V}$  supply and the output of this supply. The  $\pm 15\,\mathrm{V}$  supply is held stable as previously explained. If the  $\pm 100\,\mathrm{V}$  output changes, this change

appears at the base of the Error Amplifier, Q1540, as an error signal. The change on the collector of Q1540 is emitter-coupled through Q1545 to the base of Q1550, and the conduction of Q1550 either increases or decreases to restore the supply to +100 volts. Q1541 is connected as a diode and provides temperature compensation for Q1540. Zener diode D1540 provides DC coupling to the base of Q1545 without any appreciable loss. D1554 is a protection diode that clamps the base of Q1540 at -0.6 volts.

# +275 Volt Supply

The bridge rectifier consisting of D1502A-D provides the rectified voltage for Series Regulator Q1520. The  $\pm$ 275 volt supply operates in a manner similar to the supplies previously explained. The  $\pm$ 100 volt supply is connected to

the negative side of the +275 volt supply to elevate the output level to +275 volts. D1503 clamps the negative side of the +275 volt supply at  $-0.6\,\mathrm{V}$  to prevent the  $+100\,\mathrm{V}$  supply from going negative if the +275 volt supply is accidentally shorted. D1510 protects Q1510 against reverse breakdown.

# **Graticule Lights**

The graticule lights are connected in series with Q1560 between the unregulated  $+10\,\mathrm{V}$  and the  $-15\,\mathrm{V}$  supplies. The current through Q1560 determines the intensity of the lights. The base voltage of Q1560 is controlled by R1564, SCALE ILLUM, a variable resistor connected between the  $+10\,\mathrm{V}$  and  $-15\,\mathrm{V}$  supplies.

# **NOTES**

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# SECTION 4 MAINTENANCE

Change information, if any, affecting this section will be found at the rear of the manual.

# Introduction

This section of the manual contains maintenance information for use in preventive maintenance, corrective maintenance or troubleshooting of the Type R520.

# Cover Removal

The top and bottom covers of the instrument are held in place by slot-headed fasteners located on the top and bottom of the instrument. To remove the covers, use a coin to turn the fasteners 90° counterclockwise. Lift the covers off the instrument.

# PREVENTIVE MAINTENANCE

#### General

Preventive maintenance consists of cleaning, visual inspection, lubrication, etc. Preventive maintenance performed on a regular basis may prevent instrument breakdown and will improve the reliability of this instrument. The severity of the environment to which the Type R520 is subjected determines the frequency of maintenance. A convenient time to perform preventive maintenance is preceding recalibration of the instrument.

# Cleaning

**General.** The Type R520 should be cleaned as often as operating conditions require. Accumulation of dirt in the instrument can cause overheating and component breakdown. Dirt on components acts as an insulating blanket and prevents efficient heat dissipation. It also provides an electrical conduction path.

## CAUTION

Avoid the use of chemical cleaning agents which might damage the plastics used in this instrument. Avoid chemicals which contain benzene, toluene, xylene, acetone or similar solvents.

The top and bottom covers provide protection against dust in the interior of the instrument. Operation without the covers in place increases the frequency of cleaning.

**Exterior.** Loose dust accumulated on the outside of the Type R520 can be removed with a soft cloth or small paint brush. The paint brush is particularly useful for dislodging dirt on and around the front-panel controls. Dirt which remains can be removed with a soft cloth dampened in a mild detergent and water solution. Abrasive cleaners should not be used.

**CRT.** Clean the smoke-gray light filter, IRE graticule, light guide and the CRT face with a soft, lint-free cloth dampened with denatured alcohol.

Interior. Dust in the interior of the instrument should be removed occasionally due to its electrical conductivity under high-humidity conditions. The best way to clean the interior is to blow off the accumulated dust with dry, low-velocity air. Remove any dirt which remains with a soft paint brush or a cloth dampened with a mild detergent and water solution. A cotton tipped applicator is useful for cleaning in narrow spaces or for cleaning the circuit boards.

The high-voltage circuits, particularly parts located in the high-voltage compartment should receive special attention. Excessive dirt in these areas may cause high-voltage arcing and result in improper instrument operation.

#### Lubrication

**General.** The reliability of potentiometers, rotary switches and other moving parts can be maintained if they are kept properly lubricated. Use a cleaning-type lubricant (e.g., Tektronix Part No. 006-0218-00) on switch contacts. Lubricate switch detents with a heavier grease (e.g., Tektronix Part No. 006-0219-00). Potentiometers which are not permanently sealed should be lubricated with a lubricant which does not affect electrical characteristics (e.g., Tektronix Part No. 006-0220-00). The pot lubricant can also be used on shaft bushings. Do not over-lubricate. A lubrication kit containing the necessary lubricants and instructions is available from Tektronix, Inc. Order Tektronix Part No. 003-0342-00.

# Visual Inspection

The Type R520 should be inspected occasionally for such defects as broken connections, loose or disconnected pin connectors, improperly seated transistors, damaged circuit boards and heat-damaged parts.

The corrective procedure for most visible defects is obvious; however, particular care must be taken if heat-damaged components are found. Overheating usually indicates other trouble in the instrument; therefore, it is important that the cause of overheating be corrected to prevent recurrence of the damage.

# Transistor and Integrated Circuit Checks

Periodic checks of the transistors and integrated circuits in the Type R520 are not recommended. The best check of transistor and integrated circuit performance is its actual operation in the instrument. Performance of the circuits is thoroughly checked during recalibration; substandard transistor and integrated circuits will usually be detected at that time.

#### Recalibration

To assure accurate measurements, check the calibration of this instrument after each 1000 hours of operation or every six months if used infrequently. In addition, replacement of components may necessitate recalibration of the affected circuits. Complete calibration instructions are given in the Calibration section.

The calibration procedure can also be helpful in localizing certain troubles in the instrument. In some cases, minor troubles may be revealed and/or corrected by recalibration.

# **TROUBLESHOOTING**

## Introduction

The following information is provided to facilitate troubleshooting of the Type R520. Information contained in other sections of this manual should be used along with the following information to aid in locating the defective component. An understanding of the circuit operation is very helpful in locating troubles. See the Circuit Description section for complete information.

# Troubleshooting Aids

**Diagrams.** Circuit diagrams are given on foldout pages in Section 9. The component number and electrical value of each component in this instrument are shown on the diagrams. Each main circuit is assigned a series of component numbers. Table 4-1 lists the main circuits in the Type R520 and the series of component numbers assigned to each. Important voltages and waveforms are also shown on the diagrams. The portions of the circuit mounted on circuit boards are enclosed with a blue line.

TABLE 4-1
Component Numbers

Component Numbers on Diagrams	Diagram Number	Circuit				
1-199	1	Input Amp/Test Circle Oscil- lator and Sync				
200-299	2	Subcarrier Regenerator				
300-399	3	Precision $\phi$ Shifter & Goniometers				
400-599	4	Demodulators				
600-699	5	Filter & Horiz/Vert Driver Amp				
700-899	6	Vertical Amplifier				
900-1099	7	Horizontal Amplifier				
1100-1399	8 .	Sweep				
1400-1499	9	CRT Circuit				
1500-1699	10	Power Supply				

**Circuit Boards.** Fig. 4-9 through Fig. 4-27 for instruments SN B150100 and up, and Fig. 4-9 through Fig. 4-26 for instruments below SN B150100 show the circuit boards used in the Type R520. Fig. 4-8 shows the location of each board within the instrument. Each electrical component on the

boards is identified by its circuit number. The circuit boards are also outlined on the diagrams with a blue line. These pictures, used along with the diagrams aid in locating the components mounted on the circuit boards.

For instruments SN B150100 and up, some component and pin connector locations on the circuit boards are not used in this instrument but they are used in another instrument (Type 520 MOD 188M). For example, transistor Q1360 and surrounding area on the Sweep board (see Fig. 4-22A) is not used.

Wiring Color-Code. All insulated wire and cable used in the Type R520 is color-coded to facilitate circuit tracing. Signal carrying leads are identified with one or two colored stripes. Voltage supply leads are identified with three stripes to indicate the approximate voltage using the EIA resistor color code. A white background color indicates a positive voltage and a tan background indicates a negative voltage. The widest color stripe identifies the first color of the code. Table 4-2 gives the wiring color-code for the power-supply voltages used in the Type R520.

TABLE 4-2
Power Supply Wiring Color Code

Supply	Color Code
+275 V	Orange-Black-Brown on White
+100 V	Brown-Black-Brown on White
+10 V	Brown-Red-Black on White
+3.6 V	Black-Orange on White
—15 V	Brown-Green-Black on Tan

**Resistor Color-Code.** In addition to the brown composition resistors, some metal-film resistors and some wire-wound resistors are used in the Type R520. The resistance values of wire-wound resistors are printed on the body of the component. The resistance values of composition resistors and metal-film resistors are color-coded on the components with EIA color-code (some metal-film resistors may have the value printed on the body). The color-code is read starting with the stripe nearest the end of the resistor. Composition resistors have four stripes which consist of two significant figures, a multiplier and a tolerance value (see Fig. 4-1). Metal-film resistors have five stripes consisting of three significant figures, a multiplier and a tolerance value.

**Capacitor Marking.** The capacitance values of common disc capacitors and small electrolytics are marked in microfarads on the side of the component body. The white ceramic capacitors used in the Type R520 are color coded in picofarads using modified EIA code (see Fig. 4-1).

**Diode Color-Code.** The cathode end of each glass-encased diode is indicated by a stripe, a series of stripes or a dot. For most silicon or germanium diodes with a series of stripes, the first stripe (pink or blue) of the color-code identifies that the following three stripes are the three significant digits of the Tektronix Part Number using the resistor color-code system (e.g., a diode color-coded pink-(or blue) browngray-green indicates Tektronix Part Number 152-0185-00). The cathode and anode ends of a metal-encased diode can be identified by the diode symbol marked on the body.

**Transistor Lead Configuration.** Fig. 4-2 shows the topview electrode configurations of the transistors and integrated circuits used in this instrument.

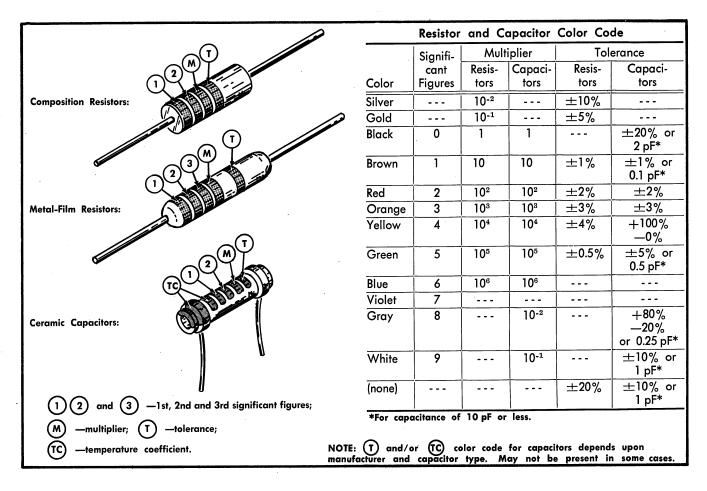


Fig. 4-1. Color code for resistors and ceramic capacitors.

# **Troubleshooting Equipment**

The following equipment is useful for troubleshooting the Type R520.

#### 1. Transistor Tester

Description: Tektronix Type 575 Transistor-Curve Tracer or equivalent.

Purpose: To test the semiconductors used in this instrument.

# 2. Multimeter

Description: VTVM, 10 megohm input impedance and 0 to 500 volts range; ohmmeter, 0 to 50 megohms. Accuracy, within 3%. Test prods must be insulated to prevent accidental shorting.

Purpose: To check voltages and for general troubleshooting in this instrument.

## NOTE

A 20,000 ohms/volt DC VOM can be used to check the voltages in this instrument if allowances are made for the circuit loading of the VOM at highimpedance points.

## 3. Test Oscilloscope

Description: DC to 8 MHz frequency response. 10 millivolts to 5 volts/division deflection factor. Use a 10× probe.

Purpose: To check waveforms in this instrument.

# Troubleshooting Techniques

This troubleshooting procedure is arranged in an order which checks the simple possibilities before proceeding with extensive troubleshooting. The first few checks assure proper connection, operation and calibration. If the trouble is not located by these checks, the remaining steps aid in locating the defective component. When the defective component is located, it should be replaced following the replacement procedures given under Corrective Maintenance.

- 1. Check Control Settings. Incorrect control settings can indicate a trouble that does not exist. If there is any question about the correct function or operation of any control, see the Operating Instructions section of this manual.
- **2.** Check Associated Equipment. Before proceeding with troubleshooting of the Type R520, check that the equipment used with this instrument is operating correctly. Check that the signal is properly connected and that the interconnecting cables are not defective. Also, check the power source.

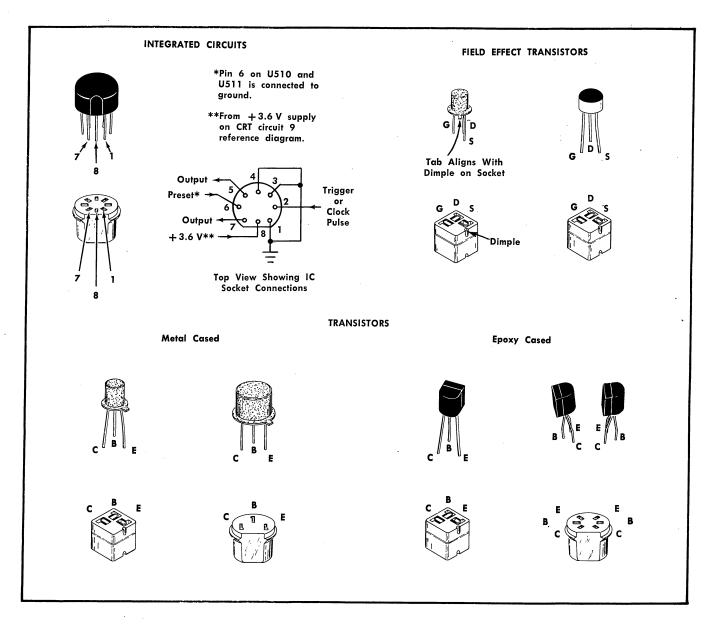


Fig. 4-2. Electrode configuration for socket-mounted transistors and integrated circuits, top view.

- **3. Visual Check.** Visually check the portion of the instrument in which the trouble is located. Many troubles can be located by visual indications such as unsoldered connections, disconnected or loose pin connectors, broken wires, damaged circuit boards, damaged components, etc.
- **4. Check Instrument Calibration.** Check the calibration of this instrument, or the affected circuit if the trouble exists in one circuit. The apparent trouble may only be a result of misadjustment or may be corrected by calibration. Complete calibration instructions are given in the Calibration section of this manual.
- **5. Isolate Trouble to a Circuit.** To isolate trouble to a circuit, note the trouble symptom. The symptom often identifies the circuit in which the trouble is located. For example, poor focus indicates that the CRT (includes high voltage) circuit is probably at fault. When trouble symptoms

appear in more than one circuit, check affected circuits by taking voltage and waveform readings.

Incorrect operation of all circuits often indicates trouble in the power supply. Check first for correct voltage of the individual supplies. However, a defective component elsewhere in the instrument can appear as a power-supply trouble and may also affect the operation of other circuits. Table 4-3 lists the tolerances of the power supplies in this instrument. If a power-supply voltage is within the listed tolerance, the supply can be assumed to be working correctly. If outside the tolerance, the supply may be misadjusted or operating incorrectly. Use the procedure given in the Calibration section to adjust the power supplies.

Figs. 3-1 through 3-6 in the Circuit Description section provide a guide for isolating a trouble to a block or circuit. These illustrations are functional block diagrams showing

**TABLE 4-3**Power Supply Tolerance

Power Supply	Tolerance
+275 V	±7% or ±19.25 V
+100 V	$\pm 3.5\%$ or $\pm 3.5  \text{V}$
+10 V	$\pm 3.5\%$ or $\pm 0.35\mathrm{V}$
+3.6 V	±5% or ±0.18 V
—15 V	$\pm 0.5\%$ or $\pm 0.075\mathrm{V}$

signal flow for six different modes of operation. By selecting a mode of operation, it is possible to bypass some blocks and connect others into the circuit to determine the blocks that function properly and those that do not. The only blocks that cannot be bypassed are the Input Amplifier, Vertical Amplifier, low-voltage power supply (not shown) and CRT circuit. Detailed voltage and waveform checks will have to be made to find the cause of trouble in these circuits.

After the defective circuit has been located, proceed with steps 6 through 8 to locate the defective component(s).

**6. Check Circuit Board Interconnections.** After the trouble has been isolated to a particular block or circuit, check the pin connectors on the circuit board for correct connections. Fig. 4-9 through Fig. 4-27 for instruments SN B150100 and up, and Fig. 4-9 through Fig. 4-26 for instruments below SN B150100 show the correct connections for each board.

The pin connectors used in this instrument also provide a convenient means of circuit isolation. For example, a short in a power supply can be isolated to the power supply itself by disconnecting the pin connectors for that voltage at the remaining boards.

**7. Check Voltage and Waveforms.** Often the defective component can be located by checking for the correct voltage or waveform in the circuit. Typical voltages and waveforms are given on the diagrams.

## NOTE

Voltages and waveforms given on the diagrams are not absolute and may vary slightly between instruments. To obtain operating conditions similar to those used to take these readings, see the first diagram page.

# WARNING

"Ground lugs" and shield braids are not always at ground potential. Check the schematic before using such connections as a ground for the voltmeter test prod or oscilloscope probe. Some transistor cases may be elevated from 0 to 275 V. This warning note also applies to recessed screws that hold the low voltage power supply transistors to the rear panel.

- **8. Check Individual Components.** The following procedures describe methods of checking individual components in the Type R520. Components which are soldered in place are best checked by disconnecting one end. This isolates the measurement from the effects of surrounding circuitry.
- A. TRANSISTORS AND INTEGRATED CIRCUITS. The best check of transistor and integrated circuit operation is actual

performance under operating conditions. If a transistor or integrated circuit is suspected of being defective, it can best be checked by substituting a new component or one which has been checked previously. However, be sure that circuit conditions are not such that a replacement transistor or integrated circuit might also be damaged. If substitute transistors are not available, use a dynamic tester (such as Tektronix Type 575). Static-type testers are not recommended, since they do not check operation under simulated operating conditions.

B. DIODES. A diode can be checked for an open or shorted condition by measuring the resistance between terminals. With an ohmmeter scale having an internal source of between 800 millivolts and 3 volts, the resistance should be very high in one direction and very low when the leads are reversed.

# CAUTION

Do not use an ohmmeter scale that has a high internal current. High currents may damage the diode.

- C. RESISTORS. Check the resistor with an ohmmeter. Check the Electrical Part List for the tolerance of the resistors used in this instrument. Resistors normally do not need to be replaced unless the measured value varies widely from the specified value.
- D. INDUCTORS. Check for open inductors by checking continuity with an ohmmeter. Shorted or partially shorted inductors can usually be found by checking the waveform response when high-frequency signals are passed through the circuit. Partial shorting often reduces high-frequency response (roll-off).
- E. CAPACITORS. A leaky or shorted capacitor can best be detected by checking resistance with an ohmmeter on the highest scale. Do not exceed the voltage rating of the capacitor. The resistance reading should be high after initial charge of the capacitor. An open coupling capacitor can best be detected with a capacitance meter or by checking whether the capacitor passes AC signals.
- **9. Repair and Readjust the Circuit.** If any defective parts are located, follow the replacement procedures given in this section. Be sure to check the performance of any circuit that has been repaired or that has had any electrical components replaced.

# **CORRECTIVE MAINTENANCE**

# General

Corrective maintenance consists of component replacement and instrument repair. Special techniques required to replace components in this instrument are given here.

# **Obtaining Replacement Parts**

**Standard Parts.** All electrical and mechanical part replacements for the Type R520 can be obtained through your local Tektronix Field Office or representative. However, many

# Maintenance—Type 520/R520 NTSC

of the standard electronic components can be obtained locally in less time than is required to order them from Tektronix, Inc. Before purchasing or ordering replacement parts, check the parts lists for value, tolerance, rating and description.

# NOTE

When selecting replacement parts, it is important to remember that the physical size and shape of a component may affect its performance in the instrument, particularly at high frequencies. All replacement parts should be direct replacements unless it is known that a different component will not adversely affect instrument performance.

**Special Parts.** In addition to the standard electronic components, some special components are used in the Type R520. These components are manufactured or selected by Tektronix, Inc. to meet specific performance requirements, or are manufactured for Tektronix, Inc. in accordance with our specifications. These special components are indicated in the Electrical Parts List by an asterisk preceding the part number. Most of the mechanical parts used in this instrument have been manufactured by Tektronix, Inc. Order all special parts directly from your local Tektronix Field Office or representative.

**Ordering Parts.** When ordering replacement parts from Tektronix, Inc., include the following information:

- 1. Instrument type.
- 2. Instrument serial number.
- 3. A description of the part (if electrical, include circuit number).
  - 4. Tektronix Part Number.

# Soldering Techniques

# WARNING

Disconnect the instrument from the power source before soldering.

**Circuit Boards.** Use ordinary 60/40 solder and a 35- to 40-watt pencil type soldering iron on the circuit boards. The tip of the iron should be clean and properly tinned for best heat transfer to the solder joint. A higher wattage soldering iron may separate the wiring from the base material.

The following technique should be used to replace a component on a circuit board. Most components can be replaced without removing the boards from the instrument.

- 1. Grip the component lead with long-nose pliers. Touch the soldering iron to the lead at the solder connection. Do not lay the iron directly on the board.
- 2. When the solder begins to melt, pull the lead out gently. This should leave a clean hole in the board. If not, the hole can be cleaned be reheating the solder and placing a sharp object such as a toothpick into the hole to clean it out. A vacuum-type desoldering tool can also be used for this purpose.

- 3. Bend the leads of the new component to fit the holes in the board. If the component is replaced while the board is mounted in the instrument, cut the leads so they will just protrude through the board. Insert the leads into the holes in the board so the component is firmly seated against the board (or as positioned originally). If it does not seat properly, heat the solder and gently press the component into place.
- 4. Touch the iron to the connection and apply a small amount of solder to make a firm solder joint; do not apply too much solder. To protect heat-sensitive components, hold the lead between the component body and the solder joint with a pair of long nose pliers (see Fig. 4-3) or other heat sink.

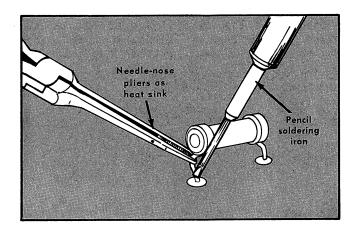


Fig. 4-3. Use of a heat sink to protect components during soldering.

- 5. Clip the excess lead that protrudes through the board.
- 6. Clean the area around the solder connection with a flux-remover solvent. Be careful not to remove information printed on the board.

**Metal Terminals.** When soldering metal terminals (e.g., switch terminals, potentiometers, etc), ordinary 60/40 solder can be used. Use a soldering iron with a 40- to 75-watt rating and a  $\frac{1}{8}$ -inch wide wedge-shaped tip.

Observe the following precautions when soldering metal terminals:

- 1. Apply only enough heat to make the solder flow freely.
- 2. Apply only enough solder to form a solid connection. Excess solder may impair the function of the part.
- 3. If a wire extends beyond the solder joint, clip off the
- 4. Clean the flux from the solder joint with a flux-remover solvent.

# **Component Replacement**

## WARNING

Disconnect the instrument from the power source before replacing components.

Circuit Board Replacement. If a circuit board is damaged beyond repair, either the entire assembly including all solder-on components, or the board only, can be replaced. Part numbers are given in the Mechanical Parts List for either the completely wired or the unwired board. Most of the components mounted on the circuit boards can be replaced without removing the boards from the instrument. Observe the soldering precautions given under Soldering Techniques in this section. However, if the bottom side of the board must be reached or if the board must be moved to gain access to other areas of the instrument, release the board from the plastic clips. Exception: The Input Amplifier board can be removed by removing four screws. The interconnecting wires on some of the boards are long enough to allow the board to be moved out of the way or turned over without disconnecting all the pin connectors.

**Cathode-Ray Tube Replacement.** The following procedure outlines the removal and replacement of the cathoderay tube:

#### WARNING

High vacuum cathode ray tubes are dangerous to handle. To prevent personal injury from flying glass in case of tube breakage, wear a face mask or safety goggles, and gloves.

Handle the CRT with extreme care. Do not strike or scratch it. Never subject it to more than moderate force or pressure when removing or installing.

Always store spare CRT's in original protective cartons. Save cartons to dispose of used CRT's.

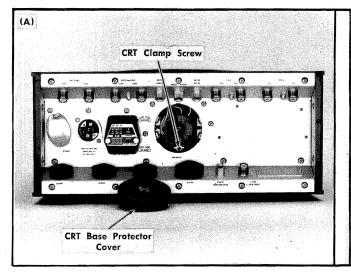
## A. REMOVAL:

- 1. Remove the top cover from the instrument.
- 2. Remove the graticule cover with associated parts.
- 3. Disconnect the deflection-plate connectors. Be careful not to bend the deflection-plate pins.
- 4. Remove the metal cover that protects the CRT base. This cover unsnaps from the rear panel.

- 5. Remove the CRT socket.
- 6. Loosen the CRT clamp screw about 4 or 5 turns (see Fig. 4-4A). Avoid loosening the screw too much because the CRT clamp wedge tightener will come loose from the screw.
- 7. From the rear of the instrument, push forward on the CRT base and hold the CRT faceplate to guide the CRT as it is removed from the front of the instrument (see Fig. 4-4B). Be careful not to bend the neck pins.

#### **B. REPLACEMENT:**

- 1. Insert the CRT into the shield. Be careful not to bend the neck pins.
- 2. Tighten the CRT clamp screw until the CRT is held snugly but will allow some freedom of movement so steps 4 and 5 can be performed.
- Reconnect the CRT socket while holding the CRT faceplate.
- 4. Reconnect the deflection-plate connectors. Correct locations is indicated on the CRT shield.
- 5. Check that the  $0^{\circ}$   $180^{\circ}$  axis on the internal vector graticule lies on a horizontal plane. If not, turn the CRT base until proper alignment is obtained. There are some guide marks on the front panel. These marks are located on each side of the CRT opening.
- 6. Check that the CRT faceplate protrudes through the front panel the same distance as the thickness of the vector graticule light guide.
  - 7. Carefully tighten the CRT base clamp.
  - 8. Install the graticule cover with all associated parts.
  - 9. Install the rear panel CRT cover.
- 10. To recalibrate the instrument, the following circuit areas need to be checked and adjusted, if necessary:
- a. Check all the adjustments shown on the Horiz/Vert Driver Amps portion of diagram No. 5.



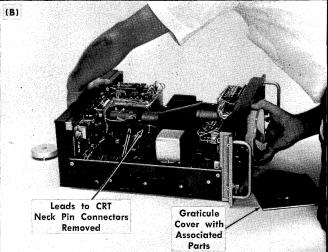


Fig. 4-4. Replacing the CRT.

- b. Check the adjustment shown on the Vertical Amplifier diagram No. 6 and Horizontal Amplifier diagram No. 7.
- c. Check all the CRT circuit adjustments given on diagram
- d. Check the A CAL and B CAL front-panel screwdriver adjustments.

Transistor and Integrated Circuit Replacement. Transistors and integrated circuits should not be replaced unless actually defective. If removed from their sockets during routine maintenance, return them to their original sockets. Unnecessary replacement of transistors and integrated circuits may affect the calibration of this instrument. When transistors or integrated circuits are replaced, check the operation of that part of the instrument which may be affected.

#### CAUTION

POWER switch must be turned off before removing or replacing transistors and integrated circuits.

Replacement transistors and integrated circuits should be of the original type or a direct replacement. Fig. 4-2 shows the lead configuration of the transistors and integrated circuits used in this instrument. Some plastic case transistors have lead configurations which do not agree with those shown here. If a transistor is replaced by a transistor which is made by a different manufacturer than the original, check the manufacturer's basing diagram for correct basing. All transistor sockets in this instrument are wired for the basing used for metal-case transistors. Transistors which have heat radiators or are mounted on the chassis use silicone grease to increase heat transfer. Replace the silicone grease when replacing these transistors.

#### WARNING

Handle silicone grease with care. Avoid getting silicone grease in the mouth or eyes. Wash hands thoroughly after use.

**Fuse Replacement.** Table 4-4 gives the rating, location, and function of the fuses used in this instrument.

**TABLE 4-4** Fuse Ratings

Circuit Number	Rating	Function	Location				
F1500	1.6 A Slow	115 V Line	Line				
F1501	0.8 A Slow	230 V Line	Voltage Selector on rear panel				
F1502 (Below SN B150100)	0.0625 A Fast	+275 V Supply	Rectifier board				
F1502 (SN B150100 up)	0.125 A Fast	+2/3 v 3upply	by power trans-				
F1532	0.25 A Fast	+100 V Supply	former				
F1562	1.5 A Fast	+10 V Supply	1				

**Switches.** If a switch is defective, replace the entire assembly. Replacement switches can be ordered by referring to the Parts List for the applicable part numbers.

When replacing a switch, tag the leads and switch terminals with corresponding identification tags as the leads are disconnected. Then, use the old switch as a guide for installing the new one. An alternative method is to draw a sketch of the switch layout and record the wire color at each

terminal. When soldering to the new switch be careful that the solder does not flow beyond the rivets on the switch terminals. Spring tension of the switch contact can be destroyed by excessive solder.

**Power Transformer Replacement.** The power transformer in this instrument is warranted for the life of the instrument. If the power transformer becomes defective, contact your local Tektronix Field Office or representative for a warranty replacement (see the Warranty note in the front of this manual). Be sure to replace only with a direct replacement Tektronix transformer.

When removing the transformer, tag the leads with the corresponding terminal numbers to aid in connecting the new transformer. After the transformer is replaced, check the performance of the complete instrument using the Performance Check procedure.

**High-Voltage Compartment.** The components located in the high-voltage compartment can be reached for maintenance or replacement by using the following procedure.

- 1. Remove the top cover of the instrument as described in this section.
- 2. Remove the six screws that hold the Input Sync board chassis to the rear panel and main chassis.
- 3. Disconnect some of the short length Sync board leads so the Sync board chassis can be tilted for access to the high voltage compartment screws.
- 4. Remove the three screws which hold the cover on the high-voltage compartment.
- 5. Remove the high-voltage cover to reach the boards inside the compartment.
- 6. To replace the high-voltage compartment, reverse the order of removal.

# NOTE

All solder joints in the high-voltage compartment should have smooth surfaces. Any protrusions may cause high-voltage arcing at high altitudes.

# Recalibration After Repair

After replacing any electrical component or circuit board, the calibration of that particular circuit area should be checked, as well as the calibration of other closely related circuits. Since the low-voltage supply affects all circuits, calibration of the entire instrument should be checked if work has been done in the low-voltage supply or if the power transformer has been replaced. The Performance Check Procedure in Section 5 provides a quick and convenient means of checking instrument operation.

# Instrument Repackaging

If the Type R520 is to be shipped for long distances by commercial means of transportation, it is recommended that the instrument be repackaged in the original manner for maximum protection. The original shipping carton can be saved and used for this purpose. Figs. 4-5 and 4-7 illustrate how to repackage the Type R520 and give the part numbers for the packaging components if new items are needed. Figs. 4-6 and 4-7 illustrate how to repackage the Type 520, with applicable part numbers.

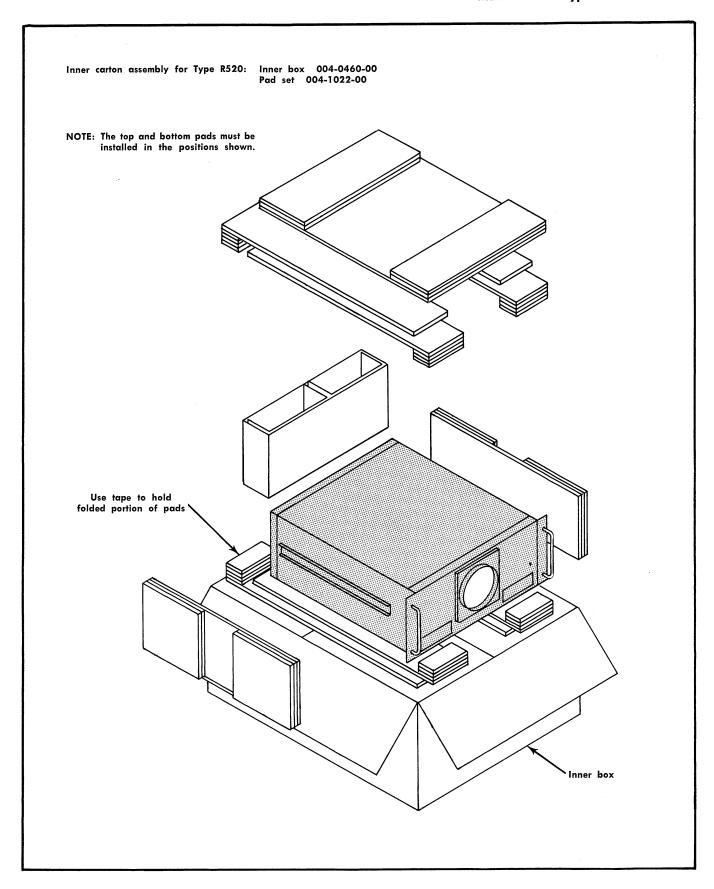


Fig. 4-5. Repackaging the Type R520 in its inner box.

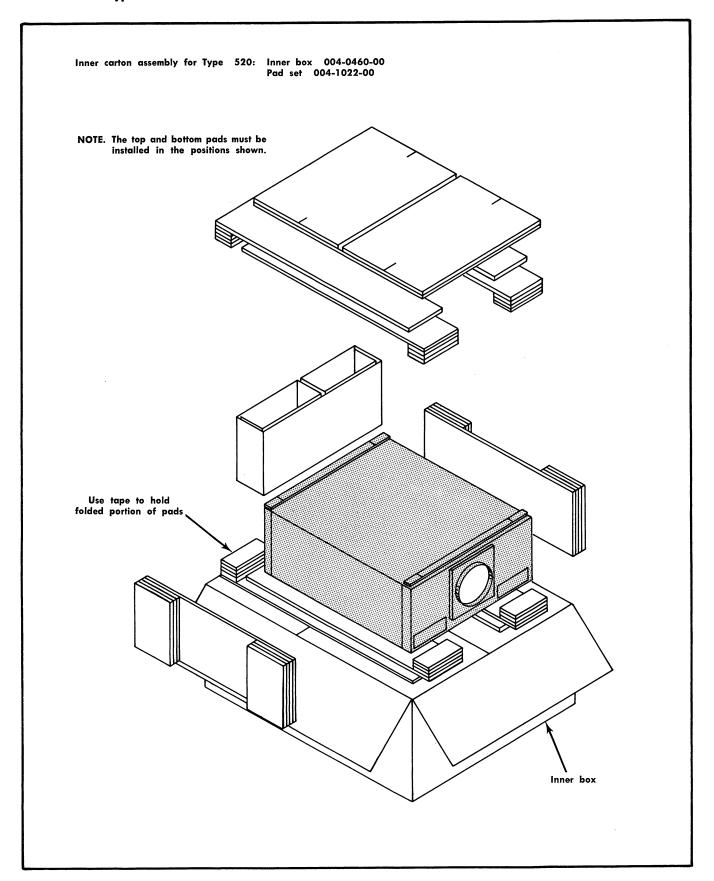


Fig. 4-6. Repackaging the Type 520 in its inner box.

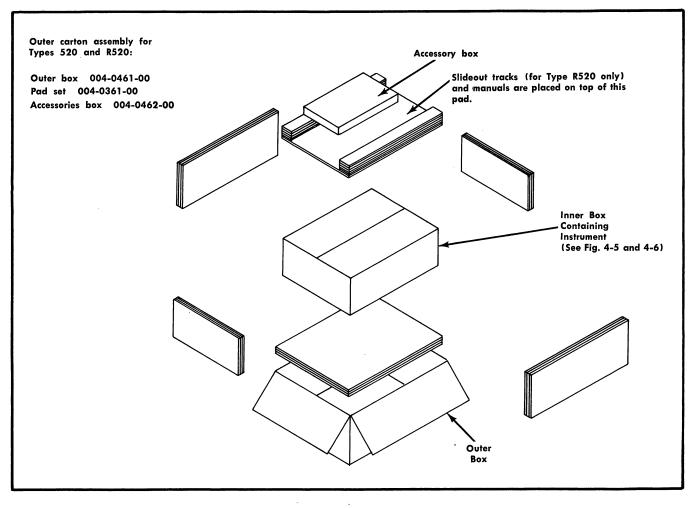


Fig. 4-7. Repackaging the Type 520 or R520 in its outer box for shipment.

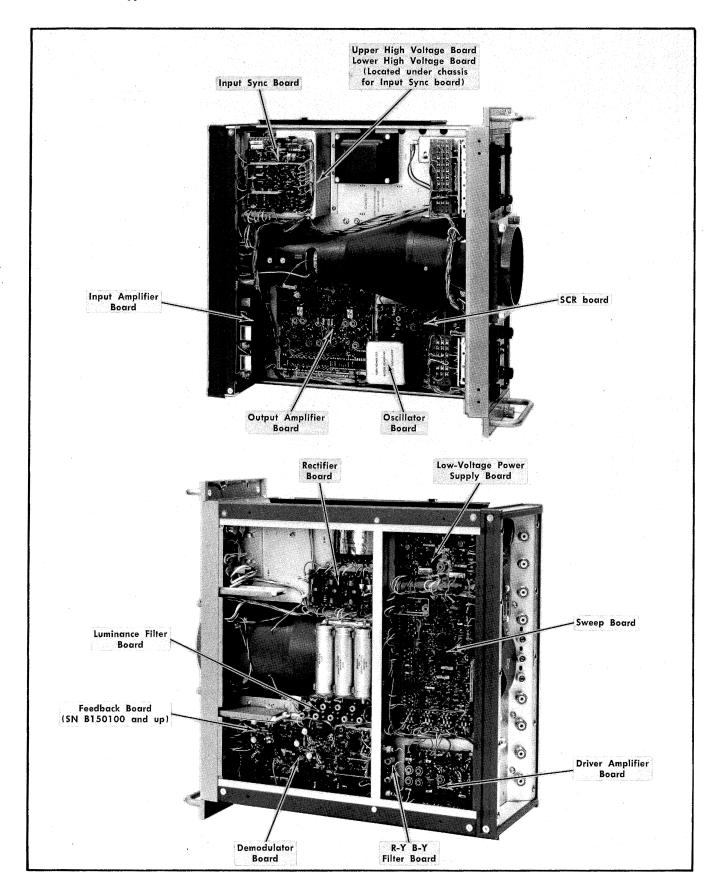


Fig. 4-8. Location of the circuit boards in the Type R520.

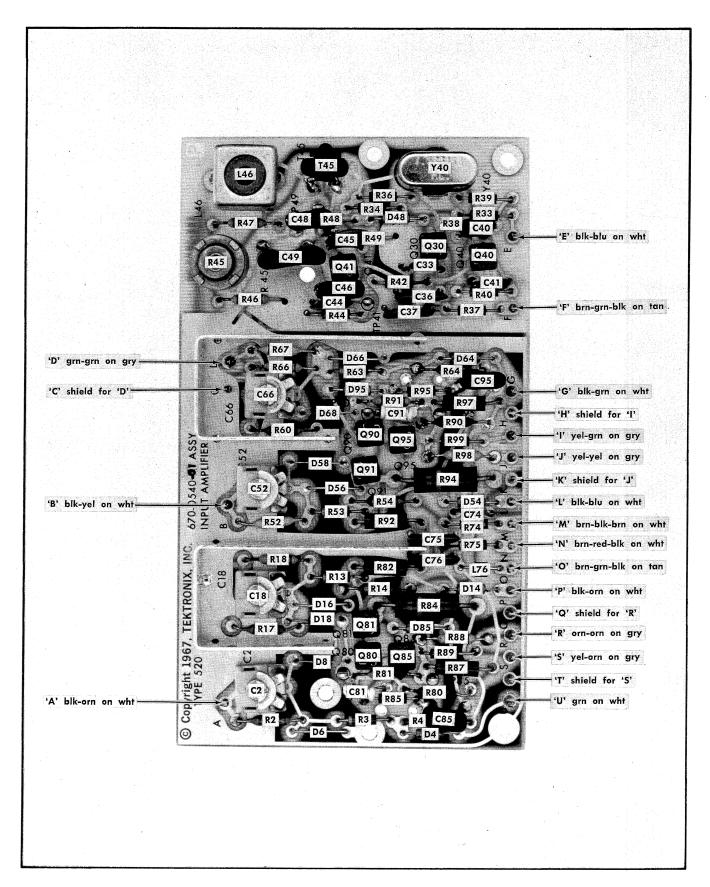


Fig. 4-9A. Input Amplifier board; component identification and wire color codes for instruments SN B150100 and up.

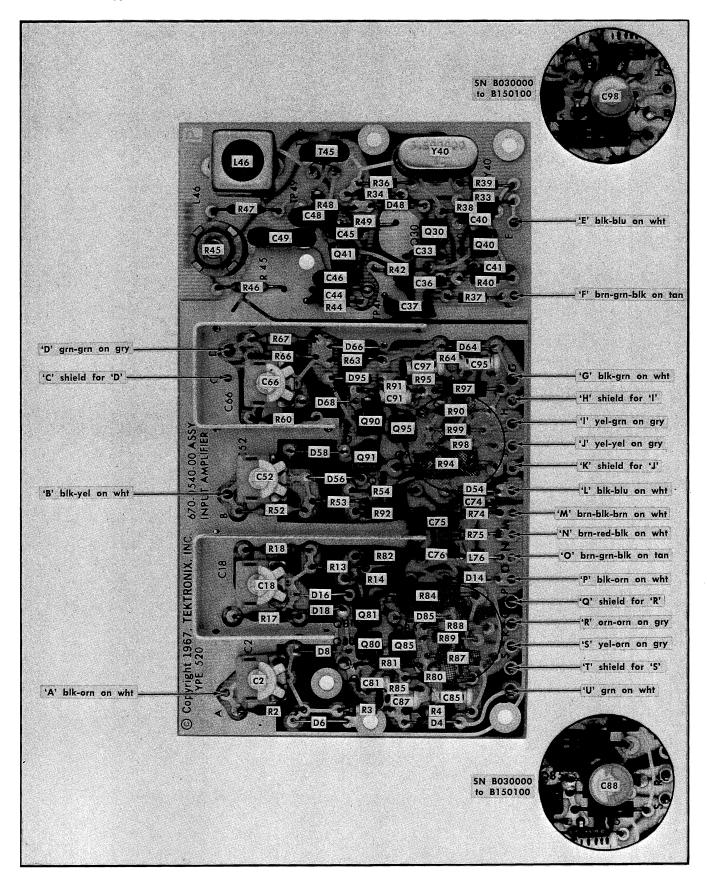


Fig. 4-9B. Input Amplifier board; component identification and wire color codes for instruments below SN B150100.

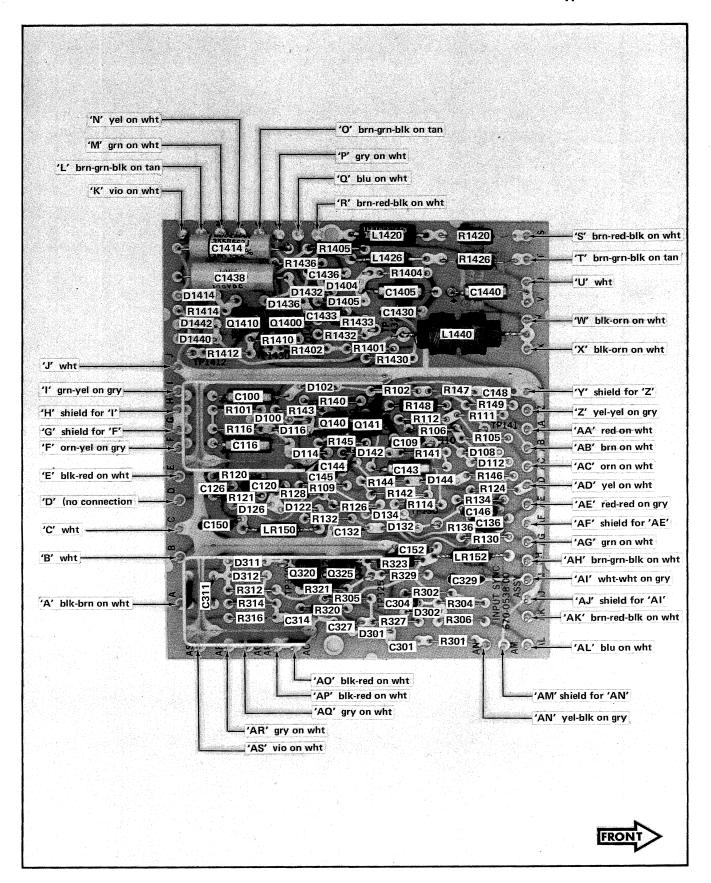


Fig. 4-10A. Input Sync board; component identification and wire color codes for instruments SN B280000-up.

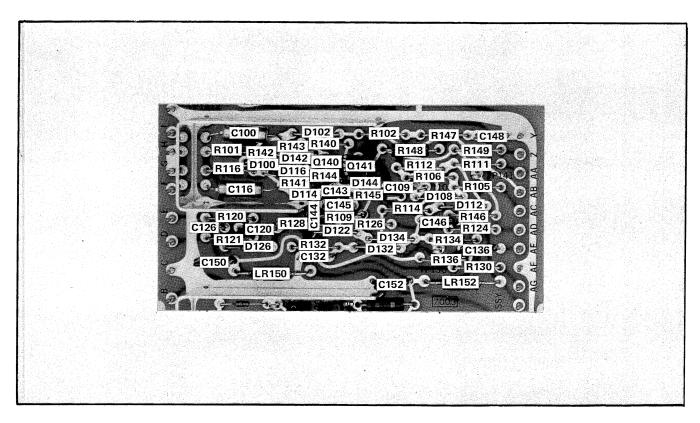


Fig. 4-10B. Input Sync partial board; component identification for instruments SN B240000-B279999.

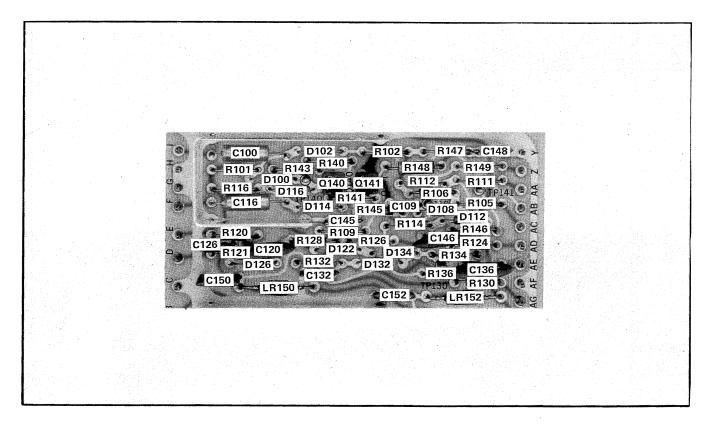


Fig. 4-10C. Input Sync partial board; component identification for instruments SN B010100-B239999.

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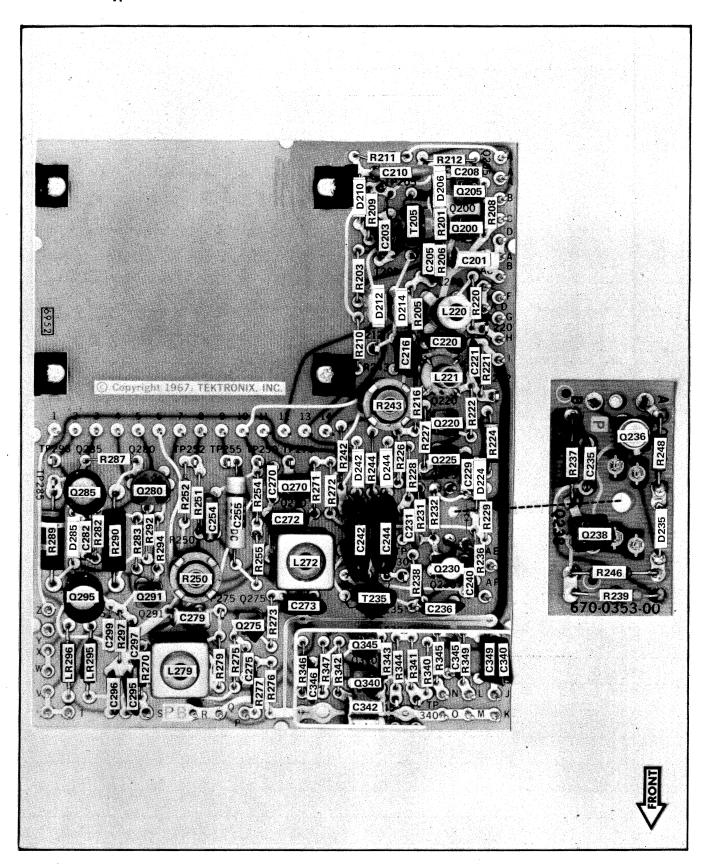


Fig. 4-11A. SCR board and SCR Limiter Board; Component identification and interconnecting wire color code for instruments SN B251880 and up.

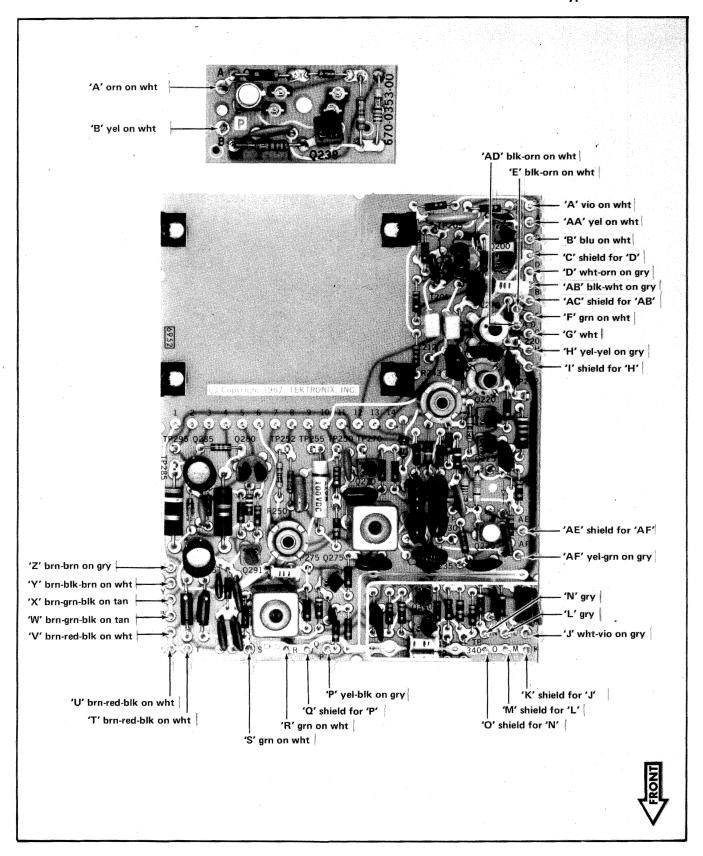


Fig. 4-11B. SCR board; wire color code for instruments SN B251880 and up.

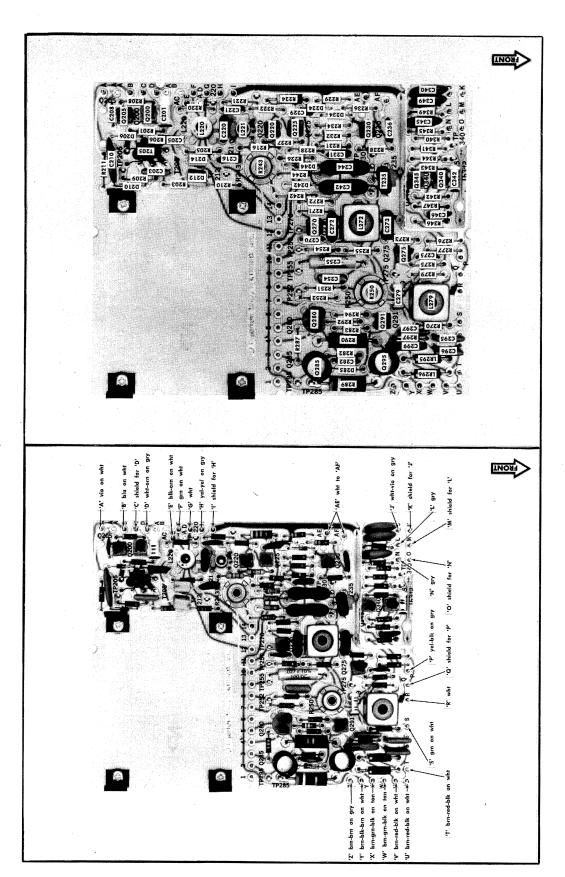


Fig. 4-12A. SCR board; component identification and wire color code for SN BI50100 through B241879.

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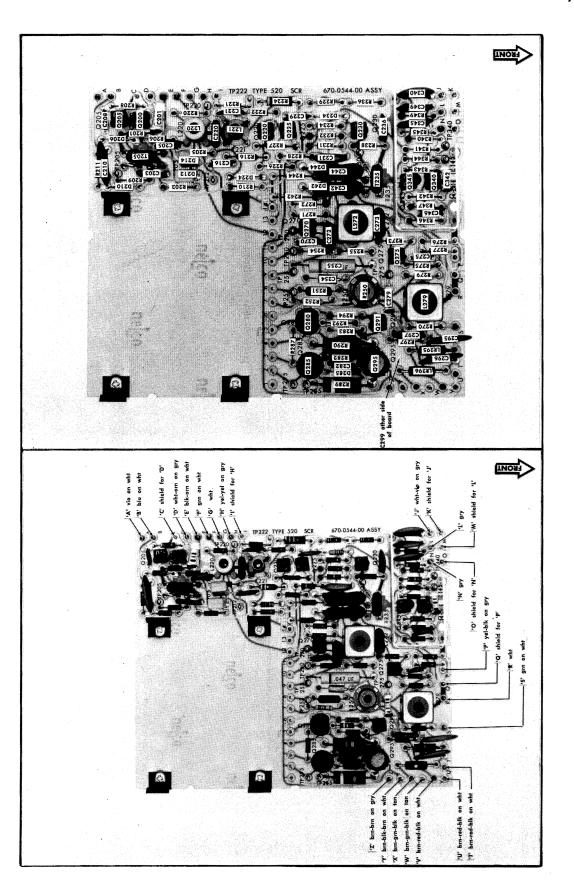


Fig. 4-12B. SCR board; component identification and wire color code for instruments below SN B150100.

4-19

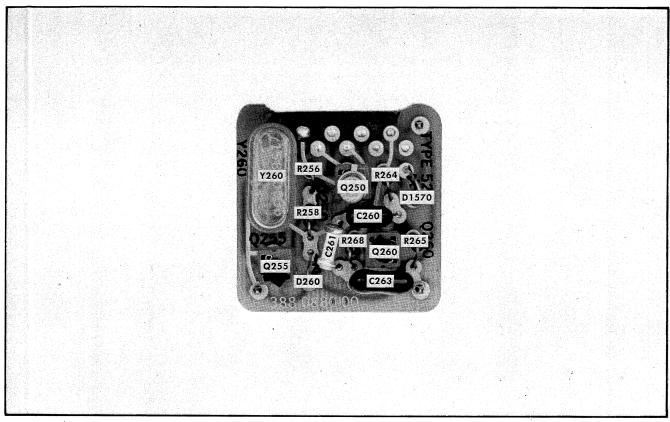


Fig. 4-13. Oscillator board; component identification.

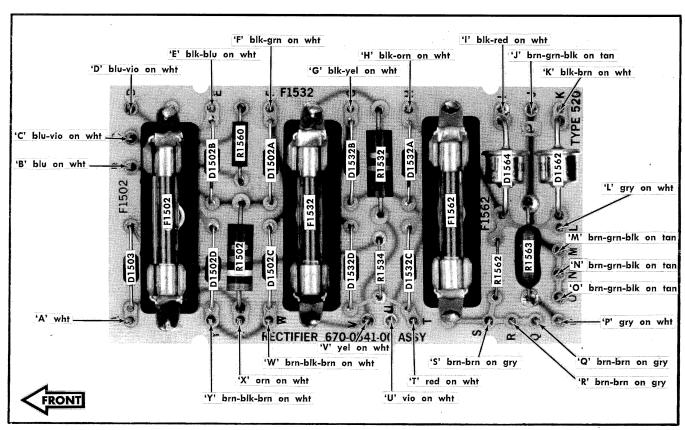


Fig. 4-14. Rectifier board; component identification and wire color codes.

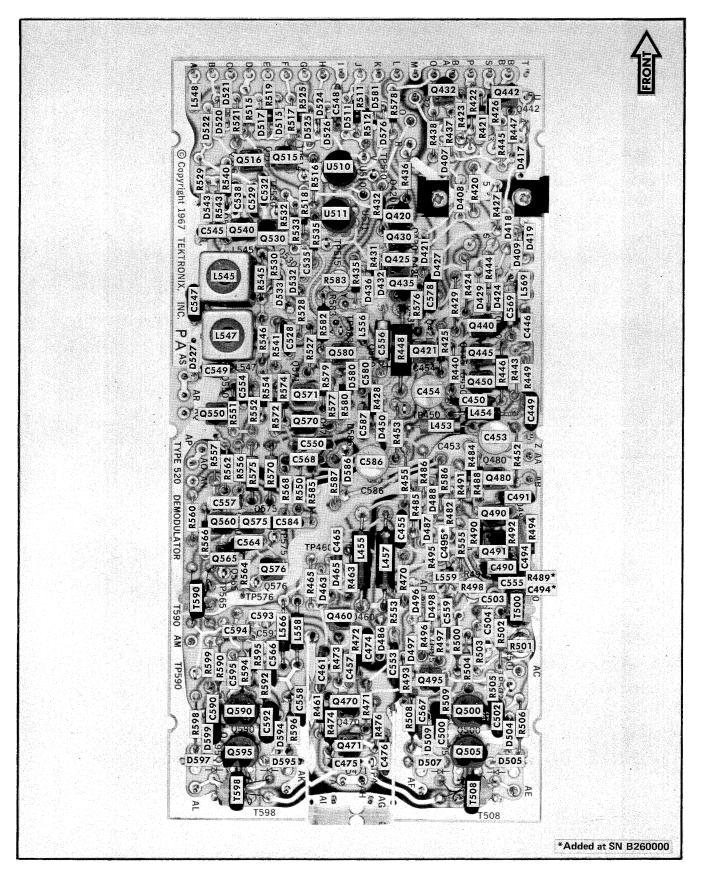


Fig. 4-15A. Demodulator board; component identification for instruments SN B150700 and up.

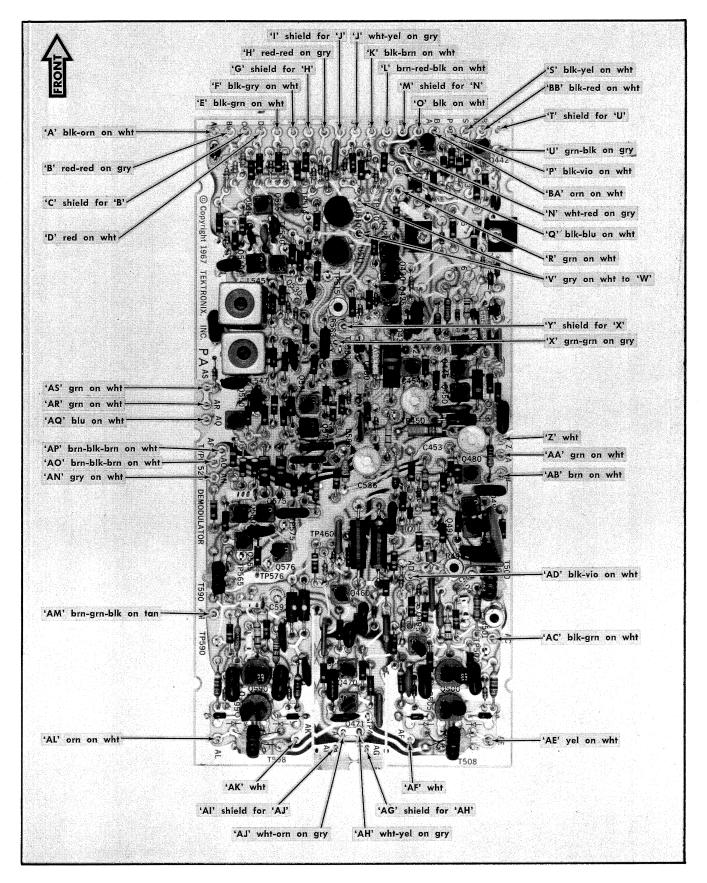


Fig. 4-158. Demodulator board; wire color codes for instruments SNB150100 and up.

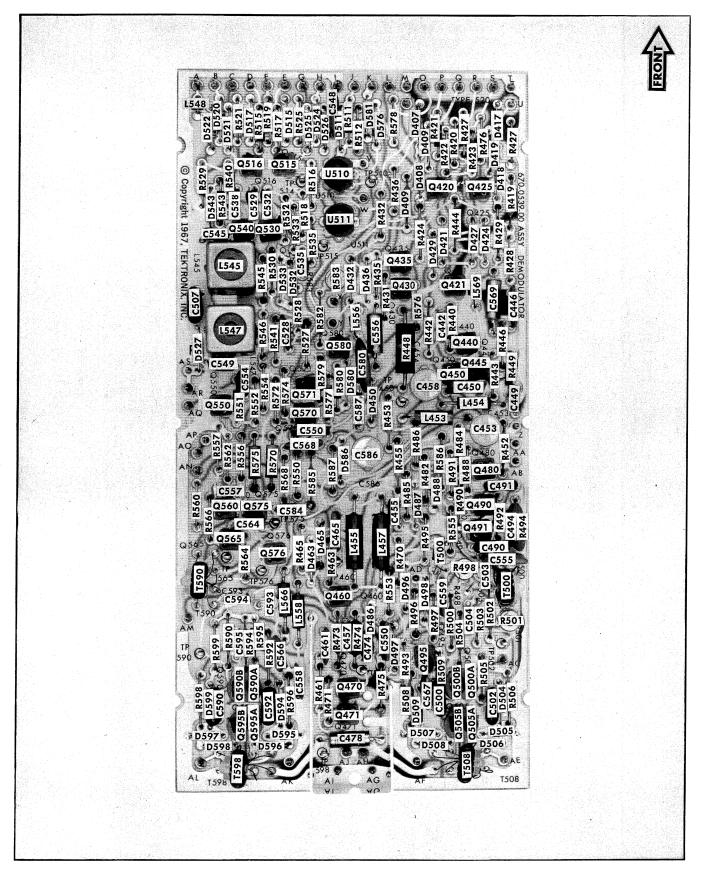


Fig. 4-16A. Demodulator board; component identification for instruments below SN B150100.

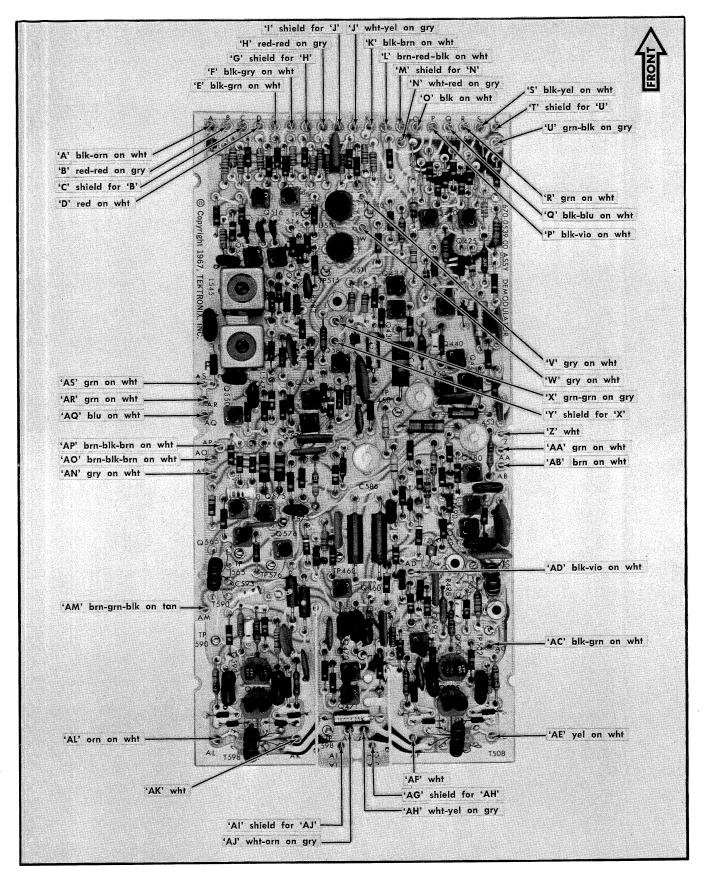


Fig. 4-16B. Demodulator board; wire color codes for instruments below SN B150100.

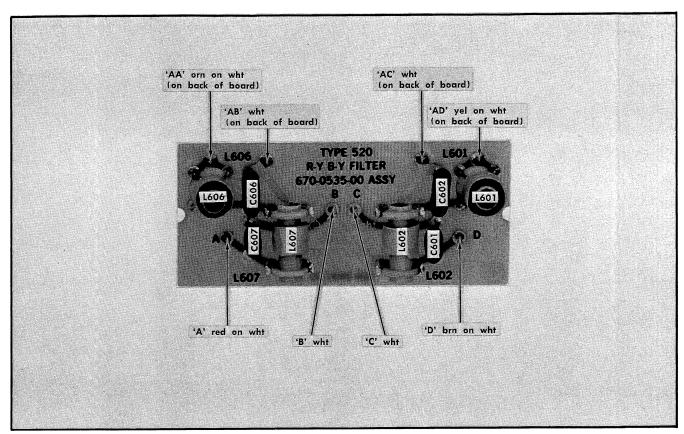


Fig. 4-17. R-Y B-Y Filter board; component identification and wire color codes.

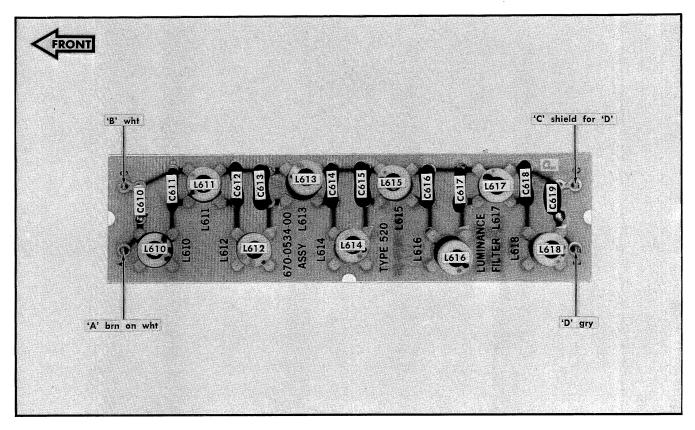


Fig. 4-18. Luminance Filter board; component identification and wire color codes.

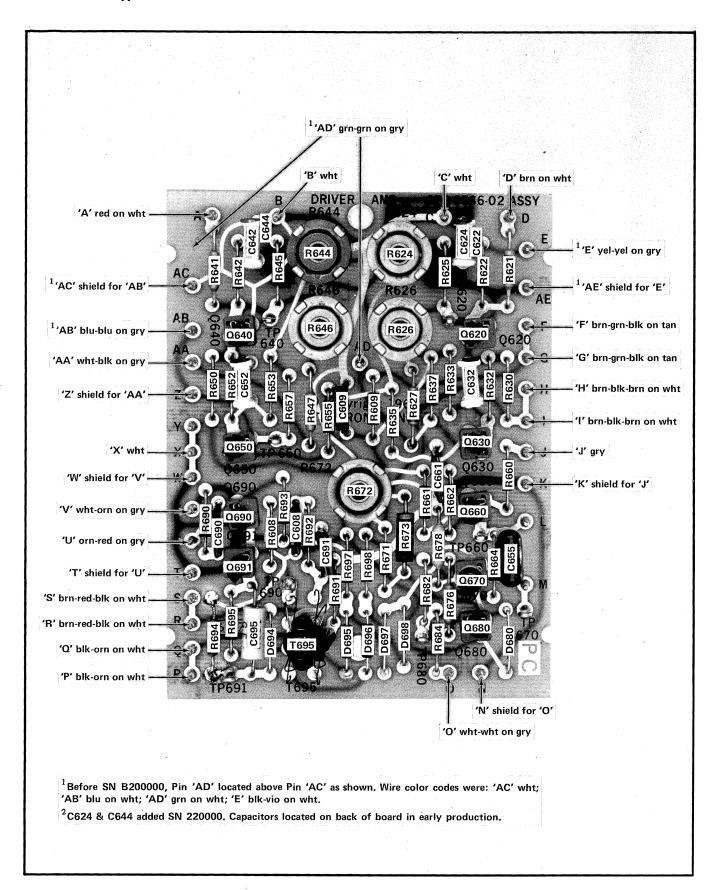


Fig. 4-19A. Driver Amplifier board; component identification and wire color codes for instruments SN B150100 and up.

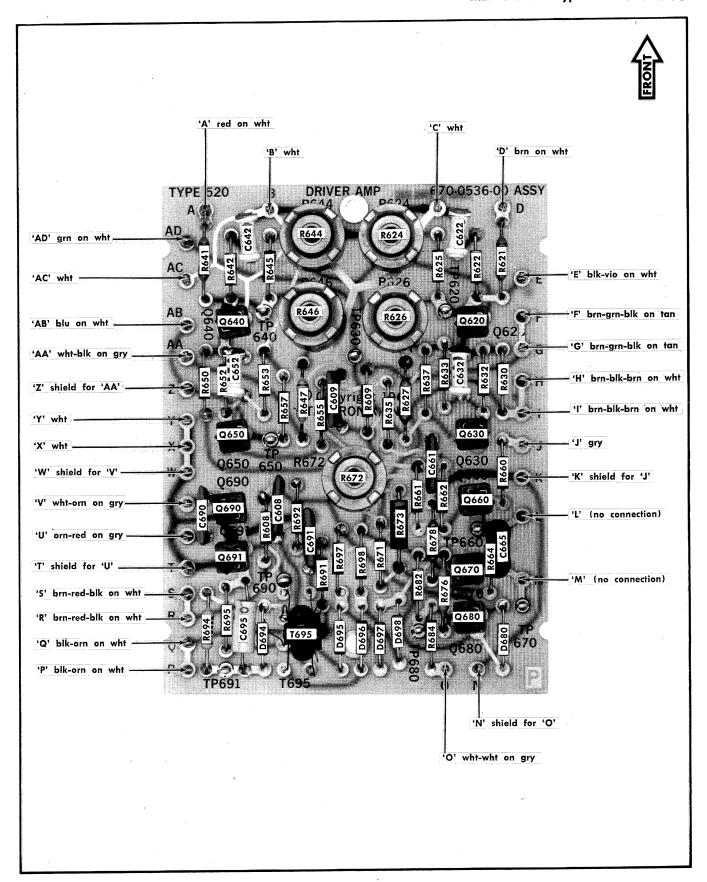


Fig. 4-19B. Driver Amplifier board; component identification and wire color codes for instruments below SN B150100.

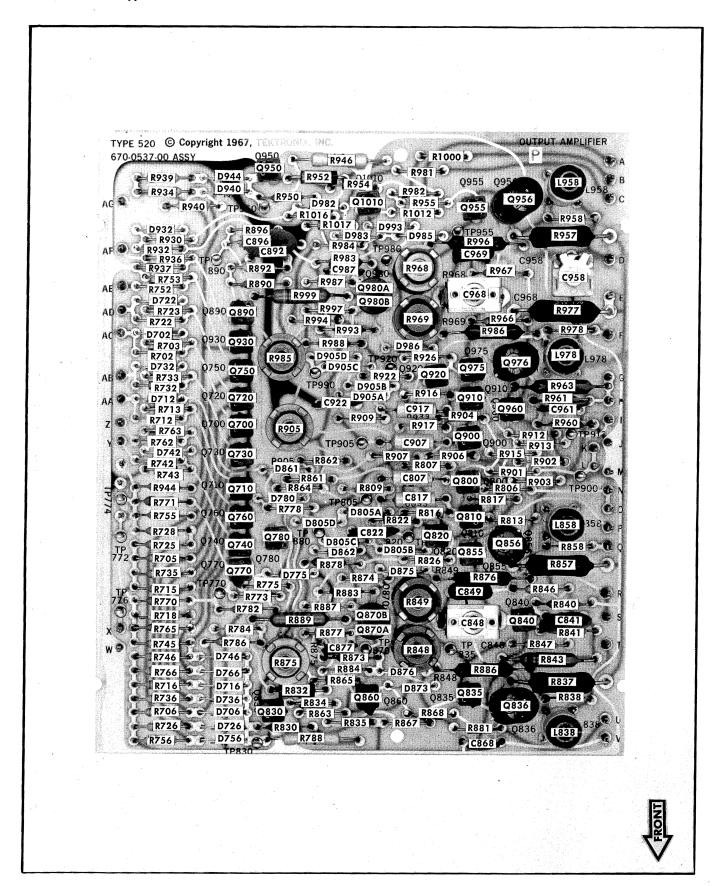


Fig. 4-20. Output Amplifier board; component identification.

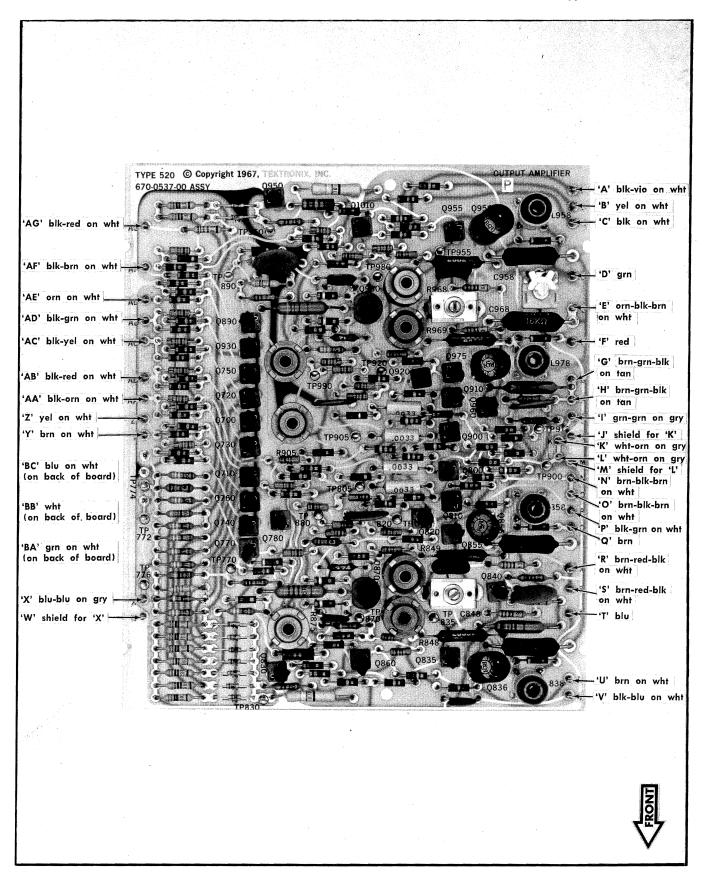


Fig. 4-21. Output Amplifier board; wire color codes.

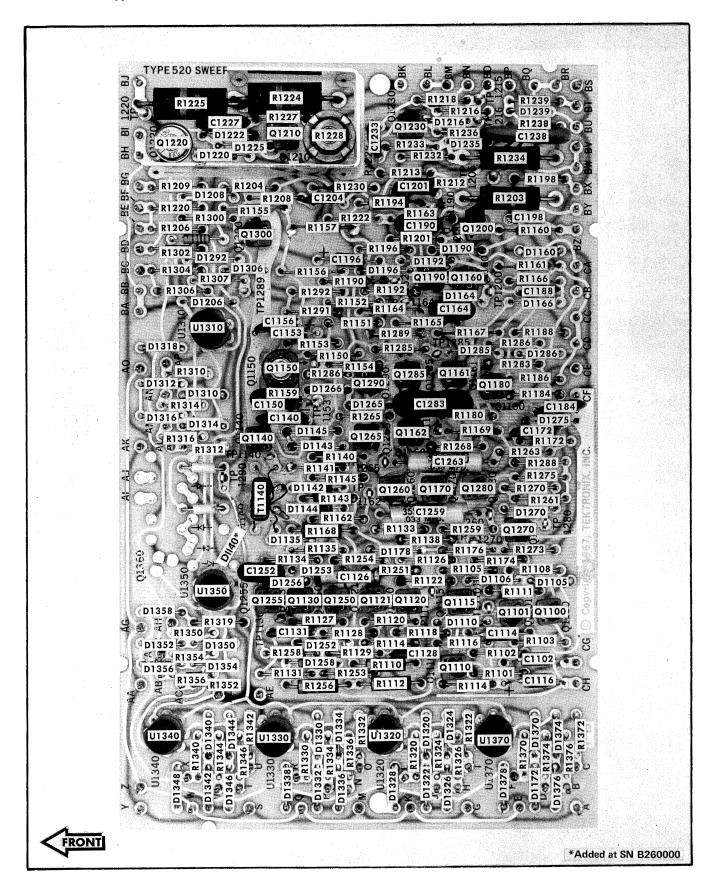


Fig. 4-22A. Sweep board; component identification for instruments SN B150100 and up.

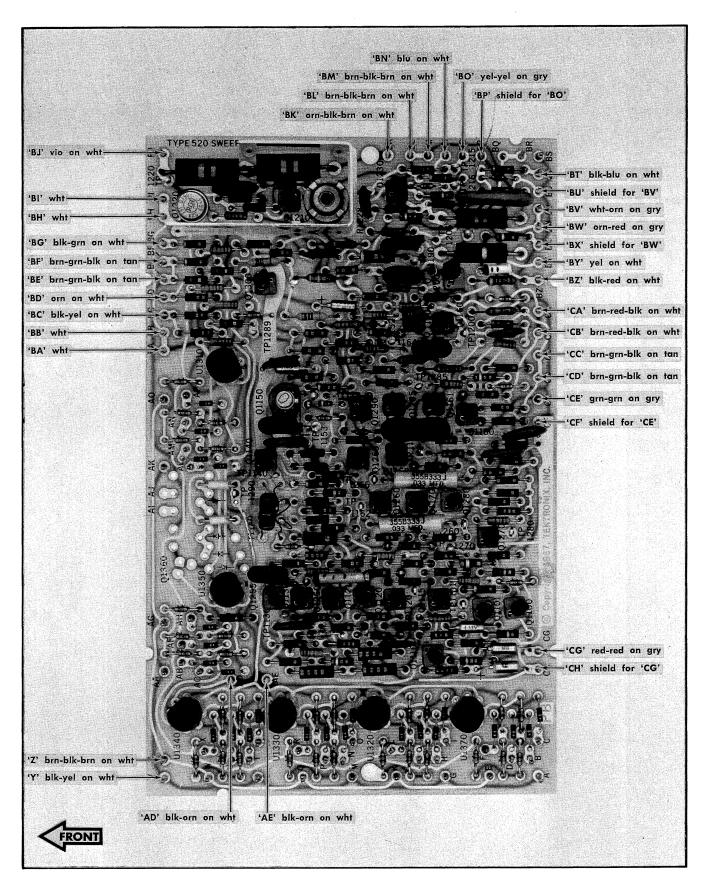


Fig. 4-22B. Sweep board; wire color codes for instruments SN B150100 and up.

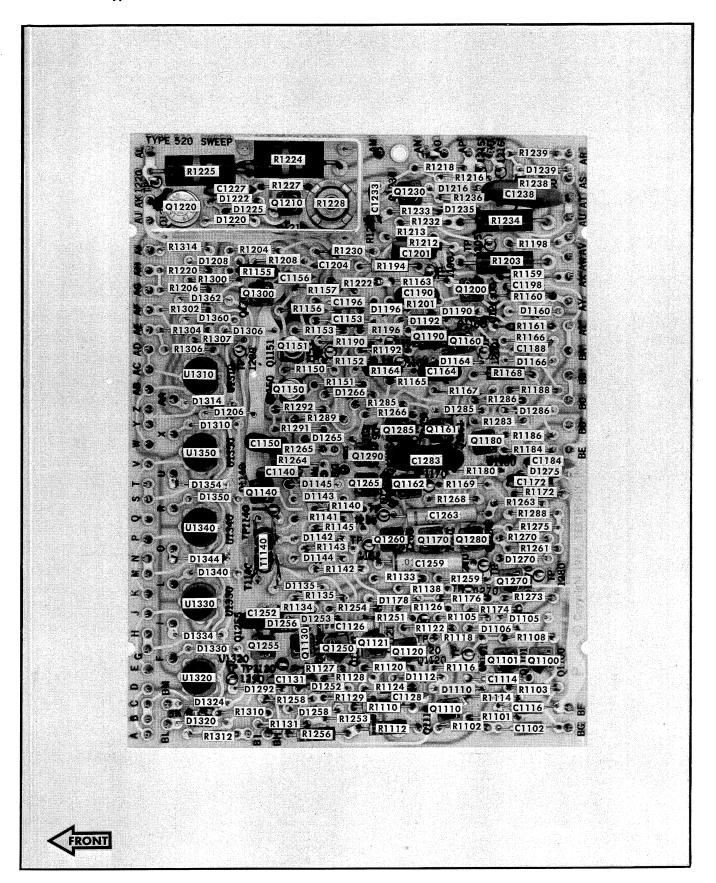


Fig. 4-23A. Sweep board; component identification for instruments below SN B150100.

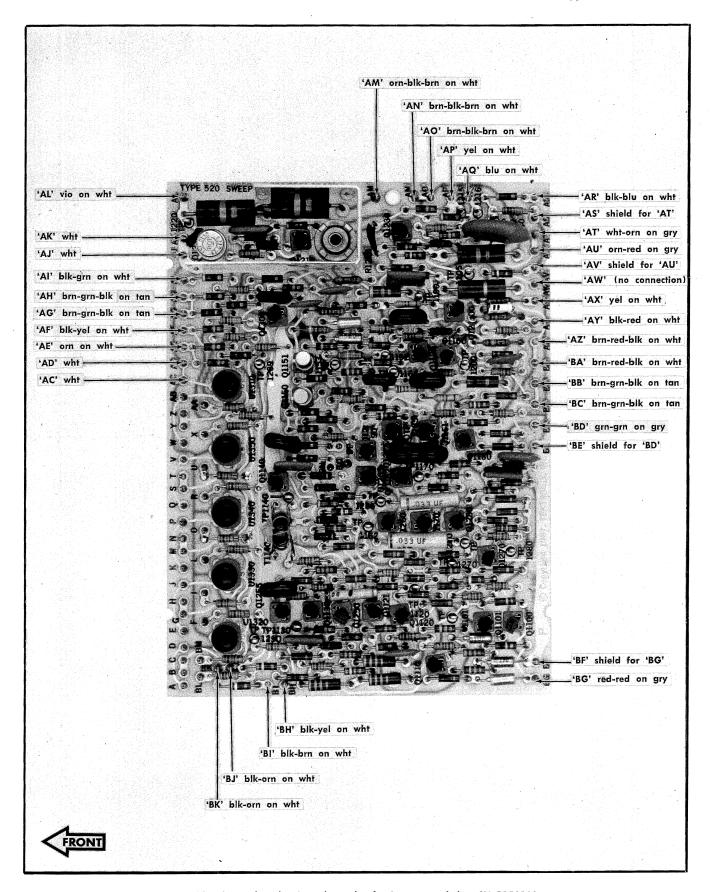


Fig. 4-23B. Sweep board; wire color codes for instruments below SN B150100.

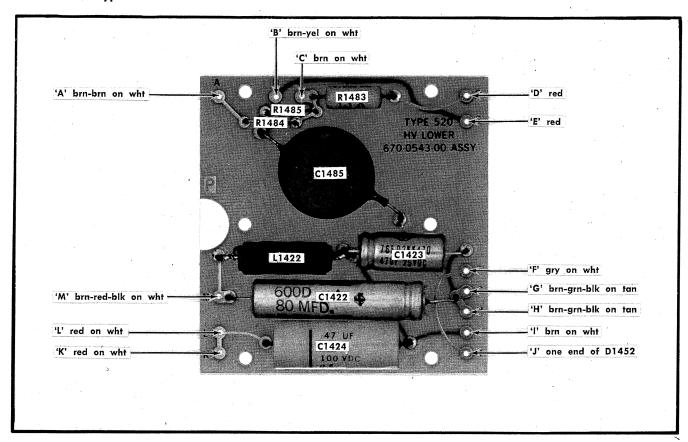


Fig. 4-24. Lower High Voltage board; component identification and wire color codes.

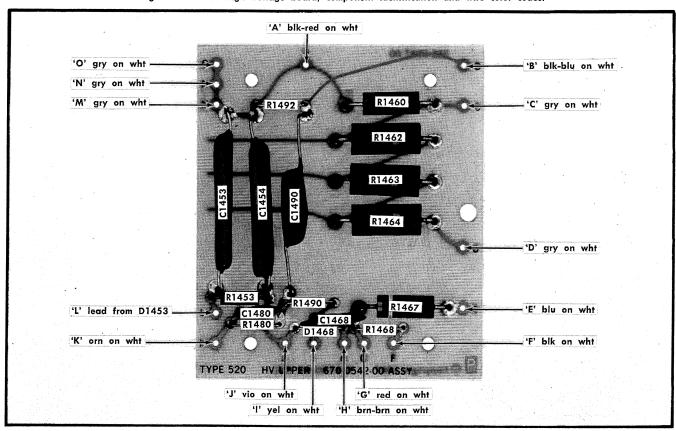


Fig. 4-25. Upper High Voltage board; component identification and wire color codes.

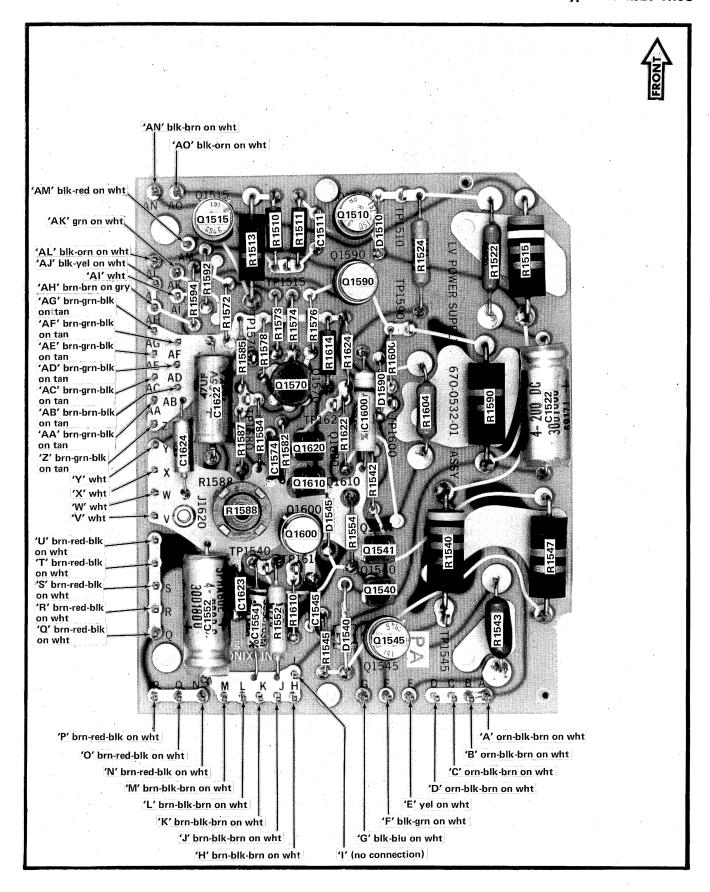


Fig. 4-26A. Low Voltage Power Supply circuit board showing components and wire codes for instruments SN B080000-up.

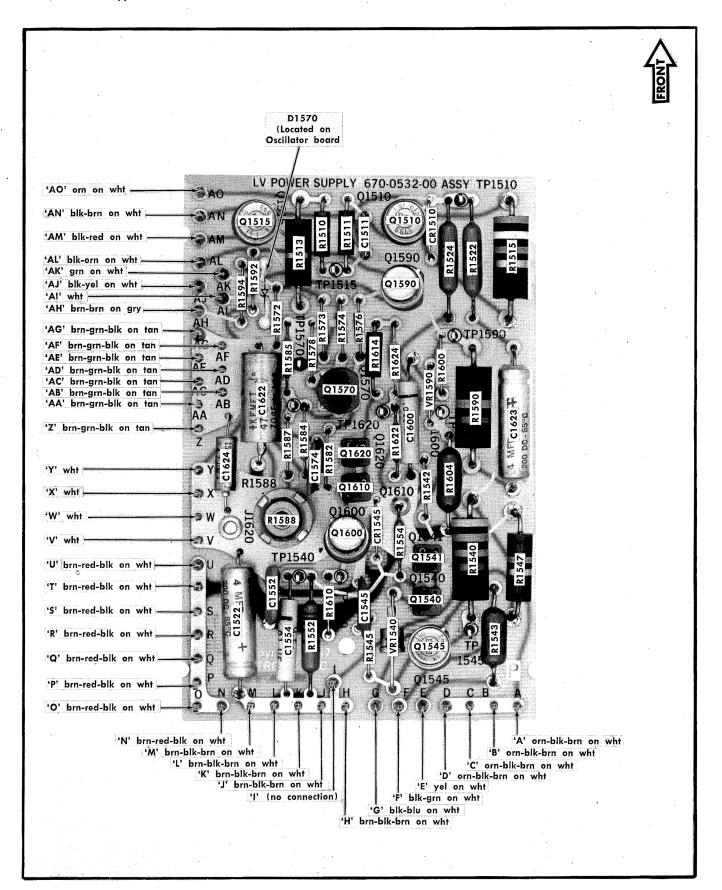


Fig. 4-26B. Low Voltage Power Supply circuit board showing components and wire codes for instruments SN B020100-B079999.

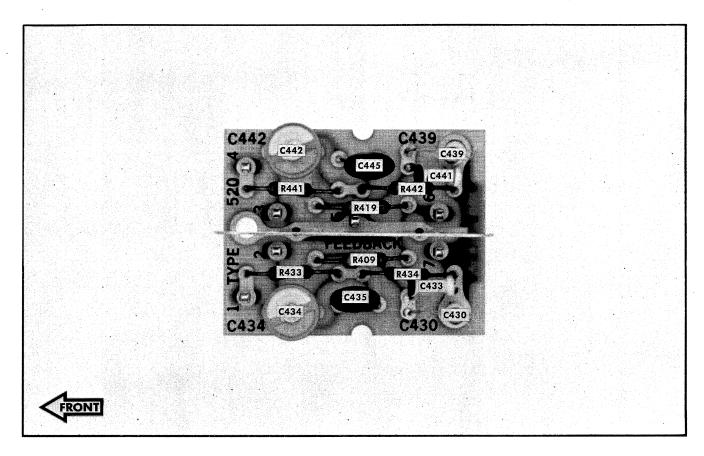


Fig. 4-27. Feedback board; component identification for instruments SN B150100 and up only.



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# SECTION 5 PERFORMANCE CHECK

Change information, if any, affecting this section will be found at the rear of the manual.

#### Introduction

This section of the manual provides a procedure for rapidly checking the performance of the Type R520. This procedure checks the operation of the instrument without removing the covers (except to gain access to internal test points) or making internal adjustments. However, screwdriver adjustments which are located on the front and rear panels are adjusted in this procedure.

If the instrument does not meet the performance requirements given in this procedure, internal checks and/or adjustments are required. See the Calibration section. All performance requirements given in this section correspond to those given in the Specification section.

#### NOTE

All waveforms shown in this section are actual waveform photographs taken with a Tektronix Oscilloscope Camera System.

#### Recommended Equipment

The following equipment is recommended for a complete performance check. Specifications given are the minimum necessary to perform this procedure. All equipment is assumed to be calibrated and operating within the given specifications. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

For the most accurate and convenient performance check, special calibration fixtures are used in this procedure. These calibration fixtures are available from Tektronix, Inc. Order by part number through your local Tektronix Field Office or representative.

- 1. Test oscilloscope. Bandwidth, DC to at least 10 MHz; minimum deflection factor, 0.005 volt/division. Tektronix Type 547 Oscilloscope with Type 1A1 and ¹Type 1A5 Plug-In Units, and a Tektronix P6023 (10X) and P6028 (1X) Probes recommended.
- 2. Video signal source. Signals available, unmodulated linearity staircase, 3.58 MHz (CW) variable between 1.5 and 2.5 V peak to peak, sync pulses at a line rate variable between 3.5 V and 7.5 V (0.7 V and 1.4 V) peak to peak, color bars of the proper amplitude for 75% saturation measurements, and multiburst within 1% of being flat at all frequencies. For example, Riker Industries, Inc. or Telemet Company equipment.
- 3. Medium frequency constant amplitude signal generator. Frequency, variable from 3 MHz to 18 MHz; output amplitude, adjustable to 1 volt; amplitude regulation accuracy,

Required only if step 32 is performed.

within  $\pm 5\%$ . Tektronix Type 191 Constant Amplitude Signal Generator recommended.

- 4. Wide bandwidth constant amplitude signal generator. Frequency, variable from below 25 Hz to above 5 MHz; output amplitude adjustable from about 1 volt to about 2 volts; amplitude regulation, 0.5%. For example Hewlett-Packard Model 652A generator.
- 5. Square-wave generator. Frequency, 20 kHz, to 40 kHz; output amplitude, adjustable to 1 volt. Tektronix Type 106 Square-Wave Generator recommended.
- 6. Standard Amplitude Calibrator. Amplitude accuracy, within 0.25%; signal amplitude, 1 volt; output frequency, 1 kHz. Tektronix calibration fixture 067-0502-00 recommended.
- 7. Cable (three) (SN B180980-up). Impedance, 75 ohm; length, 42 inches; connectors, BNC. Tektronix Part No. 012-0074-00.
- 7A. Cable (three) (SN 100-B170979). Impedance, 75 ohm; length, 42 inches; connectors, UHF. Tektronix Part No. 012-0002-00.
- 8. 067-0565-00 ramp and sine wave adder. Tektronix calibration fixture 067-0565-00 recommended.
- 9. Adapter (SN 100-B170979). Connectors, UHF female to BNC male. Tektronix Part No. 103-0032-00.
- 11. Adapter (SN 100-B170979). Connectors, UHF male to BNC female. Tektronix Part No. 103-0015-00.
- 13. Termination (two) (SN B180980-up). Impedance, 75 ohm; connector, BNC; type, end-line; accuracy  $\pm 3\%$ . Tektronix Part No. 011-0102-00.
- 13A. Termination (two) (SN 100-B170979). Impedance, 75 ohm; connector, UHF; type, end-line; accuracy  $\pm 3\%$ . Tektronix Part No. 011-0023-00.
- 14. Adapter. Connectors, GR to BNC male. Tektronix Part No. 017-0064-00.
- 15. Adapter. Connectors, UHF male to BNC female. Tektronix Part No. 103-0015-00.
- 16. Attenuator. Connectors, BNC; impedance, 50 ohms to 75 ohms; type, minimum loss when going from a 50 ohm system to a 75 ohm system. Tektronix Part No. 011-0057-00.
- 17. Termination (three). Impedance, 75 ohm; connector, UHF; type, end-line; accuracy,  $\pm 3\%.$  Tektronix Part No. 011-0023-00.
- 18. Termination. Impedance, 75 ohm; connectors, BNC; type, feed-thru; accuracy,  $\pm 3\%$ . Tektronix Part No. 011-0055-00.

#### PERFORMANCE CHECK PROCEDURE

#### **General**

In the following procedure, control settings or test equipment connections should not be changed except as noted. If only a partial check is desired, refer to the preceding step(s) for setup information. Type R520 control titles referred to in this procedure are capitalized (e.g., VERT POSITION).

The following procedure uses the equipment listed under Recommended Equipment. If equipment is substituted, control settings or setup may need to be altered to meet the requirements of the equipment used.

#### **Preliminary Procedure**

- 1. Connect the Type R520 to a suitable power source.
- 2. Set the front- and rear-panel controls of the Type R520 as follows:

#### Front-Panel Controls:

Signal Selector CHANNEL A	A CAL, FULL FIELD
100%-75%-MAX GAIN	75%
GAIN	CAL
PHASE	As is
A CAL	As is
B CAL	As is
φ REF	BURST
CHANNEL B	
100% <i>-7</i> 5%-GAIN	75%
GAIN	CAL
PHASE	As is
Display Selector	Υ
INTENSITY	As desired
LUMINANCE GAIN	CAL
SCALE ILLUM	As desired
CALIBRATED PHASE	0
POWER	ON

#### Left recessed front-panel controls:

The state of the s		
QUAD PHASE	As i	is
GAIN BAL	As i	S
HORIZ POSITION CLAMP	As i	s
BEAM ROTATE	As i	S
VERT POSITION CLAMP	As i	s

#### Right recessed front-panel controls:

FOCUS	As is
FIELD	1
VERT POSITION	As is
BURST FLAG TIMING	As is
SYNC	INT
HORIZ POSITION	As is

#### Rear-panel controls:

ASTIG	As	is
ORTHO	As	is
GEOM	As	is
UNBLANK BIAS	As	is

3. Set the Type R520 POWER switch to ON. Allow at least 20 minutes warm up at 25°C,  $\pm 5$ °C for checking instrument to the given accuracy.

#### 1. Adjust Geometry

REQUIREMENT—Vertical and/or horizontal lines should not have more than 0.05 centimeter of gradual bowing.

- a. Adjust the front-panel FOCUS control and the rearpanel ASTIG control (see Fig. 5-1) to obtain a well-defined display.
- b. CHECK—Type R520 display; should not show more than 0.05 centimeter of gradual bowing of the vertical or horizontal lines.
- c. ADJUST—GEOM control, R1472, (see Fig. 5-1) for minimum bowing of the vertical or horizontal lines.

#### 2. Adjust Astigmatism

REQUIREMENT—Should be a nearly perfect round spot in vector display when the FOCUS control is rotated fully counterclockwise.

- a. Cancel the Signal Selector A CAL pushbutton by momentarily depressing the CH A pushbutton. The Signal Selector FULL FIELD remains down.
  - b. Press the Display Selector VECTOR pushbutton.
- c. Rotate the FOCUS control to its fully counterclockwise position.
- d. CHECK—Type R520 display; should be a nearly perfect round spot near the center of the vector graticule.
- e. ADJUST—ASTIG control, R1476, see Fig. 5-1 until a nearly perfect round spot near the center of the graticule is obtained.
  - f. Set the FOCUS control to obtain a well-defined spot.

#### 3. Adjust CRT Alignment

REQUIREMENT—It must be possible to adjust the horizontal trace parallel to the 0°-180° axis of the vector graticle and perpendicular to the 90°-270° axis of the vector graticule.

- a. The Signal Selector FULL FIELD pushbutton remains depressed for this step.
  - b. Press the Display Selector Y pushbutton.
- c. CHECK—Type R520 trace alignment; trace should be parallel to the  $0^{\circ}$ -180° axis of the vector graticule.
- d. ADJUST—BEAM ROTATE control, R1470, (see Fig. 5-2) until trace is parallel to the 0°-180° axis of the vector graticule.

- e. CHECK—Type R520 trace alignment; horizontal trace should be perpendicular to the 90°-270° axis of the vector graticule.
- f. ADJUST-ORTH control, R1474, (see Fig. 5-1) until trace is perpendicular to the 90°-270° axis of the vector araticule.
- g. Repeat parts d and f of this step as necessary to remove interaction between the adjustments.

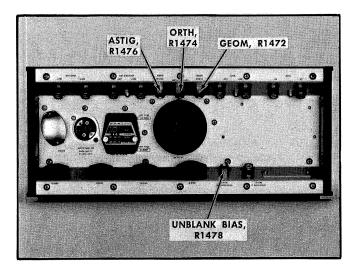


Fig. 5-1. Rear-panel control locations.

#### 4. Unblanking Bias

REQUIREMENT—The brightness of a test circle display must be adjustable so that the test circle has uniform intensity throughout its circumference.

- a. Press the Signal Selector A CAL pushbutton and the Display Selector VECTOR pushbutton.
- b. Reduce the display intensity until the test circle is barely visible.

CHECK-Type R520 display; test circle should have uni-

form intensity throughout its circumference.
d. ADJUST—UNBLANK BIAS control, R1478, (see Fig. 5-1) for a uniform intensity throughout the circumference of the test circle.

#### 5. Check VITS Intensity

REQUIREMENT—Display of a test signal must be at maximum brightness without any display defocusing.

- a. Connect a linearity staircase video signal to the CH A J1 connector via a 75 ohm coaxial cable.
- b. Connect a 75 ohm coaxial cable from the CH A J2 connector to the CH B J50 connector.
- c. Connect a 75 ohm end-line termination to the CH B J51 connector.
- d. Press Signal Selector CH A, A $\phi$  and VITS 18 pushbuttons.
  - e. Press the Display Selector LINE SWEEP pushbutton.

- f. CHECK-Type R520 display brightness; must be maximum without any display defocusing.
- g. Disconnect the video signal source, the two 75 ohm coaxial cables and the 75 ohm end-line termination.

#### 6. Adjust Vertical and Horizontal Position Clamps

REGUIREMENT—Must have enough adjustment range to position the spot to the center of the vector graticule.

- a. Depress the Signal Selector FULL FIELD pushbutton and the Display Selector VECTOR pushbutton.
- b. Reduce the intensity somewhat, so the displayed spot on the CRT of the Type R520 will not burn the phosphor.
- c. CHECK—Type R520 displayed spot position; must be at the center of the vector graticule.
- d. ADJUST-VERT POSITION CLAMP control, R880, (see Fig. 5-2) and HORIZ POSITION CLAMP control, R1002, (see Fig. 5-2) to position the spot to the centetr of the vector graticule.

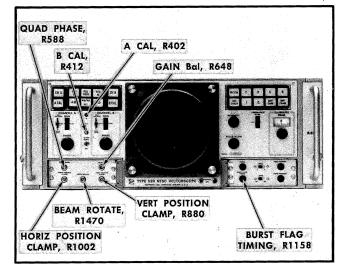


Fig. 5-2. Front-panel control locations.

#### 7. Adjust Channel A Gain

REQUIREMENT—Must have enough adjustment range to position the spot to the center of the vector graticule.

- a. Depress the Signal Selector A CAL and the Display Selector Y pushbuttons. The remaining pushbuttons remain as they are.
- b. CHECK-Type R520 display amplitude; must be exactly 140 IRE units.
- c. ADJUST-A CAL control, R402, (see Fig. 5-2) until the display on the Type R520 is exactly 140 IRE units in amplitude.

#### 8. Adjust Channel B Gain

REQUIREMENT—Must have enough adjustment range to set the gain of channel B to unity.

#### Performance Check—Type 520/R520 NTSC

- a. Depress the B CAL and  $B\phi;$  cancel the A CAL Signal Selector pushbuttons. The remaining pushbuttons remain as they are.
- b. CHECK—Type R520 display amplitude; must be exactly 140 IRE units.
- c. ADJUST—B CAL control, R412, (see Fig. 5-2) until the display on the Type R520 is exactly 140 IRE units in amplitude.

#### 9. Adjust Burst Flag Timing

REQUIREMENT—Must have enough adjustment range to cause equal amounts of the rising and falling portions of the burst to intensify.

- a. Press the Signal Selector CH A and A $\phi$  pushbuttons and the Display Selector LINE SWEEP pushbutton.
- b. Connect a color bar video signal to CH A J1 connector via a 75 ohm coaxial cable.
- c. Connect a 75 ohm end-line termination to the CH A  ${\bf J}2$  connector.
- d. Rotate the channel A PHASE control to obtain maximum positive-going burst amplitude; see Fig. 5-3.

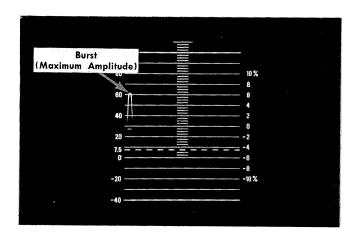


Fig. 5-3. Correct Type R520 color bar display for adjusting burst flag timing.

- e. CHECK—Type R520 display intensified portions; the intensified rising and falling portions of the burst part of the display must be equal. It may be necessary to reduce the display intensity so the intensified portions may be seen.
- f. ADJUST—BURST FLAG TIMING, R1158, (see Fig. 5-2) until the intensified rising and falling portions of the burst are equal.
- g. Disconnect the video signal source, the 75 ohm co-axial cable and the 75 ohm end-line termination.

#### 10. 33° Phase Shifter

REQUIREMENT—Must be a 33°,  $\pm 2^{\circ}$  phase shift when the I or Q Display Selector pushbutton is pressed.

a. Press the Display Selector VECTOR pushbutton. The remaining pushbuttons remain as they are.

- b. Connect a color bar video signal to CH A J1 connector via a 75 ohm coaxial cable.
- c. Connect a 75 ohm end-line termination to the CH A J2 connector.
- d. Line up the burst vector on the Type R520 exactly with the I marking on the vector graticule using the channed A PHASE control.
  - e. Press the Display Selector Q pushbutton.
- f. Rotate the CALIBRATED PHASE control until the single trace just starts to break into two traces.
- g. CHECK—Type R520 CALIBRATED PHASE dial reading; 2° or less from zero.
- h. Reset the CALIBRATED PHASE dial to its zero degree dial point.
  - i. Press the Display Selector VECTOR pushbutton.
- j. Line up the burst vector on the Type R520 exactly with the Q marking on the vector graticule using the channel A PHASE control.
  - k. Press the Display Selector I pushbutton.
- I. Rotate the CALIBRATED PHASE control until the single trace just starts to break into two traces.
- m. CHECK—Type R520 CALIBRATED PHASE dial reading; 2° or less from zero.
- n. Reset the CALIBRATED PHASE dial to its zero degree dial point.
- o. Disconnect the 75 ohm coaxial cable, video signal source and the 75 ohm end-line termination.

#### 11. Adjust Subcarrier Balance

REQUIREMENT—Trace must remain within  $\pm 3$  IRE units no matter whether the LINE SWEEP, I, Q or DIFF PHASE Display Selector pushbutton is pressed.

- a. Cancel all the Signal Selector pushbuttons except the  $\ensuremath{\mathsf{FULL}}$  FIELD pushbutton.
- b. Press the Signal Selector A CAL pushbutton and the Display Selector LINE SWEEP pushbutton.
  - c. Note trace position.
  - d. Press the Display Selector I pushbutton.
  - e. Note trace position.
  - f. Press the Display Selector Q pushbutton.
  - g. Note trace position.
  - h. Press the Display Selector DIFF PHASE pushbutton.
  - i. Note trace position.
- j. CHECK—Trace positions; the trace noted in parts c (LINE SWEEP trace), e (I trace), g (Q trace) and i (DIFF PHASE trace) must be within  $\pm 3$  IRE units of the same location.
  - k. Press the Display Selector DIFF PHASE pushbutton.
- I. CHECK—Type R520 display; it should consist of a single trace.

- m. Press the Display Selector Q pushbutton.
- n. CHECK—Type R520 display; it should consist of a single trace.

#### 12. Adjust Gain Balance

REQUIREMENT—Must have enough range to adjust the horizontal amplifier gain to be the same as the vertical gain.

- a. Press the Signal Selector  $A\phi$  pushbutton and the Display Selector VECTOR pushbutton. The remaining pushbuttons remain as they are.
- b. CHECK—Type R520 displayed test circle circularity; test circle should touch the inscribed circle on the vector graticule at the 0°, 90°, 180° and 270° points on the circumference of the test circle.
- c. ADJUST—GAIN BAL control, R648, (see Fig. 5-2) until the test circle touches the inscribed circle on the vector graticule at all points on its circumference.

#### 13. Adjust Quadrature Phase

REQUIREMENT—The two circles which make up the test circle must overlay each other at the 45° points on their circumference within 0.0366 inch.

- a. Cancel the Signal Selector A CAL and  $A\phi$  pushbuttons and press the B CAL pushbutton. The remaining pushbuttons remain as they are.
- b. Connect a linearity staircase video signal to the CH A J1 connector via 75 ohm coaxial cable.
- c. Connect a 75 ohm end-line termination to the CH A J2 connector.
- d. CHECK—Type R520 display; test circles should overlay each other at the 45° points on their circumference within 0.0366 inch.
- e. ADJUST—QUAD PHASE control, R588, (see Fig. 5-2) until the test circles overlay each other at the 45° point on their circumference within 0.0366 inch.
- f. Disconnect the video signal source, 75 ohm coaxial cable and the 75 ohm end-line termination.

#### 14. Check Chroma Bandwidth

REQUIREMENT—Upper and lower chorminance bandwidth points must be between 400 kHz and 600 kHz above and below 3.58 MHz.

- a. Press the Signal Selector CH A and  ${\rm A}\phi$  pushbuttons and Display Selector LINE SWEEP pushbutton. Cancel the Signal Selector B CAL pushbutton. The remaining pushbuttons remain as they are.
- b. Connect a 3.58 MHz sine wave signal about 0.75 volt in amplitude from a medium frequency constant amplitude signal generator via a 5 ns coaxial cable, a GR to BNC male adapter, a 75 ohm to 50 ohm minimum loss attenuator and a BNC female to UHF male adapter to the Type R520 CH A J1 connector.

- ic. Connect a 75 ohm end-line termination to the CH A J2 connector.
- d. Adjust the signal generator output amplitude control to obtain a display amplitude of exactly 140 IRE units.
- e. Increase the output frequency of the signal generator until the display amplitude falls to 98 IRE units (70% of its initial amplitude).
- f. CHECK—Signal generator output frequency; must be between 400 kHz and 600 kHz above the 3.58 MHz initial frequency.
- g. Decrease the output frequency of the signal generator through and below 3.58 MHz until the displayed amplitude falls to 98 IRE units (70% of its initial amplitude).
- h. CHECK—Signal generator output frequency; must be between 400 kHz and 600 kHz below the 3.58 MHz initial frequency.
- i. Disconnect the medium frequency constant amplitude signal generator, the 5 ns coaxial cable, GR to BNC male adapter, 75 ohm to 50 ohm minimum loss attenuator, the BNC female to UHF male adapter and the 75 ohm end-line termination.

#### 15. Check Luminance Bandwidth

REQUIREMENT—Multiburst input video signal should present a display on the Type R520 as shown in Fig. 5-4.

- a. Press the Display Selector Y pushbutton.
- b. Connect a multiburst video signal to CH A J1 connector via a 75 ohm coaxial cable.
- c. Connect a 75 ohm end-line termination to the CH A J2 connector.

#### NOTE

The multiburst video signal must be within  $\pm 1\%$  of flat at all frequencies or this check will not be valid.

d. CHECK—Type R520 display; must appear the same as that shown in Fig. 5-4, see the luminance bandwidth table for the numerical figures for the display.

#### **LUMINANCE BANDWIDTH TABLE**

Multiburst Frequency	Type R520 Response Display	Typical Type R520 IRE Units of Display (Standard Video Transmission Engi- neering Advisory Commis- sion, VITEAC)
500 kHz	90%, ±4%	77 minimum 81 nominal 85 maximum
1.5 MHz	40%, ±4%	32 minimum 36 nominal 40 maximum
2.0 MHz	20%, ±4%	14 minimum 18 nominal 22 maximum
3.0 MHz	≤3%	<b>≤2.5</b>
3.6 MHz	≤1%	≤1
4.2 MHz	≤1%	≤1

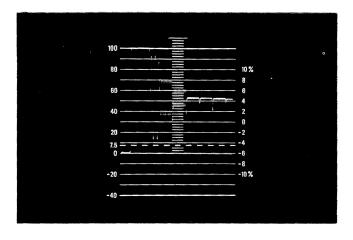


Fig. 5-4. Correct multiburst video signal display on Type R520.

e. Disconnect the video signal source, 75 ohm coaxial cable and the 75 ohm end-line termination.

#### 16. Check Luminance Step Response

REQUIREMENT—Aberrations on a 100 IRE units high square wave must be 1% or less of the display height.

- a. Connect a 30 kHz square-wave signal about 1 volt in amplitude from a square-wave generator via a 5 ns coaxial cable, a GR to BNC male adapter, a 75 ohm to 50 ohm minimum loss attenuator and a BNC female to UHF male adapter to the Type R520 CH A J1 connector.
- b. Connect a 75 ohm end-line termination to the CH A J2 connector.
- c. Slowly change the frequency of the square-wave generator until a stable display is obtained.
- d. Adjust the output amplitude of the square-wave generator until the Type R520 display is exactly 100 IRE units in amplitude.
- e. CHECK—Type R520 display; aberrations on the top of the waveform must be 1% or less of 100 IRE units in amplitude.
- f. Disconnect the square-wave generator, the 5 ns coaxial cable, 75 ohm to 50 ohm minimum loss attenuator, GR to BNC male adapter, BNC female to UHF male adapter and 75 ohm end-line termination.

#### 17. Check Input Amplitude Range

REQUIREMENT—Stable display must be obtained for input signals having sync pulse amplitudes from 200 mV to 400 mV (overall signal amplitudes from 0.7 V to 1.4 V).

- a. Press the Display Selector LINE SWEEP pushbutton.
- b. Connect a color bar video signal to the CH A J1 connector via a 75 ohm coaxial cable.
- c. Connect a 75 ohm end-line termination to the CH A J2 connector.
- d. Connect a  $10\times$  probe from the test oscilloscope vertical input connector to the input signal going to the CH A J1 connector.

- e. Set the test oscilloscope for a vertical deflection of 0.01 V/division, AC coupled, at a sweep rate of 10  $\mu$ s/division with internal triggering.
- f. Set the sync pulse amplitude of the color bar video signal to exactly 286 mV (overall signal amplitude, 1 volt) as measured on the test oscilloscope.
- g. Rotate the channel A PHASE control to obtain maximum positive-going burst amplitude; see Fig. 5-3.
- h. Check that the intensified rising and falling portions of the burst part of the Type R520 display are equal. It may be necessary to reduce the display intensity so the intensified portion may be seen. If the position of the intensified portion is not correct, adjust the BURST FLAG TIMING control, R1158, (see Fig. 5-2) until the intensified rising and falling portions of the burst are equal.
- i. Reduce the sync pulse amplitude of the color bar video signal to exactly 200 mV (overall signal amplitude, 0.7 volt) as measured on the test oscilloscope.
- j. Set the Type R520 SYNC switch to EXT for about 15 seconds, then return it to its INT position.
  - k. CHECK—Type R520 display; should be stable.
- I. Increase the sync pulse amplitude of the color bar video signal to exactly 400 mV (overall signal amplitude, 1.4 volts) as measured on the test oscilloscope.
- m. Set the Type R520 SYNC switch to EXT for about 15 seconds, then return it to its INT position.
  - n. CHECK—Type R520 display; should be stable.
- o. Disconnect the video signal source, 75 ohm coaxial cable, 75 ohm end-line termination,  $10 \times$  probe and the test oscilloscope.

## 18. Check Phase Accuracy and Incremental Phase Accuracy

REQUIREMENT—Error between dots and 10° vector graticule marks must be 1° or less at any point on the inscribed vector graticule circle. Error between dots and 2° vector graticule marks must be 0.5° or less within 10° either side of an established reference point.

#### NOTE

Bottom cover of the Type R520 must be removed to gain access to the test point.

- a. Press the Display Selector VECTOR pushbutton and set the  $\phi$  REF switch to EXT.
- b. Connect a 75 ohm coaxial cable from a 067-0546-00 calibration fixture 3.579545 MHz subcarrier 2 V p-p connector to the Type R520 EXT CW  $\phi$  REF J311 connector.
- c. Connect a 75 ohm end-line termination to the Type R520 EXT CW  $\phi$  REF J310 connector.
- d. Connect a 75 ohm coaxial cable from the 067-0546-00 calibration fixture 3.589488 MHz sideband video 707 mV connector to the Type R520 CH A J1 connector.
- e. Connect a 75 ohm end-line termination to the CH A J2 connector.

- f1. For instruments SN B150100 and up, connect a  $1\times$  probe from the 067-0546-00 calibration fixture phase-mark pulse output connector via a UHF male to BNC female adapter to pin BT on the Sweep board; see Fig. 5-51).
- f2. For instruments below SN B150100, connect a  $1\times$  probe from the 067-0546-00 calibration fixture phase-mark pulse output connector via a UHF male to BNC female adapter to TP 1230 junction of Q1230 collector and D1235 on the Sweep board, see Fig. 5-5(b).

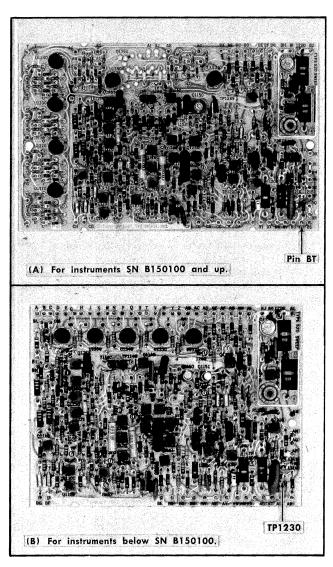


Fig. 5-5. Sweep board test point location.

- g. Connect a 75 ohm coaxial cable between the 067-0546-00 calibration fixture h sync 1 V neg connector and the Type R520 EXT SYNC J120 connector.
- h. Connect a 75 ohm end-line termination to the EXT SYNC J121 connector.
  - i. Set the Type R520 SYNC switch to EXT.
- j. Set the 067-0546-00 calibration fixture to produce positive dots 10° apart.

- k. Adjust the channel A PHASE control to align a dot with an arbitrarily established 0° point at one of the major points on the vector graticule.
- I. CHECK—Type R520 display; the error between the 10° dots from the 067-0546-00 calibration fixture and the 10° marks on the vector graticule must be 1° or less.
- m. Set the 067-0546-00 calibration fixture for an output of positive dots 2° apart.
- n. Adjust the channel A PHASE control to align a dot with the arbitrarily established 0° point.
- o. CHECK—Type R520 display; the area between the arbitrarily established 0° point and a point 10° away must have an error of 0.5° or less between the 2° dots from the 067-0546-00 calibration fixture and the 2° vector graticule marks.
- p. Disconnect the 067-0546-00 calibration fixture, the three 75 ohm coaxial cables, the three 75 ohm end-line terminations,  $1\times$  probe and the UHF male to BNC female adapter.

# 19. Check Calibrated Phase Range and Accuracy

REQUIREMENT—Rotating the CALIBRATED PHASE dial from  $-15^\circ$  to  $+15^\circ$  must cause a vector display rotation of  $30^\circ$ ,  $\pm 4^\circ$ . CALIBRATED PHASE dial accuracy must be within  $\pm 10\%$  per  $2^\circ$  change and within  $\pm 10\%$  or  $0.5^\circ$ , whichever is the lesser, of the correct dial reading from  $+14^\circ$  through  $-14^\circ$ .

#### NOTE

Bottom cover of the Type R520 must be removed to gain access to the test point.

- a. Set the  $\phi$  REF switch to Burst and SYNC switch to INT. The pushbuttons remain as they are.
- b. Connect a linearity staircase video signal to CH A J1 connector via a 75 ohm coaxial cable.
- c. Connect a 75 ohm end-line termination to CH A J2 connector.
  - d. Set the CALIBRATED PHASE dial to -15°.
- e. Using the channel A PHASE control set the Type R520 displayed vector to an arbitrarily established 0° point on the vector graticule.
  - f. Set the CALIBRATED PHASE dial to +15°.
- g. CHECK—Type R520 display; displayed vector should have rotated 30°, ±4° clockwise.
- h. Disconnect the video signal source, 75 ohm coaxial cable and 75 ohm end-line termination.
- i. Set the  $\phi$  REF switch to EXT and the CALIBRATED PHASE dial to 0.
- j. Connect a 75 ohm coaxial cable from a 067-0546-00 calibration fixture 3.579545 MHz subcarrier 2 V p-p connector to the Type R520 EXT CW  $\phi$  REF J311 connector.
- k. Connect a 75 ohm end-line termination to the Type R520 EXT CW  $\phi$  REF J310 connector.

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- I. Connect a 75 ohm coaxial cable from the 067-0546-00 calibration fixture 3.589488 MHz sideband video 707 mV connector to the Type R520 CH A J1 connector.
- m. Connect a 75 ohm end-line termination to the CH A J2 connector.
- n1. For instrument SN B150100 and up, connect a  $1\times$  probe from the 067-0546-00 calibration fixture phase-mark pulse output connector via a UHF male to BNC female adapter to pin BT on the Sweep board; see Fig. 5-5(a).
- n2. For instruments below SN B150100, connect a  $1\times$  probe from the 067-0546-00 calibration fixture phase-mark pulse output connector via a UHF male to BNC female adapter to TP1230 (junction of Q1230 collector and D1235) on the Sweep board; see Fig. 5-5(b).
- o. Connect a 75 ohm coaxial cable between the 067-0570-00 calibration fixture h sync 1 V neg connector and the Type R520 EXT SYNC J120 connector.
- p. Connect a 75 ohm end-line termination to the EXT SYNC J121 connector.
  - q. Set the Type R520 SYNC switch to EXT.
- r. Set the 067-0546-00 calibration fixture to produce positive dots 2° apart.
- s. Adjust the channel A PHASE control to align a dot with an arbitrarily established 0° point on the vector graticule.
- t. Rotate the CALIBRATED PHASE control from  $+14^{\circ}$  toward  $-14^{\circ}$  in increments of  $2^{\circ}$ .
- u. CHECK—Type R520 display 2° dot which corresponds to the dial reading being checked when that dot is aligned with the established 0° point; the dial error between any 2° increment of the dial must be 2°, within  $\pm 0.2$ ° of the dial setting noted when the dot for the previous dial setting was aligned with the established 0° point.
  - v. Set the CALIBRATED PHASE dial to  $+14^{\circ}$ .
- w. Adjust the channel A PHASE control to align a dot with an arbitrarily established 0° point on the vector graticule.
- x. Rotate the CALIBRATED PHASE control from  $+14^{\circ}$  toward  $-14^{\circ}$  in increments of  $2^{\circ}$ .
- y. CHECK—Type R520 display 2° dot which corresponds to the dial reading being checked when that dot is aligned with the estiablished 0° point; the dial error at the  $+12^\circ$  and  $+10^\circ$  dial settings must be 2°, within  $\pm 0.5^\circ$  of the correct dial setting.
- z. Disconnect the 067-0546-00 calibration fixture, the three 75 ohm coaxial cables, three 75 ohm end-line terminations,  $1\times$  probe and the UHF male to BNC female adapter.

#### 20. Check Luminance Gain Accuracy

REQUIREMENT—1 volt of square-wave input signal must produce exactly 140 IRE units of deflection within  $\pm 1\%$ .

- a. Set the  $\phi$  REF switch to BURST, depress the Display Selector Y pushbutton, and set the SYNC switch to INT.
- b. Connect a 30 kHz square-wave signal 1 volt in amplitude from a square-wave generator via a 5 ns coaxial cable, GR to BNC male adapter, a 75 ohm to 50 ohm minimum loss at-

- tenuator and a BNC female to UHF male adapter to the Type R520 CH A J1 connector.
- c. Connect a 50 ohm coaxial cable from the test oscilloscope channel 1 vertical input connector to the output square-wave signal connector of a standard amplitude calibrator.
- d. Set the controls of the standard amplitude calibrator to produce a 1 volt amplitude square-wave signal.
- e. Connect a 75 ohm coaxial cable via a BNC male to UHF female adapter and a 75 ohm BNC termination from the test oscilloscope channel 2 vertical input connector to the Type R520 CH A J2 connector.
- f. Slowly change the frequency of the square-wave generator until a stable display is obtained.
- g. Set the test oscilloscope for a vertical deflection of 0.5 V/division, AC coupled with input channels non-inverted, matched in gain and algebraically added, at a sweep rate of 5 ms/division with internal triggering.
- h. Adjust the output amplitude of the square-wave generator until a test oscilloscope display indicates that the output square-wave generator signal is exactly 1 volt in amplitude, i.e., same as standard amplitude calibrator signal amplitude.
- i. CHECK—Type R520 display; should be 140 IRE units in amplitude,  $\pm 1\%$ .
- . j. Disconnect the square-wave generator, standard amplitude calibrator, test oscilloscope, 5 ns coaxial cable, GR to BNC male adapter, 75 ohm to 50 ohm minimum loss attenuator, BNC female to UHF male adapter, BNC male to UHF female adapter, 50 ohm BNC termination, 50 ohm coaxial cable, 75 ohm coaxial cable and  $1\times$  probe.

#### 21. Check Luminance Calibrator Signal

REQUIREMENT—Must be 1 volt,  $\pm 0.5\%$  in amplitude, which will produce 140 IRE units,  $\pm 0.5\%$  of vertical deflection on the Type R520.

- a. Press the Signal Selector A CAL pushbutton.
- b. CHECK—Type R520 display amplitude; must be 140 IRE units,  $\pm 0.5\%$ . The gain error noted in step 20 of this procedure should be taken into account.

# 22. Check Differential Gain Accuracy and Differential Phase Accuracy

REQUIREMENT—DIFF GAIN; display must not deviate more than  $\pm 5$  IRE units from level in the last 90% of display. This includes both slope and aberrations. When output signal of the 067-0565-00 calibration fixture is reduced 5%, the trace must move 25 IRE units,  $\pm 3\%$ . DIFF PHASE; deviation between the two traces at any point in the last 80% of display must not be less than 0.1°.

- a. Press the Signal Selector CH A and CH B pushbuttons and the Display Selector VECTOR pushbutton. Set the SYNC switch to EXT.
- b. Connect a 067-0565-00 calibration fixture to the CH A J1 connector. Connect a 75 ohm end-line termination to the CH A J2 connector.

- c. Connect a 75 ohm coaxial cable between the 067-0565-00 calibration fixture subcarrier input connector and the 067-0546-00 calibration fixture 3.579545 MHz subcarrier 2 V p-p connector.
- d. Connect a  $10\times$  probe from the test oscilloscope vertical input connector to monitor the input signal going to the CH A J1 connector.
- e. Set the test oscilloscope for a vertical deflection of 0.01 V/division, AC coupled, at a sweep rate of 0.5 ms/division with a free-running sweep.
- f. Adjust the 067-0565-00 calibration fixture subcarrier amplitude control so a signal amplitude of exactly 143 mV is displayed on the test oscilloscope.
  - g. Disconnect the test oscilloscope and the 10 imes probe.
- h. Connect a 75 ohm coaxial cable between the 067-0570-00 calibration fixture h sync 1 V neg connector and the Type R520 EXT SYNC J120 connector.
- i. Connect a 75 ohm coaxial cable from the Type R520 EXT SYNC J121 connector to the vertical input of the test oscilloscope via a UHF female to BNC male adapter and a 75 ohm BNC termination.
- j. Set the test oscilloscope for a vertical deflection of 1 V/division, AC coupled, at a sweep rate of 5  $\mu$ s/division with internal triggering.
- k. Adjust the test oscilloscope triggering controls to obtain a stable display.
- l. Connect the center conductor of the 067-0565-00 calibration fixture ramp input connector to the test oscilloscope sawtooth output connector and set the 95%-100% switch to 100%.
- m. Connect the shield of the 067-0565-00 calibration fixture ramp input connector to a ground point.
- n. Adjust the 067-0565-00 calibration fixture ramp amplitude control for a sawtooth amplitude of exactly 140 IRE units.
- o. Set the channel A 100%-75%-MAX GAIN switch to MAX GAIN and depress the Display Selector DIFF GAIN pushbutton.
- p. Adjust the VERT POSITION control to position the display to a convenient point.
- q. CHECK—Type R520 display; horizontal display must not deviate more than  $\pm 5$  IRE units from being parallel throughout the last 90% of its length with the horizontal lines of the IRE graticule. This includes both slope and aberrations.
- r. Set the 067-0565-00 calibration fixture 95%-100% switch to 95%.
- s. CHECK—Type R520 display; trace must move 25 IRE units,  $\pm 3\%$  from the position established in part q of this step.
- t. Return the 067-0565-00 calibration fixture 95%-100% switch to 100%.
  - u. Press the Display Selector DIFF PHASE pushbutton.

- v. Bring the display into the viewing area by adjusting the channel A PHASE controls until the two traces come together at a point.
- w. Using the CALIBRATED PHASE dial, bring the traces together at different points, noting the degrees of difference between the various points.
- x. CHECK—Type R520 CALIBRATED PHASE dial readings; deviation between the two traces in the last 80% of the display at any point on the lines must be less than 0.1°.
- y. Disconnect the 067-0546-00 and 067-0565-00 calibration fixtures, test oscilloscope, three 75 ohm coaxial cables and 75 ohm end-line termination, the UHF female to BNC male adapter and the 75 ohm BNC termination.

#### 23. Check Test Circle Amplitude

REQUIREMENT—Must be the same in diameter as the inscribed circle on the vector graticule (4 inches),  $\pm 1\%$ .

- a. Press the Signal Selector A CAL pushbutton and the Display Selector VECTOR pushbutton. Set the channel A 100%-75%-MAX GAIN switch to 75% and the SYNC switch to INT.
- b. CHECK—Type R520 display; test circle must overlay within  $\pm 1\,\%$  of the inscribed circle of the vector graticule at all points.

## 24. Check 100%-75% MAX GAIN Switch Gain

REQUIREMENT—100%; display must be 75%,  $\pm 2\%$  of the display size seen in the 75% switch position. MAX GAIN; display must be 3.5 times,  $\pm 5\%$  (in chrominance functions only) of the display size seen in the 75% switch position.

- a. Press the Display Selector Y pushbutton.
- b. CHECK—Type R520 display amplitude; exactly 140 IRE units, if it is not, readjust the Type R520 gain.
- c. Set the channel A 100%-75%-MAX GAIN switch to 100%.
- d. CHECK—Type R520 display amplitude; 105 IRE units ±2.8 IRE units.
- e. Cancel the Signal Selector A CAL pushbutton. Set the channel A 100%-75%-MAX GAIN switch to 75%.
  - f. Press the Signal Selector B CAL pushbutton.
- g. CHECK—Type R520 display amplitude; exactly 140 IRE units. If it is not, readjust the Type R520 gain.
- h. Set the channel B 100%-75%-MAX GAIN switch to 100%.
- i. CHECK—Type R520 display amplitude; 105 IRE units, ±2.8 IRE units.
- j. Press the Signal Selector CH A and CH B pushbuttons and the Display Selector VECTOR pushbutton. Set the channel B 100%-75%-MAX GAIN switch to 75%.

#### NOTE

The following parts of this step apply only to instruments SN B150100 and up.

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- k. Connect a 067-0565-00 calibration fixture to the CH A J1 connector. Connect a 75 ohm end-line termination to the CH A J2 connector.
- l. Connect a 75 ohm coaxial cable between the 067-0565-00 calibration fixture subcarrier input connector and the 067-0546-00 calibration fixture 3.579545 MHz subcarrier 2V P-P connector.
- m. Connect a 75 ohm coaxial cable between the 067-0546-00 calibration fixture h sync 1 V neg connector and the Type R520 EXT SYNC J120 connector.
- n. Connect a 75 ohm end-line termination to the EXT SYNC J121 connector.
  - o. Set the Type R520 SYNC switch to EXT.
- p. Connect a 10X probe from the test oscilloscope vertical input connector to monitor the input signal going to the CH A J1 connector.
- q. Set the test oscilloscope for a vertical deflection of 0.01 V/division, AC coupled, at a sweep rate of 0.5 ms/division with a free-running sweep.
- r. Adjust the 067-0565-00 calibration fixture subcarrier amplitude control so a signal amplitude of exactly 143 mV is displayed on the test oscilloscope.
  - s. Disconnect the test oscilloscope and the 10X probe.
- t. Adjust the channel A PHASE control so the vector is aligned along the 0° reference line on the vector graticule.
- u. Set the channel A 100%-75%-MAX GAIN switch to MAX GAIN.
- v. CHECK—Type R520 display; vector must remain aligned with the 0° reference line and the end of the vector should be touching the inscribed circle on the vector graticule.
- w. Disconnect the 067-0565-00 calibration fixture from the CH A J1 connector and connect it to the CH B J50 connector. Disconnect the 75 ohm end-line termination from the CH A J2 connector and connect it to the CH B J51 connector. The input signal from the 057-0546-00 calibration fixture remains connected to the 067-0565-00 calibration fixture.
  - x. Depress the Signal Selector  $B\phi$  pushbutton.
- y. Adjust the channel B PHASE control so the vector is aligned along the 0° reference line on the vector graticule.
- z. Set the channel B 100%-75%-MAX GAIN switch to MAX GAIN.
- aa. CHECK—Type R520 display; vector must remain aligned with the 0° reference line and the end of the vector should be touching the inscribed circle on the vector graticule.
- ab. Disconnect the 067-0546-00 and 067-0565-00 calibration fixtures, two 75 ohm end-line terminations and two 75 ohm coaxial cables.

#### 25. Check Subcarrier Regenerator Pull In Range, Time and Phase Shift versus Frequency

REQUIREMENT—Range; stable display must be obtained with a frequency of 3.579545 MHz  $\pm$ 15 Hz. Time; stable display must be obtained in 15 seconds. Phase shift versus fre-

- quency change; 0.6° or less phase shift for a 15 Hz frequency change from 3.579545 MHz.
- a. Depress the Signal Selector CH A and  ${\rm A}\phi/{\rm B}\phi$  ALT pushbuttons and set the SYNC switch to EXT.
- b. Set the channel B 100%-75%-MAX GAIN switch to 75%.
- c. Connect a 75 ohm coaxial cable from a 067-0546-00 calibration fixture h-sync output connector to the Type R520 EXT SYNC J121 connector.
- d. Connect a 75 ohm coaxial cable from the 067-0546-00 calibration fixture variable offset subcarrier 286 mV p-p connector to the Type R520 CH A J1 connector.
- e. Connect a 75 ohm end-line termination to the Type R520 EXT SYNC J120 connector, to the CH B J51 connector and to the CH A J2 connector.
- f. Rotate the 067-0546-00 frequency control for a zero hertz reading on the 067-0546-00 meter. This indicates that the output frequency at the variable offset subcarrier  $286 \, \text{mV}$  p-p connector is  $3.579545 \, \text{MHz}$ .
- g. CHECK—Type R520 display; vector should be stable (not rotating).
- h. Increase the  $3.579545\,\mathrm{MHz}$  output frequency of the 067-0546-00 by  $15\,\mathrm{Hz}.$
- i. Press the Signal Selector A CAL pushbutton for about fifteen seconds, then press the Signal Selector CH A pushbutton.
- j. CHECK—Time Type R520 takes to stabilize to a stable vector display; fifteen seconds or less.
- k. Decrease the output frequency of the 067-0546-00 back to 3.579545 MHz; then decrease it an additional 15 Hz.
- I. Press the Signal Selector A CAL pushbutton for about fifteen seconds, then press the Signal Selector CH A pushbutton.
- m. CHECK—Time Type R520 takes to stablize to a stable vector display; fifteen seconds or less.
- n. Increase the output frequency of the 067-0546-00 back to 3.579545 MHz.
- o. Align the vector along the  $0^{\circ}$  axis of the vector graticule, using the channel A PHASE control.
- p. Increase the  $3.579545\,\mathrm{MHz}$  output frequency of the 067-0546-00 by  $15\,\mathrm{Hz}.$
- q. Turn off the 3.579545 MHz oscillator of the 067-0546-00 calibration fixture by pressing the pushbutton when making the following checks.
- r. CHECK—Type R520 vector position; within 0.6° of the 0° axis of the vector graticule. CALIBRATED PHASE control can be used to measure the amount of vector shift.
- s. Decrease the output frequency of the 067-0546-00 back to  $3.579545\,\mathrm{MHz}$ , then decrease it an additional  $15\,\mathrm{Hz}$ .

- t. CHECK—Type R520 vector position; within 0.6° of the 0° axis of the vector graticule. CALIBRATED PHASE control can be used to measure the amount of vector shift.
- u. Disconnect the 067-0546-00 calibration fixture, the two 75 ohm coaxial cables and the three 75 ohm end-line terminations.

#### 26. Check Vertical Positioning Range

REQUIREMENT—Trace must position 45 IRE units above and 10 IRE units below the —40 IRE units graticule line in the Y, R, G and B modes of operation.

- a. Cancel all Signal Selector pushbuttons except the full FIELD pushbutton. Press the Display Selector Y pushbutton and set the CALIBRATED PHASE dial to 0 and the SYNC switch to INT.
  - b. Turn the VERT POSITION control fully clockwise.
- c. CHECK—Type R520 trace position; must be at least 45 IRE units above the -40 IRE units graticule line on the IRE graticule.
  - d. Turn the VERT POSITION control fully counterclockwise.
- e. CHECK—Type R520 trace position; must be at least 10 IRE units below the —40 IRE units graticule line on the IRE graticule.
- f. Press the Display Selector R pushbutton.
  - g. Repeat parts b through e of this step.
  - h. Press the Display Selector G pushbutton.
  - i. Repeat parts b through e of this step.
  - j. Press the Display Selector B pushbutton.
  - k. Repeat parts b through e of this step.

#### 27. Check Horizontal Positioning Range

REQUIREMENT—Either end of the trace must position to within 0.3 centimeter of the center of the vector graticule. (On some instruments, the end of the trace may actually position past the center.)

- a. Press the Display Selector Y pushbutton.
- b. Turn the HORIZ POSITION control fully clockwise.
- c. CHECK—Type R520 trace position; not more than 0.3 centimeter of trace must be to the left of the center of the IRE graticule.
- d. Turn the HORIZ POSITION control fully counterclockwise.
- e. CHECK—Type R520 trace position; not more than 0.3 centimeter of trace must be to the right of the center of the IRE graticule.

# 28. Check Vertical and Horizontal Position Clamp Range

REQUIREMENT—Either position clamp must have sufficient range to position the spot 2.5 IRE units either side of the

vector graticule center and have a total positioning range of 20 IRE units.

- a. Press the Display Selector VECTOR pushbutton.
- b. Adjust the VERT- and HORIZ-POSITION CLAMP controls (see Fig. 5-2) to position the spot to the center of the vector graticule.
- c. Rotate the VERT POSITION CLAMP control (see Fig. 5-2) fully clockwise.
- d. CHECK—Type R520 spot position; must have moved up at least 2.5 IRE units from its initial position established in part b of this step. Use the IRE graticule to estimate the distance the spot moved.
- e. Rotate the VERT POSITION CLAMP control (see Fig. 5-2) fully counterclockwise.
- f. CHECK—Type R520 spot position; must have moved down at least 2.5 IRE units from the initial position established in part b of this step. Use the IRE graticule to estimate the distance the spot moved.
- g. CHECK—Total Type R520 spot positioning, must have a total positioning range as noted in parts d and f of this step of 20 IRE units.
- h. Rotate the HORIZ POSITION CLAMP control (see Fig. 5-2) fully clockwise.
- i. CHECK—Type R520 spot position; must have moved right at least 2.5 IRE units from the initial position established in part b of this step.
- j. Rotate the HORIZ POSITION CLAMP control (see Fig. 5-2) fully counterclockwise.
- k. CHECK—Type R520 spot position; must have moved left at least 2.5 IRE units from the initial position established in part b of this step.
- I. CHECK—Total Type R520 spot positioning; must have a total positioning range, as noted in parts i and k of this step, of 20 IRE units.
- m. Readjust the VERT and HORIZONTAL POSITION CLAMP controls (see Fig. 5-2) to position the spot to the center of the vector graticule.

#### 29. Check Channel A and B Gain Control Range

REQUIREMENT—Must cause the display amplitude to vary from 2 times its normal size to 0.7 times its normal size.

- a. Press the Signal Selector CH A and A $\phi$  pushbuttons and the Display Selector Y pushbutton.
- b. Connect a 30 kHz square-wave signal about 300 mV in amplitude from a square-wave generator via a 5 ns co-axial cable, GR to BNC male adapter, a 75 ohm to 50 ohm minimum loss attenuator and a BNC female to UHF male adapter to the Type R520 CH A J1 connector.
- c. Connect a 75 ohm end-line termination to the CH A J2 connector.
- d. Slowly change the frequency of the square-wave generator until a stable display is obtained.

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- e. Adjust the output amplitude control of the square-wave generator until a Type R520 display exactly 40 IRE units high is obtained.
- f. Rotate the channel A GAIN control just out of its  $\operatorname{CAL}$  detent position.
- g. CHECK—Type R520 display amplitude; at least 80 IRE units of deflection.
- h. Rotate the channel A GAIN control to the extreme of rotation from CAL position.
- i. CHECK—Type R520 display amplitude; 28 IRE units or less.
- j. Disconnect the square-wave generator, 5 ns coaxial cable, GR to BNC male adapter, 75 ohm to 50 ohm minimum loss attenuator, BNC female to UHF male adapter and 75 ohm end-line termination.
- k. Cancel the Signal Selector CH A pushbutton and set the channel A GAIN control to CAL position.
  - 1. Press the Signal Selector CH B and B $\phi$  pushbuttons.
- m. Connect a 15 kHz square-wave signal about 300 mV in amplitude from a square-wave generator via a 5 ns co-axial cable, GR to BNC male adapter, a 75 ohm to 50 ohm minimum loss attenuator and a BNC female to UHF male adapter to the Type R520 CH B J50 connector.
- n. Connect a  $75\,$  ohm end-line termination to the CH A J51 connector.
- o. Slowly change the frequency of the square-wave generator until a stable display is obtained.
- p. Adjust the output amplitude control of the square-wave generator until a Type R520 display exactly 40 IRE units high is obtained.
- q. Rotate the channel B GAIN control just out of CAL detent position.
- r. CHECK—Type R520 display amplitude; at least 80 IRE units of deflection.
- s. Rotate the channel A GAIN control to the extreme of rotation from CAL position.
- t. CHECK—Type R520 display amplitude; 28 IRE units or less.
- u. Disconnect the square-wave generator, 5 ns coaxial cable, GR to BNC male adapter, 75 ohm to 50 ohm minimum loss attenuator, BNC female to UHF male adapter and 75 ohm end-line termination.

#### 30. Check Luminance Gain Range

REQUIREMENT—Must cause the display amplitude to vary from 1.4 times its normal size to 0.7 times its normal size.

- a. Cancel the Signal Selector CH B pushbutton and set the channel B GAIN control to CAL position.
  - b. Press the Signal Selector CH A and  $A\phi$  pushbuttons.
- c. Connect a 30 kHz square-wave signal about 300 mV in amplitude from a square-wave generator via a 5 ns co-axial cable, GR to BNC male adapter, a 75 ohm to 50 ohm

- minimum loss attenuator and a BNC female to UHF male adapter to the Type R520 CH A J1 connector.
- id. Connect a 75 ohm end-line termination to the CH A J2 connector.
- e. Slowly change the frequency of the square-wave generator until a stable display is obtained.
- f. Adjust the output amplitude control of the square-wave generator until a Type R520 display exactly 40 IRE units high is obtained.
- g. Rotate the LUMINANCE GAIN control just out of CAL detent position.
- h. CHECK—Type R520 display amplitude; at least 56 IRE units of deflection.
- i. Rotate the LUMINANCE GAIN control to the extreme of rotation from CAL position.
- j. CHECK—Type R520 display amplitude; 28 IRE units or less.
- k. Return the LUMINANCE GAIN control to CAL position.
- I. Disconnect the square-wave generator, 5 ns coaxial cable, GR to BNC male adapter, 75 ohm to 50 ohm minimum loss attenuator, BNC female to UHF male adapter and 75 ohm end-line termination.

#### 31. Check External Phase Reference Input Range

REQUIREMENT—Test circle size and shape must not change as the 3.58 MHz  $\phi$  reference signal amplitude is varied between 1.5 volt and 2.5 volts.

- a. Press the Signal Selector B CAL pushbutton and the Display Selector VECTOR pushbutton. Set the  $\phi$  REF switch to FYT
- b. Connect a 2 volt peak to peak 3.58 MHz continuous wave (CW) video signal via a 75 ohm coaxial cable to the Type R520 EXT CW  $\phi$  REF J310 connector.
- c. Connect a color bar video signal via a 75 ohm coaxial cable to the Type R520 CH A J1 connector.
- d. Connect a 75 ohm end-line termination to the EXT CW  $\phi$  REF J311 connector and to the CH A J2 connector.
- e. Connect a 10X probe from the test oscilloscope vertical input connector to the input signal going to the EXT CW  $\phi$  REF J310 connector.
- f. Set the test oscilloscope for a vertical deflection of 0.05 V/division, AC coupled, at a sweep rate of 0.2  $\mu$ s/division with internal triggering.
- g. Adjust the peak-to-peak output amplitude of the 3.58 MHz CW video signal until a test oscilloscope display exactly 4 major divisions high is obtained.
- h. Rotate the channel A PHASE control to align the burst with the burst axis of the vector graticule.
- i. Vary the 3.58 MHz CW video signal amplitude between 1.5 volt and the 2.5 volt peak to peak, using the test oscilloscope to measure the signal amplitude.
- j. CHECK—Type R520 test circle display; test circle must not change in size or shape as part i of this step is accomplished.

k. Disconnect the video signal source, test oscilloscope, the two 75 ohm coaxial cables, the two 75 ohm end-line terminations and the 10X probe.

#### 32. Check External Horizontal Sync Range

REQUIREMENT—Stable display must be obtained with an external sync input signal whose amplitude is between 3.5 volts and 7.5 volts.

- a. Cancel the Signal Selector CH A pushbutton and press the CH B and  $B\phi$  pushbuttons.
- b. Set the  $\phi$  REF switch to BURST and press the Display Selector LINE SWEEP pushbutton.
  - c. Set the SYNC switch to EXT.
- d. Connect the linearity staircase video signal via a 75 ohm coaxial cable to the Type R520 CH B J50 connector.
- e. Connect a 4 volt peak-to-peak sync video signal via a 75 ohm coaxial cable to the EXT SYNC J120 connector.
- f. Connect a 75 ohm end-line termination to the EXT SYNC J121 connector and to the CH B J51 connector.
- g. Connect a 10X probe from the test oscilloscope vertical input connector to the input signal going to the EXT SYNC J120 connector.
- h. Set the test oscilloscope for a vertical deflection of 0.2 V/division, AC coupled, at a sweep rate of 20  $\mu$ s/division with internal triggering.
- i. Adjust the peak-to-peak output amplitude of the sync video signal until a test oscilloscope display exactly 2 major divisions high is obtained.
- j. Adjust the BURST FLAG TIMING control for the proper Type R520 display; refer to step 9 of this procedure.
- k. Vary the sync video signal amplitude between 3.5 volts and 7.5 volts peak to peak, using the test oscilloscope to measure the signal amplitude. Interrupt the sync video signal by momentarily setting the SYNC switch to INT before making the check at a particular sync video signal amplitude.
- I. CHECK—Type R520 display; a stable display must be obtained whenever the SYNC switch is set to its EXT position as part k of this step is accomplished.
- m. Disconnect the video signal source, test oscilloscope, the two 75 ohm coaxial cables, the two 75 ohm end-line terminations and the 10X probe.

#### 33. Check Instrument Return Loss

- a. Connect the 067-0576-00 calibration fixture to the vertical input connectors of the test oscilloscope.
- b. Connect a 0.5 V, 5 MHz sine-wave signal from a wide bandwidth constant amplitude sine wave generator via a 50 ohm coaxial cable and a 75 ohm to 50 ohm minimum loss attenuator to the signal input connector on the 067-0576-00 calibration fixture.
- c. Connect the matched 75 ohm terminations to the end of each coaxial cable of the 067-0576-00 calibration fixture.

- d. Set the test oscilloscope for a vertical deflection of 0.2 V/division both input channels set for A-B operation with a free running sweep.
- e. Remove one matched 75 ohm termination and adjust the constant amplitude sine wave generator for a 0.5 V, 5 MHz output sine wave signal as observed on the test oscilloscope, then replace the matched 75 ohm termination.
- f. Set the test oscilloscope for a vertical deflection of 1 mV/division, both input channels AC coupled, and set for A-B operation at a sweep rate of 20  $\mu s$ /division with a freerunning sweep.
- g. Vary the constant amplitude sine wave generator frequency from 25 Hz to 5 MHz.
- h. CHECK—Test oscilloscope display amplitude; should be 1 mV or less at any frequency between 25 Hz and 5 MHz.
- i. Disconnect a 75 ohm termination from the end of the measuring cable then, attach the measuring cable via the BNC female to UHF male adapter to the R520 CH A J1 connector and the 75 ohm termination just removed to the CH A J2 connector via the BNC female to UHF male adapter. The BNC male to UHF female adapter remains connected to the 75 ohm termination.
- j. Vary the constant amplitude sine wave generator frequency from 25 Hz to 5 MHz.
- k. Push the Type R520 Signal Selector CH A and then the A CAL pushbuttons.
- I. CHECK—Test oscilloscope display amplitude; should never be more than 5 mV minus the signal amplitude noted in part h of this step, at any frequency from 25 Hz to 5 MHz.
- m. Disconnect the measuring cable and adapter from the Type R520 CH A J1 connector and connect it to the CH B J50 connector. Disconnect the 75 ohm termination and adapters from the CH A J2 connector and connect it to the CH B J51 connector.
- n. Vary the constant amplitude sine wave generator frequency from 25 Hz to  $5\,\text{MHz}.$
- o. Push the Type R520 Signal Selector CH B and then the B CAL pushbuttons.
- p. CHECK—Test oscilloscope display amplitude; should never be more than 5 mV minus the signal amplitude noted in part h of this step, at any frequency from 25 Hz to 5 MHz.
- q. Disconnect the measuring cable and adapter from the Type R520 CH B J50 connector and connect it to the EXT CW  $\phi$  REF J310 connector. Disconnect the 75 ohm termination and adapters from the CH B J51 connector and connect it to the EXT CW  $\phi$  REF J311 connector.
- r. Vary the constant amplitude sine wave generator frequency from 25 Hz to 5 MHz.
- s. Switch the Type R520  $\phi$  REF switch between its BURST and EXT positions.
- t. CHECK—Test oscilloscope display amplitude; should never be more than 5 mV minus the signal amplitude noted in part h of this step, at any frequency from 25 Hz to 5 MHz.
- u. Disconnect the measuring cable and adapter from the Type R520 EXT CW  $\phi$  REF J310 connector and connect it to the EXT SYNC J120 connector. Disconnect the 75 ohm termi-

#### Performance Check—Type 520/R520 NTSC

nation and adapters from the EXT CW  $\phi$  REF J311 connector and connect it to the EXT SYNC J121 connector.

- v. Vary the constant amplitude sine wave generator frequency from 25 Hz to 5 MHz.
- w. Switch the Type R520 SYNC switch between its INT and  $\ensuremath{\mathsf{EXT}}$  positions.
- x. CHECK—Test oscilloscope display amplitude; should never be more than 2.5 mV (4 volt connection), or 5 mV (1 volt connection) minus the signal amplitude noted in part h of this step, at any frequency from 25 Hz to 5 MHz.
- y. Disconnect the 067-0576-00 calibration fixture (this includes the 75 ohm termination and the two BNC female to UHF male adapters and the BNC male to UHF female adapter still attached to the Type R520), wide bandwidth constant amplitude sine wave generator, test oscilloscope, 50 ohm coaxial cable and 75 ohm to 50 ohm minimum loss attenuator.

#### 34. (Optional Step) Check Phase Jitter

REQUIREMENT—Must be less than 1° of display jitter when 51 mV RMS of white noise is inserted onto an incoming video signal.

- a. Depress the Signal Selector CH A, CH B and  $A\phi/B\phi$  ALT pushbuttons and Display Selector DIFF PHASE pushbutton. Set the channel B 100%-75%-MAX GAIN switch to MAX GAIN,  $\phi$  REF to BURST and the SYNC switch to INT.
- b. Connect a color bar video signal vià a 75 ohm coaxial cable to the Type R520 CH A J1 connector.
- c. Connect a linearity staircase video signal via a 75 ohm coaxial cable to the Type R520 CH B J50 connector.
- d. Connect a 75 ohm end-line termination to the CH A J2 connector and to the CH B J51 connector.
- e. Adjust the channel B PHASE control to position the resultant linearity staircase waveform onto the display area.
- f. Insert onto the color bar video signal 51 mV RMS (73 mV peak to peak) of white noise.
- g. CHECK—Type R520 display jitter on the resultant linearity staircase waveform; must be less than 1°. Use the CALIBRATED PHASE control to measure the amount of display jitter.

This completes the performance check of the Type R520. Disconnect all test equipment and replace the bottom cover.

# SECTION 6 CALIBRATION

Change information, if any, affecting this section will be found at the rear of the manual.

#### Introduction

Complete calibration information for the Type 520 is given in this section. This procedure calibrates the instrument to the performance requirements listed in the Specification section. The Type 520 can be returned to original performance standards by completion of each step in this procedure. Limits, tolerances, and waveforms are given as calibration guides and are not instrument specifications. To merely touch up the calibration, perform only those steps entitled "Adjust. . .". A short-form calibration procedure is also provided for the convenience of the experienced calibrator.

The Type 520 should be checked, and recalibrated if necessary, after each 1000 hours of operation, or every six months if used infrequently to assure correct operation and accuracy. The Performance Check section provides a complete check of instrument performance without making internal adjustments. Use the performance check procedure to verify the calibration of the Type 520 and determine whether recalibration is required.

#### TEST EQUIPMENT REQUIRED

#### General

The following test equipment, or its equivalent, is required for complete calibration of the Type 520. Specifications given are the minimum necessary for accurate calibration of this instrument. All test equipment is assumed to be correctly calibrated and operating within the given specifications. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

The Type 520/R520 NTSC Vectorscopes (SN B180000-up) are equipped with BNC type connectors for all signal inputs.

For the quickest and most accurate calibration, special calibration fixtures are used where necessary. All calibration fixtures listed here can be obtained from Tektronix, Inc. Order by part number through your local Tektronix Field Office or representative.

1. Precision DC voltmeter. Accuracy, within  $\pm 0.025\%$ ; range 0 to 20 volts. For example, Fluke Model 825A.

- 2. DC Voltmeter (VOM). Minimum sensitivity, 20,000 ohms/volt. Accuracy within  $\pm 5\%$  at 3.6 V;  $\pm 3.5\%$  at 10 V and 100 V,  $\pm 7\%$  at 275 V, and within  $\pm 3\%$  at 3875 V. For example Triplett Model 630 NA.
- 3. Test oscilloscope: Bandwidth, DC to at least 10 MHz; minimum deflection factor, 0.005 volt/division; DC offset voltage, 0 to 7 volts; two input channels providing choice of independent channel operation, alternate-trace or algebraically added two channel operation, and one channel designed for display inversion. Tektronix Type 547 Oscilloscope with Type 1A1 and Type 1A5<sup>1</sup> Plug-In Units, and two each Tektronix P6023 (10X) and P6028 (1X) Probes recommended; or Tektronix 7403N Oscilloscope with 7A13, 7A18 and 7B53N Plug-In Units, and two P6055 (10X) and one P6011 (1X) probes recommended.
- 4. Variable autotransformer: Must be capable of supplying at least 200 volt/amperes over a voltage range of 90 to 136 volts (180 to 272 volts for 230-volt nominal line). If autotransformer does not have an AC voltmeter to indicate output voltage, monitor output with an AC voltmeter (RMS) with a range of at least 136 (or 272) volts. For example, General Radio W10MT3W Metered Variac Autotransformer.
  - 5. Video Signal Source with the following outputs:

Comp Video: Color Bar and

nd  $\left.
ight.
ight.\}$  1 V P-P into 75  $\Omega$ 

Staircase Comp Sync:

4 V into 75  $\Omega$ 

Subcarrier:

2 V into 75  $\Omega$ 

Tektronix Type 140 NTSC Test Signal Generator is used in this procedure.

- 6. Medium frequency constant amplitude signal generator. Frequency, variable from 3 MHz to 18 MHz; output amplitude, adjustable to 1 volt; amplitude regulation accuracy, within  $\pm 5\%$ . Tektronix Type 191 Constant Amplitude Signal Generator recommended.
- 7. Wide bandwidth constant amplitude generator. Frequency, variable from below 25 Hz to above 5 MHz; output

<sup>1</sup> Required only if step 52 is performed.

amplitude, adjustable from about 1 volt to about 2 volts; amplitude regulation, 0.5%. For example, Hewlett-Packard Model 652A generator.

- 8. Standard amplitude calibrator (optional); Amplitude accuracy, within 0.25%; signal amplitude, 1 volt; output frequency, 1 kHz. Tektronix calibration fixture 067-0502-00 recommended. Used in step 18A which is an alternative procedure for step 18.
- 9. Subcarrier Frequency Offset test fixture (optional). Used in step 44 to change the Type 140 subcarrier frequency  $\pm 15$  Hz. Construct the test fixture according to the information given in Fig. 6-1A.
- 10. Ramp and sine wave adder: Tektronix calibration fixture 067-0565-00 recommended.
- 11. Return loss bridge. Tektronix calibration fixture 015-0149-00 recommended.
- 12. Cable (four) (SN B180000-up): Impedance, 75 ohms; length, 42 inches, connectors, BNC. Tektronix Part No. 012-0074-00.
- 12A. Cable (four) (SN B010100-B170979): Impedance, 75 ohms, length, 42 inches, connectors, UHF; Tektronix Part No. 012-0083-00.
- 13. Cable. Impedance, 50 ohms; length, 42 inches; connectors, BNC. Tektronix Part No. 012-0057-01.
- 14. Connector, dual-input cable: Connectors, BNC. Tektronix Part No. 067-0525-00.
- 15. Attenuator. Connectors, BNC; impedance, 50 ohms to 75 ohms; type, minimum loss when going from a 50 ohm system to a 75 ohm system. Tektronix Part No. 011-0057-00.
- 16. Variable attenuator: For use in steps 50 and 51 to vary the Type 140 output signal. Construct according to the information given in Fig. 6-1B.
- 17. Termination (three) (SN B180000-up): Impedance, 75 ohms; connector, BNC; type, end-line; 0.5 W. Tektronix Part No. 011-0102-00.
- 17A. Termination (three) (SN B010100-B170979): Impedance, 75 ohms; connector, UHF; type, end-line; 0.5 W. Tektronix Part No. 011-0104-00.

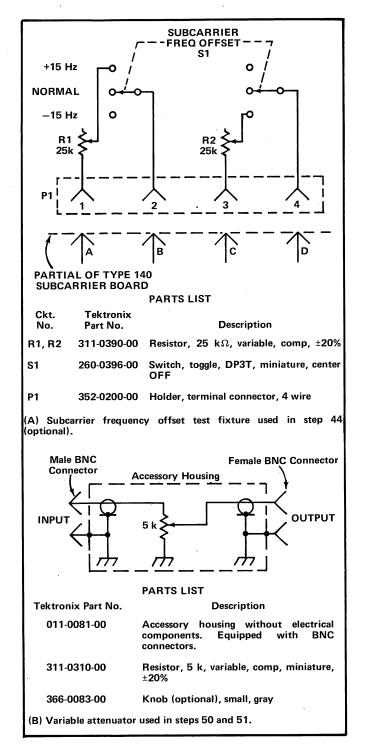


Fig. 6-1. Special test fixtures that must be constructed for use in the calibration procedure.

- 18. Termination: Impedance, 75 ohms; connectors, BNC; type, feed-thru; 1 W. Tektronix Part No. 011-0055-00.
- 19. Termination. Impedance, 50 ohms; connectors, GR to BNC male; type, feed-thru; 1 W. Tektronix Part No. 017-0083-00.

- 20. Adapter, clip lead: BNC female to alligator clip leads. Tektronix Part No. 013-0076-00.
- 21. Adapter.<sup>2</sup> Connectors, UHF male to BNC female. Tektronix Part No. 103-0015-00.
- 22. Adapter.<sup>2</sup> Connectors, UHF female to BNC male. Tektronix Part No. 103-0032-00.
- 23. Adapter: Connectors, GR to BNC male. Tektronix Part No. 017-0064-00.
  - 24. Adjustment tools.

	Description	Tektronix Part No.
a.	Tuning tool; 5 inches long, plastic for adjusting 0.1-inch (ID) hex cores.	003-0301-00
b.	Tuning tool Handle	003-0307-00
	Insert, low capacitance, with wire pin	003-0308-00
	Insert, for 5/64-inch (ID) hex cores	003-0310-00
C.	Insulated screwdriver, 1 1/2-inch shaft, non-metallic	003-0000-00
d.	Screwdriver, 3-inch shaft	033-0192-00
e.	Hexagonal wrench, 1/16-inch tip	033-0089-00
f.	Wrench, nutdriver, 1/2-inch shaft	033-0318-00
g.	Phillips screwdriver, small tip.	Not available through Tek- tronix, Inc.

#### CALIBRATION RECORD AND INDEX

This short-form calibration procedure may be used as a calibration guide by the experienced calibrator, or it may be used as a record of calibration. Since the step numbers and titles correspond to those used in the complete procedure, it also serves as an index to the complete procedure.

Type 520, Serial No	
Calibration Date	
Calibration Technician	

1. Adjust-15 Volt Power Supply, R1588

Page 6-8

- -15 volts, +0.5% (75 mV)
- 2. Check Low-Voltage Power Supply Voltages

Page 6-8

- $+3.6 \text{ volts.} \pm 5\% (\pm 0.18 \text{ V}); +10 \text{ volts.} +3.5\% (\pm 0.35 \text{ V}).$
- $+100 \text{ volts}, \pm 3.5\% (\pm 3.5 \text{ V}); +275 \text{ volts}, \pm 7\% (\pm 19.25 \text{ V}).$
- 3. Check Low-Voltage Power Supply Ripple

Page 6-9

Power Supply	Max Ripple
– 15 volt	10 mV
+3.6 volt	100 mV
+10 volt	10 mV
+100 volt	20 mV
+275 volt	500 mV

4. Check High-Voltage Power Supply

Page 6-9

 $-3.875~\text{kV}~\pm 3\%~(+116.25~\text{V}).$  Voltage reading must not change more than  $\pm 40~\text{V}$  as INTENSITY control is rotated from its fully clockwise position to its fully counterclockwise position.

5. Adjust Geometry, R1472

Page 6-9

Voltage at center arm of GEOM control should be about 20 V below voltage at upper CRT plate connection. Display of vertical and horizontal lines must have 0.05 centimeter or less of gradual bowing.

6. Adjust Astigmatism, R1476

Page 6-10

Obtain a round spot with FOCUS control set fully counterclockwise.

7. Adjust CRT alignment, R1470 and Page 6-10 R1474

R1470—A vertical trace should be parallel throughout its length with  $90^{\circ}-270^{\circ}$  axis.

R1474—A horizontal trace should be parallel throughout its length with the  $0^{\circ}\!-\!180^{\circ}$  axis.

8. Adjust Unblanking Bias, R1478

Page 6-11

Obtain uniform intensity throughout the circumference of a test circle which is barely visible.

 $<sup>^2</sup>$  Connected to item 10 when calibrating instruments SN B180000 and up. Three (total) are required, when calibrating instruments below SN B180000, to facilitate interconnection of test equipment with BNC connectors.

9. Adjust VITS Intensity, R1228

Page 6-11

With VITS 18 pushbutton pressed, should obtain maximum display brightness without display defocusing.

10. Adjust DC Balance of R-Y Amplifier, Page 6-12 R624

Voltage at pin AD (below SN B200000, TP630) must be 0.0 volt.

11. Adjust DC Balance of B-Y Amplifier, Page 6-13 R644

Voltage at TP650 must be 0.0 volt.

12. Adjust DC Balance of Y Amplifier, Page 6-13 R672

Voltage at TP680 must be +0.5 volt.

13. Adjust Horizontal Common Mode Level Page 6-13 R880, R1002, R985, and R875

R880—Vertically position spot to center of vector graticule.

R1002—Horizontally position spot to center of vector graticule.

R985—Obtain a +5.6 voltage between TP980 and ground.

R875—Obtain a +5.6 voltage between TP870 and ground.

14. Adjust Clamp Pulse Timing, R905

Page 6-14

The alternately displayed waveforms from TP805 and TP905 must meet or exceed the minimum waveform amplitude shown in Fig. 6-9.

15. Adjust Channel A and B

Page 6-14

Input Amplifier Frequency Response Gain, C2 and C52.

C2—Peaks of yellow and cyan color bars at TP85 must be equal to 100 IRE unit white bar.

C52—Peaks of yellow and cyan color bars at TP95 must be equal to 100 IRE unit white bar.

16. Adjust Test Circle Oscillator, L46 and Page 6-16 R45

Voltage at TP41 should be approximately -0.4 volt. The signal at TP49 should be approximately 707 mV in amplitude.

17. Adjust Test Circle Oscillator Compensation, C66 and C18

Channel A and B test circles should be the same diameter as that produced by the 707 mV 3.58 MHz signal applied from the generator to the Type 520.

18. Adjust Luminance Calibrator, R583

Page 6-17

Voltage reading at TP583 should be 1 volt more positive with Q571 removed than when Q570 is removed.

19. Adjust Channel A Gain, R402

Page 6-18

The signals at TP583 and TP450 must exactly match each other.

20. Adjust Channel B Gain, R412

Page 6-18

Channel B calibrator display amplitude should match the amplitude of Channel A display.

21. Adjust Subcarrier Regenerator Input Page 6-19 3.58 MHz Filter, L220 and L221

L220—Signal at TP220 should be at minimum amplitude, about 2.5 volts or less.

L221—Signal at TP222 should be at maximum amplitude, about 0.2 volt or greater.

22. Check Burst Intensification Pulse

Page 6-20

Should appear similar to the waveform shown in Fig. 6-15.

23. Adjust Burst Gate Pulse, R1158

Page 6-21

Should have a peak-to-peak amplitude of at least 7 volts or greater. Waveform should appear as shown in Fig. 6-16, Type 520 display should be stable and have no jitter. Burst sampling point should be positionable at least  $\pm 0.5~\mu s$ .

24. Adjust Subcarrier Regenerator DC Balance R250; (SN B150100-up) Centering, R243

See complete procedure.

25. Check Subcarrier Regenerator Circuit Page 6-22 3.58 MHz Output Signal

 $3.58\ \text{MHz}$  output signal must be at least 4 volts peak to peak .

26. Check Oven Preheater Operation

Page 6-23

Voltage between TP295 and ground should be the same as the voltage between pin Q, R or S of the Rectifier board and ground after the Type 520 has been on at least 20 minutes.

27. Adjust Subcarrier Filter, L545 and Page 6-24 L547

L545—3.58 MHz subcarrier signal at TP590 should be at maximum amplitude, approximately 1.2 volts peak to peak.

L547—Should be  $33^{\circ}$ ,  $\pm 2^{\circ}$  of clockwise display rotation when the VECTOR pushbutton is held depressed and the I or Q pushbutton is pressed enough to make momentary contact.

After making the above adjustments, recheck the voltage levels at pin AD (TP630) and TP650 as per steps 10 and 11 of this procedure.

28. Adjust 10.4 MHz and 18 MHz Traps, Page 6-24 C454 and C453

C454—Obtain minimum circle diameter or a spot when 1 volt of 10.4 MHz sinewave signal is connected to the input.

C453—Obtain minimum circle diameter or a spot when 1 volt of 18 MHz sinewave signal is connected to the input.

29. Adjust Subcarrier Balance, R501, C593 Page 6-25 and C503

See complete procedure.

30. Adjust Quadrature Phase Alignment, Page 6-25 C586

Test circles must overlay each other at the 45° point on their circumference within 0.0362 inch.

31. Adjust Vertical Gain, R484

Page 6-25

1 volt luminance calibrator signal should produce exactly 140 IRE units of deflection.

32. Adjust Chroma R-Y Gain, R626

Page 6-26

Test circle must be tangent to the inscribed circle on the vector graticule at the  $90^{\circ}$  and  $270^{\circ}$  points.

33. Adjust Horizontal Gain to match Vertical Gain, R968

Page 6-26

After connecting the vertical (R-Y) output to the horizontal amplifier input, obtain a trace whose length is the same as the diameter of the inscribed circle on the vector graticule.

34. Adjust Chroma B-Y Gain, R646

Page 6-26

With GAIN BAL control set to its midrange position, the test circle must be tangent to the inscribed circle on the vector graticule at the  $0^{\circ}$  and  $180^{\circ}$  points.

35. Adjust Transient Response, L610 Page 6-27 through L618, R849, C848, L858, L838, R968, R969, C968, C958, L958, L978, L601, L602, L606 and L607

See complete procedure.

36. Adjust L272, L279; Feedback Components (for instruments B150100 and up); Input Phasing (for instruments B030000 to B150100)

Differential Phase—Must have less than 0.1° deviation between the two traces at any point in the last 80% of the display.

See complete procedure.

37. Adjust Calibrated Phase Control, L331, Page 6-33 L332, and R335

See complete procedure.

38. Adjust Diff Gain Mode Compensation, Page 6-35 R498

With the baseline of the staircase waveform setting at the -40 IRE unit line and the top of the last step setting at the +100 IRE unit line of the luminance graticule when the Y pushbutton is pressed and the 100%-75%-MAX GAIN switch is set to 75%, the display when the DIFF GAIN pushbutton is pressed and the 100%-75%-MAX GAIN switch is set to MAX GAIN must be set at the 30 IRE unit line of the luminance graticule, see Figs. 6-26A and 6-26B.

39. Check Input Amplitude Range

Page 6-35

Stable display for sync pulse amplitudes between 200 mV and 400 mV, signal amplitudes between 0.7 volt and 1.4 volts.

40. Check Differential Gain Deflection Page 6-36 Factor and Differential Gain

Differential Gain—Trace must not have any aberrations or slope which will cause it to deviate more then  $\pm 5$  IRE units away from being parallel to the luminance graticule horizontal lines throughout the last 90% of its length. When output signal of the 067-0565-00 calibration fixture is reduced 5%, the trace must move 25 IRE units,  $\pm 5\%$ .

41. (For instruments SN B150100-up)— Page 6-38 Check 100%-75%-MAX GAIN Switch Gain

See complete procedure.

41A. (For instruments below S N Page 6-38 B150100)—Check 100%-75%-MAX GAIN Switch Gain

See complete procedure.

42. Check Color Bar Decoding Accuracy Page 6-39

Color bars should extend from 7.5% setup to 77 IRE units within  $\pm 3\%$  when blanking level is aligned with 0 IRE unit graticule line.

43. Check Time Sharing Switching Rate Page 6-39

Test oscilloscope display from TP776 should show two channel A displays then two Channel B displays, etc.

44. (Optional Step)—Check Subcarrier Page 6-40 Regenerator Pull In Range and Time

Type 520 should present a stable vector display of a 3.579545 MHz,  $\pm 15$  Hz, signal within 15 seconds after it is applied.

Vector position must not vary more than 0.6° as the 3.579545 MHz signal is varied 15 Hz above and below the center frequency.

45. Check Vertical Positioning Range

Page 6-40

Page 6-41

-10 IRE units and +45 IRE units from the -40 IRE units luminance graticule line in the Y, R, G and B modes of operation.

46. Check Horizontal Positioning Range

Clockwise-Not more than 3 mm of trace to left of

luminance graticule center.

Counterclockwise—Not more than 3 mm of trace to right of luminance graticule center.

47. Check Vertical and Horizontal Position Page 6-41 Clamp Range

Vertical—Must position spot at least 2.5 IRE units above and below the center of the vector graticule.

Horizontal—Must position spot at least 2.5 IRE units to the left and right of the center of the vector graticule.

48. Channel A and B Gain Control Range

Page 6-42

Signal from TP450 must be at least double when the appropriate GAIN control is just moved out of its CAL detent position.

Signal from TP450 must drop to at least 0.7 times its CAL position signal when the appropriate GAIN control is rotated fully to the far end away from CAL position.

49. Check Luminance Gain Range

Page 6-42

Signal from TP776 must increase to at least 1.4 times its CAL position signal when the LUMINANCE GAIN control is just moved out of its CAL detent position. Signal from TP776 must decrease to at least 0.7 times its CAL position signal when the LUMINANCE GAIN control is rotated fully to the far end away from CAL position.

50. Check External Phase Reference Input Page 6-43 Range

Test circle must not change in size or shape, as an external 3.58 MHz video signal is varied in amplitude from 1.5 volts to 2.5 volts peak to peak.

51. Check External Horizontal Sync Range Page 6-43

Stable display must be obtained using an external sync video signal whose amplitude is varied between 3.5 volts and 7.5 volts peak to peak. The sync video signal is interrupted momentarily before making the check at a particular sync video signal amplitude.

52. Check Instrument Return Loss

Page 6-44

See complete procedure.

53. (Optional Step) Check Phase Jitter

Page 6-46

Less than 1° of jitter on the modulated staircase resultant waveform when 51 mV RMS of white noise has been inserted onto the modulated staircase signal. Use the CALIBRATED PHASE control to measure the amount of display jitter.

#### **CALIBRATION PROCEDURE**

#### General

The following procedure is arranged in a sequence which allows the Type 520 to be calibrated with the least interaction of adjustments and reconnection of equipment. However, some adjustments affect the calibration of other circuits within the instrument, therefore, it will be necessary to check the operation of other parts of the instrument. When a step interacts with others, the steps which need to be checked are noted in the "INTERACTION—..." step.

The following procedure uses the equipment listed under Equipment Required. If equipment is substituted, control settings or test equipment setup may need to be altered to meet the requirements of the equipment used.

#### NOTE

All waveforms shown in this procedure are actual waveform photographs taken with a Tektronix Oscilloscope Camera System.

Any maintenance should be performed before proceeding with calibration. Troubles which become apparent during calibration should be corrected using the techniques given in the Maintenance section.

The steps titled "Adjust . . ." also provide a check of instrument performance, whenever possible, before the adjustment is made. The symbol ① is used to identify the steps in which an adjustment is made. To prevent recalibration of other circuits when performing a partial calibration, readjust only if the listed tolerance is not met. However, when performing a complete calibration, best overall performance will be provided if each adjustment is made to the

exact setting, even if the "CHECK— . . ." is within the allowable tolerance.

In the following procedure, a list of front-panel control settings for the Type 520 is given preceding each major group of adjustments and checks. Controls whose settings are not important to the group of adjustments are not listed. To aid in locating individual controls which have been changed during complete calibration, these control names are printed in bold type. Pushbuttons which are not called out are assumed to be cancelled. If only a partial calibration is performed, start with the nearest complete list of control settings preceding the desired portion. Type 520 front- and rear-panel and internal adjustment control titles referred to in this procedure are capitalized (e.g., INTENSITY, or LUM DC BAL).

#### **Preliminary Procedure**

- 1. Remove the top and bottom covers from the Type 520 and set the instrument on its right side.
- 2. Connect the autotransformer to a suitable power source and connect the Type 520 to the autotransformer output.
- 3. Set the autotransformer output voltage to the design center voltage for which the Type 520 line voltage selector assembly has been set.
- 4. Set the front and rear-panel controls of the Type 520 as described below.
- 5. Set the Type 520 POWER switch to ON. Allow at least 20 minutes warmup at  $25^{\circ}$ C,  $\pm 5^{\circ}$ C before making any checks or adjustments.

NOTES			
·	•		
			•

#### Front-Panel Controls:

Signal Selector CHANNEL A	FULL FIELD
100%-75%-MAX GAIN	75%
GAIN	CAL
$\phi$ REF	BURST
CHANNEL B	
100%-75%-MAX GAIN	75%
GAIN	CAL
Display Selector	No buttons pressed
INTENSITY	As desired
LUMINANCE GAIN	CAL
SCALE ILLUM	As desired
CALIBRATED PHASE	0
POWER	ON

Right recessed front-panel controls:

FIELD	1
SYNC	INT

#### 1. Adjust -15 Volt Power Supply

- a. Connect a precision DC voltmeter between ground and low voltage power supply board pin AD; see Fig. 6-2.
- b. CHECK-Voltmeter reading; -15 volts,  $\pm 0.5\%$  ( $\pm 0.07$  V).

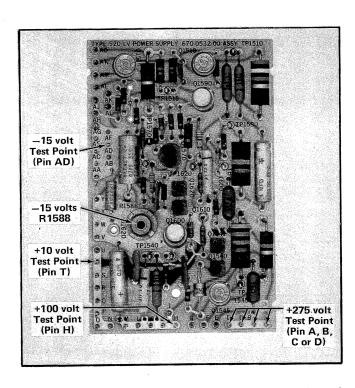


Fig. 6-2. Low-voltage power supply board voltage test point and adjustment locations,

- c. Adjust— -15 volts control, R1588 (see Fig. 6-2), for exactly -15 volts.
- d. INTERACTION—May affect operation of most circuits within the Type 520.
  - e. Disconnect the precision DC voltmeter.

#### 2. Check Low-Voltage Power Supply Voltages

- a. Connect a DC voltmeter between ground and input sync board pin W or X; see Fig. 6-3.
- b. CHECK-Voltmeter reading;  $\pm 3.6$  volts,  $\pm 5\%$  ( $\pm 0.18$  V).
- c. Move the DC voltmeter connections to ground and low-voltage power supply board pin T; see Fig. 6-2.
- d. CHECK-Voltmeter reading; +10 volts,  $\pm 3.5\%$  ( $\pm 0.35$  V).
- e. Move the DC voltmeter connections to ground and low-voltage power supply board pin H; see Fig. 6-2.
- f. CHECK-Voltmeter reading;  $\pm 100$  volts,  $\pm 3.5\%$  ( $\pm 3.5$  V).
- g. Move the DC voltmeter connections to ground and low-voltage power supply board pin A, B, C or D; see Fig. 6-2.

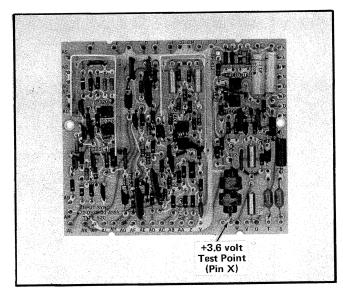


Fig. 6-3. Input sync board +3.6 V test point location.

- h. CHECK-Voltmeter reading;  $\pm 275$  volts,  $\pm 7\%$  ( $\pm 19.25$  V).
  - i. Disconnect the DC voltmeter.

#### 3. Check Low-Voltage Power Supply Ripple

- a. Set the test oscilloscope for 0.005 V/division vertical deflection factor, AC coupled, at a sweep rate of 5 ms/division, triggered with line frequency.
- b. Connect a 1X probe, from the test oscilloscope vertical input to the appropriate power supply test point as shown in Figs. 6-2 and 6-3.
- c. CHECK—Power supply ripple content as per Table 6-1 with input voltage level at both the low and high extremes of the voltage selector range.

TABLE 6-1

Voltage	Maximum Ripple Content  10 mV peak to peak	
–15 V		
+3.6 V	100 mV peak to peak	
+10 V	10 mV peak to peak	
+100 V	20 mV peak to peak	
+275 V	500 mV peak to peak	

d. Disconnect the 1X probe.

#### 4. Check High Voltage Power Supply

- a. Turn the Type 520 power off.
- b. Remove the metal CRT protector cap from the rear of the Type 520, then remove the rear cover from the CRT socket to achieve access to the interior of the socket.
- c. Connect a DC voltmeter between ground and the CRT socket terminal having a red-on-white wire attached to it (pin 2); see Fig. 6-4.
  - d. Turn the Type 520 power on.
- e. CHECK-Voltmeter reading; -3.875 kV,  $\pm 3\%$  ( $\pm 116.25$  V).

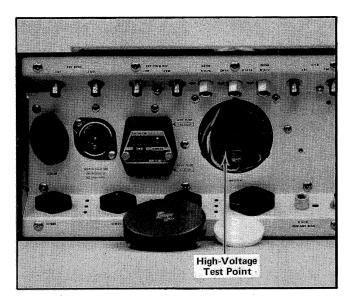


Fig. 6-4. High voltage test point location.

- f. Rotate the INTENSITY control fully clockwise.
- g. CHECK—Voltmeter reading; within  $\pm 40$  volts of the voltage reading in part e of this step.
- h. Rotate the INTENSITY control fully counterclockwise.
- i. CHECK—Voltmeter reading; within ±40 volts of the voltage reading in part e of this step.
- j. Turn off the Type 520 power, then disconnect the DC voltmeter.
- k. Re-assemble the CRT socket cover on the socket and replace the metal CRT protector cap onto the rear of the Type 520.
  - I. Turn the Type 520 power on.

#### 5. Adjust Geometry



- a. Press the Signal Selector FULL FIELD pushbutton and the Display Selector VECTOR pushbutton.
- b. Connect a DC voltmeter between ground and the upper CRT plate connection (blue wire); see Fig. 6-5A.
  - c. Note voltmeter reading.

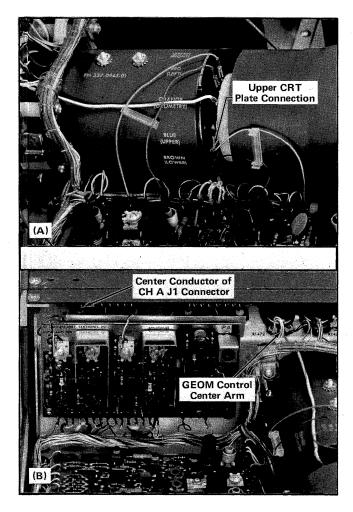


Fig. 6-5. Location of test point and adjustment locations for steps 5, 36, 39 and 40.

- d. Move the DC voltmeter connections to ground and the center arm of the GEOM control, R1472 (see Fig. 6-5B).
- e. CHECK—Voltmeter reading; should be about 20 volts below that noted in part c.
- f. ADJUST—Rear-panel GEOM control, R1472, until the voltmeter reading is the same as that described in part e.
- g. Press the Signal Selector A CAL pushbutton and the Display Selector Y pushbutton.
- h. Adjust the front-panel FOCUS control and the rear-panel ASTIG control, R1476, to obtain a well defined display.
- i. CHECK—Type 520 display; there should not be more than 0.05 centimeter of gradual bowing of the vertical or horizontal lines.

j. ADJUST-GEOM control, R1472, for minimum bowing of the vertical or horizontal lines.

#### 6. Adjust Astigmatism

•

- a. Cancel the Signal Selector A CAL pushbutton by momentarily pressing the CH A pushbutton. The Signal Selector FULL FIELD pushbutton remains depressed.
- b. Press the Display Selector VECTOR pushbutton and rotate the FOCUS control to its fully counterclockwise position.
- c. CHECK—Type 520 display should be a round spot near the center of the vector graticule.
- d. ADJUST-Rear-panel ASTIG control, R1476, until a round spot near the center of the vector graticule is obtained
  - e. Adjust the FOCUS control to obtain a focused spot.

#### 7. Adjust CRT Alignment

A

- a. Press the Signal Selector A CAL pushbutton. The Signal Selector FULL FIELD pushbutton and the Display Selector VECTOR pushbutton remain depressed for this step.
  - b. Turn off the Type 520 power.
- c. Disconnect the blue-blue on gray coax center lead (below SN B200000, blue on white wire) from pin AB on the driver amplifier board; see Fig. 6-6.
  - d. Turn on the Type 520 power.
- e. CHECK-Type 520 display alignment. Trace should be parallel throughout its length with the  $90^{\circ}$ - $270^{\circ}$  axis of the vector graticule. It may be necessary to adjust the HORIZ POSITION CLAMP to place the trace in a better position for checking.
- f. ADJUST-Front-panel BEAM ROTATE control, R1470, until trace is parallel throughout its length to the  $90^{\circ}$ -270° axis of the vector graticule.
  - g. Turn off the Type 520 power.

- h. Reconnect the wire disconnected in part c to pin AB on the driver amplifier board.
- i. Disconnect the green-green on gray coax center lead (below SN B200000, green on white wire) from pin AD on the driver amplifier board; see Fig. 6-6.
  - j. Turn on the Type 520 power.
- k. CHECK—R520 display alignment. Trace should be parallel throughout its length to the 0°-180° axis of the vector graticule. It may be necessary to adjust the VERT POSITION CLAMP to place the trace in a better position for checking.
- I. ADJUST—Rear-panel ORTH control, R1474, until trace is parallel throughout its length to the  $0^{\circ}$ -180° axis of the vector graticule.
  - m. Turn off the Type 520 power.
- n. Reconnect the wire disconnected in part i to pin AD on the driver amplifier board.
  - o. Turn on the Type 520 power.
- p. Repeat parts f and I of this step several times to minimize interaction between the adjustments.

#### 8. Adjust Unblanking Bias



- a. All pushbuttons remain as they are.
- b. Reduce the display intensity until the test circle is barely visible.
- c. CHECK—Type 520 display; test circle should have uniform intensity throughout its circumference.
- d. ADJUST—Rear-panel UNBLANK BIAS control, R1478, for a uniform intensity throughout the circumference of the test circle.

#### 9. Adjust VITS Intensity



- a. Apply a modulated staircase signal from the Type 140 comp video connector through a 75 ohm coaxial cable to the Type 520 CH A J1 connector. Connect a 75 ohm end-line termination to the CH A J2 connector.
- b. Set the Type 140 VITS controls for a VIT staircase signal on line 18 of both fields.
- c. Depress Signal Selector CH A,  $\mathrm{A}\phi$  and VITS 18 push-buttons.
  - d. Depress the Display Selector Y pushbutton.

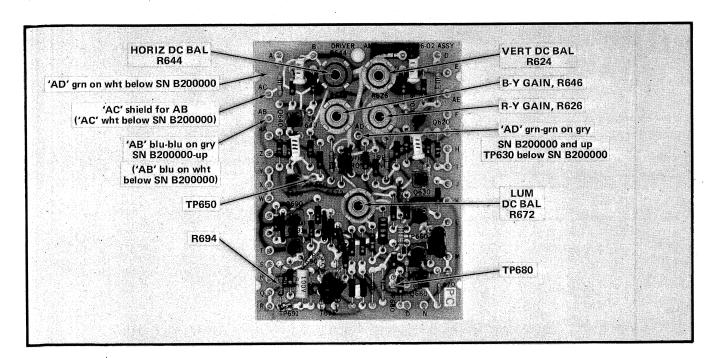


Fig. 6-6. Driver amplifier board pin connector, test point and adjustment locations.

- e. Set the Type 520 INTENSITY control for the desired display brightness.
- f. ADJUST-VIT INTENS, R1228 (see Fig. 6-7), for maximum display intensity without any display defocusing.
- g. Disconnect the video signal source, the 75 ohm coaxial cable and the 75 ohm end-line termination.

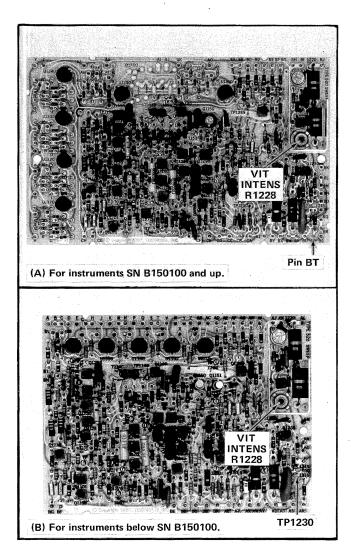


Fig. 6-7. Sweep board test point and adjustment locations.

#### Front-panel controls:

Signal Selector	FULL FIELD
CHANNEL A	
100%-75%-MAX GAIN	75%
GAIN	CAL
$\phi$ REF	BURST
CHANNEL B	
100%-75%-MAX GAIN	75%
GAIN	CAL
Display Selector	No buttons depressed
INTENSITY	As desired
LUMINANCE GAIN	CAL
SCALE ILLUM	As desired
CALIBRATED PHASE	0
POWER ON	ON

Right recessed front-panel controls:

FIELD	1
SYNC	INT

#### 10. Adjust DC Balance of R-Y Amplifier

- a. Set the test oscilloscope for a vertical deflection factor of 5 mV/division, DC coupled, at a sweep rate of 1 ms/division with internal triggering.
- b. Ground the test oscilloscope input and position the display to establish a ground reference.
- c. Connect the test oscilloscope 10X probe to the driver amplifier board pin AD (below SN B200000, TP630); see Fig. 6-6.
- d. CHECK—DC output voltage of amplifier must be 0.0 volt (ground potential).
- e. ADJUST-VERT DC BAL control, R624 (see Fig. 6-6), until the DC voltage output of the amplifier is 0.0 volt.
  - f. Disconnect the 10X probe.

#### 11. Adjust DC Balance of B-Y Amplifier

- a. Set the test oscilloscope for a vertical deflection factor of 5 mV/division, DC coupled, at a sweep rate of 1 ms/division with internal triggering.
- b. Establish a ground reference point on the test oscilloscope by grounding the input and positioning the trace to a graticule reference.
- c. Connect the test oscilloscope 10X probe to the driver amplifier board TP650 (emitter of Q650); see Fig. 6-6.
- d. CHECK—DC output voltage of amplifier must be 0.0 volt (ground potential).
- e. ADJUST-HORIZ DC BAL control, R644 (see Fig. 6-6), until the DC voltage output of the amplifier is 0.0 volt.
  - f. Disconnect the 10X probe.

#### 12. Adjust DC Balance of Y Amplifier

- a. Set the test oscilloscope for a vertical deflection factor of 10 mV/division, DC coupled, at a sweep rate of 1 ms/division with internal triggering.
- b. Establish a ground reference level on the test oscilloscope by grounding the input and positioning the display to some graticule line.
- c. Connect the test oscilloscope 10X probe to driver amplifier board TP680 (collector of Q680 via R684); see Fig. 6-6.
- d. CHECK-DC voltage output of amplifier must be  $\pm 0.5$  volt.
- e. ADJUST-LUM DC BAL control, R672 (see Fig. 6-6), until the DC voltage output of the amplifier is  $\pm 0.5$  volt.
  - f. Disconnect the 10X probe and test oscilloscope.

#### 

- a. Press the Signal Selector FULL FIELD pushbutton and the Display Selector VECTOR pushbutton.
- b. Adjust the INTENSITY control so the displayed spot on the CRT of the Type 520 will not burn the phosphor.
- c. CHECK—Type 520 displayed spot position; must be at the center of the vector graticule.
- d. ADJUST—Front panel VERT POSITION CLAMP (R880) and HORIZ POSITION CLAMP (R1002) controls to position the spot to the center of the vector graticule.

- e. Connect a DC voltmeter between ground and TP980 on the output amplifier board; see Fig. 6-8.
  - f. CHECK-Voltmeter reading; should be +5.6 volts.
- g. ADJUST-HORIZ COM MODE LEV control, R985 (see Fig. 6-8), until the voltmeter reading is exactly +5.6 volts
- h. Move the DC voltmeter connections to ground and TP870; see Fig. 6-8.
  - i. CHECK-Voltmeter reading; should be +5.6 volts.
- j. ADJUST-VERT COM MODE LEV control, R875 (see Fig. 6-8), until the voltmeter reading is exactly +5.6 volts.
  - k. Disconnect the DC voltmeter.

0

I. INTERACTION—The adjustments in part d of this step interact with the adjustments performed in parts g and j of this step.

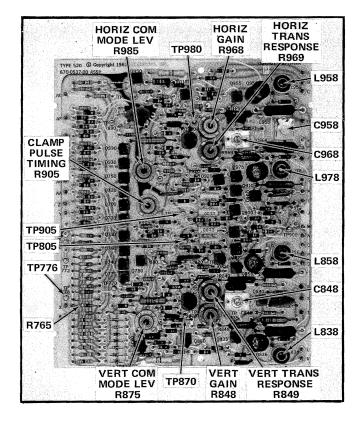


Fig. 6-8. Output amplifier board test point and adjustment locations.

#### Front-panel controls:

Signal Selector	<b>CH A, A</b> $\phi$ , and
_	FULL FIELD
CHANNEL A	
100%-75%-MAX GAIN	<b>75</b> %
GAIN	CAL
$\phi$ REF	BURST
CHANNEL B	
100%-75%-MAX GAIN	75%
GAIN	CAL
Display Selector	VECTOR
INTENSITY	As desired
LUMINANCE GAIN	CAL
SCALE ILLUM	As desired
CALIBRATED PHASE	0
POWER	ON

#### Right recessed front-panel controls:

FIELD		1
SYNC		INT

#### 14. Adjust Clamp Pulse Timing

- a. Connect a modulated staircase signal from the Type 140 comp video connector through a 75 ohm coaxial cable to the Type 520 CH A J1 connector.
- b. Connect a 75 ohm coaxial cable from the CH A J2 connector to the CH B J50 connector.
- c. Connect a 75 ohm end-line termination to the CH B J51 connector.
- d. Connect a 10X probe from the test oscilloscope channel 1 vertical input connector to TP805 on the output amplifier board; see Fig. 6-8.
- e. Connect another 10X probe from the test oscilloscope channel 2 vertical input connector to TP905; see Fig. 6-8.
- f. Set the test oscilloscope for a vertical deflection factor of 0.2 V/division, AC coupled with input channels non-inverted and alternately displayed, at a sweep rate of  $20 \,\mu\text{s}$ /division with internal triggering.
- g. CHECK—Test oscilloscope display; superimposed channel 1 and 2 waveforms displayed for the vertical and horizontal amplifiers must meet or exceed the minimum amplitude shown in Fig. 6-9.

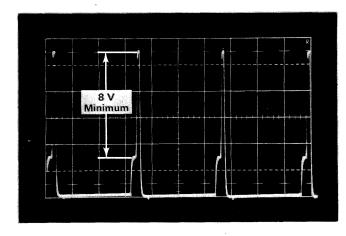


Fig. 6-9. Superimposed channel 1 and 2 waveforms showing minimum amplitude requirement for vertical and horizontal amplifiers when adjusting clamp pulse timing.

- h. ADJUST—CLAMP PULSE TIMING control, R905 (see Fig. 6-8), until the alternately displayed waveforms on the test oscilloscope meet or exceed the minimum waveform amplitude shown in Fig. 6-9, but not so far as to cause waveform distortion.
- i. Disconnect the test oscilloscope and the two 10X probes. Do not disconnect any of the video signal connections.

# 15. Adjust Channel A and B Input Amplifier Frequency Response Gain

#### NOTE

For final adjustment of C52, see step 36.

- a. Test equipment connections are as described in parts a through c in step 14.
- b. Set the Type 140 controls for a standard color bar output signal with this exception: set the White Ref switch to 100 IRE.
- c. Set the test oscilloscope for single-channel operation, a vertical deflection factor of 20 mV/division, DC coupled, at a sweep rate of 10  $\mu s$ /division with internal triggering.
- d. Connect a 10X probe from the test oscilloscope vertical input connector to TP 85; see Fig. 6-10.
- e. CHECK—Test oscilloscope display; peaks of the yellow and cyan bars are equal to the 100 IRE unit white bar as viewed on the test oscilloscope.

0

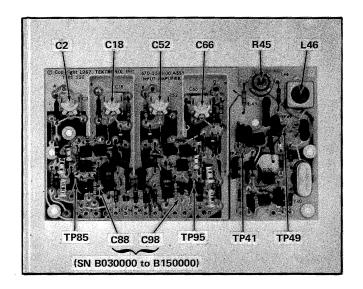


Fig. 6-10. Input amplifier board test point and adjustment locations.

- f. ADJUST-C2, see Fig. 6-10, until the peaks of the yellow and cyan bars are equal to the 100 IRE white bar as viewed on the test oscilloscope (see Fig. 6-11).
- g. Disconnect the test oscilloscope 10X probe from TP85 and connect it to TP95; see Fig. 6-10.

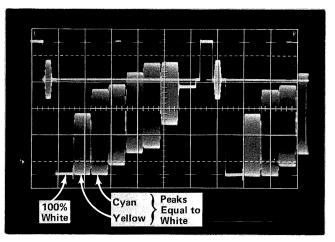


Fig. 6-11. Typical color bar display obtained when C2 and C52 are properly adjusted.

- h. CHECK—Test oscilloscope display; peaks of the yellow and cyan bars must be equal to the 100 IRE unit white bar.
- i. ADJUST-C52, see Fig. 6-10, until the peaks of the yellow and cyan bars are equal to the 100 IRE unit white bar as viewed on the test oscilloscope.
- j. Disconnect the 10X probe, video signal source, two 75-ohm coaxial cables and the 75-ohm end-line termination.

NOIES					

Front panel controls:

Signal Selector **A CAL** A $\phi$  and **FULL FIELD CHANNEL A** 100%-75%-MAX GAIN 75% GAIN CAL **BURST**  $\phi$  REF CHANNEL B 100%-75%-MAX GAIN 75% GAIN CAL Display Selector **VECTOR** INTENSITY As desired **LUMINANCE GAIN** CAL SCALE ILLUM As desired CALIBRATED PHASE n ON **POWER** 

Right recessed front-panel controls:

FIELD 1 SYNC INT

#### 16. Adjust Test Circle Oscillator

- a. Connect a DC voltmeter between ground and TP41 on the input amplifier board, see Fig. 6-10.
- b. CHECK-Voltmeter should read approximately -0.4 volt.
- c. ADJUST-L46, see Fig. 6-10, for minimum voltage reading on the voltmeter.
  - d. Disconnect the DC voltmeter.
- e. Connect a 10X probe from the vertical input connector on the test oscilloscope to TP49; see Fig. 6-10.
- f. Set the test oscilloscope for a vertical deflection factor of 20 mV/division, AC coupled, at a sweep rate of 1 ms/division with internal triggering.
- g. CHECK—Test oscilloscope display; must be 3.5 major divisions in amplitude (approximately 707 mV).
- h. ADJUST-R45, see Fig. 6-10, until the test oscilloscope display amplitude is 3.5 major divisions.
- i. Disconnect the 10X probe from the test point and the oscilloscope.

### 17. Adjust Test Circle Oscillator Compensation

a. Depress the Signal Selector CH A and B CAL pushbuttons. The other pushbuttons remain as they are.

- b. Set the test oscilloscope for a vertical deflection factor of 0.2 V/division.
- c. Connect a 100% amplitude, 0% setup, (R-Y and B-Y off) color bar signal from the Type 140 comp video connector through a 75-ohm coaxial cable, 75-ohm feed-thru termination and a dual-input cable connector to channels 1 and 2 of the test oscilloscope. Check that the two displays are matched in amplitude. If not, adjust the oscilloscope vertical gain control adjustment to obtain matched amplitude displays.
- d. Remove the dual-input cable connector and connect the signal to channel 1.
- e. Apply a 3.58 MHz signal from the Type 191 through a 50-ohm cable, a 50-ohm to 75-ohm minimum loss attenuator and a 75-ohm feed-thru termination to the test oscilloscope channel 2 Input connector.
- f. Adjust the Type 191 output amplitude until the signal extends from sync tip to the green luminance level. (The Type 191 is now preset for an output amplitude of 707 mV P-P.)
- g. Disconnect the Type 191 signal from test oscilloscope. Apply the signal through the 50-ohm cable and 50-ohm to 75-ohm minimum loss attenuator to the Type 520 CH A J1 connector.
- h. Connect the 75-ohm feed-thru termination used in part e to the Type 520 CH A J2 connector.
- i. CHECK—Type 520 displayed channel B test circle size; must be exactly the same size as the channel A displayed circle.
- j. ADJUST-C66, see Fig. 6-10, until the channel B test circle is the same size as the channel A displayed circle.
  - k. Depress the Signal Selector A CAL pushbutton.
- I. CHECK—Type 520 displayed channel A test circle size; must be exactly the same size as the channel B displayed test circle.
- m. ADJUST—C18, see Fig. 6-10, until the channel A test circle is the same size as the channel B displayed test circle.
- n. Disconnect the Type 191, the 75-ohm coaxial cable, minimum loss attenuator, and the 75-ohm feed-thru termination.

Front-panel controls:

Signal Selector A CAL,  $A\phi$  and FULL FIELD

CHANNEL A

100%-75%-MAX GAIN 75%
GAIN CAL  $\phi$  R EF BURST

CHANNEL B

100%-75%-MAX GAIN 75%
GA IN CAL
Display Selector Y
INTENSITY As des

INTENSITY As desired
LUMINANCE GAIN CAL
SCALE ILLUM As desired
CALIBRATED PHASE 0

CALIBRATED PHASE POWER

ΟŅ

Right recessed front-panel controls:

FIE LD SYNC

INT

#### 18. Adjust Luminance Calibrator

#### 0

#### NOTE

This step uses a precision DC voltmeter. Step 18A is an alternative procedure that uses a Standard Amplitude Calibrator (Tektronix calibration fixture 067-0502-00).

- a. Remove Q570 (see Fig. 6-12) from its socket on the demodulator board.
- b. Connect a precision DC voltmeter between ground and TP583 (see Fig. 6-12).
  - c. Note the voltmeter reading (about -5 mV).
  - d. Re-install Q570 and remove Q571.
- e. CHECK-Voltmeter reading; should be one volt more positive then the voltage noted in part c.
- f. ADJUST-LUMINANCE CAL control, R583 (see Fig. 6-12), until the voltmeter reading is one volt more positive than that noted in part c.
- g. Disconnect the precision DC voltmeter and re-install Q571 in its socket.

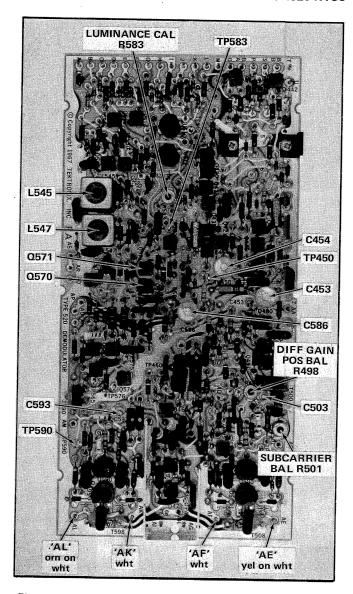


Fig. 6-12. Demodulator board test point and adjustment locations.

#### 18A. Adjust Luminance Calibrator

#### •

#### NOTE

This is an alternative procedure that can be used if a Standard Amplitude Calibrator (Tektronix calibration fixture 067-0502-00) is available.

- a. Connect a 1X probe to the test oscilloscope differential amplifier A input.
- b. Set the controls of the standard amplitude calibrator for a square-wave signal of 1 V.
- c. Connect the standard amplitude calibrator output to the differential amplifier B input.

- d. Connect the 1X probe from the test oscilloscope A input connector to TP583 on the demodulator board; see Fig. 6-12.
- e. Set the test oscilloscope for a vertical deflection factor of 50 mV/division, AC coupled, at a sweep rate of .5 ms/division with internal triggering.
- f. CHECK—Test oscilloscope display; must appear similar to Fig. 6-13. (The bottom of the upper waveform is aligned with the top of the lower waveform.)
- g. ADJUST-LUMINANCE CAL control, R583 (see Fig. 6-12) for a test oscilloscope display similar to Fig. 6-13.
- h. Disconnect the standard amplitude calibrator, the test oscilloscope and the probe.



- a. Connect a 10X probe to each input of the differential amplifier.
- b. Adjust the test oscilloscope 10X probe compensation so the two probes match each other.
- c. After the 10X probes have been matched, connect one probe from the test oscilloscope channel A vertical input connector to TP583 on the demodulator board; and the other probe from channel 2 vertical input connector to TP450; see Fig. 6-12.

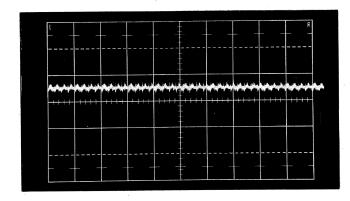


Fig. 6-13. Typical waveform obtained when LUMINANCE CAL control, R583, is correctly adjusted using step 18A procedure.

- d. Set the test oscilloscope for a vertical deflection factor of 5 mV/division, ac coupled, at a sweep rate of 1 ms/division with internal triggering.
- e. ADJUST-Front-panel A CAL control, R402, until the test oscilloscope display amplitude is minimum.
  - f. Disconnect the two 10X probes from the Type 520.

#### 20. Adjust Channel B Gain

- a. Press the Signal Selector B CAL and  ${\rm B}\phi$  pushbuttons. Do not cancel the A CAL pushbutton.
- b. ADJUST—Front-panel B CAL control, R412, until the channel B waveform overlays the channel A waveform.

# NOTES

# Front-panel controls:

Signal Selector	<b>CH A</b> , <b>A</b> $\phi$ and FULL FIELD
CHANNEL A	•
100%-75%-MAX GAIN	75%
GAIN	CAL
$\phi$ REF	BURST
CHANNEL B	
<b>100</b> %-75%-MAX GAIN	75%
GAIN	CAL
Display Selector	Υ
INTENSITY	As desired
LUMINANCE GAIN	CAL
SCALE ILLUM	As desired
CALIBRATED PHASE	0
POWER	ON

### Right recessed front-panel controls:

FIELD	1
SYNC	INT

# 21. Adjust Subcarrier Regenerator Input 3.58 MHz Filter

- a. Apply a color bar signal from the Type 140 to the CH A J1 connector via a 75 ohm coaxial cable.
- b. Connect a 75 ohm coaxial cable from the CH A J2 connector to the CH B J50 connector and a 75 ohm end-line termination to the CH B J51 connector.
- c. Connect a 10X probe from the test oscilloscope vertical input connector to TP220 on the subcarrier regenerator board; see Fig. 6-14.
- d. Connect a 75 ohm coaxial cable from the Type 140 comp video connector to the test oscilloscope trigger input connector.

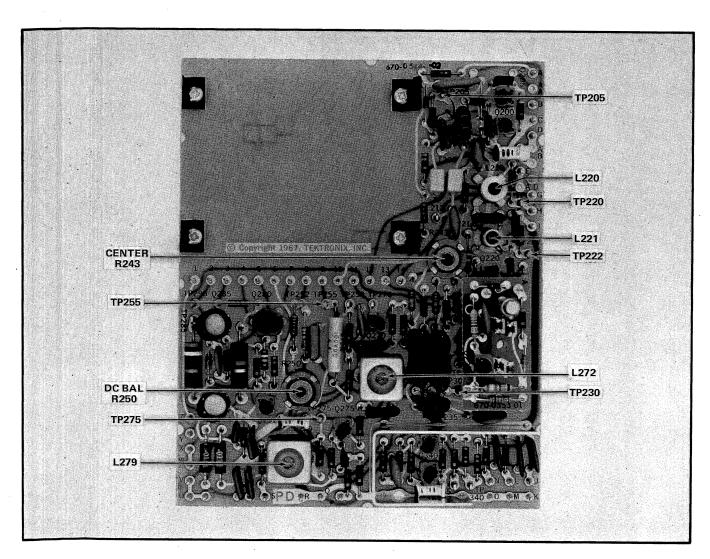


Fig. 6-14A. Subcarrier regenerator board test point and adjustment locations for instruments SN B251880 and up.

- e. Set the test oscilloscope for a vertical deflection factor of 0.05 V/division, AC coupled, at a sweep rate of 10  $\mu$ s/division with external triggering.
- f. CHECK—Test oscilloscope display amplitude; 2.5 volts or less.
- g. ADJUST-L220, see Fig. 6-14, for minimum test oscilloscope display amplitude of the 3.58 MHz burst.
- h. Disconnect the test oscilloscope 10X probe from TP220 and connect it to TP222 on the subcarrier regenerator board; see Fig. 6-14.
- i. Set the test oscilloscope for a vertical deflection factor of 0.01 V/division, AC coupled.

- j. CHECK—Test oscilloscope display amplitude; 0.2 volt or greater.
- k. ADJUST-L221, see Fig. 6-14, for maximum test oscilloscope display amplitude with the best transient response of the color bar packets.
- I. Disconnect 10X probe and test oscilloscope. Video input signal remains connected.

# 22. Check Burst Intensification Pulse

a. Connect a 10X probe from the test oscilloscope to TP205 on the subcarrier regenerator board (see Fig. 6-14). Externally trigger the test oscilloscope from the composite sync signal of the Type 140. Set Trigger Slope switch to —, and the source switch to Ext.

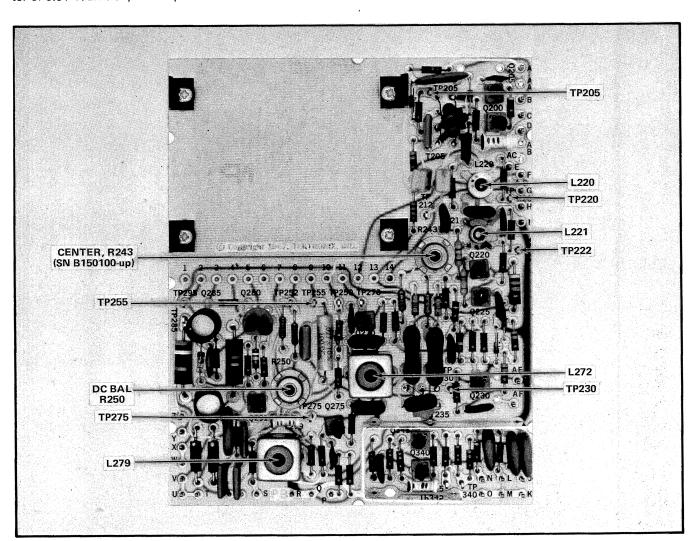


Fig. 6-14B. Subcarrier regenerator board test point and adjustment locations for instruments below SN B251880.

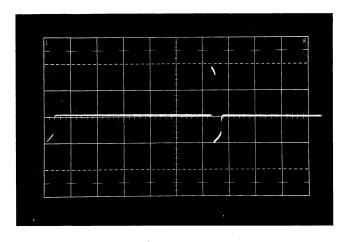


Fig. 6-15. Typical burst intensification pulse.

- b. Set the test oscilloscope for a vertical deflection factor of .2 V/division, AC coupled, at a sweep rate of 10  $\mu s/division$  .
- c. CHECK—Test oscilloscope display; should appear similar to the waveform in Fig. 6-15.

# 23. Adjust Burst Gate Pulse

- 5C
- a. Connect the 10X probe to TP230 on the subcarrier regenerator board (see Fig. 6-14).
- b. Set the test oscilloscope for a vertical deflection factor of 0.5 V/division. Leave the other controls as in step 22, parts a and b.
- c. CHECK—Test oscilloscope display; should have a minimum peak to peak amplitude of 7 volts (8 volts nominal) and appear as shown in Fig. 6-16.

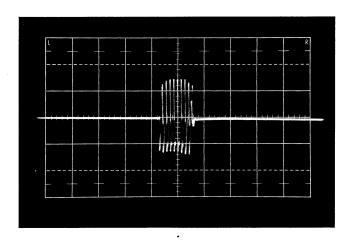


Fig. 6-16. Correct burst gate pulse waveform shape.

- d. Connect the 10X probe to TP205. Set the sweep rate to 5  $\mu$ s/division and the Horiz Magnifier to X10, (0.5  $\mu$ s/division).
- e. Depress the Display Selector LINE SWEEP pushbutton and reduce the intensity so that the intensified burst can be seen. If necessary, rotate the A PHASE control for maximum burst amplitude.
- f. Rotate the front-panel BURST FLAG TIMING control R1158 until the burst intensification is centered on the burst pulse.
  - g. Depress the Display Selector Y pushbutton.
- h. With the test oscilloscope Horizontal Position control, position a transition of the burst intensification pulse to the graticule center line.
- i. CHECK—Rotate the BURST FLAG TIMING control R1158 to each of its extremes and note when the luminance display of the Type 520 loses vertical restoration; i.e., stable blanking level. Check that at these extremes the test oscilloscope display should shift  $\pm 0.5~\mu s$  from its centered position described in part h of this step.

### NOTE

If either limit described in part i cannot be obtained, repeat step 21 procedure. Adjustment of L220 and L221 affects the range. If either limit cannot be obtained, select a new value for R694 (see Fig. 6-6).

- j. Press the Display Selector LINE SWEEP pushbutton.
- k. ADJUST—Front-panel BURST FLAG TIMING control, R1158, until the burst intensification is centered on the burst pulse.
  - I. Disconnect the 10X probe.

# 24. Adjust Subcarrier Regenerator DC • • Balance

- a. Disconnect the 75 ohm coaxial cable from the CH A J2 connector and the CH B J50 connector. The video signal to CH A J1 connector remains connected.
- b. Connect a 75 ohm end-line termination to the CH A J2 connector. The 75 ohm end-line termination on the CH B J51 connector remains connected.

- c. Press the Signal Selector CH A pushbutton and the Display Selector VECTOR pushbutton.
- d. Set the test oscilloscope for a vertical deflection factor of 0.02 V/division, DC coupled, at a sweep rate of 1 ms/division with internal triggering.
- e. Establish a ground reference point on the test oscilloscope by grounding the input and positioning the display to a graticule line.
- f. Connect the test oscilloscope 10X probe to TP255 on the subcarrier regenerator board; see Fig. 6-14.
- g. Note the DC level of the test oscilloscope display. A stable vector (oscillator locked to signal) must be obtained before this DC level can be observed. If the vector is not stable, (oscillator not locked to signal) slowly adjust the DC BAL control, R250 (see Fig. 6-14), until a stable vector is obtained; then note DC level.

#### NOTE

Parts h through r are used for instruments SN B150100 and up. For instruments below SN B150100 proceed to part s.

- h. Press the Signal Selector A CAL pushbutton.
- i. CHECK—Test oscilloscope display DC level; must be the same as that noted in part g of this step.
- j. ADJUST-DC BAL control, R250, until the test oscilloscope display DC level is the same as that noted in part g.
- k. Press the Signal Selector CH A pushbutton and note the display DC level.
- I. Repeat parts g through k of this step until the test oscilloscope DC level remains the same when either the Signal Selector CH A or A CAL pushbutton is pressed.
- m. Press the Signal Selector CH A pushbutton and set the  $\Phi\,\text{REF}$  switch to EXT.
- n. CHECK—Test oscilloscope display DC level; must be the same as noted in part k of this step.
- ADJUST—CENTER control, R243 (see Fig. 6-14), until the DC level is the same as that noted in part k.

- p. Return the  $\phi$  REF switch to BURST.
- ${\bf q}.$  Repeat parts  ${\bf g}$  through o until adjustment interaction is minimized.
- r. Disconnect the 10X probe and the test oscilloscope. (The video input signal remains connected.)

#### NOTE

Parts s through y are used for instruments below SN B150100 only.

- s. Press the Signal Selector A CAL pushbutton.
- t. CHECK—Test oscilloscope display DC level; must be the same as noted in part g of this step.
- u. ADJUST—DC BAL control, R250, (see Fig. 6-14) until the test oscilloscope display DC level is the same as that noted in part g of this step.
- v. Cancel the A CAL and press the CH A Signal Selector pushbuttons.
- w. CHECK—Type 520 display; a stable vector must be obtained 15 seconds after completion of part v of this step.
- x. Repeat parts e through g and s through w of this step until all adjustment interaction is minimized.
- y. Disconnect the 10X probe and the test oscilloscope. (The video input signal remains connected.)

# 25. Check Subcarrier Regenerator Circuit 3.58 MHz Output Signal

- a. Connect a 10X probe from the test oscilloscope vertical input connector to TP275 on the subcarrier regenerator board; see Fig. 6-14.
- b. Set the test oscilloscope for a vertical deflection factor of 0.2 V/division, AC coupled, at a sweep rate of 0.5  $\mu$ s/division with internal triggering.
- c. CHECK—Test oscilloscope display amplitude of the 3.58 MHz signal should equal approximately 4 volts peak to

peak. Adjust L272 for maximum amplitude if amplitude is below 3.5 V. Final adjustment will be made in step 36x.

d. Disconnect the 10X probe, the two 75 ohm coaxial cables, the video signal source and the 75 ohm end-line termination.

# 26. Check Oven Preheater Operation

- a. Connect a DC voltmeter between ground and pin Q, R, or S (+10 volts unregulated power supply) of the rectifier board; see Fig. 6-17.
  - b. Note voltmeter reading.
- c. Disconnect DC voltmeter from pin Q, R or S of rectifier board and connect it between TP295 and ground; see Fig. 6-14.
- d. CHECK—Voltmeter reading should be the same as that noted in part b of this step after at least 20 minutes of warmup.

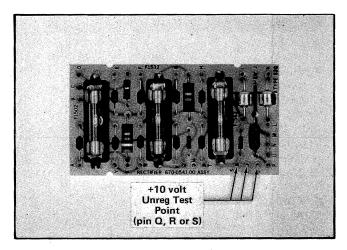


Fig. 6-17. Rectifier board test point location.

### NOTE

At initial turn-on of a cold instrument, the voltage at TP295 is about -15 volts. In 3 minutes the voltage rises to approximately +20 volts and remains at this voltage while the instrument is on.

e. Disconnect the DC voltmeter.

	•	NOTES	
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Front-panel controls:

Signal Selector

CH A, A $\phi$  and FULL FIELD

CHANNEL A

100%-75%-MAX GAIN

75% CAI

 $\begin{array}{c} \mathsf{GAIN} \\ \phi \ \mathsf{REF} \end{array}$ 

CAL BURST

**CHANNEL B** 

100%-75%-MAX GAIN

75%

GAIN
Display Selector

CAL

INTENSITY

VECTOR

LUMINANCE GAIN

As desired CAL

SCALE ILLUM

As desired

CALIBRATED PHASE

As desired

POWER

ŌN

Right recessed front-panel controls:

FIELD

1

SYNC

INT

# 27. Adjust Subcarrier Filter

- a. Connect a 10X probe from the test oscilloscope vertical input connector to TP590 on the demodulator board (see Fig. 6-12).
- b. Set the test oscilloscope for a vertical deflection factor of 0.1 V/division, AC coupled, at a sweep rate of 0.5  $\mu$ s/division with internal triggering.
- c. CHECK—Test oscilloscope display amplitude of the 3.58 MHz subcarrier waveform should be approximately 1.2 volts peak to peak.
- d. ADJUST-L545, see Fig. 6-12, for maximum 3.58 MHz subcarrier amplitude but not more than 1.2 volts peak to peak.
  - e. Disconnect the 10X probe.
- f. Apply the color bar video signal to CH A J1 connector via a 75 ohm coaxial cable and connect a 75 ohm end-line termination to the CH A J2 connector.
- g. Line up the burst vector on the Type 520 exactly with the I marking on the vector graticule, using the channel A PHASE control.
- h. Holding the Display Selector VECTOR pushbutton all the way down, press the Display Selector I pushbutton slowly until display rotation is noted.

- i. CHECK—Amount of Type 520 display rotation and direction; should rotate  $33^\circ$ ,  $\pm 2^\circ$  clockwise. This will cause the burst vector to line up with the  $90^\circ$  vector graticule point.
- j. While still holding the Display Selector VECTOR pushbutton all the way down, press the Display Selector Q pushbutton slowly until a display rotation is noted.
- k. CHECK—Amount of display rotation and direction; should rotate  $33^{\circ}$ ,  $\pm 2^{\circ}$  clockwise. This will cause the burst vector to line up with the  $90^{\circ}$  vector graticule point.
- I. ADJUST-L547, see Fig. 6-12, while performing part i or k of this step until exactly  $33^{\circ}$  of display rotation in clockwise direction is noted.
  - m. Repeat parts g through k.
- n. Repeat entire step, as needed, to remove the interaction between parts d and l.
- o. Line up the burst vector on the Type 520 exactly on the I graticule mark, then press the Display Selector Q pushbutton, allowing the VECTOR pushbutton to cancel.
- p. CHECK—That the burst portion of the display is nulled  $\pm 2^\circ$  using the CALIBRATED PHASE control.
- q. Press the Display Selector VECTOR pushbutton and line up the burst vector on the Q graticule mark, then press the Display Selector I pushbutton, allowing the VECTOR pushbutton to cancel.
- r. CHECK—That the burst portion of the display is nulled  $\pm 2^{\circ}$  using the CALIBRATED PHASE control.
- s. Disconnect the 75 ohm coaxial cable and video signal source. The 75 ohm end-line termination remains connected to the CH A J2 connector.
- t. INTERACTION—This step interacts with steps 10 and 11. Steps 10 and 11 should be repeated before proceeding.

# 28. Adjust 10.4 MHz and 18 MHz Traps

O

a. Connect a 10.4 MHz sine wave signal, 1 volt in amplitude, from a medium frequency constant amplitude signal

generator through a 5 ns coaxial cable, a GR to BNC male adapter and a 50 ohm to 75 ohm minimum loss attenuator, to the Type 520 CH A J1 connector.

- b. ADJUST—C454, see Fig. 6-12, for minimum circle diameter.
- c. Apply an 18 MHz sine wave signal, 1 volt in amplitude, from the medium frequency generator to the Type 520.
- d. ADJUST-C453, see Fig. 6-12, for minimum circle diameter.
- e. Repeat several times because the adjustments in parts **b** and d interact.
- f. Disconnect the medium frequency generator, 5 ns coaxial cable, GR to BNC male adapter and 50 ohm to 75 ohm minimum loss attenuator. The 75 ohm end-line termination remains connected to the CH A J2 connector.

# 29. Adjust Subcarrier Balance

- 1. Cancel all the Signal Selector pushbuttons except the FULL FIELD pushbutton.
- b. Press the Signal Selector A CAL pushbutton and the Display Selector LINE SWEEP pushbutton.
  - c. Note trace position.
- d. Press the Display Selector I, Q, and DIFF PHASE in sequence.
- e. CHECK—Trace positions; the trace position noted in (LINE SWEEP trace), (I trace), (Q trace) and (DIFF PHASE trace) must be the same within 3 IRE units.
- f. ADJUST-SUBCARRIER BAL control, R501 (see Fig. 6-12), so the trace remains in the same position, as the Display Selector LINE SWEEP pushbutton is pushed, then the Display Selector I, Q, and DIFF PHASE, pushbuttons are pushed.
- g. Check that a 75 ohm end-line termination is connected to the Type 520 CH A J2 connector, then press the Display Selector DIFF PHASE pushbutton.

- h. CHECK—There should be no separation of the traces on the Type 520 display.
- i. ADJUST—C593, see Fig. 6-12, for no trace separation. Press the Display Selector Q pushbutton. Adjust C503 for no trace separation.
  - j. Repeat parts e through i until interaction is removed.

# 30. Adjust Quadrature Phase Alignment

0

- a. Apply a modulated staircase signal to the CH A J1 connector via a 75 ohm coaxial cable. (Check that a 75 ohm end-line termination is connected to the CH A J2 connector.)
  - b. Set the Type 520 controls as follows:

Signal Selector

B CAL and FULL FIELD

Display Selector QUAD PHASE

VECTOR Midrange

- c. Note the degree of overlay the test circles have to each other.
- d. Rotate the QUAD PHASE control fully clockwise and note the amount of separation of the test circles with reference to the display noted in part c.
- e. Rotate the QUAD PHASE control fully counterclockwise and again note the amount of separation of the test circles.
- f. CHECK—Test circle separation noted in parts d and e of this step should be equal.
- g. ADJUST-C586 until the test circle separations are equal.
- h. Set the QUAD PHASE control for best overlay of the test circle.
- i. Disconnect the video signal source, 75 ohm coaxial cable, and the 75 ohm end-line termination.

# 31. Adjust Vertical Gain

1

a. Depress the Signal Selector A CAL and Display Selector Y pushbuttons. Cancel the B CAL pushbutton. Check that the FULL FIELD pushbutton is depressed.

- b. Align the bottom line of the calibrator signal with the -40 IRE line on the IRE graticule.
- c. CHECK—Top of calibrator signal on the Type 520 display should align with the  $\pm 100$  IRE line on the IRE graticule.
- d. ADJUST-VERT GAIN control, R848 (see Fig. 6-8) until the top of the calibrator signal aligns with the +100 IRE line on the IRE graticule.

# 32. Adjust Chroma R-Y Gain

- a. Depress the Display Selector VECTOR pushbutton. The other pushbuttons remain as they are.
- b. CHECK-Type 520 test circle position; must be tangent to the inscribed circle on the vector graticule at the  $90^{\circ}$  and  $270^{\circ}$  points.
- c. ADJUST-R-Y GAIN control, R626 (see Fig. 6-6) so test circle is tangent to the inscribed circle on the vector graticule at the  $90^{\circ}$  and  $270^{\circ}$  points.

# 33. Adjust Horizontal Gain to Match Vertical Gain

- a. Turn off the Type 520 power.
- b. Disconnect the green-green on gray coax center lead (below SN B200000, green on white wire) going to the vertical amplifier from pin AD on the driver amplifier board; see Fig. 6-6.
- c. Disconnect the blue-blue on gray coax center lead (below SN B200000, blue on white wire) going to the horizontal amplifier from pin AB on the driver amplifier board; see Fig. 6-6.
- d. Connect the wire, disconnected in part c of this step, to pin AD on the driver amplifier board.

- e. Turn on the Type 520 power.
- f. CHECK—Type 520 trace length; horizontal trace should be the same length as the diameter of the inscribed circle on the vector graticule.
- g. ADJUST—HORIZ GAIN control, R968 (see Fig. 6-8) until the trace length is equal to the diameter of the inscribed circle on the vector graticule.

#### NOTE

R968 is readjusted slightly in step 35.

- h. Turn off the Type 520 power.
- i. Disconnect the wire, described in part c of this step, from pin AD on the driver amplifier board.
- j. Reconnect the wire, disconnected in part b of this step, to pin AD on the driver amplifier board.
- k. Reconnect the wire, described in part c of this step, to pin AB on the driver amplifier board.
  - I. Turn on the Type 520 power.

### 34. Adjust Chroma B-Y Gain

a

- a. Set the front-panel GAIN BAL control, R648, to its mechanical midrange position.
- b. CHECK—Type 520 test circle position; must be tangent to the inscribed circle on the vector graticule at the  $0^{\circ}$  and  $180^{\circ}$  points.
- c. ADJUST-B-Y GAIN control, R646 (see Fig. 6-6) so test circle is tangent to the inscribed circle on the vector graticule at the  $0^{\circ}$  and  $180^{\circ}$  points.

#### Front-panel controls:

<b>CH A, A</b> $\phi$ and FULL FIELD
75%
CAL .
•
<b>75</b> %
CAL
Υ
As desired
CAL
As desired
0
ON

Right recessed front-panel controls:

FIELD		1
SYNC		INT

# 35. Adjust Transient Response

- a. Apply a modulated staircase signal at 90% APL from the Type 140 comp video connector through a 75 ohm cable to the Type 520 CH A J1 connector.
- b. Connect a 75 ohm coaxial cable from the CH A J2 connector to the CH B J50 connector and a 75 ohm end-line termination to the CH B J51 connector.
- c. Connect a 10X probe from the test oscilloscope vertical input connector to TP680 (junction of R676 and R682) located on the Driver Amplifier board; see Fig. 6-6.
- d. Set the test oscilloscope for a vertical deflection factor of 50 mV/division, AC coupled, at a sweep rate of 5  $\mu$ s/division with internal triggering.
- e. CHECK—Test oscilloscope display; waveform should have a flat top with minimum aberrations (aberrations less than 1% in amplitude); see Fig. 6-18.
- f. ADJUST-L610 through L618 located on the luminance filter board (see Fig. 6-19) for a test oscilloscope waveform having a flat top with minimum aberrations.
  - g. Disconnect the 10X probe.
- h. CHECK—Type 520 display; waveform should have a flat top with minimum aberrations (aberrations less than 1% in amplitude); see Fig. 6-20.

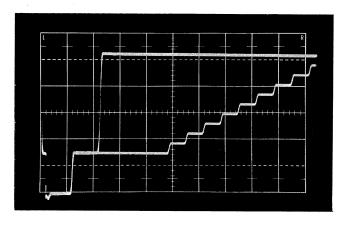


Fig. 6-18. Typical transient response of luminance filter as displayed on a test oscilloscope.

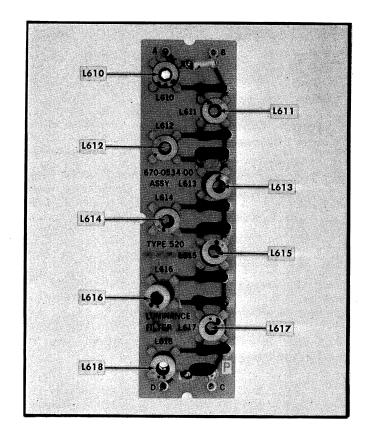


Fig. 6-19. Luminance filter board adjustment locations.

- i. ADJUST—VERT TRANS RESP, R849, C848, L838 and L858 located on the output amplifier board, see Fig. 6-8, for a waveform having a flat top with minimum aberrations; see Fig. 6-20.
  - j. Press the Signal Selector A CAL pushbutton.

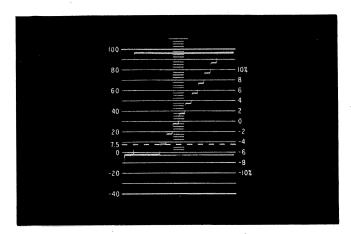
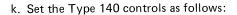


Fig. 6-20. Typical transient response of luminance filter and vertical amplifier together.



Mod Staircase	
0° Subcarrier	Down
Steps	Down
APL	80
Synchronization	
Burst	Down
Svnc	Down

- I. Turn off the Type 520 power. Disconnect the greengreen on gray coax center lead (below SN B200000, green on white wire) from pin AD on the driver amplifier board. Disconnect the blue-blue on gray coax center lead (below SN B200000, blue on white wire) from pin AB on the driver amplifier board; see Fig. 6-6.
- m. Connect a 75 ohm coaxial cable from the Type 140 comp video output connector to a BNC clip lead adapter. Connect the black lead to the Type 520 chassis and connect the red lead to the wires disconnected in part I of this step. Turn on the Type 520 power and press the Display Selector VECTOR pushbutton.
- n. CHECK—Type 520 display; should be similar to that shown in Fig. 6-21. The displayed vector should be located at 225°, have minimum overshoot (small spot size), and minimum loop amplitude (smallest loop opening).
- o. ADJUST—HORIZ GAIN R968, HORIZ TRANS RESP R969, C958, C968, L958 and L978 located on the output amplifier board; see Fig. 6-8, to position the vector display to 225°, and to obtain minimum loop amplitude and vector tip overshoot. R968 affects phase; the remaining adjustments affect transient response.
- p. Turn off the Type 520 and remove the clip lead adapter. Reconnect the wires to their respective pins on the driver amplifier board.

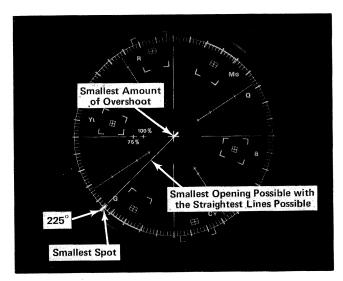


Fig. 6-21. Waveform areas to observe when adjusting horizontal amplifier transient response.

- q. Turn on the Type 520 power. Return all Type 140 switches to the up position.
- r. Apply the color bar signal from the Type 140 to the Type 520 CH A J1 connector via the 75 ohm coaxial cable.
- s. Check that the Display Selector VECTOR pushbutton is depressed. Align burst at  $180^{\circ}$  using the channel A PHASE control.
  - t. Press the Display Selector Q pushbutton.
- u. CHECK—Type 520 display; color bar waveform should have minimum aberrations on the leading front corner and a flat top.

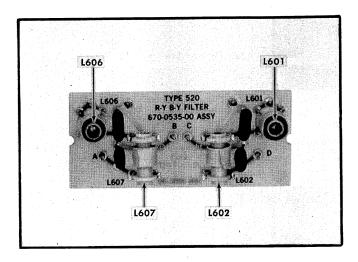


Fig. 6-22. R-Y, B-Y filter board adjustment locations.

filter board, see Fig. 6-22, for best leading edge and flat top on the displayed color bars.  w. Press the Display Selector I pushbutton.	Display Selector VECTOR pushbutton and slowly rotathe channel A PHASE control. Check that the overshoot the dots and the transient response between dots remain constant as the display is rotated 360°. Abnormal over
W. Tress the Display delector i pushbutton.	shoot indicates that the adjustments performed in this ste
x. CHECK—Type 520 display; color bars should have minimum aberrations on the leading front corner and a flat top.	are not optimum.
Lop.	
y. ADJUST-L601 and L602, see Fig. 6-22, for best leading edge and flat top on the displayed color bars.	aa. Disconnect the color bar signal, 75 ohm coaxid cable and 75 ohm end-line termination.
NC	DTES
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6-29

Front-panel controls:

B CAL and FULL FIELD Signal Selector **CHANNEL A** 100%-75%-MAX GAIN 75% GAIN CAL φ REF **BURST CHANNEL B** 100%-75%-MAX GAIN 75% GAIN CAL **Display Selector VECTOR** INTENSITY As desired

SCALE ILLUM
CALIBRATED PHASE

**LUMINANCE GAIN** 

POWER ON

Right recessed front-panel controls:

FIELD SYNC

1 INT

CAL

0

As desired

0

36. Adjust L272, L279; Feedback Components (for instruments SN B150100 and up); Input Phasing (for instruments SN B030000 to SN B150100)

- a. Connect a 10X probe from the test oscilloscope vertical input connector to TP275 on the subcarrier regenerator board; see Fig. 6-14.
- b. Set the test oscilloscope for a vertical deflection factor of 0.2 V/division, AC coupled, at a sweep rate of 0.1  $\mu$ s/division, with internal triggering.
- c. CHECK—Test oscilloscope display amplitude; should equal about 4 volts peak to peak.
- d. ADJUST-L272 and L279 (see Fig. 6-14) for maximum test oscilloscope display amplitude.
  - e. Disconnect the 10X probe.
- f. Press the Signal Selector CH A and A $\phi$  pushbuttons and cancel the B CAL pushbutton.
- g. Connect the 067-0565-00 calibration fixture to the CH A J1 connector. Connect a 75 ohm end-line termination to the CH A J2 connector.
- h. Apply the signal from the Type 140 subcarrier output connector through a 75 ohm coaxial cable and 75 ohm feed-thru termination to the 067-0565-00 calibration fixture subcarrier input connector.

- i. Connect the 10X probe, from the test oscilloscope vertical input connector, to the center conductor of the CH A J1 connector; see Fig. 6-5B.
- j. Set the test oscilloscope for a vertical deflection factor of 0.01 V/division, AC coupled, at a sweep rate of 0.5 ms/division with a free-running sweep.
- k. Set the 067-0565-00 calibration fixture 95%-100% switch to 95%. Adjust the calibration fixture subcarrier amplitude control so a signal amplitude of exactly 143 mV is displayed on the test oscilloscope.
  - I. Disconnect the 10X probe and test oscilloscope.
- m. Connect a 75 ohm coaxial cable between the Type 140 comp sync and the Type 520 EXT SYNC J120 connector. Connect a 75 ohm coaxial cable from the Type 520 EXT SYNC J121 connector to the vertical input of the test oscilloscope via a 75 ohm feed-thru termination.
- n. Set the test oscilloscope for a vertical deflection factor of 1 V/division, AC coupled, sweep rate 5  $\mu$ s/division with internal triggering.
- o. Adjust the test oscilloscope triggering controls to obtain a stable display.
- p. Connect the 067-0565-00 calibration fixture ramp input connector through a 75 ohm coaxial cable and BNC-to-clip lead adapter to the test oscilloscope sawtooth output connector. (Connect the red lead to the sawtooth output connector and the black lead to the oscilloscope ground.)
- q. Set the 067-0565-00 calibration fixture 95%-100% switch to 100%.
- r. Press the Display Selector Y pushbutton and set the SYNC switch to EXT.
- s. Adjust the 067-0565-00 calibration fixture ramp amplitude control for a sawtooth amplitude of exactly 140 IRE units as measured on the IRE graticule.
- t. Set the channel A 100%-75%-MAX GAIN switch to MAX GAIN and press the Display Selector DIFF PHASE pushbutton.

- u. Adjust the channel A PHASE control to bring the two traces together at the start of the display.
- v. CHECK—Type 520 display, deviation between the two traces must not be greater than 0.3° in the last 80% of the display. (Use the CALIBRATED PHASE dial to read the deviation between traces.)
- w. ADJUST-L272 and L279 (see Fig. 6-14) so the deviation between the traces is minimum. It is necessary to continually readjust the channel A PHASE control to keep the traces together as the adjustments are made.
- x. Move the 067-0565-00 calibration fixture from the CH A J1 connector to the CH B J50 connector. Move the 75 ohm end-line termination from the CH A J2 connector to the CH B J51 connector.
- y. Press the Signal Selector CH B pushbutton and cancel the CH A pushbutton. Set the channel B 100%-75%-MAX GAIN switch to MAX GAIN. Check that the Signal Selector A $\phi$  and FULL FIELD pushbuttons are depressed. Check that the Display Selector DIFF PHASE pushbutton is depressed.
- z. CHECK—Repeat parts u and v to check the channel B input phasing.
- aa. Disconnect the 067-0565-00 calibration fixture, test oscilloscope, 75 ohm end-line termination, four 75-ohm coaxial cables, two feed-thru terminations and the clip lead adapter.

### NOTE

Parts ab through aw of this step apply only to instruments SN B150100 and up. For instruments SN B030000 to B150100 proceed with part ax of this step.

- ab. Set the channel A and B 100%-75%-MAX GAIN switches to 75%. Press the Signal Selector CH A pushbutton and the Display Selector VECTOR pushbutton. Cancel the Signal Selector CH B pushbutton.
- ac. Connect a dual-input cable connector to the CH A J2 and CH B J50 connectors and apply a modulated staircase signal, through a 75 ohm coaxial cable and 75 ohm feed-thru termination, to the dual-input cable connector.
- ad. Connect a second cable from the Type 140 comp sync connector to the Type 520 EXT SYNC J120 connec-

- tor. Connect a 75 ohm end-line termination to the EXT SYNC J121 connector.
- ae. Adjust the channel A PHASE control so that the staircase vector coincides with the  $180^{\circ}$  reference line on the vector graticule.
- af. Set the channel A 100%-75%-MAX GAIN switch to MAX GAIN.
- ag. CHECK—Type 520 display; the vector dot should coincide with the inscribed graticule circle at 180°.
- ah. ADJUST—C434 located on the feedback board (see Fig. 6-23) until the staircase vector dot coincides with the inscribed graticule circle. Adjust C430 until the vector dot coincides with the 180° reference line on the vector graticule.
- ai. Set the channel A 100%-75%-MAX GAIN switch to 75%, then repeat parts ae through ah until interaction between C430 and C434 adjustments has been removed.
- aj. Press the Signal Selector CH B and B $\phi$  pushbuttons and cancel the CH A pushbutton.
- ak. Adjust the channel B PHASE control so that the staircase vector coincides with the  $180^{\circ}$  reference line on the vector graticule.
- al. Set the channel B 100%-75%-MAX GAIN switch to MAX GAIN.

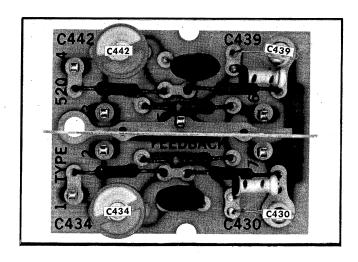


Fig. 6-23. Feedback board (SN B150100 and up) adjustment locations.

am. CHECK-Type 520 display; the vector dot should coincide with the inscribed graticule circle at  $180^{\circ}$ .

an. ADJUST-C442 (see Fig. 6-23) until the vector dot coincides with the inscribed graticule circle. Adjust C439 until the vector spot coincides with the  $180^{\circ}$  reference line on the vector graticule.

ao. Set the channel B 100%-75%-MAX GAIN switch to 75% and repeat parts ak through an until interaction between C439 and C442 adjustments has been removed.

ap. Set the Type 140 video switch up to obtain a color bar output signal and press the Signal Selector CH A and  $A\phi/B\phi$  ALT pushbuttons. (The other pushbuttons remain as they are.)

aq. Set Channel B input phasing capacitor, C411 (see Fig. 6-24), to its minimum capacitance position; that is, so the silvered half of the rotor section is toward the Signal Selector switch.

ar. CHECK—Type 520 display vector lengths. Corresponding vectors of channel A and channel B displays must be exactly the same length. (Use the channel A and B PHASE controls to superimpose the vectors.)

as. ADJUST—C52 (see Fig. 6-10) so the channel B vector is exactly the same length as the channel A vector. Do not disturb the setting of C2.

### NOTE

Initial settings for C2 and C52 are given in step 15.

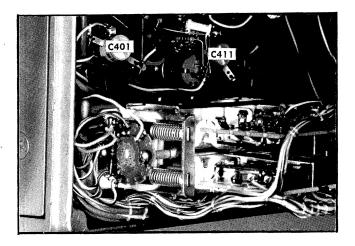


Fig. 6-24. Rear view of front-panel area below the Signal Selector switch showing location of C401 and C411 adjustments.

at. Depress the Signal Selector  $A\phi$  pushbutton. (The other pushbuttons remain as they are.)

au. CHECK-Type 520 channel A and B vector phase difference; should not exceed  $1^{\circ}$ .

av. ADJUST—C401 (see Fig. 6-24) to superimpose the channel A vector on the channel B vector. If C401 has insufficient range to complete the adjustment, adjust C411 enough to superimpose the channel A vector on the channel B vector.

aw. Repeat parts as through av until interaction between C52 and C401 has been removed.

#### NOTE

Parts ax through bg apply to instruments SN B030000 to SN B150100 only.

ax. Apply a color bar signal, via a 75 ohm coaxial cable to the BNC female connector on the dual-input cable connector.

ay. Connect the dual-input cable connector to CH A J2 connector and CH B J50 connector.

az. Connect a 75 ohm end-line termination to the CH A J1 connector and the CH B J50 connector.

ba. Set the Channel A 100%-75%-MAX GAIN switch to 75%, depress the Display Selector VECTOR pushbutton, and set the SYNC switch to INT. Other pushbuttons remain as they are.

bb. Set the CH A input phasing capacitor, C88 (see Fig. 6-10), to its minimum capacitance position (silvered half of the rotor to the right of the arrow when the arrow is pointing away from you).

bc. CHECK—Type 520 display vector lengths. Corresponding vectors of channel A and channel B displays must be exactly the same length.

bd. ADJUST—C52, see Fig. 6-10, so that channel B vectors are exactly the same length as channel A vectors.

be. CHECK-Type 520 channel A and B vector phase difference should not exceed 1°.

- bf. ADJUST—C98, see Fig. 6-10, to superimpose the channel B vectors upon the channel A vectors. If necessary, adjust C88 after C98 has run out of range to superimpose the channel A and channel B vectors upon each other (within 1° or less).
- bg. Repeat parts bd through bf until interaction of adjustments C52 and C98 has been removed.
- bh. Leave the color bar signal connected to CH A J2 and CH B J50 connectors.

### 37. Adjust Calibrated Phase Control

- a. Cancel the Signal Selector CH B pushbutton. Check that the following pushbuttons are depressed: Signal Selector CH A, A $\phi$  and FULL FIELD; Display Selector VECTOR pushbutton. Check that a color bar signal is applied to the Type 520 CH A J2 and CH B J50 connectors.
- b. Set the channel A variable GAIN control so that one of the displayed vectors overlays the graticule circle.
  - c. Set the CALIBRATED PHASE dial to  $-15^{\circ}$ .
- d. Using the channel A PHASE control, set the Type 520 displayed vector to an arbitrarily established  $0^{\circ}$  point on the vector graticule.
  - e. Set the CALIBRATED PHASE dial to +15°.
- f. CHECK-Type 520 displayed vector should have rotated  $30^{\circ}$ ,  $\pm 4^{\circ}$  clockwise.
- g. Adjust the channel A PHASE control to align a dot with an arbitrarily established  $0^{\circ}$  point on the vector graticule.
- h. Rotate the CALIBRATED PHASE control from +14° toward -14° in increments of 2°.
- i. CHECK—Type 520 display dot which corresponds to the dial reading being checked. The dial error over any  $2^{\circ}$  increment of the dial must be  $2^{\circ}$ ,  $\pm 0.2^{\circ}$  of the previous dial setting noted when the dot was aligned with the established  $0^{\circ}$  point.
  - j. Set the CALIBRATED PHASE dial to +14°.

- k. Adjust the channel A PHASE control to align a dot with an arbitrarily established  $0^{\circ}$  point on the vector graticule.
- I. Rotate the CALIBRATED PHASE control from +14° toward -14° in increments of 2°.
- m. CHECK—Type 520 display dot. The dial error at the  $\pm 12^\circ$  and  $\pm 10^\circ$  dial settings must be  $2^\circ$ ,  $\pm 0.2^\circ$ , and  $2^\circ$ ,  $\pm 0.4^\circ$  respectively of the correct dial setting, while the dial error at the other dial setting must be  $2^\circ$ ,  $\pm 0.5^\circ$  of the correct dial setting.

### NOTE

Parts n through x comprise the adjustment procedure.

- n. Preset L331 to midrange and R335 clockwise (see Fig. 6-25).
- o. Turn the CALIBRATED PHASE dial counterclockwise to the STOP setting.
- $\ensuremath{^{\circ}}$  p. ADJUST-L332 down until maximum distortion of the dots occurs.
- q. Set the CALIBRATED PHASE dial to 0 and the A PHASE control to position one of the dots to the  $0^{\circ}$  graticule mark.
  - r. Rotate the CALIBRATED PHASE dial to +14°.

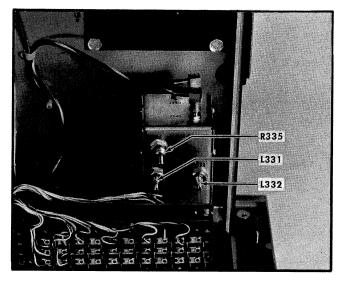


Fig. 6-25. Rear view of front-panel area below the Display Selector switch showing location of the precision phase shifter adjustments.

- s. ADJUST-R335 to position the dot to the  $+14^{\circ}$  graticule mark.
- t. Set the CALIBRATED PHASE dial to 0 and the A PHASE control to position the dot to the  $0^{\circ}$  graticule mark.
  - u. Set the CALIBRATED PHASE dial to  $-14^{\circ}$ .
- v. ADJUST-L331 to double the dot error noted from the  $-14^{\circ}$  graticule mark (if the dot is  $+1^{\circ}$  from  $-14^{\circ}$ , increase the error to  $+2^{\circ}$  with L331).
- w. Set the CALIBRATED PHASE dial to 0 and the A PHASE control to position the dot to the  $0^{\circ}$  graticule mark.
- x. Repeat parts q through w as necessary to minimize interaction, then check calibrated phase range and accuracy by repeating parts c through m.
- y. If continuing on to step 38, disconnect the dual input

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### Front-panel controls:

**POWER** 

Signal Selector CH A,  $A\phi$  and **FULL FIELD CHANNEL A** 100%-75%-MAX GAIN 75% GAIN CAL  $\phi$  REF BURST **CHANNEL B** 100%-75%-MAX GAIN 75% GAIN CAL Display Selector Υ INTENSITY As desired **LUMINANCE GAIN** CAL SCALE ILLUM As desired **CALIBRATED PHASE** 

Right recessed front-panel controls:

FIELD 1 SYNC INT

# 38. Adjust DIFF GAIN Mode Compensation

ON

- a. Apply a modulated staircase signal to the CH A J1 connector via a 75 ohm coaxial cable.
- b. Connect a 75 ohm end-line termination to the CH 2 J2 connector.
- c. Adjust the HORIZ POSITION control to position the display so all steps of the staircase signal can be seen.
- d. Using the VERT POSITION control, superimpose the base line of the staircase upon the —40 IRE unit line on the IRE graticule.
- e. Adjust the channel A GAIN control so the top of the last step is superimposed upon the +100 IRE unit line on the IRE graticule; see Fig. 6-26A.
- f. Press the Display Selector DIFF GAIN pushbutton and set the channel A 100%-75%-MAX GAIN switch to MAX GAIN. Do not touch the VERT POSITION control again during this step.
- g. CHECK—Type 520 display; should have the information part of the waveform displayed at the 30 IRE unit line on the IRE graticule; see Fig. 6-26B.
- h. ADJUST-DIFF GAIN POS BAL control, R498 (see Fig. 6-12) until the information part of the displayed wave-

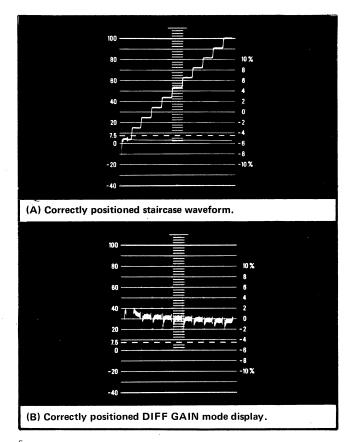


Fig. 6-26. Typical displays obtained when performing step 38.

form is superimposed upon the 30 IRE unit line on the IRE graticule; see Fig. 6-26B.

# 39. Check Input Amplitude Range

- a. Press the Display Selector LINE SWEEP pushbutton.
- b. Set the Type 140 video switch up to obtain a color bar output signal.
- c. Connect a 10X probe, from the test oscilloscope vertical input connector, to the center conductor of the CH A J1 connector; see Fig. 6-5B.
- d. Set the test oscilloscope for a vertical deflection factor of 0.01 V/division, AC coupled, at a sweep rate of 10  $\mu$ s/division with internal triggering.
- e. Set the sync pulse amplitude, of the color bar video signal, to exactly 286 mV (overall signal amplitude 1 volt) as measured on the test oscilloscope.
- f. Rotate the channel A PHASE control to obtain maximum positive-going burst amplitude; see Fig. 6-27.

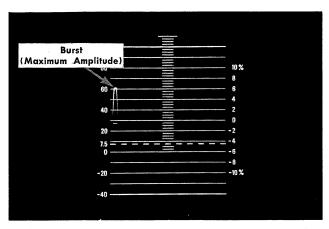


Fig. 6-27. Correct Type 520 color bar display for adjusting burst flag timing.

- g. Check that the intensified rising and falling portions of the burst part of the Type 520 display are equal. It may be necessary to reduce the display intensity so the intensified portion may be seen. If the position of the intensified portion is not correct, adjust the front-panel BURST FLAG TIMING control, R1158, until the intensified rising and falling portions of the burst are equal.
- h. Reduce the sync amplitude of the color bar video signal to exactly 200 mV (overall signal amplitude 0.7 volt) as measured on the test oscilloscope.
- i. Set the Type 520 SYNC switch to EXT for about 15 seconds, then return it to its INT position.
  - j. CHECK-Type 520 display, should be stable.
- k. Increase the sync pulse amplitude of the color bar video signal to exactly 400 mV (overall signal amplitude 1.4 volts) as measured on the test oscilloscope.
- I. Set the Type 520 SYNC switch to EXT for about 15 seconds, then return it to its INT position.
  - m. CHECK-Type 520 display, should be stable.
- n. Disconnect the video signal source, 75 ohm coaxial cable and 10X probe. Leave the termination connected to the CH A J2 connector.

# 40. Check Differential Gain Deflection Factor and Differential Gain

a. Set the SYNC switch to EXT.

- b. Connect a 067-0565-00 calibration fixture to the CH A J1 connector. Check that a 75 ohm end-line termination is connected to the CH A J2 connector.
- c. Connect a 75 ohm coaxial cable between the 067-0565-00 calibration fixture subcarrier input connector and the Type 140 subcarrier connector.
- d. Connect a 10X probe from the test oscilloscope vertical input connector to the center conductor of the CH A J1 connector; see Fig. 6-5B.
- e. Connect a 75 ohm coaxial cable between the Type 140 composite sync connector and the Type 520 EXT SYNC J120 connector.
- f. Connect a 75 ohm coaxial cable from the Type 520 EXT SYNC J121 connector to the vertical input of the test oscilloscope via a 75 ohm feed-thru termination.
- g. Set the test oscilloscope for a vertical deflection factor of 1 V/division, AC coupled, at a sweep rate of 5  $\mu$ s/division with internal triggering.
- h. Adjust the test oscilloscope triggering controls to obtain a stable display.
- i. Connect the 067-0565-00 calibration fixture ramp input connector through a 75 ohm coaxial cable and BNC-to-clip lead adapter to the test oscilloscope sawtooth output connector. (Connect the red lead to the sawtooth output connector and the black lead to the oscilloscope ground.)
- j. Set the 067-0565-00 calibration factor 95%-100%-MAX GAIN switch to 100%, then adjust the ramp amplitude control for a sawtooth amplitude of exactly 140 IRE units measured on the IRE graticule.
- k. Set the channel A 100%-75%-MAX GAIN switch to MAX GAIN and press the Display Selector VECTOR push-button.
- l. Adjust the calibration fixture subcarrier amplitude control so that the vector dot coincides with the inscribed graticule circle. Rotate the Type 520 A PHASE control to align the dot to  $180^\circ$ .
- m. Press the Display Selector DIFF GAIN pushbutton and adjust the VERT POSITION control to position the display to a convenient point.

- n. CHECK—Deviation of the Type 520; horizontal display must not exceed  $\pm 5$  IRE units from the horizontal lines of the IRE graticule throughout the last 90% of its length. This includes both slope and aberrations.
- o. Set the 067-0565-00 calibration fixture 95%-100%-MAX GAIN switch to 95%.
- p. CHECK—Position of the Type 520 display; should be 25 IRE units  $\pm 1.25$  IRE units below its position in part n of this step.
- q. Return the 067-0565-00 calibration fixture 95%-100% switch to 100%. If requirements cannot be met, select R765 (see Fig. 6-8) for proper differential gain deflection factor as described in part p.

- r. Move the 067-0565-00 calibration fixture from the CH A J1 connector to the CH B J50 connector. Move the 75 ohm termination from the CH A J2 connector to the CH B J51 connector.
  - s. Press the Signal Selector CH B pushbutton.
- t. Using parts k through n as a guide, check the differential gain for channel B.
- u. If continuing on to step 41, leave the 75 ohm termination connected to CH A J2 connector and remove all other connections to the Type 520.

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Front-panel controls:

Signal Selector **CH A**,  $A\phi$  and **FULL FIELD** 

. CHANNEL A

100%-75%-MAX GAIN 75% GAIN CAL  $\phi$  REF **BURST** 

**CHANNEL B** 

100%-75%-MAX GAIN 75% GAIN CAL

**VECTOR Display Selector** INTENSITY As desired **LUMINANCE GAIN** CAL As desired SCALE ILLUM 0

CALIBRATED PHASE **POWER** 

ON

Right recessed front-panel controls:

**FIELD** SYNC

# 41. Check 100%-75%-MAX GAIN Switch Gain (For instruments SN B150100 and up)

INT

- a. Apply a 75% amplitude, 7.5% setup, color bar signal, from the Type 140 comp video connector, through a 75 ohm coaxial cable to the Type 520 CH A J1 connector.
- b. Connect a 75 ohm coaxial cable from the CH A J2 connector to the CH B J50 connector and a 75 ohm endline termination to the CH B J51 connector.
- c. Check that the Signal Selector CH B pushbutton is cancelled, then set the channel A PHASE control so that the burst vector is at 180°.
- d. Set the channel A 100%-75%-MAX GAIN switch to 100% and the Type 140 color bar amplitude switch to 100%.
- e. CHECK-Type 520 display color vectors must be in their boxes.
- f. Cancel the Signal Selector CH A pushbutton and set the channel A 100%-75%-MAX GAIN switch to 75%.
- g. Press the Signal Selector CH B pushbutton. Set the channel A PHASE control so that the burst vector is at 180°.
- h. Set the channel B 100%-75%-MAX GAIN switch to 100%.

- i. CHECK-Type 520 display color vectors must be in their boxes.
- i. Set the channel B 100%-75%-MAX GAIN switch to 75%.
- k. Cancel the Signal Selector CH B pushbutton. (The other pushbuttons remain as they are.)

# 41A. Check 100%-75%-MAX GAIN Switch Gain (For instruments below SN B150100)

- a. Press both the Signal Selector A CAL and the Display Selector Y pushbuttons.
- b. CHECK-Type 520 display amplitude should equal 140 IRE units. If it is not, readjust the Type 520 channel A GAIN control to obtain the correct display.
- c. Set the channel A 100%-75%-MAX GAIN switch to 100%.
- d. CHECK-Type 520 display amplitude; 105 IRE units, ±2,8 IRE units.
- e. Cancel the Signal Selector A CAL pushbutton and set the channel A 100%-75%-MAX GAIN switch to 75%.
  - f. Press Signal Selector B CAL pushbutton.
- g. CHECK-Type 520 display amplitude; exactly 140 IRE units. If it is not, readjust the Type 520 channel B GAIN control to obtain the correct display.
- h. Set the channel B 100%-75%-MAX GAIN switch to 100%.
- i. CHECK-Type 520 display amplitude, 105 IRE units, ±2.8 IRE units.
- j. Set the channel B 100%-75%-MAX GAIN switch to 75%.
- k. Connect a 10X probe, from the test oscilloscope vertical input connector, to TP450 (junction of R452 and Q450 emitter) on the demodulator board; see Fig. 6-12.
- I. Set the test oscilloscope for a vertical deflection factor of 0.05 V/division, AC coupled, at a sweep rate of 0.5 ms/division with internal triggering.

- m. Adjust the test oscilloscope vertical deflection factor so that exactly one major division of display is observed on the test oscilloscope.
- n. Set the channel B 100%-75%-MAX GAIN switch to MAX GAIN.
- o. CHECK—Test oscilloscope display amplitude; 3.5 major divisions, ±5%.
- p. Cancel the Signal Selector B CAL pushbutton and set the channel B 100%-75%-MAX GAIN switch to 75%.
  - q. Depress the Signal Selector A CAL pushbutton.
- r. Adjust the test oscilloscope vertical deflection factor so that exactly one major division of display is observed on the test oscilloscope.
- s. Set the channel A 100%-75%-MAX GAIN switch to MAX GAIN.
- t. CHECK—Test oscilloscope display amplitude; 3.5 major divisions, ±5%.
  - u. Set the Type 520 controls as follows:

Signal Selector

 $A\phi$ , FULL FIELD

CH A

100%-75%-MAX GAIN

75%

Channel A and B GAIN

CAL

Display Selector

VECTOR

v. Disconnect the test oscilloscope and the 10X probe.

# 42. Check Color Bar Decoding Accuracy

- a. Check that the Type 140 75% amplitude, 7.5% setup, and color bar signal is applied to the Type 520 as described in parts a through c of step 41.
- b. Press the Signal Selector CH A pushbutton. Check that the Signal Selector  $A\phi$  and FULL FIELD pushbuttons

and the Display Selector VECTOR pushbutton are depressed.

- c. Using the A PHASE control, position the  $\rm Y_L$  vector dot into the graticule  $\rm Y_L$  inner box.
- d. Depress the Display Selector R, G, and B push-buttons in succession.
- e. CHECK—The color bars should extend from 7.5% setup to 77 IRE units, within  $\pm 3\%$ , when the blanking level is aligned with the 0 IRE unit graticule line.

### 43. Check Time Sharing Switching Rate

- a. Press the Signal Selector B $\phi$  pushbutton and the Display Selector VECTOR pushbutton. Check that the remaining controls, except the A $\phi$  pushbutton, are set to the same positions as those given in the list that precedes step 41.
- b. Set the Type 140 controls for a convergence crosshatch pattern (all switches in the up position).
- c. Change the interconnections between the Type 140 and Type 520 so that the color bar signal is applied to the CH B J50 connector and the convergence crosshatch pattern is applied to the CH A J1 connector. Connect a 75 ohm end-line termination to the CH A J2 connector. Check that a termination is connected to the CH B J51 connector.
- d. Connect a 10X probe from the test oscilloscope vertical input connector to TP776 (junction of R705 and R715) on the output amplifier board; see Fig. 6-8.
- e. Set the test oscilloscope for a vertical deflection factor of 0.05 V/division, AC coupled, at a sweep rate of 20  $\mu$ s/division with internal triggering.
- f. CHECK—Test oscilloscope display should be two complete channel A signals followed by two complete channel B signals, then two channel A signals followed by two channel B signals.
- g. Disconnect the video signal source, test oscilloscope, the two 75 ohm coaxial cables, the two 75 ohm end-line terminations and the 10X probe.

Front-panel controls:

Signal Selector CH A,  $\mathbf{A}\phi$  and **FULL FIELD CHANNEL A** 100%-75%-MAX GAIN 75% GAIN CAL  $\phi$  REF **BURST CHANNEL B** 100%-75%-MAX GAIN 75% GAIN CAL **VECTOR** Display Selector INTENSITY As desired **LUMINANCE GAIN** CAL SCALE ILLUM As desired CALIBRATED PHASE POWER ON

Right recessed front-panel controls:

FIELD 1 SYNC INT

# 44. (Optional Step) Check Subcarrier Regenerator Pull-In Range and Time

#### NOTE

In general, if the Type 520 subcarrier regenerator (SCR) locks in on the color bar signal after the signal is turned off or disconnected for a period of time, the SCR is operating properly. A more complete check can be made if the following test fixture (item 9) is used to offset the Type 140 subcarrier frequency ±5 Hz as described in the procedure that follows.

Subcarrier Frequency Offset test fixture used to change the Type 140 subcarrier frequency  $\pm 15$  Hz. Construct the test fixture according to the information given in Fig. 6-1A. Connect the test fixture to the Type 140 subcarrier board. Connect the Type 140 subcarrier signal through a 75 ohm coaxial cable and a 75 ohm feed-thru termination to an accurate (at least  $\pm 1$  Hz) frequency counter. Set the test fixture switch S1 to +15 Hz and adjust R1 until the frequency counter indicates 3.579560 MHz. Mark the position of R1 and leave the control set at this point. Set S1 to -15 Hz and adjust R2 until the frequency counter indicates 3.579530 MHz. Mark the position of R2 and leave the control at this point. The test fixture is now calibrated to offset this Type 140 subcarrier frequency  $\pm 15$  Hz. Disconnect the frequency counter.

- a. Apply a color bar signal from the Type 140 comp video connector through a 75 ohm coaxial cable to the Type 520 CH A J1 connector.
- b. Check that a 75 ohm end-line termination is connected to the CH A J2 connector.

- c. Connect the test fixture to the Type 140 subcarrier board and set the test fixture switch S1 to the Normal position.
- d. CHECK—Type 520 display, vector should be stable (not rotating).
  - e. Set the test fixture switch S1 to +15 Hz.
- f. CHECK—Time that the Type 520 takes to stabilize vector display; fifteen seconds or less.
- g. Set the test fixture switch S1 to Normal and allow the display to stabilize.
  - h. Set the test fixture switch S1 to -15 Hz.
- i. CHECK—Time that the Type 520 takes to stabilize to a stable vector display; fifteen seconds or less.
- j. Set the test fixture switch S1 to Normal. Using the Type 520 A PHASE control, position the burst vector to  $180^{\circ}$ 
  - k. Set the test fixture switch S1 to +15 Hz.
- I. CHECK—Type 520 burst vector position; should be within 0.6° of the 180° point on the vector graticule. The CALIBRATED PHASE control can be used to measure the amount of burst vector shift.
  - m. Set the test fixture switch S1 to -15 Hz.
  - n. CHECK-Repeat part I of this step.
- o. Disconnect the test fixture. Leave the color bar signal connected to the Type 520.

### 45. Check Vertical Positioning Range

- a. Check that a color bar signal is applied from the Type 140 comp video connector through a 75 ohm coaxial cable to the Type 520 CH A J1 connector.
- b. Check that a 75 ohm end-line termination is connected to the CH A J2 connector.

- c. Press the Display Selector Y pushbutton.
- d. Check that the Signal Selector CH A, A $\phi$  and FULL FIELD pushbuttons are depressed.
  - e. Turn the VERT POSITION control fully clockwise.
- f. CHECK—Type 520 display, blanking level must be located at least 45 IRE units above the -40 IRE unit graticule line on the IRE graticule.
- g. Turn the VERT POSITION control fully counterclockwise.
- h. CHECK—Type 520 display; blanking level must be located at least 10 IRE units below the -40 IRE unit graticule line of the IRE graticule.
  - i. Press the Display Selector R pushbutton.
- j. CHECK—Position range, by repeating parts e through h.
  - k. Press the Display Selector G pushbutton.
- I. CHECK—Position range by repeating parts ethrough h.
  - m. Press the Display Selector B pushbutton.
- n. CHECK—Position range by repeating parts e through h.

### 46. Check Horizontal Positioning Range

- a. Press the Display Selector Y pushbutton and turn the HORIZ POSITION control fully clockwise.
- b. CHECK—Type 520 display position; not more than 3 mm of the display must be to the left of the center of the IRE graticule. (The display may appear entirely to the right of center.)
- c. Turn the HORIZ POSITION control fully counter-clockwise.
- d. CHECK-Type 520 display position; not more than 3 mm of the display must be to the right of the center of the

IRE graticule. (The display may appear entirely to the left of center.)

# 47. Check Vertical and Horizontal Position Clamp Range

- a. Press the Display Selector VECTOR pushbutton. Cancel the Signal Selector CH A pushbutton.
- b. Adjust the VERT and HORIZ POSITION CLAMP controls to position the spot to the center of the vector graticule.
- c. Rotate the VERT POSITION CLAMP control fully clockwise.
- d. CHECK—Type 520 spot position; must have moved up at least 2.5 IRE units from its initial position established in part b of this step. Use the IRE graticule to estimate the distance the spot moved.
- e. Rotate the VERT POSITION CLAMP control fully counterclockwise.
- f. CHECK—Type 520 spot position; must have moved down at least 2.5 IRE units from the initial position established in part b of this step. Use the IRE graticule to estimate the distance the spot moved.
- g. CHECK—Type 520 spot positioning must have a total positioning range, as noted in parts d and f, of 20 IRE units.
- h. Rotate the HORIZ POSITION CLAMP control fully clockwise.
- i. CHECK—Type 520 spot position; must have moved right at least 2.5 IRE units from the initial position established in part b of this step.
- j. Rotate the HORIZ POSITION CLAMP control fully counterclockwise.
- k. CHECK—Type 520 spot position; must have moved left at least 2.5 IRE units from the initial position established in part b.
- I. CHECK—Total Type 520 spot positioning range as noted in parts i and k, must equal or exceed 20 IRE units.

m. Readjust the VERT and HORIZ POSITION CLAMP controls to position the spot to the center of the vector graticule.

# 48. Check Channel A and B Gain Control Range

- a. Press the Signal Selector CH A and Display Selector Y pushbuttons.
- b. Set the Type 140 video switch down to obtain a modulated staircase output signal.
- c. Move the 75 ohm end-line termination from the CH A J2 connector to the CH B J51 connector. Connect a 75 ohm coaxial cable from the CH A J2 connector to the CH B J50 connector.
- d. Connect a 10X probe from the test oscilloscope vertical input connector to TP450 on the demodulator board; see Fig. 6-12.
- e. Set the test oscilloscope for a vertical deflection factor of 20 mV/division, AC coupled, at a sweep rate of 0.1 ms/division with free-running sweep.
- f. Adjust the test oscilloscope vertical deflection factor for a display of exactly 3 major divisions on the test oscilloscope.
- g. Rotate the channel A GAIN control throughout its range.
- h. CHECK—Test oscilloscope display amplitude must vary from 6 major divisions or more to 1.2 divisions or less.
- i. Return the channel A GAIN control to its CAL position. Cancel the Signal Selector CH A pushbutton and press the CH B and  ${\rm B}\phi$  pushbuttons.
- j. Adjust the test oscilloscope vertical deflection factor for a display of exactly 3 major divisions on the test oscilloscope.

- k. Rotate the channel B GAIN control throughout its range.
- I. CHECK—Test oscilloscope display amplitude; must vary from 6 major divisions or more to 1.2 divisions or less.
- m. Return the channel B GAIN control to CAL position. Disconnect the video signal source, the test oscilloscope, the two 75 ohm coaxial cables, 75 ohm end-line termination, and the 10X probe.

# 49. Check Luminance Gain Range

- a. Cancel the Signal Selector CH B pushbutton and depress the CH A and  $A\phi$  pushbuttons.
- b. Apply a modulated staircase signal via a 75 ohm coaxial cable to the Type 520 CH A J1 connector.
- c. Connect a 75 ohm end-line termination to CH A J2 connector.
- d. Connect a 10X probe from the test oscilloscope vertical input connector to TP776 on the output amplifier board; see Fig. 6-8.
- e. Set the test oscilloscope for a vertical deflection factor of 0.1 V/division, AC coupled, at a sweep rate of 0.1 ms/division with a free-running sweep.
- f. Adjust the test oscilloscope vertical deflection factor for a display of exactly 2 major divisions on the test oscilloscope.
- g. Rotate the LUMINANCE GAIN control out of its CAL detent position.
- h. CHECK—Test oscilloscope display amplitude; must vary from 2.8 major divisions to 1.4 major divisions.
- Return the LUMINANCE GAIN control to its CAL position.

### Front-panel controls:

Signal Selector	B Cal and FULL FIELD
100%-75%-MAX GAIN	75%
GAIN	CAL
$\phi$ REF	EXT
CHANNELB	
100%-75%-MAX GAIN	75%
GAIN	CAL
Display Selector	VECTOR
INTENSITY	As desired
LUMINANCE GAIN	CAL
SCALE ILLUM	As desired
CALIBRATED PHASE	0
POWER	ON

Right recessed front-panel controls:

FIELD	1
SYNC	INT

# 50. Check External Phase Reference Input Range

- a. Apply a 2 volt peak to peak subcarrier signal from the Type 140 subcarrier output connector, via a variable attenuator and a 75 ohm coaxial cable, to the Type 520 EXT CW  $\phi$  REF J310 connector.
- b. Connect a 10X probe from the test oscilloscope vertical input connector to the center conductor of the EXT CW  $\phi$  REF J310 connector; see Fig. 6-28.
- c. Set the test oscilloscope for a vertical deflection factor of 0.05 V/division, AC coupled, at a sweep rate of 0.2  $\mu$ s/division with internal triggering.

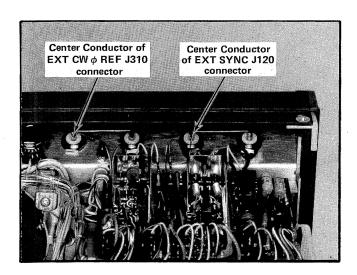


Fig. 6-28. Location of step 50 test points.

- d. Adjust the peak-to-peak output amplitude of the 3.58 MHz CW video signal for a test oscilloscope display of exactly 4 major divisions.
- e. Vary the 3.58 MHz CW video signal amplitude between 1.5 volt and 2.5 volts peak-to-peak, using the test oscilloscope to measure the signal amplitude.
- f. CHECK—Type 520 test circle display must not change in size or shape as the 3.58 MHz signal amplitude is varied.
  - g. Disconnect the signal source and 10X probe.

# 51. Check External Horizontal Sync Range

- a. Press the Signal Selector CH B and B $\phi$  pushbuttons.
- b. Set the  $\phi$  REF switch to BURST and press the Display Selector LINE SWEEP pushbutton.
  - c. Set the SYNC switch to EXT.
- d. Apply a modulated staircase signal via a 75 ohm co-axial cable to the Type 520 CH B J50 connector.
- e. Connect a 75 ohm end-line termination to the CH B  ${\sf J51}$  connector.
- f. Apply a 4 volt peak-to-peak composite sync signal via a variable attenuator and a 75 ohm coaxial cable to the EXT SYNC J120 connector.
- g. Connect a 10X probe from the test oscilloscope vertical input connector to the center conductor of the EXT SYNC J120 connector (R12 if nominal 1 volt sync signal is being used); see Fig. 6-28).
- h. Set the test oscilloscope for a vertical deflection factor of 0.2 V/division, (0.05 V/division), AC coupled, at a sweep rate of 20  $\mu s/division$  with internal triggering.
- i. Adjust the peak-to-peak output amplitude of the sync video signal for a test oscilloscope display of exactly 2 major divisions in amplitude.
- j. Adjust the BURST FLAG TIMING control for the proper Type 520 display; refer to step 23 of this procedure.

- k. Vary the sync video signal amplitude between 3.5 volts and 7.5 volts peak-to-peak, using the test oscilloscope to measure the signal amplitude. Interrupt the sync video signal by momentarily setting the SYNC switch to INT before making the check at a particular sync video signal amplitude.
- I. CHECK—A stable display must be obtained whenever the SYNC switch is set to its EXT position as part k of this step is performed.
- m. Disconnect the video signal source, variable attenuator, test oscilloscope, the two 75 ohm coaxial cables, the 75 ohm end-line termination, and the 10X probe.

#### 52. Check Instrument Return Loss

A differential amplifier required for this step.

- a. Connect the 015-0149-00 calibration fixture to the vertical input connectors of the test oscilloscope.
- b. Apply a 5 MHz sine wave signal, approximately 1 volt in amplitude, from a wide bandwidth constant amplitude sinewave generator via a 50 ohm coaxial cable and a 50 ohm to 75 ohm minimum loss attenuator to the signal input connector on the 015-0149-00 calibration fixture.
- c. Connect the matched 75 ohm terminations to the end of each coaxial cable of the 015-0149-00 calibration fixture.
- d. Set the test oscilloscope for a vertical deflection factor of 0.2 V/division (both input channels set for A-B operation) with a free running sweep.
- e. Remove one matched 75 ohm termination and adjust the constant amplitude sinewave generator for a  $0.5\ V$ ,  $5\ MHz$  output sinewave signal as observed on the test oscilloscope, then replace the matched  $75\ ohm$  termination.
- f. Set the test oscilloscope for a vertical deflection factor of 1 mV/division, both input channels AC coupled, and set for A-B operation at a sweep rate of 20  $\mu$ s/division with a free-running sweep.
- g. Vary the constant amplitude sinewave generator frequency from 25 Hz to 5 MHz.
- h. CHECK—Test oscilloscope display amplitude should be 1 mV or less at any frequency between 25 Hz and 5 MHz.

- i. Disconnect a 75 ohm termination from the end of the measuring cable. Attach the measuring cable to the Type 520 CH A J1 connector and the 75 ohm termination just removed to the CH A J2 connector.
- j. Vary the constant amplitude sinewave generator frequency from 25 Hz to 5 MHz.
- k. Press the Type 520 Signal Selector CH A and then the A CAL pushbuttons.
- I. CHECK—Test oscilloscope display amplitude should not exceed 2.5 mV minus the amplitude noted in part h for any frequency from 25 Hz to 5 MHz.
- m. Disconnect the measuring cable and adapter from the Type 520 CH A J1 connector and connect it to the CH B J50 connector. Disconnect the 75 ohm termination from the CH A J2 connector and connect it to the CH B J51 connector.
- n. Vary the constant amplitude sinewave generator frequency from 25 Hz to 5 MHz.
- o. Press the Type 520 Signal Selector CH B and then the B CAL pushbuttons.
- p. CHECK—Test oscilloscope display amplitude; should never be more than 2.5 mV minus the signal amplitude noted in part h at any frequency from 25 Hz to 5 MHz.
- q. Disconnect the measuring cable from the Type 520 CH B J50 connector and connect it to the EXT CW  $\phi$  REF J310 connector. Disconnect the 75 ohm termination from the CH B J51 connector and connect it to the EXT CW  $\phi$  REF J311 connector.
- r. Vary the constant amplitude sinewave generator frequency from 25 Hz to 5 MHz.
- s. Switch the Type 520  $\phi$  REF switch between its BURST and EXT positions.
- t. CHECK—Test oscilloscope display amplitude; should never be more than  $2.5\ \text{mV}$  minus the signal amplitude noted in part h.
- u. Disconnect the measuring cable from the Type 520 EXT CW  $\phi$  REF J310 connector and connect it to the EXT

SYNC J120 connector. Disconnect the 75 ohm termination from the EXT CW  $\phi$  REF J311 connector and connect it to the EXT SYNC J121 connector.

- v. Vary the constant amplitude sinewave generator frequency from 25 Hz to 5 MHz.
- $\ensuremath{\text{w}}.$  Switch the Type 520 SYNC switch between its INT and EXT positions.
- x. CHECK—Test oscilloscope display amplitude; should never be more than 2.5 mV (4 volt connection) or 5 mV (1 volt connection) minus the signal amplitude noted in part h at any frequency from 25 Hz to 5 MHz.
- y. Disconnect the 015-0149-00 calibration fixture, 75 ohm termination, wide bandwidth sinewave generator, test oscilloscope, 50 ohm coaxial cable and 50 ohm to 75 ohm minimum loss attenuator.

NOTES

### Front-panel controls:

Signal Selector

CH A, CH B,  $A\phi/B\phi$  ALT

and FULL FIELD

CHANNEL A

100%-75%-MAX GAIN

75% CAL

GAIN  $\phi$  REF

**BURST** 

**CHANNEL B** 

100%-75%-MAX GAIN

MAX GAIN CAL

GAIN **Display Selector** 

**DIFF PHASE** 

INTENSITY LUMINÁNCE GAIN SCALE ILLUM

As desired CAL

CALIBRATED PHASE

As desired

**POWER** 

0 ON

Right recessed front-panel controls:

FIELD **SYNC** 

INT

# 53. (Optional Step) Check Phase Jitter

a. Connect a color bar video signal via a 75 ohm coaxial cable to the Type 520 CH A J1 connector.

- b. Apply a modulated staircase signal via a 75 ohm coaxial cable to the Type 520 CH B connector.
- c. Connect a 75 ohm end-line termination to the CH A J2 connector and to the CH B J51 connector.
- d. Adjust the channel B PHASE control to position the modulated staircase resultant waveform onto the display area.
- e. Insert onto the color bar video signal 51 mV RMS (73 mV peak-to-peak) of white noise.
- f. CHECK-Type 520 display jitter on the modulated staircase resultant waveform; must be less than 1°. Use the CALIBRATED PHASE control to measure the amount of display jitter.

This completes the calibration of the Type 520. Disconnect all test equipment and replace the top and bottom

# **PARTS LIST ABBREVIATIONS**

внв	binding head brass	int	internal
BHS	binding head steel	lg	length or long
сар.	capacitor	met.	metal
cer	ceramic	mtg hdw	mounting hardware
comp	composition	OD	outside diameter
conn	connector	OHB	oval head brass
CRT	cathode-ray tube	OHS	oval head steel
csk	countersunk	P/O	part of
DE	double end	РНВ	pan head brass
dia	diameter	PHS	pan head steel
	division	plstc	plastic
div		PMC	paper, metal cased
elect.	electrolytic	poly	polystyrene
EMC	electrolytic, metal cased	prec	precision
EMT	electrolytic, metal tubular	PT	paper, tubular
ext	external	PTM	paper or plastic, tubular, molded
F&I	focus and intensity	RHB	round head brass
FHB	flat head brass	RHS	round head steel
FHS	flat head steel	SE	single end
Fil HB	fillister head brass	SN or S/N	serial number
Fil HS	fillister head steel	S or SW	switch
h	height or high	TC	temperature compensated
hex.	hexagonal	THB	truss head brass
HHB	hex head brass	thk	thick
HHS	hex head steel	THS	truss head steel
HSB	hex socket brass	tub.	tubular
HSS	hex socket steel	var	variable
ID	inside diameter	w	wide or width
inc	incandescent	WW	wire-wound

# PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix, Inc. Field Office or representative.

Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number, instrument type or number, serial or model number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix, Inc. Field Office or representative will contact you concerning any change in part number.

# SPECIAL NOTES AND SYMBOLS

×000	Part first added at this serial number
$00 \times$	Part removed after this serial number
*000-0000-00	Asterisk preceding Tektronix Part Number indicates manufactured by or for Tektronix, Inc., or reworked or checked components.
Jse 000-0000-00	Part number indicated is direct replacement.

Over assembly 119-0151.00/ Type 520/R520 NTSC

# SECTION 7 ELECTRICAL PARTS LIST

Values are fixed unless marked Variable.

Ckt. No.	Tektronix Part No.	Serial/Ma Eff	odel No. Disc		Descri	ption					
Bulbs											
B1560 B1562 B1563 B1565 B1566	150-0045-00 150-0047-00 150-0047-00 150-0001-00 150-0001-00			Incandescent #6 Incandescent #0 Incandescent #0 Incandescent #4 Incandescent #4	CN8-398 200 CN8-398 200 7 150 mA	O mA O mA					
B15 <b>67</b> B15 <b>68</b>	150-0001-00 150-0001-00			Incandescent #4 Incandescent #4							
			Сарас	itors							
Tolerance ±20%	unless otherwise	indicated.		•							
C1 C2 C4 C14 C18	290-0290-00 281-0077-00 283-0000-00 283-0000-00 281-0077-00			10 μF 1.3-5.4 pF, Var 0.001 μF 0.001 μF 1.3-5.4 pF, Var	Elect. Air Cer Cer Air	25 V 500 V 500 V					
C33 C36 C37 C40 C41	283-0032-00 283-0026-00 283-0026-00 283-0599-00 283-0116-00			470 pF 0.2 μF 0.2 μF 98 pF 820 pF	Cer Cer Cer Mica Cer	500 V 25 V 25 V 500 V 500 V	5% 5% 5%				
C44 C45 C46 C48 C49	283-0003-00 283-0004-00 283-0598-00 283-0598-00 283-0617-00			0.01 μF 0.02 μF 253 pF 253 pF 4700 pF	Cer Cer Mica Mica Mica	150 V 150 V 300 V 300 V 300 V	5% 5% 10%				
C51 C52 C54 C64 C66	290-0290-00 281-0077-00 283-0000-00 283-0000-00 281-0077-00			10 μF 1.3-5.4 pF, Var 0.001 μF 0.001 μF 1.3-5.4 pF, Var	Elect. Air Cer Cer Air	25 V 500 V 500 V					
C74 C75 C76 C81 C85	283-0000-00 283-0026-00 283-0026-00 281-0610-00 281-0623-00	B010100	B149999	0.001 μF 0.2 μF 0.2 μF 2.2 pF 650 pF	Cer Cer Cer Cer	500 V 25 V 25 V 200 V 500 V	±0.1 pF 5%				

Ctt. No.   Part No.   Eff   Disc   Description		Tektronix		odel No.				
C87	Ckt. No.	Part No.	Eff	Disc		Descrip	tion	
C87	CO.	000 0700 00	D1 50000		110 E	Mina	200 \	20/
C6BB         281-006-00         x8030000         B149999Y         2.2 pF         Cer         200 V         ±0.1 pF           C95         281-0623-00         B010100         B149999         650 pF         Cer         200 V         ±0.1 pF           C95         283-0633-00         B150000         B149999X         BpF         Cer         500 V         ±0.5 pF           C98         281-0940-00         X8030000         B149999X         2.8 pF, Vor         Cer         500 V         ±0.5 pF           C100         290-0135-00         15 μF         Elect.         20 V         ±0.5 pF           C1107         283-0003-00         15 μF         Elect.         20 V         ±0.5 pF           C1108         290-0135-00         15 μF         Elect.         20 V         ±0.5 pF           C122         283-0039-00         15 μF         Cer         150 V         Elect.         20 V         ±0.5 pF           C122         283-0039-00         15 μF         Elect.         20 V         ±0.5 pF         25 V         ±0.5 pF         20 V         ±0.5 pF         ±0.5 pF         ±0.5 pF				D1 40000V				±05 nF
C95					opr		300 ¥	pi
C25			XB030000	B147777X			200 V	01 aE
C95   283.4033.00   B150000   B149999X   B150000   B149999X   B150000   B149999X   B1500000   B149999X   B1500000   B149999X   B1500000   B149999X   B1500000   B149999X   B1500000   B149999X   B1500000   B149999X   B150000   B149999X   B150000   B149999X   B150000   B150000   B149999X   B150000   B1500			D010100	D1 40000				
C97         281-0503-00         B010100         B149999X         2.8 pF, Vor Cer         Cer         500 V         ±0.5 pF           C100         290-0135-00         15 μF         Elect.         20 V         15 μF         Elect.         20 V           C100         283-0035-00         15 μF         Elect.         20 V         15 μF         Elect.         20 V           C120         283-0055-00         1 μF         Cer         25 V         +80%-20%         5%           C132         283-0055-00         0.001 μF         Cer         100 V         5%           C132         283-0055-00         0.001 μF         Cer         25 V         +80%-20%           C132         283-0055-00         NB240000         6.8 μF         Elect.         35 V         +80%-20%           C143         290-0261-00         XB240000         1 μF         Cer         25 V         +80%-20%           C144         283-0059-00         XB240000         1 μF         Cer         25 V         +80%-20%           C144         283-0059-00         XB240000         1 μF         Cer         25 V         +80%-20%           C144         283-0059-00         NB24000         1 μF         Cer         25 V<	C95	281-0623-00	R010100	B149999	650 pF	Cer	500 V	5%
C298	C95	283-0603-00	B150000					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	C97	281-0503-00	B010100	B149999X	8 pF		500 V	$\pm$ 0.5 pF
C109	C98	281-0060-00	XB030000	B149999X		Cer		
C116	C100	290-0135-00			15 μF			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	C109	283-0003-00			0.01 μF	Cer	150 V	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	C116	290-0135-^0			15 μF	Elect.	20 V	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						Cer	25 V	+80%-20%
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					0.001 μF			
C136								5%
C1.43         290-0261-00         XB240000         6.8 μF         Elect.         35 V           C1.44         283-0059-00         XB240000         1 μF         Cer         25 V         +80%-20%           C1.45         283-0059-00         0.001 μF         Cer         100 V         5%           C1.46         283-0059-00         1 μF         Cer         25 V         +80%-20%           C1.48         283-0065-00         0.2 μF         Cer         25 V         -80%-20%           C1.50         283-0026-00         0.2 μF         Cer         25 V         -25 V           C152         283-0026-00         0.2 μF         Cer         25 V         -20 V           C201         281-0512-00         27 pF         Cer         25 V         -20 %           C203         283-0059-00         1 μF         Cer         25 V         +80%-20%           C205         283-001-00         0.02 μF         Cer         150 V         -20 %           C206         283-0081-00         0.01 μF         Cer         150 V         -25 %           C210         283-001-00         0.02 μF         Cer         150 V         -25 %           C210         283-0615-00         33 p								
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					·			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C143	290-0261-00	XB240000				35 V	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	C144	283-0059-00	XB240000		1 μF			
C148  283-0065-C0  0.001 μF  Cer 100 V  5%  C150  283-0026-00  C152  283-0026-00  0.2 μF  Cer 25 V  C201  281-0512-00  27 pF  Cer 25 V  C203  283-0059-00  1 μF  Cer 25 V  10%  C205  283-0004-00  0.003 μF  Cer 25 V  +80%-20%  C206  C208  283-0051-00  0.003 μF  Cer 150 V  C210  283-0081-00  0.01 μF  Cer 25 V  +80%-20%  C210  283-0081-00  0.11 μF  Cer 25 V  +80%-20%  C210  283-0081-00  0.01 μF  Cer 150 V  C220  283-0615-00  33 pF  Mica 500 V  5%  C221  283-0119-00  0.002 μF  Cer 150 V  5%  C222  283-004-00  0.002 μF  Cer 150 V  5%  C229  283-0004-00  0.002 μF  Cer 500 V  5%  C231  283-0001-00  0.005 μF  Cer 500 V  C235  283-0004-00  0.001 μF  Cer 500 V  C236  C236  283-0004-00  0.001 μF  Cer 150 V  C244  283-0593-00  0.01 μF  Cer 150 V  1%  C244  283-0593-00  0.01 μF  Cer 150 V  1%  C254  283-0593-00  0.01 μF  Cer 150 V  1%  C255  285-0629-00  B010100  B149999  1 μF  Cer 100 V  1%  C260  283-0593-00  0.01 μF  Cer 100 V  1%  C273  283-0622-00  80 pF  Mica 300 V  2%  C273  283-0622-00  450 pF  Mica 300 V  1%  C273  283-0622-00  450 pF  Mica 300 V  1%  C275  283-0655-00  0.001 μF  Cer 100 V  5%  C275  283-0650-00  0.001 μF  Cer 100 V  2%  C275  283-0650-00  0.001 μF  Cer 100 V  2%  C275  283-0650-00  0.001 μF  Cer 100 V  2%  C273  283-0652-00  450 pF  Mica 300 V  1%  C275  C275  283-0650-00  0.001 μF  Cer 100 V  5%  C275  283-0650-00  0.001 μF  Cer 100 V  2%  C275  C275  283-0652-00  0.001 μF  Cer 100 V  5%  C275  283-0652-00  0.001 μF  Cer 100 V  2%  C275  283-0655-00  0.001 μF  Cer 100 V  2%  C275  283-0655-00  0.001 μF  Cer 100 V  2%  C275  C275  283-0652-00  0.001 μF  Cer 100 V  2%  C275  C275  C276  C277  C278  C279  C279  C279  C279  C279  C279  C270  C	C145	283-0065-00			0.001 $\mu$ F		100 V	5%
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C146	283-0059-00			1 μF	Cer		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C148	<b>28</b> 3-0065-C0			0.001 μF	Cer	100 V	5%
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C150	283-0026-00			0.2 μF	Cer	25 V	•
$ \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c}$								
$ \begin{array}{c} 203 \\ 283-0059-00 \\ 283-0004-00 \\ 283-0004-00 \\ 283-0004-00 \\ 283-0004-00 \\ 283-0001-00 \\ 283-0001-00 \\ 283-0001-00 \\ 283-0010-00 \\ 283-0015-00 \\ 283-0015-00 \\ 283-0015-00 \\ 283-0015-00 \\ 283-0019-00 \\ 2200 pF \\ 283-0019-00 \\ 283-001$								10%
C205         283-0004-00         0.02 μF         Cer         150 V           C208         283-0051-00         0.0033 μF         Cer         100 V         5%           C210         283-0081-00         0.1 μF         Cer         25 V         +80%-20%           C216         283-0004-00         0.02 μF         Cer         150 V         5%           C220         283-0615-00         33 pF         Mica         500 V         5%           C221         283-0119-00         2200 pF         Cer         200 V         5%           C229         283-0004-00         0.02 μF         Cer         500 V         5%           C231         283-0003-00         XB250000         0.01 μF         Cer         150 V         0.02 μF							25 V	+80%-20%
C210         283-0081-00         0.1 μF         Cer         25 V         +80%—20%           C216         283-0004-00         0.02 μF         Cer         150 V           C220         283-0615-00         33 pF         Mica         500 V         5%           C221         283-0119-00         2200 pF         Cer         200 V         5%           C229         283-0004-00         0.02 μF         Cer         500 V         5%           C231         283-0003-00         XB250000         0.010 μF         Cer         500 V         0.02 μF         Cer         150 V         0.02 μF         0.02 μF         Cer         150 V         0.02 μF         0.02 μF         Cer         150 V         0.02 μF         0.00 μF         0.00 V         1%         0.00 V								
C210         283-0081-00         0.1 μF         Cer         25 V         +80%—20%           C216         283-0004-00         0.02 μF         Cer         150 V           C220         283-0615-00         33 pF         Mica         500 V         5%           C221         283-0119-00         2200 pF         Cer         200 V         5%           C229         283-0004-00         0.02 μF         Cer         500 V         5%           C231         283-0003-00         XB250000         0.010 μF         Cer         500 V         0.02 μF         Cer         150 V         0.02 μF         0.02 μF         Cer         150 V         0.02 μF         0.02 μF         Cer         150 V         0.02 μF         0.00 μF         0.00 V         1%         0.00 V	C208	283_0051_00			0 0033 uF	Cer	100 V	5%
C216         283-004-00         0.02 μF         Cer         150 V           C220         283-0615-00         33 pF         Mica         500 V         5%           C221         283-0119-00         2200 pF         Cer         200 V         5%           C229         283-0004-00         0.02 μF         Cer         150 V         200 V         5%           C231         283-0001-00         0.005 μF         Cer         500 V         200 V         200 V         200 V         200 V         200 V         5%           C236         283-0003-00         XB250000         0.01 μF         Cer         150 V         200 V         200 V         1%         200 V         2			•					+80%-20%
C220   283-0615-00   283-0619-00   2200 pF   Cer   200 V   5%				•	0.02 "F			1 == 70
C221         283-0119-00         2200 pF         Cer         200 V         5%           C229         283-0004-00         0.02 μF         Cer         150 V           C231         283-0001-00         0.005 μF         Cer         500 V           C235         283-0003-00         XB250000         0.01 μF         Cer         150 V           C236         283-004-00         0.02 μF         Cer         150 V           C242         283-0593-00         0.01 μF         Mica         100 V         1%           C244         283-0593-00         0.01 μF         Mica         100 V         1%           C254         290-0267-00         B010100         B149999         1 μF         Elect.         35 V           C254         293-0129-00         B150000         0.56 μF         Cer         100 V           C255         285-0629-00         B010100         B149999         0.047 μF         PTM         100 V           C255         285-0624-00         B150000         0.027 μF         PTM         100 V         10%           C260         283-059-00         39 pF         Cer         200 V         200 V         200 V         200 V         200 V         200 V         2								5%
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								5%
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				•		_		
C235 283-003-00 XB250000 0.01 μF Cer 150 V C236 283-004-00 0.02 μF Cer 150 V C242 283-0593-00 0.01 μF Mica 100 V 1% C244 283-0593-00 0.01 μF Mica 100 V 1% C254 290-0267-00 B010100 B149999 1 μF Elect. 35 V C254 283-0129-00 B150000 0.56 μF Cer 100 V C255 285-0629-00 B010100 B149999 0.047 μF PTM 100 V C255 285-0624-00 B150000 0.027 μF PTM 100 V 10% C260 283-0599-00 8150000 0.027 μF PTM 100 V 10% C261 281-0615-00 3.9 pF Cer 200 V C263 283-0604-00 304 pF Mica 300 V 2% C270 283-003-00 0.01 μF Cer 150 V C272 283-0622-00 450 pF Mica 300 V 1% C273 283-0622-00 450 pF Mica 300 V 1% C273 283-0650-00 450 pF Mica 300 V 1% C275 283-065-00 0.001 μF Cer 100 V 5% CER 10								
C236         283-0004-00         0.02 μF         Cer         150 V           C242         283-0593-00         0.01 μF         Mica         100 V         1%           C244         283-0593-00         0.01 μF         Mica         100 V         1%           C254         290-0267-00         B010100         B149999         1 μF         Elect.         35 V           C254         283-0129-00         B150000         0.56 μF         Cer         100 V           C255         285-0629-00         B010100         B149999         0.047 μF         PTM         100 V           C255         285-0624-00         B150000         0.027 μF         PTM         100 V         10%           C260         283-0599-00         98 pF         Mica         500 V         5%           C261         281-0615-00         3.9 pF         Cer         200 V           C263         283-0604-00         304 pF         Mica         300 V         2%           C270         283-003-00         0.01 μF         Cer         150 V           C272         283-0622-00         450 pF         Mica         300 V         1%           C273         283-0659-00         450 pF         Cer <td>C231</td> <td>283-0001-00</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	C231	283-0001-00						
C242         283-0593-00         0.01 μF         Mica         100 V         1%           C244         283-0593-00         0.01 μF         Mica         100 V         1%           C254         290-0267-00         B010100         B149999         1 μF         Elect.         35 V           C254         283-0129-00         B150000         0.56 μF         Cer         100 V           C255         285-0629-00         B010100         B149999         0.047 μF         PTM         100 V           C255         285-0624-00         B150000         0.027 μF         PTM         100 V         10%           C255         285-0624-00         B150000         0.027 μF         PTM         100 V         10%           C260         283-0599-00         98 pF         Mica         500 V         5%           C261         281-0615-00         3.9 pF         Cer         200 V           C263         283-0604-00         304 pF         Mica         300 V         2%           C270         283-0003-00         0.01 μF         Cer         150 V           C272         283-0622-00         450 pF         Mica         300 V         1%           C275         283-0065-00<			XB250000		$0.01~\mu\text{F}$			
C244 283-0593-00					$0.02~\mu\text{F}$			1.0/
C254         290-0267-00         B010100         B149999         1 μF         Elect.         35 V           C254         283-0129-00         B150000         0.56 μF         Cer         100 V           C255         285-0629-00         B010100         B149999         0.047 μF         PTM         100 V           C255         285-0624-00         B150000         0.027 μF         PTM         100 V         10%           C260         283-0599-00         98 pF         Mica         500 V         5%           C261         281-0615-00         3.9 pF         Cer         200 V           C263         283-0604-00         304 pF         Mica         300 V         2%           C270         283-0003-00         0.01 μF         Cer         150 V           C272         283-0622-00         450 pF         Mica         300 V         1%           C273         283-065-00         450 pF         Mica         300 V         1%           C275         283-065-00         0.001 μF         Cer         100 V         5%	C242	283-0593-00			0.01 μF	Mica	100 V	1%
C254       290-0267-00       B010100       B149999       1 μF       Elect.       35 V         C254       283-0129-00       B150000       0.56 μF       Cer       100 V         C255       285-0629-00       B010100       B149999       0.047 μF       PTM       100 V         C255       285-0624-00       B150000       0.027 μF       PTM       100 V       10%         C260       283-0599-00       98 pF       Mica       500 V       5%         C261       281-0615-00       3.9 pF       Cer       200 V         C263       283-0604-00       304 pF       Mica       300 V       2%         C270       283-0003-00       0.01 μF       Cer       150 V         C272       283-0622-00       450 pF       Mica       300 V       1%         C273       283-065-00       450 pF       Mica       300 V       1%         C275       283-065-00       0.001 μF       Cer       100 V       5%	C244	283-0593-00			0.01 μF			1%
C254       283-0129-00       B150000       0.56 μF       Cer       100 V         C255       285-0629-00       B010100       B149999       0.047 μF       PTM       100 V         C255       285-0624-00       B150000       0.027 μF       PTM       100 V       10%         C260       283-0599-00       98 pF       Mica       500 V       5%         C261       281-0615-00       3.9 pF       Cer       200 V         C263       283-0604-00       304 pF       Mica       300 V       2%         C270       283-0003-00       0.01 μF       Cer       150 V       1%         C272       283-0622-00       450 pF       Mica       300 V       1%         C273       283-0652-00       450 pF       Mica       300 V       1%         C275       283-065-00       0.001 μF       Cer       100 V       5%			B010100	B149999		Elect.		
C255       285-0629-00       B010100       B149999       0.047 μF       PTM       100 V       10%         C255       285-0624-00       B150000       0.027 μF       PTM       100 V       10%         C260       283-0599-00       98 pF       Mica       500 V       5%         C261       281-0615-00       3.9 pF       Cer       200 V         C263       283-0604-00       304 pF       Mica       300 V       2%         C270       283-0003-00       0.01 μF       Cer       150 V         C272       283-0622-00       450 pF       Mica       300 V       1%         C273       283-0622-00       450 pF       Mica       300 V       1%         C275       283-065-00       0.001 μF       Cer       100 V       5%					<b>0.</b> 56 μ <b>F</b>	Cer	100 V	
C255       285-0624-00       B150000       0.027 μF       PTM       100 V       10%         C260       283-0599-00       98 pF       Mica       500 V       5%         C261       281-0615-00       3.9 pF       Cer       200 V         C263       283-0604-00       304 pF       Mica       300 V       2%         C270       283-0003-00       0.01 μF       Cer       150 V         C272       283-0622-00       450 pF       Mica       300 V       1%         C273       283-0622-00       450 pF       Mica       300 V       1%         C275       283-065-00       0.001 μF       Cer       100 V       5%				B149999		PTM		
C261       281-0615-00       3.9 pF       Cer       200 V         C263       283-0604-00       304 pF       Mica       300 V       2%         C270       283-0003-00       0.01 μF       Cer       150 V         C272       283-0622-00       450 pF       Mica       300 V       1%         C273       283-0622-00       450 pF       Mica       300 V       1%         C275       283-065-00       0.001 μF       Cer       100 V       5%					$0.027~\mu$ F	PTM	100 V	10%
C261       281-0615-00       3.9 pF       Cer       200 V         C263       283-0604-00       304 pF       Mica       300 V       2%         C270       283-0003-00       0.01 μF       Cer       150 V         C272       283-0622-00       450 pF       Mica       300 V       1%         C273       283-0622-00       450 pF       Mica       300 V       1%         C275       283-065-00       0.001 μF       Cer       100 V       5%	C260	<b>283_</b> 0599_00	-		98 pF	Mica	500 V	5%
C263       283-0604-00       304 pF       Mica       300 V       2%         C270       283-0003-00       0.01 μF       Cer       150 V         C272       283-0622-00       450 pF       Mica       300 V       1%         C273       283-0622-00       450 pF       Mica       300 V       1%         C275       283-065-00       0.001 μF       Cer       100 V       5%								- 70
C270       283-0003-00       0.01 μF       Cer       150 V         C272       283-0622-00       450 pF       Mica       300 V       1%         C273       283-0622-00       450 pF       Mica       300 V       1%         C275       283-065-00       0.001 μF       Cer       100 V       5%         C276       283-065-00       0.001 μF       Cer       100 V       5%								2%
C272 283-0622-00 450 pF Mica 300 V 1%  C273 283-0622-00 450 pF Mica 300 V 1%  C275 283-0065-00 0.001 μF Cer 100 V 5%								,,
C273 283-0622-00 450 pF Mica 300 V 1% C275 283-0065-00 0.001 μF Cer 100 V 5%								1%
C275 283-0065-00 0.001 μF Cer 100 V 5%	-				•			
C275 283-0065-00 0.001 $\mu$ F Cer 100 V 5%	C273	283-0622-00						1%
								5%
		281-0638-00			240 pF	Cer	500 V	5%

cı - No	Tektronix		Model No.				
Ckt - No.	Part No.	Eff	Disc		Desc	ription	
C282	283-0003-00			0.01 μF	Cer	150 V	
C295	283-0059-00			1 μF	Cer	25 V	1.000/ .000
C296	283-0059-00			1 μF	Cer	25 V	+80%-20%
C297	283-0059-00			1 μF	Cer	25 V	+80%-20%
C2 <b>99</b>	283-0111-00			0.1 μF	Cer	50 V	+80%-20%
C30 1	283-0065-00			0.001 μF	Cer	100 \/	
C30-4	283-0065-00			0.001 μF	Cer	100 V	5%
C31 7	283-0065-00			0.001 μF	Cer	100 V	5%
C31 4	283-0065-00			0.001 μF	Cer	100 V 100 V	5% 5%
C327	283-0065-00			0.001 μF	Cer	100 V	5% 5%
C32 <b>9</b>	283-0003-00			0.01 μF	Cer	1501/	
C332	283-0612-00			82 pF	Mica	150 ∨ 500 ∨	
C335A)	281-0109-01			1-16.5 pF		ston Assembly	
C34O	283-0079-00			0.01 μF	Cer	250 V	
6246	281-0580-00						
C34 <b>2</b> C34 <b>5</b>	283-0079-00			470 pF	Cer	500 V	10%
C34 <b>6</b>	283-0004-00			0.01 μF	Cer	250 V	,-
C34 <b>9</b>	283-0079-00			0.02 μF	Cer	150 V	
C3521	200 00,7 00			0.01 µF	Cer	250 V	
C358 <sup>1</sup> C362 <sup>2</sup> C364 <sup>2</sup> C368 <sup>2</sup> C401	281-0063-00	XB150000		9-35 pF, Var	Cer		
C404	281-0550-00	XB150000	B239999	120 pF	Cer	500 V	100/
C404				750 pF			
C411				9-35 pF, Var	Cer		5 /6
C414			B239999		Cer	500 V	10%
C414					Mica	500 V	
C430	261-0054-00	XR120000		0.25-1.5 pF, Var	Tub.		<b>3</b> 78
C433	281-0611-00	XB150000		2.7 pF	Cer	200 V	+0 25 nE
C434				9-35 pF, Var			0.25 pi
C435				65 pF	Mica	500 V	1%
C439				0.25-1.5 pF, Var	Tub.		. 76
C441	201-0011-00	VD120000		2.7 pF	Cer	200 V	$\pm$ 0.25 pF
C442	281-0615-00	B010100	B149999	3.9 pF	Cer	200 V	
C442				9-35 pF, Var	Cer		
C445		XB150000		62 pF	Mica	500 V	1%
C446		D010100	D1 (0000	0.2 μF	Cer		• 76
C449	203-0108-00	BOTOTOO	B149999	220 pF	Cer	200 V	10%
C449	283-0641-00	B150000		180 pF	Mica	100 V	1 %
C450					Cer		' /0
C453		•		2-8 pF, Var	Cer		
C454				2-8 pF, Var	Cer		
C455		_		56 pF	Mica	100 V	1%
	281-0550-00 283-0524-00 281-0063-00 281-0550-00 281-0550-00 281-0054-00 281-0092-00 281-0064-00 281-0611-00 281-0611-00 281-0615-00 281-0692-00 283-0629-00 283-0629-00 283-0026-00 283-0108-00	XB150000 B240000 XB150000 XB150000 XB150000 XB150000 XB150000 XB150000 XB150000 XB150000 XB150000 AB150000 AB150000 AB150000 AB150000 AB150000 AB150000	B239999  B149999  B149999	120 pF 750 pF 9-35 pF, Var 120 pF 750 pF 0.25-1.5 pF, Var 2.7 pF 9-35 pF, Var 65 pF 0.25-1.5 pF, Var 2.7 pF 3.9 pF 9-35 pF, Var 62 pF 0.2 μF 220 pF	Cer Mica Cer Mica Tub. Cer Mica Tub. Cer Mica Cer Cer Mica Cer Cer Cer Cer Cer Cer Cer	500 V 200 V 200 V 200 V 500 V 25 V 200 V	1%

Ckt. No.	Tektronix Serial/Model No. Part No. Eff Disc			Description			
				42 - E	Mica	500 V	5%
C457	283-0600-00	D010100	D1 40000	43 pF 0.02 μF	Cer	150 V	
C461	283-0004-00	B010100	B149999	0.02 μF	Cer	25 V	
C461	283-0026-00	B150000		0.2 μι 1Ε	Cer	25 V	+80%-20%
C465	283-0059-00	VD000000	D1 40000V	1 μF 3.9 pF	Cer	200 V	, , , , , , , , , , , , , , , , , , , ,
C471	281-0615-00	XB030000	B149999X	3.7 μι	<b>C</b> U.		
C474	283-0599-00	B010100	B149999	98 pF	Mica	500 V	5%
C474 C474	283-0632-00	B150000		87 pF	Mica	100 V	1%
C474	283-0004-00	XB150000		0.02 μF	Cer	150 V	000/ 000/
C476	283-0059-00	XB150000		1 μF	Cer	25 V	+80%-20%
C478	290-0135-00	XB030000	B149999X	15 μF	Elect.	20 V	
C400	283-0598-00	B010100	B259999	253 pF	Mica	300 V	5%
C490	281-0528-00	B260000		82 pF	Cer	500 V	10%
C490 C491	283-0615-00	520000		33 pF	Mica	500 V	5%
C491 C494	283-0079-00	B010100	B029999	0.01 μF	Cer	250 V	
C494	283-0027-00	B030000	B259999	$0.02~\mu \text{F}$	Cer	50 V	
C 40.4	285-0683-00	B260000		0.022 μF	PTM	100 V	5%
C494	283-003-00	XB260000		1 μF	Cer	25 V	+80%-20%
C495	283-0604-00	ABZOOGG		304 pF	Mica	300 V	2% 2%
C500	283-0604-00			304 pF	Mic <b>a</b>	300 V	2%
C502 C503	281-0064-00			0.25-1.5 pF, Var	Tub.		
	281-0619-00	B010100	B149999	1.2 pF	Cer	200 V	
C504	281-0609-00	B150000	<b>3</b>	1 pF	Cer	200 V	10%
C504 C528	283-0004-00	B130000		0.02 μF	Cer	150 V	F0/
C529	283-0032-00			470 pF	Cer	500 V	5%
C532	283-0032-00			470 pF	Cer	500 V	5%
CFOF	283-0065-00			0.001 μF	Cer	100 V	5%
C535	283-0103-00			180 p <b></b> F	Cer	500 V	5%
C538	283-0600-00		•	43 pF	Mica	500 V	5%
C545 C547	283-0604-00			304 pF	Mica	300 V	2%
C548	283-0059-00			1 μF	Cer	<b>2</b> 5 V	+80%—20%
65.40	283-0600-00			43 pF	Mica	500 V	5%
C549 .	283-0006-00			0.2 μF	Cer	25 V	
C550	283-0026-00			0.2 μF	Cer	25 V	==1
C553 C554	283-0600-00			43 pF	Mica	500 V	5%
C555	283-0059-00			1 μF	Cer	25 V	+80%-20%
CET!	290-0284-00			4.7 μF	Elect.	35 V	10%
C556	281-0528-00			82 pF	Cer	500 V	10%
C557	283-0004-00			0.02 μF	Cer	150 V	
C558	283-0026-00			0.2 μF	Cer	25 V	
C559 C564	283-0004-00			0.02 μF	Cer	150 V	
CF.//	283-0004-00			0.02 μF	Cer	150 V	
C566	283-0004-00			0.01 μF	Cer	150 V	
C567	283-0003-00			0.2 μF	Cer	25 V	
C568	290-0284-00			4.7 μF	Elect.	35 V	10%
C569 C578	283-0603-00	XB150000		113 pF	Mica	300 V	2%
		B010100	B149999	0.004 <b>7</b> μF	Cer	500 V	5%
C580	283-0083-00	B010100	0147777	0.0047 μι 0.01 μF	Cer	50 V	10%
C580	283-0155-00	B150000 B010100	B149999	180 pF	Mica	100 V	1%
C584	283-0641-00	סטוטוס	U14////	F.			

	Tektronix	Serial/M	odel No.	e de la companya de l			
Ckt. No.	Part No.	Eff	Disc		Descri	ption	
C584 <b>C586</b>	283-0631-00 281-0093-00	B150000 B010100	B259999	95 pF 5.5-18 pF, Var	Mica Cer	100 V	1%
C586	281-0092-00	B260000		9-35 pF, Var	Cer		
C587 C590	283-0003-00			0.01 μF	Cer	150 V	
C370	283-0622-00	•		450 pF	Mica	300 V	. 1%
C592 C593	283-0622-00 281-0064-00		ě.	450 pF 0.25-1.5 pF, Var	Mica Tub.	300 V	1%
C594	281-0619-00			1.2 pF	Cer	200 V	
C595 C601	281-061 <i>5</i> -00 283-05 <b>%8-0</b> 0			3.9 pF	Cer	200 V	
	203-0376-00			253 pF	Mica	300 V	5%
C602 C606	283-0639-00			56 pF	Mica	100 V	1%
C607	283-0598-00 283-0639-00			253 pF	Mica	300 V	5%
C608	283-0026-00			56 pF	Mica	100 V	1%
C609	283-0026-00			0.2 μF 0.2 μF	Cer Cer	25 V	
	200 0020 00			<b>0.2</b> μΓ	Cer	25 V	
C610 C611	281-0653-00 283-0637-00			3.3 pF	Cer	200 V	±1 pF
C612	283-0636-00			20 pF	Mica	100 V	1%
C613	283-0635-00			36 pF 51 pF	Mica Mica	100 V 100 V	1%
C614	283-0634-00			65 pF	Mica	100 V	1% 1%
				•	Mica	100 ¥	1 /0
C615 C616	283-0633-00			<i>7</i> 7 pF	Mica	100 V	1%
C617	283-0632-00 283-0631-00			87 pF	Mica	100 V	1%
C618	283-0630-00			95 pF 110 pF	Mica	100 V	1%
C619	283-0641-00			180 pF	Mica Mica	100 V 100 V	1% 1%
C622	281-0528-00	B010100	B189999	00 F	•	500.14	
C622	281-0549-00	B190000	D107777	82 pF 68 pF	Cer	500 V	10%
C624	283-0026-00	XB220000		$0.2~\mu \text{F}$	Cer Cer	500 V 25 V	10%
C632	281-0511-00			22 pF	Cer	500 V	10%
C642	281-0528-00			82 pF	Cer	500 V	10%
C644	283-0026-00	XB220000		0.2 μF	Cer	25 V	
C652	281-0511-00			22 pF	Cer	500 V	10%
C661	283-0026-00			0.2 μF	Cer	25 V	. 0 78
C665	283-0594-00			$0.001 \mu F$	Mica	100 V	1%
C686	<b>283</b> -0599-00			98 pF	Mica	500 V	5%
C688	281-0637-00			91 pF	Cer	500 V	5%
C690 C691	283-0026-00			$0.2~\mu$ F	Cer	25 V	
C695	283-0059-00 285-0443-00			1 μF	Cer	25 V	+80%-20%
C807	285-0643-00 285-0627-00			0.0047 μF	PTM	100 V	5%
C007	263-0627-00	•		0.0033 μF	PTM	100 V	5%
C817	285-0627-00			0.0033 μF	PTM	100 V	5%
C822 C841	283-0079-00 283-0079-00			0.01 μF	Cer	250 V	•
C848	281-0118-00			0.01 μF	Cer	250 V	
C849	283-0622-00			8-90 pF, <b>Va</b> r 450 pF	Mica Mica	300 V	1%
C868	202 0110 00			·			. ,0
C877	283-0110-00 283-0110-00			0.005 μF	Cer	150 V	
C892	283-0079-00			0.005 μF 0.01 μF	Cer	150 V	
C896	290-0114-00			47 μF	Cer Elect.	250 V 6 V	
					2.001.	0 7	

Ckt. No.	Tektronix Part No.				Description			
C907 C917 C922 C958 C961	285-0627-00 285-0627-00 283-0079-00 281-0076-00 281-0079-00			0.0033 μF 0.0033 μF 0.01 μF 1.2-3.5 pF, Var 0.01 μF	PTM PTM Cer Air Cer	100 V 100 V 250 V	5% 5%	
C968 C969 C987 C1102 C1114	281-0118-00 283-0622-00 283-0110-00 290-0267-00 290-0244-00		•	8-90 pF, Var 450 pF 0.005 μF 1 μF 0.47 μF	Mica Mica Cer Elect. Elect.	300 V 150 V 35 V 35 V	1 % 5%	
C1116 C1126 C1128 C1131 C1140	290-0282-00 281-0521-00 283-0004-00 283-0059-00 283-0059-00			0.047 μF 56 pF 0.02 μF 1 μF 1 μF	Elect. Cer Cer Cer Cer	35 V 500 V 150 V 25 V	10% 10% +80%—20% +80%—20%	
C1150 C1153 C1156 C1164 C1172	283-0594-00 290-0276-00 283-0004-00 283-0594-00 283-0059-00			0.001 μF 0.68 μF 0.02 μF 0.001 μF 1 μF	Mica Elect. Cer Mica Cer	100 V 35 V 150 V 100 V 25 V	1 % 10 % 1 % +80 % —20 %	
C1184 C1188 C1190 C1196 C1198	283-0010-00 283-0004-00 283-0594-00 290-0267-00 281-0613-00			0.05 μF 0.02 μF 0.001 μF 1 μF 10 pF	Cer Cer Mica Elect. Cer	50 V 150 V 100 V 35 V 200 V	1% 1%	
C1201 C1204 C1227 C1233 C1238	283-0059-00 283-0004-00 283-0010-00 283-0119-00 283-0057-00			1 μF 0.02 μF 0.05 μF 2200 pF 0.1 μF	Cer Cer Cer Cer	25 V 150 V 50 V 200 V 200 V	+80%-20% +80%-20%	
C1252 C1259 C1263 C1283 C1405	283-0594-00 285-0702-00 285-0702-00 283-0593-00 290-0135-00	т.		0.001 μF 0.033 μF 0.033 μF 0.01 μF 15 μF	Mica PTM PTM Mica Elect.	100 V 100 V 100 V 100 V 20 V	1% 5% 5% 1%	
C1414 C1422 C1423 C1424 C1424	285-0684-00 290-0274-00 290-0287-00 285-0623-00 285-0633-00	B010100 B310000	B309999	0.056 μF 80 μF 47 μF 0.47 μF 0.22 μF	PTM Elect. Elect. PTM PTM	100 V 50 V 25 V 100 V 100 V	5% +75%—10%	
C1430 C1433 C1436 C1438 C1440	283-0026-00 283-0059-00 283-0026-00 285-0622-00 290-0297-00	ſ		0.2 μF 1 μF 0.2 μF 0.1 μF 39 μF	Cer Cer Cer PTM Elect.	25 V 25 V 25 V 100 V 10 V	+80%-20%	
C1452 C1453 C1454 C1468 C1478	283-0036-00 283-0071-00 283-0071-00 283-0006-00 283-0003-00			$2500 \text{ pF} \\ 0.0068  \mu\text{F} \\ 0.0068  \mu\text{F} \\ 0.02  \mu\text{F} \\ 0.01  \mu\text{F}$	Cer Cer Cer Cer	6000 V 5000 V 5000 V 500 V 150 V		

# Capacitors (cont)

	Tektronix	Serial/Mo					
Ckt. No.	Part No.	Eff	Disc		Descri	ption	
C1480	283-0087-00			300 pF	Cer	1000 V	10%
C1485	283-0033-00			0.001 μF	Cer	6000 V	10 /0
C1490	283-0033-00			0.001 μF	Cer	6000 V	
C1502	290-0336-00			130 μF	Elect.	300 V	+50%-10%
C1511	283-0000-00	*		0.001 μF	Cer	500 V	+50%-10%
C1 500	000 0005 00				<b>=1</b> .		
C1522 C1524	290-0285-00	VD210000		4 μF	Elect.	200 V	+50%—10%
	283-0659-00	XB310000		1160 pF	Mica	500 V	2%
C1532 C1545	290-0335-00	D010100	D200000	240 μF	Elect.	200 V	+50%-10%
C1545	283-0079-00 283-0617-00	B010100 B310000	B309999	0.01 μ <b>F</b> 4700 pF	Cer Mica	250 V 300 V	10%
01.550			•				
C1552	290-0285-00			4 μF	Elect.	200 V	+50%—10%
C1554	285-0569-00	B010100	B309999	0.01 μF	PTM	200 V	
C1554	283-0659-00	B310000		1160 pF	Mica	500 V	2%
C1562	290-0337-00			2300 μF	Elect.	50 V	+75%—10%
C1574	283-0026-00			$0.2~\mu$ F	Cer	25 V	
C1600	285-0683-00			$0.022~\mu extsf{F}$	PTM	100 V	5%
C1622	290-0312-00			47 μF	Elect.	35 V	10%
C1623	283-0059-00			$1 \mu$ F	Cer	25 V	+80%-20%
C1624	290-0284-00			4.7 μF	Elect.	35 V	10%
	,		Diod	es			
D4	*152-0185-00			Silicon	Re	placeable by	/ 1N4152
D6	152-0141-00	B010100	B159999	Silicon		4152	
D6	152-0141-02	B160000		Silicon		4152	*
D8	*152-0322-00			Silicon		< Spec	
D14	*152-0185-00			Silicon		olaceable by	1N4152
D16	152-0141-00	B010100	B159999	Silicon		4152	1141132
D16	152-0141-02	B160000		Silicon	11	4152	
D18	*152-0322-00	5100000		Silicon		Spec	
D48	*152-0185-00			Silicon		olaceable by	1814150
D54	*152-0185-00			Silicon			
D56	152-0141-00	B010100	B159999	Silicon		olaceable by 4152	1114152
D56	152-0141-02	B160000	D13////	Silicon		4152	
D58	*152-0322-00			Silicon	Tek	Spec	
D64	*152-0185-00		_	Silicon		olaceable by	1N4152
D66	152-0141-00	B010100	B159999	Silicon		4152	114132
D66	152-0141-02	B160000		Silicon		4152	
D68	*152-0322-00			Silicon		Spec	
085	*152-0185-00			Silicon		olaceable by	1N4152
D95	*152-0185-00			Silicon	Res	olaceable by	1N4152
D100	*152-0185-00			Silicon		olaceable by	
0102	*152-0185-00	•		Silicon	Ret	placeable by	1N4152
D108	*152-0185-00			Silicon		placeable by	
0112	*152-0185-00			Silicon		placeable by	
0114	*152-0185-00			Silicon		laceable by	
0116	*152-0185-00			Silicon	Rep	laceable by	
0122	*152-0185-00			Silicon	Rep	laceable by	1N4152
0126	*152-0185-00			Silicon	Rep	laceable by	1N4152
0132	*152-0185-00			Silicon	Rep	laceable by	1N4152
0134	*152-0185-00			Silicon	Rep	laceable by	1N4152
0142	152-0279-00			Zener	1N	751A 400 m\	V, 5.1 V, 5%
D144	*152-0185-00	XB240000		Silicon	Rep	laceable by	1N4152
*152- *152- *152- *152- 152-	0185-00 0185-00 0185-00 0185-00 0279-00	XB240000 XB240000		Silicon Silicon Silicon Silicon Zener	Rep Rep Rep Rep 1 N	placeable by placeable by placeable by placeable by 751A 400 m	1N4152 1N4152 1N4152 1N4152 V, 5.1 V, 5%

Ckt. No.	Tektronix Part No.	Serial/Mo Eff	odel No. Disc		Description
D206 D210	*152-0185-00 *152-0185-00			Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152
D212 ) D214 }	*153-0035-00			Silicon	(Matched pair)
D224	*152-0185-00			Silicon	Replaceable by 1N4152
D234 D235 D242 D244 D257	*152-0185-00 *152-0185-00 *152-0153-00 *152-0153-00 152-0226-00	B010100 XB250000 XB230000	B249999X	Silicon Silicon Silicon Silicon Zener	Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4244 Replaceable by 1N4244 1N751A 0.4W, 5.1V, 5%
D260 D285 D301 D302 D311	152-0358-00 152-0278-00 *152-0185-00 *152-0185-00 *152-0185-00			Silicon Zener Silicon Silicon Silicon	Voltage Variable Capacitance 1N4372A 0.4 W, 3 V, 5% Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D312 D407 D408 D408 D409	*152-0185-00 *152-0322-00 152-0141-00 152-0141-02 *152-0322-00	B010100 B160000	B159999	Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Tek Spec 1N4152 1N4152 Tek Spec
D417 D418 D418 D419 D421	*152-0322-00 152-0141-00 152-0141-02 *152-0322-00 *152-0185-00	B010100 B160000	B159999	Silicon Silicon Silicon Silicon Silicon	Tek Spec 1N4152 1N4152 Tek Spec Replaceable by 1N4152
D424 D424 D427 D429 D429	152-0141-00 152-0141-02 *152-0185-00 152-0141-00 152-0141-02	B010100 B160000 B010100 B160000	B159999	Silicon Silicon Silicon Silicon Silicon	1N4152 1N4152 Replaceable by 1N4152 1N4152 1N4152
D432 D436 D450 D463 D465	*152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00			Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D486 D486 D487 D488 D488	152-0141-00 152-0141-02 *152-0322-00 152-0141-00 152-0141-02	B010100 B160000 B010100 B160000	B159999 B159999	Silicon Silicon Silicon Silicon Silicon	1N4152 1N4152 Tek Spec 1N4152 1N4152
D494 D496 D497 D498 D504	152-0141-02 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00	XB260000		Silicon Silicon Silicon Silicon Silicon	1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D505 D506 D507 D506 ) D508 }	*152-0322-00 *152-0322-00 *152-0322-00 *153-0037-00	B010100 B150000	B149999	Silicon Silicon Silicon Silicon	Tek Spec Tek Spec Tek Spec (matched pair)
D508 D509 D511	*152-0322-00 *152-0185-00 *152-0185-00	B010100	B149999	Silicon Silicon Silicon	Tek Spec Replaceable by 1N4152 Replaceable by 1N4152

	Tektronix	Serial/M	odel No.		·
Ckt. No.	Part No.	Eff	Disc		Description
D515 D517 D520 D521 D522	*152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00			Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D524 D525 D526 D527 D532	*152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00			Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D533 D543 D576 D580 D581	*152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00			Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D586 D586 D594 D595 D596	*152-0269-00 *152-0270-00 *152-0185-00 *152-0322-00 *152-0322-00	B010100 B150000	B149999 B149999	Silicon Silicon Silicon Silicon Silicon	Voltage Variable Capacitance Tek Spec Voltage Variable Capacitance Tek Spec Replaceable by 1N4152 Tek Spec Tek Spec
D597 D598 D596 )	*152-0322-00 *152-0322-00	B010100	B149999	Silicon Silicon	Tek Spec Tek Spec
D598 <b>)</b> D599	*153-0037-00 *152-0185-00	B150000		Silicon Silicon	(matched pair)  Replaceable by 1N4152
D680 D694 D695 D696 D697	*152-0185-00 *152-0185-00 152-0278-00 152-0278-00 *152-0185-00	÷		Silicon Silicon Zener Zener Silicon	Replaceable by 1N4152 Replaceable by 1N4152 1N4372A 0.4 W, 3 V, 5% 1N4372A 0.4 W, 3 V, 5% Replaceable by 1N4152
D698 D702 D706 D706 D712	*152-0185-00 *152-0185-00 152-0141-00 152-0141-02 *152-0185-00	B010100 B160000	B159999	Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 1N4152 1N4152 Replaceable by 1N4152
D716 D716 D722 D726 D726	152-0141-00 152-0141-02 *152-0185-00 152-0141-00 152-0141-02	B010100 B160000 B010100 B160000	B159999 B159999	Silicon Silicon Silicon Silicon Silicon	1N4152 1N4152 Replaceable by 1N4152 1N4152 1N4152
D732 D736 D736 D742 D746	*152-0185-00 152-0141-00 152-0141-02 *152-0185-00 152-0141-00	B010100 B160000	B159999	Silicon Silicon Silicon	Replaceable by 1N4152 1N4152 1N4152 Replaceable by 1N4152
D746 D756 D756 D760 D766	152-0141-00 152-0141-02 152-0141-00 152-0141-02 *152-0185-00 152-0141-00	B010100 B160000 B010100 B160000	B159999 B159999	Silicon Silicon Silicon Silicon Silicon Silicon	1N4152 1N4152 1N4152 1N4152 Replaceable by 1N4152 1N4152
D766 D775 D780 D805A,B,C,D	152-0141-02 *152-0185-00 *152-0185-00 *152-0185-00	B160000	2.0///	Silicon Silicon Silicon Silicon	1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152

Ckt. No.	Tektronix Part No.	Serial/Mo Eff	odel No. Disc		Description
D861 D862 D873 D875 D876	*152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00			Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D905A,B,C,D D932 D940 D940 D944	*152-0185-00 *152-0185-00 152-0141-00 152-0141-02 152-0141-00	B010100 B160000 B010100	B159999 B159999	Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 1N4152 1N4152 1N4152
D944 D982 D983 D985 D986	152-0141-02 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00	B160000		Silicon Silicon Silicon Silicon Silicon	1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D993 D1105 D1106 D1110 D1112	*152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00	B010106	B149999X	Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D1135 D1140 D1142 D1143 D1144	*152-0185-00 *152-0185-00 152-0280-00 152-0245-00 152-0280-00	XB260000		Silicon Silicon Zener Silicon Zener	Replaceable by 1N4152 Replaceable by 1N4152 1N753A 0.4 W, 6.2 V, 5% High Speed 1N753A 0.4 W, 6.2 V, 5%
D1145 D1160 D1164 D1166 D1178	152-0245-00 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00			Silicon Silicon Silicon Silicon Silicon	High Speed Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D1190 D1192 D1196 D1206 D1208	*152-0061-00 *152-0185-00 *152-0185-00 *152-0185-00 *152-0185-00			Silicon Śilicon Silicon Silicon Silicon	Tek Spec Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152
D1216 D1220 D1222 D1225 D1235	*152-0185-00 *152-0185-00 *152-0061-00 *152-0061-00 *152-0061-00			Silicon Silicon Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 Tek Spec Tek Spec Tek Spec
D1239 D1252 D1252 D1253 D1256	*152-0185-00 *152-0061-00 152-0283-00 *152-0185-00 *152-0185-00	B010100 B060000	B059999	Silicon Silicon Zener Silicon Silicon	Replaceable by 1N4152 Tek Spec 1N976B 0.4 W, 43 V, 5% Replaceable by 1N4152 Replaceable by 1N4152
D1258 D1265 D1266	*152-0185-00 *152-0185-00 *152-0185-00	··		Silicon Silicon Silicon	Replaceable by 1N4152 Replaceable by 1N4152 Replaceable by 1N4152

ore No	Tektronix		Model No.		
Ckt. No.	Part No.	Eff	Disc		Description
D1 <b>2</b> 70	*152-0185-00			Silicon	Paulmanhla III 1814150
D1 <b>2</b> 75	*152-0185-00			Silicon	Replaceable by 1N4152
D1285	*152-0185-00			Silicon	Replaceable by 1N4152
D1286	*152-0185-00			Silicon	Replaceable by 1N4152 Replaceable by 1N4152
D1292	*152-0185-00	*		Silicon	Replaceable by 1N4152
				Gilleon	Replaceable by 1141152
D1 <b>30</b> 6	*152-0185-00			Silicon	Parla III I INIGE
D1310	*152-0185-00			Silicon	Replaceable by 1N4152
D1312	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1314	*152-0185-00			Silicon	Replaceable by 1N4152 Replaceable by 1N4152
D1316	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
				06011	Replaceable by 1144132
D1318	*152-0185-00	XB150000		Silicon	Paulous abla 1 101/150
D1320	*152-0185-00	7.5.0000		Silicon	Replaceable by 1N4152
D1322	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1324	*152-0185-00			Silicon	Replaceable by 1N4152 Replaceable by 1N4152
D1326	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
•				·	Replaceable by 114132
D1000	*150 0105 00	VD1 50000			
D1 <b>32</b> 8 D13 <b>3</b> 0	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1332	*152-0185-00 *152-0185-00	VD150000		Silicon	Replaceable by 1N4152
D1334	*152-0185-00 *152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1334 D1336	*1 <i>5</i> 2-0185-00 *1 <i>5</i> 2-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1338	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1330	132-0103-00	XB130000		Silicon	Replaceable by 1N4152
D1340	*152-0185-00			6:1:	
D1342	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1344	*152-0185-00	XB130000		Silicon Silicon	Replaceable by 1N4152
D1346	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1348	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
2,0		7.5150000		Silicon	Replaceable by 1N4152
D1350	*152-0185-00	•		Silicon	Poulous abla 1 1214150
D1352	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1354	*152-0185-00			Silicon	Replaceable by 1N4152
D1356	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152 Replaceable by 1N4152
D135 <b>8</b>	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
		4			Replacedble by 1144152
D1359	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1360	*152-0185-00	B010100	B149999X	Silicon	Replaceable by 1N4152
D1362	*152-0185-00	B010100	B149999X	Silicon	Replaceable by 1N4152
D13 <b>70</b>	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D13 <b>72</b>	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1374	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1376	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1378	*152-0185-00	XB150000		Silicon	Replaceable by 1N4152
D1404	*152-0185-00			Silicon	Replaceable by 1N4152
D1405	*152-0107-00			Silicon	Replaceable by 1N647
D1414	*152-0185-00			Silicon	Replaceable by 1N4152
D1432	152 01 41 00	D010100	D1 50000	0111	
D1432 D1432	152-0141-00 152-0141-02	B010100	B159999	Silicon	1N4152
D1436	152-0141-00	B160000 B010100	B159999	Silicon	1N4152
D1436	152-0141-00	B160000	0137777	Silicon	1N4152
D1440	152-0333-00	5100000		Silicon Silicon	1N4152
D1442	152-0333-00			Silicon	High Speed and Conductance
2				JIICON	High Speed and Conductance

Ckt. No.	Tektronix Part No.	Serial/Model Eff	No. Disc		Description
D1 452 D1 453 D1 468 D1 502A,B,C,D D1 503	152-0192-00 152-0192-00 *153-0034-00 152-0066-01 152-0066-01			Silicon Silicon Zener Silicon Silicon	7701-5X, Varo 7701-5X, Varo 0.4 W, 105 V, 5% at 200 μA 400 V, 0.75 A 400 V, 0.75 A
D1510 D1532A,B,C,D D1540 D1554 D1562	*152-0185-00 152-0066-01 152-0295-00 *152-0185-00 152-0198-00			Silicon Silicon Zener Silicon Silicon	Replaceable by 1N4152 400 V, 0.75 A 1N3042B 82 V, 5% Replaceable by 1N4152 MR1032A (Motorola)
D1564 D1570 D1590	152-0198-00 152-0123-00 152-0055-00			Silicon Zener Zener	MR1032A (Motorola) 1N935A 0.4 W, 9.1 V, 5% TC 1N962B 0.4 W, 11 V, 5%
. •			Fuse	<b>95</b>	
F1 500 F1 501 F1 502 F1 502 F1 532 F1 562 F1 562 F1 562	159-0034-00 159-0018-00 159-0024-00 159-0052-00 159-0028-00 159-0016-00 159-0041-00 159-0034-00	B050000 B010100	3 <b>049999</b> 3299999 3309999	1.6 A 3AG 4/5 A 3AG 1/16 A 3AG 1/8 A 3AG 1/4 A 3AG 1-1/2 A 3AG 1-1/4 A 3AG 1.6 A 3AG	Slo-Blo Slo-Blo Fast-Blo Fast-Blo Fast-Blo Fast-Blo Slo-Blo Slo-Blo
			Conne	ctors	
J1 J1 J2 J2 J50	131-0081-00 131-0126-00 131-0081-00 131-0126-00 131-0081-00	B180000 B010100 B180000	B179999 B179999 B179999	1 Contact, female 1 Contact, BNC 1 Contact, female 1 Contact, BNC 1 Contact, female	
J50 J51 J51 J120 J120	131-0126-00 131-0081-00 131-0126-00 131-0081-00 131-0126-00	B180000	B179999 B179999	1 Contact, BNC 1 Contact, female 1 Contact, BNC 1 Contact, female 1 Contact, BNC	
J121 J121 J310 J310 J311	131-0081-00 131-0126-00 131-0081-00 131-0126-00 131-0081-00	B180000 B010100 B180000	B179999 B179999 B179999	1 Contact, female 1 Contact, BNC 1 Contact, female 1 Contact, BNC 1 Contact, female	
J311 J330 J340 J1210 J1210	. 131-0126-00 131-0372-00 131-0372-00 131-0081-00 131-0302-00		B019999 B069999	1 Contact, BNC Coaxial Coaxial 1 Contact, female UHF	
J1210 J1210 J1500 J1620	131-0320-00 131-0274-00 131-0171-00 210-0652-00	B070000 B180000	B179999	UHF BNC Motor Base, 3 wire Eyelet :	

#### Inductors

Ck <b>#</b>	<b>M</b> o.	Tektronix Part No.		Model No. Disc	
L1 L46 L51 L76 L220		*108-0527-00 114-0234-00 *108-0527-00 276-0507-00 *114-0247-00	XB180000 XB180000		100 nH 10-20 μH, Var Core not replaceable 100 nH Core, Ferramic Suppressor 30-85 μH, Var Core 276-0540-00
L22 1 L27 2 L27 9 L33 1 L33 2		*114-0246-00 114-0235-00 114-0235-00 *114-0250-00 *114-0249-00			0.7-1.1 μH, Var Core 276-0506-00 6-12 μH, Var Core not replaceable 6-12 μH, Var Core not replaceable 15-30 μH, Var Core not replaceable 27-60 μH, Var Core not replaceable
L40 1 L40 2 L41 1 L41 2 L453		*108-0360-00 *108-0200-01 *108-0360-00 *108-0200-01 108-0317-00	XB150000 B010100 XB150000 B010100	B149999X B149999X	46 μΗ <b>40 μ</b> Η 46 μΗ <b>40 μ</b> Η 15 μΗ
L45 <b>4</b> L45 <b>5</b> L45 <b>6</b> L45 <b>7</b> L45 <b>7</b>		*108-0443-00 *108-0472-00 108-0249-00 *108-0200-01 *108-0200-00	XB200000 B010100 B240000	B239999	25 μΗ 160 μΗ 12 μΗ 40 μΗ 40 μΗ
L54 <b>5</b> L54 <b>7</b> L54 <b>8</b> L55 <b>6</b> L55 <b>8</b>		114-0209-00 114-0209-00 276-0507-00 *108-0474-00 *108-0111-01	B010100	B239999	28-60 $\mu$ H, Var Core not replaceable 28-60 $\mu$ H, Var Core not replaceable Core, Ferramic Suppressor 2 $\mu$ H 5.5 $\mu$ H
L55 <b>8</b> L55 <b>9</b> L56 <b>6</b> L566 L56 <b>9</b>		*108-0111-00 *120-0286-00 *108-0111-01 *108-0111-00 *108-0474-00	B240000 B010100 B240000	B239999	$5.5~\mu H$ Toroid, <b>2</b> turns, bifilar $5.5~\mu H$ $5.5~\mu H$ $5.5~\mu H$ <b>2</b> $\mu H$
L601 L602 L606 L607 L610		*114-0238-00 *114-0237-00 *114-0238-00 *114-0237-00 *114-0239-00			300-470 μH, Var Core 276-0506-00 120-185 μH, Var Core 276-0506-00 300-470 μH, Var Core 276-0506-00 120-185 μH, Var Core 276-0506-00 6-15 μH, Var Core not replaceable
L611 L612 L613 L614 L615		*114-0240-00 *114-0241-00 *114-0242-00 *114-0243-00 *114-0243-00			14-35 μH, Var Core not replaceable 23-64 μH, Var Core not replaceable 29-80 μH, Var Core not replaceable 40-118 μH, Var Core not replaceable 40-118 μH, Var Core not replaceable
L616 L617 L618 L838 L858		*114-0244-00 *114-0244-00 *114-0245-00 *114-0248-00 *114-0248-00			$50$ -143 $\mu$ H, Var Core not replaceable $50$ -143 $\mu$ H, Var Core not replaceable $80$ -182 $\mu$ H, Var Core not replaceable $500$ -800 $\mu$ H, Var Core 276-0506-00 $\mu$ H, Var Core 276-0506-00
L958 L978 L1420 L1420 L1422		*114-0248-00 *114-0248-00 *108-0020-01 *108-0020-00 *108-0473-00	B010100 B240000	B239999	500-800 μH, Var Core 276-0506-00 500-800 μH, Var Core 276-0506-00 7.1 μH 7.1 μH 150 μH
L1426 L1440 L1470 L1474		*108-0288-00 108-0205-00 *108-0227-00 *108-0295-00			1.2 µH 1 mH Beam Rotator Y-Axis Alignment

## Inductors (cont)

Ckt. No.	Tektronix Part No.	Serial/Mod Eff	del No. Disc		Description
LR150 LR152 LR295 LR295 LR296 LR296	*108-0288-00 *108-0288-00 *108-0111-01 *108-0111-00 *108-0111-01 *108-0111-00	B010100 B240000 B010100 B240000	B239999 B239999	1.2 $\mu$ H (wound or 1.2 $\mu$ H (wound or 5.5 $\mu$ H (wound o	n a 6.2 $\Omega$ resistor) n a 15 $\Omega$ resistor) n a 15 $\Omega$ resistor)
			Transis	tors	
Q30 Q40 Q41 Q80 Q81	151-0188-00 151-0190-00 151-0188-00 *151-0192-00 *151-0192-00			Silicon Silicon Silicon Silicon Silicon	2N3906 2N3904 2N3906 Replaceable by MP3 6521 Replaceable by MPS 6521
Q85 Q90 Q91 Q75 Q140	151-0188-00 *151-0192-00 *151-0192-00 151-0188-00 151-0188-00	,		Silicon Silicon Silicon Silicon Silicon	2N3906 Replaceable by MPS 6521 Replaceable by MPS 6521 2N3906 2N3906
Q141 Q200 Q205 Q220 Q225	151-0190-00 151-0190-00 151-0190-00 151-0190-00 151-0188-00			Silicon Silicon Silicon Silicon Silicon	2N3904 2N3904 2N3904 2N3904 2N3906
Q230 Q230 Q236 Q238 Q250	151-0190-00 *151-0230-00 *151-0230-00 151-0190-00 151-1015-00	B010100 B250000 XB250000 XB250000	B249999	Silicon Silicon Silicon Silicon Silicon	2N3904 Selected from RCA 40235 Selected from RCA 40235 2N3904 FET
Q255 Q260 Q270 Q275 Q280A	*151-0192-00 151-0190-00 151-0190-00 151-0188-00 151-0188-00			Silicon Silicon Silicon Silicon Silicon	Replaceable by MPS 6521 2N3904 2N3904 2N3906 2N3906
Q280B Q285 Q291 Q295 Q320	151-0188-00 *151-0136-00 151-0190-00 *151-0136-00 151-0190-00			Silicon Silicon Silicon Silicon Silicon	2N3906 Replaceable by 2N3053 2N3904 Replaceable by 2N3053 2N3904
Q325 Q340 Q345 Q420 Q421	151-0190-00 151-0190-00 151-0190-00 151-0188-00 151-0190-00			Silicon Silicon Silicon Silicon Silicon	2N3904 2N3904 2N3904 2N3906 2N3904
Q425 Q430 Q432 Q435 Q440	151-0188-00 151-0190-00 151-0190-00 151-0190-00 *151-0192-00	XB150000		Silicon Silicon Silicon Silicon Silicon	2N3906 2N3904 2N3904 2N3904 Replaceable by MPS 6521
Q442 Q445 Q450 Q460 Q470 Q471	151-0190-00 *151-0192-00 151-0188-00 151-0188-00 *151-0198-00 *151-0198-00	XB150000 B010100	B149999	Silicon Silicon Silicon Silicon Silicon Silicon	2N3904 Replaceable by MPS 6521 2N3906 2N3906 Replaceable by MPS 918 Replaceable by MPS 918

## Transistor (cont)

Ckt. No.	Tektronix Part No.	Serial/M Eff	odel No. Disc		Description
Q471	151-0188-00	B150000		Silicon	2N3906
Q480	151-0190-00			Silicon	2N3904
Q490	151-0190-00			Silicon	2N3904
Q491	*151-0195-00			Silicon	Replaceable by MPS 6515
Q495	151-0188-00	•		Silicon	2N3906
Q500A (	*153-0547-00			Cilt	
Q500B \				Silicon	(matched pair) MPS 918
Q505A	*151-0198-00	B010100	B149999	Silicon	Replaceable by MPS 918
Q505B	*151-0198-00	B010100	B149999	Silicon	Replaceable by MPS 918
Q505A { Q505B }	*153-0547-00	B150000		Silicon	(matched pair) MPS 918
Q515	*151-0198-00			Silicon	Replaceable by MPS 918
Q516	*151-0198-00			Silicon	Replaceable by MPS 918
Q530	*151-0198-00			Silicon-	Replaceable by MPS 918
Q540	*151-0192-00			Silicon	Replaceable by MPS 6521
Q550 Q540	151-0190-00			Silicon	2N3904
Q560	151-0190-00			Silicon	2N3904
Q565	*151-0195-00			Silicon	Replaceable by MPS 6515
Q570	151-0190-00			Silicon	2N3904
Q571	151-0190-00			Silicon	2N3904
Q575	151-0190-00			Silicon	2N3904
Q576	151-0190-00			Silicon	2N3904
Q580	151-0188-00			Silicon	2N3906
Q590A ( Q590B	*153-0547-00			Silicon	(matched pair) MPS 918
Q595A Q595 <b>B</b>	*151-0198-00 *151-0198-00	B010100 B010100	B149999 B149999	Silicon Silicon	Replaceable by MPS 918 Replaceable by MPS 918
O505 Å ±	:	·			
Q595A ( Q595B (	*153-0547-00	B150000		Silicon	(matched pair) MPS 918
Q620	*151-0192-00			Silicon	Replaceable by MPS 6521
Q630	*151-0192-00			Silicon	Replaceable by MPS 6521
Q640	*151-0192-00			Silicon	Replaceable by MPS 6521
Q650	*151-0192-00			Silicon	Replaceable by MPS 6521
Q660	151-0190-00			Silicon	2N3904
Q670	151-1005-00			Silicon	FET
Q680	151-0188-00			Silicon	2N3906
Q690	151-0190-00			Silicon	2N3904
Q691	151-0190-00	•		Silicon	2N3904
Q <b>7</b> 00	151-0188-00			Silicon	2N3906
Q710	151-0188-00			Silicon	2N3906
Q720	151-0188-00			Silicon	2N3906
Q <b>7</b> 30	151-0188-00			Silicon	2N3906
Q740	151-0188-00			Silicon	2N3906
<b>Q750</b>	151-0188-00			Silicon	2N3906
2760	151-0188-00			Silicon	2N3906
	151 0100 00			Silicon	
2 <i>7</i> 70 2780	151-0190-00			Silicon	2N3904

#### Transistor (cont)

Ckt. No.	Tektronix Part No.	Serial/Mo Eff	del No. Disc		Description
Q800 Q810 Q820 Q830 Q835	151-0190-00 151-0190-00 151-1005-00 151-0190-00 151-0190-00			Silicon Silicon Silicon Silicon	2N3904 2N3904 FET 2N3904 2N3904
Q836 Q840 Q855 Q856 Q860	151-0169-00 151-0190-00 151-0190-00 151-0169-00 151-0188-00			Silicon Silicon Silicon Silicon Silicon	2N3439 2N3904 2N3904 2N3439 2N3906
Q870A ) Q870B ) Q890 Q900 Q910	*153-0558-00 151-0190-00 151-0190-00 151-0190-00			Silicon Silicon Silicon Silicon	(matched pair) 2N3906 2N3904 2N3904 2N3904
Q920 Q930 Q950 Q955 Q956	151-1005-00 151-0188-00 151-0190-00 151-0190-00 151-0169-00			Silicon Silicon Silicon Silicon Silicon	FET 2N3906 2N3904 2N3904 2N3439
Q960 Q975 Q976 Q980A ) Q980B )	151-0190-00 151-0190-00 151-0169-00 *153-0558-00			Silicon Silicon Silicon	2N3904 2N3904 2N3439 (matched pair) 2N3906
Q1010 Q1100 Q1101 Q1110 Q1115	151-0190-00 151-0188-00 151-0190-00 *151-0192-00 151-0188-00	XB150000		Silicon Silicon Silicon Silicon	2N3904 2N3906 2N3904 Replaceable by MPS 6521 2N3906
Q1120 Q1121 Q1130 Q1140 Q1150	151-0190-00 151-0190-00 151-0190-00 151-0190-00 *151-0126-00	B010100	B149999X	Silicon Silicon Silicon Silicon Silicon	2N3904 2N3904 2N3904 2N3904 Selected from 2N2484
Q1150A,B Q1151 Q1160 Q1161 Q1162	151-1011-00 *151-0126-00 *151-0192-00 *151-0192-00 151-0190-00	XB150000 B010100	B149999X	Silicon Silicon Silicon Silicon Silicon	Dual FET Selected from 2N2484 Replaceable by MPS 6521 Replaceable by MPS 6521 2N3904
Q1170 Q1180 Q1190 Q1200 Q1210	151-0190-00 151-0190-00 *151-0192-00 *151-0192-00 151-0190-00	u <sup>1</sup>		Silicon Silicon Silicon Silicon Silicon	2N3904 2N3904 Replaceable by MPS 6521 Replaceable by MPS 6521 2N3904

# Transistor (cont)

Ckt. No.	Tektronix Part No.	Serial/Model No. Eff Disc	Description
Q1220	151-0150-00	Silicon	2N3440
Q1230	151-0190-00	Silicon	2N3904
Q1250	151-0190-00	Silicon	2N3904
Q1255	151-0190-00	Silicon	2N3904
Q1260	151-0190-00	Silicon	2N3904
Q1265	151-0190-00	Silicon	2N3904
Q1270	151-0188-00	Silicon	2N3906
Q1280	151-0190-00	Silicon	2N3904
Q1285	151-0190-00	Silicon	2N3904
Q1290	151-0190-00	Silicon	2N3904
Q1300	151-0190-00	Silicon	2N3904
Q1400	151-0188-00	Silicon	2N3906
Q1410	*151-0195-00	Silicon	Replaceable by MPS 6515
Q1420	151-0140-00	Silicon	2N3055
Q1510	151-0150-00	Silicon	2N3440
Q1515 Q1520 Q1540 Q1541 Q1545	151-0150-00 151-0149-00 *151-0192-00 *151-0192-00 151-0150-00	Silicon Silicon Silicon Silicon	2N3440 2N3441 Replaceable by MPS 6521 Replaceable by MPS 6521 2N3440
Q1550	151-0149-00	Silicon	2N3441
Q1560	*151-0148-00	Silicon	Selected 40250 (RCA)
Q1570A	*151-0192-00	Silicon	Replaceable by MPS 6521
Q1570B	*151-0192-00	Silicon	Replaceable by MPS 6521
Q1590	*151-0183-00	Silicon	Selected from 2N2192
Q1600	*151-0183-00	Silicon	Selected from 2N2192
Q1610	*151-0195-00	Silicon	Replaceable by MPS 6515
Q1620	*151-0195-00	Silicon	Replaceable by MPS 6515
Q1630	151-0140-00	Silicon	2N3055

#### Resistors

Resistors are fixed, composition,  $\pm 10\%$  unless otherwise indicated.

R2 <sup>3</sup> R3 R4 R5 R13	*312-0648-00 315-0392-00 321-0412-00 315-0103-00 315-0392-00			15 kΩ 3.9 kΩ 191 kΩ 10 kΩ 3.9 kΩ	1/8 W 1/4 W 1/8 W 1/4 W 1/4 W	Prec Prec	1 % 5 % 1 % 5 % 5 %
R14 R14 R17 <sup>3</sup> R18 R33	321-0409-00 321-0410-00 *312-0648-00 321-0306-00 315-0334-00	B010100 B150000	B149999	178 kΩ 182 kΩ 15 kΩ 15 kΩ 330 kΩ	1/8 W 1/8 W 1/8 W 1/8 W 1/4 W	Prec Prec Prec Prec	1% 1% 1% 1% 5%

<sup>3</sup>Matched pair, furnished as a unit.

Resistors (cont)

CIA NI-	Tektronix Part No.	Serial/Mo Eff	odel No. Disc		Descript	rion	
Ckt. No.	1411 140.						
R34	315-0105-00			1 ΜΩ	1/4 W		5%
R36	315-0223-00			22 kΩ	1/4 W		5%
R37	315-0220-00			22 Ω	1/ <sub>4</sub> W		5% 5% 5%
R38	315-0103-00			10 kΩ	1/4 W		5%
R39	315-0101-00			100 Ω	1/₄ W		5%
R40	315-0152-00			1.5 kΩ	¹/₄ W		5%
R42	315-0820-00			82 Ω	¹/₄ W		5%
	315-0331-00			330 Ω	⅓ W		5%
R44	311-0462-00	B010100	B319999	1 kΩ, Var	• •		
R45 R45	311-1225-00	B320000	B017777	1 kΩ, Var			
				<b>2.49</b> kΩ	1/8 ₩	Prec	1%
R46	321-0231-00			2.49 kΩ 2.49 kΩ	1/8 W	Prec	1%
R47	321-0231-00				1/4 W	1166	5%
R48	315-0151-00			150 Ω			5%
R49	315-0751-00			750 Ω	1/₄ W 1/ <sub>8</sub> W	Prec .	1%
R52⁴	*312-0648-00			15 kΩ	78 44	riec .	. 76
R53	315-0392-00			3.9 kΩ	1/ <sub>4</sub> W	_	5%
R54	321-0412-00			191 kΩ	1/ <sub>8</sub> W	Prec	1%
R55	315-0103-00			10 kΩ	1/4 W	_	5%
R60	321-0127-00			205 $\Omega$	1/ <sub>8</sub> W	Prec	1%
R63	315-0392-00			<b>3.9</b> kΩ	⅓ W		5%
D24	321-0409-00	B010100	B149999	178 kΩ	1/ <sub>8</sub> W	Prec	. 1%
R64	321-0410-00	B150000		1 <b>8</b> 2 kΩ	1/ <sub>8</sub> W	Prec	1%
R64	321-0306-00	D133000		15 kΩ	1/ <sub>8</sub> W	Prec	.1 %
R66	*312-0648-00			15 kΩ	1/ <sub>8</sub> W	Prec	1%
R67 <sup>4</sup> R74	315-0470-00			47 Ω	1/₄ W		5%
	21 5 0 470 00			47 Ω .	1/ <sub>4</sub> W		5%
R75	315-0470-00			30.1 kΩ	1/8 W	Prec	19
R80	321-0335-00	•		15 kΩ	1/8 W	Prec	19
R81	321-0306-00		•	1.5 kΩ	⅓ W		5%
R82	301-0152-00			1.5 kΩ	'î W		5%
R84	303-0183-00			10 K22			
R85	315-0390-00	B010100	B149999	39 Ω	1/4 W		<b>5</b> % 5%
R85 .	315-0270-00	B150000		27 Ω	⅓ W		5 °,
R87	301-0152-00			1.5 kΩ	¹/₂ W	Prec	1 %
R88	321-0155-00	B010100	B239999	402 Ω	1/ <sub>8</sub> W	Prec	i
R88	321-0151-00	B240000		365 Ω	¹/ <sub>8</sub> ₩	1160	
R89	315-0152-00			1.5 kΩ	1/₄ W	D., -	5°
R90	321-0335-00			30.1 kΩ	⅓ W	Prec	] °
R91	321-0306-00			15 kΩ	⅓ W	Prec	59
R92	301-0152-00			$1.5 \mathrm{k\Omega}$	1/ <sub>2</sub> W		59
R94	303-0183-00			18 kΩ	1 W		J ,
R95	315-0390-00	B010100	B149999	39 Ω	1/ <sub>4</sub> W		59
R95	315-0270-00	B150000		27 Ω	1/ <sub>4</sub> W		59
R97	301-0152-00			$1.5~\mathrm{k}\Omega$	1/ <sub>2</sub> W	_	59
R98	321-0155-00	B010100	B239999	402 Ω	1/8 W	Prec	19
R98	321-0151-00	B240000		<b>3</b> 65 Ω	1/ <sub>8</sub> W	Prec	19
DOO	315-0152-00			1.5 kΩ	1/ <sub>4</sub> W		5
R99	315-0332-00			3.3 kΩ	1,∕₄ W		5° 5°
R101	315-0332-00			1 ΜΩ	1, ₩		5
R102	313-0103-00						

<sup>&</sup>lt;sup>4</sup>Matched pair, furnished as a unit.

Ckt. No.	Tektronix Part No.	Serial/i Eff	Model No. Disc		D		
		<u> </u>	Disc	<del></del>	Descri	ption	
R105	315-0222-00			$2.2~\mathrm{k}\Omega$	1/4 W		5%
R106	315-0182-00			1.8 kΩ	1/4 W		5%
R109	315-0362-00			3.6 kΩ	1/4 W		5%
R111	315-0222-00			$2.2~\text{k}\Omega$	1/4 W		5%
R112	315-0182-00	•		1.8 kΩ	1/4 W		5% 5% 5% 5% 5%
R114	315-0105-00			1 ΜΩ	1/4 W		5%
R116	315-0332-00			3.3 kΩ	⅓ W		5%
R120 R121	315-0563-00 315-0752-00			56 kΩ	1/ <sub>4</sub> W		5%
R124	315-0392-00	•		7.5 kΩ	1/4 W		5% 5% 5% 5% 5%
				3.9 kΩ	⅓ W		5%
R126	315-0105-00			1 ΜΩ	1/4 W		5% 5% 5%
R128 R130	315-0822-00			8.2 kΩ	1/4 W		5%
R132	315-0392-00 315-0105-00			3.9 kΩ	1/4 W		5%
R134	315-0822-00			1 ΜΩ	1/4 W		5%
R136	315-0682-00			8.2 kΩ	1/4 W		5%
R140	315-0332-00	B010100	B239999	6.8 kΩ 3.3 kΩ	¼ W		5%
R140	321-0252-00	B240000	0237777	3.3 kΩ 4.12 kΩ	¼ W		5%
R141	315-0302-00	524000		3 kΩ	¹/ <sub>8</sub> W ¹/₄ W	Prec	1%
R142	321-0260-00	XB240000		4.99 kΩ	1/ <sub>8</sub> W	Prec	5% 1%
R143	315-0103-00			10 kΩ	1/ <sub>4</sub> W	*****	5%
R144	315-0102-00	XB240000		1 kΩ	1/4 W		5%
R145	315-0100-00			10 Ω	'¼W		5%
R146	315-0153-00			15 kΩ	¹/₄ W		5%
R147	315-0100-00			10 Ω	⅓ W		5%
R148	301-0471-00	B010100	B239999	470 Ω	¹/₂ W		5%
R148	301-0271-00	B240000		$270 \Omega$	¹/₂ W		5%
R149 R201	315-0510-00			51 Ω	⅓ W		5%
R203	315-0222-00 315-0330-00			2.2 kΩ	1/ <sub>4</sub> W		5%
	313-0330-00			33 Ω	¹/₄ W		5%
R205	315-0330-00			33 Ω	1/4 W		5%
R206	315-0152-00			$1.5~\mathrm{k}\Omega$	1/ <sub>4</sub> W		5%
R208	315-0472-00			$4.7~\mathrm{k}\Omega$	1/₄ W		5%
R209	315-0271-00			270 Ω	⅓ W		5%
R210	315-0333-00			33 kΩ	1/ <sub>4</sub> W		5%
R211	315-0103-00			10 kΩ	1/₄ ₩		5%
R216	321-0093-00		a.	90.9 Ω	⅓ W	Prec	1%
R220	315-0101-00	•		100 Ω	⅓ W		5%
R221 R222	315-0151-00			150 Ω	1/4 W		5%
	315-0101-00			100 Ω	⅓ W		5%
R224	301-0433-00			<b>43</b> kΩ	1/ <sub>2</sub> W		5%
R226	315-0682-00			6.8 kΩ	1/ <sub>4</sub> W		5%
R227	321-0289-00	B010100	B189999	10 kΩ	⅓ W	Prec	1%
R227 R228	<b>32</b> 1-02 <b>3</b> 9-00 31 <i>5</i> -0242-00	B190000		3.01 kΩ	1/ <sub>8</sub> W	Prec	1%
5				2.4 kΩ	¹/₄ W		5%
R229	315-0330-00	D010100	DO 10005	33 Ω	1/ <sub>4</sub> W		5%
R231 R231	315-0104-00	B010100	B249999	100 kΩ	1/4 W		5%
R232	<b>321-0391-00</b> 315-0562-00	B250000 B010100	D2/0000	115 kΩ	⅓ W	Prec	1%
R232 R232	321-0265-00	B250000	B249999	5.6 kΩ	1/₄ W	_	5%
				5.62 kΩ	1/ <sub>8</sub> W	Prec	1%
R234	315-0102-00	B010100	B249999X	1 kΩ	1/4 W		5%
R235	317-0101-00	XB280000		100 Ω	⅓ W		5%
R236	315-0330-00			33 Ω	1⁄4 W		5%
							- 70

Ckt. No.	Tektronix Part No.	Serial/Mo Eff	del No. Disc		Descript	ion	
R237 R238 R239 R242 R243 R243	321-0180-00 315-0681-00 321-0280-00 321-1485-00 311-0508-00 311-1234-00	XB250000 XB250000 XB150000 B320000	B319999	732 Ω 680 Ω 8.06 kΩ 1.11 MΩ 50 kΩ, Var 50 kΩ, Var	1/8 W 1/4 W 1/8 W 1/8 W	Prec Prec Prec	1% 5% 1% 1%
R244 R246 R248 R250 R250 R251	321-1485-00 321-0274-00 315-0302-00 311-0463-00 311-1227-00 321-0261-00	XB250000 XB250000 B010100 B320000	B319999	$1.11~\text{M}\Omega$ $6.98~\text{k}\Omega$ $3~\text{k}\Omega$ $5~\text{k}\Omega$ , Var $5~\text{k}\Omega$ , Var $5.11~\text{k}\Omega$	1/8 W 1/8 W 1/4 W	Prec Prec	1 % 1 % 5 %
R252 R254 R255 R255 R256	321-0321-00 316-0336-00 315-0303-00 315-0623-00 315-0104-00	B010100 B150000	B149999	21.5 kΩ 33 MΩ 30 kΩ 62 kΩ 100 kΩ	1/8 W 1/4 W 1/4 W 1/4 W 1/4 W	Prec	1 % 5 % 5 % 5 %
R257 R258 R264 R265 R268	315-0202-00 315-0104-00 315-0473-00 315-0473-00 315-0153-00	XB230000		2 kΩ 100 kΩ 47 kΩ 47 kΩ 15 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5% 5%
R270 R271 R272 R273 R275	315-0103-00 315-0512-00 315-0512-00 315-0101-00 315-0681-00			10 kΩ 5.1 kΩ 5.1 kΩ 100 Ω 680 Ω	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5%
R276 R277 R279 R280A R280B R280C R280D	315-0151-00 315-0510-00 315-0301-00			150 Ω 51 Ω 300 Ω	1/4 W 1/4 W 1/4 W		5% 5% 5%
R282 R283 R287 R289 R290	315-0332-00 315-0152-00 315-0133-00 304-0392-00 304-0153-00			3.3 kΩ 1.5 kΩ 13 kΩ 3.9 kΩ 15 kΩ	1/4 W 1/4 W 1/4 W 1 W 1 W		5% 5% 5%
R292 R294 R297	315-0394-00 315-0332-00 315-0182-00			390 kΩ 3.3 kΩ 1.8 kΩ	1/4 W 1/4 W 1/4 W		5% 5% 5%
R299 <sup>5</sup> R301	315-0752-00			7.5 kΩ	1/ <sub>4</sub> W		5%
R302 R304 R305 R306 R311	315-0103-00 315-0105-00 315-0332-00 315-0392-00 315-0153-00			10 kΩ 1 MΩ 3.3 kΩ 3.9 kΩ 15 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5%
R312 R314 R316 R320 R321	315-0103-00 315-0105-00 315-0392-00 315-0103-00 315-0512-00	Oven Assembl	(*OOE OOGS 03	10 kΩ 1 MΩ 3.9 kΩ 10 kΩ 5.1 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5%

<sup>5</sup>Furnished as a unit with partial Oven Assembly (\*205-0083-01).

Resistors (cont)

Ckt. No.	Tektronix Part No.	Serial/ <i>N</i> Eff	lodel No. Disc	•	Descri	ption	
R <b>3</b> 23 R <b>3</b> 27 R <b>3</b> 29 R <b>3</b> 31 R <b>3</b> 33	301-0182-00 315-0100-00 315-0330-00 321-0220-00 321-0097-00			1.8 kΩ 10 Ω 33 Ω 1.91 kΩ 100 Ω	1/ <sub>2</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>8</sub> W	Prec Prec	5% 5% 5% 1%
R335 R337 R340 R341 R342	311-0169-00 321-0220-00 315-0330-00 315-0303-00 315-0331-00			$100~\Omega,~{ m Var}$ $1.91~{ m k}\Omega$ $33~\Omega$ $30~{ m k}\Omega$ $330~\Omega$	1/8 W 1/4 W 1/4 W 1/4 W	Prec	1% 5% 5% 5%
R3.43 R3.44 R3.45 R3.46 R3.47	315-0682-00 315-0682-00 315-0470-00 315-0330-00 315-0332-00			6.8 kΩ 6.8 kΩ 47 Ω 33 Ω 3.3 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5%
R3 <i>49</i> R3 <i>54</i> <sup>6</sup> R3 <i>58</i> <sup>6</sup> ( R3 <i>64</i> <sup>7</sup> )	315-0470-00			47 Ω	1/4 W		5%
R401 R402 R402 R403 <sup>8</sup> R404	321-0128-00 311-0608-00 311-1079-00 311-0685-00 321-0039-00	B010100 B260000 B010100	B259999 B239999	$\begin{array}{c} 210 \ \Omega \\ 2 \ k\Omega, \ \mbox{Var} \\ 2 \ k\Omega, \ \mbox{Var} \\ 100 \ \Omega, \ \mbox{Var} \\ 24.9 \ \Omega \end{array}$	1/ <sub>8</sub> ₩	Prec	1%
R4O4 R4O5 R4O6 R4O6 R4O7	321-0010-00 321-0160-00 321-0130-00 321-0126-00 321-0135-00	B240000 B010100 B240000	B239999	12.4 Ω 453 Ω 221 Ω 200 Ω 249 Ω	1/8 W 1/8 W 1/8 W 1/8 W 1/8 W	Prec Prec Prec Prec Prec	1% 1% 1% 1%
R409 R411 R412 R412 R413°	321-0253-00 321-0128-00 311-0608-00 311-1079-00 311-0685-00	B010100 B260000	B259999	$4.22~\mathrm{k}\Omega$ $210~\Omega$ $2~\mathrm{k}\Omega$ , Var $2~\mathrm{k}\Omega$ , Var $100~\Omega$ , Var	1/ <sub>8</sub> W 1/ <sub>8</sub> W	Prec Prec	1 % 1 %
R414 R414 R415 R416 R416	321-0039-00 321-0010-00 321-0160-00 321-0130-00 321-0126-00	B010100 B240000 B010100 B240000	B239999 B239999	24.9 Ω 12.4 Ω 453 Ω 221 Ω 200 Ω	1/8 W 1/8 W 1/8 W 1/8 W 1/8 W	Prec Prec Prec Prec Prec	1 % 1 % 1 % 1 % 1 %
R417 R419 R420 R421	321-0135-00 321-0253-00 315-0472-00 315-0132-00			249 Ω 4.22 kΩ 4.7 kΩ 1.3 kΩ	1/8 W 1/8 W 1/4 W 1/4 W	Prec Prec	1% 1% 5% 5%

<sup>&</sup>lt;sup>6</sup>Furnished as a unit with CH A Goniometer (\*119-0133-00).

<sup>&</sup>lt;sup>7</sup>Furnished as a unit with CH B Goniometer (\*119-0133-00).

<sup>\*</sup>Furnished as a unit with SW403.

PFurnished as a unit with SW413.

Cla No	Tektronix Part No.	Serial/Mod Eff	lel No. Disc		Descript	ion	
Ckt. No.	run 140.	L11					
R422	315-0153-00			15 kΩ	1/4 W		5% 5%
R423	315-0153-00			15 kΩ	1/4 W	_	5%
R424	321-0239-00			3.01 kΩ	1/8 W	Prec	1%
R425	315-0472-00			4.7 kΩ	1/ <sub>4</sub> W		5%
R426	315-0132-00			1.3 kΩ	1/ <sub>4</sub> W		5%
R427	315-0472-00			4.7 kΩ	1/ <sub>4</sub> W		5%
R428	315-0122-00			1.2 kΩ	¼ W		5%
R429	321-0239-00	_		3.01 kΩ	⅓ W	Prec	1%
R431	315-0562-00			5.6 kΩ	"∕₄ W		5%
R432	315-0103-00			10 kΩ	1/4 W		5%
D (00	321-0224-00	XB150000		<b>2</b> .1 kΩ	¹/8 W	Prec	1%
R433	321-0224-00	XB150000		2.1 kΩ 2.1 kΩ	1/8 ₩	Prec	1%
R434	321-0224-00 315-0562-00	VP120000		5.6 kΩ	1/4 W		5%
R435	315-0302-00			10 kΩ	1∕⁄₄ W		5%
R436 R437	315-0105-00	XB150000		1 ΜΩ	1/4 W		5%
							F 9/
R438	315-0472-00	XB150000		$4.7 k\Omega$	1/₄ W		5%
R439	315-0682-00	XB150000		6.8 kΩ	1/ <sub>4</sub> W		5%
R440	315-0101-00			100 Ω	1/₄ W		5%
R441	321-0224-00	XB150000		2.1 kΩ	⅓ W	Prec	1%
R442	321-0253-00	B010100	B149999	4.22 kΩ	1/8 ₩	Prec	1%
R442	321-0224-00	B150000		2.1 kΩ	1/8 W	Prec	1%
R443	315-0222-00			2.2 kΩ	⅓ W	_	5%
R444	321-0253-00			4.22 kΩ	1/ <sub>8</sub> W	Prec	1%
R445	315-0105-00	XB150000		1 MΩ	1/ <sub>4</sub> W		5% 5%
R446	315-0152-00	B010100	B149999	1.5 kΩ	1/4 W		5 /6
<b>R44</b> 6	301-0152-00	B150000		1.5 kΩ	1/ <sub>2</sub> W		5%
R447	315-0472-00	XB150000	•	$4.7~\mathrm{k}\Omega$	1/ <sub>4</sub> W		5%
R448	303-0183-00			18 kΩ	1 W		5%
R449	315-0470-00	B010100	B149999	47 Ω	1/ <sub>4</sub> W		5%
R449	315-0682-00	B150000		6.8 kΩ	1/ <sub>4</sub> W		5%
P450	315-0101-00	XB150000		100 Ω	1/ <sub>4</sub> W		5%
R450 R452	321-0193-00	ABIOODO		1 kΩ	¹/ <sub>8</sub> ₩	Prec	1%
R453	321-0164-00			499 Ω	1/ <sub>8</sub> W	Prec	1%
R455	321-0164-00			499 Ω	1/8 W	Prec	1%
R461	315-0152-00			$1.5  \mathrm{k}\Omega$	¹/₄ W		5%
D.4.42	315-0203-00	B010100	B149999	<b>20</b> kΩ	1/4 W		5%
R463	315-0203-00	B150000	017///	33 kΩ	1/4 W		5%
R463	315-0393-00	1.50000		39 kΩ	1/4 W		5%
R465 R470	315-0393-00			30 kΩ	1/4 W		5%
R470 R471	315-0303-00			2.2 kΩ	1/4 W		5%
R471 R472	315-0430-00	XB150000		43 Ω	⅓ W		5%
D 170	001 0070 00	DO10100	B149999	7.87 kΩ	⅓ W	Prec	1%
R473	321-0279-00	B010100	D147777	6.2 kΩ	1/4 W		5%
R473	315-0622-00	B150000 B010100	B199999	2.21 kΩ	'/ <sub>8</sub> ₩	Prec	1%
R474	321-0226-00 321-0224-00	B200000	B239999	2.1 kΩ	⅓ W	Prec	1 %
R474	321-0219-00	B240000	520,777	1.87 kΩ	1/8 W	Prec	1%
R474 R475	315-0511-00	B010100	B149999X	510 Ω	1,∕₄ W		5%
K47 D	313-0311-00	201,0100			• •		

Ckt. No.	Tektronix Part No.	Serial/Mo Eff	odel No. Disc		Descrip	ation	
			2130		Descri		
R476	315-0271-00	XB150000		270 Ω	1/4 W		5%
R482	315-0242-00			$2.4~\mathrm{k}\Omega$	1/4 W		5%
R484	315-0472-00			4.7 kΩ	¼ W		5% 5%
R485	315-0751-00			750 Ω	1/4 W		5%
R486	315-0512-00	,		5.1 kΩ	1/ <sub>4</sub> W 1/ <sub>4</sub> W	•	5%
R488	315-0242-00			2.4 kΩ	1/4 W		5%
R489	315-0222-00	XB260000		2.2 kΩ	1/4 W		5%
R490	315-0101-00	B010100	B259999	$100\Omega$	ŴW		5%
R490	315-0221-00	B260000		$220 \Omega$	⅓ W ⅓ W		5%
R491	315-0102-00			1 kΩ	1/4 W		5%
R492	315-0472-00			4.7 kΩ	1/4 W		5%
R493	315-0331-00			$330 \Omega$	1/4 W		5%
R494	315-0471-00			470 Ω	1/₄ W		5%
R495	315-0911-00	B010100	B149999	910 Ω	¼ W		5%
R495	315-0561-00	B150000		560 Ω	1/ <sub>4</sub> W		5%
R496	315-0224-00			<b>220</b> kΩ	1/4 W		5%
R497	315-0223-00			<b>22</b> kΩ	⅓ W		5%
R498	311-0614-00			30 kΩ, Var			
R500	321-0187-00			866 Ω	1/8 ₩	Prec	1%
R501	311-0607-00		•	10 k $\Omega$ , Var			
R502	321-0229-00			2.37 kΩ	1/8 W	Prec	1%
R503	315-0223-00			22 kΩ	1/4 W		5%
R504	321-0170-00	B010100	B149999	576 Ω	1/8 W	Prec	1%
R504	321-0135-00	B150000		249 Ω	¹/ <sub>8</sub> ₩	Prec	1%
R505	315-0153-00			15 kΩ	1/ <sub>4</sub> W		5%
R506	321-0216-00	B010100	B149999	1.74 kΩ	1/ <sub>8</sub> ₩	Prec	1%
R506	321-0192-00	B150000		976 Ω	⅓ W	Prec	1%
R508	321-0216-00	B010100	B149999	1.74 kΩ	1/ <sub>8</sub> W 1/ <sub>8</sub> W	Prec	1%
R508	321-0192-00	B150000		976 Ω	⅓ W	Prec	1%
R509	315-0153-00			15 kΩ	1/ <sub>4</sub> W	•	5%
R511	315-0183-00	B010100	B149999	18 kΩ	1/4 W		5%
R511	315-0153-00	B150000		15 kΩ	1/ <sub>4</sub> W		5%
R512	315-0272-00			2.7 kΩ	1/4 W		5%
R515 R516	315-0822-00 315-0471-00			8.2 kΩ 470 Ω	1/ <sub>4</sub> W 1/ <sub>4</sub> W		5% 5%
.,,,,	0,00,00			47 0 12	/4 **		J / <sub>0</sub>
R517	315-0822-00			8.2 kΩ	1/4 W		5%
R518	315-0471-00			470 Ω	1/4 W		5%
R519	315-0822-00			8.2 kΩ	1/ <sub>4</sub> W		5%
R521	315-0562-00	•		5.6 kΩ	1/4 W		5%
R525	315-0562-00			5.6 kΩ	⅓ W		5%
R527	315-0752-00			7.5 kΩ	1/ <sub>4</sub> W		5%
R528	315-0622-00			6.2 kΩ	1/4 W		5%
R529	315-0682-00			6.8 kΩ	1/4 W		5%
R530	315-0513-00			51 kΩ	1/4 W		5%
R532	315-0202-00			2 kΩ	¹/₄ W		5%
R533	315-0202-00			2 kΩ	1/4 W		5% 5%
	315-0152-00				/4 11		J /n

Ckt. No.	Tektronix Part No.	Serial/M Eff	odel No. Disc		Descrip	tion	
R540 R541 R543 R543 R545	315-0473-00 315-0103-00 315-0242-00 315-0302-00 315-0153-00	B010100 B150000	B149999	47 kΩ 10 kΩ 2.4 kΩ 3 kΩ 15 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5%
R546 R546 R550 R551 R552	315-0152-00 315-0272-00 315-0220-00 315-0272-00 315-0152-00	B010100 B150000	B149999	1.5 kΩ 2.7 kΩ 22 Ω 2.7 kΩ 1.5 kΩ	1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W		5% 5% 5% 5% 5%
R553 R554 R555 R556 R557	315-0470-00 315-0104-00 315-0220-00 315-0911-00 315-0132-00			47 Ω 100 kΩ <b>22</b> Ω 910 Ω 1.3 kΩ	1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W		5% 5% 5% 5%
R560 R562 R564 R566 R568	315-0331-00 315-0472-00 315-0471-00 315-0202-00 315-0220-00			330 Ω 4.7 kΩ 470 Ω 2 kΩ 22 Ω	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5% 5%
R570 R572 R574 R575 R576	301-0303-00 315-0152-00 315-0152-00 301-0303-00 315-0113-00			30 kΩ 1.5 kΩ 1.5 kΩ 30 kΩ 11 kΩ	1/ <sub>2</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>2</sub> W 1/ <sub>4</sub> W		5% 5% 5% 5% 5%
R577 R578 R579 R580 R582	315-0392-00 315-0562-00 315-0222-00 315-0103-00 321-0212-00	B010100	B289999	3.9 kΩ 5.6 kΩ 2.2 kΩ 10 kΩ 1.58 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/8 W	Prec	5% 5% 5% 5% 1%
R582 R583 R583 R585 R586 R587	321-0216-00 311-0634-00 311-0605-00 321-0175-00 321-0175-00 315-0104-00	B290000 B010100 B290000	B289999	1.74 kΩ 500 Ω, Var 200 Ω, Var 649 Ω 649 Ω 100 kΩ	1/8 W 1/8 W 1/8 W 1/4 W	Prec Prec Prec	1% 1% 1% 5%
R588 R590 R592 R594 R594	311-0361-00 321-0187-00 321-0225-00 321-0170-00 321-0135-00	B010100 B150000	B149999	500 kΩ, Var 866 Ω 2.15 kΩ 576 Ω 249 Ω	1/8 W 1/8 W 1/8 W 1/8 W	Prec Prec Prec Prec	1% 1% 1% 1%
R595 R596 R596 R598 R598 R599	315-0153-00 321-0216-00 321-0192-00 321-0216-00 321-0192-00 315-0153-00	B010100 B150000 B010100 B150000	B149999 B149999	15 kΩ 1.74 kΩ 976 Ω 1.74 kΩ 976 Ω 15 kΩ	1/4 W 1/8 W 1/8 W 1/8 W 1/4 W	Prec Prec Prec Prec	5% 1% 1% 1% 1% 5%

Ckt	<b>N</b> o.	Tektronix Part No.	Serial/M Eff	odel No. Disc		Descri		
CKI.	140.	1411 140.		Disc		Descri	prion	
R608		307-0103-00			2.7 Ω	1/ <sub>4</sub> W		5%
R609		315-0100-00			10 Ω	1/4 W		5% 5%
R621		321-0193-00			1 kΩ	1∕8 W	Prec	1%
R622	•	315-0470-00			47 Ω	1/4 W		1 % 5%
R624		311-0510-00	B010100	B319999	10 kΩ, Var	,-		<b>9</b> 70
R624		311-1228-00	B320000		10 kΩ, Var			
R625		315-0183-00			18 kΩ	1/4 W		5%
R626		311-0496-00	B010100	B319999	$2.5 \ k\Omega$ , Var			
R626		311-1226-00	B320000		$2.5 \text{ k}\Omega$ , Var		·	
R627		321-0284-00			8.87 kΩ	⅓ W	Prec	1%
R630		315-0683-00			68 kΩ	⅓ W		5% 5%
R632		315-0153-00			15 kΩ	1/ <sub>4</sub> W		5%
R633		315-0753-00			<b>7</b> 5 kΩ	⅓ W		5%
R635		315-0101-00			100 Ω	⅓ W		5% 5%
R637		315-0152-00			1.5 kΩ	1,∕₄ W		5%
R641		321-0193-00			1 kΩ	1/8 W	Prec	1%
R642		315-0470-00	2010100		47 Ω	1/4 W		5% 1% 5%
R644		311-0510-00	B010100	B319999	10 kΩ, Var			
R644		311-1228-00	B320000		10 kΩ, Var			
R645		315-0183-00			18 kΩ	1/4 W		5%
R64 <b>6</b>		311-0496-00	B010100	B319999	$2.5 \ k\Omega$ , Var			- 70
<b>R</b> 646		311-1226-00	B320000		2.5 kΩ, Var			
R647		321-0283-00			8.66 kΩ	¹/ <sub>8</sub> ₩	Prec	1%
R648		311-0486-00			500 Ω, Var			
R650		315-0683-00			68 kΩ	1/4 W		5%
R652		315-0153-00			$15  \mathrm{k}\Omega$	1∕₄ W		5% 5%
R653		315-0753-00			75 kΩ	1/4 W		5%
R655		315-0101-00			100 Ω	1⁄⁄₄ W		5%
R657		315-0152-00			1.5 kΩ	1/4 W	•	5%
R660		315-0102-00			1 kΩ	1/ <sub>4</sub> W		5%
R661		315-0100-00			10 Ω	ί⁄₄ ₩		5%
R662		315-0101-00			100 Ω	⅓ W		5%
R664		315-0302-00			<b>3</b> kΩ	⅓ W		5%
R671		315-0623-00			<b>62</b> kΩ	1/4 W		5%
R672		311-0465-00	B010100	B319999	100 kΩ, <b>V</b> ar			
R672	•	311-1235-00	B320000		100 kΩ, Var			
R673		301-0333-00		•	<b>3</b> 3 kΩ	¹/₂ W		5%
R676		321-0164-00			499 Ω	⅓ W	Prec	1%
R678		321-0121-00			178 Ω	1/8 W	Prec	1%
R682		315-0472-00			4.7 kΩ	1/4 W		5%
R684		315-0820-00			82 Ω	1/ <sub>4</sub> W		5%
R68510	1	311-0656-00	B010100	B259999	5 kΩ, Var	/4 . *		<i>→</i> /0
R68510		311-1080-00	B260000		5 kΩ, Var		•	
R686		321-0175-00	•		649 Ω	⅓ W	Prec	1%
R687		321-0137-00			261 Ω	⅓ <sub>8</sub> W	Prec	1%
R688		321-0184-00			806 Ω	⅓ W	Prec	1%
R690		315-0471-00	XB150000		470 Ω	¹/₄ W		5%
R691		315-0511-00			510 Ω	¹/₄ W		5%
R692		315-0102-00			1 kΩ	1/ <sub>4</sub> W		5%
R693		315-0153-00	XB150000		15 kΩ	1/ <sub>4</sub> W		5%
R694		321-0239-00			3.01 kΩ	Sele	cted (nominal value)	
10Eni	chad as a .	init with SWAS						

Resistors (cont)

Ckt. No.	Tektronix Part No.	Serial/Mo Eff	del No. Disc	Description				
R695 R697 R698 R702 R703	315-0222-00 315-0682-00 315-0123-00 315-0303-00 315-0303-00			2.2 kΩ 6.8 kΩ 12 kΩ 30 kΩ 30 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5% 5%	
R705 <sup>11</sup> R706 R712 R713 R715 <sup>11</sup>	*312-0647-00 321-0277-00 315-0303-00 315-0303-00 *312-0647-00			4.99 kΩ 7.5 kΩ 30 kΩ 30 kΩ 4.99 kΩ	1/8 W 1/8 W 1/4 W 1/4 W 1/4 W	Prec Prec Prec	1% 1% 5% 5% 1%	
R716 R718 R722 R723 R725 <sup>11</sup>	321-0277-00 321-0283-00 315-0303-00 315-0303-00 *312-0647-00	·		7.5 kΩ 8.66 kΩ 30 kΩ 30 kΩ. 4.99 kΩ	1/8 W 1/8 W 1/4 W 1/4 W 1/8 W	Prec Prec	1 % 1 % 5 % 5 % 1 %	
R726 R728 R732 R733 R735 <sup>11</sup>	321-0277-00 321-0259-00 315-0303-00 315-0303-00 *312-0647-00			7.5 kΩ 4.87 kΩ 30 kΩ 30 kΩ 4.99 kΩ	1/8 W 1/8 W 1/4 W 1/4 W 1/8 W	Prec Prec	1% 1% 5% 5% 1%	
R736 R742 R743 R745 R746	321-0277-00 315-0303-00 315-0303-00 321-0260-00 321-0277-00			7.5 kΩ 30 kΩ 30 kΩ 4.99 kΩ 7.5 kΩ	1/8 W 1/4 W 1/4 W 1/8 W 1/8 W	Prec Prec Prec	1% 5% 5% 1% 1%	
R752 R753 R755 R756 R762 R763	315-0303-00 315-0303-00 321-0260-00 321-0277-00 315-0303-00 315-0303-00			30 kΩ 30 kΩ 4.99 kΩ 7.5 kΩ 30 kΩ 30 kΩ	1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>8</sub> W 1/ <sub>8</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W	Prec Prec	5% 5% 1% 1% 5%	
R765 R765 R765 R765 R766 R770	321-0178-00 321-0193-00 321-0191-00 321-0192-00 321-0277-00 321-0244-00	B010100 B150000 B190000 B240000	B149999 B189999 B239999	698 Ω 1 kΩ 953 Ω 976 Ω 7.5 kΩ 3.4 kΩ	1/8 W 1/8 W 1/8 W 1/8 W 1/8 W	Prec Prec	ominal value) 1% 1% ominal value) 1%	
R771 R773 R775 R778 R782	321-0262-01 315-0683-00 315-0912-00 315-0474-00 321-0194-00			5.23 kΩ 68 kΩ 9.1 kΩ 470 kΩ 1.02 kΩ	1/8 W 1/4 W 1/4 W 1/4 W 1/8 W	Prec Prec	½% 5% 5% 5% 1%	
R784 R786 R788 R806 R807	315-0472-00 321-0260-00 323-0356-00 315-0124-00 315-0243-00		furnished as a	4.7 kΩ 4.99 kΩ 49.9 kΩ 120 kΩ 24 kΩ	1/4 W 1/8 W 1/2 W 1/4 W 1/4 W	Prec Prec	5% 1% 1% 5% 5%	

Ckt. No.	Tektronix Part No.	Serial/Mo Eff	odel No. Disc		Descrip	tion	
R809 R813 R816 R817 R822	315-0275-00 315-0153-00 315-0124-00 315-0243-00 315-0104-00			2.7 ΜΩ 15 kΩ 120 kΩ 24 kΩ 100 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5% 5%
R826 R830 R830 R832 R834	315-0153-00 <b>321-025</b> 1-00 321-0247-00 301-0363-00 315-0362-00	B010100 B030000	B029999	15 kΩ 4.02 kΩ 3.65 kΩ 36 kΩ 3.6 kΩ	1/ <sub>4</sub> W 1/ <sub>8</sub> W 1/ <sub>8</sub> W 1/ <sub>2</sub> W 1/ <sub>4</sub> W	Prec Prec	5% 1% 1% 5% 5%
R835 R837 R838 R840 R841	315-0153-00 308-0461-00 315-0912-00 321-0193-00 321-0235-00			15 kΩ 16 kΩ 9.1 kΩ 1 kΩ 2.74 kΩ	1/4 W 4 W 1/4 W 1/8 W 1/8 W	WW Prec Prec	5% 1% 5% 1%
R843 R843 R846 R846 R847 R847	323-0176-00 323-0164-00 321-0116-00 321-0116-00 321-0126-00	B010100 B150000 B010100 B150000 B010100 B150000	B149999 B149999 B149999	665 Ω 499 Ω 158 Ω 118 Ω 158 Ω	1/ <sub>2</sub> W 1/ <sub>2</sub> W 1/ <sub>8</sub> W 1/ <sub>8</sub> W 1/ <sub>8</sub> W	Prec Prec Prec Prec Prec	1% 1% 1% 1% 1%
R848 R848 R849 R849 R855 R857	311-0496-00 311-1226-00 311-0480-00 311-1224-00 303-0183-00 308-0461-00	B010100 B320000 B010100 B320000 XB150000	B319999 B319999	2.5 kΩ, Var 500 Ω, Var 500 Ω, Var 500 Ω, Var 18 kΩ 16 kΩ	1 W 4 W	ww	<b>5%</b> 1%
R858 R860A ) R860B ) R861 R862	315-0912-00 311-0694-00 315-0474-00 315-0155-00			9.1 kΩ 50 kΩ, Var 10 kΩ, Var 470 kΩ 1.5 MΩ	1/4 W 1/4 W 1/4 W		5% 5% 5%
R863 R864 R865 R867 R868	315-0335-00 315-0223-00 315-0753-00 315-0204-00 315-0114-00			3.3 ΜΩ 22 kΩ 75 kΩ 200 kΩ 110 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5% 5%
R873 R874 R875 R875 R876	321-0334-00 315-0563-00 311-0463-00 311-1227-00 323-0414-00	B010100 B320000	B319999	29.4 k $\Omega$ 56 k $\Omega$ 5 k $\Omega$ , Var 5 k $\Omega$ , Var 200 k $\Omega$	1/8 W 1/4 W	Prec Prec	1 % 5 %
R877	315-0392-00	٠.		3.9 kΩ 5.23 kΩ	1⁄ <sub>4</sub> ₩	Prec	5%
R878 R880 R881 R883 R884	321-0262-01 311-0329-00 315-0474-00 321-0331-00 315-0563-00			5.23 kΩ 50 kΩ, Var 470 kΩ 27.4 kΩ 56 kΩ	1/4 W 1/8 W 1/4 W	Prec	½% 5% 1% 5%

Ckt. No.	Tektronix Part No.	Serial/M Eff	odel No. Disc		Descrip	tion	
R886 R887 R889 R890 R892	323-0414-00 315-0392-00 323-0354-00 321-0203-00 321-0181-00			200 kΩ 3.9 kΩ 47.5 kΩ 1.27 kΩ 750 Ω	1/ <sub>2</sub> W 1/ <sub>4</sub> W 1/ <sub>2</sub> W 1/ <sub>8</sub> W 1/ <sub>8</sub> W	Prec Prec Prec Prec	1% 5% 1% 1%
R896 R901 R902 R903 R904	315-0102-00 315-0103-00 315-0622-00 315-0393-00 315-0333-00			1 kΩ 10 kΩ 6.2 kΩ 39 kΩ 33 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W	•	5% 5% 5% 5%
R905 R905 R906 R907 R909 R912	311-0510-00 311-1228-00 315-0124-00 315-0243-00 315-0275-00 315-0103-00	B010100 B320000	B319999	$10~\mathrm{k}\Omega,~\mathrm{Var}$ $10~\mathrm{k}\Omega,~\mathrm{Var}$ $120~\mathrm{k}\Omega$ $24~\mathrm{k}\Omega$ $2.7~\mathrm{M}\Omega$ $10~\mathrm{k}\Omega$	1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5%
R913 R915 R916 R917 R922	315-0512-00 315-0153-00 315-0124-00 315-0243-00 315-0104-00			5.1 kΩ 15 kΩ 120 kΩ 24 kΩ 100 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5% 5%
R926 R930 R932 R934 R936	315-0153-00 315-0102-00 315-0224-00 321-0277-00 315-0303-00			15 kΩ 1 kΩ 220 kΩ 7.5 kΩ 30 kΩ	1/4 W 1/4 W 1/4 W 1/8 W 1/4 W	Prec	5% 5% 5% 1% 5%
R937 R939 R940 R944 R946	315-0303-00 321-0277-00 321-0368-00 321-0260-00 323-0356-00			30 kΩ 7.5 kΩ 66.5 kΩ 4.99 kΩ 49.9 kΩ	1/4 W 1/8 W 1/8 W 1/8 W 1/2 W	Prec Prec Prec Prec	5% 1% 1% 1% 1%
R950 R950 R952 R954 R955	321-0251-00 321-0247-00 301-0363-00 315-0362-00 315-0153-00	B010100 B030000	B029999	4.02 kΩ 3.65 kΩ 36 kΩ 3.6 kΩ 15 kΩ	1/8 W 1/8 W 1/2 W 1/4 W 1/4 W	Prec Prec	1% 1% 5% 5% 5%
R957 R958 R960 R961 R963	308-0461-00 315-0912-00 321-0193-00 321-0235-00 323-0176-00	B010100	B149999	16 kΩ 9.1 kΩ 1 kΩ <b>2.74</b> kΩ <b>665</b> Ω	4 W 1/ <sub>4</sub> W 1/ <sub>8</sub> W 1/ <sub>8</sub> W 1/ <sub>2</sub> W	WW Prec Prec Prec	1 % 5 % 1 % 1 % 1 %
R963 <b>R966</b> R966 <b>R967</b> R967	323-0164-00 321-0116-00 321-0104-00 321-0116-00 321-0126-00	B150000 B010100 B150000 B010100 B150000	B149999 B149999	499 Ω 158 Ω 118 Ω 158 Ω 200 Ω	½ W ⅓8 W ⅓8 W ⅓8 W ⅓8 W	Prec Prec Prec Prec Prec	1% 1% 1% 1%

Ckt. No.	Tektronix Part No.	Serial/Mo Eff	odel No. Disc		Descrip	tion	
R968 R968 R969 R969 R975	311-0496-00 311-1226-00 311-0480-00 311-1224-00 303-0183-00 308-0461-00	B010100 B320000 B010100 B320000 XB150000	B319999 B319999	2.5 k $\Omega$ , Var 2.5 k $\Omega$ , Var 500 $\Omega$ , Var 500 $\Omega$ , Var 18 k $\Omega$ 16 k $\Omega$	1 W 4 W	ww	5% 1%
R978 R980A R980B R981 R982	315-0912-00 311-0694-00 315-0623-00 315-0244-00			9.1 k $\Omega$ 10 k $\Omega$ , Var 50 k $\Omega$ , Var 62 k $\Omega$ 240 k $\Omega$	1/4 W 1/4 W 1/4 W		5% 5% 5%
R983 R984 R985 R985 R986 R987	321-0334-00 315-0563-00 311-0463-00 311-1227-00 323-0414-00 315-0392-00	B010100 B320000	B319999	29.4 kΩ 56 kΩ 5 kΩ, Var 5 kΩ, Var 200 kΩ 3.9 kΩ	1/ <sub>8</sub> W 1/ <sub>4</sub> W 1/ <sub>2</sub> W 1/ <sub>4</sub> W	Prec Prec	1 % 5 % 1 % 5 %
R988 R993 R994 R996 R997 R999	321-0260-00 321-0330-00 315-0563-00 323-0414-00 315-0392-00 323-0354-0			4.99 kΩ 26.7 kΩ 56 kΩ 200 kΩ 3.9 kΩ 47.5 kΩ	1/8 W 1/8 W 1/4 W 1/2 W 1/4 W 1/2 W	Prec Prec Prec	1% 1% 5% 1% 5%
R1000 R1002 R1012 R1016 R1017	315-0474-00 311-0329-00 315-0224-00 315-0104-00 315-0303-00			470 kΩ 50 kΩ, Var 220 kΩ 100 kΩ 30 kΩ	1/ <sub>4</sub> W	Trec	5% <b>5%</b> 5% 5%
R1101 R1102 R1103 R1105 R1108	315-0243-00 315-0222-00 315-0104-00 315-0682-00 315-0274-00			24 kΩ 2.2 kΩ 100 kΩ 6.8 kΩ 270 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5%
R1110 R1111 R1112 R1114 R1116	301-0333-00 315-0471-00 301-0333-00 315-0433-00 315-0243-00	XB150000		33 kΩ 470 Ω 33 kΩ 43 kΩ 24 kΩ	1/2 W 1/4 W 1/2 W 1/4 W 1/4 W		5% 5% 5% 5% 5%
R1118 R1120 R1122 R1124 R1126	315-0822-00 315-0273-00 315-0821-00 315-0472-00 315-0302-00			8.2 kΩ 27 kΩ 820 Ω 4.7 kΩ 3 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5% 5%
R1127 R1128 R1129 R1131 R1133	315-0103-00 315-0182-00 315-0133-00 315-0100-00 315-0513-00			10 kΩ 1.8 kΩ 13 kΩ 10 Ω 51 kΩ	1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W		5% 5% 5% 5%

Ckt. No.	Tektronix Part No.	Serial/M Eff	odel No. Disc		Descript	ion	
R1134 R1135 R1138 R1140 R1141	315-0751-00 315-0333-00 315-0682-00 315-0100-00 315-0470-00			750 Ω 33 kΩ 6.8 kΩ 10 Ω 47 Ω	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5% 5%
R1142 R1143 R1145 R1150 R1150	315-0101-00 315-0224-00 315-0104-00 315-0204-00 315-0473-00	B010100 B010100 B150000	B149999X B149999	100 Ω <b>220</b> kΩ 100 kΩ 200 kΩ 47 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5%
R1151 R1151 R1152 R1152 R1153	315-0106-00 315-0154-00 315-0243-00 315-0823-00 315-0241-00	B010100 B150000 B010100 B150000	B149999 B149999	10 ΜΩ 150 kΩ 24 kΩ 82 kΩ <b>240</b> kΩ	1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W		5% 5% 5% 5%
R1154 R1155 R1156 R1156 R1157	315-0333-00 321-0289-00 321-0363-00 321-0335-00 321-0332-00	XB150000 B010100 B150000 B010100	B149999 B149999	33 kΩ 10 kΩ 59 kΩ 30.1 kΩ 28 kΩ	1/4 W 1/8 W 1/8 W 1/8 W 1/8 W	Prec Prec Prec Prec	5% 1% 1% . 1%
R1157 R1158 R1159 R1159 R1160	321-0353-00 311-0170-00 321-0350-00 317-0107-00 321-0696-00	B150000 B010100 B150000	B149999	$46.4 \text{ k}\Omega$ $20 \text{ k}\Omega$ , $\text{Var}$ $43.2 \text{ k}\Omega$ $100 \text{ M}\Omega$ $40.2 \text{ k}\Omega$	1/8 W 1/8 W 1/8 W 1/8 W	Prec Prec Prec	1% 1% 5% <b>½</b> %
R1161 R1162 R1163 R1164 R1165	321-0677-00 315-0151-00 321-0258-00 321-0289-00 321-0391-00	XB150000		<b>30.4</b> kΩ 150 Ω 4.75 kΩ 10 kΩ 115 kΩ	1/8 W 1/4 W 1/8 W 1/8 W 1/8 W	Prec Prec Prec Prec	72% 5% 1% 1%
R1166 R1167 R1168 R1169 R1172	315-0331-00 321-0258-00 301-0102-00 315-0332-00 315-0100-00	,		330 Ω 4.75 kΩ 1 kΩ 3.3 kΩ 10 Ω	1/4 W 1/8 W 1/2 W 1/4 W 1/4 W	Prec	5% 1% 5% 5% 5%
R1174 R1176 R1180 R1184 R1186	315-0392-00 315-0103-00 315-0223-00 315-0222-00 315-0183-00			3.9 kΩ 10 kΩ 22 kΩ 2.2 kΩ 18 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W		5% 5% 5% 5% 5%
R1188 R1190 R1190 R1192 R1194	315-0272-00 321-0353-01 321-0345-00 315-0470-00 301-0473-00	B010100 B150000	B149999	2.7 kΩ 46.4 kΩ 38.3 kΩ 47 Ω 47 kΩ	1/4 W 1/8 W 1/8 W 1/4 W 1/2 W	Prec Prec	5% ½% 1% 5% 5%

Ckt. No.	Tektronix Part No.	Serial/ <i>N</i> Eff	Aodel No. Disc		Description	
R1196 R1198 R1201 R1203 R1204	315-0362-00 315-0391-00 315-0100-00 304-0152-00 <b>315-0222-0</b> 0			3.6 kΩ 390 Ω 10 Ω 1.5 kΩ 2.2 kΩ	1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1 W 1/ <sub>4</sub> W	5% 5% 5% 5%
R1206 R1208 R1209 R1212 R1213	315-0562-00 315-0103-00 315-0472-00 315-0223-00 315-0103-00	XB150000		5.6 kΩ 10 kΩ 4.7 kΩ 22 kΩ 10 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W	5% 5% 5% 5% 5%
R1216 R1218 R1220 R1222 R1224	315-0472-00 315-0103-00 315-0472-00 315-0332-00 305-0223-00			4.7 kΩ 10 kΩ 4.7 kΩ 3.3 kΩ 22 kΩ	'/4 W '/4 W '/4 W '/4 W 2 W	5% 5% 5% 5%
R1225 R1227 R1228 R1228	305-0223-00 315-0473-00 311-0465-00 311-1235-00	B010100 B320000	B319999	22 kΩ 47 kΩ 100 kΩ, Var	2 W 1⁄4 W	5% 5%
R1230 R1232	321-0447-00 315-0393-00	B320000		100 kΩ, Var 442 kΩ 39 kΩ	¹/ <sub>8</sub> W Prec ¹/ <sub>4</sub> W	1% 5%
R1233 R1234 R1236 R1238 R1239	315-0124-00 303-0203-00 315-0684-00 315-0105-00 315-0472-00			120 kΩ 20 kΩ 680 kΩ 1 MΩ 4.7 kΩ	1/4 W 1 W 1/4 W 1/4 W 1/4 W	5% 5% 5% 5%
R1251 R1253 R1254 R1256 R1258	315-0102-00 315-0393-00 315-0154-00 301-0333-00 315-0222-00			1 kΩ 39 kΩ 150 kΩ 33 kΩ 2.2 kΩ	1/4 W 1/4 W 1/4 W 1/2 W 1/4 W	5% 5% 5% 5%
R1259 R1261 R1263 R1264 R1265	316-0825-00 315-0133-00 315-0332-00 315-0624-00 315-0105-00	B010100 B010100	B149999X B149999	8.2 ΜΩ 13 kΩ 3.3 kΩ 620 kΩ 1 ΜΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W	5% 5% 5% 5%
R1265 R1266 R1268 R1270 R1273	315-0125-00 315-0393-00 315-0752-00 315-0102-00 315-0512-00	B150000		1.2 MΩ 39 kΩ 7.5 kΩ 1 kΩ 5.1 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W	5% 5% 5% 5%
R1275 R1283 R1283 R1285 R1286	315-0752-00 315-0332-00 315-0132-00 315-0105-00 315-0393-00	B010100 B150000 B010100	B149999	7.5 kΩ 3.3 kΩ 1.3 kΩ 1 MΩ 39 kΩ	1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W 1/ <sub>4</sub> W	5% 5% 5% 5%

Ckt. No.	Tektronix Part No.	Serial/Mo Eff	del No. Disc		Description	
R1286 R1288 R1288 R1289 R1289	317-0393-00 315-0752-00 315-0302-00 315-0222-00 315-0152-00	B150000 B010100 B150000 B010100 B150000	B149999 B149999	39 kΩ 7.5 kΩ 3 kΩ 2.2 kΩ 1.5 kΩ	1/8 W 1/4 W 1/4 W 1/4 W 1/4 W	5% 5% 5% 5% 5%
R1291 R1292 R1292 R1300 R1302	315-0132-00 315-0472-00 315-0332-00 315-0562-00 315-0103-00	B010100 B150000	B149999	1.3 kΩ 4.7 kΩ 3.3 kΩ 5.6 kΩ 10 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/4 W	5% 5% 5% 5%
R1304 R1306 R1307 R1310	315-0223-00 315-0103-00 315-0562-00 315-0392-00 317-0103-00	B010100 B150000	B149999	22 kΩ 10 kΩ 5.6 kΩ 3.9 kΩ 10 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/8 W	5% 5% 5% 5%
R1312 R1312 R1314 R1314 R1316	315-0392-00 317-0103-00 315-0472-00 317-0103-00 317-0103-00	B010100 B150000 B010100 B150000 XB150000	B149999 B149999	3.9 kΩ 10 kΩ <b>4.7</b> kΩ 10 kΩ 10 kΩ	1/4 W 1/8 W 1/4 W 1/8 W 1/8 W	5% 5% <b>5%</b> 5%
R1319 R1320 R1322 R1324 R1326	315-0752-00 317-0103-00 317-0103-00 317-0103-00 317-0103-00	XB150000 XB150000 XB150000 XB150000 XB150000		7.5 kΩ 10 kΩ 10 kΩ 10 kΩ 10 kΩ	1/4 W 1/8 W 1/8 W 1/8 W 1/8 W	5% 5% 5% 5% 5%
R1330 R1332 R1334 R1336 R1340	317-0103-00 317-0103-00 317-0103-00 317-0103-00 317-0103-00	XB150000 XB150000 XB150000 XB150000 XB150000		10 kΩ 10 kΩ 10 kΩ 10 kΩ 10 kΩ	1/8 W 1/8 W 1/8 W 1/8 W 1/8 W	5% 5% 5% 5% 5%
R1342 R1344 R1346 R1350 R1352	317-0103-00 317-0103-00 317-0103-00 317-0103-00 317-0103-00	XB150000 XB150000 XB150000 XB150000 XB150000		10 kΩ 10 kΩ 10 kΩ 10 kΩ 10 kΩ	1/8 W 1/8 W 1/8 W 1/8 W 1/8 W	5% 5% 5% 5% 5%
R1354 R1356 R1370 R1372 R1374	317-0103-00 317-0103-00 317-0103-00 317-0103-00 317-0103-00	XB150000 XB150000 XB150000 XB150000 XB150000		10 kΩ 10 kΩ 10 kΩ 10 kΩ 10 kΩ	1/8 W 1/8 W 1/8 W 1/8 W 1/8 W	5% 5% 5% 5% 5%
R1376 R1401 R1402 R1404 R1405	317-0103-00 315-0105-00 315-0472-00 315-0221-00 301-0100-00	XB150000		10 kΩ 1 MΩ 4.7 kΩ 220 Ω 10 Ω	1/8 W 1/4 W 1/4 W 1/4 W 1/2 W	5% 5% 5% 5% 5%

CI. N	Tektronix		lodel No.	•			
Ckt. No.	Part No.	Eff	Disc		Descri	otion	
R1410 R1412 R1414 R1420 R1426	315-0393-00 315-0123-00 315-0392-00 308-0245-00 308-0245-00			39 kΩ 12 kΩ 3.9 kΩ 0.6 Ω 0.6 Ω	1/4 W 1/4 W 1/4 W 2 W 2 W	ww ww	5% 5% 5% 5%
R1430 R1432 R1433 R1436 R1453	315-0561-00 315-0103-00 315-0183-00 315-0101-00 301-0223-00	·		560 Ω 10 kΩ 18 kΩ 100 Ω 22 kΩ	1/4 W 1/4 W 1/4 W 1/4 W 1/2 W		5% 5% 5% 5%
R1460 R1461 R1462 R1462 R1463	303-0685-00 315-0103-00 305-0825-00 305-0755-00 305-0825-00	XB150000 B010100 B020000	B01 <b>9</b> 999	6.8 MΩ 10 kΩ 8.2 MΩ 7.5 MΩ 8.2 MΩ	1 W 1/4 W 2 W 2 W 2 W		5% 5% 5% 5%
R1464 R1465 R1467 R1467 R1468	305-0825-00 311-0647-00 303-0395-00 303-0475-00 316-0105-00	B010100 B020000	B019999 ·	8.2 M $\Omega$ 5 M $\Omega$ , Var 3.9 M $\Omega$ 4.7 M $\Omega$ 1 M $\Omega$	2 W 1 W 1 W 1/4 W		5% 5% 5%
R1469 R1470 R1472 R1474 R1476	311-0314-01 311-0086-00 311-0366-00 311-0475-00 311-0366-00			$\begin{array}{l} 2\ M\Omega,\ Var \\ 2.5\ k\Omega,\ Var \\ 500\ k\Omega,\ Var \\ 5\ k\Omega,\ Var \\ 500\ k\Omega,\ Var \end{array}$			
R1478 R1480 R1483 R1484 R1485	311-0357-00 316-0474-00 308-0459-00 316-0104-00 316-0103-00			$10~\mathrm{k}\Omega,~\mathrm{Var}$ 470 $\mathrm{k}\Omega$ $1.1~\Omega$ $100~\mathrm{k}\Omega$ $10~\mathrm{k}\Omega$	1/4 W 3 W 1/4 W 1/4 W	ww	5%
R1490 R1492 R1502 R1510 R1511	316-0105-00 316-0105-00 304-0393-00 301-0623-00 301-0823-00			1 ΜΩ 1 ΜΩ 39 kΩ 62 kΩ 82 kΩ	1/4 W 1/4 W 1 W 1/2 W 1/2 W		5% 5%
R1513 R1515 R1522 R1524 R1532	304-0101-00 306-0393-00 323-0369-00 323-0345-00 304-0153-00			100 Ω 39 kΩ 68.1 kΩ 38.3 kΩ 15 kΩ	1 W 2 W ½ W ½ W 1 W	Prec Prec	1% 1%
R1534 R1540 R1542 R1543 R1545	315-0100-00 305-0433-00 315-0182-00 308-0460-00 315-0390-00			10 Ω 43 kΩ 1.8 kΩ 56 Ω 39 Ω	1/4 W 2 W 1/4 W 3 W 1/4 W	ww	5% 5% 5% 5% 5%

Ckt. No.	Tektronix Part No.	Serial/Mode Eff	el No. Disc		Descript	ion	
R1547	306-0223-00			22 kΩ	2 W		
R1552	323-0328-00			25.5 kΩ	1/ <sub>2</sub> W	Prec	1%
R1554	321-0249-00			3.83 kΩ	1/8 W	Prec	1%
R1560	302-0270-00			27 Ω	⅓ W		
R1562	315-0103-00			10 kΩ	1/ <sub>4</sub> W		5%
R1563	308-0405-00			70 Ω	3 W	ww	5%
R1564	311-0632-00			2 kΩ, Var	1/4 W		5%
R1572	315-0821-00			820 Ω 470 Ω	1/4 W		5%
R1573 R1574	315-0471-00 315-0181-00			180 Ω	¼ W		5%
	21.5 0101 00			100 Ω	1/ <sub>4</sub> W		5%
R1576	315-0101-00 315-0621-00			620 Ω	1/ <sub>4</sub> W		5%
R1578 R1582	315-0621-00			100 Ω	1/4 W		5% 5%
R1584	321-0211-00			1.54 kΩ	1∕₃ W	Prec	1%
R1585	321-0193-00			1 kΩ	1/ <sub>8</sub> W	Prec	1%
R1 <i>587</i>	315-0512-00			5.1 kΩ	1/4 W		5%
R1588	311-0510-00	B010100	B319999	10 kΩ, Var			
R1588	311-1228-00	B320000		10 kΩ, Var	2 /4/		5%
R1590	305-0203-00			<b>2</b> 0 kΩ <b>2</b> kΩ	2 W 1/ <sub>4</sub> W		5 % 5 %
R1592	315-0202-00			47 Ω	1/4 W		5%
R1594	315-0470-00			47 22	74 11		
R1600	315-0101-00			100 Ω	⅓ W	WW	5% 5%
R1604	308-0388-00			47 Ω 910 Ω	3 W 1/ <sub>4</sub> W	** **	5 % 5%
R1610	315-0911-00			820 Ω	1/2 W		5% 5%
R1614 R1622	<b>301</b> -0821-00 <b>321-0202-0</b> 0			1.24 kΩ	1/8 W	Prec	1%
R1624	321-0202-00			1.87 kΩ	⅓ W	Prec	1%
			Swite	:hes			
Unv	vired or Wired						
SW5	*260-0916-00			Push	CH		
SW55	*260-0917-00			Push	CH		
SW130	260-0583-01			Slide	SYI		
SW510 ) 12	_ ,			0 5 11 12 11	A		
SW515 }	260-0880-00			3 Function Button	Во	<sup>ρ</sup> φ/Β φ ALT	
SW520 )					^	φ/υ φ Αι	
SW210 \						e Sweep	
SW530					dA		
SW550 }	260-0893-00			5 Function Button	1		,
SW552				(Bottom)	Q d	<b>.</b>	
SW570 /	•				u (	Ψ	
SW30 \						CTOR	
SW700					G		
SW710 >	<b>2</b> 60-0892-00			5 Function Button	R		
SW720 \ SW730 \				(Top)	B Y		
					1		

#### Switches (cont)

Ckt. No.	Tektronix Part No.	Serial/M Eff	odel No. Disc		Description
SW305	260-0642-00			Toggle	$\phi$ REF
SW403 <sup>18</sup>	311-0685-00	201:01.00	D1 (0000		<b></b>
SW405	260-0894-00	B010100	B149999	Lever	CH A 100%-75%-MAX GAIN
SW405	260-0894-01	B150000		Lever	CH A 100%-75%-MAX GAIN
SW413 <sup>14</sup>	311-0685-00	•			
SW415	260-0894-00	B010100	B149999	Lever	CH B 100%-75%-MAX GAIN
SW41 <b>5</b>	260-0894-01	B150000		Lever	CH B 100%-75%-MAX GAIN
SW685 <sup>15</sup>	311-0656-00	B010100	B259999		•
SW685 <sup>15</sup>	311-1080-00	B260000			
SW1305	260-0583-01			Slide	FIELD
SW:310 ) 16					VITS 18
SW1312 }	260-0880-00			3 Function Button	VITS 19
SW1314 )					FULL FIELD
SW1500 SW1502 <sup>17</sup>	<b>2</b> 60-0834-00			Toggle	POWER ON
SW1503 <sup>17</sup>					
			Tl		
TK280 <sup>18</sup>			Thermal	Curour	
				•	
•			Test P		
TP41	*214-0579-00			Pin, Test Point	<i>:</i>
TP49	*214-0579-00			Pin, Test Point	
TP80	*214-0579-00			Pin, Test Point	
TP85	*214-0579-00			Pin, Test Point	
TP90	*214-0579-00			Pin, Test Point	
TP95	*214-0579-00			Pin, Test Point	
ΓP110	*214-0579-00			Pin, Test Point	
TP130	*214-0579-00			Pin, Test Point	•
TP140	*214-0579-00			Pin, Test Point	
TP141	*214-0579-00			Pin, Test Point	
TP <b>2</b> 05	*214-0579-00	B010100	B249999	Pin, Test Point	
TP205	131-0633-00	B250000		Terminal, Pin	
TP212	*214-0579-00			Pin, Test Point	
TP220	*214-0579-00			•	
TP222	*214-0579-00			Pin, Test Point	•
TP230	*214-0579-00			Pin, Test Point	
TP250	*214-0579-00			Pin, Test Point	
TP252	*214-0579-00			Pin, Test Point	
ΓP255	*214-0579-00	•		Pin, Test Point	
TP270	*214-0579-00			Pin, Test Point	
TP275	*214-0579-00			Pin, Test Point	
	:				
	unit with R403.			•	
*Furnished as a	unit with R413.				

<sup>&</sup>lt;sup>14</sup>Furnished as a unit with R413.

<sup>&</sup>lt;sup>15</sup>Furnished as a unit with R685.

<sup>&</sup>lt;sup>16</sup>Furnished as a unit with SW510, SW515 and SW520.

<sup>&</sup>lt;sup>17</sup>See Mechanical Parts List. Line Voltage Selector (\*204-0279-00).

<sup>&</sup>lt;sup>18</sup>Furnished as a unit with partial Oven Assembly (\*205-0083-01).

Test Points (cont)

Ckt. No.	Tektronix Part No.	Serial/Model No. Eff Disc	Description	
TP285 TP295 TP320 TP325 TP340	*214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00		Pin, Test Point	
TP345 TP450 TP460 TP471	*214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00		Pin, Test Point	
TP502 TP510 TP514	*214-0579-00 *214-0579-00 *214-0579-00		Pin, Test Point Pin, Test Point Pin, Test Point	
TP515 TP530 TP565	*214-0579-00 *214-0579-00 *214-0579-00		Pin, Test Point Pin, Test Point Pin, Test Point	-
TP575 TP576 TP583 TP590 TP598	*214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00	XB150000 B010100 B149999X	Pin, Test Point	
TP620 TP630 TP640 TP650 TP660	*214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00		Pin, Test Point	
TP670 TP680 TP690 TP691 TP770	*214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00		Pin, Test Point	
TP772 TP774 TP776 TP805 TP820	*214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00		Pin, Test Point	
TP830 TP835 TP870 TP880 TP890	*214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00		Pin, Test Point	
TP900 TP905 TP913 TP920 TP950	*214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00 *214-0579-00	·	Pin, Test Point	

## Test Points (cont)

	Tektronix	Serial/Mo	del No.			
Ckt. No.	Part No.	Eff	Disc		Description	
T <b>P9</b> 55	*214-0579-00			Pin, Test Point		•
TP <b>9</b> 80	*214-0579-00					
TP <b>9</b> 90	*214-0579-00			Pin, Test Point		
TP 1101	*214-0579-00			Pin, Test Point		
TP 1120	*214-0579-00	•		Pin, Test Point Pin, Test Point		
11 1120	214-03/7-00	·		rin, Test Foint		
TP1 130	*214-0579-00			Die T. D. L.		
				Pin, Test Point		
TP1 140	*214-0579-00 *214-0579-00			Pin, Test Point		
TP1 152 TP1 153	*214-0579-00	•		Pin, Test Point		
	*214-0579-00			Pin, Test Point		
TP1 162	214-03/7-00			Pin, Test Point		
TD3 1/4	*01 / 0570 00			D		
TP1 164	*214-0579-00 *014-0570-00			Pin, Test Point		
TP1 170	*214-0579-00			Pin, Test Point		
TP1 190	*214-0579-00			Pin, Test Point		
TP1 200	*214-0579-00			Pin, Test Point		
TP1 205	*214-0579-00			Pin, Test Point	•	
TP1 215	*214-0579-00		•	Dia T. I. D. I. I.		
TP1 216	*214-0579-00			Pin, Test Point		
TP1 220	*214-0579-00			Pin, Test Point		
TP1 230	*214-0579-00	B010100	D1 40000V	Pin, Test Point		
TP1 260	*214-0579-00	ВОТОТОО	B149999X	Pin, Test Point		
171 200	214-03/ 7-00			Pin, Test Point		
TP1 265	*214-0579-00			Pin, Test Point		
TP1 270	*214-0579-00			Pin, Test Point		¥
TP1 280	*214-0579-00			Pin, Test Point		
TP1 285	*214-0579-00			Pin, Test Point		*
TP1 289	*214-0579-00			Pin, Test Point		
TP1 290	*214-0579-00			Pin, Test Point		
TP1 405	*214-0579-00			Pin, Test Point		
TP1410	*214-0579-00			Pin, Test Point		
TP1.412	*214-0579-00			Pin, Test Point		
TP1 430	<b>*214</b> -0579-00			Pin, Test Point		
TP1 432	<b>*2</b> 14-0579-00			Dir T . D		
TP1510	*214-0579-00			Pin, Test Point		
TP1 <i>5</i> 15	*214-0579-00			Pin, Test Point		
TP1 540	*214-0579-00			Pin, Test Point		
TP1 545	*214-0579-00			Pin, Test Point		
111343	214-03/ 7-00			Pin, Test Point		
TP1 <i>57</i> 0	*214-0579-00			Pin, Test Point		
TP1 580	*214-0579-00			Pin, Test Point		
TP1 590	*214-0579-00			Pin, Test Point		
TP1600	*214-0579-00			Pin, Test Point		
TP1610	*214-0579-00			Pin, Test Point		
TP1620	*214-0579-00	•		Pin, Test Point		
				,		
			Transfor	more		
T45	*120 0520 00		Hallston			
T45	*120-0528-00 *120-0525-00			Toroid, two 22	turn windings	
T205	*120-0525-00 *120-0529-00			Toroid, 7 turns,	quadtilar	
T235 T355 <sup>19</sup>	*120-0529-00			Toroid, 24 turns,	, tritilar	
T365 <sup>20</sup>		_				
<sup>19</sup> Furnished as a	unit with CH A Go	niometer (*119-	0133-00).			

<sup>20</sup>Furnished as a unit with CH B Goniometer (\*119-0133-00).

# Electrical Parts List—Type 520/R520 NTSC

#### Transformers (Cont)

Ckt. No.	Tektronix Part No.	Serial/Model Eff	No. Disc	Des	cription	:
T500 T508 T590 T598 T695	*120-0527-00 *120-0526-00 *120-0526-00 *120-0526-00 *120-0524-00			Toroid, 12 turns, bifilar Toroid, 12 turns, quadfilo Toroid, 12 turns, quadfilo Toroid, 12 turns, quadfilo Toroid, 12 turns, quadfilo	ar ar	
T1140 T1450 T1501	*120-0525-00 *120-0523-00 *120-0498-00			Toroid, 7 turns, quadfilar H.V. Power L.V. Power	r	
			ntegrated	Circuits		
U510 U511 U1310 U1320 U1330 U1340 U1350	156-0012-00 156-0012-00 156-0012-00 156-0012-00 156-0012-00 156-0012-00 156-0012-00			Clocked J-K Flipflop Clocked J-K Flipflop Clocked J-K Flipflop Clocked J-K Flipflop Clocked J-K Flipflop Clocked J-K Flipflop Clocked J-K Flipflop	Replaceable by Fairchi Replaceable by Fairchi Replaceable by Fairchi Replaceable by Fairchi Replaceable by Fairchi Replaceable by Fairchi Replaceable by Fairchi	d μL923 ld μL923 ld μL923 ld μL923 ld μL923 ld μL923
U1370	156-0012-00	XB150000		Clocked J-K Flipflop	Replaceable by Fairchi	ld μL923
V1 <i>4</i> 70	*154-0513-00		Electron	Tube T5201-31-4 CRT Standard	d Phosphor	
			Crys	<b>L</b> alo		
Y40 Y260	158-0038-00 158-0036-00	4	Grys	3.59 MHz 3.59 MHz		

#### FIGURE AND INDEX NUMBERS

Items in this section are referenced by figure and index numbers to the illustrations which appear either on the back of the diagrams or on pullout pages immediately following the diagrams of the instruction manual.

#### INDENTATION SYSTEM

This mechanical parts list is indented to indicate item relationships. Following is an example of the indentation system used in the Description column.

Assembly and/or Component
Detail Part of Assembly and/or Component
mounting hardware for Detail Part
Parts of Detail Part
mounting hardware for Parts of Detail Part
mounting hardware for Assembly and/or Component

Mounting hardware always appears in the same indentation as the item it mounts, while the detail parts are indented to the right. Indented items are part of, and included with, the next higher indentation.

Mounting hardware must be purchased separately, unless otherwise specified.

#### PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix, Inc. Field Office or representative.

Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number, instrument type or number, serial or model number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix, Inc. Field Office or representative will contact you concerning any change in part number.

Change information, if any, is located at the rear of this manual.

#### ABBREVIATIONS AND SYMBOLS

For an explanation of the abbreviations and symbols used in this section, please refer to the page immediately preceding the Electrical Parts List in this instruction manual.

# INDEX OF MECHANICAL PARTS LIST ILLUSTRATIONS

(Located behind diagrams)

FIG. 1 FRONT

FIG. 2 CRT SHIELD, HIGH VOLTAGE & CHASSIS

FIG. 3 CIRCUIT BOARDS

FIG. 4 REAR

FIG. 5 CABINET & FRAME

FIG. 6 ACCESSORIES

# SECTION 8 MECHANICAL PARTS LIST

TIO. I INCINI	FIG	. 1	FR	ONI
---------------	-----	-----	----	-----

			1 INOINI
		Q	
	odel No.	t	Description
Eff	Disc	у	1 2 3 4 5
•		1	DANIEL from
		1	PANEL, front
		4	mounting hardware: (not included w/panel)
•		4	SCREW, thread forming, $2-32 \times \frac{3}{16}$ inch, PHS
•			
		1	PANEL, right insert
		-	mounting hardware: (not included w/panel)
		3	SCREW, 6-32 x <sup>5</sup> / <sub>16</sub> inch, PHS
		1	PANEL, left insert
		·	mounting hardware: (not included w/panel)
		4	SCREW, 6-32 x 5/16 inch, PHS
			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
0010100	D000000		DE7EL
B010100	B039999	1	BEZEL, graticule
B040000 B320000	B319999	1	BEZEL, graticule BEZEL, graticule
B320000			bezel includes:
B010100	B199999X	4	PAD, cushioning
B010100	B039999X	4	STUD, snap fastener
2010100		•	mounting hardware for each: (not included w/stud)
B010100	B039999X	1	SCREW, thread forming, #6 x 3/8 inch, PHS
			·
		1	FILTER, light, smokey gray
D010100	D100000	j	GRATICULE
B010100	B199999	1	MASK, graticule
B200000		2 1	MASK, graticule LIGHT CONDUCTOR, graticule illumination
B010100	B039999	4	SOCKET, snap fastener
B040000	2007777	4	THUMBSCREW, 1/4-20 x 1.369 inch long
		1	KNOB, pushbutton—CH A
		1	KNOB, pushbutton—VITS 18
		1	KNOB, pushbutton—FULL FIELD
		1	KNOB, pushbutton—VITS 19
		1	KNOB, pushbutton—CH B
		1	KNOB, pushbutton—A CAL
		1	KNOB, pushbutton—A $\phi$ KNOB, pushbutton—A $\phi$ B $\phi$ ALT.
		1	KNOB, pushbutton—B $\phi$
		i	KNOB, pushbutton—B CAL
		į	KNOB, pushbutton—VECTOR
		1	KNOB, pushbutton—Y
		1	KNOB, pushbutton—R
4		1	KNOB, pushbutton—G
		1	KNOB, pushbutton—B
		1	KNOB, pushbutton—DIFF PHASE
		1	KNOB, pushbutton—DIFF GAIN
		1	KNOB, pushbutton—Q
		1	KNOB, pushbutton—I
R010100	BU80000	1	KNOB, pushbutton—LINE SWEEP KNOB, gray—CALIBRATED PHASE
	D00///7		KNOB, gray—CALIBRATED PHASE
2070000			knob includes:
		2	SCREW, set, 5-40 x 1/8 inch HSS
	010100 090000		1 1010100 B089999 1 090000 1

#### FIG. 1 FRONT (cont)

Fig. & Index No.	Tektronix Part No.	Serial/Model Eff	No. Disc	Q t y	Description 1 2 3 4 5
1-35	119-0152-00			1	ASSEMBLY, precision phase shifter
-36	331-0189-00			1	assembly includes: LENS, tape, dial
-37	211-0105-00			2	mounting hardware: (not included w/lens) SCREW, 4-40 x <sup>3</sup> / <sub>16</sub> inch, FHS
-38 -39	386-1290-00 407-0386-00			1	PLATE, mounting BRACKET, dial mounting mounting hardware: (not included w/bracket)
-40 -41 -42	211-0139-00 211-0138-00 361-0165-00			1 2 3	SCREW, $5-40 \times 4^{13}/_{16}$ inches, RHS SCREW, $5-40 \times 2^{9}/_{16}$ inches, RHS SPACER, sleeve, $0.155$ OD $\times 7/_{8}$ inch long
-43 -44 -45	361-0167-00 361-0166-00 210-0449-00			3 1 3	SPACER, sleeve, 0.155 OD x 13/8 inches SPACER, sleeve, 0.155 OD x 21/4 inches long NUT, hex., 5-40 x 1/4 inch
-46	331-0188-00			1	DIAL, tape
-47 -48	401-0042-00  210-1043-00			2 - 1	BEARING, sleeve mounting hardware for each: (not included w/bearing) WASHER, plastic, 0.253 IDx 5/8 inch OD
-49	386-1299-00 210-0803-00			i 1	PLATE, retaining WASHER, flat, 0.150 ID x 3/8 inch OD
-50	354-0233-00			1	RING, retaining
-51 -52	384-0678-00 214-0953-00			1	SHAFT, 1/4 OD x 1.45 inches long GEAR, spur
-53	213-0075-00			- 4 1	gear includes: SCREW, set, 4-40 x <sup>3</sup> / <sub>32</sub> inch CAPACITOR
-54	211-0065-00			2	mounting hardware: (not included w/capacitor) SCREW, $4-40 \times {}^{3}/_{16}$ inch, PHS
	358-0042-00 210-0269-00	XB020000 XB020000		1	BUSHING, plastic LUG, terminal
-55				2 1	COIL, w/mounting hardware RESISTOR, variable
	210-0046-00 210-0583-00			1	mounting hardware: (not included w/resistor) LOCKWASHER, internal, ½ ID x 0.400 inch OD NUT, hex., ¼-32 x 5/16 inch
-56 -57	131-0372-00 441-0751-00			2 1 1	CONNECTOR, coaxial, w/hardware CHASSIS SHIELD
-58 -59	337-0957-00  213-0055-00			- 8	mounting hardware: (not included w/shield) SCREW, thread forming, 2-32 x 3/16 inch, PHS
-60	129-0098-00			2	POST, hex., 1/4 inch diameter x 0.406 inch long
-61 - <b>62</b>	210-0004-00 211-0008-00			1 1	mounting hardware for each: (not included w/post) LOCKWASHER, internal #4 SCREW, 4-40 x 1/4 inch, PHS
-63 -64	211-0008-00 210-0012-00 210-0978-00 210-0590-00	•		2 1 1	mounting hardware: (not included w/assembly) SCREW, 4-40 x ½ inch, PHS LOCKWASHER, internal, 3/8 ID x ½ inch OD WASHER, flat, 3/8 ID x ½ inch OD NUT, hex., 3/8-32 x 7/16 inch

Fig. & Index No.		Serial/M Eff	odel No. Disc	Q t y	Description 1 2 3 4 5
1-65 -66 -67 -68 -69	366-0429-00 366-0429-00 366-0429-00 366-0429-00 260-0583-01			1 1 1 1	KNOB, gray—HORIZ POSITION KNOB, gray—VERT POSITION KNOB, gray—BURST FLAG TIMING KNOB, gray—FOCUS SWITCH, slide—FIELD
	211-0001-00 210-0405-00 210-0001-00		·	2 2 2	mounting hardware: (not included w/switch) SCREW, 2-56 x ½ inch, RHS NUT, hex., 2-56 x ¾ inch LOCKWASHER, internal #2
-70	260-0583-01  211-0001-00 210-0405-00 210-0001-00			! 2 2 2	SWITCH, slide—SYNC mounting hardware: (not included w/switch) SCREW, 2-56 x ½ inch, RHS NUT, hex., 2-56 x ³/16 inch LOCKWASHER, internal #2
<i>-7</i> 1	366-0436-00 366-0497-00	B010100 B090000	B089999	1	KNOB, gray—SCALE ILLUM KNOB, gray—SCALE ILLUM knob includes:
-72	<b>2</b> 13-0153-00			2	SCREW, set, 5-40 x 1/8 inch, HSS RESISTOR, variable mounting hardware; (not included w/resistor)
-73	361-0143-00 210-0940-00 210-0583-00			1 1	SPACER, ring, 0.281 ID $\times$ 0.562 inch OD WASHER, flat, $\frac{1}{4}$ ID $\times$ $\frac{3}{6}$ inch OD NUT, hex., $\frac{1}{4}$ -32 $\times$ $\frac{5}{16}$ inch
-74	260-0834-00			1	SWITCH, toggle—POWER ON mounting hardware: (not included w/switch
-75	210-0940-00 210-0562-00			1	WASHER, flat, $\frac{1}{4}$ ID x $\frac{3}{8}$ inch OD NUT, hex., $\frac{1}{4}$ -40 x $\frac{5}{16}$ inch
-76	136-0223-00 			1 1 1	SOCKET, light w/hardware mounting hardware: (not included w/socket) NUT, hex., $\frac{1}{4}$ -40 x $\frac{5}{16}$ inch LUG, solder, $\frac{1}{4}$ ID x $\frac{7}{16}$ inch OD, SE WASHER, flat, $\frac{1}{4}$ ID x $\frac{3}{8}$ inch OD
-77	366-0435-00 366-1024-00	B010100 B090000	B089999	1	KNOB, gray—INTENSITY KNOB, gray—INTENSITY knob includes:
-78	213-0153-00			2	SCREW, set, 5-40 x 1/8 inch, HSS RESISTOR, variable
-79 -80 -81	210-0207-00 210-0012-00 210-0978-00 210-0590-00			1 1 1 1	mounting hardware: (not included w/resistor) LUG, solder, $\frac{3}{8}$ ID x $\frac{5}{8}$ inch OD, SE LOCKWASHER, internal, $\frac{3}{8}$ ID x $\frac{1}{2}$ inch OD WASHER, flat, $\frac{3}{8}$ ID x $\frac{1}{2}$ inch OD NUT, hex., $\frac{3}{8}$ -32 x $\frac{7}{16}$ inch

Fig. & Index No.	Tektronix Part No.	Serial/Model N Eff [	Q No. t Disc y	Description
1-82 -83	200-0745-00 366-0431-00		1	COVER, plastic, variable resistor KNOB, gray—LUMINANCE GAIN
-84	213-0076-00		2 1	knob includes: SCREW, set, 2-56 x 1/8 inch, HSS RESISTOR, variable
-85	210-0046-00 210-0940-00 210-0583-00		1 1 2	mounting hardware: (not included w/resistor) LOCKWASHER, internal, $\frac{1}{4}$ ID x 0.400 inch OD WASHER, flat, $\frac{1}{4}$ ID x $\frac{3}{8}$ inch OD NUT, hex., $\frac{1}{4}$ -32 x $\frac{5}{16}$ inch
-86	407-0375-00		3	BRACKET, angle mounting hardware for each: (not included w/bracket)
-87	220-0413-00		2	NUT, hex., $4-40 \times \frac{3}{16} \times 0.562$ inch long
-88	366-0482-00 366-0498-00	B010100 B08999 B090000	99 1 1	KNOB, gray—PHASE (CH B) KNOB, gray—PHASE (CH B) knob includes:
	213-0153-00		2	SCREW, set, 5-40 x 1/8 inch, HSS mounting hardware: (not included w/knob)
	210-1106-00 210-0894-00	X272150 X272150	1	WASHER, spring tension WASHER, plastic, 0.19 ID x 0.438 inch, OD
-89	119-0133-00		2	GONIOMETER, w/hardware mounting hadware for each: (not included w/goniometer)
	220-0576-00	X272150	1	NUT, hex., 0.312-32 x 0.438 inch
-90	366-0482-00 366-0498-00	B010100 B08999 B090000	99 1 1	KNOB, gray—PHASE (CH A) KNOB, gray—PHASE (CH A) knob includes:
-91 -92	213-0153-00 366-0215-02 260-0894-00 260-0894-01	B010100 B1499 B150000	1	SCREW, set, 5-40 x 1/8 inch, HSS KNOB, gray—100% (CH A) SWITCH, lever—100% (CH A) SWITCH, lever—100% (CH A)
-93	220-0413-00		2	mounting hardware: (not included w/switch) NUT, hex., $4-40 \times \sqrt[3]{_{16}} \times 0.562$ inch long
-94 -95	366-0215-02 260-0894-00 260-0894-01	B010100 B1499 B150000	1 999 1 1	KNOB, gray—100% (CH B) SWITCH, lever—100% (CH B) SWITCH, lever—100% (CH B)
-96	220-0413-00		2	mounting hardware: (not included w/switch) NUT, hex., $4-40 \times \sqrt[3]{16} \times 0.562$ inch long
-97	366-0431-00		1 -	KNOB, gray—GAIN (CH A) knob includes:
-98	213-0076-00 		2 1 1	SCREW, set, 2-56 x $\frac{1}{8}$ inch, HSS RESISTOR, variable mounting hardware: (not included w/resistor) WASHER, flat, $\frac{1}{4}$ ID x $\frac{3}{8}$ inch OD NUT, hex., $\frac{1}{4}$ -32 x $\frac{5}{16}$ inch
-99	366-0431-00		1	KNOB, gray—GAIN (CH B)
	213-0076-00	<u>.</u> ·	2	knob includes: SCREW, set, 2-56 x 1/8 inch, HSS

	< Tektronix		rial/Model No.	t	Doomination.
70.	Part No.	Eff	Disc	у	Description 1 2 3 4 5
_ 1 <i>0</i> 0		_		1	RESISTOR, variable
-,0		•			mounting hardware: (not included w/resistor)
	210-0940-00		•	1	WASHER, flat, 1/4 ID x 3/8 inch OD
	210-0583-00	)		1	NUT, hex., 1/4-32 x 5/16 inch
101	260-0916-00			1	SWITCH, pushbutton
- 00	211 0541 00	-		•	mounting hardware: (not included w/switch)
102	211-0541-00	,		1	SCREW, 6-32 x 1/4 inch, FHS
103	260-0880-00			2	SWITCH, pushbutton
	211-0541-00			-	mounting hardware for each: (not included w/switch)
	211-0541-00			. 2	SCREW, 6-32 x 1/4 inch, FHS
104	260-0917-00			1	SWITCH, pushbutton
	211 0541 00				mounting hardware: (not included w/switch)
105	211-0541-00			1	SCREW, 6-32 x 1/4 inch, FHS
106		•		2	RESISTOR, variable
	213-0020-00				mounting hardware for each: (not included w/resistor)
	213-0020-00			1	SCREW, set, 6-32 x 1/8 inch, HHS
107	260-0892-00			1	SWITCH, pushbutton
	011 0541 00			-	mounting hardware: (not included w/switch)
	211-0541-00			2	SCREW, 6-32 x 1/4 inch, FHS
108	260-0893-00			1	SWITCH, pushbutton
	011 0541 00				mounting hardware: (not included w/switch)
•	211-0541-00			2	SCREW, $6-32 \times \frac{1}{4}$ inch, FHS
109	124-0206-00			2	STRIP, trim, blue (Type 520 only)
–	407-0377-01	B010100	B319999	2	BRACKET, handle (Type R520 only)
4	407-0377-03	B320000		2	BRACKET, handle (Type R520 only)
11 2	212-0560-00			2	mounting hardware for each: (not included w/bracket) SCREW, 10-32 x 5/16 inch, FHS
••				-	30KEW, 1002 X 7/18 IIICH, FFIS
	333-1038-00 333-1630-00	B010100	B319999	1	PANEL, front, right (Type R520 only)
_	67-0076-00	B320000		1	PANEL, front, left (Type R520 only)
-				-	HANDLE, carrying (Type R520 only) mounting hardware for each: (not included w/handle)
14 2	12-0506-00			2	SCREW, 10-32 x 3/8 inch, FHS
15 3	33-1039-00	B010100	B319999	1	INSERT front panel blank /T. psoc
3	33-1630-00	B320000		i	INSERT, front panel, blank (Type R520 only) INSERT, front panel, blank (Type R520 only)
	67-0073-00	B010100	B209999	1	HANDLE, carrying (Type 520 only)
	67-0073 01 67-0073-02	B210000 B220000	B219999	1	HANDLE, carrying (Type 520 only)
-		522000		-	HANDLE, carrying (Type 520 only) mounting hardware: (not included w/handle)
••	13-0155-00			4	SCREW, 10-32 x 0.40 inch long, machine (Type 520 only)
18 38	36-1283-00			2	PLATE, plastic, mounting (Type 520 only)
19 20	00-0728-00			2	COVER, plastic, handle (Type 520 only)
20 38	86-1260-01	B010100	B319999	1	SUB-PANEL, front
38	6-1260-04	B320000		1	SUB-PANEL, front

# Mechanical Parts List—Type 520/R520 NTSC

Fig. & Index No.	Tektronix Part No.	Serio Eff	II/Model No. Disc	Q t y	Description 1 2 3 4 5
	200-0761-01 200-0873-00 426-0370-00	B010100 B170000 B010100	B169999 B169999X	2 2 2	DOOR, access panel DOOR, access panel FRAME, door guide mounting hardware for each: (not included w/frame)
	211-0507-00	B010100	B169999X	2	SCREW, 6-32 x <sup>5</sup> / <sub>16</sub> inch, PHS
-123	351-0136-00	B010100	B169999	2	GUIDE, door mounting hardware for each: (not included w/guide)
-124	211-0007-00	B010100	B169999	1	SCREW, 4-40 x <sup>3</sup> / <sub>16</sub> inch, PHS
	351-0148-00 351-0149-00 105-0067-00 214-0239-00	B170000 B170000 B010100	B169999X	2 2 2 2	TRACK, top right, bottom left TRACK, top left, bottom right CATCH, friction FASTENER, thumb screw (Type R520 only) mounting hardware for each: (not included w/fastener)
	210-0917-00 354-0025-00			2 1	WASHER, plastic, 0.191 ID $\times$ 0.625 inch OD RING, snap
	358-0301-00 407-0394-00  212-0518-00			2 1 - 2	BUSHING, plastic, gray BRACKET, angle mounting hardware: (not included w/bracket) SCREW, 10-32 x 5/16 PHS
	210-0583-00			2	RESISTOR, variable mounting hardware for each: (not included w/resistor) NUT, hex., 1/4-32 x 5/16 inch
	210-0046-00 210-0583-00			2 1 1	RESISTOR, variable mounting hardware for each: (not included w/resistor) LOCKWASHER, internal, $\frac{1}{4}$ ID x 0.400 inch OD NUT, hex., $\frac{1}{4}$ -32 x $\frac{5}{16}$ inch
	337-0972-00 5 260-0642-00 210-0046-00 210-0490-00 210-0562-00			2 1 - 1 1 1	SHIELD, light SWITCH, toggle— $\phi$ REF mounting hardware: (not included w/switch) LOCKWASHER, internal, 0.261 ID x 0.400 inch OD WASHER, flat, $\frac{1}{4}$ ID x $\frac{3}{8}$ inch OD NUT, hex., $\frac{1}{4}$ -40 x $\frac{3}{16}$ inch

## FIG. 2 CRT SHIELD, HIGH VOLTAGE & CHASSIS

Fig. & Index No.	Tektronix Part No.	Serial/Mode Eff	el No. Disc	Q t y	Description 1 2 3 4 5
2-1	441-0741-00	B010100 B2	69999	1	CHASSIS, main
	441-0741-01	B270000		1	CHASSIS, main
					mounting hardware: (not included w/chassis)
	212-0043-00			4	SCREW, 8-32 x 1/2 inch, FHS
	212-0070-00			8	SCREW, 8-32 x 5/16 inch, FHS
	212 007 0 00			J	SCREWY S SEX 718 Men, THE
-2	407-0370-00			1	BRACKET, capacitor
		,	•	-	mounting hardware: (not included w/bracket)
-3	212-0001-00	•		6	SCREW, 8-32 x 1/4 inch, PHS
Ū	212 0001 00			Ū	CONTINUE TO SERVICE THE SERVICE TO SERVICE THE SERVICE TO SERVICE THE SERVICE
-4	344-0118-00			6	CLIP, capacitor mounting
				-	mounting hardware for each: (not included w/capacito
-5	211-0507-00			1	SCREW, 6-32 x <sup>5</sup> / <sub>16</sub> inch, PHS
-6	210-0457-00			1	NUT, keps, 6-32 x 5/16 inch
Ū	210 0 107 00			•	716 Man
-7	386-1259-00			1	PLATE, chassis support
				-	mounting hardware: (not included w/plate)
	212-0004-00			3	SCREW, 8-32 x 5/16 inch, PHS
	212-0040-00			2	SCREW, 8-32 x 3/8 inch, FHS
-8	210-0458-00			5	NUT, keps, 8-32 x 11/ <sub>32</sub> inch
Ū				Ū	737 men
-9	348-0063-00			5	GROMMET, plastic, 1/2 inch diameter
	348-0050-00			2	GROMMET, plastic, 3/4 inch diameter
-11	348-0031-00	-		1	GROMMET, plastic, $\frac{3}{32}$ inch diameter
	348-0055-00			1	GROMMET, plastic, 1/4 inch diameter
	348-0141-00			i	GROMMET, plastic, "U" shaped
	344-0143-00			40	CLIP, circuit board mounting
-1-4					mounting hardware for each: (not included w/clip)
-15	213-0088-00			1	SCREW, thread forming, #4 x 1/4 inch, PHS
-13	213-0000-00			•	SCREW, miedd forming, #4x /4 mcn, 1113
-16				4	RESISTOR, variable
				-	mounting hardware for each: (not included w/resistor)
-17	210-0046-00			1	LOCKWASHER, internal, 1/4 ID x 0.400 inch OD
	358-0075-00			i	BUSHING, panel
-10	030-00/ 3-00				bootinite, paner
-19				1	RESISTOR, variable
.,					mounting hardware: (not included w/resistor)
-20	210-0223-00			1	LUG, solder, 1/4 ID x 7/16 inch OD, SE
	358-0075-00			i	BUSHING, panel
-21	330-00/ 3-00			•	Boshinto, punei
-22				1	TRANSFORMER
		•			mounting hardware: (not included w/transformer)
-23	212-0515-00			4	SCREW, 10-32 x 2 <sup>1</sup> / <sub>4</sub> inches, HHS
	210-0812-00			. 4	WASHER, fiber, $\frac{3}{16}$ ID x $\frac{3}{8}$ inch OD
	220-0410-00			4	NUT, keps, $10-32 \times \frac{3}{8}$ inch

FIG. 2 CRT SHIELD, HIGH VOLTAGE & CHASSIS (cont)

Fig. & Index No.	Tektronix Part No.	Serial/ Eff	Model No. Disc	Q t	Description	
	337-0888-00		2130	<u>y</u>	1 2 3 4 5	-4
2-26 -27	621-0430-00			1	SHIELD, high voltage box ASSEMBLY, high voltage	
-28	380-0115-00			1	assembly includes: HOUSING, high voltage	
-29	670-0543-00			1	ASSEMBLY, circuit board—H.V. #2	
	388-0883-00			1	assembly includes: BOARD, circuit	
-30	211-0097-00	B010100	B080559	- 4	mounting hardware: (not included w/assembly) SCREW, 4-40 x <sup>5</sup> / <sub>16</sub> inch, PHS	
55	211-0040-00	B080560		4	SCREW, 4-40 x 1/4, BH plastic	
-31	361-0137-00			4	SPACER, 1/4 OD x 1.39 inches long	
-32	670-0542-00			1	ASSEMBLY, circuit board—H.V. #1 assembly includes:	
	388-0887-00			1	BOARD, circuit	
-33	211-0097-00	B010100	B080559	4	mounting hardware: (not included w/assembly) SCREW, 4-40 x <sup>5</sup> / <sub>16</sub> inch, PHS	
	211-0040-00	B080560		4	SCREW, $4-40 \times \frac{1}{4}$ , BH plastic	
-34	166-0319-00			3	SLEEVE, plastic	
-35	166-0368-00			1	SLEEVE, plastic, anode lead	
-36	200-0714-00			1 -	COVER, plastic, high voltage mounting hardware: (not included w/cover)	
-3 <i>7</i> -38	211-0537-00 211-0545-00			1 2	SCREW, $6.32 \times \frac{3}{8}$ inch, THS SCREW, $6.32 \times \frac{1}{4}$ inches, THS	
-39	136-0272-00			1	CABLE HARNESS, CRT	
-40	136-0202-00			1	cable harness includes: SOCKET, CRT, 14 pin	
-41	179-1218-00		•	1	CABLE HARNESS, high voltage mounting hardware: (not included w/assembly)	
-42	211-0507-00			3	SCREW, 6-32 x 5/16 inch, PHS	
-43	200-0616-00			1	COVER, plastic, CRT socket	
-44	337-0945-01			1	SHIELD, cathode ray tube	
-45	211-0537-00			4	mounting hardware: (not included w/shield) SCREW, 6-32 x 3/8 inch, THS	
	211-0596-00 210-0803-00			2 6	SCREW, 6-32 x $\frac{3}{8}$ inch, PHB WASHER, flat, 0.150 ID x $\frac{3}{8}$ inch OD	
	210-0000-00			Ū	WYNOTER, IIII, 0.130 ID X 78 IIICII GD	
-46	348-0085-00			1	GROMMET, plastic, "U" shaped	
-47	343-0131-00			1 -	CLAMP, coil form mounting hardware: (not included w/clamp)	
-48 -49	211-0534-00 210-0457-00			2 2	SCREW, sems, 6-32 x <sup>5</sup> / <sub>16</sub> inch, PHS NUT, keps, 6-32 x <sup>5</sup> / <sub>16</sub> inch	
-47	Z10-043/-00			2	1401, Keps, 0-02 x /18 IIICII	
-50	352-0091-01			2	HOLDER, CRT retainer	
-51	211-0590-00			- 2	mounting hardware for each: (not included w/holder) SCREW, $6-32 \times \frac{1}{4}$ inch, PHS	
<b>-</b>				_		•

# FIG. 2 CRT SHIELD, HIGH VOLTAGE & CHASSIS (cont)

	Fig. 8 Index No.	Tektronix	Serial/Mode Eff		Q t	Description
ا ا	140.	Part No.	CII	Disc	у	1 2 3 4 5
	2-52 -53 -54 -55	343-0123-00 211-0600-00 220-0444-00 343-0124-00		٠	2 1 1 1	CLAMP, CRT retainer SCREW, 6-32 x 2 inches, FIL HS NUT, square, 6-32 x 1/4 inch CLAMP, plastic, retainer
	-56 -57	211-0599-00 220-0444-00			1	mounting hardware: (not included w/clamp) SCREW, 6-32 $\times$ $^3$ / $_4$ inch, FIL HS NUT, square, 6-32 $\times$ $^1$ / $_4$ inch
	-58	343-0122-01 		•	2 - 1 2	CLAMP, CRT shield mounting hardware for each: (not included w/clamp) SCREW, 6-32 $\times$ $^{3}/_{8}$ inch, THS WASHER, flat, $^{9}/_{64}$ ID $\times$ $^{1}/_{2}$ OD $\times$ $^{1}/_{16}$ inch thick
$\Gamma$	-59	210-0457-00			1	NUT, keps, 6-32 x 5/16 inch
L	-60 -61 -62	136-0035-00 			4 - 1 1	SOCKET, graticule lights mounting hardware for each: (not included w/socket) SCREW, sems, $6-32 \times \frac{5}{16}$ inch, PHS WASHER, flat, 0.150 ID $\times \frac{3}{8}$ inch OD
<b>/</b> ~~	-63	210-0457-00			1	NUT, keps, 6-32 x <sup>5</sup> / <sub>16</sub> inch
	-64	136-0264-00			2	SOCKET, light mounting hardware for each: (not included w/socket)
	-65	211-0116-00 210-0801-00 210-0586-00			1	SCREW, sems, $4-40 \times \frac{5}{16}$ inch, PHS WASHER, flat, 0.140 ID $\times$ 0.281 inch OD NUT, keps, $4-40 \times \frac{1}{16}$ inch
<u> </u>	- <b>6</b> 6				1	COIL, beam rotating
lu m	-67 -68	213-0088-00 354-0321-00			1 1	mounting hardware: (not included w/coil) SCREW, thread forming, 4-40 x 1/4 inch, PHS RING, CRT shockmount
	-69 -70	179-1221-00 179-1221-01 179-1220-00	B150000 B010100 B14	49999 49999	] ] ]	CABLE HARNESS, main chassis CABLE HARNESS, main chassis CABLE HARNESS, power
	-71 -72	179-1220-01 344-0111-00 179-0588-00 179-0641-00	B150000		2 1 1	CABLE HARNESS, power CLIP, plastic deflection plate WIRE, CRT lead, striped orange white, 5½ inch w/connector WIRE, CRT lead, striped brown, 3 inch w/connector
	<i>-7</i> 3	179-0642-00 179-0705-00 179-0706-00 210-0201-00 213-0004-00			1 1 1 1 1 1	WIRE, CRT lead, striped blue, 4 inch w/connector WIRE, CRT lead, striped green, 6 inch w/connector WIRE, CRT lead, striped red, 5 inch w/connector UIG, solder, SE #4 mounting hardware: (not included w/lug) SCREW, thread forming, 5-32 x 3/16 PHS
		200-0174-00 343-0088-00 343-0089-00			1 <b>2</b> 5	COVER, plastic, screw CLAMP, plastic, small CLAMP, plastic, large

### FIG. 3 CIRCUIT BOARDS

Fig. &				Q	
Index No.	Tektronix Part No.	Serio Eff	al/Model No. Disc	t	Description
140.	Full 140.	<b>L</b> II		у	1 2 3 4 5
3-	670-0353-00	XB250000	B279999	1	ASSEMBLY, circuit board—SCR LIMITER
	670-0353-01	B280000		1	ASSEMBLY, circuit board—SCR LIMITER
	200 1/05 00	B250000	B279999	1	assembly includes: BOARD, circuit
	388-1685-00 388-1685-01	B280000	DZ/ 77,77	i	BOARD, circuit
	131-0589-00	D200000		2	TERMINAL, pin, 0.50 inch long
	136-0220-00			2	SOCKET, transistor, 3 pin, square
	136-0263-03	B250000	B279999	4	SOCKET, connector pin
	136-0327-01	B280000		4	SOCKET, connector pin
-1	670-0544-00	B010100	B149999	1	ASSEMBLY, circuit board—SCR
	670-0544-01	B150000	B249999	] ]	ASSEMBLY, circuit board—SCR ASSEMBLY, circuit board—SCR
	670-0544-02	B250000		'-	assembly includes:
	388-0878-00	B010100	B149999	1	BOARD, circuit
	388-0878-01	B150000	B249999	1	BOARD, circuit
	388-0878-02	B250000		1	BOARD, circuit
-2	352-0125-00			1	HOLDER, plastic, toroid, clear
-3	352-0134-00			1	HOLDER, plastic, toroid, black
-4	334-0143-00			4	CLIP, plastic, mounting mounting hardware for each: (not included w/clip)
-5	211-0097-00			1	SCREW, 4-40 x 5/16 inch, PHS
-5	210-0589-00			i	NUT, hex., locking, 4-40 x 1/4 inch
	2.0 000. 00				
-6	337-0950-00			1	SHIELD, electrical
-7	136-0220-00			10	SOCKET, transistor, 3 pin
-8	136-0235-00			1	SOCKET, transistor, 6 pin SOCKET, transistor, 3 pin
-9 -10	136-0183-00 214-0269-00			2 2	HEAT SINK
-10 -11	214-0506-00	B010100	B149999	26	PIN, test point
-11	214-0506-00	B150000	5147777	24	PIN, test point
-12	214-0579-00			14	PIN, connector, male
-13	131-0557-00	B010100	B14999	14	CONNECTOR, post
	131-0591-00	B150000		14	TERMINAL, pin
	19-0151-00			1	ASSEMBLY, crystal oven
1.4	200 0770 00			1	assembly includes: COVER, oven, outer
-14	200-0770-00			· .	mounting hardware: (not included w/cover)
-15	210-0589-00			2	NUT, hex., locking, 6-32 x 5/16 inch
	, , , , , , , , , , , , , , , , , ,				
-16	214-0952-00			1	INSULATOR, oven, thermal
-1 <i>7</i>	200-0769-00			1	COVER, oven, liner
-18	348-0126-00			]	PAD, cushioning
-19	205-0083-01			1	ASSEMBLY, heater winding INSULATOR, oven, thermal
-20 -21	214-0951-00 670-0548-00			1	ASSEMBLY, circuit board—oven mounting
-21	6/0-0346-00				assembly includes:
	388-0902-00		•	1	BOARD, circuit
-22	136-0263-00	B010100	B050389	14	SOCKET, pin connector
	136-0263-01	B050390		14	SOCKET, pin connector
-23	670-0547-00			1	ASSEMBLY, circuit board—CRYSTAL OVEN
		D010100	D000000		assembly includes:
	388-0880-00	B010100	B229999	]	BOARD, circuit
0.4	388-0880-02	B230000		1 3	BOARD, circuit SOCKET, transistor, 3 pin
-24 -25	136-0220-00 136-0234-00			2	SOCKET, transition, 3 pini SOCKET, crystal
-25 -26	214-0506-00			3	PIN, connector, male
20				•	

## FIG. 3 CIRCUIT BOARDS (cont)

	x Tektronix		I/Model No.	Q t	Description			
_No	. Part No.	Eff	Disc	у	1 2 3 4 5			
3-27	670-0537-00			1		ard—OUTPUT AMPLIFIER		
	388-0890-00			1	assembly includes: BOARD, circuit		,	
-28			•	4	SOCKET, transistor,	3 nin		
-29		•		27	SOCKET, transistor,	3 pin		
-30				2	SOCKET, transistor,			
-31				36	PIN, connector, ma			
-32			•	19	PIN, test point			
-33	21 4-0269-00		•	4	HEAT SINK, transist	for		
-34	670-0538-00			1	ASSEMBLY, circuit boo	ard—INPUT SYNC		
	388-0889-00			ī	assembly includes:			
	388-0889-00	B010100	B279999	1	BOARD, circuit BOARD, circuit	·		
	388-0889-01	B280000	52////	i	BOARD, circuit			
-35	136-0220-00			6	SOCKET, transistor,	3 nin		
-36	214-0506-00			45	PIN, connector, mal			
-37	21 4-0579-00			11	PIN, test point			
-38	337-0950-00			2	SHIELD, electrical			
-39	670-0539-00	B010100	B0149999	1	ASSEMBLY, circuit boa			
	670-0539-01	B150000	B259999	1	ASSEMBLY, circuit boo			
	67 <b>0</b> -0539-02 67 <b>0</b> -0539-03	B260000 B290000	B289999	1	ASSEMBLY, circuit boo			
	0/0-0337-03	B270000			ASSEMBLY, circuit boa assembly includes:	ird—DEMODULATOR		
	388-0877-00	B010100	B149999	1	BOARD, circuit			
	388-0877-01	B150000	2	i	BOARD, circuit			
	131-0557-00	XB150000	B160869	7	CONTACT, electrica	ľ		
	131-0591-00	B160870		7	TERMINAL, pin			
	344-0143-00	XB150000		2	CLIP, circuit board			
	211-0597-00	XB150000		2	SCREW, 4-40 x 0.312			
-40	210-0589-00 136-0220-00	XB150000 B010100	B149999	2	NUT, locking, 4-40 x			
-40	136-0220-00	B150000	D147777	27 29	SOCKET, transistor, SOCKET, transistor,			
-41	136-0235-00	D130000	•	4	SOCKET, transistor, o			
-42	136-0237-00			2	SOCKET, transistor, 8			
-43	214-0506-00	B010100	B149999	49	PIN, connector, male			
	214-0506-00	B150000		51	PIN, connector, male			
-44	214-0579-00			13	PIN, test point			
-45	337-0950-00			1	SHIELD, electrical			
-46	352-0125-00 352-0134-00			2 2	HOLDER, toroid			
	337-1031-00	XB080000	B169999X	1	HOLDER, toroid SHIELD, circuit board			
		ABOOOOO	BIOTTIA	-	mounting hardware: (no	ot included w/shield)		
	211-0504-00			2	SCREW, 6-32 x 0.25 inc			
-47	670-0540-00	B010100	B149999	1	ASSEMBLY, circuit book	rd—INPUT AMPLIFIER		
	670-0540-01	B150000		1	ASSEMBLY, circuit boar			
			•	-	assembly includes:			
	388-0888-00			1	BOARD, circuit			
-48	136-0220-00			9	SOCKET, transistor,	3 pin		
-49 50	352-0096-00			1	HOLDER, crystal	•		
-50 -51	214-0506-00 214-0579-00			22 6	PIN, connector, male			
-52	337-0950-00			2	PIN, test point SHIELD, electrical			
-53	352-0134-00			1	HOLDER, toroid			
-54	136-0234-00			2	SOCKET, crystal			

#### FIG. 3 CIRCUIT BOARDS (cont)

Fig. &				Q	
_	Tektronix	Seria	I/Model No.	t	Description
No.	Part No.	Eff	Disc	У	1 2 3 4 5
	<del></del>				
2.55	670-0533-00	DO10100	B149999	1	ASSEMBLY, circuit board—SWEEP
3-55		B010100	B259999	i	ASSEMBLY, circuit board—SWEEP
	670-0533-01	B150000			ASSEMBLY, circuit board—SWEEP
	670-0533-02	B260000	B289999	]	
	670-0890-01	B290000		1	ASSEMBLY, circuit board—SWEEP
				-	assembly includes:
	388-0882-00	B010100	B149999	1	BOARD, circuit
	388-0882-01	B150000		1	BOARD, circuit
	131-0566-00	XB150000		2	LINK, terminal
	136-0235-00	XB150000		1	SOCKET, transistor, 6 pin
-56	136-0183-00	•		1	SOCKET, transistor, 3 pin
-57	136-0220-00	B010100	B149999	24	SOCKET, transistor, 3 pin
	136-0220-00	B150000		26	SOCKET, transistor, 3 pin
-58	136-0237-00	B010100	B149999	5	SOCKET, transistor, 8 pin
	136-0237-00	B150000		6	SOCKET, transistor, 8 pin
-59	214-0506-00	B010100	B149999	68	PIN, connector, male
	214-0506-00	B150000		72	PIN, connector, male
-60	214-0579-00	B010100	B149999	24	PIN, test point
	214-0579-00	B150000		23	PIN, test point
-61	337-0950-00			1	SHIELD, electrical
-62	352-0125-00			1	HOLDER, toroid
-63	670-0536-00	B010100	B149999	1	ASSEMBLY, circuit board—DRIVER AMPLIFIER
•	670-0536-01	B150000	B199999	1	ASSEMBLY, circuit board—DRIVER AMPLIFIER
	670-0536-02	B200000		1	ASSEMBLY, circuit board—DRIVER AMPLIFIER
		220000		-	assembly includes:
	388-0896-00	B010100	B189999	1	BOARD, circuit
	388-0896-01	B190000	B199999	1	BOARD, circuit
	388-0896-02	B020000	B209999	1	BOARD, circuit
	388-0896-03	B210000	B272069	i	BOARD, circuit
	388-0896-04	B272070	<b>52. 200.</b>	i	BOARD, circuit
-64	136-0220-00	BZ/ 20/ 0		9	SOCKET, transistor, 3 pin
-65	214-0506-00	B010100	B069999	31	PIN, connector, male
-05	214-0506-00	B070000		32	PIN, connector, male
-66	214-0579-00	B0/ 0000		9	PIN, test point
-67	352-0125-00			í	HOLDER, toroid
-68	670-0532-00	B010100	B269999	i	ASSEMBLY, circuit board—LOW VOLTAGE POWER SUPPLY
-00	670-0532-01	B270000	DZO////	i	ASSEMBLY, circuit board—LOW VOLTAGE POWER SUPPLY
		B27 0000			assembly includes:
	200 0070 00			1	BOARD, circuit
/0	388-0879-00			5	SOCKET, transistor, 3 pin
-69 70	136-0183-00			4	SOCKET, transistor, 3 pin
-70	136-0220-00			1	SOCKET, transistor, 6 pin
-71 -70	136-0235-00			i	EYELET, gold plated
-72 -72	210-0652-00			41	PIN, connector, male
-73	214-0506-00			10	PIN, test point
-74	214-0579-00				mounting hardware: (not included w/assembly)
	011 011 ( 00	VD07000		- 4	SCREW, sems, 4-40 x 0.312 inch, PHB
	211-0116-00	XB270000		4	JCKLYY, SCIIIS, 4-40 X 0.312 IIICII, 1110

## FIG. 3 CIRCUIT BOARDS (cont)

Fig. & Index No.	Tektronix Part No.	Serial/Model Eff	No. Disc	Q t y	Description
<b>3</b> -75	670-0541-00			1	ASSEMBLY, circuit board—RECTIFIER
				-	assembly includes:
	388-0881-00			1	BOARD, circuit
-76	<b>2</b> 14-0506-00			25	PIN, connector, male
-77	352-0031-00			3	HOLDER, fuse
	·			-	mounting hardware for each: (not included w/holder)
-78	211-0012-00			1	SCREW, 4-40 x 3/8 inch, PHS
	210-0994-00			1	WASHER, flat, #4
	210-0586-00		•	1	NUT, keps, $4-40 \times \frac{1}{4}$ inch
-79	670-0535-00			1	ASSEMBLY, circuit board—R-Y B-Y FILTER
		•		-	assembly includes:
	388-0891-00			1	BOARD, circuit
	214-0506-00			8	PIN, connector, male
-81	670-0534-00			1	ASSEMBLY, circuit board—LUMINANCE FILTER
				-	assembly includes:
	388-0876-00			1	BOARD, circuit
				4	PIN, connector, male
-83	<i>670-</i> 061 <b>3</b> -00	XB150000		1	ASSEMBLY, circuit board—FEED BACK
	• • • • • • • • • • • • • • • • • • •			-	assembly includes:
	388-1014-00			1	BOARD, circuit
	136-0263-00			1	SOCKET, connector pin
-85	337-0896-00			1	SHIELD

### FIG. 4 REAR

Fig. & Index No.	Tektronix Part No.	Serial, Eff	/Model No. Disc	Q t y	Description 1 2 3 4 5
4-1	386-1252-00 386-1252-01	B010100 B070000	B069999	1	PLATE, rear sub-panel PLATE, rear sub-panel mounting hardware: (not included w/plate)
-2	212-0069-00			10	SCREW, 8-32 x 1/4 inch, THS
-3	386-1254-00			2	PLATE, trim mounting hardware for each: (not included w/plate)
-4	212-0506-00			2	SCREW, 10-32 x 3/8 inch, FHS
-5 -6 -7 -8 -9 -10	426-0326-03 426-0325-03 124-0201-00 361-0159-00 361-0160-00 426-0373-00 			1 1 2 1 1 1	FRAME, section, cabinet, left rear FRAME, section, cabinet, right rear STRIP, trim, blue SPACER, frame, right SPACER, frame, left FRAME, section, cabinet bottom mounting hardware: (not included w/frame) SCREW, 10-32 x 3/8 inch, FHS
-11	426-0374-00			1	FRAME, section, cabinet top mounting hardware: (not included w/frame)
-12	212-0506-00			4	SCREW, 10-32 x 3/8 inch, FHS
-13 -14 -15	124-0188-00 441-0742-00 			1 1 - 3 3	STRIP, trim, blue (Type R520 only) CHASSIS, Input Sync mounting hardware: (not included w/chassis) SCREW, $6-32 \times \frac{1}{4}$ inch, PHS SCREW, $6-32 \times \frac{3}{8}$ inch, THS
-16 -17	344-0143-00 344-0143-00  213-0088-00	B010100 B270000	B269999	6 2 -	CLIP, circuit board mounting CLIP, circuit board mounting mounting hardware for each: (not included w/clip) SCREW, thread forming, #4 x 1/4 inch, PHS
-18	131-0171-00 211-0542-00 210-0803-00 210-0202-00 210-0457-00			1 2 2 2 2 2	CONNECTOR, motor base mounting hardware: (not included w/connector) SCREW, 6-32 $\times$ $^5$ /16 inch, THS WASHER, flat, 0.150 ID $\times$ $^3$ /8 inch OD LUG, solder, SE #6 NUT, keps, 6-32 $\times$ $^5$ /16 inch
-19	204-0279-00			1	BODY, line voltage selector mounting hardware: (not included w/body)
-20	210-0407-00 210-0006-00			2 2	NUT, hex., 6-32 x 1/4 inch LOCKWASHER, internal #4
-21	200-0762-00			1	COVER, line voltage selector cover includes:
-22	352-0102-00			2	HOLDER, fuse mounting hardware for each: (not included w/holder)
-23	213-0088-00			2	SCREW, thread cutting, 4-40 x 1/4 inch

# FIG. 4 REAR (cont)

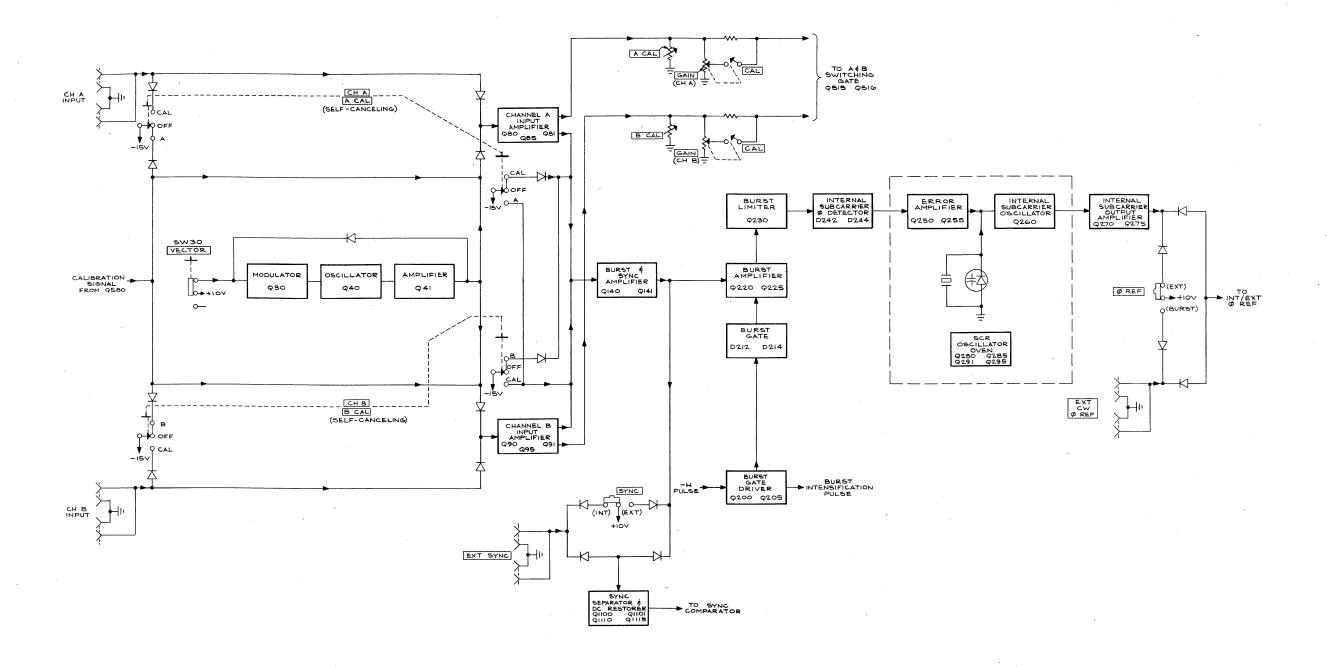
Fig. 8 Index No.	t Tektronix Part No.	Serial/ <i>N</i> Eff	Nodel No. Disc	Q t y	Description
<b>4-24</b> - <b>2</b> 5	200-0777-00			1	COVER, CRT socket access TRANSISTOR
-26 -27	211-0510-00 211-0511-00		•	1 1	mounting hardware for each: (not included w/transistor) SCREW, 6-32 x $\frac{3}{8}$ inch, PHS SCREW, 6-32 x $\frac{1}{2}$ inch, PHS
-28 -29	200-0669-00 386-0143-00			i 1	COVER, transistor PLATE, insulating, mica
-30 -31	210-0975-00 210-0803-00			2 .	WASHER, shouldered, 0.140 ID $\times$ $^{3}/_{8}$ inch OD WASHER, flat, 0.150 ID $\times$ $^{3}/_{8}$ inch OD
-32 -33	210-0303-00 210-0202-00 210-0457-00			1 2	LUG, solder, SE #6 NUT, keps, 6-32 x 5/16 inch
-34				. 1	TRANSISTOR
-35	211-0510-00			1	mounting hardware: (not included w/transistor) SCREW, $6-32 \times \frac{3}{8}$ inch, PHS
-36	211-0513-00 200-0692-00			1 1	SCREW, 6-32 x 5/8 inch, PHS COVER, transistor
-37 -38	386-0978-00 210-0975-00			1 2	PLATE, insulating, mica WASHER, shouldered, 0.140 ID x 3/8 inch OD
-39	210-0803-00			2	WASHER, flat, 0.150 ID x 3/8 inch OD
-40 -41	210-0202-00 210-0457-00			1 2	LUG, solder, SE #6 NUT, keps, 6-32 x <sup>5</sup> / <sub>16</sub> inch
-42				1	TRANSISTOR mounting hardware: (not included w/transistor)
-43 -44	210-0510-00			2	SCREW, 6-32 x 3/8 inch, PHS
-44	386-0978-00 210-0975-00			1 2	PLATE, insulating, mica WASHER, shouldered, 0.140 ID x 3/8 inch OD
	210-0803-00 210-0202-00			2 1	WASHER, flat, 0.150 ID $\times$ $\frac{3}{8}$ inch OD LUG, solder, SE #6
	210-0457-00			2	NUT, keps, 6-32 x <sup>5</sup> / <sub>16</sub> inch
-45	200-0805-00 200-0500-00	B010100 B030000	B029999	1	COVER, transistor shield COVER, transistor, black plastic
-46	211-0061-00			2	mounting hardware: (not included w/cover) SCREW, $4-40 \times \frac{1}{2}$ inch, FIL HS
-47	210-0586-00			2	NUT, keps, 4-40 x 1/4 inch
-48				3	RESISTOR, variable
-49 50	210-0840-00			1	mounting hardware for each: (not included w/resistor) WASHER, flat, 0.390 ID x %16 inch OD NUT have 3/ 22 v 1/ v 7/ in the
-50	210-0421-00			1	NUT, hex., $\frac{3}{8}$ -32 x $\frac{1}{2}$ x $\frac{7}{16}$ inch
-51			•	1	RESISTOR, variable mounting hardware: (not included w/resistor)
-52 -53	210-0012-00 210-0207-00			1	LOCKWASHER, internal, $\frac{3}{8}$ ID x $\frac{1}{2}$ inch OD
-53 -54	210-0421-00			1	LUG, solder, $\frac{3}{8}$ ID × $\frac{5}{8}$ inch OD, SE NUT, hex., $\frac{3}{8}$ -32 × $\frac{1}{2}$ × $\frac{7}{16}$ inch

### FIG. 4 REAR (cont)

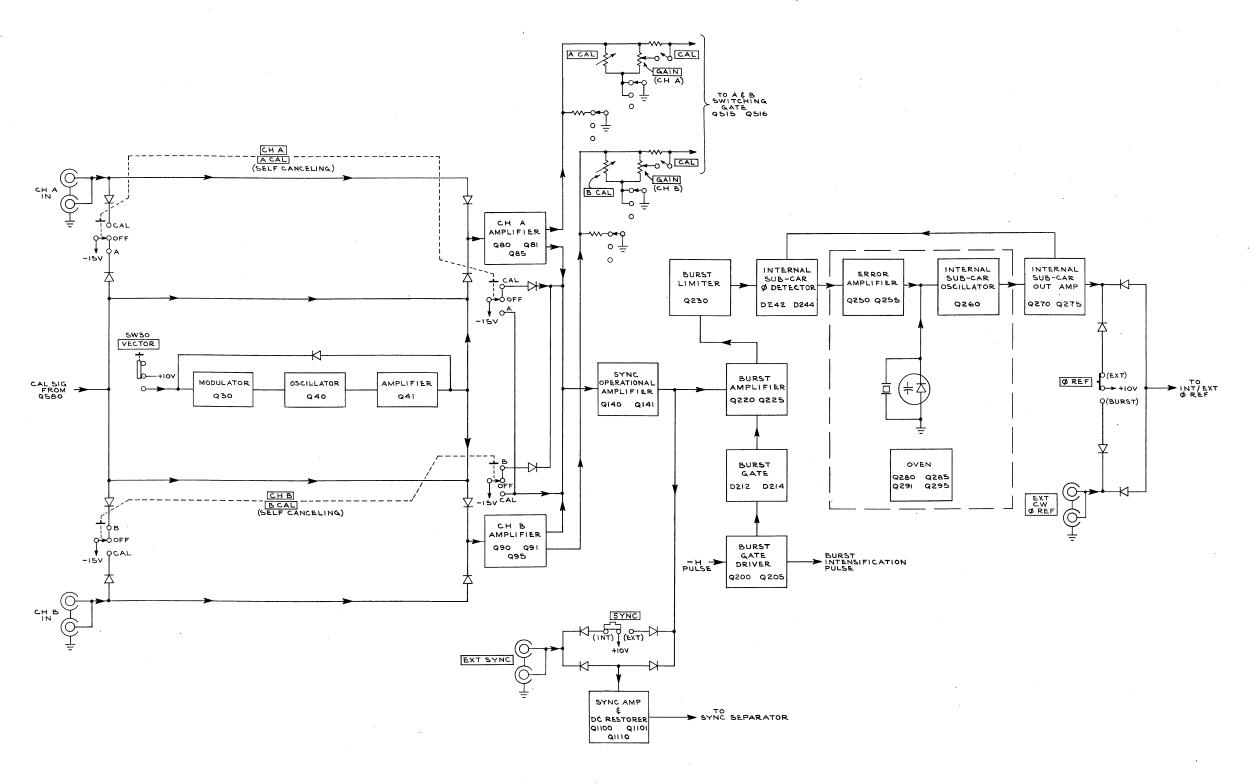
Fig. & Index No.		Serial/M Eff	Nodel No. Disc	Q t y	Description 1 2 3 4 5
4-55 -56	131-0081-00 131-0126-00 131-0081-00 131-0081-00 131-0126-00 	B010100 B180000 B010100 B020000 B180000	B179999 B019999 B179999	5 5 4 3 4	CONNECTOR, 1 contact, UHF w/hardware CONNECTOR, 1 contact, BNC w/hardware CONNECTOR, 1 contact, UHF w/hardware CONNECTOR, 1 contact, UHF w/hardware CONNECTOR, 1 contact, UHF w/hardware CONNECTOR, 1 contact, BNC w/hardware mounting hardware for each: (not included w/connector) LUG, solder connector
· ·	131-0302-00 131-0320-00 131-0274-00 210-0207-00 210-0814-00 210-0865-00 210-0255-00 210-0840-00	B020000 B070000 B180000 B020000 B020000 B020000 B020000 B020000	B069999 B179999	1 1 1 1 1 1	CONNECTOR, 1 contact, UHF CONNECTOR, 1 contact, UHF w/hardware CONNECTOR, 1 contact, BNC w/hardware mounting hardware: (not included w/connector) LUG, solder, 3/8 inch WASHER, fiber, 3/8 ID x 5/8 inch OD WASHER, fiber, 3/8 inch UG, solder, 3/8 inch WASHER, flat, 0.390 ID x 9/16 inch OD
-58 -59 -60	200-0776-00 211-0008-00 210-0586-00			1 - 2 2	COVER, connector access mounting hardware: (not included w/cover) SCREW, 4-40 $\times$ $\frac{1}{4}$ inch, PHS NUT, keps, 4-40 $\times$ $\frac{1}{4}$ inch
-61 -62	385-0018-00 211-0542-00			2	ROD, plastic, $\frac{5}{16} \times 1\frac{1}{4}$ inches mounting hardware for each: (not included w/rod) SCREW, $6-32 \times \frac{5}{16}$ inch, THS
-63 -64 -65	343-0005-00  210-0803-00 211-0507-00	·		2	CLAMP, cable, $\frac{7}{16}$ inch plastic mounting hardware for each: (not included w/clamp) WASHER, flat, 0.150 ID x $\frac{3}{6}$ inch OD SCREW, 6-32 x $\frac{5}{16}$ inch, PHS
-66 -67	129-0006-00  210-0401-00			3	POST, connecting, insulated mounting hardware for each: (not included w/post) NUT, cap, hex., 6-32 x 5/16 inch
-68 -69	337-0993-00 367-0073-00 367-0073-01 367-0073-02 213-0155-00	B010100 B210000 B220000	B209999 B219999	1 1 1 1	SHIELD, electrical HANDLE, carrying (Type 520 only) HANDLE, carrying (Type 520 only) HANDLE, carrying (Type 520 only) mounting hardware: (not included w/handle) SCREW, 10-32 x 0.40 inch long, machine (Type 520 only)
-71 -72 -73 -74 -75	386-1352-00 200-0728-00 179-1217-00 343-0088-00 343-0089-00			2 1 1 1	PLATE, plastic, mounting (Type 520 only)  COVER, plastic, handle (Type 520 only)  CABLE HARNESS, line voltage selector  CLAMP, plastic, small  CLAMP, plastic, large

## FIG. 5 CABINET & FRAME

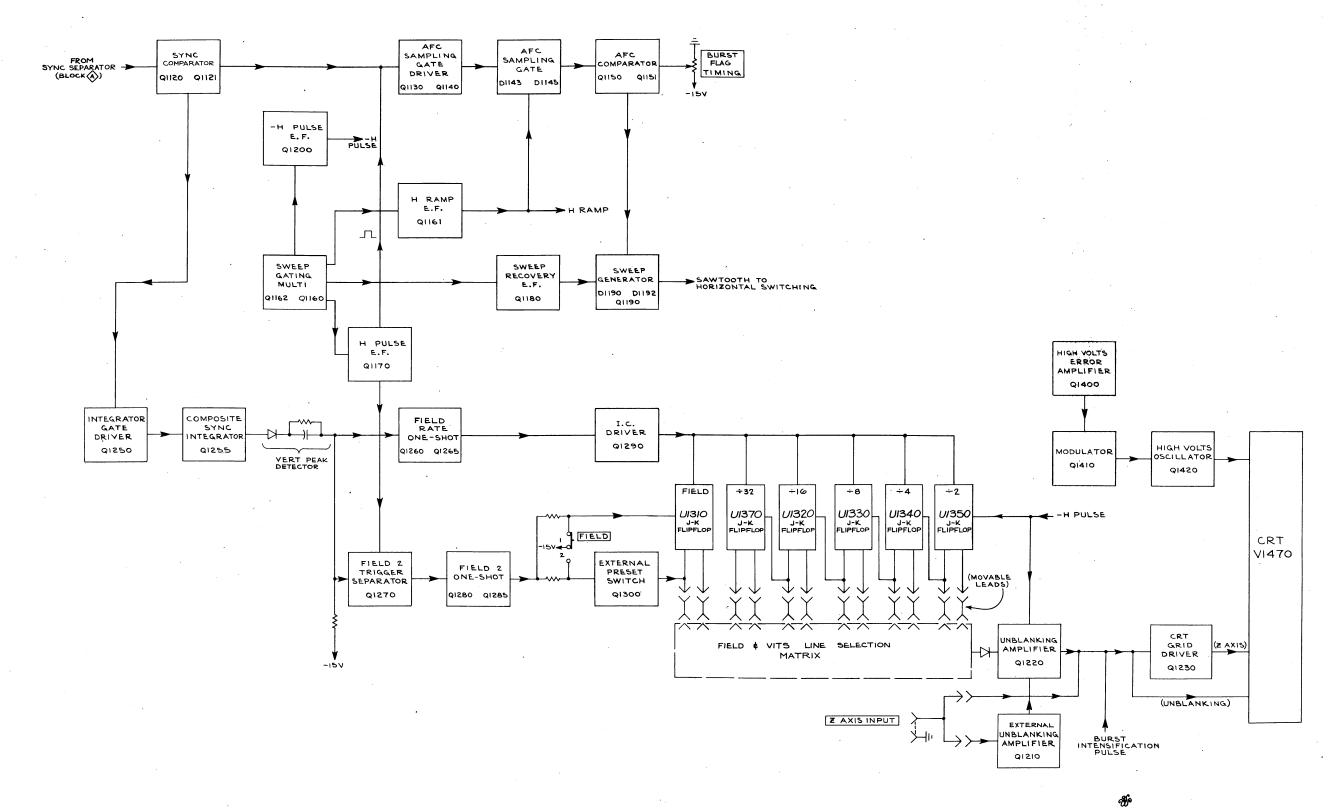
Fig. & Index No.		Serial/Model Eff	No. Disc	Q † y	Description 1 2 3 4 5
5-1	390-0010-00			1	CABINET, top
J-1	370-0010-00			1	cabinet includes:
-2	214-0812-00			4	ASSEMBLY, latch
-4-	214-0012-00		÷	-	each assembly includes:
-3	214-0603-01			1	PIN, securing
-4	214-0604-00			i	SPRING
-5	386-0227-00			1	PLATE, plastic, index
-6	386-0226-00			1	PLATE, locking
-7	390-0011-00	•		1	CABINET, bottom
		•		•	cabinet includes:
-8	214-0812-00			4	ASSEMBLY, latch
_				-	each assembly includes:
-9	214-0603-01			1	PIN, securing
	214-0604-00			]	SPRING
-11	386-0227-00			!	PLATE, plastic, index
	386-0226-00			1	PLATE, locking
-13	426-0372-00			1	FRAME, section, right
	212-0506-00			4	mounting hardware: (not included w/frame) SCREW, 10-32 x <sup>3</sup> / <sub>8</sub> inch, FHS
-14	426-0371-00			1	FRAME, section, left
					mounting hardware: (not included w/frame)
-15	212-0506-00			4	SCREW, 10-32 x 3/8 inch, FHS
-16	351-0104-00			1	SLIDE, section tilt type, 1 pair, (Type R520 only)
				-	mounting hardware: (not included w/slide)
	212-0068-00			3	SCREW, 8-32 x 5/16 inch, THS
-1 <i>7</i>	348-0080-01			4	FOOT, plastic, (Type 520 only)
			•	-	mounting hardware for each: (not included w/foot)
-18	211-0511-00			1	SCREW, 6-32 x 1/2 inch, PHS
-19	210-0006-00			1	LOCKWASHER, internal #6

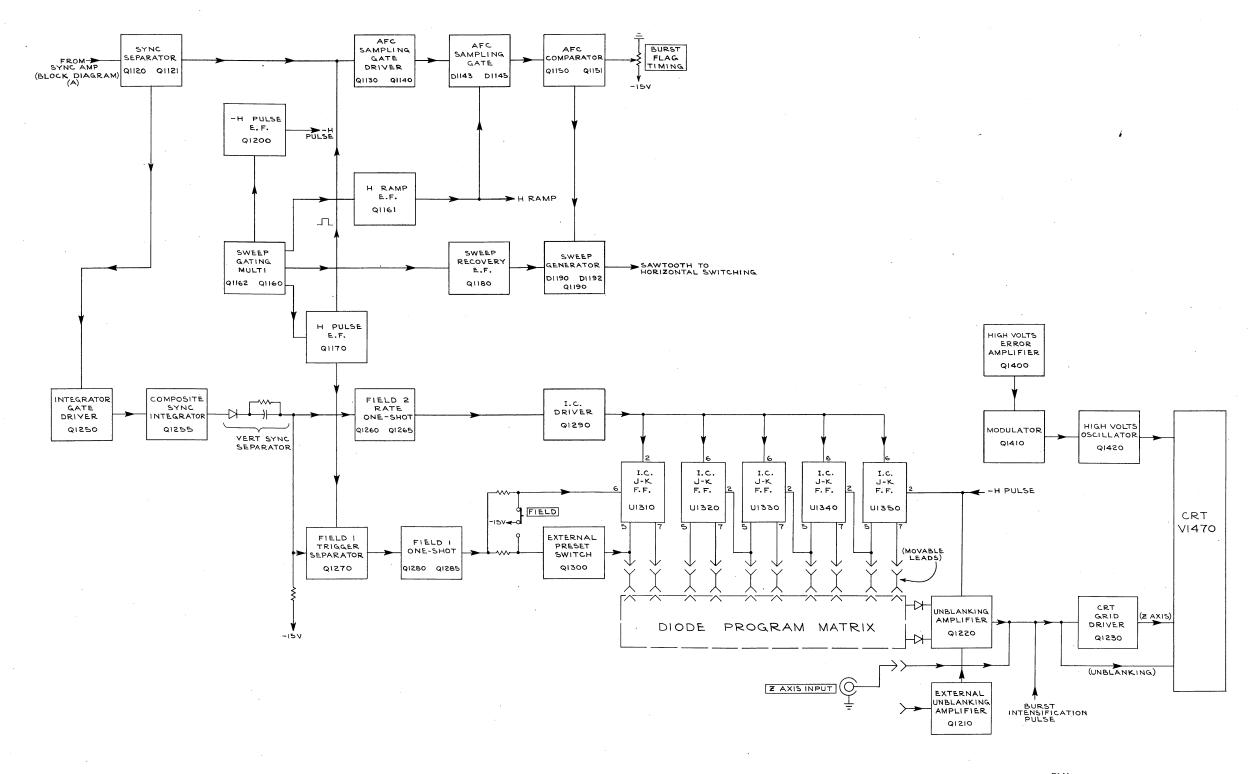


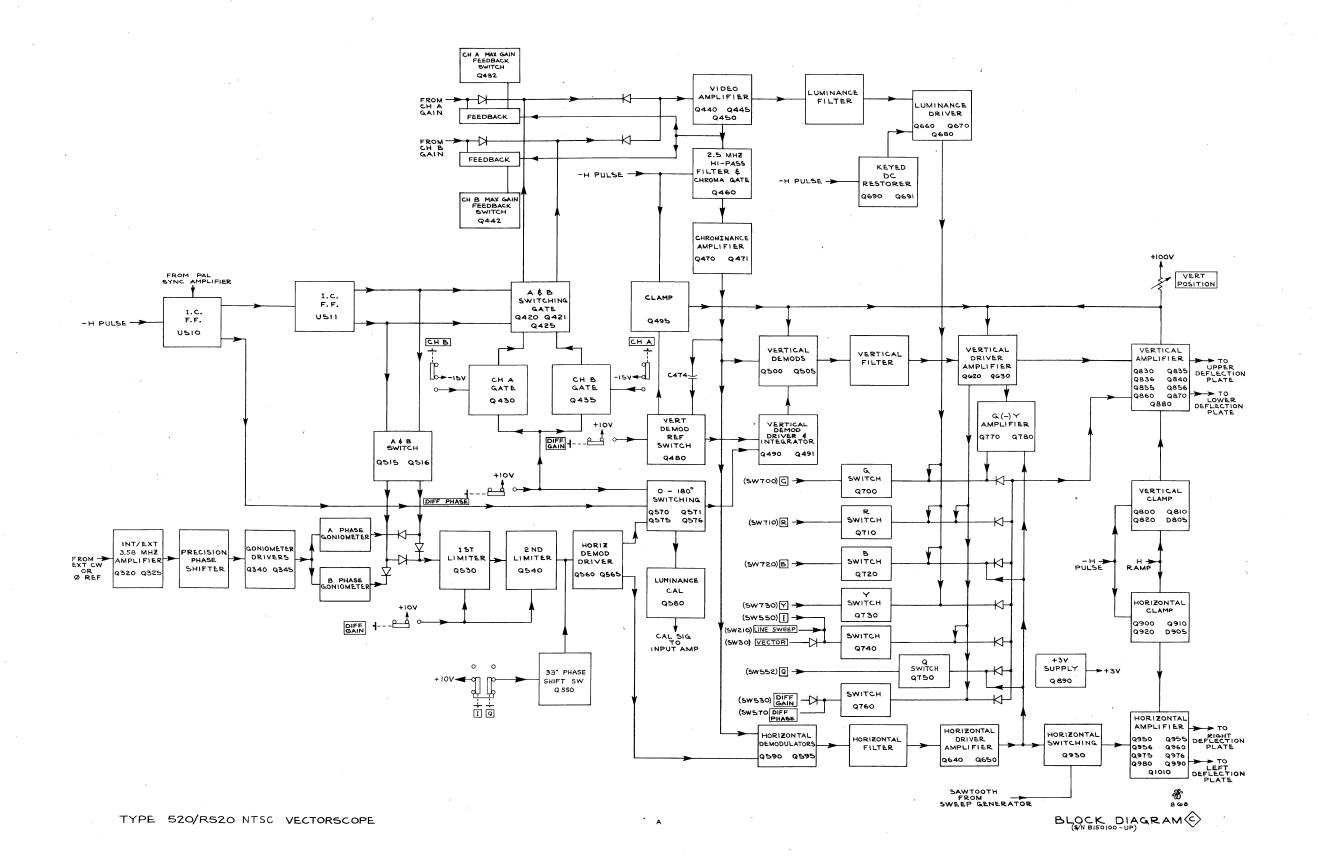
BLOCK DIAGRAM (A)

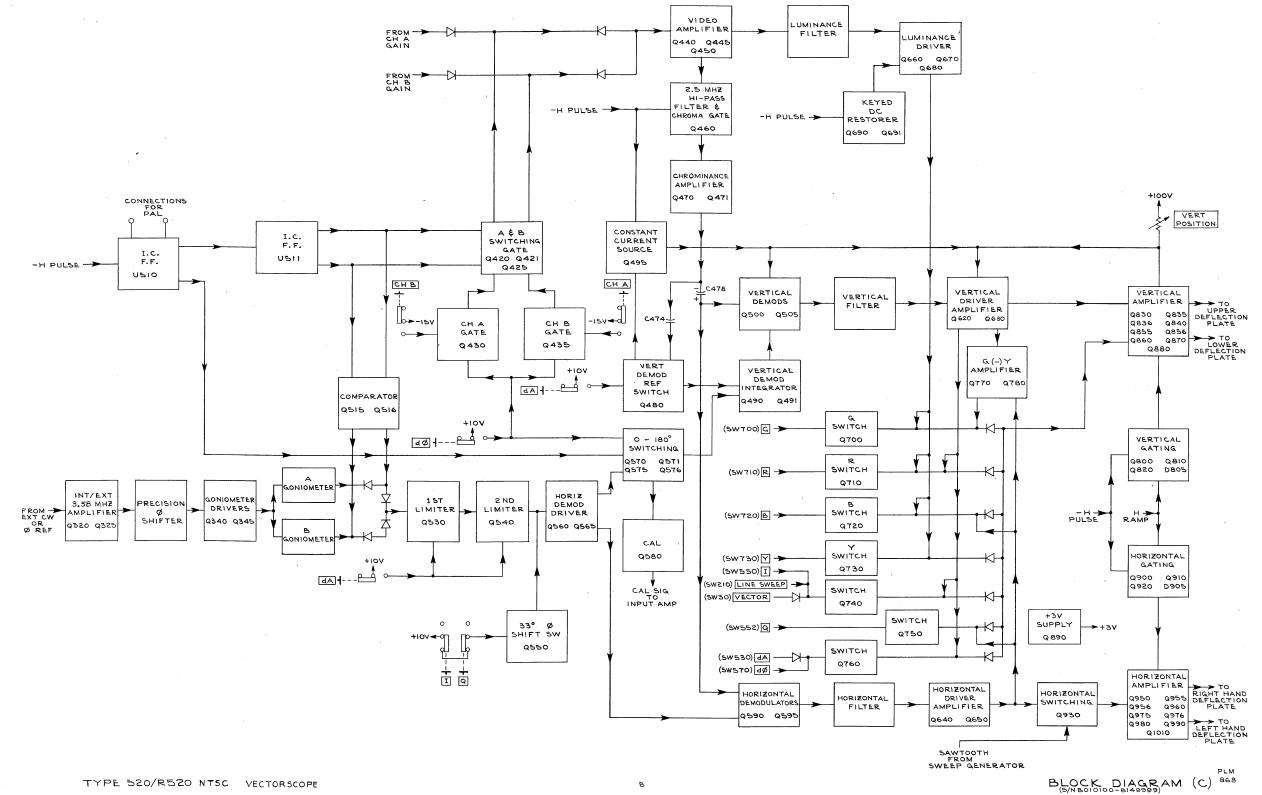


BLOCK DIAGRAM (A)









#### VOLTAGE AND WAVEFORM CONDITIONS

Circuit voltages measured with a 20,000  $\Omega$ /volt VOM, All reading in volts. Voltages are measured with respect to chassis ground unless otherwise noted. Numbers contained in parenthesis are the peak to peak voltage value of the reference subcarrier.

Waveforms shown are actual waveform photographs taken with a Tektronix Oscilloscope Camera System and Projected Graticule.

Voltages and waveforms on the diagrams (shown in blue) are not absolute and may vary between instruments because of differing component tolerances, internal calibration or front-panel control settings.

The test oscilloscope used had the following characteristics: deflection factor, 1 mV/cm to 50 V/cm; frequency response, DC to 8 MHz; sweep rates, 0.1  $\mu$ s/cm to 5 s/cm; DC input coupling was used unless otherwise specified.

Chassis ground was used for all voltage readings and as probe ground for all waveforms taken.

A standard color bar signal was connected to channel A input of the Type R520 for all waveforms and voltage readings unless otherwise specified.

The trigger source for the test oscilloscope is specified on the individual diagrams.

#### Type R520 Controls

For all front and rear panel screwdriver adjustments refer to the calibration section of this manual.

POWER ON SCALE ILLUM As desired INTENSITY As desired

FOCUS A well defined display
CH A and CH B GAIN CAL

100%-75%-MAX GAIN 75%

Signal Selector CH A, B CAL, FULL

FIELD and  $A\Phi/B\Phi$ 

ALT

A PHASE Position Burst to the

180° position on the

vector graticule.

B PHASE No affect  $\Phi$  REF BURST

Display Selector VECTOR
CALIBRATED PHASE 0

CALIBRATED PHASE 0
LUMINANCE GAIN CAL
FIELD 2
SYNC INT

BURST FLAG TIMING As set forth in oper-

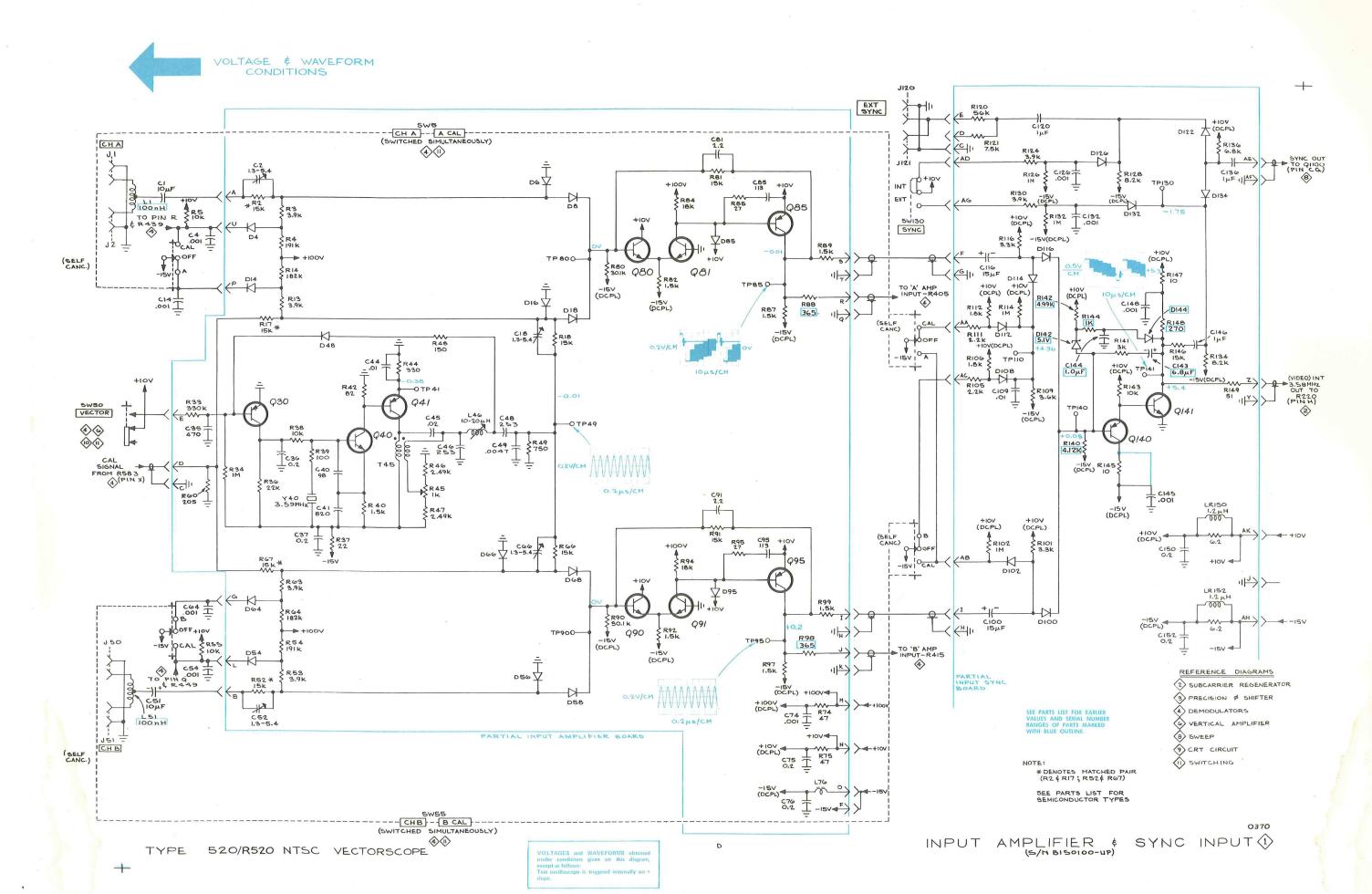
ating instructions,

First-Time Operating

Procedure.

#### WARNING

"Ground lugs" and shield braids are not always at ground potential. Check the schematic before using such connections as a ground for the voltmeter test prod or oscilloscope probe. Some transistor cases may be elevated from 0 to 275 V. This warning note also applies to recessed screws that hold the low voltage power supply transistors to the rear panel.



#### **VOLTAGE AND WAVEFORM CONDITIONS**

Circuit voltages measured with a 20,000  $\Omega$ /volt VOM, All reading in volts. Voltages are measured with respect to chassis ground unless otherwise noted. Numbers contained in parenthesis are the peak to peak voltage value of the reference subcarrier.

Waveforms shown are actual waveform photographs taken with a Tektronix Oscilloscope Camera System and Projected Graticule.

Voltages and waveforms on the diagrams (shown in blue) are not absolute and may vary between instruments because of differing component tolerances, internal calibration or front-panel control settings.

The test oscilloscope used had the following characteristics: deflection factor, 1 mV/cm to 50 V/cm; frequency response, DC to 8 MHz; sweep rates, 0.1  $\mu$ s/cm to 5 s/cm; DC input coupling was used unless otherwise specified.

Chassis ground was used for all voltage readings and as probe ground for all waveforms taken.

A standard color bar signal was connected to channel A input of the Type R520 for all waveforms and voltage readings unless otherwise specified.

The trigger source for the test oscilloscope is specified on the individual diagrams.

#### Type R520 Controls

For all front and rear panel screwdriver adjustments refer to the calibration section of this manual.

POWER ON

SCALE ILLUM As desired

INTENSITY As desired

FOCUS A well defined display

CH A and CH B GAIN CAL

100%-75%-MAX GAIN 75%

Signal Selector CH A, B CAL, FULL

FIELD and  $A\Phi/B\Phi$ 

ALT

A PHASE Position Burst to the

180° position on the vector graticule.

 B PHASE
 No affect

 Φ REF
 BURST

 Display Selector
 VECTOR

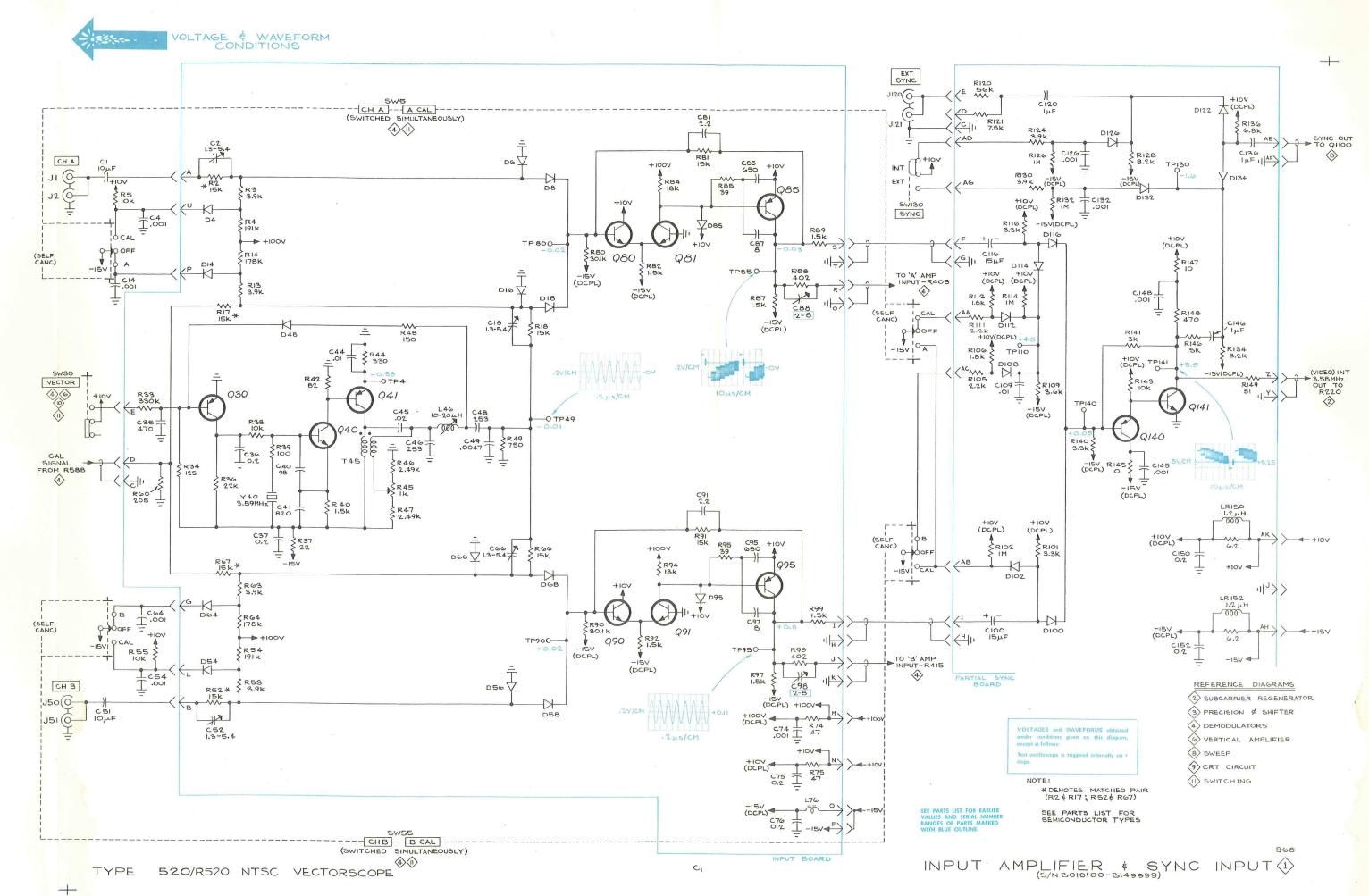
Display Selector VECTO
CALIBRATED PHASE 0
LUMINANCE GAIN CAL
FIELD 2

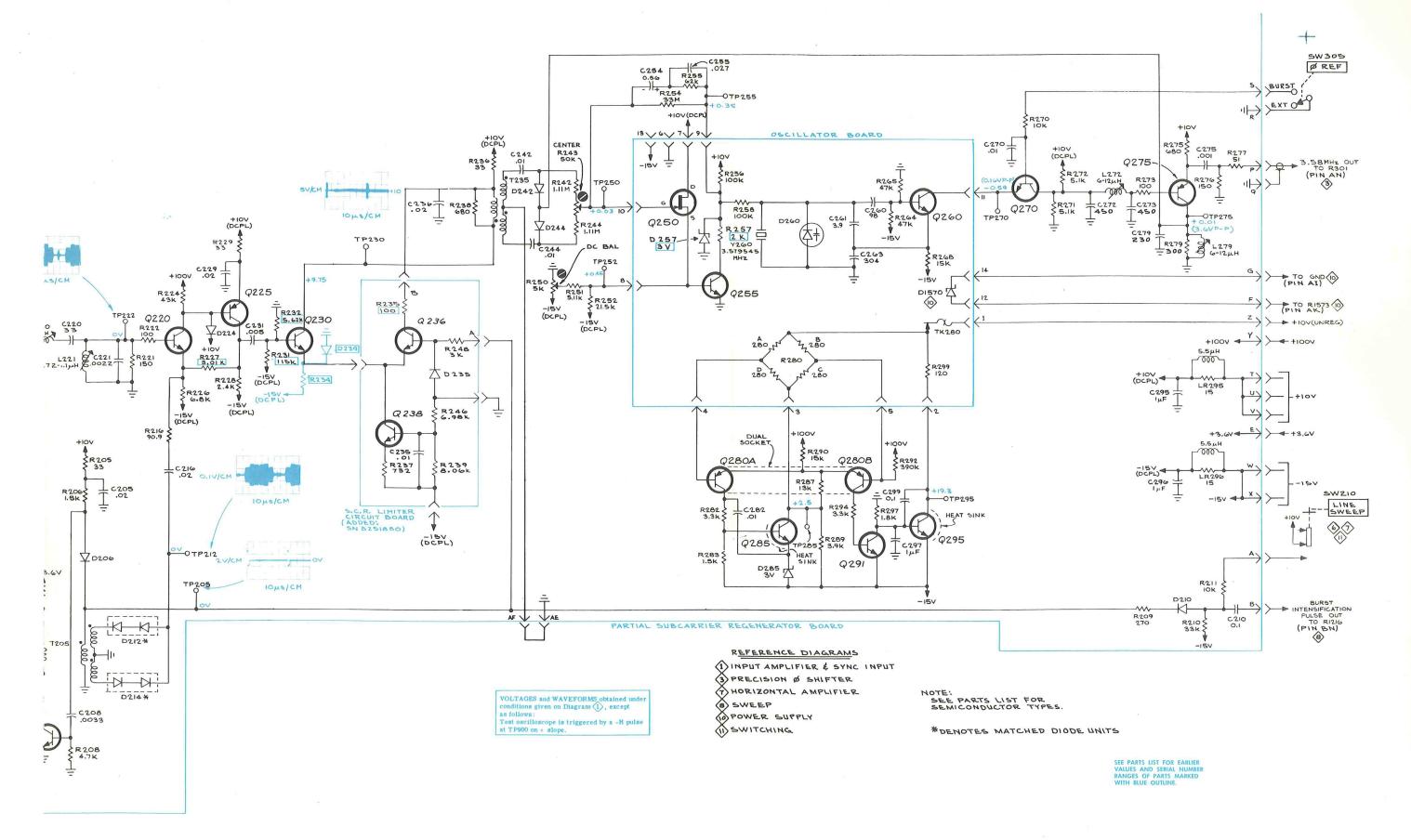
SYNC INT
BURST FLAG TIMING As

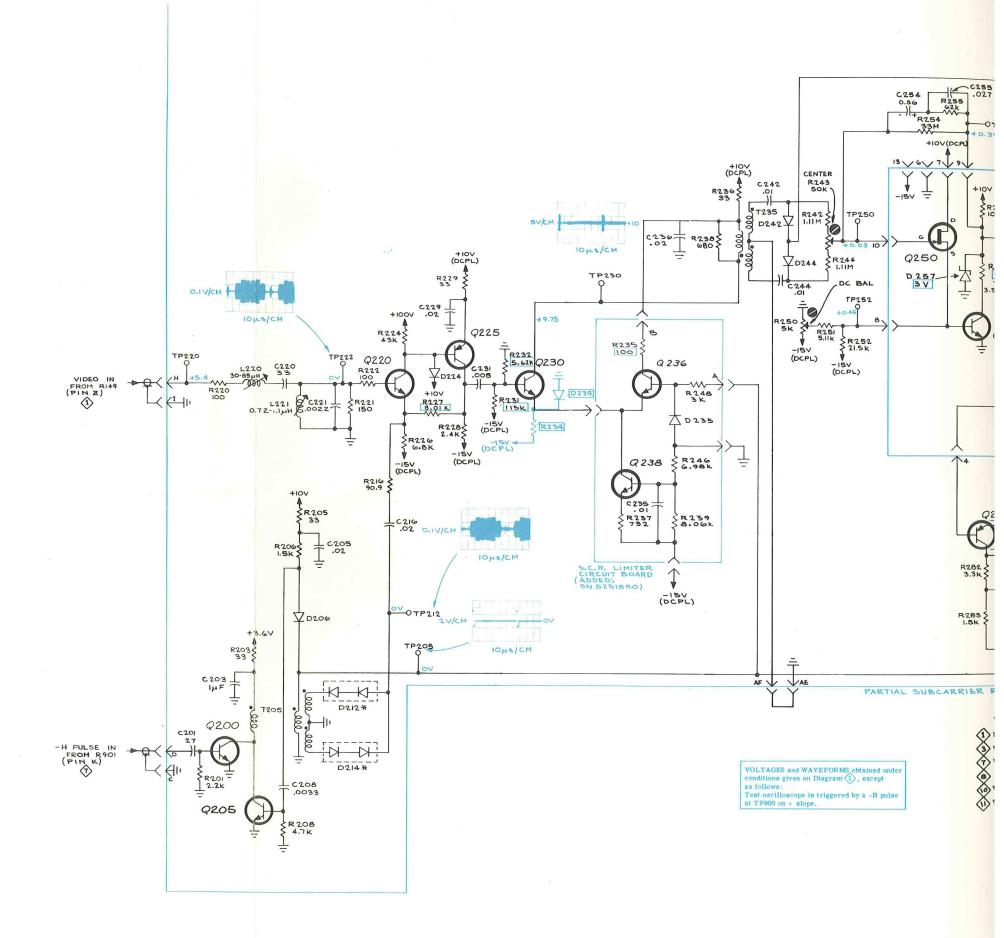
As set forth in operating instructions, First-Time Operating Procedure.

#### WARNING

"Ground lugs" and shield braids are not always at ground potential. Check the schematic before using such connections as a ground for the voltmeter test prod or oscilloscope probe. Some transistor cases may be elevated from 0 to 275 V. This warning note also applies to recessed screws that hold the low voltage power supply transistors to the rear panel.

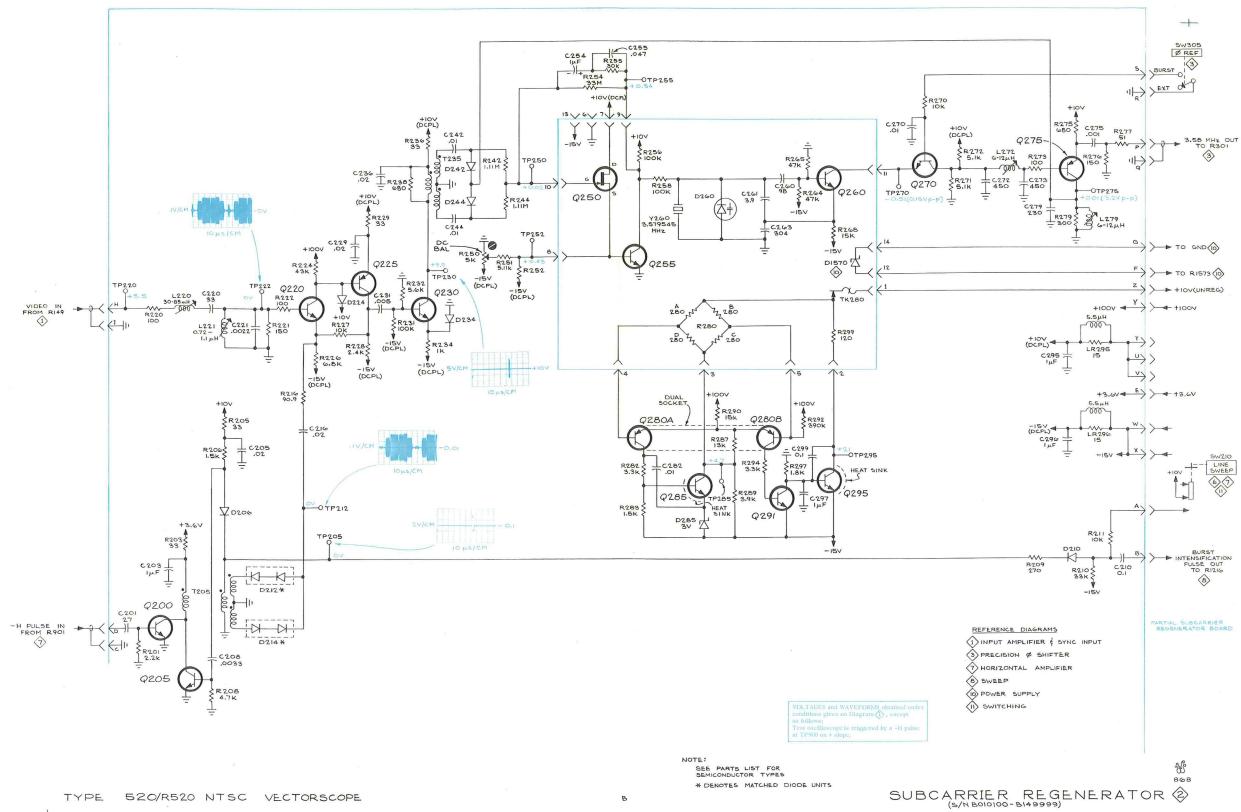


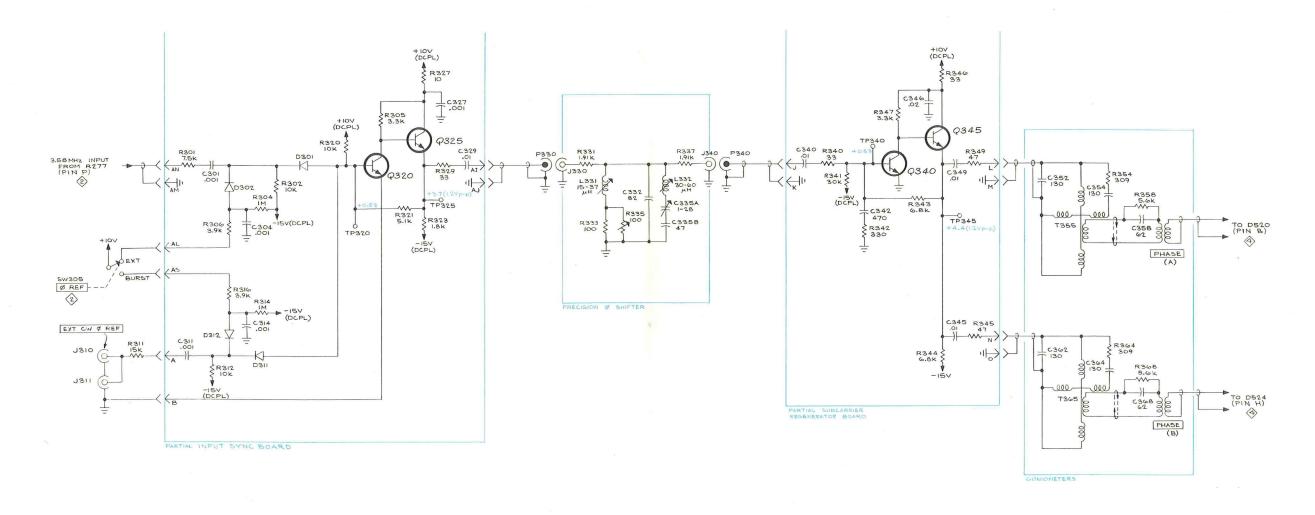




TYPE 520/R520 NTSC VECTORSCOPE

+





REFERENCE DIAGRAMS

INPUT AMPLIFIER & SYNC INPUT

SUBCARRIER REGENERATOR 4 DEMODULATORS

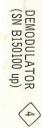
9 CRT CIRCUIT

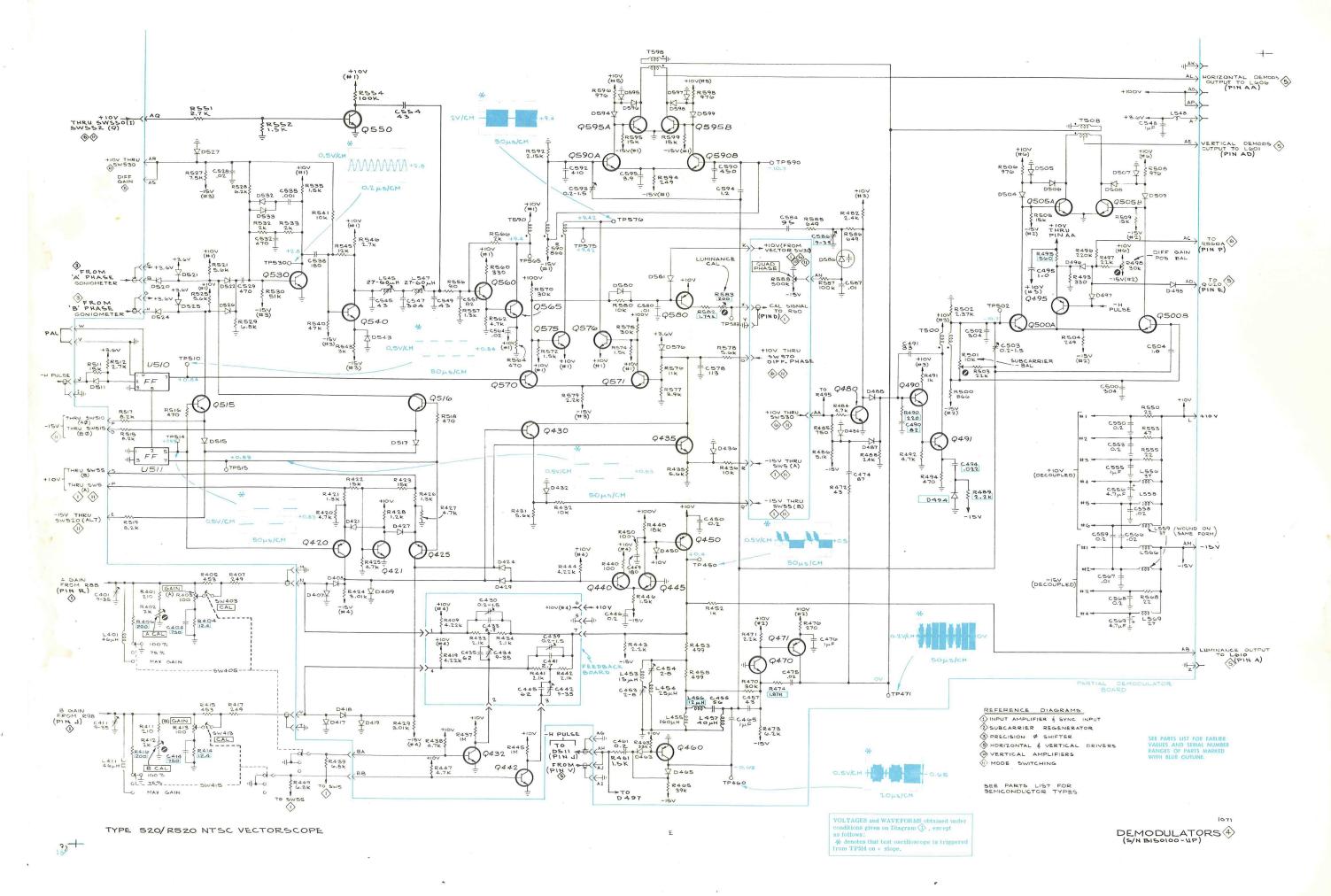
SEE PARTS LIST FOR SEMICONDUCTOR TYPES

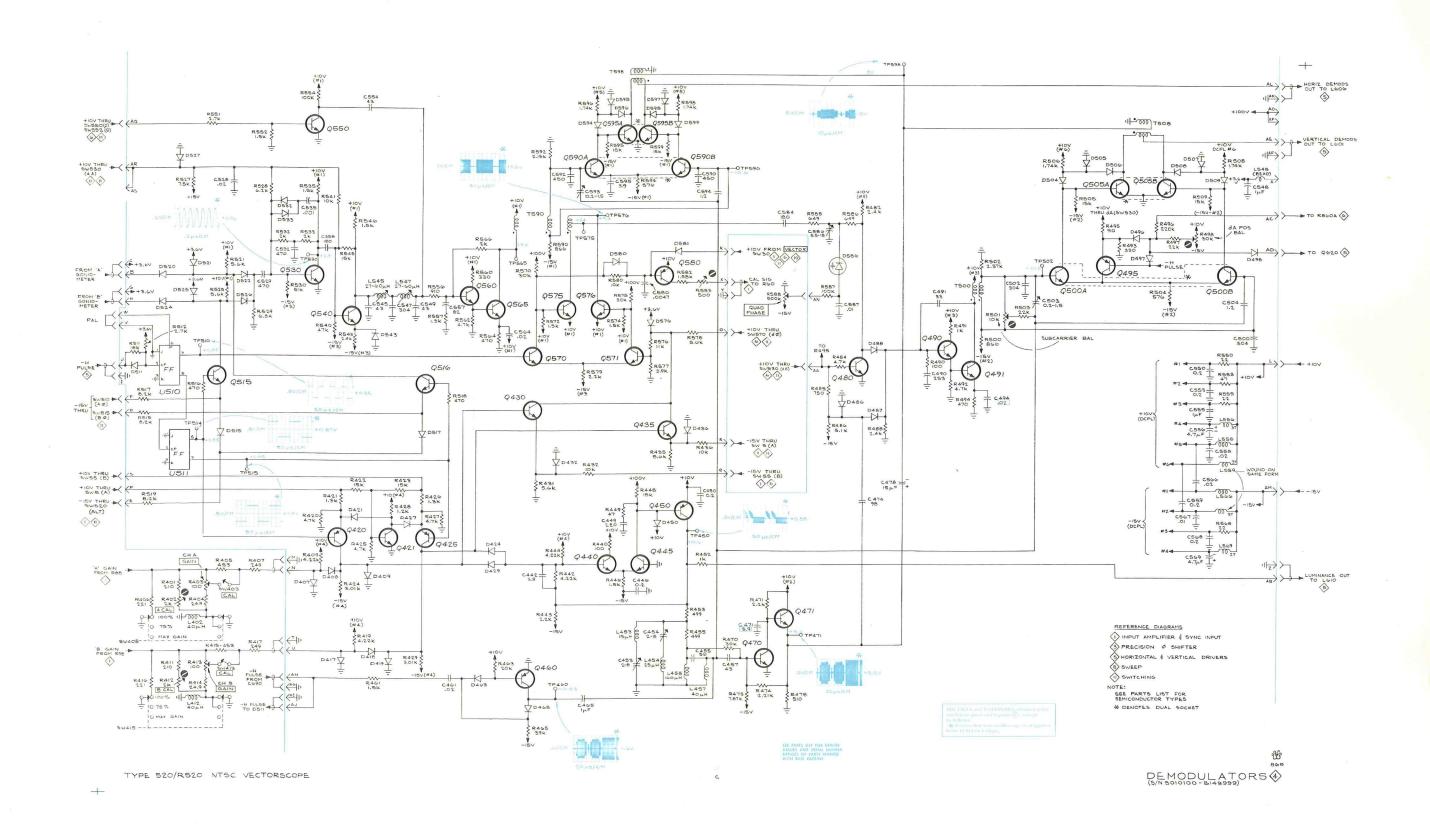
NOTE:

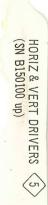
PRECISION Ø SHIFTER 3

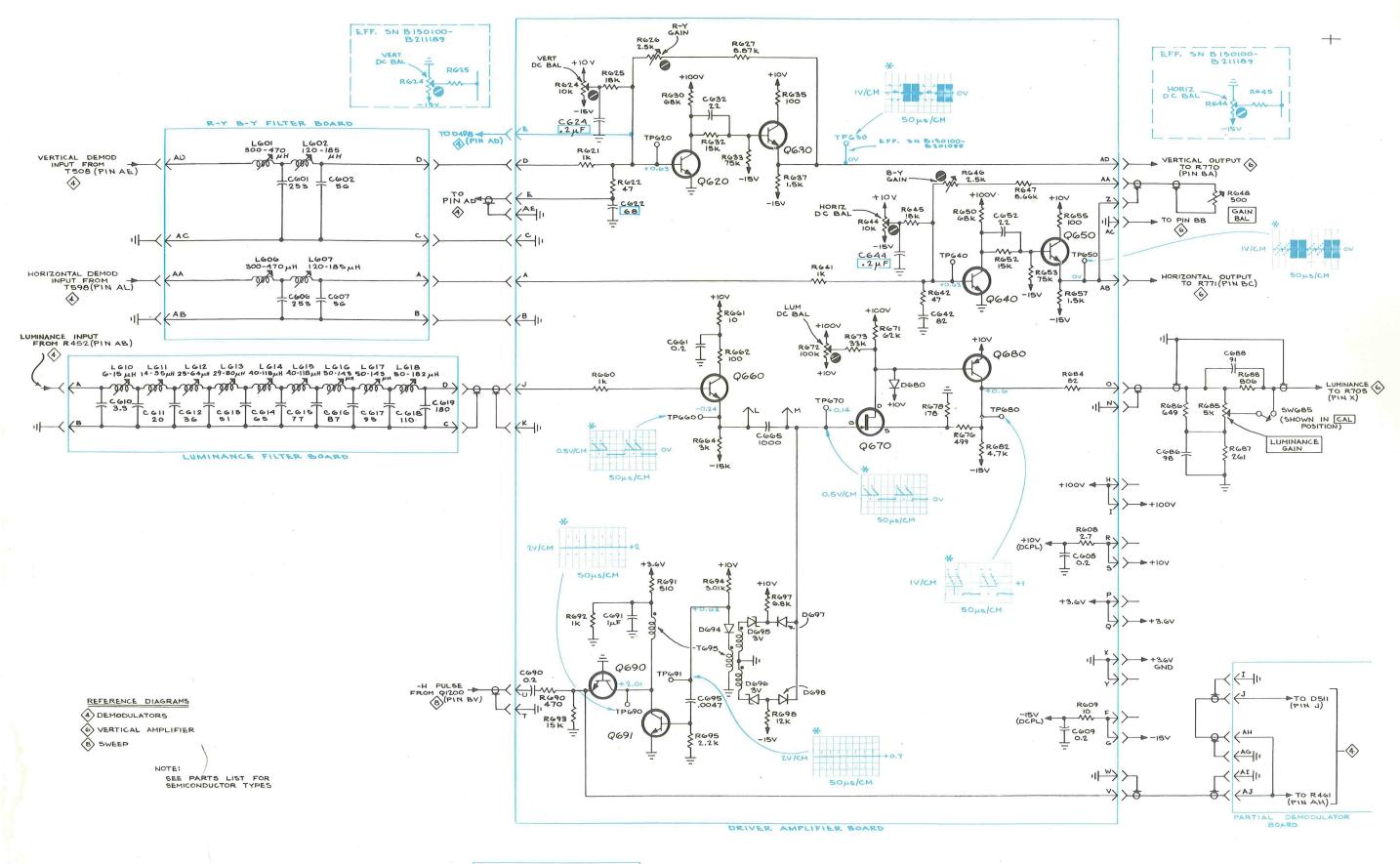
TYPE 520/R520 NTSC VECTORSCOPE









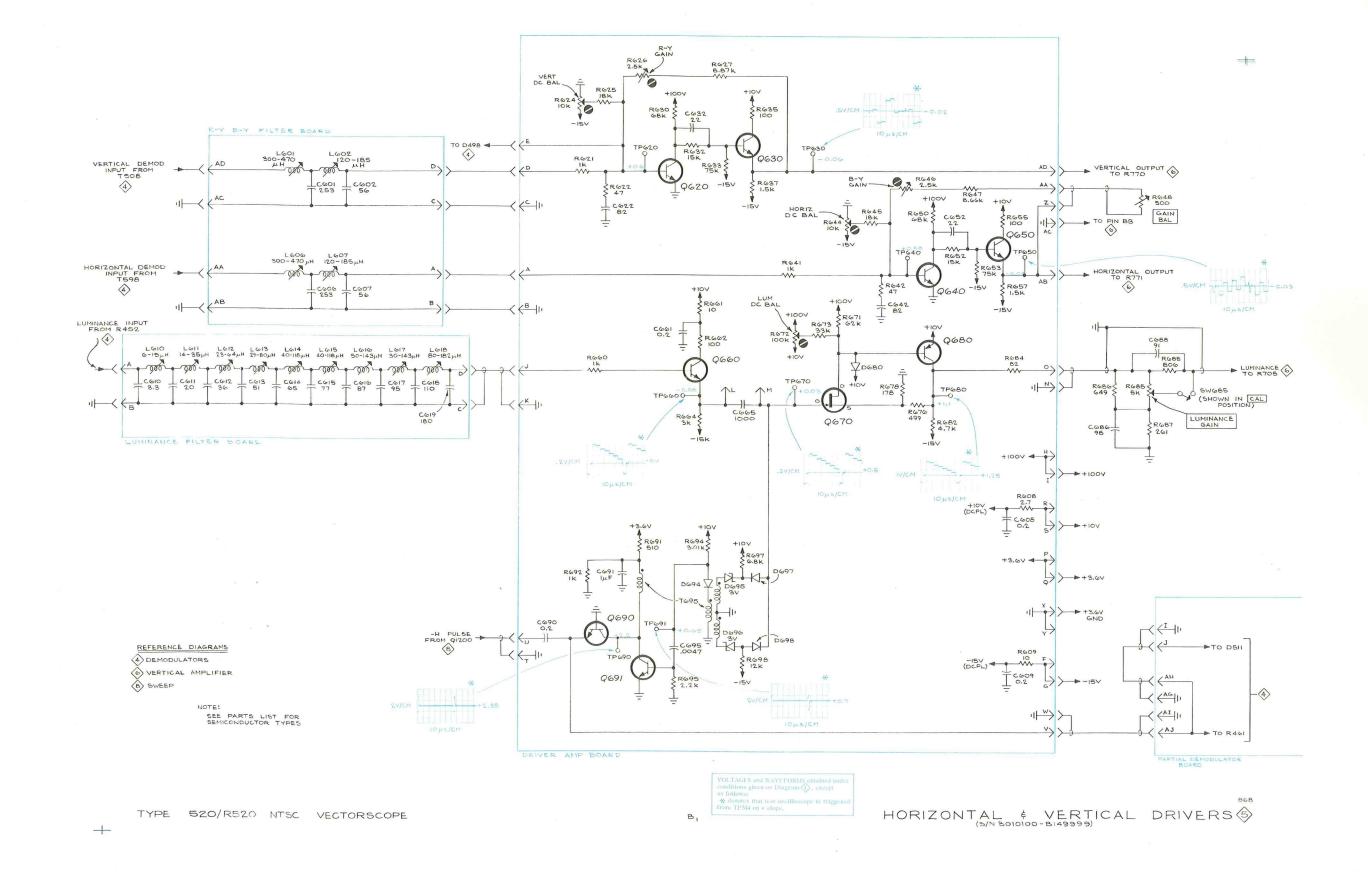


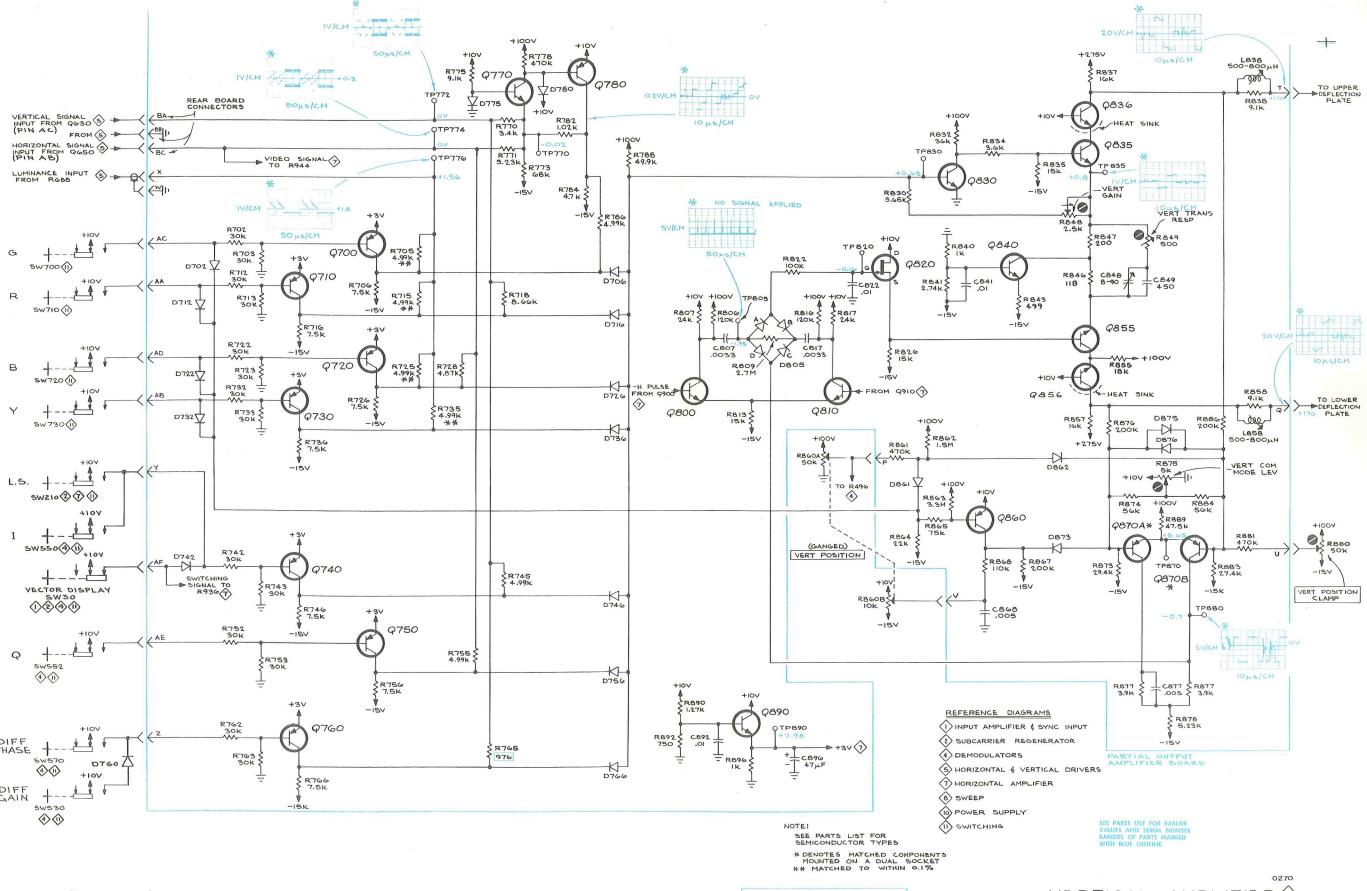
TYPE 520/R520 NTSC VECTORSCOPE

VOLTAGES and WAVEFORMS obtained under conditions given on Diagram (1), except as follows:

\*\*X\* denotes that test oscilloscope is triggered from TP 514 on + slope.

HORIZONTAL & VERTICAL DRIVERS \$





TYPE 520/R520 NTSC VECTORSCOPE

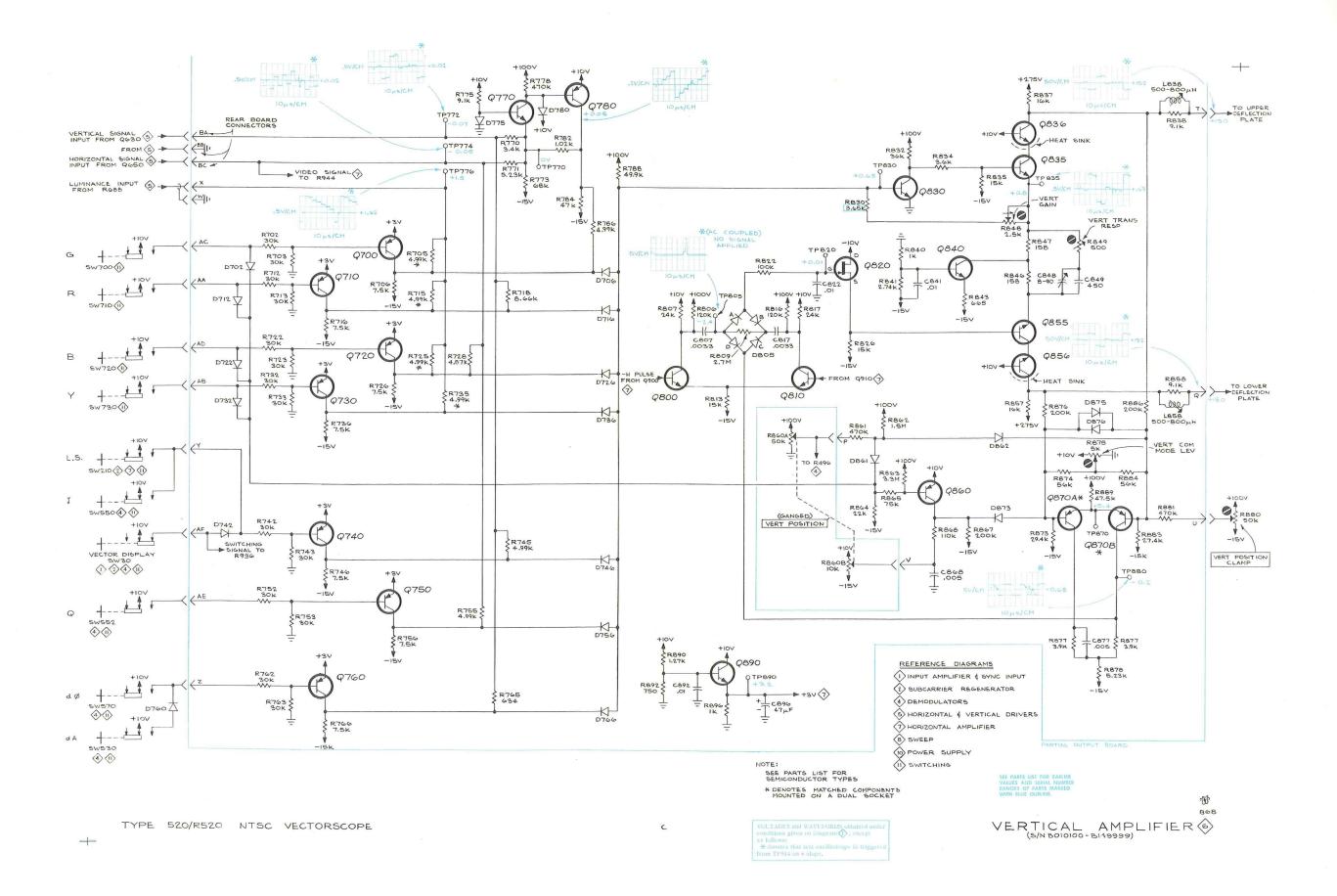
+

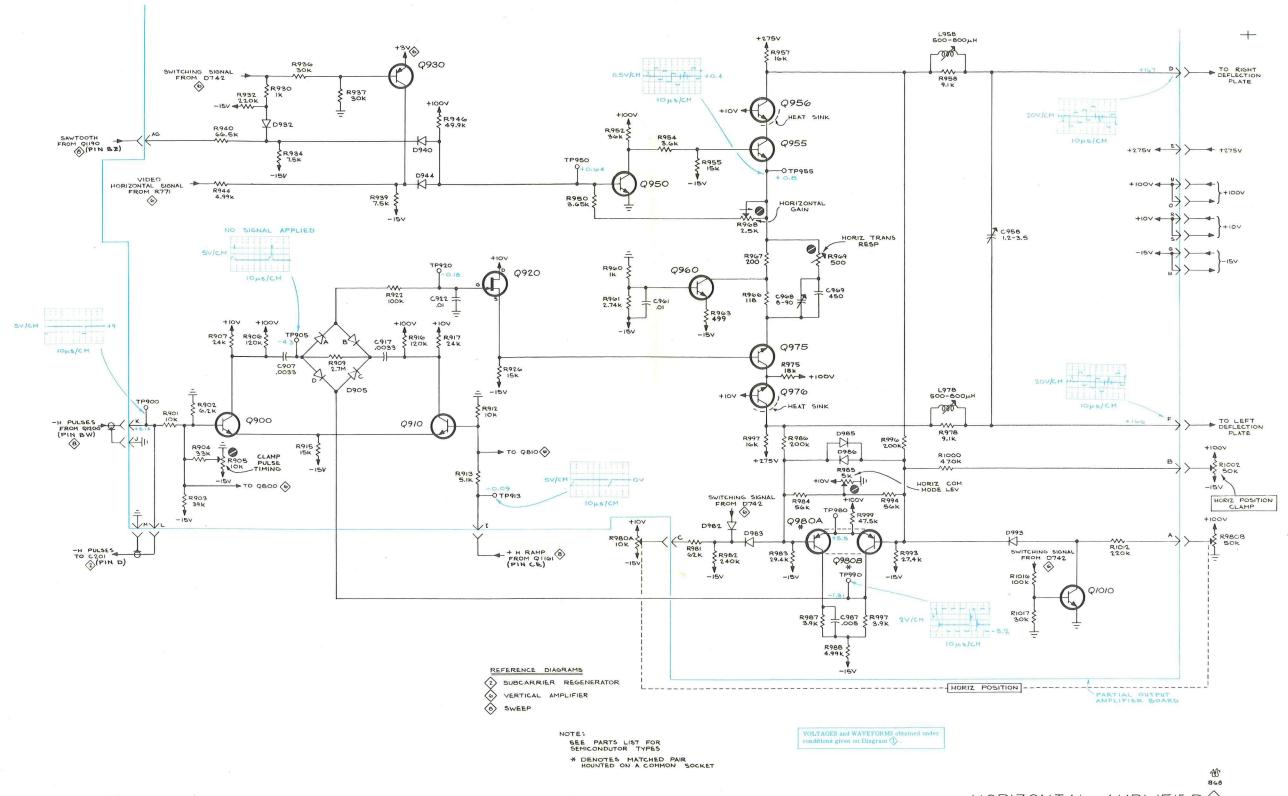
VOLTAGES and WAVE FORMS obtained under conditions given on Diagram ①, except as follows:

\* denotes that test oscilloscope is triggered from TP 514 on + slope.

VERTICAL AMPLIFIER 6

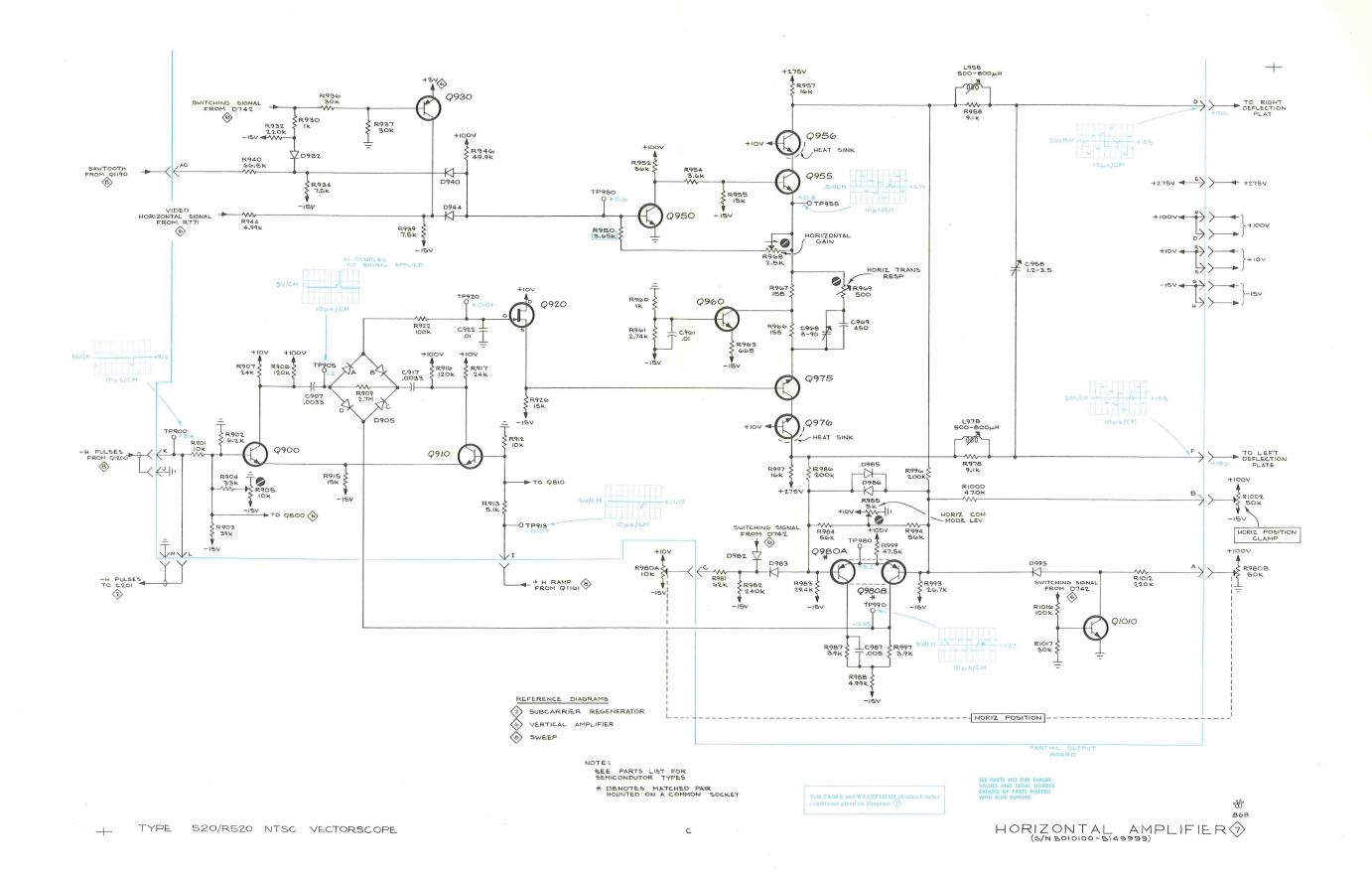
c,

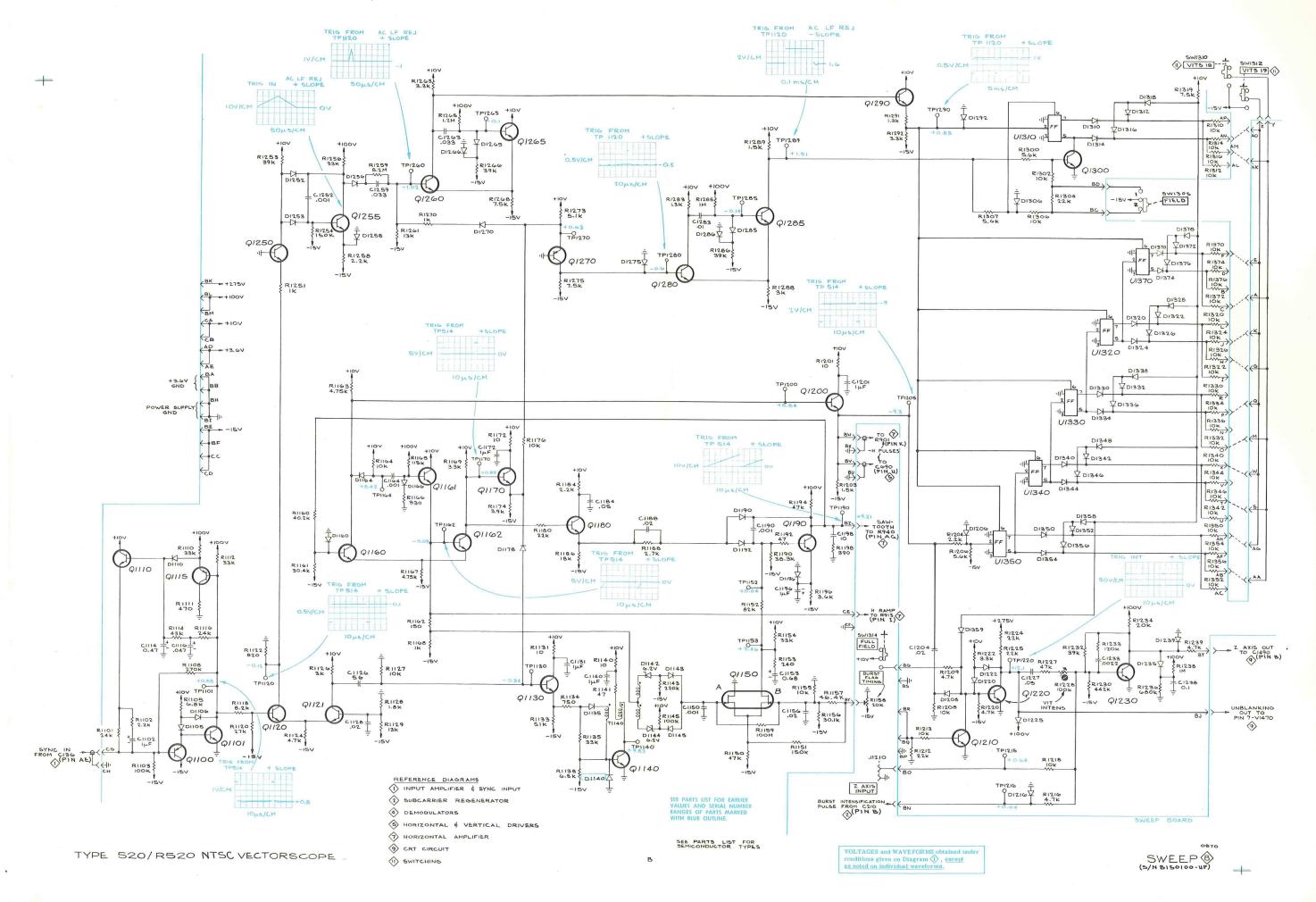


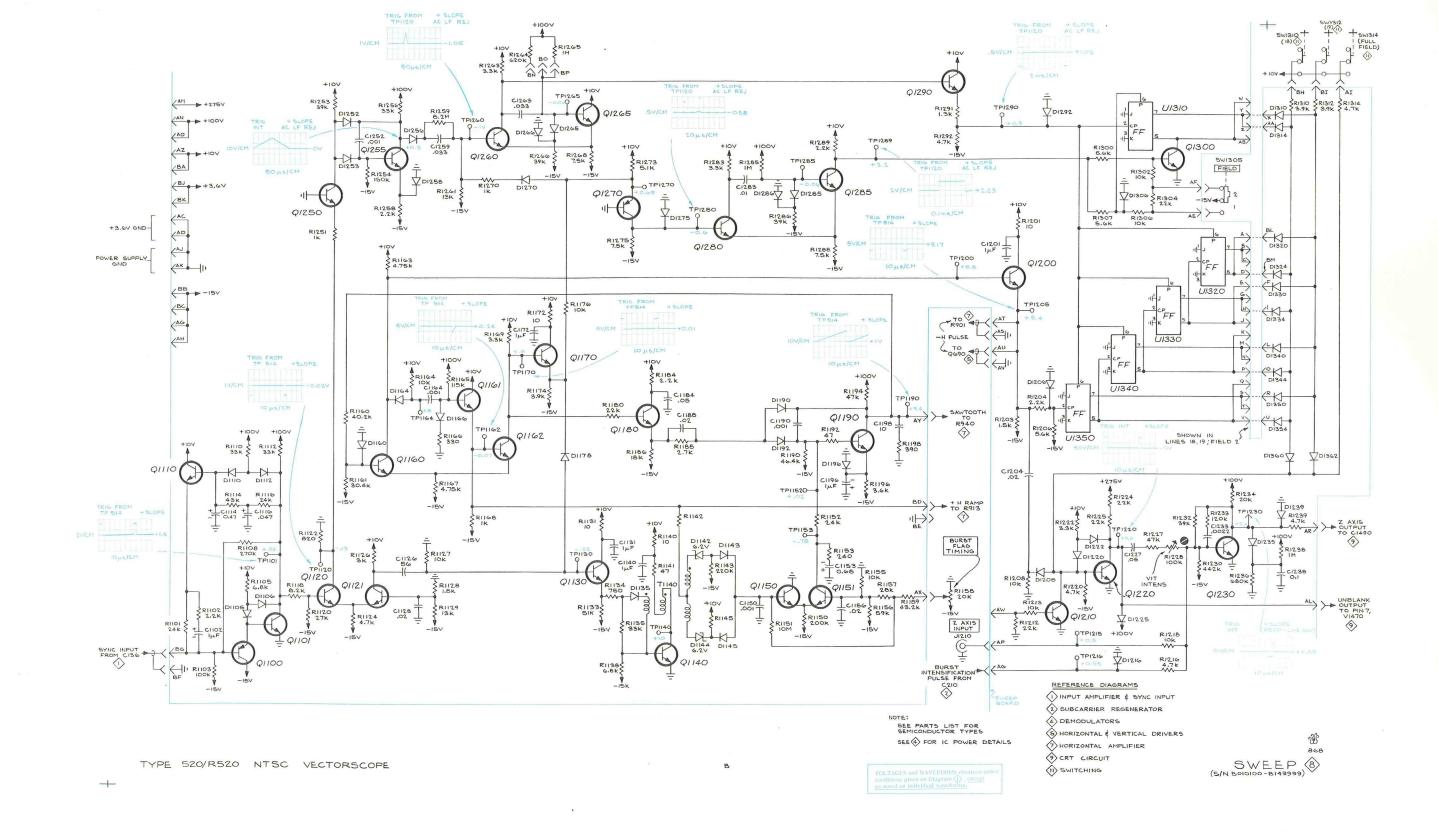


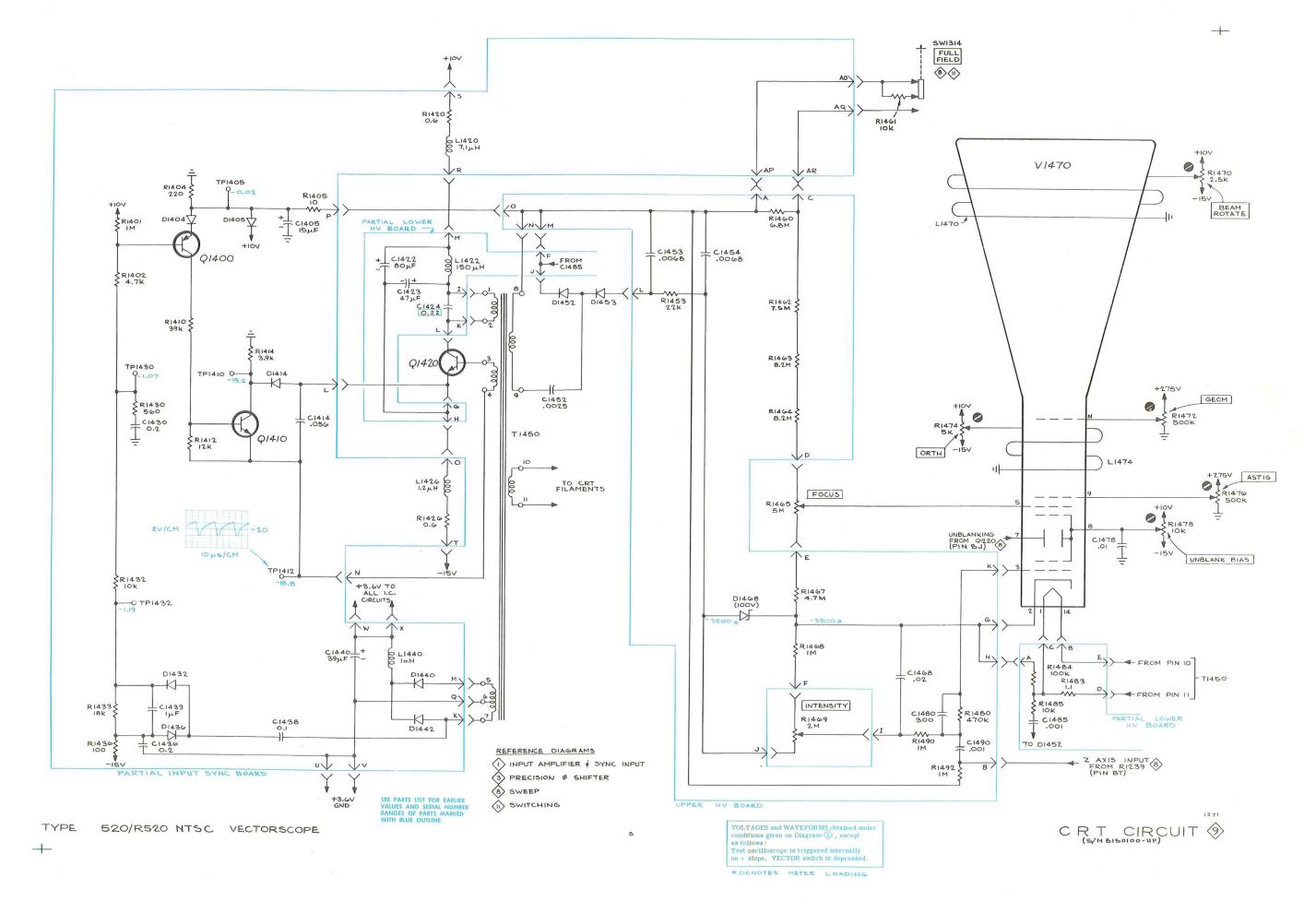
TYPE 520/R520 NTSC VECTORSCOPE

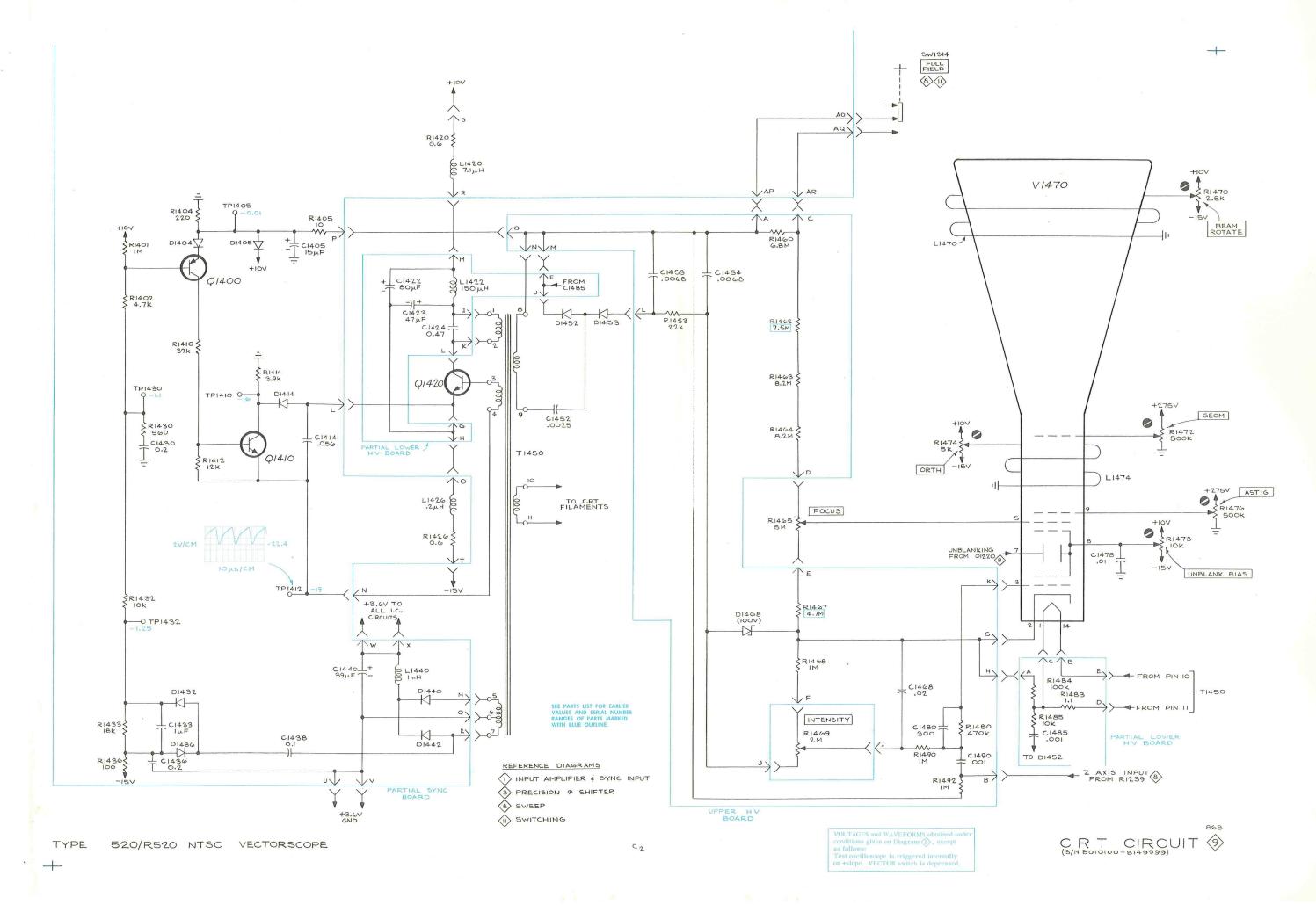
HORIZONTAL AMPLIFIER



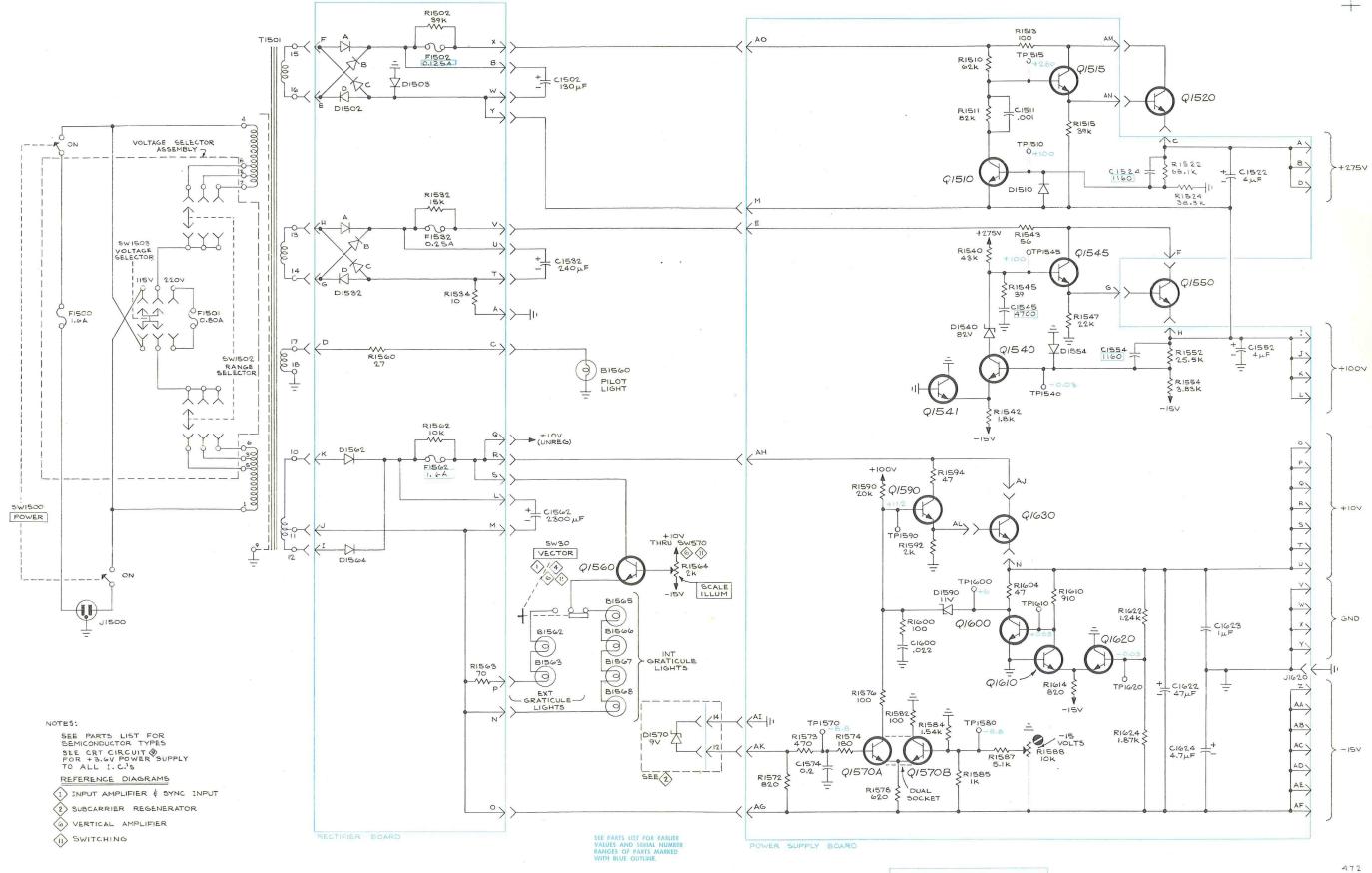








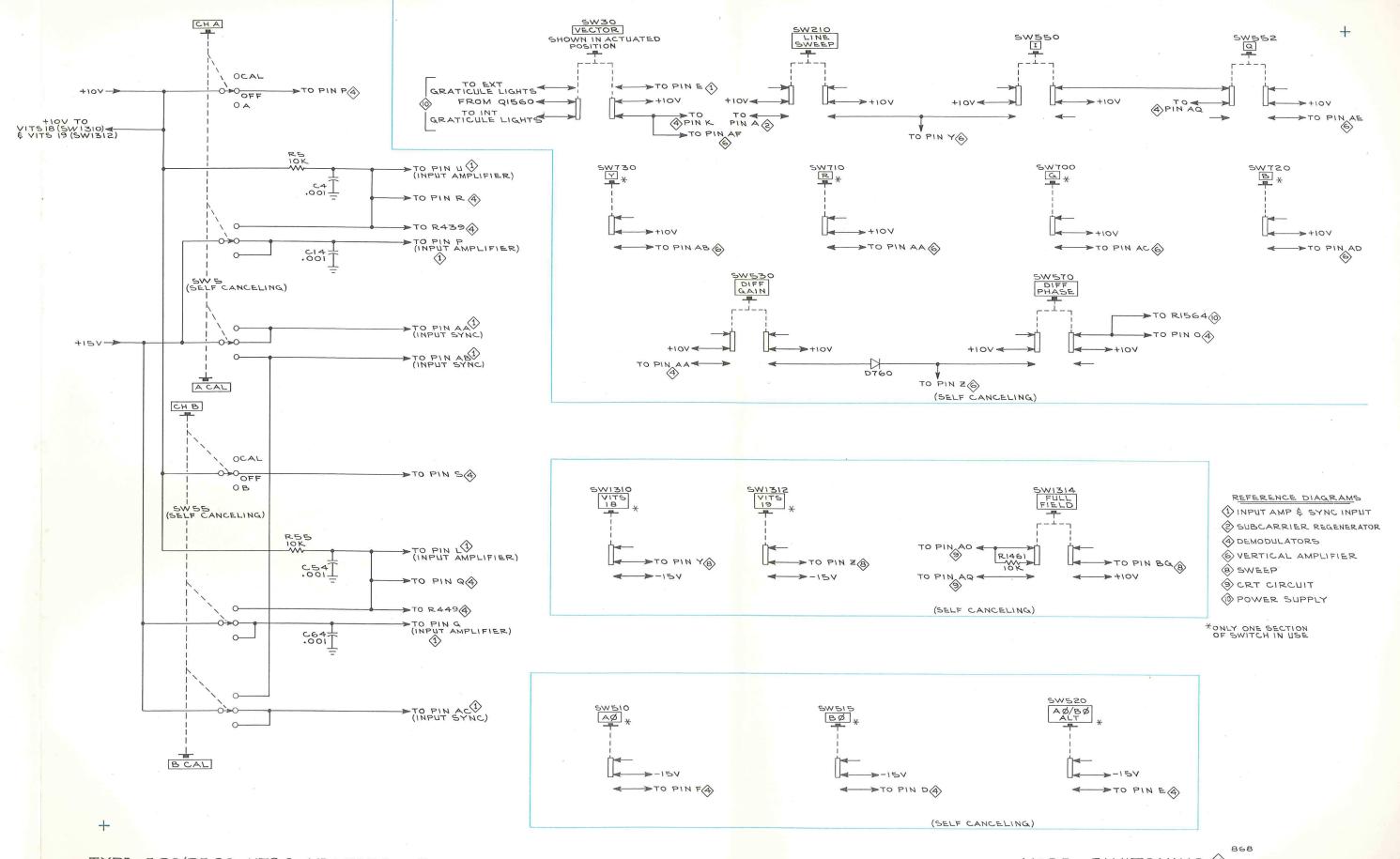
6



TYPE 520/R520 NTSC VECTORSCOPE

VOLTAGES obtained under conditions given on Diagram  $\bigodot$ .

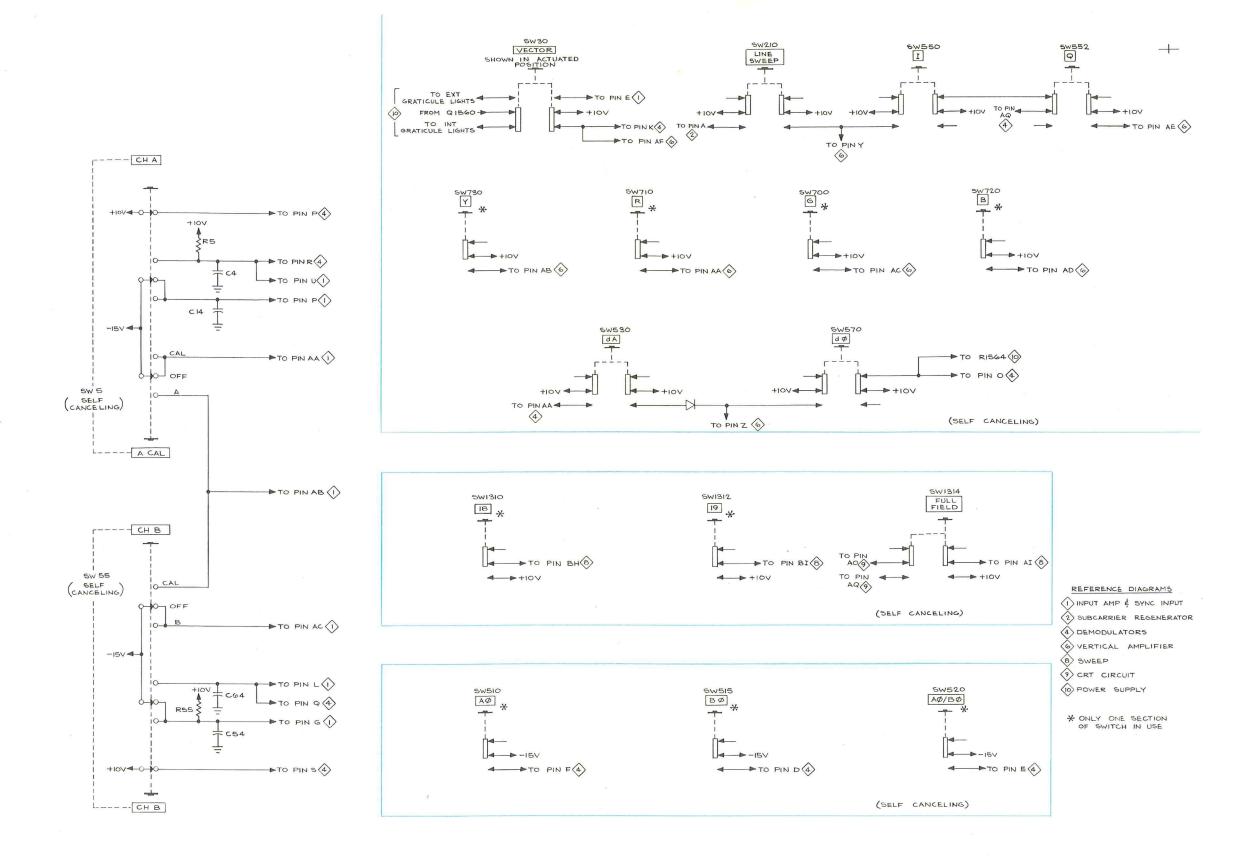
POWER SUPPLY 🕸



TYPE 520/R520 NTSC VECTORSCOPE

MODE SWITCHING (I)

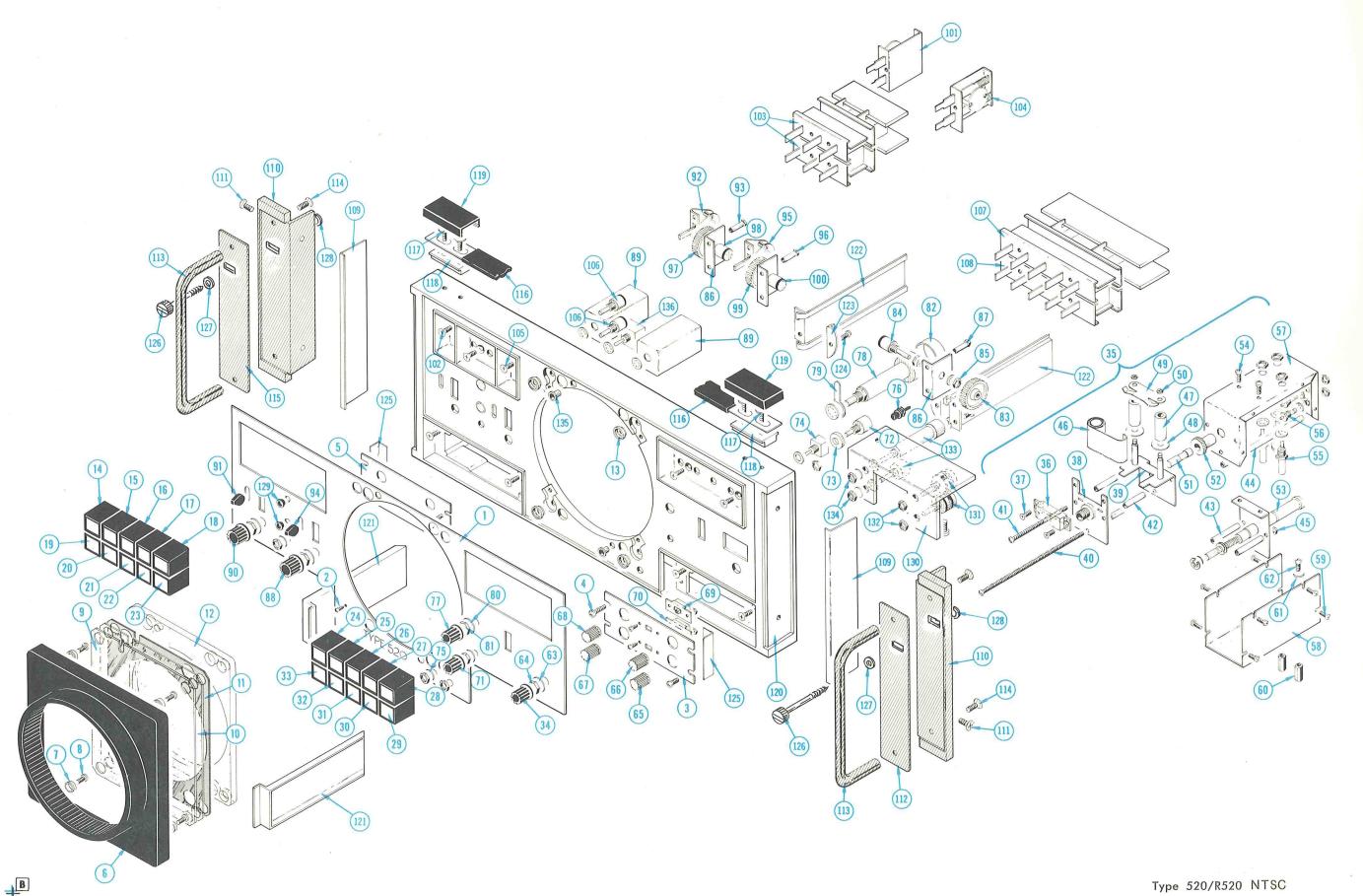
A

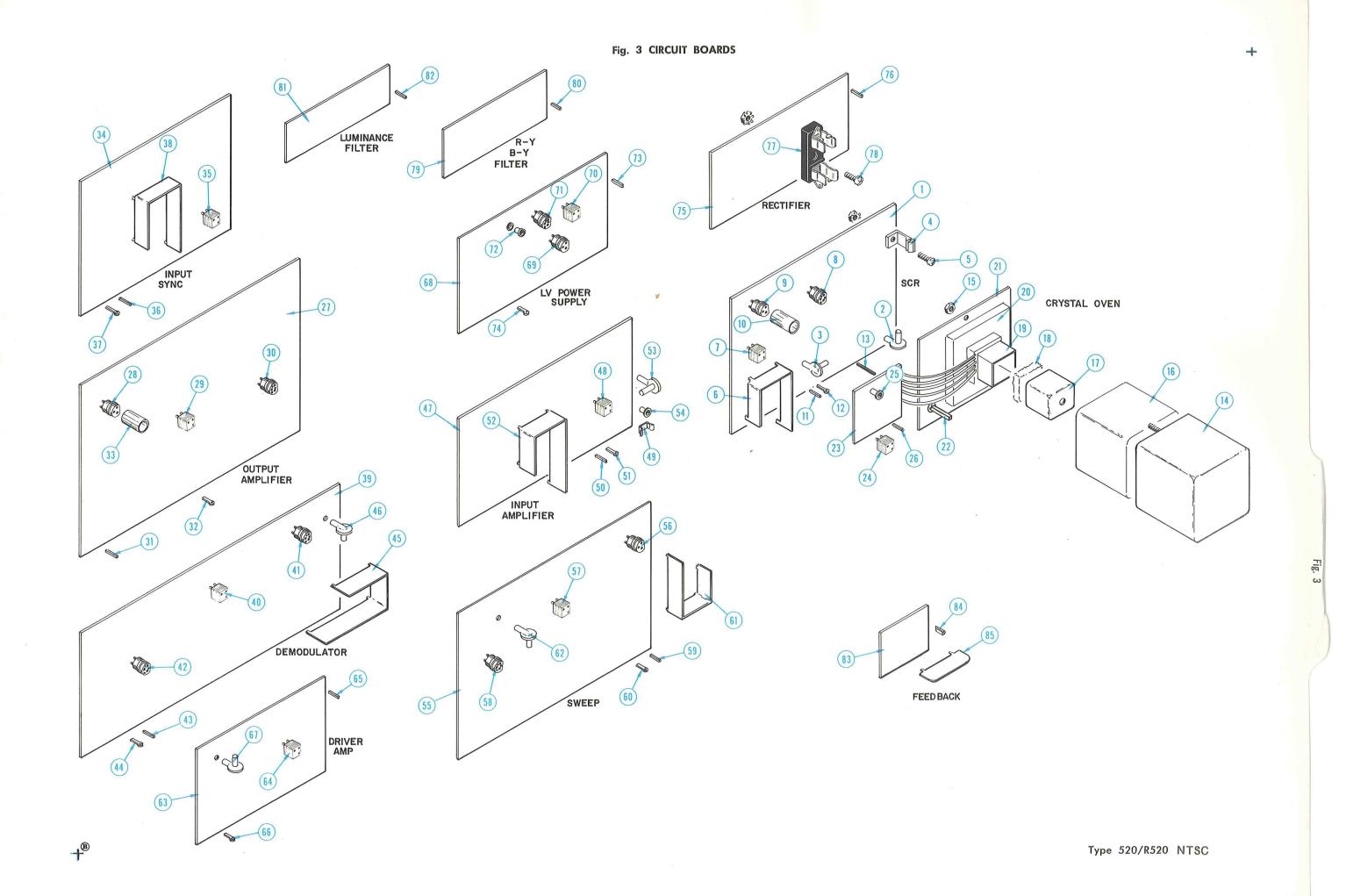


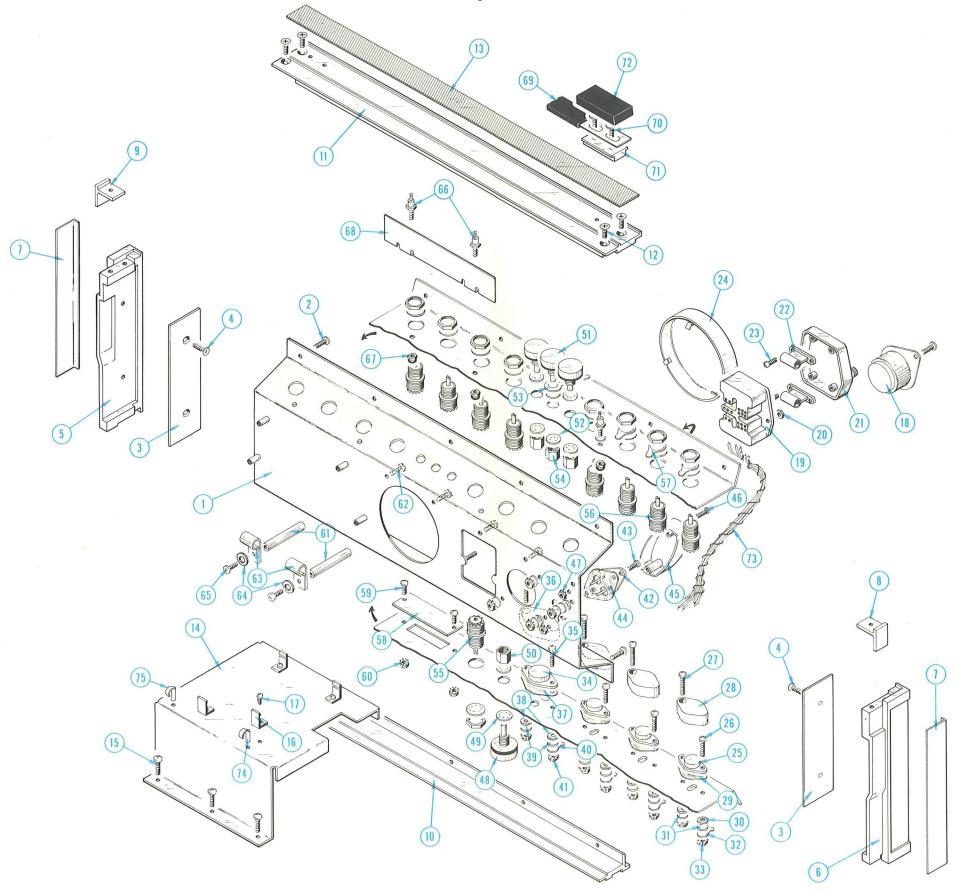
TYPE 520/R520 NTSC VECTORSCOPE

+

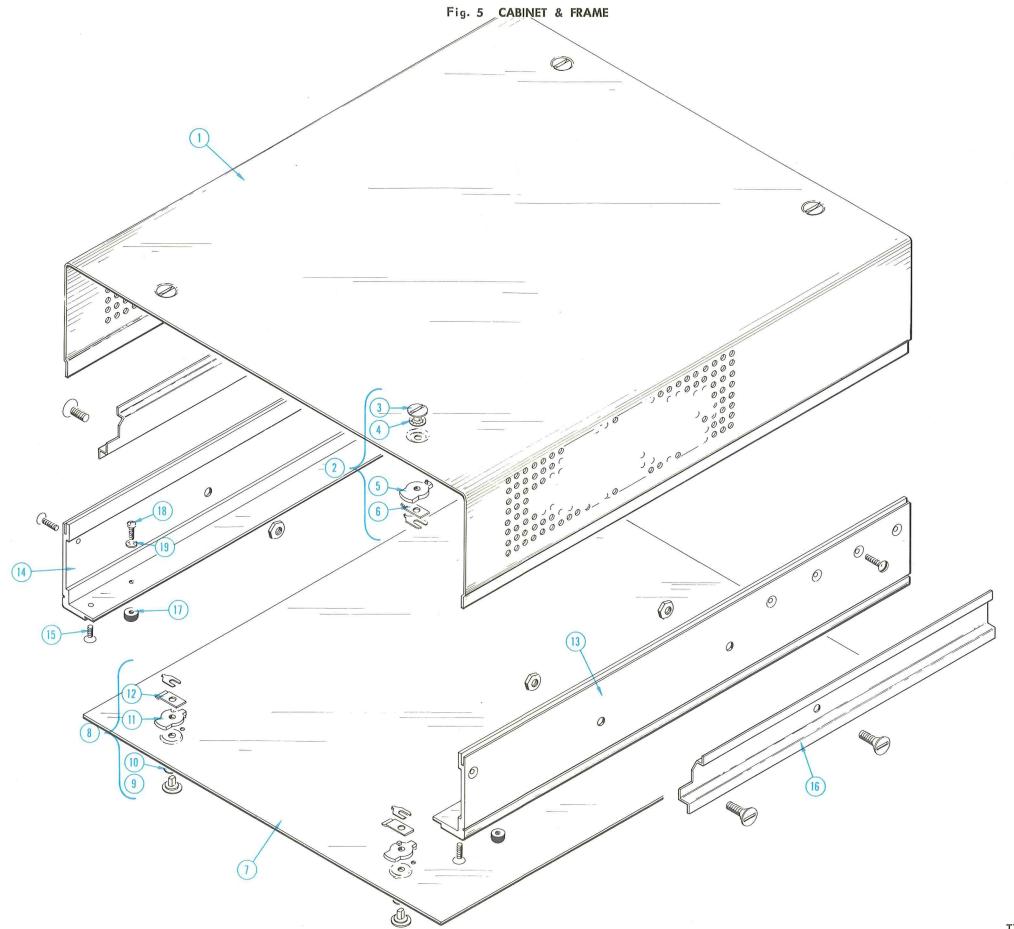
MODE SWITCHING (1)







A



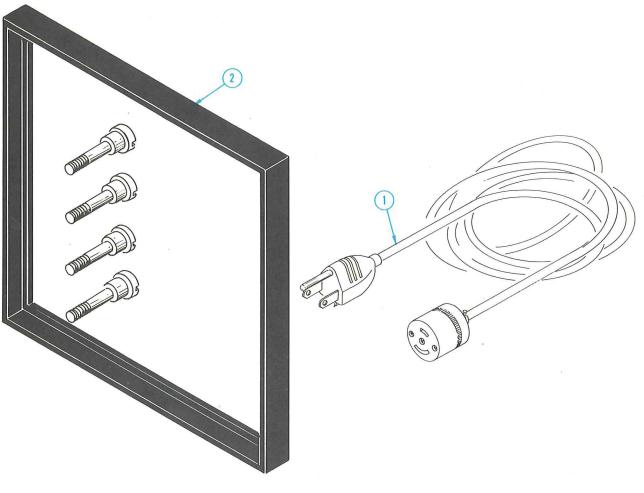


Fig. & Index No.		Serial/Mod Eff	Q el No. t Disc y	Description 1 2 3 4 5			
6-1 -2	161-0036-00 016-0114-00 070-0639-01		1 1 1	CABLE ASSEMBLY, power 7 feet 6 inches long KIT, light seal & screws MANUAL, instruction (not shown)			
	OTHER PARTS FURNISHED W/R520 ONLY						
	351-0101-00 351-0195-00	B010100 B B200000	99999 1 1	SLIDE chassis track, 1 pair (not shown) SLIDE chassis track, 1 pair (not shown)			

# SECTION 10 RACKMOUNTING

#### Introduction

This section of the manual contains information for field converting the rackmount model of the Vectorscope into a

bench model and vice versa. There is also some information about 3-3/g-inch wide Tilt-Lock Slideout Track availability, and rackmounting installation instructions using the 13/4-inch wide slideout tracks in a non-tilt installation.

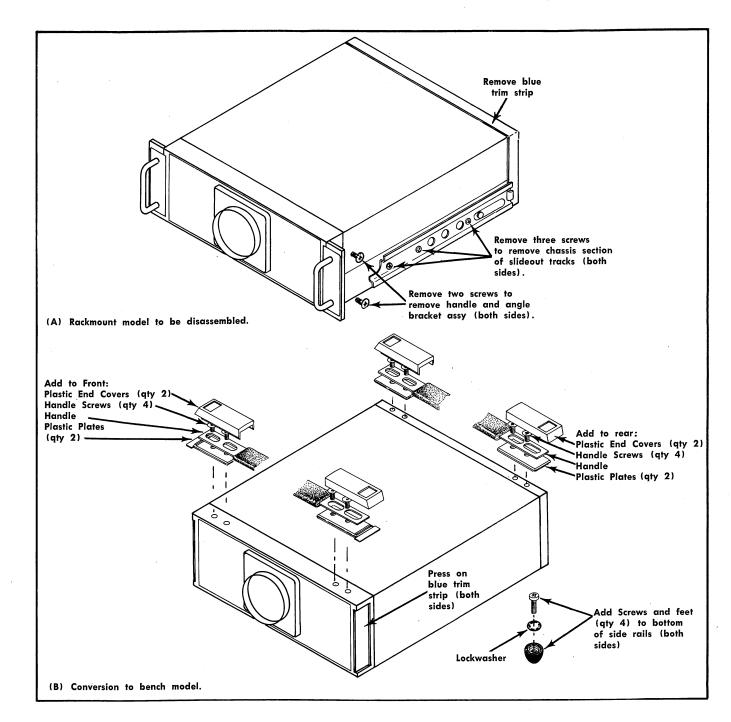


Fig. 10-1. Converting a rackmount Vectorscope into a bench model.

#### **RACKMOUNT-TO-BENCH CONVERSION**

# Converting the Vectorscope From a Rackmount Model (Type R520) to a Bench Model (Type 520).

Remove these parts (see Fig. 10-1A):

- 1. Adhesive-backed blue trim strip from top rear-portion of the instrument.
- 2. Remove the chassis section of the slideout tracks (both sides).
- 3. Remove two screws from each angle bracket (both sides of the instrument) to remove the handle and angle bracket assembly as a unit.

Add these parts (see Fig. 10-1B):

- 1. Mount the front handle on the instrument by first laying the front plastic plates in line with the holes on the top edge of the front casting. Then, align the handle over the plates and fasten these parts to the instrument using the 10-32 x 0.40 inch screws.
- 2. Mount the rear handle on the instrument by first laying the rear plastic plates in line with holes on the top of the rear casting. Then, align the handle over the plates and fasten these parts to the instrument using the  $10-32 \times 40$  inch screws.
- 3. Lay the plastic end cover over the handle screws. Apply finger pressure to snap the cover into place. Repeat this procedure to install all four covers.
- 4. Peel the paper backing from the adhesive side of the blue trim strips. Press the blue strips into place at the left and right sides of the instrument where the rackmount angle brackets have been removed.

- 5. Remove the bottom from the instrument and install the four feet. Each foot can be easily installed by holding the screw in the hole and threading the foot onto the screw. Repeat this procedure for all four feet.
- 6. Install the bottom cover.

#### **BENCH-TO-RACKMOUNT CONVERSION**

# Converting a Bench Model (Type 520) to a Rackmount Model (Type R520).

Remove the parts that were added in Fig. 10-1B and described in the previous procedure. Add the parts that were removed in the previous procedure and illustrated in Fig. 10-1A. To install the blue trim strip, remove the paper backing and press the trim strip into place where the rear handle was removed.

#### NOTE

Before mounting the rackmount handles on the instrument, the parts for the handle and angle bracket assembly may be pre-assembled as shown in the Fig. 10-2 illustration. Use appropriate size retaining ring pliers to install the retaining ring on the thumb screw shaft.

When mounting the chassis sections of the slideout tracks, the pivot screw and tilt stop hardware supplied by the slideout track manufacturer are not used. Instead, use the  $8-32 \times 5/16$ -inch screws (212-0068-00) to mount the chassis sections to the sides of the instrument for a non-tilt installation.

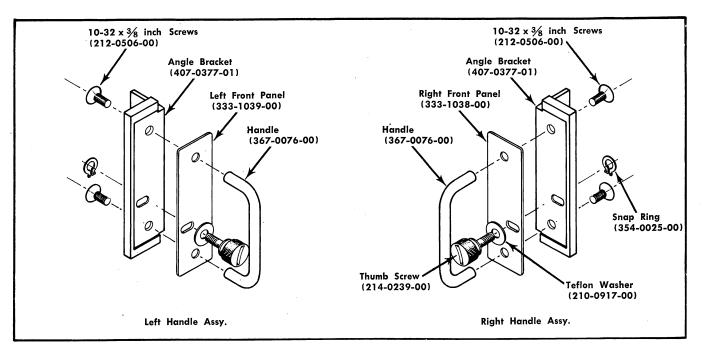


Fig. 10-2. Assembling the handles for the rackmount model.

#### MECHANICAL PARTS LIST FOR RACKMOUNT MODEL

Tektronix Part No.	. Serial/Model No.		Qty.	Description
	Eff	Disc	_	
				Parts for Handle Assembly (left & right)
407-0377-01			2	Bracket, angle (mounting hardware for bracket is shown in Fig. 10-2)
367-0076-00			2	Handle (mounting hardware for handle is shown in Fig. 10-2)
333-1039-00			1	Panel, left front
333-1038-00			1	Panel, right front
212-0506-00			4	Screw, $10-32 \times \frac{3}{8}$ inch, FHS (holds handle & panel to
				angle bracket)
212-0560-00			4	Screw, 10-32 x 5/16 inch, FHS (mounts handle assembly to chassis)
214-0239-00			2	Screw, knurled thumb, fastener
210-0917-00			2 2 2	Washer, teflon
354-0025-00			2	Ring, retaining
124-0188-00			ī	Strip, trim, blue, 16.3 x 0.876 inches
				Parts for Slideout Tracks
351-0104-00			1 pr.	Chassis section
212-0068-00			6	Screw, 8-32 $\times \frac{5}{16}$ inch, THS (mounts chassis sections to
			•	chassis)
351-0101-00	B010100	B199999	1 pr.	Intermediate & stationary section with mounting hard- ware
351-0195-00	B200000		1 pr.	Intermediate & stationary section with mounting hardwa

#### MECHANICAL PARTS LIST FOR BENCH MODEL

386-1283-00	2	Plate, plastic (for front handle)
386-1352-00	. 2	Plate, plastic (for rear handle)
367-0073-00	2	Handle, blue
200-0728-00	4	Cover, handle end, plastic, blue
213-0155-00	8	Screw, 10-32 x 0.40 inch (mounts plates & handles to instruments)
124-0201-00	2	Strip, trim, blue (covers rackmount handle bracket holes)
348-0080-01	4	Feet, black, vinyl
210-0006-00	4	Lockwasher, internal, #6
211-0511-00	4	Screw, $6-32 \times \frac{1}{2}$ inch, PHS (mounts feet to bottom of side rails)

#### TILT-LOCK SLIDEOUT TRACKS

On special order, the Type R520 can be equipped with premounted side-rail extrusions that accept 33/8-inch wide Tilt-Lock Slideout Tracks. The chassis sections of the slideout tracks are also premounted at the factory. These tracks permit the instrument to be tilted up or down when fully extended from the rack. In the fully extended position, the instrument can be locked into one of seven positions: horizontal; 45°, 90°, or 105° above or below the horizontal position. For further details, contact your Tektronix Field Engineer or Field Office.

#### **RACKMOUNTING INSTRUCTIONS**

#### Mounting Method (Figs. 10-3, 10-4 and 10-7)

This instrument will fit most commercial consoles and most 19-inch wide racks whose front and rear rail holes conform to Universal hole spacing. An extra hole in each rail must be drilled (and tapped, if desired) to permit mounting the

Type R520 in a rack having EIA/RETMA/Western Electric hole spacing (see Fig. 10-7A).

Fig. 10-3 shows the instrument installed in a cabinet type rack with 13/4-inch wide slideout tracks for a non-tilt installation. The instrument is secured into the rack by means of two knurled thumb screws. When the thumb screws on the front panel are loosened to release the instrument, the instrument can be pulled out of the rack like a drawer to its fully extended position (see Fig. 10-4). This position permits many routine maintenance functions to be performed without completely removing the instrument from the rack.

The slideout tracks easily mount to the cabinet rack front and rear vertical mounting rails if the inside distance between the front and rear rails is within 10%/16 inches to 243/8 inches. Some means of support (for example, make extensions for the rear mounting brackets) is needed to support the rear ends of the slideout tracks if the tracks are going to be installed in a cabinet rack whose inside dimension between front and rear rails is not the proper distance (10%/16 inches to 243/8 inches).

#### Instrument Dimension

The last pullout page in this section shows dimensional drawings exclusive of the power cord and cables.

#### Rack Dimensions

Width—A standard 19-inch rack may be used. The dimension or opening between the front rails must be at least 175/8 inches (see Fig. 10-4) for a cabinet rack in which the front lip of the stationary section is mounted behind an untapped front rail as shown in Fig. 10-7B. If the front rails are tapped and the stationary section is mounted in front of the front rail as shown in Fig. 10-7C, the dimension between the front rails should be at least 173/4 inches. These dimensions allow room on each side of the instrument for the slideout tracks to operate so the instrument can move freely in and out of the rack.

**Depth**—For proper circulation of cooling air, allow at least 2 inches clearance behind the rear of the instrument and any enclosure on the rack (see dimensional drawing). If it is sometimes necessary or desirable to operate the Type R520 in the fully extended position, use cables that are long enough to reach from the signal source to the instrument.

#### Rackmounting in a Cabinet Rack

General Information—The slideout tracks for the instrument consist of two assemblies, one for the left side of the instrument and one for the right side. Each assembly consists of three sections as illustrated in Fig. 10-5. The stationary section attaches to the front and rear rails of the rack with inside dimensions as indicated in Fig. 10-4, the chassis section attaches to the instrument and is installed at the factory; the intermediate section fits between the other two sections to allow the instrument to fully extend out of the rack.

The small hardware components included with the slideout track assemblies are shown in Fig. 10-6. The hardware shown in Fig. 10-6 is used to mount the slideout tracks to the rack rails having this compatibility:

- (a) Front and rear rail holes must be large enough to allow inserting a 10-32 screw through the rail mounting holes if the rails are untapped (see Fig. 10-7B).
- (b) Or, front and rear rail holes must be tapped to accept a 10-32 screw if Fig. 10-7C mounting method is used. Note in Fig. 10-7C right hand illustration that a #10 washer (not supplied) may be added to provide increased bearing surface for the slideout track stationary section front flange.
- (c) Front and rear rail holes must be located on Universal spacing, that is the sequence for the hole spacing is:  $\frac{5}{8}$  inch,  $\frac{1}{2}$  inch,  $\frac{5}{8}$  inch,  $\frac{1}{2}$  inch,  $\frac{5}{8}$  inch,  $\frac{1}{2}$  inch, etc.

Because of the above compatibility, there will be some small parts left over.

The stationary and intermediate sections for both sides of the rack are shipped as a matched set and should not be separated. The matched sets for both sides including hardware are marked 351-0195-00 on the package for instruments SN B200000 and up. To identify the assemblies, note that the automatic latch and intermediate section stop are both located near the top of the matched set.

**Mounting Procedure**—Use the following procedure to mount both sets. See Fig. 10-7 for installation details.

- 1. To mount the instrument directly above or below another instrument in the cabinet rack, select the appropriate holes in the front rack rails for the stationary sections using Fig. 10-7A as a guide.
- 2. Mount the stationary slideout track sections to the front rack rails using either of these methods:
- (a) If the front flanges of the stationary sections are to be mounted **behind the front rails** (rails are countersunk or not tapped), mount the stationary sections as shown in Fig. 10-7B right-hand illustration. Note that the bar nut is positioned so the 1/2-inch spaced holes are located near the top so the upper-most threaded hole will accept the thumb screw when the Type R520 is fully installed.
- (b) If the front flanges of the stationary sections are to be mounted **in front of** the front rails (rails are tapped for 10-32 screws), mount the stationary sections as shown in Fig. 10-7C righthand illustration. To provide increased bearing surface for the screw head to securely fasten the front flange to the rail, a flat washer (not suppled) may be added under the screw head. However, consider that using this mounting method, the front panel will not fit flush against the front rail because of the stationary section and washer thickness. If a flush fit is preferred, method 2 (a) should be used.
- 3. Mount the stationary slideout track sections to the rear rack rails using either of these methods:
- (a) If the rear rack rail holes are **not tapped** to accept 10-32 machine screws, mount the left stationary section with hardware provided as shown in the left-hand or center illustration of Fig. 10-7B. Note that the rear mounting bracket can be installed either way so the slideout tracks will fit a deep or shallow cabinet rack. Use Fig. 10-7B as a guide for mounting the right stationary section. Make sure the stationary sections are horizontally aligned so they are level and parallel with each other.
- (b) If the rear rack rail holes are **tapped** to accept 10-32 machine screws, mount the left stationary section with hardware provided as shown in the left-hand or center illustration of Fig. 10-7C. Note that the rear mounting bracket can be installed either way so the slideout tracks will fit a deep or shallow cabinet rack. Use Fig. 10-7C as a guide for mounting the right stationary section. Make sure the stationary sections are horizontally aligned so they are level and parallel with each other.

#### Adjustments

To adjust the slideout tracks for smooth operation, proceed as follows:

- 1. Insert the instrument into the rack as shown in Fig. 10-8.
- 2. Adjust the slideout tracks for proper spacing as shown in Fig. 10-9.

#### Maintenance

The slideout tracks require no lubrication. The special dark gray finish on the sliding parts is a permanent lubrication.

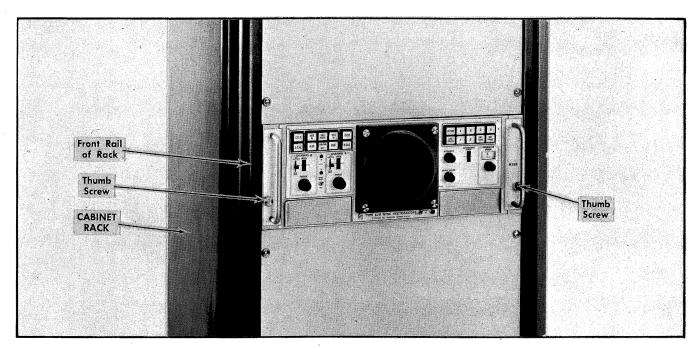


Fig. 10-3. The Type R520 installed in a cabinet type rack.

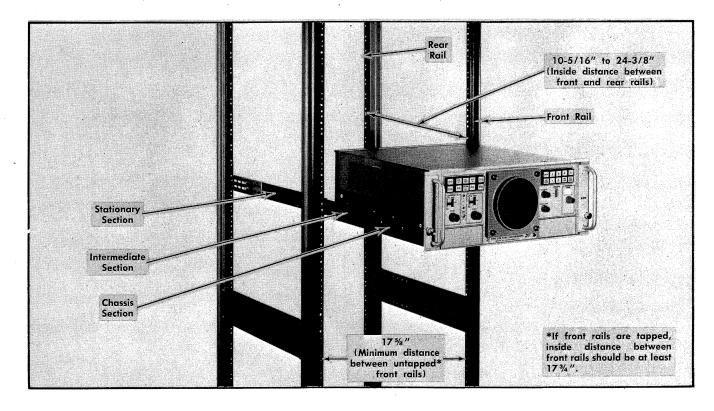


Fig. 10-4. The Type R520 shown in the fully extended position. The cabinet sides have been removed from the rack to show mounting details.

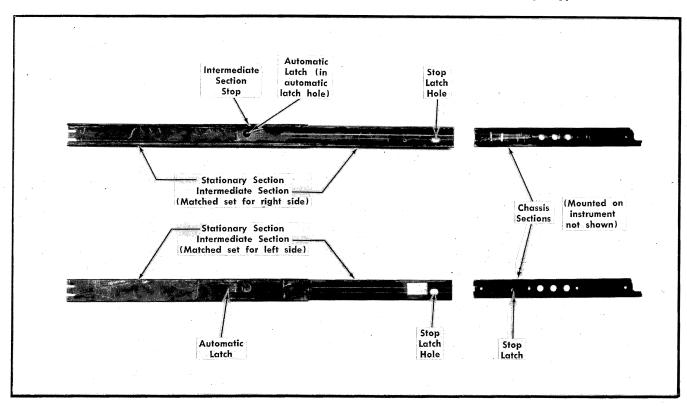


Fig. 10-5. Illustrations showing the 1 3/4-inch wide slideout track assemblies.

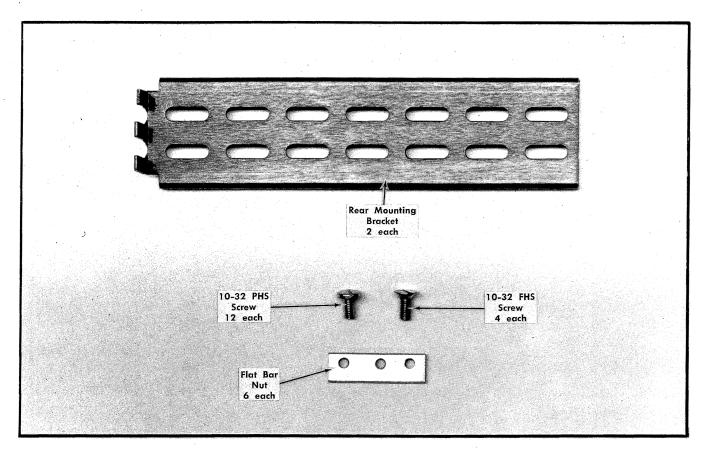


Fig. 10-6. Small hardware components for mounting the stationary sections to the rack rails.

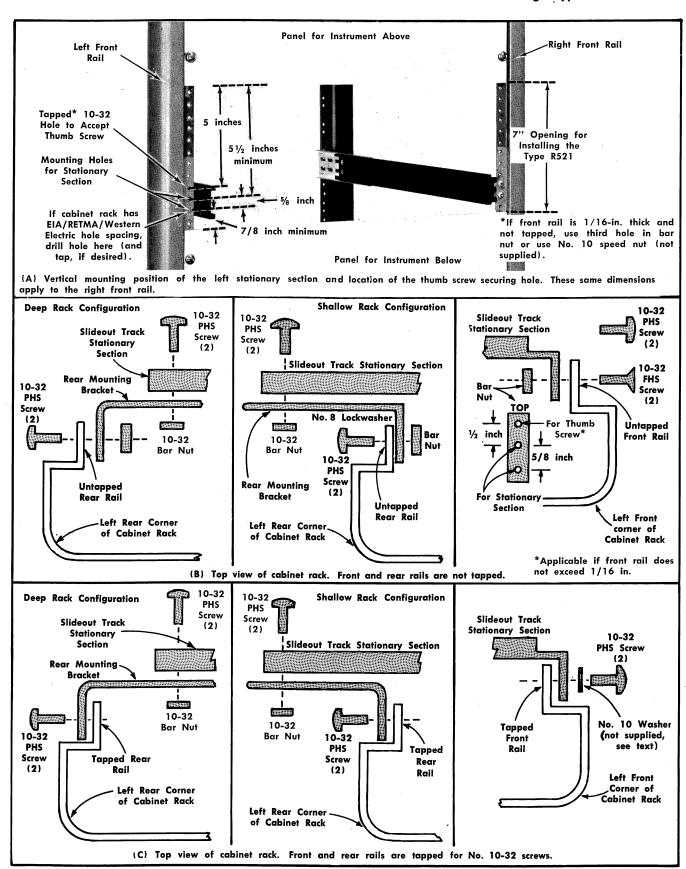


Fig. 10-7. Mounting the left stationary section (with its matched intermediate section, not shown in illustrations B and C) to the rack rails.

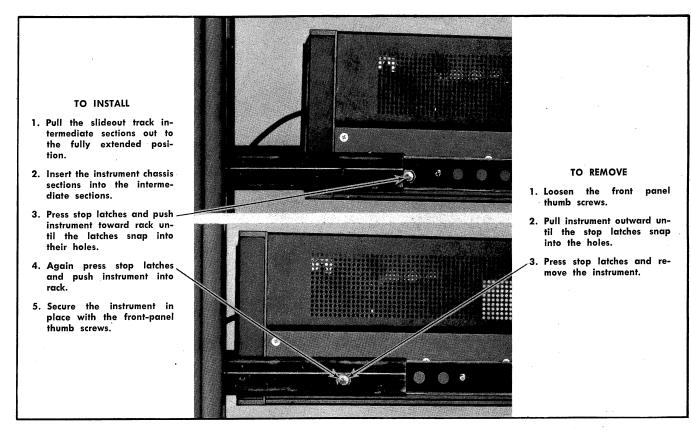


Fig. 10-8. Installing and removing the instrument.

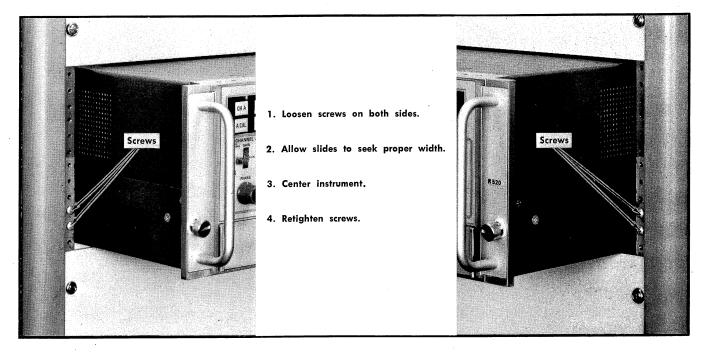
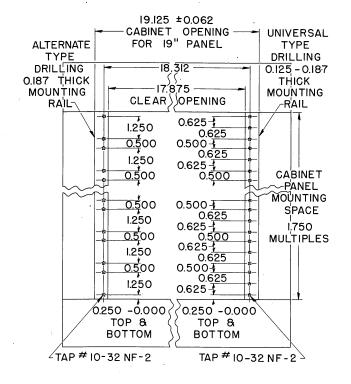
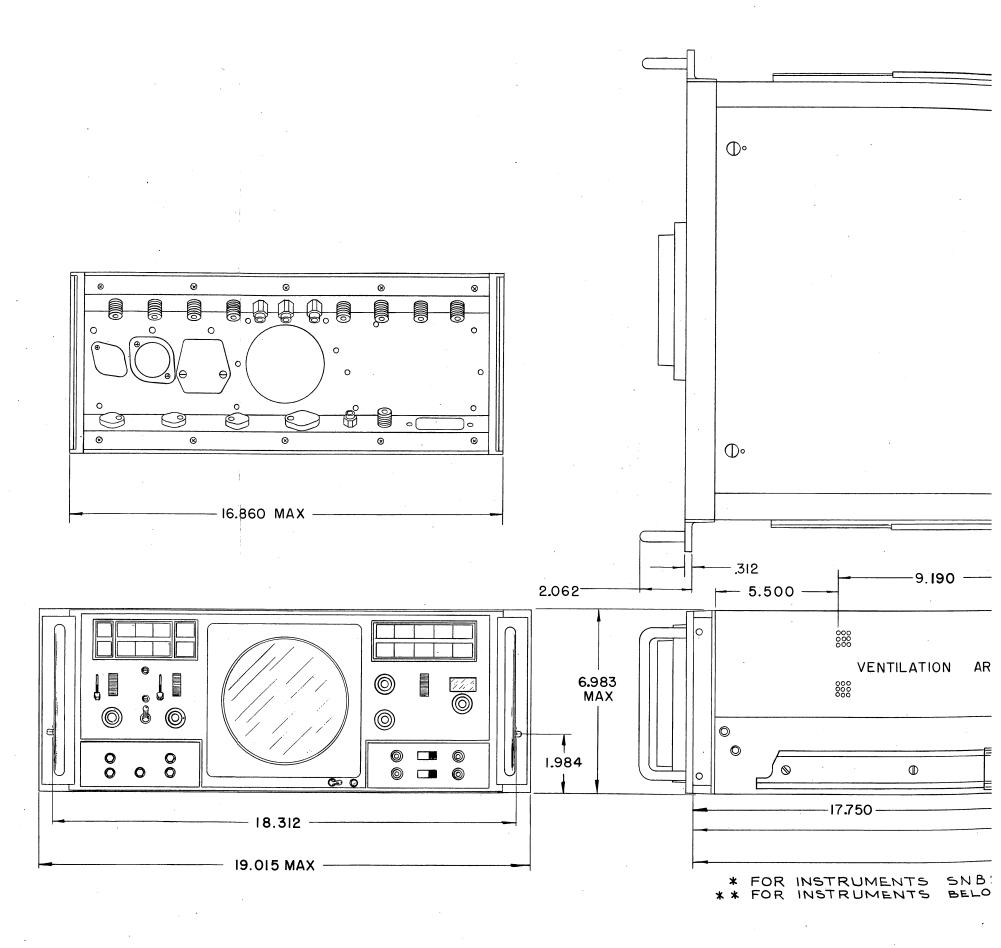


Fig. 10-9. Adjusting the slideout tracks for smooth sliding action.

10-7

#### RACK RAIL TYPES





TYPE R520 NTSC VECTORSCOPE

Dis-	Type of Check or	Signal Applied to	Buttons [	) epressed			
play No.	Display Using the Vectorscope	Vectorscope Rear- Panel Connector	Signal Selector	Display Selector	Other Pertinent Control Settings	Measurement Information	Display
1	Luminance ampli- tude calibration	None required -	A CAL, FULL FIELD, Αφ (or Βφ)	Y	Ch A 100%-75%-MAX GAIN: 75%, Ch A GAIN: CAL. LUMINANCE GAIN: CAL.	Display amplitude should be 140 IRE units (see Fig. 2-14). If not, go to step 12 in the First-Time Operation procedure.	140 180 181 191 191 191 191 191 191 191 191 191
2	Test circle cali– bration	None required	A CAL, FULL FIELD, A $\phi$ (or B $\phi$ )	VECTOR	Ch A 100%-75%-MAX GAIN: 75%. Ch A GAIN: CAL. $\phi$ REF: BURST.	Vectorscope is properly calibrated if test circle coincides with vector graticule guide circle (see Fig. 2-15A). If not, refer to step 13 in the First-Time Operation procedure.	Test
3	Unstable display (due to misadjusted BURST FLAG TIMING adjustment)	Composite color video to CH A	CH A, FULL FIELD, Αφ (or Βφ)	LINE SWEEP	SYNC: INT Ch A 100%-75%-MAX GAIN: 75%. Ch A GAIN: CAL. φ REF: BURST. A PHASE: Adjust for maximum burst amplitude.	Adjust BURST FLAG TIMING control for equal rising and fall- ing intensified portions on burst waveform (see Fig. 2-12A and step 9 in First-Time Operation procedure).	Account Accoun
4	Vector reference point calibration	None.	FULL FIELD, $\mathbf{A}\phi$ (or $\mathbf{B}\phi$ )	VECTOR	$\phi$ REF: BURST.	Reference dot should be located at center of vector graticule guide circle; if not, go to Display No. 2 in this table.	Centered Dot
5	Normal color vector display	Color-bar signal to CH A	CH A, FULL FIELD, Αφ (or Βφ)	VECTOR	SYNC: INT.  Ch A 100%-75%-MAX GAIN: 75%  Ch A GAIN: CAL.  \$\phi\$ REF: BURST.  A PHASE: Adjusted so burst coincides  with 180° position.	Normal display: Burst tip at 75% mark and color vector dots in inner boxes (see Fig. 2–17A). If not, refer to topic, "Vector Displays".	The state of the s
6	Normal luminance amplitude display of color bar signal	Color-bar signal to CH A	CH A, FULL FIELD, Αφ (or Βφ)	Y	SYNC: INT. Ch A 100%-75%-MAX GAIN: 75%. Ch A GAIN: CAL. φ REF: BURST. LUMINANCE GAIN: CAL.	Display will appear similar to that shown in Fig. 2–17B in the First-Time Operation procedure.	
7	Displaying the red, green, or blue wave- form of a color bar test signal.	Color-bar signal to Ch A	A CAL, FULL FIELD, A $\phi$ (or B $\phi$ )	VECTOR	SYNC: INT. Ch A 100%-75%-MAX GAIN: 75%. Ch A GAIN: CAL. φ REF: BURST. Αφ: Adjusted so burst coincides with 180° position.	First, obtain a normal vector display as described in Display No. 5.  Next, depress the Function Selector R, G or B button to display the desired output waveform.	Blue Output Waveform -21 -51
8	Differential gain	Subcarrier mod- ulated staircase signal to CH A	CH A, FULL FIELD, Αφ (or Βφ)	DIFF GAIN	SYNC: INT. Ch A 100%-75%-MAX GAIN: MAX GAIN. Ch A GAIN: CAL. $\phi$ REF: BURST.	Straight line display indicates no differential gain. Vertical- amplitude variations indicate stairsteps are non-linear (dif- ferential gain). Horizontally positioning the desired step to graticule center scale facilitates measurement.	80

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9.	Differential phase	Subcarrier mod- ulated staircase signal to CH A	CH A, FULL FIELD, Αφ (or Βφ)	DIFF PHASE	SYNC: INT.  Ch A 100%-75%-MAX GAIN: MAX GAIN.  Ch A GAIN: CAL. $\phi$ REF: BURST.  A PHASE: Adjusted to center the display.	Two straight parallel traces indicate no differential phase. Vertical-amplitude variations in the traces indicate presence of differential phase (see Fig. 2-18E and F, step 23 in the First-Time Operation procedure).	HARPE PL
10.	Color VITS on line 18 of field 2	Color VITS to CH A	CH Α, VITS 18, Αφ (or Βφ)	See Column 7	SYNC: INT. Ch A 100%-75%-MAX GAIN: See column 7. Ch A GAIN: CAL. φ REF: BURST. LUMINANCE GAIN: CAL. FIELD: 2.	Exact nature of this signal to be defined by the National Television Committee.	
	Subcarrier modulated staircase	Composite video with	CH A,	DIFF GAIN	Same as Display No. 8	with FIELD switch set to 2.	
11.	VITS: on line 19 of field 2	staircase VITS to CH A	VITS 19, $\mathbf{A}\phi$ (or $\mathbf{B}\phi$ )	DIFF PHASE	Same as Display No. 9	with FIELD switch set to 2.	
12.	Color encoder Q component	Composite color bars with 1 com- ponent of the color bars turned off to CH A	CH A, FULL FIELD, Αφ (or Βφ)	VECTOR	SYNC: INT. Ch A 100%-75%-MAX GAIN: 75%. Ch A GAIN: CAL. φ REF: BURST.	Associated color vector dots are displayed along the Q axis (see Fig. 2-2D). Lack of dot coincidence with Q-axis marks indicate gain or linearity troubles (refer to topic, "Color Encoder")	Color Vector Dots on Q Axis
13.	Color encoder I component	Composite color bars with Q com- ponent of the color bars turned off to CH A	CH A, FULL FIELD, Αφ (or Βφ)	VECTOR	Same as Display No. 12.	Same as Display No. 12 except associated color vector dots are displayed along the I axis. (Refer to topic, "Color Encoder").	Color Vector Dots on I Axis
14.	Color encoder subcarrier im-	Encoder out- put with sub- carrier (Y, I and Q signals	CH A, FULL FIELD,	VECTOR	SYNC: INT. Ch A 100%-75%-MAX GAIN: 75%.	VECTOR MODE: Dot should be centered if subcarrier is bal- anced and Display No. 2 conditions are fulfilled. If dot is not centered, imbalance exists.	
14.	balance	of the color bars turned off) to CH A DIFF PHASE	$\mathbf{A}\phi$ (or $\mathbf{B}\phi$ )	DIFF PHASE	Ch A GAIN: CAL. $\phi$ REF: BURST.	DIFF PHASE MODE: Allows precise measurement of inbalance and permits accurate balancing of subcarrier component.	
15.	Dual displays for matching outputs from two color cameras	Reference color camera signal to CH A; other signal to CH B.	CH A, CH B, FULL FIELD, Αφ/Βφ ALT	VECTOR	SYNC: INT.  Ch A & B 100%-75%-MAX GAIN: 75%.  Ch A & B GAIN: CAL.  φ REF: BURST.  A & B PHASE: Adjusted so burst coincides with 180° position.	If Ch B color vectors do not match Ch A color vector loca- tions, adjust the Ch B color camera for proper matching to Ch A signal	
16.	Color Saturation	Composite color video to CH A	CH A, FULL FIELD, Aφ (or Βφ)	VECTOR	SYNC: INT.  Ch A GAIN: CAL. $\phi$ REF: BURST.  A PHASE: Adjusted so burst coincides with $180^\circ$ position.	Set the Ch A 100%-75%-MAX GAIN switch to a position (100% or 75%) that will cause the color vector dots to appear in the target area. Note the location of the burst tips. If located at the 75%, vector graticule markings, the colors are 75% saturated; if located at the 100% marking, the colors are 100% saturated. The Ch A 100%-75%-MAX GAIN switch position will also correspond to the burst tip locations.	Burst Tips at 75% for 75% Saturated Colors

17	Phase vs time delay	Composite color video camera signals to ÇHA and CHB. Assume CHA signal is the reference.	CH A, FULL FIELD, Αφ	VECTOR	SYNC: INT.  Ch A & B 100%-75%-MAX GAIN: 75%.  Ch A & B GAIN: CAL.  \$\phi\$ REF: BURST.  A PHASE: Adjusted so burst coincides with 180° position.	Obtain a normal Ch A vector display as described in Display No. 5. Depress the Ch B button to obtain a time-shared dual display. Note the Ch B vector display locations compared to Ch A. Any phase difference can be converted to time delay by noting that 360° is equal to 280 nanoseconds of time; hence, 1° equals 0.8 nanoseconds or 8 inches of cable length if the cable has a delay of 1.2 ns/foot. Adjust cable lengths for one camera to match the displays.	
18	Line intensification	Composite color video to CH A	CH A, FULL FIELD, Αφ (or Βφ)	Y	SYNC: INT. Ch A 100%-75%-MAX GAIN: 75%. Ch A GAIN: CAL. φ REF: BURST. LUMINANCE GAIN: CAL.	Check that the Z axis input lead is connected to pin BO on the Sweep board. Apply the negative-going intensifying pulse to the Z AXIS INPUT connector. Turn the INTENSITY to a level such that the intensified line will appear as a bright display on the CRT. The non-intensified lines will appear dim. Instruments below SN B150100: Z axis input lead is connected to pin AP on the Sweep board.	
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#### MANUAL CHANGE INFORMATION

At Tektronix, we continually strive to keep up with latest electronic developments by adding circuit and component improvements to our instruments as soon as they are developed and tested.

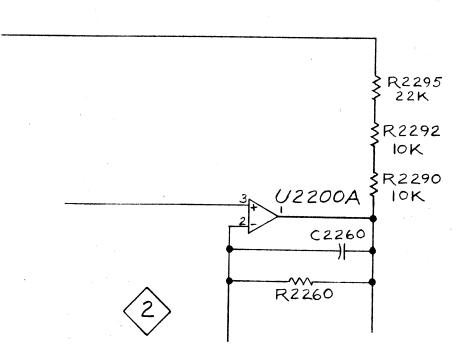
Sometimes, due to printing and shipping requirements, we can't get these changes immediately into printed manuals. Hence, your manual may contain new change information on following pages.

A single change may affect several sections. Sections of the manual are often printed at different times, so some of the information on the change pages may already be in your manual. Since the change information sheets are carried in the manual until ALL changes are permanently entered, some duplication may occur. If no such change pages appear in this section, your manual is correct as printed.

## ELECTRICAL PARTS LIST AND SCHEMATIC CORRECTION

CHA	NO	T.	TO	
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CHANGE IU:			
R2290 315-0103-00	10 kΩ	1/4 W	5%
ADD: (to EPL only)		•	
R2098 315-0224-00	220 kΩ	1/4 W	5%
ADD:			
R2292 315-0103-00	10 kΩ	1/4 W	5%



PARTIAL-SUBCARRIER REGENERATOR

## 520A NTSC

## TEXT CORRECTION

SECTION 2

Operating Instructions

Page 2-11

TABLE 2-3

CHANGE as follows:

TABLE 2-3

Resistor Circuit Number	Resistance	escription Wattage	Tolerance	Tektronix Part Number
R301	3.9 kΩ	1/4	5%	315-0392-00
R320	7.5 kΩ	1/4	5%	315-0752-00
R321	10 kΩ	1/4	5%	315-0103-00

#### TEXT CORRECTION

When reference is made to a "75% saturated color bar signal", the text should be changed to read, "100% saturated, 75% amplitude color bar signal". Similarly, when reference is made to colors that are "75% saturated", the text should read, "75% amplitude".

A reference to "100% saturated color bar signal" should be changed to read "100% saturated, 100% amplitude color bar signal". Colors that are "100% saturated" should be changed to read "100% amplitude".

#### TEXT CORRECTION

SECTION 6 Calibration

Pages 6-16, 6-17, 6-18 and 6-19

For proper sequence of calibration steps, move steps 16 and 17 so that they follow step 20 (Adjust Channel B Gain).

CHANGE to read as follows:

- 16. Adjust Luminance Calibrator
- 16A. Adjust Luminance Calibrator
- 17. Adjust Channel A Gain
- 18. Adjust Channel B Gain
- 19. Adjust Test Circle Oscillator
- 20. Adjust Test Circle Oscillator Compensation

# 520/R, 520A/R EFF SN B340000-up

# ELECTRICAL PARTS LIST CORRECTION

CHANGE TO:

Q420	151-0221-00	Silicon	PNP	2N4258
Q425	151-0221-00	Silicon	PNP	2N4258

# R520A EFF SN B350000-up

ELECTRICAL PARTS LIST CORRECTION

CHANGE TO:

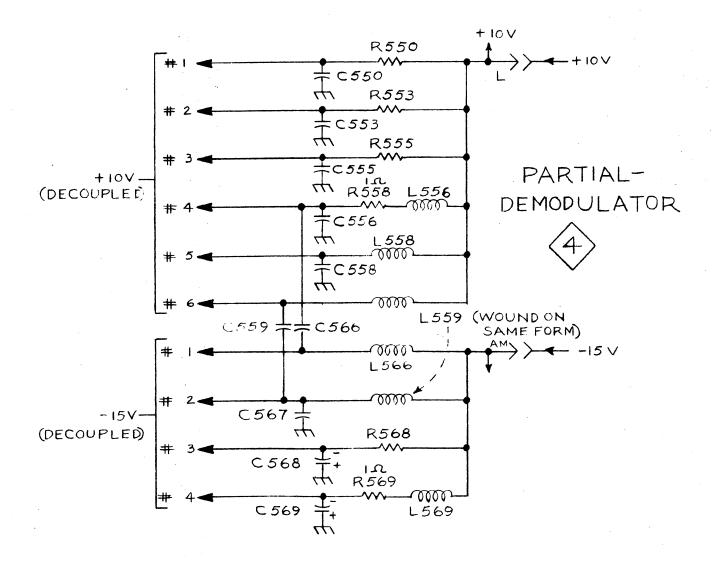
SW1316 260-1460-01 LINE SELECTOR

R520A EFF SN B360000-up R521A EFF SN B160000-up R522A EFF SN B090000-up

#### ELECTRICAL PARTS LIST AND SCHEMATIC CORRECTION

#### ADD:

R558	308-0433-00	1 Ω	1/4 W	10%
R569	308-0433-00	1 Ω	1/4 W	10%



# R520A EFF SN B360000-up

# ELECTRICAL PARTS LIST AND SCHEMATIC CORRECTION

CHANGE TO:

C584

283-0616-00

75 pF (nominal value) Selected

520A/R EFF SN B343460 521A/R EFF SN B151100 522A/R EFF SN B090210

ELECTRICAL PARTS LIST AND SCHEMATIC CORRECTION

DRIVER AMPLIFIER Circuit Board Assembly

CHANGE TO:

R694

321-0247-00

 $3.65~k\Omega$ 

Selected

(nominal value)