# INSTRUMENT REFERENCE BOOK 

for the Tektronix Type
106
square-wave generator

For all serial numbers
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RACK ADAPTER 016~0086~00

The rack adapter is designed to house, provide forced air cooling, and AC power for fractional rack=width instruments such as the 106, 114, 184, and 191. The rack adapter is fixed in a standard 19 inch rack. It does not mount on chassis tracks because of the ease with which the individual instruments in the rack can be extended. Any combination of two instruments can be mounted (less cabinets) side. by side in only $5 \frac{1}{4}$ inches of panel height. The price of the rack adapter is $\$ 125$. It will be shown at IEEE.

The front panel power switch on the rack adapter controls the power to the four internal convenience outlets used to power the instruments and the two selfcontained fans. A center divider provides shielding and proper ventilation with one or two of the above instruments installed. A door is provided to install over the vacant hole in single instrument installations in order to provide proper air circulation. The customer who purchases the rack adapter and two instruments would discard the door (Part Number 016-0081-00, \$7.50).

Those instruments that fit in the rack adapter can be ordered without the cabinet. An 18 inch power cord is substituted for the standard cord. The customer should order 106 MOD 146B; 114 MOD 146B; 184 MOD 146B; or 191 MOD 146B. The price of MOD 146B is catalog price less \$25. Availability is the same as the corresponding standard instrument on the PAL or three-week minimum.

| 106 MOD 146B | $\$ 565$ |
| :--- | ---: |
| 114 MOD 146B | 325 |
| 184 MOD 146B | 650 |
| 191 MOD 146B | 375 |

We would like to discourage the purchase of MOD 146B if the instrument is not to be used in the rack adapter. Cabinets are available for those customers who decide to use the instrument out of the rack adapter after having purchased a MOD 146B for use in the rack adapter. The price of each replacement cabinet is \$35.

| Instrument | Rep1acement Cabinet Part Number |
| :---: | :---: |
|  |  |
| 106 | $437-0080-00$ |
| 114 | $437-0077-00$ |
| 184 | $437-0078-00$ |
| 191 | $437-0078-00$ |

TYPE 106 SQUARE WAVE GENERATOR

The Type 106 is a small, lightweight, compact, general-purpose square wave generator with a repetition rate range of 10 hertz to 1.0 megahertz, 12 volts into 50 ohms with $<12$ ns risetime, and $1 / 2$ volts into 50 ohms with $\leq 1$ ns risetime.

Basically the Type 106 is a combination of the 105 and 107 in an instrument about the size of the 184 .

Tentative characteristics:


Hish Amplitude

+ Fast-rise output

- Fast-rise output

Trigeer output


Fig. 1. Illustrates time relationship between trigger and output waveforms. Arrow indicates best comer of the generated square wave.

Front-panel controls:
Amplitude: Three amplitude controls appear on the front panel:
High Amplitude
+Fast-Rise Amplitude
-Fast-Rise Amplitude
Repetition Rate Range Switch, calibrated in steps from 10 hertz to 100 khz
Repetition Rate Multiplier, continuously variable from 1 to 10 Symmetry
Switch, toggle; Left-hand throw labelled "High Amplitude", right-hand throw labelled "Fast-Rise".

Comparison with Type 105:
Advantages of the Type 106 are:
Smaller size: $6^{\prime \prime}$ x $9^{\prime \prime}$ x $15^{\prime \prime}$ vs $17^{\prime \prime}$ x $10^{\prime \prime}$ x $15^{\prime \prime}$
Less weight: 16 lbs . vs 34 lbs .
Panel calibration of repetition rate.
Comparison with Type 107:
Advantages of the Type 106 are:
Much shorter risetime: $\leq 1$ ns vs 3 ns .
Wide-range variable repetition rate.
Design History: Two factors contributed to the development of an instrument containing both the 105 and 107: (1) Inadequate risetime of the 107 for use with 580 -Series scopes; (2) Bench space required to install both a 105 and 107. These factors led to a test fixture (067-0509-00) incorporating the 105 and 107, with improved performance characteristics.

Decision has been made to package the 067-0509-00 test fixture for sale as a catalog instrument to be known as the Type 106.

RACKFRAME MOUNTING FOR THE 114, 184, 191, AND 106

Mechanical Instrument Design is currently working on rackframe mounts for these instruments. All four instruments are in modules of a standard size and shape, with rear panel connectors in standardized locations. The rackframe mounting for this particular module wi=1 be $5-1 / 4^{\prime \prime}$ in height.

Present plans are to provide a rackframe (cradle), which will hold any combination of two instruments, side by side, in a 19" rack. These instrument modules are small enough so that no special provision will be made for mounting in backless racks.

Several optional features will be available for each rackframe.

1. A partition will be provided for shielding between instruments. The use of the optional shield is recommended whenever two instruments are used side by side.
2. Blank panels will be available to cover an unused half of the rackframe.
3. Various combinations of fans will be available, but the actual mechanical design will not be complete until further environmental information is obtained.

Stan Foss/jm
Product Technical Information
November 17, 1965


## INSTRUCTION MANUAL

## MODIFICATION INSERT

TYPE 106
MOD 146B
This manual insert describes the special features of the Type 106. MOD 146B which has been shipped without the standard cabinet, for mounting in a rack adapter. Also, the power cord normally shipped with this instrument has been changed to a coil cord.

## PARTS LIST

The following changes have been made to the parts list of this modified instrument. When ordering replacement parts, specify instrument type, serial number, and MOD number. Include the part number and description of the desired item.

CABINET, Assembly
Delete 1 437-0080-00
POWER CORD, 3-conductor Change 1 161-0031-00

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TYPE 106

MOD 146B

ENGINEERING INSTRUMENT SPECIFICATION
CHANGE NOTICE

Instrument Type:
106 Squarewave Generator
Publication affected: EIS No. 141A Dated 3-7-67 . N
Page: $\quad 1-2 \quad$ Item_ Rep Rate Range - MULTIPLIER

Changed from:

MULTIPLIER
1X to 10X multiplication, variable
Accuracy
$\pm 10 \%$ of indicated value

## Changed to:

MULTIPLIER At least 1 X to 10 X multiplication, variable
(Delete Accuracy statement.)

NOTE: The enclosed slit-punched page replaces the corresponding page in the EIS.

Reason for change:
Clarification


Page 1 of 3

Date March 7, 1967

## REVISION NOTICE

This is a revised Type 106 Square-Wave Generator Engineering

Instrument Specification, and supersedes the Type 106 Square-Wave Generator
Engineering Instrument Specification No. 141 dated 10/18/65.

The following changes/additions have been incorporated into this revision.
Italicized items are new entries. Applicable Electrical and Environmental Performance Validation procedures have been revised to reflect the following changes.

| FROM | TO |
| :--- | :--- |
| Page 1-2: Risetime |  |
| $\leq 12 \mathrm{~ns}$ into $50 \Omega, \leq 70 \mathrm{~ns}$ with |  |
| no external load |  |$\quad$| Page 1-2: Risetime |
| :--- |
| $\leq 12 \mathrm{~ns}$ into $50 \Omega$ at 12 V output amplitude |
| 20 ns into $50 \Omega$ at 0.5 V output amplitude |
| $\leq 120 \mathrm{~ns}$ with no external load |

NOTE: This revision notice is punched for easy removal and insertion in the EIS.

Page 2 of 3

| FROM | T0 |
| :---: | :---: |
| Page 1-3: + OUTPUT and OUTPUT Risetime $\leq 1 \mathrm{~ns} \text { into } 50 \Omega$ | Page 1-4: Risetime (+ OUTPUT and OUTPUT) <br> $\leq 1 \mathrm{~ns}$ into $50 \Omega$ at 500 mV output amplitude |
| Page 1-3: + OUTPUT - OUTPUT AMPLITUDE Range <br> 50 mV to 500 mV into $50 \Omega$ | Page 1-4: TRANSITION AMPLITUDE Range $\leq 50 \mathrm{mV}$ to $\geq 500 \mathrm{mV}$ into $50 \Omega$ |
| Page 1-3: + OUTPUT - OUTPUT <br> Aberration -- Leading Edge <br> $\leq 2 \%$ in first 5 ns | ```Page 1-4: Aberration (Leading Edge) \leq + and - 2% or + and - 6 mV whichever is greater, in the first 5 ns into 50 \Omega``` |
| Page 1-3: Symmetry Change with Amplitude <br> Less than 150 ns | Page 1-4: Duty Cycle Change with TRANSITION AMPLITUDE $\begin{aligned} & \leq 150 \mathrm{~ns}, 50 \mathrm{mV} \text { to } 500 \mathrm{mV} \text { output } \\ & \text { amplitude } \end{aligned}$ |
| Page 1-4: Pulse or Squarewave <br> 2.5 to 50 V amplitude | Page 1-4: Pulse or Squarewave <br> Amplitude Range: 2.5 V to 50 V <br> Frequency Range: 100 Hz to 1 MHz |
| Page 1-4: Sinewave 5 to 100 pp | Page 1-4: Sinewave <br> Amplitude Range: 5 V to 100 V P-P <br> Frequency Range: 100 Hz to 1 MHz |
| Page 1-4: Risetime <br> $\leq 50 \mathrm{~ns}$ into $50 \Omega$ | $\begin{aligned} & \text { Page 1-5: Risetime (Rate of Change) } \\ & \leq 50 \mathrm{~ns} \text { into } 50 \Omega, 0 \mathrm{~V} \text { to } 0.1 \mathrm{~V} \\ & \text { output amplitude } \end{aligned}$ |
| $\begin{aligned} & \text { Page } 1-4: \text { Amp1itude } \\ & \geq 0.4 \mathrm{~V} \text { into } 50 \Omega \end{aligned}$ | $\begin{aligned} & \text { Page } 1-5: \text { Amplitude } \\ & \geq 0.1 \mathrm{~V} \text { into } 50 \Omega \\ & \geq 0.4 \mathrm{~V} \text { with no external load } \end{aligned}$ |
| Page 1-4: Delay Time <br> Less than 50 ns from + trigger <br> leading edge to leading edge of all outputs | Page 1-5: Delay Time <br> $\leq 50 \mathrm{~ns}$ from + trigger leading edge to leading edge of all outputs |
| Page 1-4: Fuse <br> 2.0 A, slow blow, 3 ag 115 V operation <br> 1.0 A , slow blow, 3 ag 230 V operation | Page 1-5: Fuse Data <br> 1.25 A slow-blowing type for 115 V operation 0.6 A slow-blowing type for 230 V operation |

Page 3 of 3

| FROM | T0 |
| :---: | :---: |
| $\begin{array}{ll} \text { Page } 1-5: & \text { Regulation } \\ \text { "A" Supply } & 12 \mathrm{~V} \text { squarewave }+10 \%, \\ & \begin{array}{l} \text { into } 50 \Omega, \text { over line } \\ \\ \\ \\ +150 \mathrm{~V} \\ -150 \mathrm{~V} \\ +10.0 \mathrm{~V} \\ -10.0 \mathrm{~V} \\ - \pm 10 \% \\ \pm \pm 10 \% \\ \pm \\ \hline \end{array} \\ & \leq 10 \% \end{array}$ | $\begin{aligned} & \text { Page 1-6: Tolerance (Long Term) } \\ & \text { "A" } 1 \text { " } 150 \frac{\text { "A" }-150}{ \pm 10 \%} \frac{\text { "A" }-20}{ \pm 10 \%} \frac{-10}{ \pm 10 \%} \frac{+10}{ \pm 15 \%} \\ & \frac{\text { "A" Supp1y }}{\text { Variable }} \end{aligned}$ |
| $\begin{array}{ll} \text { Page 1-5: } & \text { Ripple } \\ \text { "A" Supply } & \leq 0.5 \mathrm{~V} \mathrm{pp} \\ +150 \mathrm{~V} & \leq 0.5 \mathrm{~V} \mathrm{pp} \\ -150 \mathrm{~V} & \leq 0.5 \mathrm{~V} \mathrm{pp} \\ +10.0 \mathrm{~V} & \leq 0.2 \mathrm{~V} \mathrm{pp} \\ -10.0 \mathrm{~V} & \leq 0.2 \mathrm{~V} \mathrm{pp} \end{array}$ | $\begin{aligned} & \text { Page 1-6: Ripp1e (P-P) } \\ & \frac{\text { "A" }+150}{0.75 \mathrm{~V}} \frac{\text { "A" }-150}{0.75 \mathrm{~V}} \frac{\text { "A" }-20}{0.75 \mathrm{~V}} \frac{-10}{0.2 \mathrm{~V}} \frac{+10}{0.2} \\ & \frac{\text { "A" Supp1y }}{0.75 \mathrm{~V}} \end{aligned}$ |
| Page 1-5: "A" Supply <br> 12 V squarewave into $50 \Omega$ at 115 VAC line | DELETE |

# ENGINEERING INSTRUMENT SPECIFICATION 

# TYPE 106 <br> SQUARE-WAVE GENERATOR 

FOR INTERNAL USE ONLY TEKTRONIX, INC.

## ENGINEERING

## INSTRUMENT SPECIFICATION

TYPE 106

SQUARE WAVE

GENERATOR

Prepared by Engineering Writing Dept. Engineering Writer_ Eal Earl Neuman


FOR INTERNAL USE ONLY

TEKTRONIX, INC.

## PREFACE

This Engineering Instrument Specification is the reference document for all company activity concerning the electrical and environmental performance of the subject instrument. This document is printed in two issues: a tentative copy printed on or before Prototype Release of the instrument, and a final copy printed following Engineering Release. Occasionally, if justified by the number of changes, the final copy is updated and reissued following Pilot Production.

The major function of the Engineering Instrument Specification is to provide electrical and environmental performance information to the following departments:

Manuals
Product Technical Information
Engineering Product Reliability
Marketing Technical Training
Product Manufacturing Staff Engineering

## Advertising

International Manufacturing
Technical Support
International Marketing
Manufacturing Quality Assurance
Manufacturing Management

Performance Requirements listed in Section 1 are customer performance requirements, and are to be treated as prescribed by their respective code (see page 1-1 for code description). Factory test limits are excluded from the Engineering Instrument Specification. Those items coded Internal Use Onlu are not to be interpreted as factory test limits. Factory test limits are established by Product Manufacturing Staff Engineering, and appear in documents issuing from that department.

Periodically, an Engineering Instrument Specification may be revised and reprinted. The revised Engineering Instrument Specification will then have a 3-digit specification number followed by a capital letter printed in the upper right corner of the front cover, e.g. 000A for the first revision, 000B for the second revision, etc.

Changes in the Engineering Instrument Specification may be made only via the Instrument Performance Characteristic Change Request form of which 3 are included at the back of this copy (contact the PE\&M Engineering Writing Department for additional forms).

Abbreviations and symbols appearing in the Engineering Instrument Specification conform to Tektronix Standard No. A-100, Recommended Short Forms.

This page is used as a guide to insure that all changes to this book have been made. When a Change Notice is received, $\log$ it on this page, then write in the actual change information on the appropriate page. Change Notice numbers are assigned in sequence ( $X X X-1$, XXX-2, etc.). Absence of a number from the sequence indicates a change which has not been entered.

| CHANGE NOTICE NUMBER | EFFECTIVE DATE OF CHANGE | PAGE NUMBER |
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## INTRODUCTION

This is the Engineering Instrument Specification for the Type 106 Square-Wave Generator, and is the reference document for all company activity concerning performance requirements. This specification is for internal use only, and supersedes the Type 106 Engineering Instrument Specification dated October 18, 1965.

## Description

The Type 106 is a squarewave generator that can be used as a laboratory or general purpose instrument. It produces variable repetition rate squarewaves of high-amplitude slow rise, or low-amplitude fast rise. One unique feature of this instrument is that all squarewave outputs are from either a positive or negative potential to ground.

The high-amplitude function provides variable amplitude squarewaves up to 120 V in amplitude with no external termination, or 12 V ( 240 mA ) into a $50 \Omega$ load.

The fast-rise function provides variable amplitude, positive and negativegoing squarewaves of less than 1 ns risetime into a $50 \Omega$ load, that can be used independently or simultaneously by means of two output connectors.

Provision has been made for sync input and trigger output via front-panel BNC connectors.

Sync operation can be obtained through the use of sinewaves, squarewaves or pulses.

The trigger output waveform is a differentiated squarewave that coincides with the squarewave outputs as follows:

TRIGGER OUTPUT

HI AMPLITUDE OUTPUT


Functions of Controls and Connectors
REPETITION RATE RANGE

A five-position switch that selects the minimum repetition rate. Each step increases the repetition rate by a factor of 10.

## MULTIPLIER

Allows continuously variable repetition rates between ranges of the REPETITION RATE RANGE switch, and extends the 100 kHz setting to 1 MHz .

## SYMMETRY

Allows the duty cycle to be varied from approximately 45 to $55 \%$.

```
HI AMPLITUDE - FAST RISE
```

A two-position switch that selects high amplitude slow-rise or fast-rise low amplitude operation.

## AMPLITUDE

Controls the output amplitude of the high amplitude function.

+ TRANSITION AMPLITUDE
Controls the output amplitude of the fast-rise + OUTPUT.
- TRANSITION AMPLITUDE

Controls the output amplitude of the fast-rise + OUTPUT.
SYNC INPUT
BNC connector.
TRIGGER OUTPUT
BNC connector.
OUTPUT
GR 874 connector.

+ OUTPUT

GR 874 connector.

- OUTPUT

GR 874 connector.
Miscellaneous Information
Ventilation
The Type 106 cabinet provides for a minimum air flow of $12^{13} / \mathrm{min}$.

## Finish

Front panel is anodized aluminum. Cabinet is finished in blue vinyl paint. Warm-up Time

Twenty minutes for rated accuracies at $25^{\circ} \mathrm{C} \pm 5^{\circ} \mathrm{C}$.
Dimensions
9" W, 6" H, 14-3/4" L.
Weight
$\cong 10.5 \mathrm{lbs}$, without cabinet

## SECTION 1

ELECTRICAL CHARACTERISTICS

## IMPORTANT

The following performance requirements and their related validation procedures in Section 3 apply only to a calibrated system operating within the environmental limits specified in Section 2, Environmental Characteristics, unless stated otherwise.

Performance requirements are validated by Engineering according to Section 3. Production test methods may differ.

Conditions under which a performance requirement is valid may be listed under Supplemental Information or in Section 3 (Electrical Performance Validation). These conditions are an essential part of the performance requirement.

The following codes are used to categorize performance requirements:
G (General Use) This performance requirement may be quoted to a customer.

I (Internal Use Only) This performance requirement will not be quoted to a customer.

A (A11) It is recommended by Engineering that electrical testing of this performance requirement be performed on $100 \%$ of instruments.

S (Sampled) This performance requirement carries a high confidence level and may be tested on a sample basis.

N (Not Tested)

NOTE: Code column also provides step number of related validation procedure.


| 1.3 HI AMPLITUDE OUTPUT (cont'd) |  |  |  |
| :---: | :---: | :---: | :---: |
| Characteristic | Performance Requirement | Code | Supplemental Information |
| AMPLITUDE Range | $\leq 0.5 \mathrm{~V}$ to $\geq 12 \mathrm{~V}$ into $50 \Omega$ | $\begin{gathered} 3.4 .2 \\ \mathrm{GA} \end{gathered}$ | At 115 VAC line voltage |
|  | $\leq 7 \mathrm{~V}$ to $\geq 120 \mathrm{~V}$ with no external load |  |  |
| Aberration (Leading Edge) | $\leq+$ and $-2 \%$ in the first 100 ns , into $50 \Omega$ | $\begin{gathered} 3.4 .3 \\ \mathrm{GA} \end{gathered}$ | Measured on positivegoing transition. Flat top aberration is typically less than $0.5 \%$ P-P after the first 100 ns . Exclude preshoot in the last 100 ns preceeding the negative-going transition. |
| Low-Frequency Distortion | $\leq 15 \%$ into $50 \Omega$ at 10 Hz | $3.4 .4$ | At 115 VAC line and with |
| (Slope) | $\leq 5 \%$ into $50 \Omega$ at 100 Hz |  |  |
| Duty Cycle Change with Repetition Rate | $\leq 5 \%$ | $\begin{gathered} 3.4 .5 \\ \text { IS } \end{gathered}$ |  |
| Repetition Rate Change with SYMMETRY | $\leq 10 \%$ | $\begin{gathered} 3.4 .6 \\ \text { IS } \end{gathered}$ |  |
| OUTPUT Amplitude Change with Line Voltage | < $20 \%$ reduction in output amplitude from 126.5 VAC to 103.5 VAC with output terminated in $50 \Omega$, and AMPLITUDE maximum cw | $\begin{gathered} 3.4 .7 \\ \text { IA } \end{gathered}$ |  |
| Output Impedance |  | GN | $\begin{aligned} & \simeq 600 \Omega \text { paralleled by } \\ & \simeq 85 \mathrm{pF} \end{aligned}$ |


| 1.4 FAST RISE OUTPUTS |  |  |  |
| :---: | :---: | :---: | :---: |
| Characteristic | Performance Requirement | Code | Supplemental Information |
| $\begin{aligned} & \text { Risetime (+ OUTPUT and - } \\ & \text { OUTPUT) } \end{aligned}$ | $\leq 1 \mathrm{~ns}$ into $50 \Omega$ at 500 mV output amplitude | $\begin{gathered} 3.5 .1 \\ \mathrm{GA} \end{gathered}$ |  |
| TRANSITION AMPLITUDE Range | $\leq 50 \mathrm{mV}$ to $\geq 500 \mathrm{mV}$ into 50 ת | $\begin{gathered} 3.5 .2 \\ \mathrm{GA} \end{gathered}$ |  |
| Aberration (Leading Edge) | $\begin{aligned} & \leq+ \text { and }-2 \% \text { or }+ \text { and }-6 \mathrm{mV} \text { whichever is greater, } \\ & \text { In the first } 5 \mathrm{~ns} \text { into } 50 \Omega \end{aligned}$ | $\underset{\mathrm{GA}}{3.5 .3}$ | Measure positive-going transition for + OUTPUT and negative-going transition for - OUTPUT. High frequency ringing must be greater than 500 MHz . Flat top aberration is typically less than $0.5 \%$ $\mathrm{P}-\mathrm{P}$ after the first 5 ns . |
| Duty Cycle Change with TRANSITION AMPLITUDE | $\leq 150 \mathrm{~ns}, 50 \mathrm{mV}$ to 500 mV output amplitude | $\underset{G A}{3.5 .4}$ |  |
| 1.5 SYNC INPUT |  |  |  |
| Pulse or Squarewave | 2.5 V to 50 V | $\begin{gathered} 3.6 .1 \\ \mathrm{GA} \end{gathered}$ | To insure stable operation risetime should be less than $12.5 \%$ of the period |
| Amplitude Range |  |  |  |
| Frequency Range | 100 Hz to 1 MHz |  |  |
| Sinewave | 5 V to 100 V P-P | $\begin{gathered} 3.6 .2 \\ G S \end{gathered}$ |  |
| Amplitude Range |  |  |  |
| Frequency Range | 100 Hz to 1 MHz |  |  |


| 1.6 TRIGGER OUTPUT |  |  |  |
| :---: | :---: | :---: | :---: |
| Characteristic | Performance Requirement | Code | Supplemental Information |
| + and - Triggers | $\leq 50 \mathrm{~ns}$ into $50 \Omega, 0 \mathrm{~V}$ to 0.1 V output amplitude |  | The + and - triggers are coincident with the rise |
| Risetime (Rate of Change ) |  | $\begin{gathered} 3.7 .1 \\ \mathrm{GA} \end{gathered}$ | and fall of the HI AMPLITUDE OUTPUT |
| Amplitude | $\geq 0.1 \mathrm{~V}$ into $50 \Omega$ | $\begin{gathered} 3.7 .2 \\ \mathrm{GA} \\ \mathrm{IN} \end{gathered}$ |  |
|  | $\geq 0.4 \mathrm{~V}$ with no external load |  |  |
| Time Jitter | $\leq 300 \mathrm{ps}$ | $\underset{\mathrm{GA}}{3.7 .3}$ | Check jitter one full cycle from triggering edge of pulse |
| Delay Time | < 50 ns from + trigger leading edge to leading edge of all outputs | $\underset{\mathrm{GA}}{3.7 .4}$ |  |
| 1.7 | POWER SOURCE |  |  |
| Line Voltage Ranges | 103.5 VAC to 126.5 VAC | $\begin{gathered} 3.8 .1 \\ G S \end{gathered}$ |  |
|  | 207 VAC to 253 VAC |  |  |
| Line Frequency | 50 Hz to 60 Hz | $\begin{gathered} 3.8 .2 \\ \text { IS } \end{gathered}$ |  |
| Fuse Data | 1.25 A slow-blowing type for 115 VAC operation | GN |  |
|  | 0.6 A slow-blowing type for 230 VAC operation |  |  |
| Power Consumption |  | GN | $\simeq 85 \mathrm{~W}$ at 115 VAC line |

See page 1-1 for coding legend


SECTION 2
ENVIRONMENTAL CHARACTERISTICS

The following Environmental Characteristics apply only when the instrument is tested as described in Section 4, Environmental Performance Validation. The Type 106 is a laboratory instrument.

| Characteristic | Performance Requirement | Supplemental Information |
| :---: | :---: | :---: |
| Temperature |  |  |
| Nonoperating | $-40^{\circ} \mathrm{C}$ to $+65^{\circ} \mathrm{C}$ |  |
| Operating | $0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$ |  |
| Altitude |  |  |
| Nonoperating | To 50,000 feet |  |
| Operating | To 15,000 feet |  |
| Vibration |  |  |
| Operating | 15 minutes along each axis at 0.015". Vary the frequency from 10 to 50 to $10 \mathrm{c} / \mathrm{s}$ in 1-minute cycles. Three minutes at any resonant point or at $50 \mathrm{c} / \mathrm{s}$. | ```Tested with instrument secured to vibration platform``` |
| Shock |  |  |
| Nonoperating | 30 g 's, $1 / 2$ sine, 11 ms duration, 1 shock per axis | Guillotine-type shocks |
| Transportation |  |  |
| Package Vibration | 1 hour, slightly in excess of 1 g | Package should just leave vibration surface |
| Package Drop | $30^{\prime \prime}$ on 1 corner, all edges radiating from that corner and all flat surfaces for a total of 10 drops |  |

## SECTION 3

## ELECTRICAL PERFORMANCE VALIDATION

| 1 | Oscilloscope | Tektronix Type 540-series |
| :---: | :---: | :---: |
| 1 | Dual-Trace Plug-in Unit | Tektronix Type 1A1 |
| 1 | Sampling Oscilloscope | Tektronix Type 661 |
| 1 | Dual-Trace Sampling Unit | Tektronix Type 4S1 |
| 1 | Timing Unit | Tektronix Type 5T3 |
| 1 | Standard Amplitude Calibrator | Tektronix Part no. 067-0502-00 |
| 1 | Constant Amplitude Signal Generator | Tektronix Type 191 |
| 1 | DC Voltage Bridge | Tektronix Part No. 067-0543-99 |
| 1 | Line Voltage Control Unit | Tektronix Type 76 TU |
| 1 | Line Frequency Control Unit | Tel-Instrument Type 4100-I-H10S |
| 1 | 10x Probe, P6006 | Tektronix Part No. 010-0127-00 |
| 1 | 1X Probe, P6028 | Tektronix Part No. 010-0074-00 |
| 1 | BNC T Connector | Tektronix Part No. 103-0030-00 |
| 1 | 10:1 Attenuator, $50 \Omega$ | Tektronix Part No. 011-0059-00 |
| 1 | $50 \Omega$ Termination | Tektronix Part No. 011-0049-00 |
| 1 | $50 \Omega$ Termination, 2 W | Tektronix Part No. 017-0083-00 |

### 3.2 REPETITION RATE

### 3.2.1 Repetition Rate Range

Performance Requirement: Multiplier: 1 to 10X multiplication, variable

Accuracy : $\pm 10 \%$ of indicated value
Procedure: Set REPETITION RATE RANGE at 100 kHz and MULTIPLIER at 10. Connect test scope 10X Probe to the HI AMPLITUDE OUTPUT, and set test scope Time/cm at $1 \mu \mathrm{~s}$. Check for 1 cycle/cm.

Set REPETITION RATE RANGE at 10 kHz and MULTIPLIER at 1 . Set test scope Time/cm at $100 \mu$ s and check for 1 cycle/cm.

Check all other positions of the REPETITION RATE RANGE switch, with the MULTIPLIER at X1 and X10, for less than $10 \%$ deviation from the indicated value.

### 3.3 SYMMETRY

### 3.3.1 SYMMETRY Range

Performance Requirement: Varies duty cycle from $\leq 45 \%$ to $\geq 55 \%$
Procedure: Connect test scope as in 3.2 .1 and set REPETITION RATE RANGE and MULTIPLIER for 1 cycle/10 cm . Vary SYMMETRY from limit to limit and check duty cycle.

### 3.4 HI AMPLITUDE OUTPUT

3.4.1 Risetime

Performance Requirement:
$\leq 12$ ns into $50 \Omega$ at 12 V output amplitude
$\leq 20$ ns into $50 \Omega$ at 0.5 V output amplitude $\leq 120$ ns with no external load

Procedure: Connect 10X GR attenuator to 106 HI AMPLITUDE OUTPUT--5 ns RG-8 cable-m-vertical input of 4 Sl sampling system. Check risetime at 0.5 V and 12 V amplitude.

Remove GR cable and 10X attenuator from Type 106 and check unterminated risetime with test scope 10X probe.
3.4.2 AMPLITUDE Range

Performance Requirement:

$$
\begin{aligned}
& \leq 0.5 \mathrm{~V} \text { to } \geq 12 \mathrm{~V} \text { into } 50 \Omega \\
& \leq 7 \mathrm{~V} \text { to } \geq 120 \mathrm{~V} \text { with no external load }
\end{aligned}
$$

Procedure: Terminate HI AMPLITUDE OUTPUT in $50 \Omega$ and connect to 1 Al vertical input. Check output amplitude over the range of the AMPLITUDE control.

Remove the $50 \Omega$ termination and again check output amplitude over the range of AMPLITUDE control.
3.4.3 Aberration (Leading Edge)

Performance Requirement: $\leq+$ and $-2 \%$ in the first 100 ns , into $50 \Omega$

Procedure: Connect 10X GR attenuator to 106 HI AMPLITUDE OUTPUT ---5 ns RG-8 cable---vertical input of 4 S1 sampling system. Set
-

4S1 vertical sensitivity at $0.2 \mathrm{~V} / \mathrm{cm}$ and adjust AMPLITUDE for 5 cm of deflection. Increase vertical sensitivity by a factor of 10. (Sensitivity now equals $2 \% / \mathrm{cm}$ ). With 4 Sl DC offset, position top of the squarewave on screen and check aberrations in the first 100 ns as per illustration below.

3.4.4 Low-Frequency Distortion on Negative Half-Cycle (Slope)

Performance Requirement: $\leq 15 \%$ into $50 \Omega$ at 10 Hz
Procedure: Terminate HI AMPLITUDE OUTPUT in $50 \Omega$, then connect to 1 Al vertical input. Set AMPLITUDE cw and REPETITION RATE RANGE at 10 Hz . Check slope at bottom of squarewave.

Set REPETITION RATE RANGE at 100 Hz , and again check slope at bottom of squarewave.
3.4.5 Duty Cycle Change with Repetition Rate

Performance Requirement: $\leq 5 \%$
Procedure: Connect HI AMPLITUDE OUTPUT to 4 Sl vertical input. Set $5 \mathrm{~T} 3 \mathrm{Time} / \mathrm{cm}$ and 106 REPETITION RATE RANGE to observe one full cycle. Turn the REPETITION RATE RANGE switch throughout its range, changing $5 \mathrm{~T} 3 \mathrm{Time} / \mathrm{cm}$ as necessary, and check duty cycle change.
3.4.6 Repetition Rate Change with SYMMETRY

Performance Requirement: $\leq 10 \%$
Procedure: Connect HI AMPLITUDE OUTPUT to 4 Sl vertical input. Set $5 \mathrm{~T} 3 \mathrm{Time} / \mathrm{cm}$ and 106 REPETITION RATE RANGE to observe one cycle/cm. Turn SYMMETRY control from one limit to the other and check change in repetition rate.

### 3.4.7 Output Amplitude Change with Line Voltage

Performance Requirement: $\leq 20 \%$ reduction in output amplitude from 126.5 VAC to 103.5 VAC with output terminated in $50 \Omega$, and AMPLITUDE maximum cw

Procedure: Terminate HI AMPLITUDE OUTPUT to $50 \Omega$, then connect to 1A1 vertical input. Set AMPLITUDE fully cw. With Line Voltage Control Unit, set line voltage at 126.5 VAC and note amplitude. Set line voltage to 103.5 VAC and check amplitude change.

### 3.5 FAST RISE OUTPUTS

3.5.1 Risetime (+ OUTPUT and - OUTPUT)

Performance Requirement: $\leq 1 \mathrm{~ns}$ into $50 \Omega$ at 500 mV output amplitude

Procedure: Connect FAST RISE + OUTPUT to 4 S1 vertical input. Set + TRANSITION AMPLITUDE for 500 mV of signal. Set 4 Sl Millivolts/cm switch and Variable to observe a 4 cm display. Check risetime. Repeat for FAST RISE - OUTPUT.

### 3.5.2 TRANSITION AMPLITUDE Range

Performance Requirement: $\leq 50 \mathrm{mV}$ to $\geq 500 \mathrm{mV}$ into $50 \Omega$
Procedure: Connect FAST RISE + OUTPUT to 4 Sl vertical input. Check amplitude of squarewave over the range of + TRANSITION AMPLITUDE control. Repeat for FAST RISE - OUTPUT.
3.5.3 Aberration (Leading Edge)

Performance Requirement: $\leq+$ and $-2 \%$ or + and -6 mV whichever is greater, in the first 5 ns into $50 \Omega$

Procedure: Connect FAST RISE + OUTPUT to 4 Sl vertical input. Set + TRANSITION AMPLITUDE fully cw . Set $4 \mathrm{~S} 1 \mathrm{Millivolts/cm} \mathrm{at} 10$ (one cm of deflection now equals $2 \%$ ) and check aberrations in the first 5 ns starting at the $98 \%$ amplitude point as pictured below. Repeat this check for the FAST RISE - OUTPUT.


### 3.5.4 Duty Cycle Change with TRANSITION AMPLITUDE

Performance Requirement: $\frac{\leq}{\text { amplitude }} 150 \mathrm{~ns}, 50 \mathrm{mV}$ to 500 mV output

Procedure: Set REPETITION RATE RANGE at 100 kHz and MULTIPLIER at 10. Set $4 \mathrm{~S} 1 \mathrm{Time} / \mathrm{cm}$ to observe one cycle in 10 cm . Externally trigger 4 Sl from 106 TRIGGER OUTPUT. Turn TRANSITION AMPLITUDE from one limit to the other and check duty cycle change. Repeat for FAST RISE - OUTPUT.

### 3.6 SYNC INPUT

### 3.6.1 Pulse or Squarewave

Performance Requirement: Amplitude Range --- 2.5 V to 50 V
Frequency Range --- 100 Hz to 1 MHz
Procedure: Connect a 2 V squarewave from a Standard Amplitude Calibrator through a BNC $T$ to Type 106 SYNC INPUT and to Channel 1 of 1 Al test scope. Connect HI AMPLITUDE OUTPUT to Channe1 2 of 1A1. Set REPETITION RATE RANGE and MULTIPLIER so Type 106 is free-running at a frequency slightly below the Standard Amplitude Calibrator frequency. Set SAC at 5 V and check that Type 106 is now running at the same frequency as the $S A C$.

### 3.6.2 Sinewave

Performance Requirement: Amplitude Range --- 5 V to 100 V P-P Frequency Range --- 100 Hz to 1 MHz

Procedure: Check for sync operation as in 3.6.1 with a sinewave generator at 100 Hz and $1 \mathrm{MHz}, 5 \mathrm{~V}$ P-P signal applied.

### 3.7 TRIGGER OUTPUT

3.7.1 Risetime (Rate of Change)

Performance Requirement: $\leq 50 \mathrm{~ns}$ into $50 \Omega, 0 \mathrm{~V}$ to 0.1 V output amplitude

Procedure: Connect a $50 \Omega$ termination to TRIGGER OUTPUT connector. With Type 1A1 test scope, check risetime of both + and - trigger output waveforms.


### 3.7.1 Risetime (Rate of Change) (cont ${ }^{\text {d }}$ )



### 3.7.2 Amp1itude

Performance Requírement: $\geq 0.1 \mathrm{~V}$ into $50 \Omega$
Procedure: Connect a $50 \Omega$ termination to TRIGGER OUTPUT and check output amplitude of both the + and -triggers with a 1 Al test scope.
3.7.3 Time Jitter

Performance Requirement: $\leq 300 \mathrm{ps}$
Procedure: Connect FAST RISE + OUTPUT to 4 SI vertical input, and externally trigger $4 S 1$ from Type 106 positive-going TRIGGER OUTPUT. Check width of the leading edge of the positive-going squarewave for jitter. Repeat this check for the FAST RISE OUTPUT and HI AMPLITUDE OUTPUT as illustrated.


### 3.7.4 Delay Time

Performarce Requirement: $\leq 50 \mathrm{~ns}$ from + trigger leading edge to leading edge of all outputs

Procedure: Connect TRIGGER OUTPUT through a $50 \Omega$ termination to Channel 1 of lAl test scope. Connect FAST RISE + OUTPUT through a $50 \Omega$ termination of Channel 2 of 1Al test scope. Set V/CM switches on 1A1 for approximately equal amplitude waveforms. Set 1A1 Mode switch at Alt, then check delay from + leading edge of trigger waveform to leading edge of FAST RISE + OUTPUT. Check delay from + leading edge of trigger waveform to all other squarewave outputs.
3.8 POWER SOURCE

### 3.8.1 Line Voltage Ranges

Performance Requirement: 103.5 VAC to 126.5 VAC 207 VAC to 253 VAC

Procedure: Check with TU-76 Line Voltage Control Unit to vary the line voltage while monitoring the regulated DC power supplies with test scope.
3.8.2 Line Frequency

Performance Requirement: 50 Hz to 60 Hz
Procedure: Check with Tel-Instrument Type 4100-I-H10S. Monitor the regulated DC supplies with test scope and check line frequency over the above limits.
3.9 INTERNAL POWER SUPPLIES
3.9.1 Tolerance (Long Term)

Performance Requiremient:

$$
\frac{\text { "A" }+150}{ \pm 10 \%} \frac{\text { "A" }-150}{ \pm 10 \%} \frac{\text { "A" -20 }}{ \pm 10 \%} \quad \frac{-10}{ \pm 15 \%} \quad \frac{ \pm 10}{ \pm 15 \%} \frac{\text { "A" Supply }}{\text { Variable }}
$$

Procedure: Measure the DC supplies with DC Voltage Bridge. The supplies will be within their respective tolerances at $+25^{\circ} \mathrm{C} \pm 5^{\circ} \mathrm{C}$ for any 500 hour period after the first 200 hours.

### 3.9.2 Ripple ( $\mathrm{P}-\mathrm{P}$ )

Performance Requirement:

$$
\frac{" A "+150}{0.75 \mathrm{~V}} \quad \frac{" \mathrm{~A} "-150}{0.75 \mathrm{~V}} \quad \frac{" \mathrm{~A} "-20}{0.75 \mathrm{~V}} \quad \frac{-10}{0.2 \mathrm{~V}} \frac{+10}{0.2 \mathrm{~V}} \frac{\text { "A" Supp1y }}{0.75 \mathrm{~V}}
$$

Procedure: Measure ripple with test scope and 1X probe connected to the supply under test. Check each supply over line voltage limits.

## SECTION 4

ENVIRONMENTAL PERFORMANCE VALIDATION

### 4.1 Temperature

Perform all tests in a single chamber and, when changing chamber ambient temperature, do not exceed a change rate of $5^{\circ} \mathrm{C}$ per minute.

### 4.1.1 Nonoperating

Perform all electrical tests, described in Section 3, at $25^{\circ} \mathrm{C}$. Then turn the instrument off and store at $-40^{\circ} \mathrm{C}$ ambient for 4 hours.

Change ambient temperature to $+65^{\circ} \mathrm{C}$ and again store for 4 hours.

Return the ambient temperature to $25^{\circ} \mathrm{C}$, allow 4 hours for stabilization, and again perform all electrical tests.

## Failure Criteria

Instrument and components must meet performance requirements before and after storage. If necessary, internal or external adjustments may be performed to meet required accuracies.

Cracking, warping, discoloration or any deformation which interferes with a normal mechanical function also constitute failures.

### 4.1.2 Operating

Perform all electrical tests, described in Section 3, at $25^{\circ} \mathrm{C}$.

With the instrument turned off, change ambient temperature to $0^{\circ} \mathrm{C}$ and allow the instrument to stabilize for 4 hours. At the end of this period, turn the instrument on, allow 20 minutes for warm-up, then check accuracy and operation of all front-panel functions.

With the instrument operating, change the chamber ambient temperature to $+50^{\circ} \mathrm{C}$ and allow 4 hours for stabilization.

At the end of 4 hours, again check the accuracy and operation of all front-panel functions.

Return the instrument to $25^{\circ} \mathrm{C}$, allow 4 hours for stabilization, then perform all electrical tests described in Section 3.

## Failure Criteria

Instrument must meet performance requirements at each step in the test. Controls and switches must operate normally.

### 4.2 Altitude

Altitudes described in this section are referred to sea level. "Normal altitude", when used, refers to the natural elevation (outside the chamber) of the test facility site.

### 4.2.1 Nonoperating

Perform all electrical tests described in Section 3 at $25^{\circ} \mathrm{C}$ and normal altitude. Then store, with the instrument turned off for 4 hours at 50,000 feet and $-40^{\circ} \mathrm{C}$.

Return chamber to normal altitude and $25^{\circ} \mathrm{C}$, and allow 4 hours for stabilization. At the end of this period, repeat the electrical tests.

This test may be performed with the nonoperating temperature test (4.1.1).

Failure Criteria
The instrument must meet performance requirements before and after the altitude test, and must experience no cracking or warping, nor any deformation which interferes with a normal mechanical function.

### 4.2.2 Operating

Perform all electrical tests described in Section 3 at $25^{\circ} \mathrm{C}$ and at normal altitude.

Operate the instrument for 4 hours at 15,000 feet. At the end of this period, maintain that altitude and measure accuracy and operation of front-panel functions.

When necessary, open the vacuum chamber and perform required switching as rapidly as possible. Then return the chamber to the specified altitude and allow 1 hour for stabilization before continuing the tests.

Return the instrument to normal altitude and repeat all electrical tests described in Section 3.

Failure Criteria

Instrument will meet performance requirements before, during, and after the operating altitude tests. Any evidence of malfunction constitutes failure.
4.3 Vibration

### 4.3.1 Operating

Perform all electrical tests described in Section 3 before vibrating the instrument.

Fasten the instrument securely to the vibration platform.

With the instrument operating, vibrate for 15 minutes along each of the 3 axes at a total displacement of $0.015^{\prime \prime}\left(1.9 \mathrm{~g}^{\prime} \mathrm{s}\right.$ at $50 \mathrm{c} / \mathrm{s}$ ), and with the frequency varied from 10 to 50 to $10 \mathrm{c} / \mathrm{s}$ in 1 -minute cycles. Hold at any resonant point for 3 minutes.

If no resonances are present, vibrate at $50 \mathrm{c} / \mathrm{s}$ for 3 minutes in each axis for a total vibration time of about 55 minutes.

Turn off the vibration platform and repeat all electrical tests described in Section 3.

Failure Criteria

The instrument must meet performance requirements before and after the vibration tests. (Sporadic output during vibration is permissible.)

Mechanical failures are indicated by:

Broken leads
Broken chassis
Broken components
Loose parts
Excessive wear
Component fatigue
Change in component value outside rated tolerance
Deformation which interferes with a normal mechanical function

Test will be completely rerun after repairing any of these failures except vacuum tubes. Vacuum tubes may be replaced and the test continued at the point of failure.
4.4 Shock
4.4.1 Nonoperating

Perform all electrical tests described in Section 3 before proceeding with the shock tests.

Subject the instrument to guillotine-type shocks of 30 g 's, $1 / 2$ sine, 11 ms duration; 1 such shock each direction along each of the 3 major axis for a total of 6 shocks.

Repeat all electrical tests described in Section 3.
Failure Criteria
The instrument will meet performance requirements before and after the shock tests.

There must be no cracked or broken chassis, components or leads; component deformation of 0.100 " or more; nor any deformation which interferes with a normal mechanical function.

### 4.5 Transportation

Perform all tests described in Section 3 before conducting the transportation tests, then place the instrument in the carton in the manner in which it is normally shipped.

### 4.5.1 Package Vibration

Vibrate for 1 hour in a manner causing the package to just leave the vibration platform (slightly in excess of 1 g ).
4.5.2 Package Drop

Drop the package from a height of $30^{\prime \prime}$ on one corner, on all edges radiating from that corner, and on all flat surfaces for a total of 10 drops.

After the transportation tests, repeat all electrical tests described in Section 3.

Failure Criteria
The instrument must meet performance requirements before and after the transportation tests. There must be no broken components, leads, or chassis members, nor any deformation vhich interferes with a normal mechanical function.

This form requests changes in the Engineexing Instrument Specification (salmon book) or in performance characteristics quoted to the customer via publications such as the Catam log or Instruction Manual. When the instrument has an Engineering Instrument Specification, then it is the controlling document.

Return completed form to Product Evaluation and Modification Engineering Writing 50/425 for approval and distribution.

Instrument Type: $\qquad$
Publication affected: $\qquad$ No. Dated $\qquad$
Requested by: $\qquad$ Dept. $\qquad$ Date

Page no: $\qquad$ Item

Now reads: $\qquad$
$\qquad$
$\qquad$
$\qquad$
Change to/add: $\qquad$
$\qquad$
$\qquad$
$\qquad$
Reason for change: $\qquad$
$\qquad$
$\qquad$ $\square$

## Approval: (Initial in proper space)

Make change immediately
Make change at next rewrite
Reject
or


## ADVERTISING CORRECTION HISTORY NOTICE

Instrument: 106
Publication
Catalog 非25, page 206
(Specification change)

| Present Form: | Correct Form: |
| :---: | :---: |
| Under heading HI-AMPLITUDE OUTPUT, first sentence: |  |
| $\leq 12-\mathrm{ns} \text { risetime into }$ $50 \Omega .$ | S 12 -ns risetime into $50 \Omega$, $\leq 120$-ns unterminated. |
| Under TRIGGER OUTPUT, last sentence: |  |
| $\begin{aligned} & \leq 50 \text {-ns risetime into } \\ & 50 \Omega, \geqq 0.15 \mathrm{~V} \text { into } 50 \end{aligned}$ | $\leqslant 50$-ns risetime into $50 \Omega$, from 0 V to 0.1 |
| $\Omega, \underline{=} 300-\mathrm{ps}$ time jitter. | $\begin{aligned} & \mathrm{V} . \geq 0.1 \mathrm{~V} \text { amplitude } \\ & \text { into } 50 \Omega, \leq 300-\mathrm{ps} \\ & \text { time jitter. } \end{aligned}$ |

PROBLEM The $\mathrm{A}-150 \mathrm{~V}$ supply fails on what appears at first to be a random occurrence - the instrument operates satisfactorily for days or weeks and then experiences a rash of failures.

D224 and Q224 are destroyed when the REPETITION RANGE switch is moved slowly from one range to another. The detent spring on the switch is shorting the junction of R17, R24 to ground - a situation which is rather hard on V25 as well as the A-150 V supply.

SOLUTION Two solutions are possible depending on the circumstances:
The production solution is to increase the length of the aluminum spacers between the detent plate and the first wafer from 0.281 inches to 0.312 inches and reduce the length of the second pair of spacers from 2.062 inches to 2.0131 inches. The switch must be unwired, removed from the instrument, disassembled and new spacers inserted.

The field solution is to slip a \# 4 internal lock washer between the detent plate and the spacer.

Proceed as follows:

1) Remove the screws, knobs and panel nut from the switch;
2) Unsolder the white-blue and white-yellow wires from the rear wafer;
3) Remove the switch from the front panel and loosen the switch screws;
4) With a pair of diagonal cutters, cut out a portion of the lock washer to form a " C " ring configuration;
5) Slip the lock washers into place between the detent plate and the spacer and tighten the screws; (Do not make the screws too tight or the fiber washers will be broken.)
6) Readjust the RANGE MULTIPLIER pot so the pot shaft fits snugly against the connecting spring;
7) Reinstall the switch.

## MAINTENANCE NOTES

DECORATIVE INSERT REPAIR
Nick Stadtfeld, 8-29-67
Decorative inserts or strips are used to rubber contact cement. An equivalent cover certain screw and bolt heads on the adhesive, such as rubber cement, will do outside of many of our instruments. The the job when replacement is necessary.徘 strips are installed with 3M EC 847, a

## FACTORY TEST LIMITS

QUALIFICATION
Factory test limits are qualified by the conditions specified in the main body of the factory calibration procedure. Instruments may not meet factory test limits if calibration or checkout methods and test equipment differ substantially from those in the factory procedure.

These limits usually are tighter than advertised performance requirements, thus helping to insure the instrument will meet or be within advertised performance requirements after shipment and during subsequent recalibrations. Instruments that have left the factory may not meet factory test limits but should meet catalog or instruction manual performance requirements.

POWER SUPPLIES
AMPLITUDE range into $50 \Omega: 0.5 \mathrm{~V}$ P to P , max, to 12 V P to P , min
AMPLITUDE range unterminated: $7 \mathrm{~V} P$ to P , max, to 120 V P to P , min
12 V square-wave: $\pm 10 \%$ max, into $50 \Omega$
\# $\quad 100 \mathrm{~Hz}: 5 \%$ tilt, $\max$ $10 \mathrm{~Hz}: \quad 15 \%$ tilt, $\max$

Supply Tolerance $\quad \begin{array}{r}\text { max } \\ \text { freq ripe }\end{array}$
2V P to
-10
\# A -20V $\quad \pm 10 \% \quad 0.75 \mathrm{~V}$ P to
\# A $+150 \mathrm{~V} \quad \pm 10 \% \quad 0.75 \mathrm{~V}$ P to P
\# A -150V ${ }^{ \pm} 10 \% \quad 0.75 \mathrm{~V}$ P to P
\# A supply ---- 0.75 V P to P
SYMMETRY
Symmetry Range (R9): 50\% duty cycle at 10 kHz
Check SYMMETRY duty cycle: adjustable from 45 to $55 \%$
Rep rate change with SYMMETRY: $10 \%$, max

REP RATE MULTIPLIER CAL
Rep Rate Multiplier Cal X10 (R6):
$10 \mu \mathrm{~s} / \mathrm{cyc} 1 \mathrm{e}$
Rep Rate Multiplier Cal X1 (R30): $10 \mu \mathrm{~s} / \mathrm{cycle}$
Bias Level (R39): 50\% duty cycle
at 1 MHz and 10 kHz from 103.5
to 126.5 V AC (line).

REPETITION RATE RANGE AND
MULTIPLIER ACCURACY
$\pm 10 \%$, max
SYNC INPUT
Square-wave sync: 2 to 50 V
Sinewave sync: 5V P to P at
100 Hz and 1 MHz

## TRIGGER OUTPUT

\# Amplitude: 0.1V, min, into $50 \Omega$
非 Rate of rise into $50 \Omega$ : 50 ns , max, from 0 V to 0.1 V
Delay time: 50ns, max
HIGH AMPLITUDE NO LOAD RISETIME
\# 120 ns , max

## HIGH AMPLITUDE INTO 50

Risetime into 50 : 12 ns , max
Aberrations in first $100 \mathrm{~ns}: \pm 2 \%$, max
FAST RISE OUTPUT
FAST RISE + \& - AMPLITUDE
ccw: $50 \mathrm{mV}, \max$
cw: $\quad 500 \mathrm{mV}$, min
C127, C138
Risetime: lns, max, into $50 \Omega$
Aberrations: 2\%, max in first 5ns C107, C118

Risetime: 1ns, max, into $50 \Omega$
Aberrations: $2 \%$, max, in first 5ns Symmetry/amplitude change: 150ns, max

## TRIGGER JITTER

300ps, max $\cdot$


HORIZ. AMP 610-0247-00


VERT. AMP 610-0248-00

| Mod. |  |
| :--- | :--- |
| Date |  |
| Ket $^{2} *$ |  |

## 'A SUPPLY' RELIABILITY IMPROVEMENT

For Tektronix Type 106
SQUARE WAVE GENERATOR
Serial numbers 200-1354

## DESCRIPTION

The reliability and stability of the 'A Supply' is improved by replacing the series regulator transistor Q247, a 2 N3440 or a 2 N3739, with a 2 N4240 transistor, and making several other associated component changes.

(B)

Publication:
Instructions for 040-0476-00
November 1967
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## PARTS LIST

Quantity Part Number (1 ea) 1 ea 290-0075-00 1 ea 386-0252-00
lea 151-0251-00
1 ea 210-0202-00
2 ea 210-0457-00
2 ea 210-0802-00
2 ea 210-0811-00
2 ea 211-0510-00
1 ea 214-0210-00
2 ea 290-0159-00
1 ea 306-0270-00
1 ea 316-0470-00
lea 316-0472-00
1 ea 386-0143-00

## Descriprion

Assembly, capacitor, consisting of: Capacitor, $2 \times 10 \mu \mathrm{~F} 250 \mathrm{~V}$ Plate, capacitor mounting
Transistor, 2N4240
Lug, solder, SE6
Nut, Keps, $6-32 \times 1 / 4$
Washer, steel, $65 \times 5 / 16$
Washer, shouldered, \#6
Screw, 6-32 x 3/8 PHS
Spool, $w / 3 \mathrm{ft}$. silver-bearing solder
Capacitor, $\quad 2 \mu \mathrm{~F} \quad 150 \mathrm{~V}$
Resistor, comp, $27 \Omega \quad 2 \mathrm{~W} \quad 10 \%$
Resistor, comp, $47 \Omega \quad 1 / 4 \mathrm{~W} \quad 10 \%$
Resistor, comp, 4.7k 1/4W 10\%
Plate, mica insulator

IMPORTANT: When soldering to the ceramic strips, use the silver-bearing solder supplied with this kit.

## INSTRUCTIONS

STEP 1 APPLIES TO INSTRUMENTS SN 779-1354 AND TO INSTRUMENTS SN 200-778 THAT HAVE REPLACED Q247 PER PARTS REPLACEMENT KIT 050-0367-00
( ) 1. Replace Q247, a 2N3739 chassis-mounted transistor, with the 2N4240 transistor from the kit.

STEPS 2 THROUGH 5 APPLY TO INSTRUMENTS SN 200-778 ONLY
( ) 2. Remove the spacer rod above Q247.
( ) 3. Remove Q247, a 2N3440 chassis-mounted transistor, and discard the ${ }^{\#} 4$ mounting hardware.
( ) 4. Refer to Fig. 1 and drill a new $7 / 32 \mathrm{in}$. hole near Q234 and, using a rattail file, enlarge the rear mounting hole as shown.


FIG. 1

## INSTRUCTIONS (cont)

5. Mount the new Q247, 2N4240 transistor (from kit), using the \#6 hardware (from kit) as shown in Fig. 2, and wire as follows:
a) Install a bare wire from solder lug (collector of Q247) to CSC-12.
b) Install a bare wire from the emitter of Q247 to the ground lug near Q233.
c) Install a bare wire from the base of Q247 to CSC-10.

Re-install the spacer rod removed in step 2.


FIG. 2

| Item No. | Part Number | Description |
| :---: | :---: | :--- |
| 1 | $211-0510-00$ | Screw, 6-32 $\times 3 / 8$ |
| 2 | $152-0201-00$ | Transistor, 2 N3739 |
| 3 | $386-0143-00$ | Insulator, mica |
| 4 | $210-0811-00$ | Washer, fiber |
| 5 | $210-0802-00$ | Washer, steel |
| 6 | $210-0457-00$ | Nut, hex, 6-32 |
| 7 | $210-0202-00$ | Lug, solder, SE6 |

INSTRUCTIONS (cont)

STEP 6 APPLIES TO INSTRUMENTS SN 200-464 ONLY
( ) 6. Replace R237, a $22 \mathrm{k} \mathrm{l} / 4 \mathrm{~W} 10 \%$ resistor located as shown in Fig. 3, with a 4.7 k $1 / 4 \mathrm{~W} 10 \%$ resistor from the kit.

THE REMAINING STEPS APPLY TO ALL INSTRUMENTS
( ) 7. Replace R241, a $100 \Omega 1 / 4 \mathrm{~W} 10 \%$ resistor located as shown in Fig. 3, with a $47 \Omega$ 1/4W 10\% resistor from the kit.
( ) 8. Replace R242, a $150 \Omega 10 \mathrm{~W}$ wirewound resistor located as shown in Fig. 3, with a $27 \Omega 2 \mathrm{~W} 10 \%$ resistor from the kit.


FIG. 3

## INSTRUCTIONS (cont)

() 9. Replace C 56 , a $2 \times 40 \mu \mathrm{~F} 250 \mathrm{~V}$ chassis-mounted capacitor near V 94 , with a $2 \times 10 \mu \mathrm{~F}$ 250 V capacitor from the kit. See Fig. 4.
( ) 10. Install the series combination of C247-C248, two $2 \mu \mathrm{~F} 150 \mathrm{~V}$ capacitors, between R246, the AMPLITUDE potentiometer, and the ground lug on V94 tube socket. See Fig. 4.


FIG. 4

## THIS COMPLETES THE INSTALLATION.

() Check wiring for accuracy.
( ) Refer to your Instruction Manual and recalibrate as necessary.

JT:Is

## INSTRUOTION MANUAL

# 'A SUPPLY' RELIABILITY IMPROVEMENT 

$$
\begin{aligned}
& \text { TYPE } 106 \text { SQUARE WAVE GENERATOR -- SN 200-1354 } \\
& \text { Installed in Type } 106 \text { SN__D_ Date }
\end{aligned}
$$

This insert has been written to supplement the Instruction Manual for this instrument. The information given in this insert will supersede that given in the manual.

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## GENERAL INFORMATION

The reliability and stability of the 'A Supply' is improved by replacing the series regulator transistor Q247, a 2 N3440 or a 2 N3739, with a 2N4240 transistor, and making several other associated component changes.

## ELECTRICAL PARTS LIST

Ckt.No. Part Number
Description
CAPACITORS
C56
290-0075-00
290-0159-00 290-0159-00
C248

| $10 \mu \mathrm{~F}$ | 250 V |
| ---: | ---: |
| $2 \mu \mathrm{~F}$ | 150 V |
| $2 \mu \mathrm{~F}$ | 150 V |

RESISTORS

| R237 | $316-0472-00$ | 4.7 k | $1 / 4 \mathrm{~W}$ | $10 \%$ |  |
| :--- | ---: | :---: | :---: | :---: | :---: |
| R241 | $316-0470-00$ | $47 \Omega$ | $1 / 4 \mathrm{~W}$ | $10 \%$ |  |
| R242 | $306-0270-00$ | $27 \Omega$ | 2 W | $10 \%$ |  |
|  |  | TRANSISTORS |  |  |  |
|  |  |  |  |  |  |
| Q247 | $151-0251-00$ | Silicon | 2N4240 |  |  |

SCHEMATICS


## MODIEICATION KNTT

## OUTPUT PULSE WAVESHAPE IMPROVEMENTS

## For the Tektronix Type 106 SQUARE WAVE GENERATOR

Serial numbers 200-1479

## DESCRIPTION

This modification provides the following improvements:

1) Overshoot in the HIGH AMPLITUDE output is minimized by relocating R99 closer to the generator circuit and by changing the output to a $50 \Omega$ system.
2) Ripple in the FAST RISE output is eliminated by replacing Q217 and by making several component changes in the $+10 \mathrm{~V},-10 \mathrm{~V}$ power supply.
3) Aberrations in the HIGH AMPLITUDE output waveform are greatly reduced by the following changes:
a) the drive to the output amplifier is improved by rewiring the grid circuit of the output amplifier and by removing an unnecessary dropping resistor, R56.
b) the output amplifier screen resistor is removed and the screens are bussed together and by-passed to ground.
c) the drive to the grids is delayed from one tube to the next by adding inductors in series with the grid lines.

## Publication:

Instructions for 040-0479-00
March 1968
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## PARTS LIST

| Quantity | Part Number | Description |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 ea | 151-0190-00 | Transistor, 2N3904 |  |  |  |  |
| 1 ea | 151-0208-00 | Transistor, 2N4036 |  |  |  |  |
| 2 ea | 152-0185-00 | Diode, 6185 |  |  |  |  |
| 3 ea | 210-0201-00 | Lug, solder, SE-4 |  |  |  |  |
| 1 ea | 210-0203-00 | Lug, solder, SE-6 |  |  |  |  |
| 1 ea | 210-0457-00 | Nut, Keps, 6-32 $\times 5 / 16$ |  |  |  |  |
| 1 ea | 211-0514-00 | Screw, 6-32 $\times 5 / 16$ |  |  |  |  |
| 1 ea | 214-0210-00 | Spool, w/3 ft. silver-bearing solder |  |  |  |  |
| 6 ea | 276-0507-00 | Ferrite bead |  |  |  |  |
| 1 ea | 281-0525-00 | Capacitor, cer, | 470 pF | 500 V |  |  |
| 2 ea | 283-0008-00 | Capacitor, cer, | $0.1 \mu \mathrm{~F}$ | 500 V |  |  |
| 1 ea | 283-0059-00 | Capacitor, cer, | $1 \mu \mathrm{~F}$ | 25 V |  |  |
| 2 ea | 290-0137-00 | Capacitor, EMT, | $100 \mu \mathrm{~F}$ | 30 V |  |  |
| 1 ea | 301-0131-00 | Resistor, comp, | $130 \Omega$ | 1/2W | 5\% |  |
| 1 ea | 301-0473-00 | Resistor, comp, | 47 k | 1/2W | 5\% |  |
| 1 ea | 301-0562-00 | Resistor, comp, | 5.6k | 1/2W | 5\% |  |
| 1 ea | 304-0100-00 | Resistor, comp, | $10 \Omega$ | 1 W | 10\% |  |
| 1 ea | 343-0015-00 | Clamp, 1/2" ID |  |  |  |  |
| 1 ea | 385-0079-00 | Rod, alum, hex, | /4 $\times 3 / 8$ |  |  |  |
| 1 ea |  | Tubing, thermo-fi |  | 0531-00, | black, | 1/2" |
| 1 ea |  | Cable, coax, $50 \Omega$ |  | -0284-00, |  | 3-3/4" |
| 1 ea |  | Cable, coax, $50 \Omega$ |  | 0284-00, |  | $4 "$ |
| 1 ea |  | Wire, \#14 solid, |  | 0119-00, | bare, | $2{ }^{\prime \prime}$ |

IMPORTANT: When soldering to the ceramic strips, use the silver-bearing solder supplied with this kit.

## INSTRUCTIONS

A. TO REWIRE HIGH AMPLITUDE OUTPUT CONNECTOR AND FAST RISE SWITCH:

SW 200-345 ONLY -- See Fig. $1 \quad \oplus$ Indicates parts from the kit
( ) 1. Unsolder the brass strip (tinned) and R99, a $600 \Omega 14 \mathrm{~W}$ resistor from the HIGH AMPLITUDE OUTPUT connector. Unsolder the grounded end of R99 and remove.
( ) 2. Unsolder two brass strips from the HIGH AMPLITUDE - FAST RISE switch SW242A. (Discard the short piece.)
( ) 3. Cut off the brass strip on the forward side of R93 and discard.
( ) $\oplus$ 4. Replace the ${ }^{\#} 4$ internal lockwasher on the outboard mounting screw of V64, V84, and V94, with a ${ }^{\#} 4$ solder lug.
( ) 5. Drill a 5/32" hole near V64. Note: Hole location is not critical. Locate the hole to provide good lead dress of R99.
( ) $\oplus$ 6. Mount R99 (removed in A-1) with a 1/2" clamp on the top of the hex rod, using the $6-32 \times 3 / 4$ screw. Install the ${ }^{\#} 6$ solder lug between the rod and the chassis. Connect the end of R99 with short lead to the solder lug and the other end to the brass strip near R63.
( ) $\oplus$ 7. Solder the center conductor of the 4 " coax cable (from kit) to the center terminal of SW242A.
( ) Solder the center conductor of the 3-3/4" coax cable to the outside terminal of SW242A. Solder the other end of the 3-3/4" coax, center conductor to the center terminal of the OUTPUT connector, and the shield to the shell of the OUTPUT connector.
(.) Solder the center conductor of the 4" coax to the output plate line near V94 and solder its shield to the outboard solder lug on V94 socket.


FIG. 1

INSTRUCTIONS (cont)
B. TO REWIRE OUTPUT AMPLIFIER: SN 200-626 -- See Fig. 2
( ) $\oplus$ 1. Replace R56, a $10 \Omega 1 \mathrm{~W} 10 \%$ resistor connected between the negative terminal of C 56 and pin 3 of V94, with a length of ${ }^{\#} 14$ bare wire from the kit.
( ) $\oplus$ 2. Replace C95, a 200 pF capacitor located between pin 3 of V84 and solder lug, with a $0.1 \mu \mathrm{~F}$ capacitor, and relocate to connect it between pin 3 of V 64 and solder lug near V64.
( ) $\oplus$ 3. Replace C94, a 1000 pF 500V capacitor located between pin 3 of V64 and CSA -6 , with a $1 \mu \mathrm{~F} 25 \mathrm{~V}$ capacitor, and relocate to connect it between pin 3 of V64 and CSA-1.
( ) $\oplus$ 4. Install C43, a $0.1 \mu \mathrm{~F} 500 \mathrm{~V}$ capacitor, between the negative terminal of C56 and CSD-1.
( ) $\oplus$ 5. Connect pin 6 of $V 64-V 74,-V 84$ and $V 94$ together with a 3-1/2" length of \# 16 bare wire.
( ) 6. Remove R55, a $270 \Omega 1 \mathrm{~W}$ resistor, located between pin 3 of V64 and CSA-2.
( ) $\oplus$ 7. Temporarily unsolder R91, R81 and R71 from the output tubes grid line. Install L64, L65, two ferrite beads on the grid line between R61 and R71, resolder R71 to grid line.
()$\oplus \quad$ In a like manner install L74 and L75 between R71 and R81, and L84 and L85 between R81 and R91.
( ) 8. Install R55, a $270 \Omega$ resistor removed in step $B-6$, between the negative terminal of C56 and the junction of R91 and the output tubes grid line.
( ) $\oplus$ 9. Install C92, a 470 pF 500 V capacitor, between pin 6 of V84 and ground lug near V84.
( ) $\oplus$ 10. Replace Q34, a 151-0108-00 type transistor, with a $2 N 3904$, PN 151-0190-00 type transistor.
C. TO MODIFY +10V AND -10V SUPPLY: SN 200-679 ONLY -- See Fig. 3
( ) $\oplus$ 1. Replace R217, a $27 \Omega$ IW $10 \%$ resistor located between CSE-3 and CSF-3, with a $10 \Omega 1 \mathrm{~W} 10 \%$ resistor.
( ) $\oplus$ 2. Replace Q217, a 2N2905 type transistor with a 2 N 4036.
( ) $\oplus$ 3. Install a bare wire from CSE-2 to the ground lug next to CSE.
( ) $\oplus$ 4. Install C213, a $100 \mu \mathrm{~F} 30 \mathrm{~V}$ capacitor, -end to CSE-2 and tend to CSF-1.
( ) $\oplus$ 5. Install a ${ }^{\#} 22$ white wire from terminal 15 of T201 to the ground lug near Q233, if not present.
() $\oplus$ 6. * Install C217, a $100 \mu \mathrm{~F} 30 \mathrm{~V}$ capacitor tend to CSE-6 and - end to CSF-5.

* SN 200-345 ONLY

```
INSTRUCTIONS (cont)
```



FIG. 2


FIG. 3

## INSTRUCTIONS (cont)

D. TO REWIRE TRIGGER CIRCUIT: See Figs. 2 and 4
( ) Temporarily remove C262 to gain access to components on ceramic strips.
Steps 1 through 5 apply to SN 200-1479
( ) 1. Remove D33, a germanium diode, located between CSC-6 and CSD-6, above Q34.
( ) 2. Relocate a bare wire from CSD-6 to CSD-3. Other end is connected to base of Q34.
( ) $\oplus$ 3. Install D33, a 6185 type diode, between CSC-6 and CSD-6. Install with cathode, banded end, to CSC-6.
( ) $\oplus$ 4. Install R34, a $130 \Omega$ 1/2W 5\% resistor, between CSD-3 and CSC-5.
() $\oplus$ 5. Install D32, a 6185 type diode, between CSD-3 and CSD-6. Install with cathode to CSD-3.

Steps 6 and 7 apply to SN 200-626 ONLY
( ) $\oplus$ 6. Replace R 35 , a $3.9 \mathrm{k} 1 / 4 \mathrm{~W} 5 \%$ resistor located between CSB-5 and CSC-5, with a $5.6 \mathrm{k} \mathrm{l} / 2 \mathrm{~W}$ resistor.
( ) $\oplus$ 7. Replace R36, an $82 \mathrm{k} \mathrm{1/4W} 5 \%$ resistor located between CSB-6 and CSC-7; with a 47 k l/2W resistor.
( ) 8. Reinstall C262.


FIG. 4

## THIS COMPLETES THE INSTALLATION.

( ) Check wiring for accuracy.
( ) Refer to your Instruction Manual and recalibrate as necessary.

JT:Is

## INSTRUCTION MANUAL

# OUTPUT PULSE WAVESHAPE IMPRROVEMENTS 

TYPE 106 - SN 200-1479<br>Installed in Type 106 SN<br>$\qquad$ Date<br>$\qquad$

This insert has been written to supplement the Instruction Manual for this instrument. The information given in this insert will supersede that given in the manual.

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## GENERAL INFORMATION

This modification provides the following improvements:

1) Overshoot in the HIGH AMPLITUDE output is minimized by relocating R99 coloser to the generator circuit and by changing the output to a $50 \Omega$ system.
2) Ripple in the FAST RISE output is eliminated by replacing Q217 and by making several component changes in the $+10 \mathrm{~V},-10 \mathrm{~V}$ power supply.
3) Aberrations in the HIGH AMPLITUDE output waveform are greatly reduced by the following changes:
a) the drive to the output amplifier is improved by rewiring the grid circuit of the output amplifier and by removing an unnecessary dropping resistor, R56.
b) the output amplifier screen resistor is removed and the screens are bussed together and by-passed to ground.
c) the drive to the grids is delayed from one tube to the next by adding inductors in series with the grid line.

| Ckt. No. | Part Number | Description |  |
| :---: | :---: | :---: | :---: |
|  |  | CAPACITORS |  |
| C43 | 283-0008-00 | $0.1 \mu \mathrm{~F}$ | 500 V |
| C92 | 281-0525-00 | 470 pF | 500 V |
| C94 | 283-0059-00 | $1 \mu \mathrm{~F}$ | 25 V |
| C95 | 283-0008-00 | $0.1 \mu \mathrm{~F}$ | 500 V |
| C213 | 290-0137-00 | $100 \mu \mathrm{~F}$ | 30 V |
| C217 | 290-0137-00 | $100 \mu \mathrm{~F}$ | 30 V |
|  |  | DIODES |  |
| D32 | 152-0185-00 | 6185 |  |
| D33 | 152-0185-00 | 6185 |  |

INDUCTORS
Ferrite bead
Ferrite bead
Ferrite bead
Ferrite bead
Ferrite bead Ferrite bead

## TRANSISTORS

2N3904
2N4036

## RESISTORS

R15
R34
R35
R36
R217
Q34
Q217
151-0190-00 151-0208-00

> Delete
> $301-0131-00$
> $301-0562-00$
> $301-0473-00$
> $304-0100-00$

| $130 \Omega$ | $1 / 2 W$ | $5 \%$ |
| ---: | ---: | ---: |
| $5.6 k$ | $1 / 2 W$ | $5 \%$ |
| $47 k$ | $1 / 2 W$ | $5 \%$ |
| $10 \Omega$ | $1 W$ | $10 \%$ |

## MECHANICAL PARTS LIST

Clamp, 1/2" ID
Lug, solder, SE-4
Lug, solder, SE-6
Nut, Keps, $6-32 \times 5 / 16$
Rod, alum, hex, $1 / 4 \times 3 / 8$
Screw, 6-32 $\times 5 / 16$

## SCHEMATICS



## PARTS REPLACEMENT KOT

## POWER SUPPLY TRANSISTOR, Q247

For Tektronix Type 106 Square-Wave Generator
Serial numbers 200-778

DESCRIPTION
Power supply transistor 2N3739 $451-2201-00$ used for Q247, replaces 2N3440 (151-0126-00), offering greater reliabili

To install the new yopercnsistor it is necessargy to drill a new hale inthe chossis and enlange an existing hole.

NOTE: In theserial mumber of yone instrument is above those lisind, of if the mod has been installed, disregard the instructions as PN 151-0201-00 is d d/rect replacement.

Publication:
Instructions for 050-0367-00
March 1967
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## PARTS LIST

Quantity
Part Number

| 1 ea | $151-0201-00$ |
| :--- | :--- |
| 1 ea | $210-0202-00$ |
| 2 ea | $210-0457-00$ |
| 2 ea | $210-0802-00$ |
| 2 ea | $210-0811-00$ |
| 2 ea | $211-0510-00$ |
| 1 ea | $214-0210-00$ |
| 1 ea | $386-0143-00$ |

Description
Transistor, silicon, 2N3739, NPN
Lug, solder, SE6
Nut, Keps, 6-32 $\times 1 / 4$
Washer, steel, $6 \mathrm{~S} \times 5 / 16$
Washer, shoulder, \#6
Screw, 6-32 $\times 3 / 8$ PHS
Spool, $w / 3 \mathrm{ft}$. silver-bearing solder
Plate, mica insulator

## INSTRUCTIONS

IMPORTANT: When soldering to the cepquic strips bise the silver-bearing solder supplied with thetsit
( ) 1. Remove instrument from cokhot and removerpacer above Q247.
( ) 2. Remove Q247, a 2N3440 chessis-mounyed transfifor and discard the \#4 mounting hardware.
( ) 3. Refer to Fig. land driv \& nem $7 / 32$ in. hole near Q234 and, using a rattail file, enlarge the reanmountins ho as shogen.
( ) 4. Mount thenew 224 a 2N3739 is transistor (from kit), using the \#6 hardware (from रi it) asmen in Flg. 2 , ast wire as follows:
( ) a) instaN a bare y ire fromsolder lug (collector of Q247) to CSC-12.
( ) b4 nosick a pare wire form the emitter of Q247 to the ground lug near Q233.
( ) CX hastil a bare wiz from the base of Q247 to CSC-10.
( ) 5. Re-instarl the spacer rod removed in step l.
THIS COMPLETES THE INSTALLATION.
( ) Check wiring for accuracy.
( ) Refer to your Instruction Manual and recalibrate as necessary.

JT:Is


| Item No. | Part Number | Description |
| :---: | :---: | :--- |
| 1 | $211-0510-00$ | Screw, 6-32 $\times 3 / 8$ |
| 2 | $152-0201-00$ | Transistor, 2 N 3739 |
| 3 | $386-0143-00$ | Insulator, mica |
| 4 | $210-0811-00$ | Washer, fiber |
| 5 | $210-0802-00$ | Washer, steel |
| 6 | $210-0457-00$ | Nut, hex, 6-32 |
| 7 | $210-0202-00$ | Lug, solder, SE6 |

## MODIFICATION SUMMARY


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## INDEX

## MODIFICATION SUMMARY

| GENERATOR |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Mod No. | Description | Kit/MI No. | Eff SN | Page |
| M11324-1 | SW242 Rewired to Reduce Aberrations | Info Only | 346 | 4 |
| M11537-1 | Adds Protective Diode to Q54 |  | 610 | 6 |
| M11537-2 | D114, D134 Changed to Faster Diodes |  | 610 | 7 |
| M11790 | Improve Waveform at Low Amplitudes | . | 627 | 8 |
| M11927 | D4 Changed to Improve Temp \& Freq Stability |  | 698 | 14 |
| M12309 | Q134 Changed to Improve Risetime |  | 930 | 17 |
| M12606-1 | Q103, Q114 Replaced to Reduce Failures | Info Only | 1190 | 19 |
| M12606-2 | + \& - Transistion Amp Pot Changed | MI - 12606-2 | 1190 | 19 |
| M13083 | R116-136 Change Allows Tolerance Change in R115-135 | Info Only | 1450 | 26 |
| M13187 | Modified to Improve Output and Symmetry | MI - 13187 | 1480 | 28 |
| M13204 | C247 \& C248 Replaced by C249 | Info Only | 1550 | 30 |
| M13393 | Adds Bleeder Resistor to Timing Capacitors | Info Only | 1590 | 3. |
|  | - |  |  |  |
| POWER SUPPLY |  |  |  |  |
| M11032 | Wire Color Changed on -20 V | Info Only | 320 | 3 |
| M11324-2 | Reduce Ripple in +10 V | Info Only | 346 | 4 |
| M11271 | Prevent Q43 From Oscillating |  | 430 | 4.1 |
| M11190 | Layout Changed to Prevent Shorts | Info Only | 440 | 5 |
| M11468 | R237Changed to Prevent Runaway of 'A' Supply |  | 465 | 5 |
| M11316 | Q257 Mount Changed to Prevent Shorts |  | 510 | 6 |
| M11451 | Improve +10 V Regulation |  | 680 | 12 |
| M12074 | Q247 Changed to Improve Reliability | 040-0476-00 | 778 | 15 |
| M13127 | Q247 Replaced With a 2 N 4240 | 040-0476-00 | 1355 | 24 |
| M13204 | C247 \& C248 Replaced by C249 | Info Only | 1550 | 30 |
| M13660 | Line Selector Switch Changed to Meet Safety Standards | Info Only | 1620 | 31 |

## MODIFICATION SUMMARY

| MISCELLANEOUS |  |  |  |  |
| :--- | :--- | ---: | ---: | ---: |
| Mod No. | Description | Kit/MI No. | Eff SN | Page |
| M9271 | Motor Base Assembly Improved | Info Only | 802 | 17 |
| M11191 | Zener Diodes Replaced with $5 \%$ Type | Info Only | none | 3 |
| M11292 | Improves Power Cord Ground | $040-0424-01$ | 970 | 18 |
| M11678 | Mod 146B Made Production Special | Info Only | 1500 | 29 |
| M12031 | Power Light Changed | Info Only | 1170 | 18 |
| M12174 | Add Plastic Shield to Motor Base |  | 1290 | 22 |

Effective Prod SN 320
FRONT PANEL SYMPTOM: None.
PROBLEM: Change Notice 11012, which was a complete rework, changed the voltage of the -15 V supply to -20 V , to eliminate component selection. Changing the -15 V supply to -20 V caused the wire color-code to be incorrect.

PRODUCTION CHANGE: The wire color-code for the -20 V supply was changed from tan-brown-red-black to tan-red-black-black. There was no part number changes of the reworked cables.
$10 \%$ AND $20 \%$ ZENER DIODES
CHANGED TO STANDARD 5\% UNITS
INFORMATION ONLY
M11191
Effective Prod SN None
NOTE: All diodes in any one instrument will not necessarily change at the same time. The effective SN furnished will be when the final diode in the particular instrument is changed.

FRONT PANEL SYMPTOM: None.
PROBLEM: Zener diode values are at present widely scattered in both voltage and tolerance. The proposed modifications will standardize all 400 mW 1 W 1.5 W and 10 W Zeners, now listed as 10 and $20 \%$ to $5 \%$ tolerance, and change the majority of non-standard parts to standard JEDEC units. One of these changes is to minimize the number of active part numbers. There will be no increase in cost for the $5 \%$ Zeners.

PRODUCTION CHANGE: Voltage tolerance for $10 \%$ and $20 \%$ Zener diodes was changed to $5 \%$ for all uses. At the same time, all 250 mW Zener diodes were changed to 400 mW . Refer to parts removed and added list for details.

Parts Removed:

| D264 | Diode, 1N3027A $20 \mathrm{~V} \pm 10 \%$ | $152-0060-00$ |
| :--- | :--- | :--- |
| D124, D104 | Diode, 1N4372 | $3 \mathrm{~V} \pm 10 \%$ |

Parts Added:
D264
Diode, 1N3027B $20 \mathrm{~V} \pm 5 \%$
152-0291-00
D124, D104
Diode, $1 \mathrm{~N} 4372 \mathrm{~A} 3 \mathrm{~V} \pm 5 \%$
152-0278-00

HI AMP - FAST RISE SELECTOR SWITCH REWIRED TO REDUCE ABERRATIONS

Effective Prod SN 346 $\begin{array}{lllllll}\text { modified out of sequence: } & 200-1 & 221 & 238-9 & 264 & 305 & 323-33 \\ & 210-13 & 228 & 243 & 292 & 314 & 335-42 \\ & 219 & 234-6 & 262 & 300 & 320-1 & 344\end{array}$

FRONT PANEL SYMPTOM: None.
PROBLEM: Inductance in the switch, connected in series with the High Amplitude output was causing excessive overshoot. The amplitude of the overshoot ranged from $2.1 \%$ to $3.8 \%$. See M11451 and M11790.

PRODUCTION CHANGE: The wiring to the HIGH AMPLITUDE output connector from the output amplifier via the HIGH AMPLITUDE - FAST RISE switch was changed from $1 / 4 \mathrm{in}$. brass strap to two pieces of $50 \Omega$ coax. R99 was relocated physically closer to the generator to minimize overshoot in the output wave form. The switch still represents a discontinuity.

Parts Removed:
R99

$$
\begin{array}{ll}
\text { Resistor, fixed, WW, } 600 \Omega 14 \mathrm{~W} & 308-0392-00 \\
\text { Strip, brass } 12 \times 0.250 & 124-0179-00
\end{array}
$$

Parts Added:
R99

$$
\begin{array}{ll}
\text { Resistor, fixed, WW, } 600 \Omega 1 / 4 \mathrm{~W} & 308-0392-00 \\
\text { Lug, solder, SE-6 } & 210-0203-00 \\
\text { Clamp, CL16 ss } 1 / 2 \text { "ID } & 343-0015-00 \\
\text { Rod, alum, hex, } 1 / 4 \times 3 / 8 & 385-0079-00 \\
\text { Strip, brass, } 3-3 / 4 \times 0.250 & 124-0179-01 \\
\text { Cable, coax, } 50 \Omega, \text { consisting of: } & 175-0284-00
\end{array}
$$

## +10 V POWER SUPPLY MODIFIED TO

MINIMIZE RIPPLE IN FAST RISE OUTPUT
INFORMATION ONLY
M11324-2
Effective Prod SN 346
modified out of sequence: See M11324-1
FRONT PANEL SYMPTOM: Ripple on FAST RISE OUTPUT.
PROBLEM: Ripple is present in the FAST RISE OUTPUT, especially at low line, which is a direct result of ripple out of the 10 V supply.

PRODUCTION CHANGE: A wire connecting terminal 15 of T201 (center tap of the 10 V Power Supply winding) to ground near Q233 was removed.
At the same time C217, a $100 \mu \mathrm{~F} 30 \mathrm{~V}$ capacitor, was added from the junction of R216-R217-R218 (in the 10V Power Supply) to ground.
This mod is superseded by M11451. The wire from terminal 15 of T 201 should be left in place.

Parts Removed: None
Parts Added:
C217
Capacitor, EMT, $100 \mu \mathrm{~F} 30 \mathrm{~V}$
290-0137-00

Usable in field instruments SN 200-429

FRONT PANEL SYMPTOM: An oscillation occurs at rep rates less than 500 k Hz on the ground side of the square wave. The frequency of oscillation is approximately 200 kHz . See below.

BEFORE


## AF TER



PROBLEM: Insufficient isolation of emitter follower Q43 from the power supply causes it to oscillate.

PRODUCTION CHANGE: A $100 \Omega$ resistor was added in series with the collector of Q43. Parts Added:

R42
Resistor, comp, $100 \Omega 1 / 4 \mathrm{~W} 10 \%$


Effective Prod SN 440
FRONT PANEL SYMPTOM: None.
PROBLEM: Present location of parts, in the $-20 \mathrm{~V} \&+150 \mathrm{~V}$ power supply, could cause the two supplies to become shorted to each other.

PRODUCTION CHANGE: R226, a 40 k 8 W resistor, and associated wiring were relocated.
At the same time, the bare wire that connected C212 to the ceramic strips were changed to insulated stranded wire to improve access to parts on the same chassis.
'A' SUPPLY SERIES REGULATOR RESISTOR CHANGED TO PERMIT OPERATION AT HIGHER TEMPERATURES

Effective Prod SN 465

| w/exceptions | $200-1$ | $234-6$ | 300 | 341 | 408 | 438 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | $210-3$ | $238-9$ | 305 | 346 | 413 | $447-8$ |
|  | 219 | 243 | 324 | 357 | 426 | $453-5$ |
|  | 221 | 264 | 329 | 390 | 428 | 457 |
|  | 228 | 292 | 339 | $403-5$ | $433-5$ | $459-60$ |
|  |  |  |  |  |  | Also 364 |

FRONT PANEL SYMPTOM: None.

See SQB
M11468

Usable in field instruments SN 200-464
$305 \quad 346 \quad 413 \quad 447-8$
$324 \quad 357 \quad 426 \quad 453-5$
$\begin{array}{llll}329 & 390 & 428 & 457\end{array}$
403-5 433-5
Also 364

PROBLEM: Series regulator in 'A' supply goes into Thermal runaway at high temperatures.
PRODUCTION CHANGE: R237 was reduced in value from 22 k to 4.7 k .
Parts Removed:
R237 22k 1/4 W 10\% resistor 316-0223-00
Parts Added:
R237 $4.7 \mathrm{k} \mathrm{1/4} \mathrm{~W} \mathrm{10} \mathrm{\%} \mathrm{resistor} \mathrm{316-0472-00}$
INSTALLATION INSTRUCTIONS:
Parts Required: See 'Parts Added'.
Installation Procedure:
Replace R 237, a $22 \mathrm{k} 1 / 4 \mathrm{~W} 10 \%$ resistor, connected between the emitter of Q233 and a ceramic strip notch (CSC-3), with a $4.7 \mathrm{k} 1 / 4 \mathrm{~W} 10 \%$ resistor.

FRONT PANEL SYMPTOM: None.
PROBLEM: Q257, the Constant Voltage Source transistor in the A +150V supply was shorting to the chassis via the metal anodized washers.
PRODUCTION CHANGE: Mounting hardware for Q257 was changed from two anodized washers to two shouldered fiber washers.

Parts Removed:
(2) Washer, shouldered, anodized alum, w/\#6 hole 210-0983-00

Parts Added
(2) Washer, shouldered, fiber \#6 210-0811-00

INSTALLATION INSTRUCTIONS
Parts Required: See 'Parts Added'.
Installation Procedure: Replace the anodized aluminum washers, used to mount Q257, with \#6 shouldered fiber washers.

DIODE (D54) CHANGED TO A DIODE
WITH HIGHER PIV RATING
Effective Prod SN 610 (Tent)

See SQB
M11537-1

Usable in field instruments SN 200-609 (Tent)

FRONT PANEL SYMPTOM: With REPETITION RATE set to about 500 kHz and AMPLITUDE at maximum, the waveform shown below may appear.

BEFORE


AF TER


PROBLEM: Test was selecting D54 for high PI V. At maximum AMPLITUDE settings, D54 was being subjected to voltages that caused it to start breaking down in the reverse direction.

PRODUCTION CHANGE: D54 was changed from 152-0071-00 to 152-0079-00 which has a higher P I V rating.
continued

Parts Removed:
D54
Germanium diode
152-0071-00
Parts Added:
D54
Germanium diode
152-0079-00
INSTALLATION INSTRUCTIONS:
Parts Required: See 'Parts Added'。
Installation Procedure:
Replace D54, a germanium diode, located bet ween CSA-2 and CSB-2 with an HD1841 type diode. Install with the cathode (banded end) to CSA-2.


FAST RISE + AND - OUTPUT CLAMP DIODES REPLACED WITH FASTER

See SQB

Effective Prod SN 610 (Tent)
Usable in field instruments SN 200-609 (Tent)
FR ONT PANEL SYMPTOM: SYMMETRY changed more than the allowed 150 ns when switching between HI AMPLITUDE AND FAST RISE.

PROBLEM: Storage time in diodes D114-D134 was excessive and diodes tended to have too much leakage.

PRODUCTION CHANGE: Type of diode for D114 and D134 was changed from an ED-2007 type diode to an HD1841 type diode.

Parts Removed:
D114, D134 Germanium diode 152-0071-00

Parts Added:
D114, D134 Germanium diode
152-0079-00

INSTALLATION INSTRUCTIONS:
Parts Required: See 'Parts Added'.
Installation Procedure:
a) Replace D114, a germanium diode, located on the +FAST RISE OUTPUT board next to D117 and D118 with an HD1841 type diode. Install with cathode (banded end) to ground.
b) Replace D134, a germanium diode, located on the -FAST RISE OUTPUT board next to D137 and D138, with an HD1841 type diode. Install with cathode (banded end) to the junction of D137, R134 and the collector of Q134.

OUTPUT AMPLIFIER CIRCUIT

MODIFIED TO IMPROVE WAVEFORM AT LOW AMPLITUDES

Eff ective Prod SN 627

| w/exception | $200-1$ | 341 | 435 |
| :--- | :--- | :--- | :--- |
|  | $212-3$ | 346 | 532 |
| 219 | 357 | 534 |  |
|  | 234 | 390 | 537 |
|  | 243 | $404-5$ | 539 |
|  | 339 | 426 | 541 |

See SQB
M1 1790

Usable in field instruments SN 202-626 **

| $544-5$ | $567-82$ | $599-604$ |
| :--- | :--- | :--- |
| 547 | $584-5$ | 606 |
| 549 | 589 | $609-11$ |
| $551-2$ | 592 | $615-25$ |
| $554-9$ | 594 | Also 364 |
| $561-4$ | $596-7$ |  |

FRONT PANEL SYMPTOM: None.
PROBLEM: Cathode moving, screen feed-thru, drive voltage not clean, resulting in high amplitude aberrations, in the output waveform, when the AMPLITUDE control is in fully counter-clockwise position.

PRODUCTION CHANGE: The drive voltage was cleaned up. The cathode resistor removed and the screens bussed together and by-passed to ground. Also the drive of the grids is being delayed from one tube to another.
** Mod 11451 should be installed when installing M11790.
Parts Removed:

| Q34 | Transistor | 151-0108-00 |
| :---: | :---: | :---: |
|  | Cable, coax $50 \Omega \mathrm{imp}$ (5-1/2 long) . $4.58^{\circ}$ | 175-0248-00 |
| C94 | Capacitor 1000 pF 500 V | 281-0536-00 |
| C95 | Capacitor 200 pF 500 V | 281-0605-00 |
| R56 | Resistor, 10 Q 1 W 10\% | 304-0100-00 |
| R35 | Resistor, $3.9 \mathrm{k} \mathrm{1/4} \mathrm{~W} \mathrm{5} \mathrm{\%}$ | 315-0392-00 |
| R36 | Resistor, $82 \mathrm{k} 1 / 4 \mathrm{~W} 5 \%$ | 315-0823-00 |
| Parts Added: | Lockwasher, int \#4 (2) | 210-0004-00 |
| Q34 | * Transistor, 2N3904 | 151-0190-00 |
| $\begin{aligned} & \text { L64, L65, L74, } \\ & \text { L75, L84, L85 } \end{aligned}$ | * Ferrite beads | 276-0507-00 |
| C92 | * Capacitor, 470 pF 500 V | 281-0525-00 |
| C43, C95 | * Capacitor, $0.1 \mu \mathrm{~F} 500 \mathrm{~V}$ | 283-0008-00 |
| C94 | * Capacitor, $1 \mu \mathrm{~F} 25 \mathrm{~V}$ | 283-0059-00 |
| R36 | * Resistor, $47 \mathrm{k} 1 / 2 \mathrm{~W} 5 \%$ | 301-0473-00 |
| R35 | *Resistor, 5.6k 1/2 W 5\% | 301-0562-00 |
|  | * Lug, solder, SE-4 | 210-0201-00 |
|  | Cable, coax, $50 \Omega \mathrm{imp}$ ( 4 in .1 long ) . 333 ft . | 175-0248-00 |

## INSTA LLATION INSTRUCTIONS:

Parts Required: See 'Parts Added' with asterisks. For instruments SN 202-345, see 'Parts Added' with asterisks and parts listed below:
C217
Capacitor, EMT, $100 \mu \mathrm{~F} 30 \mathrm{~V}$
290-0137-00
Lug, solder, SE-6
210-0203-00
Nut, Keps, 6-32 x 5/16
210-0457-00
Screw, 6-32 x 5/16
211-0514-00
Rod, aluminum, hex, $1 / 4 \times 3 / 8$ 385-0079-00
Clamp, $1 / 2$ in. ID
343-0015-00
Cable, coax, 3-3/4 in.
175-0284-00
Cable, coax, 4 in.
175-0284-00
continued

continued

## Installation Procedure:

## PART I -- FOR SN 202-345 ONLY

a) Unsolder the brass strip (tinned) and R99, a $600 \Omega 14 \mathrm{~W}$ resistor from the High Amplitude output connector. Unsolder the grounded end of R99 and remove.
b) Unsolder two brass strips from the HIGH AMPLITUDE-FAST RISE switch SW242A. (Discard the short piece.)
c) Cut off the brass strip on the forward side of R93 and discard.
d) Replace the \#4 int lockwasher on the outboard mounting screw of V84, with a \#4 solder
e) Drill a $5 / 32 \mathrm{in}$. hole near V64, as shown on ceramic strip layout drawing (Fig. 1). Note: Hole location is not critical. Locate the hole to provide good lead dress of R99.
f) Mount R99, with the $1 / 2 \mathrm{in}$. clamp on top of the hex rod, with the $6-32 \times 3 / 4$ screw. Install the \#6 solder lug between the rod and chassis. Connect one end of R99 to solder lug and the other end to the brass strip near R63.
g) Make up coax leads with ground leads on each end to $/ 58 \mathrm{in}$. See Fig. 2 .

Join the shields (on one end) of the two coaxes, solder and cover with shrink-on tubing. Solder the center conductor of the 4 in . cable to the center of SW242A. (The other end will be soldered later.)
Solder the center conductor of the 3-3/4 in. cable to the outside terminal of SW242A, other end, center conductor to output connector and ground to solder lug on trigger output connector. Note: It may be necessary to add a solder lug to the trigger output connector.
h) On Power Supply Chassis: Install a bare wire from CSE-6 to ground lug. Install C217, a $100 \mu \mathrm{~F} 30 \mathrm{~V}$ capacitor ( + ) end to CSE-6 and (-) end to CSF-5.


FIG. 1


FIG. 2
continued


FIG. 3
continued

## PART II -- ALL INSTRUMENTS (SN 202-626)

a) Replace the \#4 lockwashers on the outboard tube socket mounting screws of V64 and V94, with \#4 solder lugs.
b) Unsolder the coax, if present, (center conductor) from the plate buss of V64-V94, and the shield from solder lug near V94.
c) Replace R56, a $10 \Omega 1 \mathrm{~W} 10 \%$ resistor, connected between C56 (-term) and pin 3 of V94 with a length of \#14 bare wire.
d) Replace C95, a 200 pF capacitor, located between pin 3 of V84 and solder lug, with a $0.1 \mu \mathrm{~F}$ capacitor, and relocate to connect between pin 3 of V64 and solder lug near V64.
e) Replace R35, a $3.9 \mathrm{k} 1 / 4 \mathrm{~W} 5 \%$ resistor, located between CSB-5 and CSC-5, with a $5.6 \mathrm{k} 1 / 2 \mathrm{~W}$ resistor.
f) Replace R36, a $82 \mathrm{k} \mathrm{1/4W} 5 \%$ resistor, located between CSB-6, and CSC-7, with a $47 \mathrm{k} 1 / 2 \mathrm{~W}$ resistor.
g) Replace C94, a 1000 pF 500 V capacitor, located between pin 3 of V64 and CSA-6, with a $1 \mu \mathrm{~F} 25 \mathrm{~V}$ capacitor, and relocate to connect between pin 3 of V64 and CSA-1.
h) Install C43, a $0.1 \mu \mathrm{~F} 500 \mathrm{~V}$ capacitor, between the negative terminal of C 56 and CSD-1.
j) Connect pin 6 of V64-V74, - V84 and V94 together with a 3-1/2 in. length of \#16 bare wire.
k) Remove R55, a $270 \Omega 1 \mathrm{~W}$ resistor located between pin 3 of V64 and CSA-2.
m) Temporarily unsolder R91, R81, and R71 from the output tubes grid line. Install L64, L65, two ferrite beads on the grid line between R61 and R71, resolder R71 to grid line.
In a like manner, install L74 and L75 between R71 and R81, and L84 and L85 between R81 and R91.
n) Install R55, a $270 \Omega$ resistor, removed in step k, between the negative terminal of C56 and other end to the junction of R91 and the output tubes grid line.
p) Solder the center conductor of coax to output plate line near V94 and ground to outboard solder lug on V94 socket.
q) Install C93, a 470 pF 500 V capacitor, between pin 6 of V84 and ground lug near V84.
r) Replace Q34, a 151-0108-00 type transistor, with a 2N3904, PN 151-0190-00 type transistor.

FRONT PANEL SYMPTOM: Ripple on FAST RISE OUTPUT.

BEFORE



PROBLEM: Ripple on the 10 V supply under worst case power line conditions.
When we have the following conditions there will be ripple on the FAST RISE OUTPUT:

1. Low Power Line Voltage ( 105).

2a. A +TRANSITION AMPLITUDE minimum (ccw) - TRANSITION AMPLITUDE maximum (cw) or
2 b . The reverse of 2 a .
The Ripple on the OUTPUT is a direct function of the 10 V supply.
PRODUCTION CHANGE: Q217, the -10 V constant voltage source transistor, was changed from a 2 N 2905 to a 2 N 4036 . Use of the new transistor necessitated changing the collector resistor R 217 from $27 \Omega$ to $10 \Omega$, and connecting terminal 15 of T 201 to ground. M11324 ungrounded terminal 15. At the same time, C213 a $100 \mu \mathrm{~F}$ capacitor was added to the collector of Q213 to ground. This Mod supersedes a portion of M11324.

## Parts Removed:

Q217
R217
Parts Added:
Q217
C213
R217

Transistor, 2N2905
Resistor, $27 \Omega 1 \mathrm{~W} 10 \%$

Transistor, 2N4036
151-0208-00
Capacitor, $100 \mu \mathrm{~F} 30 \mathrm{~V}$
Resistor, $10 \Omega 1 \mathrm{~W} 10 \%$
Wire, \#22 solid ins. white

151-0134-00 304-0270-00

INSTALLATION INSTRUCTIONS:
Parts Required: See 'Parts Added'.
continued.
a) Replace R217, a $27 \Omega 1 \mathrm{~W} 10 \%$ resistor, located between CSE-3 and CSF-3, with a $10 \Omega 1 \mathrm{~W} 10 \%$ resistor.
b) Replace Q217, a 2 N 2905 type transistor with a 2 N 4036 .
c) Install a bare wire from CSE-2 to the ground lug next to CSE.
d) Install C213, a $100 \mu \mathrm{~F} 30 \mathrm{~V}$ capacitor, between CSE-2 and CS F-1.
e) Install a " 22 white wire from terminal 15 of T201 to ground lug near Q233, if not present.




AFTER

Effective Prod SN 698 w/exception 201 212 234 243 341 346 364

390 404-5 426 435 532 534 549

Usable in field instruments SN 200-697

| $563-4$ | 602 | 627 | $663-4$ | 692 |
| :--- | :--- | :--- | :--- | :---: |
| 569 | 604 | $634-5$ | $667-70$ | 694 |
| $573-6$ | 609 | $637-8$ | 673 | Also 592 |
| 582 | 611 | $643-50$ | 676 |  |
| 585 | 616 | $652-5$ | 679 |  |
| 596 | $621-3$ | $657-9$ | 684 |  |
| $599-600$ | 625 | 661 | 688 |  |

FRONT PANEL SYMPTOM: Frequency change with temperature.
PROBLEM: D4 leakage changes with temperature, causing the bias and output impedance of Q4 to change. Approximately $5 \%$ change in frequency occurs for every $30^{\circ} \mathrm{F}$ change. This change was also observed when only D4 temperature was changed.

PRODUCTION CHANGE: D4 was changed from an ED2007 diode to a signal diode with a 2.7 M resistor added in parallel.

Parts Removed:
D4
Diode ED 2007
152-0071-00
Parts Added:
D4
Diode, signal 6185
152-0185-00
R5
Resistor, comp 2.7M5\% 1/2 W
301-0275-00

INSTALLATION INSTRUCTION:
Parts Required: See 'Parts Added'.
Installation Procedure:
Replace D4, an ED2007 type diode, located between CSG-5 and CSH-5, with a signal diode. Install with banded end to CSG-5.
Install R5, a $2.7 \mathrm{M} 5 \%$ resistor, in parallel with D4.


Effective Prod SN 778
modified out of sequence

| 201 | 549 | 609 | $652-5$ | 699 |
| :--- | :--- | :--- | :--- | :--- |
| 212 | $563-4$ | 611 | $657-9$ | 701 |
| 234 | $573-6$ | 616 | 664 | 719 |
| 243 | 582 | $621-3$ | 668 | 721 |
| 341 | 585 | 625 | 670 | 723 |
| 346 | 596 | 627 | $673-8$ | $725-6$ |
| $404-5$ | 599 | $634-5$ | $680-1$ | $753-4$ |
| 426 | 600 | $637-8$ | $685-7$ | 764 |
| 532 | 602 | 643 | $689-2$ | 775 |
| 534 | 604 | 650 | 696 |  |

FRONT PANEL SYMPTOM: Output remains at maximum amplitude irrespective of amplitude control.

PROBLEM: Power dissipated by Q247 exceeds limits, and the transistor goes into secondary breakdown. Also, the supplier of Q247 (151-0196-00) changed the flange on Q247, which resulted in an increased thermal resistance between Q247 and its flange. This change was enough to make the problem show more severely. This mod is superseded by M13127.

PRODUCTION CHANGE: Q247 was changed to 2N3739 (151-0201-00) type transistor.
Parts Removed:

Q247

| Chassis | $441-0664-00$ |
| :--- | :--- |
| Transistor, silicon NPN 2N3440 | $151-0196-00$ |
| Nut, Keps steel 4-40 x 1/4 (2) | $210-0586-00$ |
| Washer, fiber \#4 shoulder (2) | $210-0849-00$ |
| Screw, 4-40 x 5/16 Pan HS (2) | $211-0097-00$ |
| Insul. plate mica | $386-1094-00$ |
| Washer, flat steel . 125 TD x . 250 OD (2) | $210-0994-00$ |

Parts Added:
Chassis 441-0664-01
Q247 Transistor, silicon NPN 2N3739
Lug, solder SE-6
Nut, Keps st eel $6-32 \times 1 / 4$ (2)
Washer, steel $6 \mathrm{~S} \times 5 / 16$ (2)
Washer, shoulder \#6 (2)
Screw, $6-32 \times 3 / 8$ PHS (2)
Plate, mica insul
151-0201-00
210-0202-00
210-0457-00
210-0802-00
210-0811-00
211-0510-00
386-0143-00
continued

INSTALLATION INSTRUCTIONS:
Parts Required:
Modification Kit 040-0476-00
Installation Procedure:
Refer to kit instructions.

MOTOR BASE CONNECTOR CHANGED
TO FACILITATE ASSEMBLY AND REDUCE COST

Effective Prod SN 802
FRONT PANEL SYMPTOM: None.
PROBLEM: To reduce cost and facilitate fabrication of Tek made motor bases by adapting them for automated machinery .

This mod is superseded by M12876.
The ground connection for the three wire motor base installed by the mod proved to be inadequate.
PRODUCTION CHANGE: Tek made motor bases 131-0102-00, 131-0150-00 and 131-0430-00 were replaced with new Tek made motor bases 131-0102-01, 131-0150-01 and 131-0430-01 respectively. New and old differ in method used for their assembly and their subparts. Old motor bases use a \#4 nut, lockwasher and screw on one side and a \#4 nut, lockwasher and externally threaded ground post on other side.

New motor bases use a \#4 self-tapping screw into new cover 200-0185-01 on one side and a \#4 sems screw into new interanlly threaded ground post 129-0041-01 on other side.

| Parts Removed: | Motor base | $131-0102-00$ |
| :--- | :--- | :--- |
| Parts Added: | Motor base | $131-0102-01$ |

FRONT PANEL SYMPTOM: The risetime at the negative output of the fastrise exceeds 1 ns .
PROBLEM: The 151-0109-00 transistors supplied by a second source, do not produce the required risetime at the output, even though they meet specifications. Shipment by the first source was delayed.

PRODUCTION CHANGE: Q134 was changed to meet the 1 ns maximum risetime requirement.

## Parts Removed:

Q134 Transistor, silicon, NPN 151-0109-00
Parts Added:
Q134
Transistor, 2N4275, silicon NPN, plastic
151-0223-00
INSTALLATION INSTRUCTIONS:
Parts Required: See 'Parts Added'.
Installation Procedure:
Replace Q134, a silicon transistor located on the negative output circuit board, with a 2 N 4275 type transistor. The new transistor is a direct replasement.

See SQB
M11292 GROUND CONNECTION IMPROVED
BY THE ADDITION OF A SPRING
Effective Prod SN 970
(Accessories)

Usable in field instruments SN 200-969

FRONT PANEL SYMPTOM: None.
PROBLEM: Inadequate ground connection between power cord and instrument motor base.
PRODUCTION CHANGE: A ground spring was added to the non-current carrying ground receptacle on the female connector end of the power cord.

Parts Removed: None
Parts Added: Spring, power cord ground 214-0698-00 (subpart of power cord (161-0024-01)

INSTALLATION INSTRUCTIONS:
Parts Required:
See 'Parts Added', or part listed below.
Field Modification Kit 040-0424-01
NOTE: Field Mod Kit includes enough springs to modify 25 power cords.
Installation Procedure:
Refer to mod kit instructions.

POWER LIGHT COLOR CHANGED
TO STANDARD GREEN
INFORMATION ONLY
M12031
Effective Prod SN 1170
FRONT PANEL SYMPTOM: None.
PROBLEM: More than one color was being used for the POWER ON light.
PRODUCTION CHANGE: All lights were changed to green.
Parts Removed:
B219
Lamp, cart 10 V 40 mA white
150-0052-00
Parts Added:
B219
Lamp, cart 10 V 40 mA green lens, flat
150-0065-00

Effective Prod SN 1190
modified out of sequence $\begin{array}{llllllll}942 & 953 & 1032 & 1044 & 1067 & 1077 & 1081\end{array}$
$\begin{array}{lllll}1089 & 1156-7 & 1159 & 1163-4 & 1168-71\end{array}$
FRONT PANEL SYMPTOM: None.
PR OBLEM: 1) The range of adjustment of C107 and C127 was not large enough in all cases requiring the Test Department to select caps at the high end of the tolerance range.
2) Lower cost transistors are available to replace Q103 and Q114 and are direct replacements.

PRODUCTION CHANGE: 1) C107 and C1 27 were changed from $2-8 \mathrm{pF}$ variable capacitors to $5.5-18 \mathrm{pF}$ caps.
2) Q103 was changed from a 2 N 2501 to a 2 N 4275 type transistor and Q114 was changed from a 151-0142-00 to a 2 N 4258 type transistor.

Parts Removed:

C107, C127
Q103
Q114
Parts Added:
C107, C127
Q103
Q114

Capacitor, var ceramic 2-8pF
Transistor, 2N2501 silicon
Transistor, silicon PNP

Capacitor, var ceramic 5.5-18pF
Transistor, 2N4275 silicon
Transistor, 2 N 4258 silicon
281-0091-00

$$
151-0108-00
$$

$$
151-0142-00
$$

+ AND - TRANSITION AMPLITUDE
CONTROL CIR CUITS MODIFIED
TO ELIMINATE NOISE
See SQB

M1 2606-2

Effective Prod SN 1190
Usable in field instruments SN 200-1189 modified out of sequence $\begin{array}{llllllll}942 & 953 & 1032 & 1044 & 1067 & 1077 & 1081\end{array}$
$\begin{array}{lllll}1089 & 1156-7 & 1159 & 1163-4 & 1168-71\end{array}$
FRONT PANEL SYMPTOM: The + and - TRANSITION AMPLITUDE controls can cause jump or skip in the amplitude while rotating the control.

PROBLEM: The + and - TRANSISTION AMPLITUDE pots, R115 and R135, two 5 k 5 W wire wound log taper pots, may become noisy with age.

PRODUCTION CHANGE: Emitter followers were added between the Transition Amplitude pots and the collector resistors of the output stages to isolate the pots from the output collectors. The addition of the emitter followers, necessitated making several changes. The collector resistor of the output was reduced in value. A resistor was added between the transition pots and ground to limit the lower range. At the same time, the pots were changed from log type wire wounds to linear type carbon pots.
continued

continued

Parts Removed:
R115, R135
Resistor, var 5 k $5+10 \%$ WW
311-0587-00
Circuit Board Assy, -OUTPUT
670-0222-00
Circuit Board Assy, +OUTPUT
670-0223-00
Parts Added:
R115, R135 Potentiometer, comp 5k $\pm 20 \%$ lin 311-0117-00
Circuit Board Assy, -OUTPUT 670-0222-01
Circuit Board Assy, +OUTPUT
670-0223-01

- Output Circuit Board Assembly 670-0222-01 is the same as 670-0222-00 except for the following:
Parts Removed:
R134 Resistor, comp 240 R 1/2W 5\% 301-0241-00
Circuit Board -OUTPUT 388-0686-00
Parts Added:

Q135
Socket, 3-pin transistor
136-0220-00
Transistor, 2N3904 151-0190-00
R134
Resistor, comp 200 』 1/2 W 5\%
301-0201-00
R136
Resistor, comp 2k 1/4 W 5\%
315-0202-00
Circuit Board - OUTPUT
388-0686-01

+ Output Circuit Board Assembly 670-0223-01 is the same as 670-0223-00 except for the following:
Parts Removed:
R114
Resistor, comp 240 ? $1 / 2 \mathrm{~W} 5 \%$
301-0241-00
Circuit Board +OUTTPUT
388-0685-00
Parts Added:

Q115
Socket, 3-pin transistor
136-0220-00
R114
Transistor, 2N3906 silicon
Resistor, comp 200 ก $1 / 2 \mathrm{~W} 5 \%$
151-0188-00
R116
Resistor, comp 2k 1/4 W 5\%
301-0201-00
Circuit Board +OUTPUT
315-0202-00
388-0685-01
INSTALLATION INSTRUCTIONS:
See MI - 12606-2

FRONT PANEL SYMPTOM: None.
PROBLEM: Motor base connector does not meet Canadian Standards Association acceptance standards.

PRODUCTION CHANGE: A plastic insulating shield was added to motor base connector.
Parts Removed: Screw, 6-32 x 5/16 THS (2) 211-0542-00
Parts Added: Shield, motor base polycarbonate 337-0955-00
$2.035 \times 1.00 \mathrm{w} /$ insert (2) 358-0322-00
Screw, 6-32 x 3/4 PHS (2)
211-0514-00
INSTALLATION INSTRUCTIONS:
Parts Required: See 'Parts Added'.
Installation Procedure:
Install motor base connector shield, as shown in drawing using new mounting screws shown in add list.


Effective Prod SN 1355
Usable in fiéld instruments SN 200-1354
modified out of sequence $\begin{array}{llllllll}928 & 937 & 1036 & 1191 & 1193 & 1196 & 1202\end{array}$
1213-19 1222-29 $\quad 1232-59 \quad 1244 \quad 1246-52$
FRONT PANEL SYMPTOM: None.
PROBLEM: The present motor base grounding is not adequate, due to cold flow of the plastic between the ground post and the mounting plate.

PRODUCTION CHANGE: The method used to attach the ground post in the motor base assemblies was changed. The new mounting eliminates plastic between the ground post and the mounting plate and provides a metal to metal ground connection. To insure a good fit between mating parts, the size of the mounting screws was changed from \#4 to \#6, and the clearance holes in the mounting plate and shell were increased to \#6.

To prevent corrosion between new ground post and mounting plate, the plate was changed from etched aluminum to cad plated steel.

| Parts Removed: | Motor base | $131-0102-01$ |
| :--- | :--- | :--- |
| Parts Added: | Motor base | $131-0102-02$ |

INSTALLATION INSTRUCTIONS:
See MI - 12876

Effective Prod SN 1355
Usable in field instruments SN 778-1354

| 928 | 1202 | $1255-57$ | 1278 | 1311 |
| ---: | :--- | :--- | :--- | :--- |
| 937 | 1209 | $1258-59$ | $1292-3$ | $1313-4$ |
| 1036 | $1213-19$ | $1262-66$ | 1298 | 1320 |
| 1191 | $1222-29$ | $1268-69$ | 1300 | 1328 |
| 1193 | $1232-44$ | 1272 | 1305 | $1330-1$ |
| 1196 | $1246-52$ | $1275-76$ | $1308-9$ | $1334-54$ |

FRONT PANEL SYMPTOM: None.
PROBLEM: The series regulator Q247, a 2N3739, is being operated beyond its safe operating region. If Q247 shorts monentarily, Q234 saturates and places approximately 150 V across R 235 , a $3 \mathrm{k} 1 / 4 \mathrm{~W}$ resistor which destroys it.

PRODUCTION CHANGE: Q247 was changed from a 2N3739 transistor to a 2 N 4240 . To accommadate the transistor, several circuit components must also be changed. See schematic.

Parts Removed:

Q247
C56
R242
R241
Transistor, silicon NPN 2N3739
Capacitor, $2 \times 40 \mu \mathrm{~F} 250 \mathrm{~V}$ EMC
Resistor, $150 \Omega 10 \mathrm{~W}$ WW
Resistor, $100 \Omega 1 / 4 \mathrm{~W} 10 \%$

Transistor, silicon 2N4240
151-0251-00
Capacitor, $2 \times 10 \mu \mathrm{~F} 250 \mathrm{~V}$
290-0075-00
Resistor, $27 \Omega 2 \mathrm{~W} 10 \%$
Resistor, $47 \Omega 1 / 4$ W $10 \%$
306-0270-00
R241
C247, C248
Capacitor, $2 \mu \mathrm{~F} 150 \mathrm{~V}$ EMC
316-0470-00
290-0159-00
*290-0075-00 is a $2 \times 10 \mu \mathrm{~F}$ capacitor. Only one $10 \mu \mathrm{~F}$ section will be utilized for C56.

INSTALLATION INSTRUCTIONS:
Parts Required:
Modification Kit 040-0476-00
Installation Procedure:
Use kit instructions.
continued


+ AND - TRANSITION AMPLITUDE
POTENTIOMETER RANGE CHANGED
TO ALLOW FOR GREATER POT
Effective Prod SN 1450
FRONT PANEL SYMPTOM: $\ddagger$ and - FAST RISE outputs will not reduce to less than 50 mV .
PROBLEM: The resistors, R116 and R136, in series with the TRANSITION AMPLITUDE pots installed by M12606-2 to limit the lower range of the TRANSITION AMPLITUDE controls, do not allow for pot tolerances.

PRODUCTION CHANGE: R116 and R136 were reduced in value to 1.8 k .
Parts Removed:
R116, R136 Resistor, comp 2k 1/4W5\% 315-0202-00
Parts Added:
R116, R136
Resistor, comp 1.8k 1/4W5\%
315-0182-00
continued


FRONT PANEL SYMPTOM: Trigger output amplitude not making specifications at 1 MHz or output pulse symmetry range not making specifications at 1 MHz , when it does at 10 kHz .

PROBLEM: D33 was breaking down with 15 V reverse bias causing it to act like a 15 V zener. This limited the TRIGGER OUTPUT Amplitude.

The forward current required to pass through D33 did not generate sufficient forward voltage drop to keep Q34 from saturating. This caused the symmetry to be out of specifications.

PRODUCTION CHANGE: The circuit and the diodes used to prevent Q34 from saturating were changed as shown to a circuit less sensitive to the characteristics of components.

Parts Removed:
D33 Diode, germanium 152-0071-00
R15
Resistor, $130 \Omega 1 / 2 \mathrm{~W} 5 \%$
301-0131-00
Parts Added:

D32, D33
R34

Diode, silicon
Resistor, $130 \Omega 1 / 2 \mathrm{~W} 5 \%$

152-0185-00
301-0131-00

## INSTALLATION INSTRUCTIONS:

See MI - 13187
continued


FRONT PANEL SYMPTOM: None.
PROBLEM: There was an increase in demand for Special Mod 146B, a mod which provides a standard instrument with a rack mounting adapter in place of a standard cabinet.

PRODUCTION CHANGE: Mod 146B, a mod which consists of a regular instrument with a rack mount adapter in place of a standard cabinet was set up as a production special. To accommodate the mod, the front panel was changed by the addition of a mod slot. Regular instruments will have a blank tag.

Parts Removed:
Parts Added:

None.
Tag, mod insert, blank 334-0829-00 Cable assembly, power elec.

161-0031-00

Effective Prod SN 1550
FRONT PANEL SYMPTOM: None
PROBLEM: M13127 added C247-C248, two $2 \mu \mathrm{~F} 150 \mathrm{~V}$ EMC capacitors connected in series. A $1 \mu \mathrm{~F} 450 \mathrm{~V}$ capacitor is now available to replace the two $2 \mu \mathrm{~F}$ capacitors.

PRODUCTION CHANGE: Two $2 \mu \mathrm{~F} 150 \mathrm{~V}$ series connected capacitors, C247-C248, were replaced by a single $1 \mu \mathrm{~F} 450 \mathrm{~V}$ capacitor, C249.

Parts Removed:
C247, C248 Capacitor, $2 \mu$ F 150 V EMC 290-0159-00
Parts Added:
C249
Capacitor, $1 \mu \mathrm{~F}-10 \%+50 \%, 450 \mathrm{~V}$
290-0397-00

GENERATOR FREQUENCY MULTIPLIER
TIMING CAPS DISCHARGED BY
INFORMATION ONLY
M1 3393
ADDING A BLEEDER RESISTOR
Effective Prod SN 1590
FRONT PANEL SYMPTOM: None.
PROBLEM: The timing capacitors do not have a bleeder resistor and consequently do n t t discharge when they are switched out of the circuit.

PRODUCTION CHANGE: A bleeder resistor was added in parallel with each timing capacitor.

Parts Removed: None.
Parts Added:

| $\left.\begin{array}{l}\text { R17B ,R27B } \\ \text { R17C,R27C } \\ \text { R17D,R27D }\end{array}\right\}$ | Resistor comp. $, 20 \mathrm{M}, 1 / 2 \mathrm{~W} 5 \%$ | $301-0206-00$ |
| :--- | :--- | :--- |
| R17E,R27E | Resistor comp. $, 22 \mathrm{M}, 1 / 2 \mathrm{~W} 5 \%$ | $301-0226-00$ |
| Resistor comp. $, 9.1 \mathrm{M}, 1 / 2 \mathrm{~W} 5 \%$ | $301-0915-00$ |  |

JT:bl

Effective Prod SN 1620
FRONT PANEL SYMPTOM: None.
PROBLEM: The line selector switch does not meet Canadian safety standards. The spacing between the switch terminals and the case is such that solder build-up on terminals presents a possible short between the terminals and the case.

PRODUCTION CHANGE: A fiberboard solder shield is added over the terminals before soldering.

Parts Removed: None.
Parts Added:
Shield, solder, S.L. Switch
337-1036-00

JT:bl

## ELIMINATES NOISE CAUSED BY TRANSITION AMPLITUDE POTENTIOMETERS

This modification replaces the wirewound, log taper potentiometers, R115 and R135, the + and - TRANSITION AMPLITUDE potentiometers with composition linear taper type potentiometers.
The wirewound potentiometer had a tendency to by noisy and to cause jump or skip in the output waveform when the control was rotated.
This modification adds an emitter follower in series with the transition amplitude potentiometers, and changes the value of several components.

## PARTS REQUIRED

Quantity Tektronix Part Number

| 2 ea | $136-0220-00$ |
| :--- | :--- |
| 1 ea | $151-0188-00$ |
| 1 ea | $151-0190-00$ |
| 2 ea | $301-0201-00$ |
| 2 ea | $311-0117-00$ |
| 2 ea | $315-0182-00$ |

Description
Socket, transistor, 3-pin
Transistor, 2N3906 PNP
Transistor, 2N3904 NPN
Resistor, comp, $200 \Omega$ l/2W 5\%
Resistor, comp, 5 k linear $\pm 20 \%$ var
Resistor, comp, l.8k 1/4W 5\%

## INSTALLATION

1) Remove R115 and R135, the + and - TRANSITION AMPLITUDE potentiometers, located on the front panel. Install the new type potentiometers. They will be wired in later steps.
2) Remove R114 on the + Output board and R134 on the - Output board, two $240 \Omega$ 1/2 W 5\% resistors.
3) Unsolder the white-green wire from the back of the + Output board. The other end was connected to R115.
4) Unsolder the white-blue wire from the back of the - Output board. The other end was connected to R135.
5) Unsolder the white-brown-red-black wire from the front of the - Output board.
6) Unsolder the tan-brown-black-brown wire from the back of the + Output board. The other end was connected to R115.
continued

## INSTALLATION (continued)

7) Install a 3-pin transistor socket on the - Output board as follows: See Figs. 1 and 2.
a. Emitter lead in hole vacated by R134 near the edge of the board.
b. Collector lead in the hole vacated by white-brown-red-black wire.
c. Base lead will not be soldered to the board. Solder the white-blue wire (removed in step 4) between the base pin and the center terminal of R135.
8) Install a 3-pin transistor socket on the + Output board in a similar manner to step 7. See Figs. 3 and 4.
a. Emitter lead in hole vacated by R114.
b. Collector lead in hole vacated by the tan-brown-black-brown wire.
c. Base lead will not be soldered to the board. Solder the white-green wire (removed in step 3) between the base pin and the center terminal of RII5.
9) Install R114, a $200 \Omega 1 / 2 \mathrm{~W} 5 \%$ resistor, on the + Output board in its new location. See Fig. 3.
10) Install R134, a $200 \Omega 1 / 2 \mathrm{~W} 5 \%$ resistor, on the - Ouput board in its new location. See Fig. 1.
11) Install R116, a $1.8 \mathrm{k} 1 / 4 \mathrm{~W} 5 \%$ resistor, between the inside terminal of R115 and ground on the + Output board.
12) Install R136, a $1.8 \mathrm{k} \mathrm{1/4W5} 5$ resistor, between the inside terminal of R135 and ground on the - Output board.
13) Install the white-brown-red-black wire (unsoldered in step 5) between the outside terminal of R135 and the collector pin of the new socket on the - Output board.
14) Install the tan-brown-black-brown wire (unsoldered in step 6) between the outside terminal of R115 and the collector pin of the new socket on the + Output board.
15) Install Q115, a 2N3906 transistor, in the new socket on the + Output board.
16) Install Q135, a 2N3904 transistor, in the new socket on the - Output board.

JT:Is

Type 106 Square-Wave Generator

FIG. 1


FIG. 2


FIG. 3


FIG. 4


## TRIGGER OUT AMPLITUDE AND PULSE OUT SYMMETRY IMPROVED

To assure proper Output Trigger amplitude and Pulse Out symmetry, it is recommended that diode D33 be replaced, and diode D32 and resistor R34 be added.
These component changes make the Q34 amplifier stage less sensitive to component characteristics, which will help assure proper pulse and trigger output characteristics.

## PARTS REQUIRED

Quantity Tektronix Part Number

$$
\begin{array}{ll}
2 \text { ea } & 152-0185-00 \\
1 \text { ea } & 301-0131-00
\end{array}
$$

## Description

Diode, 6185
Resistor, comp, $130 \Omega$ 1/2 W 5\%

## INSTALLATION

Refer to Fig. 1 for steps 1 through 5 .

1) Remove D33, a germanium diode, located between CSC-6 and CSD-6, above Q34.
2) Relocate a bare wire from CSD -6 to $C S D-3$. Other end is connected to the base of Q34.
3) Install D33, a 6185 type diode, between CSC-6 and CSD-6. Install with cathode, banded end, to CSC-6.
4) Install R34, a $130 \Omega 1 / 2 \mathrm{~W} 5 \%$ resistor, between CSD-3 and CSC-5.
5) Install D32, a 6185 type diode, between CSD-3 and CSD-6. Install with cathode to CSD-3.


FIG. 1
continued
6) Remove R15, a $130 \Omega 1 / 2 \mathrm{~W}$ resistor, located between pin 7 of V 15 and CSE-4. See Fig. 2.


FIG. 2


JT:Is

## MOTOR BASE REDESIGNED TO IMPROVE GROUNDING

The present motor base ground post mounts against the plastic motor base body . Due to cold flow in the plastic it is possible for the ground post to loosen, causing poor ground connection.

A new motor base has been designed which eliminates the plastic between the ground post and the metal mounting plate, thereby assuring a good ground connection.

| Instrument | Serial No. | Instrument | Serial No. | Instrument | Serial No. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 106 | 200-1354 | 317 | 101-5069 | 543B/RM | 100-1588 |
| 109 | 101-1479 | RM17 | 101-929 | 544/RM | 100-979 |
| 111 | 101-1327 | 422 | 100-10649 | 545B/RM | 100-8229 |
| 114 | 100-1699 | 502A | 20000-27719 | 546 | 100-1099 |
| R116 | 100-1199 | RM503 | 101-6859 | RM546 | 100-519 |
| 125 | 101-3129 | RM504 | 101-2549 | 547/RM | 100-7209 |
| 127 | 101-2317 | 507 | 101-822 | 549 |  |
| 129 | 100-599 | 515A | 1001-9679 | 551 | 101-7009 |
| 130 | 101-9879 | RM15 | 101-3539 | 555 |  |
| 132 | 101-2419 | 516 | 101-4419 | 556 | 100-2085 |
| 133 | 101-789 | 519 | 101-1148 | R556 | 100-1049 |
| 160A | 620-11499 | 524 AD | 101-7858 | 561A | 5001-19207 |
| 175 | 101-794 | 526 | 101-2723 | RM561A | 5001-12409 |
| 184 | 100-2628 | 531A | 20001-27419 | 564 | 101-10719 |
| 191 | 100-1878 | RM531A | 1001-27419 | RM564 | 101-2919 |
| 262 | 101-549 | 533A | 3001-5529 | 565/RM | 101-2749 |
| 1121 | 101-1709 | RM533A | 1001-5529 | 567/RM | 101-3039 |
| 067-0502-00 | 2210-869 | 535A | 20001-34929 | 575 | 101-12389 |
| R293 |  | RM535A | 1001-34929 | 581A | 3975-6149 |
| 310A | 10001-22319 | 536 | 101-3749 | 585A | 5969-13429 |
|  |  |  |  | RM585A | 100-1689 |
|  |  |  |  | R647 |  |
|  |  |  |  | 661 | 101-3459 |

Parts required for the following:

| 106 | 191 | RM15 | RM531A | RM543B | 581A |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 109 | 317 | 516 | 533A | RM544 | $585 A$ |
| 111 | RM17 | 519 | RM533A | RM545B | RM585A |
| 127 | RM503 | 524AD | 535A | RM546 | 661 |
| 130 | RM504 | 526 | RM535A | RM547 | 1121 |
| $160 A$ | $515 A$ | $531 A$ | 536 | $567 / R M$ | $067-0502-00$ |

## PARTS REQUIRED:

Quantity 1 ea
continued

Tektronix Part Number
131-0102-02

Description
Connector, motor base

Parts required for the following:

| 114 | 175 | $543 B$ | 549 | 561 A | 575 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 125 | R293 | 544 | 551 | RM561A | RM647 |
| 129 | $310 A$ | $545 B$ | 555 | 564 | $016-0072-00$ |
| 132 | 502 A | 546 | 556 | RM564 |  |
| 133 | 507 | 547 | R556 | $565 /$ RM |  |

PARTS REQUIRED:

| Quantity | Tektronix Part Number | Description |
| :---: | :---: | :---: |
| 1 ea | $131-0572-00$ | Connector, motor base |

Parts required for the following: R116 184

## PARTS REQUIRED:

Quantity Tektronix Part Number Description
1 ea
131-0430-02
Connector, motor base
INSTALLATION
Replace the motor base connector with the new type.

JT:fb

## INSTRUCTION MANUAL

Serial Number $\qquad$

## WARRANTY

All Tektronix instruments are warranted against defective materials and workmanship for one year. Tektronix transformers, manufactured in our own plant, are warranted for the life of the instrument.

Any questions with respect to the warranty mentioned above should be taken up with your Tektronix. Field Engineer.

Tektronix repair and replacement-part service is geared directly to the field, therefore all requests for repairs and replacement parts should be directed to the Tektronix Field Office or representative in your area. This procedure will assure you the fastest possible service. Please include the instrument Type and Serial or Model Number with all requests for parts or service.

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Fig. 1-1. Type 106 Square-Wave Generator.

## SECTION I

## CHARACTERISTICS

## Introduction

The Tektronix Type 106 Square-Wave Generator is a compact, general-purpose square-wave generator. This instrument provides three square-wave outputs; a high-amplitude output ( 120 volts unterminated), and positive-going and negative-going fast-rise outputs (one nanosecond or less risetime into 50 ohms). Repetition rate of the output square waves is variable from 10 Hz to 1 MHz . A sync input feature
is provided to synchronize the Type 106 with an external signal source. A trigger output allows the Type 106 to trigger external devices.

The Performance Check procedure given in Section 5 of this manual provides a convenient means of checking the performance requirements. The following characteristics apply over an ambient temperature range of $0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$. Warm-up time for given accuracy is five minutes.

## ELECTRICAL CHARACTERISTICS

## Square-Wave Generator

| Characteristic | Performance Requirement |  | Supplemental Information |
| :---: | :---: | :---: | :---: |
| Repetition Rate | 10 hertz to 1 megahertz |  | In 5 decade steps. Variable between steps with MULTIPLIER control |
| Repetition Rate Accuracy | Within $\pm 10 \%$ of indicated value |  | Symmetry control centered |
| Multiplier Range | Provides continuously variable repetition rate to 10 times the rate selected by the REPETITION RATE RANGE switch |  |  |
| Symmetry | Duty cycle variable from $45 \%$ or less to $55 \%$ or more |  |  |
| High Amplitude Output Risetime | 12 nanoseconds or less into 50 -ohm load at 12 volts <br> 20 nanoseconds or less into 50 -ohm load at 0.5 volts |  | 120 nanoseconds or less unterminated (risetime when unterminated can be calculated by: $\mathrm{T}_{\mathrm{r}}=2.2 \mathrm{RC}$, where R is the 600 -ohm internal resistance of the Type 106 and C is capacitance of load) |
|  | Into 50 -ohm load | Unterminated |  |
| Amplitude range | 0.5 volts or less to 12 volts or greater | 7 volts or less to 120 volts or greater | 240 milliamps maximum |
| Leading edge aberrations | $\pm 2 \%$ or less in first 100 nanoseconds into 50 ohms |  | Measured on positive-going transition of signal |
| Flat top aberrations |  |  | $0.5 \%$ or less, peak to peak, after first 100 nanoseconds |
| Trailing edge aberrations |  |  | Disregard aberrations in the last 100 nanoseconds preceding trailing edge |
| Polarity | Output level measured from a negative potential to ground |  |  |
| Output impedance |  |  | 600 ohms at OUTPUT connector |
| Fast Rise Output Risetime |  |  | Up to 500 millivolts |
| Amplitude range | 50 millivolts or less to 500 millivolts or more into 50 -ohm load |  |  |
| Polarity | Simultaneous fast-rising positive-going and negative-going outputs |  |  |
| Leading edge aberrations | + and $-2 \%$, or less, or + and -6 millivolts, whichever is greater in the first 5 nanoseconds |  | Measured on positive-going transition of + OUTPUT signal and negative-going transition of - OUTPUT signal |
| Flat top aberrations |  |  | Less than 0.5\% after first 5 nanoseconds |
| Symmetry change with change in amplitude |  |  | 150 nanoseconds, or less, 50 millivolts to 500 millivolts |
| Output impedance |  |  | 50 ohms at + OUTPUT and - OUTPUT connectors |


| Characteristic | Performance Requirement | Supplemental Information |
| :---: | :---: | :---: |
| Sync Input Requirements Pulse or square wave | 2.5 volts to 50 volts, 100 Hertz to 1 Megahertz | For stable operation, risetime of applied pulse should be less than $12.5 \%$ of the period |
| Sine wave |  | 5 volts to 100 volts peak to peak, 100 Hertz to 1 Megahertz |
| Input resistance |  | Approximately 1 megohm at DC |
| Trigger Output Output signal | Positive and negative trigger pulses coincident with the rise and fall of the OUTPUT (HI AMPLITUDE) signal |  |
| Risetime (rate of change) | 50 nanoseconds or less into 50 -ohm load, between 0 and 0.1 volt |  |
| Time jitter | 300 picoseconds or less | Jitter measured one full cycle after test oscilloscope is triggered (see Section 6) |
| Delay time | 50 nanoseconds or less from leading edge of trigger pulse to leading edge of all output signals (positive trigger pulse only for fast-rise outputs) |  |
| Amplitude | 0.10 volt or more into 50 -ohm load | Approximately 0.4 volts unterminated |
| Output impedance |  | 150 ohms |
|  | Power Supply |  |
| Line Voltage 115-volts nominal | 103.5 to 126.5 volts, RMS, AC line voltage provides regulated DC voltages | Range selected by $115 \mathrm{~V}-230 \mathrm{~V}$ Selector |
| 230 -volts nominal | 207 to 253 volts, RMS, AC line voltage provides regulated DC voltages | switch on rear panel |
| Line Frequency | 50 to 60 hertz |  |
| Line Fuse 115 -volts nominal |  | 1.25 A, slow blow |
| 230-volts nominal |  | 0.6 A, slow blow |
| Power Consumption |  | Approximately 85 watts at 115-volt line |

## ENVIRONMENTAL CHARACTERISTICS

The following environmental test limits apply when tested in accordance with the recommended test procedure. This instrument will meet the electrical performance requirements given in this section following environmental test. Complete
details on environmental test procedures, including failure criteria, etc., may be obtained from Tektronix, Inc. Contact your local Tektronix Field Office or representative.

| Characteristic | Performance Requirement | Supplemental Information |
| :--- | :--- | :--- |
| Temperature <br> Operating | $0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$ | Fan at rear circulates air throughout instru- <br> ment. <br> Automatic resetting thermal cutout protects <br> instrument from overheating. |
| Non-operating | $-40^{\circ} \mathrm{C}$ to $+65^{\circ} \mathrm{C}$ |  |
| Altitude <br> Operating | 15,000 feet maximum | May be tested during non-operating tem- <br> perature tests |
| Non-operating | 50,000 feet maximum |  |
| Vibration <br> Operating and <br> non-operating | Vibrate for 15 minutes along each axis at <br> a total displacement of 0.015 inch (1.9g <br> at $50 \mathrm{c} / \mathrm{s}$ with the frequency varied from <br> $10-50-10 \mathrm{c} / \mathrm{s}$ in one minute cycles. Hold <br> at any resonant point for 3 minutes. If <br> no resonant points are found, vibrate at <br> $50 \mathrm{c} / \mathrm{s} \mathrm{for} 3$ minutes on each axis. | Intal vibration time, about 55 minutes. |


| Characteristic | Performance Requirement | Supplemental Information |
| :--- | :--- | :--- |
| Shock <br> Non-operating | One shock of 30 g, one-half sine, 11 milli- <br> second duration along each major axis | Guillotine type shock |
| Transportation | Meets National Safe Transit type of test <br> when correctly packaged <br> Vibrate for one hour slightly in excess of <br> 1 g | Package should just leave vibration sur- <br> face |
| Package drop | Drop from a height of 30 inches on one <br> corner, all edges radiating from that corner <br> and all flat surfaces | Total of 10 drops |

## MECHANICAL CHARACTERISTICS

| Characteristic | Information |
| :--- | :--- |
| Construction <br> Chassis | Aluminum alloy |
| Cabinet | Aluminum alloy with blue-vinyl <br> finish |
| Panel | Aluminum alloy with anodized <br> finish |
| Circuit boards | Glass-epoxy laminate |
| Overall Dimensions <br> (measured at <br> maximum points) <br> Height | 6 inches |
| Width 9 inches <br> Depth $143 / 4$ inches |  |


| Connectors <br> SYNC INPUT | BNC |
| :--- | :--- |
| TRIGGER OUTPUT | BNC |
| OUTPUT | GR874 |
| + OUTPUT | GR874 |
| - OUTPUT | GR874 |

## Standard Accessories

Standard accessories supplied with the Type 106 are listed on the last pullout page at the rear of this manual. For optional accessories available for use with the Type 106, see the current Tektronix, Inc. catalog.

## NOTES

## SECTION 2

## OPERATING INSTRUCTIONS

## General

To use the Type 106 effectively, the operation and capabilities of the instrument must be known. This section describes the function of the front- and rear-panel controls and connectors, gives first-time and general operating information and lists some basic applications for this instrument.

## Voltage Considerations

The Type 106 can be operated from either a 115- or a 230 -volt nominal line. The $115 \mathrm{~V}-230 \mathrm{~V}$ Selector switch on the rear panel changes the instrument from one operating range to the other. Use a small screwdriver or other pointed tool to slide this switch to the desired position.

## CAUTION

The Type 106 should not be operated when the $115 \mathrm{~V}-230 \mathrm{~V}$ Selector switch is in the wrong position for the nominal line voltage applied. Operation of the instrument in the wrong voltage range will either provide incorrect operation or damage the instrument.

When changing operating ranges, the line fuse must be changed. Table 2-1 lists the correct fuse for the applicable nominal line voltage.

TABLE 2-1
Line Fuses

| Nominal Line <br> Voltage | Fuse Rating |
| :---: | :---: |
| 115 -volts | 1.25 A, slow-blow |
| 230 -volts | 0.6 A, slow-blow |

## Cooling

To maintain a safe operating temperature, the Type 106 is cooled with air drawn in at the rear, and blown out the top and bottom of the cabinet. A thermal cutout in the instrument provides thermal protection and disconnects the power to the instrument if the internal temperature exceeds a safe operating level. Power is automatically restored when the temperature returns to a safe level. The cabinet is designed to distribute air flow throughout the instrument for the most efficient cooling. Operation of the instrument for extended periods without the cabinet may cause it to overheat and the thermal cutout to open more frequently.

Adequate clearance must be provided on all sides to allow heat to be dissipated away from the instrument. The clearance provided by the feet at the bottom and rear should be maintained. If possible, allow about one inch of clearance on the sides and top. Do not block or restrict the air flow from the air-intake holes in the cabinet.


Fig. 2-1. Handle and bail-fype stand.

## Handle and Stand

The handle of the Type 106 can be pulled out for convenient carrying of the instrument. When not in use, the handle folds out of the way, into the trim of the instrument cabinet (see Fig. 2-1).

A bail-type stand is mounted beneath the cabinet. This stand permits the Type 106 to be positioned for convenient operation (see Fig. 2-1). The instrument may also be set on the rear feet either for operation or storage.

## CONTROLS AND CONNECTORS

A brief description of the function or operation of the front- and rear-panel controls and connectors follows. Fig. $2-2$ shows the front and rear panels of the instrument. More detailed operation is given in this section under General Operating Information.

## Fronf Panel

REPETITION Determines the repetition rate of the outRATE RANGE

MULTIPLIER Provides variable repetition rate within the range selected by the REPETITION RATE RANGE switch.

SYMMETRY Varies the duty cycle of the output square wave.


Fig. 2-2. Front- and rear-panel controls and connectors.

| AMPLITUDE | Determines amplitude of the square wave <br> available at the OUTPUT (HI AMPLITUDE) <br> connector. |
| :--- | :--- |
| SYNC INPUT * |  |

## Rear Panel

Fuse
115 V - 230 V Selector

Power
Fuse for power input.
Selects nominal operating range of instrument.

Input connector for line power.

## FIRST-TIME OPERATION

The following steps will demonstrate the basic function of the controls and connectors of the Type 106. It is recommended that this procedure be followed completely for firsttime familiarization with this instrument.

1. Set the front-panel controls as follows:

| REPETITION RATE | 1 kHz |
| :--- | :--- |
| RANGE |  |
| MULTIPLIER | 1 |
| SYMMETRY | Midrange |
| AMPLITUDE | Midrange |
| HI AMPLITUDE |  |
| FAST RISE | HI AMPLITUDE |
| +TRANSITION | Midrange |
| AMPLITUDE | Midrange |
| -TRANSITION | OMPLITUDE |

2. Connect the Type 106 to a power source that meets the voltage and frequency requirements of this instrument.
3. Check to be sure that the $115 \mathrm{~V}-230 \mathrm{~V}$ Selector switch on the rear panel is in the correct position for the applied voltage.
4. Set the POWER switch to ON. Allow about five minutes warm up before proceeding.
5. Connect the five-nanosecond GR cable from the OUTPUT (HI AMPLITUDE) connector through the in-line termination to the vertical input of a test oscilloscope (Tektronix Type 545B/1A2 or equivalent).
6. Set the test oscilloscope controls for a display three to four divisions in amplitude, DC coupled, with about one complete cycle displayed on the CRT.
7. Set the REPETITION RATE RANGE switch to 10 kHz . Note that the repetition rate is increased ten times as shown by about one cycle/division. Return the REPETITION RATE RANGE switch to 1 kHz .
8. Turn the MULTIPLIER control to 10. Note that the repetition rate of the square wave is increased about ten times as shown by about one cycle/division. Return the MULTIPLIER control to 1.
9. Rotate the SYMMETRY control throughout its range. Note that the duty cycle (symmetry) of the square wave changes from about $55 \%$ in the counterclockwise position to about $45 \%$ in the clockwise position. Return the SYMMETRY control to midrange.
10. Rotate the AMPLITUDE (HI AMPLITUDE) control throughout its range. Note the change in output amplitude between about 0.5 volt and 12 volts. Also note that the square wave starts from a negative reference potential and goes positive to zero volts. The positive-going transition of the square wave is the portion to which the risetime and aberration characteristics apply.
11. If the test oscilloscope has a dual-trace vertical system, connect a 50 -ohm BNC cable between the TRIGGER OUTPUT connector and the remaining vertical input connector. Note that the trigger output pulses are ghos reith the rise and fall of the OUTPUT (HI AMPLITUDE) square wave. (If the test oscilloscope is single trace, compare coincidence of trigger output pulses and square-wave rise and fall on separate displays.) Disconnect the 50 -ohm BNC cable.
12. Disconnect the five-nanosecond cable from the OUTPUT connector and connect it to the + OUTPUT connector. Set the HI AMPLITUDE-FAST RISE switch to FAST RISE. Adjust the vertical deflection factor to produce a display about three divisions in amplitude.
13. Rotate the + TRANSITION AMPLITUDE control throughout its range. Note the change in output amplitude between about 50 millivolts and 500 millivolts. Also note that the square wave starts from a negative potential and goes to zero volts. The fast-rise portion of the square wave is the positive-going transition.
14. Disconnect the five-nanosecond cable from the + OUTPUT connector and connect it to the - OUTPUT connector.
15. Rotate the - TRANSITION AMPLITUDE control throughout its range. Note the change in output amplitude between about 50 millivolts and 500 millivolts. Also note that the square wave starts from a positive potential and goes to zero volts. The fast-rise portion of the square wave is the negative-going transition.
16. If an external signal is available ( $2.5-50$ volt square wave or $5-100$ volt sine wave) the function of the SYNC INPUT connector can be demonstrated (suggested source, $\mathrm{l}-\mathrm{kHz}$ oscilloscope calibrator). Connect the external signal

| AMPLITUDE | Determines amplitude of the square wave <br> available at the OUTPUT (HI AMPLITUDE) <br> connector. |
| :--- | :--- |
| SYNC INPUT | Input conector for a synchronizing signal. |
| POWER | Switch: Applies power to instrument. <br> Light: Indicates when POWER switch is on <br> and the instrument is connected to a <br> power source. |
| TRIGGER | Output connector for trigger signal which <br> is coincident with the rise and fall of the |
| OUTPUT | OUTPUT (HI AMPLITUDE) signal. <br> Output connector for the HI AMPLITUDE <br> square-wave signal. |
| OUTPUT |  |
| HI AMPLITUDE- | Selects either the HI AMPLITUDE or the <br> FAST RISE |
| FTRANSITION square-wave output. |  |

## Rear Panel

Fuse Selector

Power
$115 \mathrm{~V}-230 \mathrm{~V}$ Selects nominal operating range of instru-
Fuse for power input. ment.

Input connector for line power.

## FIRST-TIME OPERATION

The following steps will demonstrate the basic function of the controls and connectors of the Type 106. It is recommended that this procedure be followed completely for firsttime familiarization with this instrument.

1. Set the front-panel controls as follows:

| REPETITION RATE | 1 kHz |
| :--- | :--- |
| RANGE |  |
| MULTIPLIER | 1 |
| SYMMETRY | Midrange |
| AMPLITUDE | Midrange |
| HI AMPLITUDE - |  |
| FAST RISE | HI AMPLITUDE |
| +TRANSITION | Midrange |
| AMPLITUDE | Midrange |
| -TRANSITION | AMPLITUDE |

2. Connect the Type 106 to a power source that meets the voltage and frequency requirements of this instrument.
3. Check to be sure that the $115 \mathrm{~V}-230 \mathrm{~V}$ Selector switch on the rear panel is in the correct position for the applied voltage.
4. Set the POWER switch to ON. Allow about five minutes warm up before proceeding.
5. Connect the five-nanosecond GR cable from the OUTPUT (HI AMPLITUDE) connector through the in-line termination to the vertical input of a test oscilloscope (Tektronix Type 545B/1A2 or equivalent).
6. Set the test oscilloscope controls for a display three to four divisions in amplitude, DC coupled, with about one complete cycle displayed on the CRT.
7. Set the REPETITION RATE RANGE switch to 10 kHz . Note that the repetition rate is increased ten times as shown by about one cycle/division. Return the REPETITION RATE RANGE switch to 1 kHz .
8. Turn the MULTIPLIER control to 10. Note that the repetition rate of the square wave is increased about ten times as shown by about one cycle/division. Return the MULTIPLIER control to 1.
9. Rotate the SYMMETRY control throughout its range. Note that the duty cycle (symmetry) of the square wave changes from about $55 \%$ in the counterclockwise position to about $45 \%$ in the clockwise position. Return the SYMMETRY control to midrange.
10. Rotate the AMPLITUDE (HI AMPLITUDE) control throughout its range. Note the change in output amplitude between about 0.5 volt and 12 volts. Also note that the square wave starts from a negative reference potential and goes positive to zero volts. The positive-going transition of the square wave is the portion to which the risetime and aberration characteristics apply.
11. If the test oscilloscope has a dual-trace vertical system, connect a 50 -ohm BNC cable between the TRIGGER OUTPUT connector and the remaining vertical input connector. Note that the trigger output pulses are coincident with the rise and fall of the OUTPUT (HI AMPLITUDE) square wave. (If the test oscilloscope is single trace, compare coincidence of trigger output pulses and square-wave rise and fall on separate displays.) Disconnect the 50 -ohm BNC cable.
12. Disconnect the five-nanosecond cable from the OUTPUT connector and connect it to the + OUTPUT connector. Set the HI AMPLITUDE-FAST RISE switch to FAST RISE. Adjust the vertical deflection factor to produce a display about three divisions in amplitude.
13. Rotate the + TRANSITION AMPLITUDE control throughout its range. Note the change in output amplitude between about 50 millivolts and 500 millivolts. Also note that the square wave starts from a negative potential and goes to zero volts. The fast-rise portion of the square wave is the positive-going transition.
14. Disconnect the five-nanosecond cable from the + OUTPUT connector and connect it to the - OUTPUT connector.
15. Rotate the - TRANSITION AMPLITUDE control throughout its range. Note the change in output amplitude between about 50 millivolts and 500 millivolts. Also note that the square wave starts from a positive potential and goes to zero volts. The fast-rise portion of the square wave is the negative-going transition.
16. If an external signal is available (2.5-50 volt square wave or 5-100 volt sine wave) the function of the SYNC INPUT connector can be demonstrated (suggested source, $1-\mathrm{kHz}$ oscilloscope calibrator). Connect the external signal

## TYPE 106


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Fig. 2-3. Control set-up chart.
to the SYNC INPUT connector. Set the REPETITION RATE RANGE switch to 100 kHz and the MULTIPLIER to about 7. Note the repetition rate of the square wave and then disconnect the sync signal. Note the change in repetition rate indicating that the square wave is no longer synchronized with the external signal.
17. This completes the basic operation procedure for the Type 106. More information will be given under General Operating Information in this section.

## CONTROL SETUP CHART

Fig. 2-3 shows the front panel of the Type 106. This chart can be reproduced and used as a test-setup record for special measurements, applications or procedures, or it may be used as a training aid for familiarization with this instrument.

## GENERAL OPERATING INFORMATION

## Output Signals

The output signals available from the Type 106 are shown in Fig. 2-4. These waveform photographs were taken on an oscilloscope which was triggered from the TRIGGER OUTPUT signal to show time relationship of the signals. Notice the zero reference level shown for the square-wave outputs, in particular, the fast-rise outputs. The signal available at the + OUTPUT connector is a positive-going signal which starts from a negative potential and goes to zero volts. The signal available at the - OUTPUT connector is a negativegoing signal which starts from a positive potential and goes to zero volts. The polarity indications on the front panel refer to the portion of the square wave which possesses the desired characteristics (e.g., the + OUTPUT signal has a fast-rising, positive-going leading edge).

## Output Termination

Minimum risetime and optimum pulse characteristics can be obtained only if the outputs are terminated in 50 ohms. A special in-line termination is supplied with the Type 106 for this purpose. This termination also serves as an adapter from the GR outputs of the Type 106 to a BNC input connector on the device under test. If terminations other than this in-line termination are used, they must be capable of dissipating the power available at the OUTPUT (HI AMPLITUDE) connector.

To obtain output amplitudes above about 12 volts from the OUTPUT (HI AMPLITUDE) connector, the output cable must be unterminated. This will result in slower risetime and more pulse aberrations. However, the resultant waveform is satisfactory for most applications where a high-amplitude square wave is needed such as checking the compensation of an attenuator.

## Trigger Output

In some applications, it may be desirable to trigger the device under test from a signal which is coincident with the leading edges of the square-wave signal applied. The signal available at the TRIGGER OUTPUT connector is intended for


Fig. 2-4. Output signals available from the Type 106. Dotted line shows zero-volt DC level for each waveform (repetition rate, 100 kHz ).
this purpose. The positive-going and negative-going trigger pulses are coincident with the rise and fall, respectively, of the square wave at the OUTPUT (HI AMPLITUDE) connector. The positive-going trigger pulses are coincident with the fast-rise outputs. However, the negative-going pulses may lead the trailing edge of the fast-rise outputs.

## Symmetry

The SYMMETRY control on the front panel allows the relationship betwen the time duration of the positive and negative portions of the square wave to be adjusted with respect to each other. This control allows at least $\pm 5 \%$ change in the duty cycle of the output square wave. The symmetry of the square wave may be adjusted to provide equal time duration for the positive and negative portions, or it may be adjusted to make either portion longer in duration. The SYMMETRY control may need re-adjustment when changing repetition rate, output amplitude or when using sync operation as described in the following topic.

## Sync Operation

The output square waves of the Type 106 can be synchronized with an external signal source or an accurate frequency source (such as a Tektronix Type 184 Time-Mark Generator) by applying the external signal to the SYNC INPUT connector. Use the following procedure to synchronize the Type 106 output signals with an external signal.

1. Connect the external signal to the SYNC INPUT connector. If the signal is a pulse or a square wave, it must be between 2.5 and 50 volts in amplitude; if it is a sine wave, it must be between 5 and 100 volts in amplitude, peak to peak.
2. Set the REPETITION RATE RANGE switch and the MULTIPLIER control to a repetition rate setting slightly less than that of the applied synchronizing signal.
3. Adjust the symmetry control for a symmetrical output square wave.

## BASIC APPLICATIONS

The following information describes the procedure and technique for using the Type 106 Square-Wave Generator to make basic measurements. These applications are not described in detail since each application must be adapted to the requirements of the indivivdual measurements. Familiarity with the Type 106 will permit these basic techniques to be applied to a wide variety of uses.

## Risetime Measurements

The Type 106 can be used in conjunction with an oscilloscope to measure risetime. Risetime is normally measured between the $10 \%$ and $90 \%$ points on the leading edge of a waveform. Falltime can be measured using this same basic technique to measure the time between the $90 \%$ and $10 \%$ point on the trailing edge.

Before measuring the risetime of the device under test, the combined risetime of the Type 106 and the oscilloscope


Fig. 2-5. Risetime measurement on a typical waveform.
must be known. Steps 1 through 4 of the following procedure measure this combined risetime. These steps may also be used to measure the risetime of an oscilloscope vertical system by substituting the resultant risetime in the formula given in step 8 (see Example 2) and computing the risetime.

1. Connect the + or - OUTPUT signal to the input of the oscilloscope. Terminate the output of the Type 106 correctly as described in this section.
2. Set the oscilloscope to display the leading edge of the waveform.
3. Determine the $10 \%$ and $90 \%$ points on the leading edge of the waveform.
4. Measure the time duration between these points (see Fig. 2-5). This is the combined risetime of the Type 106 and the oscilloscope ( $\mathrm{T}_{\mathrm{re}}$ ).
5. Connect the output of the Type 106 to the input of the device under test. Terminate the Type 106 output as in step 1.
6. Connect the output of the device under test to the input of the oscilloscope. Terminate the device in its characteristic impedance for optimum performance.
7. Set the oscilloscope controls to display the leading edge of the waveform.
8. Measure the time duration between the $10 \%$ and $90 \%$ points on the leading edge of the waveform. This is the overall risetime $\left(T_{r t}\right)$. Substitute this value in the formula:

$$
T_{r}=\left(T_{r t}{ }^{2}-T_{r e}{ }^{20}\right)^{1 / 2}
$$

Where $T_{r}=$ Risetime of device under test
$T_{r t}=$ Overall risetime
$T_{\text {re }}=$ Risetime of measuring equipment

## NOTE

When the combined risetime of the measuring equipment is 0.1 times or less that of the overall risetime, it affects the calculations very slightly and may be ignored for most computations. The risetime of the device under test then becomes the value measured in step 8.
.
-

## Instruction Manual. Operating Instr. Addendum operating instrucions-Type 106

Example 1. To illustrate the use of this method to medsure the risetime of an external device, assume that the overall risetime is 17 nanoseconds and the risetime of the measuring equipment is 7 nanoseconds.

Substituting the given values in the formula:
T. $\begin{array}{llll}\left(17^{*}-7^{3}\right) \\ 1 / 2 & (289-49) & 1 / 2 & \text { (240) } 1 / 2\end{array}$

The risetime of the device under test is 15.5 nanoseconds.
Example 2. To illustrate the use of this method to measure the vertical risetime of an oscilloscope, assume that the


Fig. 2-6. Typical waveforms showing correct and incorrect compensaion adjustments.

Fig. 2-7. Typical waveform showing limited low-frequency response.

$$
\text { C.V.S. } 1-25-67
$$

Example 1. To illustrate the use of this method to measure the risetime of an external device, assume that the overall risetime is 17 nanoseconds and the risetime of the measuring equipment is 7 nanoseconds.

Substituting the given values in the formula:

$$
T_{r}=\left(17^{2}-7^{2}\right)^{1 / 2}=(289-49)^{1 / 2}=(240) 1 / 2
$$

The risetime of the device under test is 15.5 nanoseconds.
Example 2. To illustrate the use of this method to measure the vertical risetime of an oscilloscope, assume that the

A. Overshoot and top not flat.

B. Correct compensation (square corner, flat top).

C. Rolloff and top not flat.

Fig. 2-6. Typical waveforms showing correct and incorrect compensation adjustments.
overall risetime is 5 nanoseconds. The risetime of the applied signal (Type 106 fast-rise output) is 1 nanosecond.

Substituting the given values in the formula:

$$
T_{r}=\left(5^{2}-1^{2}\right) 1 / 2=(25-1)^{1 / 2}=(24) 1 / 2
$$

The risetime of the device under test is 4.9 nanoseconds.
Notice that although the risetime of the measuring equipment (generator) is 0.2 times the overall risetime it decreases the actual risetime by only 0.1 nanosecond.

## Checking System Response

The square-wave output of the Type 106 can be used for checking the response of active or passive systems. Since the characteristics of the Type 106 pulse are known (see Characteristics section), distortion of the waveform beyond these limits is due to the device under test. The following procedures list several of the tests which can be made.

Compensation. The compensation of an AC-voltage divider such as is used in the input attenuator of an oscilloscope or a passive attenuator probe, can be checked by observing its response when a square-wave signal is applied. Correct response is shown by optimum square corner on the displayed waveform. If the waveform has spike, rolloff or front-corner rounding, the system is not correctly compensated. Fig. 2-6 shows typical waveforms illustrating correct and incorrect compensation adjustments.

Low-Frequency Response. Limited low-frequency response is shown by a trailing-edge droop in the flat-top portion of the square wave (see Fig. 2-7). Apply a symmetrical squarewave of a repetition rate which is not affected by the low-frequency limit. Note the amplitude and then slowly reduce the square-wave frequency until the trailing corner of the square wave falls to $63 \%$ of the amplitude at the leading edge. The low-frequency response ( $30 \%$ down) of


Fig. 2-7. Typical waveform showing limited low-frequency response.
the system is twice the repetition rate of the applied squarewave signal at this point.

High-Frequency Response. Incorrect high-frequency response will be shown by aberrations at the front corner of the square wave. Ringing indicates incorrect peaking adjustments. Overshoot and roll-off indicate incorrect capacitive compensation. Fig. 2-8 shows these effects on a typical waveform (see Fig. 2-6 for effect of compensation).

Limited high-frequency response is also shown by a slower risetime. Risetime of the waveform is measured as discussed under Risetime Measurements. The upper frequency response limit (at 30\% down) can be calculated from the measured risetime using the formula:

$$
\mathfrak{f}=\frac{0.35}{T_{r}}
$$

Where $\mathrm{f}=$ upper $30 \%$ down frequency

$$
T_{r}=\text { Risetime }
$$



Fig. 2-8. Typical waveform showing ringing at front corner.

## CIRCUIT DESCRIPTION

## Introduction

This section of the manual contains an electrical description of the circuits in the Type 106 Square-Wave Generator. A detailed block diagram is given in the following circuit description. Complete schematic diagrams are given in the Diagrams section. Refer to these diagrams for electrical values and relationship throughout the following circuit description.

## GENERATOR CIRCUIT

## Multivibrator

The frequency of the output square wave is determined by the Multivibrator, V15 and V25. These tubes are connected as an astable multivibrator with the feedback connected from the plate of each tube to the control grid of the other. The repetition rate of the output square wave is changed by selecting the feedback capacitors, C17A-E and C27A-E, with the REPETITION RATE RANGE switch, SW17. The MULTIPLIER control, R31, varies the repetition rate within the range selected by SW17, by changing the voltage level to which the feedback capacitors C17 and C27 charge. The emitter follower Q33 isolates the MULTIPLIER control, R31, from the multivibrator and allows a more linear change in repetition rate. The Rep Rate Multiplier Cal ( $\times 1$ ) adjustment, R30, provides calibration of the repetition rate when the MULTIPLIER control is set to 1 .

The Symmetry Range adjustment, R9, is adjusted to balance the plate current of V 15 and V 25 to produce a symmetrical square wave when the SYMMETRY control is set to midrange. The RC networks R12-C12 and R22-C22 provide correct operation of the multivibrator for low-frequency operation. L13 and L23 provide high-frequency peaking and aid in switching the multivibrator.

Symmetry of the square wave can be controlled by the front-panel SYMMETRY control. This control changes the balance between the levels on the screen grids of the multivibrator tubes to alter their cycle of operation. The symmetry of the output square wave can be changed from a duty cycle of $45 \%$ or less to $55 \%$ or more. The Rep Rate Multiplier Cal $(\times 10)$ adjustment, R6, varies the level of the screen grids equally to provide correct repetition rate when the MULTIPLIER control is set to 10.

## Sync Amplifier

Synchronizing signals connected to the SYNC INPUT connector are AC -coupled to the base of Q 4 by Cl . Transistor Q4 is normally biased off. Therefore, only the input pulses which exceed this bias are allowed to pass to the Multivibrator stage through D5. This diode disconnects the two circuits when the Multivibrator voltage goes more negative than the voltage at the collector of Q4.
The output signal is sychronized with an external signal in the following manner. The synchronizing signal from Q4 and D5 is applied to the grid of V15 through C27 and

R14. This pulse will switch V15 off and force the multivibrator to operate at a different frequency than that selected by the REPETITION RATE RANGE switch and the MULTIPLIER control. However, in order for this forced switching to occur, the multivibrator must be operating at a repetition rate slightly less than the repetition rate of the applied signal. When V15 is forced off, V25 will come on and conduct in the normal manner through its half of the cycle. The output square wave produced in this manner will be unsymmetrical, since V25 conducts for the normal period and V25 is forced out of conduction sooner than normal. This can be compensated for in normal use by balancing the duty cycle of the square wave with the SYMMETRY control.

## Shaper Amplifier and Trigger Output

The output square wave from the Multivibrator stage is shaped and amplified by Q34. When the signal at the cathode of V15 goes positive, it will have some overshoot at the leading edge. Q34 eliminates this overshoot and produces a square-cornered signal at its collector.

Emitter-follower Q43 provides isolation between the Drive Amplifier and Trigger Output stages and the Shaper Amplifier. The trigger signal available at the front-panel TRIGGER OUTPUT connector is obtained at the emitter of Q43. This signal is differentiated by the network C45-R46.

## Driver Amplifier

The Driver Amplifier Q54 provides the final amplification for the control signal before it is applied to the Output Amplifier stage. D53 and D54 protect the transistor from being overdriven by a large signal at the base. The output signal at the collector of Q54 is coupled to the grids of the Output Amplifier tubes to control the frequency of the output square wave.

## Output Amplifier

The four tubes in the Output Amplifier, V64-V74-V84-V94, are connected in parallel to provide high output current. The load resistor for this stage is R99 when operated unterminated. When the OUTPUT connector is connected to a terminated system, the load resistor is R99 paralleled by the external termination. The square corner and flat top of the output square wave is achieved by switching the plates of the Output Amplifier tubes from a negative potential to ground. The cathodes are at a negative potential. When the rising portion of the square wave begins, the plates of the Output Amplifier tubes are also at a negative potential. The signal applied from the Driver Amplifier stage turns the Output Amplifier tubes off and their plates rise positive to ground. Then, when the Multivibrator stage switches, the Output Amplifier tubes conduct and the plates go negative again to complete the cycle.

The amplitude of the output square wave is controlled by varying the cathode potential of the Output Amplifier tubes.


Fig. 3-1. Detailed block diagram of the Generator circuit.

The AMPLITUDE control, R246, (located in the Power Supply), varies the output of the A Supply which is connected to the cathodes. As the cathode level is raised (towards ground) the current through the tubes is limited to produce a squarewave output of less amplitude.

The output of the Output Amplifier stage is connected either to the OUTPUT connector when the HI AMPLITUDE - FAST RISE switch is set to HI AMPLITUDE or to the + and - Output Amplifiers in the FAST RISE position.

## + Output Amplifier

When the HI AMPLITUDE - FAST RISE switch is set to FAST RISE, the amplitude of the square wave produced by the Output Amplifier stage is fixed at maximum by SW242B in the Power Supply. This square-wave output signal is applied to transistors Q103 and Q124 through the compensating networks $\mathrm{Cl} 102-\mathrm{Cl} 03-\mathrm{R} 103$ and $\mathrm{Cl} 22-\mathrm{Cl} 23-\mathrm{R} 123$. Emitter follower Q103 passes the signal on to Q114. The purpose for Q103 is to match the delay that exists in the - Output stage because of the inverter transistor Q124. D103 protects the base of Q103 from going more negative than the emitter. D105 clamps the signal which is applied to Q114 so it is always positive.

Quiescently when Q114 is off, current is flowing between ground and the - 10 -Volt supply through R119, D118, D117, R114 and R115. As Q114 comes on, this current is interrupted and current flows between the +10 -Volt supply and the - 10-Volt supply through D104, Q103, R107, Q114, R114 and R115. This reverse biases D117 and D118 which interrupts current through R119. D117 and D118 are low-capacitance, fast turnoff diodes which provide a fast leading edge. When these diodes turn off, the voltage at the +OUTPUT connector rises quickly from a negative potential to ground which produces a positive-going fast-rise square-wave output. The +TRANSITION AMPLITUDE control, R115, varies the output amplitude by changing the current which flows quiescently through R119. C 107 and C 118 provide adjustment for optimum square corner on the leading edge of the output square wave. D114 clamps the output so it does not rise above ground potential.

## - Output Amplifier

The -Output Amplifier operates in much the same manner as described for the +Output Amplifier. Q124 inverts the signal applied to Q134, D123 protects Q124, and D125 clamps the signal so it is always negative. Quiescently, current is flowing between ground and the +10 -Volt supply through R139, D138, D137, R134 and R135. As Q114 comes on, this current is interrupted and current flows between the - 10 -Volt supply and the +10 -Volt supply through D124, Q124, R127, Q134, R134 and R135. This reverse biases D137 and D138 which interrupts current through R139. When D137 and D138 turn off, the voltage at the -OUTPUT connector goes quickly from a positive potential to ground which produces a negative-going fast-rise square-wave output. The -TRANSITION AMPLITUDE control, R135, varies the output amplitude by changing the current which flows quiescently through $\mathrm{R} 139 . \mathrm{Cl} 27$ and Cl 38 provide adjustment for optimum square corner on the leading edge of the square wave. D134 clamps the output so it does not go below ground potential.

## POWER SUPPLY

## General

The Power Supply provides the operating power for the Type 106 from five regulated supplies. Electronic regulation is used to provide stable output voltages. A switch on the rear panel changes the instrument from 115 -volt nominal line to 230 -volt nominal line operation.

## Power Input

Power is applied to the instrument through P201 and is applied to the primary of the transformer, T201, through the line fuse F201, POWER switch SW201, thermal cutout TK201 and the $115 \mathrm{~V}-230 \mathrm{~V}$ Selector switch SW202. The fan is connected across one half of the split primary winding. The $115 \mathrm{~V}-230 \mathrm{~V}$ Selector switch connects the split primaries of T201 in parallel for 115 -volt nominal operation or in series for 230 -volt nominal operation.

Thermal cutout TK201 provides thermal protection for the instrument by opening to interrupt the applied power if the internal temperature becomes too high.

## A - 150-Volt Supply

The output of one secondary winding of T201 is rectified by bridge rectifier D222 to provide power for the A -150 Volt Supply. The rectified power is regulated as follows to provide a stable output voltage:
Reference for this supply with respect to the A Supply is provided by zener diode D224 which holds the emitter of Q224 approximately 75 volts more positive than the output of the A - 150 Volt Supply. Divider R228-R229 sets the base voltage of Q224 about half way between the output voltages of the A Supply and this supply, and the collector current of Q224 controls the conduction of Q227 to regulate the output. As the A Supply voltage is changed to adjust output pulse amplitude, the resulting voltage changes through Q224 and Q227 cause the output of this supply to follow the A Supply at a level approximately 150 volts more negative than the $A$ Supply.

Ripple in the output voltage is held to a minimum by feeding a sample of the output back to the regulator transistor Q227. To understand this operation, assume that the ripple is in the negative half of its cycle. This negative voltage change at the output is connected to the emitter of the error amplifier Q224 through D224 resulting in increased current flow through Q224. The increased collector current of Q224 pulls the base of Q227 negative and reduces its collector current. The result is a reduction in output current which opposes the original output change due to ripple, and provides a stable output voltage. In a similar manner, the regulator circuit compensates for changes in input voltage or changes in load current.

## A Supply

Rectified voltage for operation of the A Supply is provided by voltage divider R246-R247-R248 between the -20-Volt Supply and ground. The A Supply in reference to ground


Fig. 3-2. Detailed block diagram of Power Supply circuit.
is a variable voltage output that is held constant at a selected value by the differential amplifier Q233-Q234. The differential amplifier samples the A Supply voltage and compares it against an adjustable voltage derived from the -20 Volt Supply. The AMPLITUDE conrol, R246 and the Amplitude Cal adjustment, R247 comprise the voltage divider to select the A Supply voltage. The AMPLITUDE control changes the level at the base of Q234 to vary the output of this supply (resulting in a change in the square-wave amplitude). The Amplitude Cal adjustment is adjusted to provide correct maximum amplitude of the square wave. Q223 and Q234 comprise the error amplifier and Q247 is the regulator transistor. Regulation is controlled in a manner similar to that described for the A -150 -Volt Supply.

## $A+150$-Volt Supply

Rectifier D252 provides power for operation of the A + 150 -Volt Supply. Zener diode D255 provides reference voltage for the output of the supply. Since the anode of D255 is connected to the output of the A Supply, it will maintain a voltage at the base of Q257 which follows the changes of the A Supply but is 150 volts more positive. The output voltage at the emitter of the constant voltage source transistor,

Q257, will follow the voltage at its base and maintain a +150 volt difference between this supply and the A Supply.

## A - 20-Volt Supply

Rectifier D262 provides power for operation of the A -20-Volt Supply. Zener diode D264 provides the reference for the output of this supply. D264 is connected from the base of Q267 to the A - 20 -Volt output and maintains a 20 volt difference between the base-emitter of Q267 and the output. The output voltage follows the level at the emitter of Q267 (A Supply voltage) but is always 20 volts more negative.

## +10 -Volt and - 10-Volt Supplies

Rectifier D212 provides power for operation of the +10 Volt and -10-Volt Supplies. Transistors Q213 and Q217 are constant voltage source transistors whose emitters follow the voltage established at the base. The +10 -volt output is established by Zener diode D213 at the base of Q213. The - 10 -volt output is established by Zener diode D216 connected to the base of Q217. The POWER ON light is connected to the output of the - 10 -Volt Supply to indicate when power is applied and the instrument is turned on.

## SECTION 4

# MAINTENANCE 

## Introduction

This section of the manual contains maintenance information for use in preventive maintenance, corrective maintenance, or troubleshooting of the Type 106.

## PREVENTIVE MAINTENANCE

## General

Preventive maintenance consists of cleaning, visual inspection, lubrication, etc. Preventive maintenance performed on a regular basis will help pervent instrument failure and will improve reliability of the instrument. The severity of the environment to which the Type 106 is subjected will determine the frequency of maintenance.

## Cleaning

The Type 106 should be cleaned as often as operating conditions require. Accumulation of dirt in the instrument can cause overheating and component breakdown. Dirt on components prevents efficient heat dissipation. It also provides an electrical conduction path.

## CAUTION

Avoid the use of chemical cleaning agents which might damage the plastics used in this instrument. Some chemicals to avoid are benzene, toluene, xylene, acetone or similar solvents.

Air Filter. The air filter should be visually checked every few weeks and cleaned or replaced if dirty. More frequent inspections are required under severe operating conditions. The following procedure is suggested for cleaning the filter. If the filter is to be replaced, order new air filters from your local Tektronix Field Office or representative; order by Tektronix Part No. 378-0035-01.

1. Remove the filter by pulling it out of the retaining frame on the rear panel. Be careful not to drop any of the accumulated dirt into the instrument.
2. Flush the loose dirt from the filter with a stream of hot water.
3. Place the filter in a solution of mild detergent and hot water.
4. Squeeze the filter to wash out any dirt which remains.
5. Rinse the filter in clear water and allow it to dry.
6. Coat the dry filter with an air-filter adhesive (available from air conditioner suppliers or order Tektronix Part No. 006-0680-00).
7. Let the adhesive dry thoroughly.
8. Re-install the filter in the retaining frame.

Exterior. Loose dust accumulated on the outside of the Type 106 can be removed with a soft cloth or small paint brush. The paint brush is particularly useful for dislodging dirt on and around the front-panel controls. Dirt which remains can be removed with a soft cloth dampened with a mild solution of water and detergent. Abrasive cleaners should not be used.

Interior. Dust in the interior of the instrument should be removed occasionally due to its electrical conductivity under high-humidity conditions. The best way to clean the interior is to blow off the accumulated dust with dry, low-velocity air. Remove any dirt which remains with a soft paint brush or a cloth dampened with a mild detergent and water solution. A cotton-tipped applicator is useful for cleaning in narrow spaces or for cleaning ceramic terminal strips and circuit boards.

## Lubrication

The reliability of potentiometers, rotary switches, and other moving parts can be maintained if they are kept properly lubricated. Use a cleaning-type lubricant (such as Tektronix Part No. 006-0218-00) on shaft bushings and switch contacts. Lubricate switch detents with a heavier grease (such as Tektronix Part No. 006-0219-00). Potentiometers should be lubricated with a lubricant which will not affect electrical characteristics (such as Tektronix Part No. 006-0220-00). Do not use excessive lubrication. A lubrication kit containing the necessary lubricants and instructions is available from Tektronix, Inc. Order Tektronix Part No. 003-0342-00.

During routine maintenance, the fan-motor bearings should be lubricated. Fig. 4-1 shows the lubrication holes in the fan. Place a few drops of light machine oil in the holes. Remember that too much lubrication is as harmful to the fan motor as too little lubrication.

## Visual Inspection

The Type 106 should be inspected occasionally for such defects as broken connections, broken or damaged ceramic terminal strips, improperly seated tubes or transistors, damaged circuit boards or heat-damaged parts.

The remedy for most visible defects is obvious; however, care must be taken if heat-damaged parts are located. Overheating is usually only a symptom of trouble. For this reason, it is essential to determine the actual cause of overheating before the heat-damaged part is replaced; otherwise, the damage may be repeated.

## Tube and Transistor Checks

Periodic checks of the tubes and transistors in the Type 106 are not recommended. The best check of tube or transistor performance is its actual operation in the instrument. More detail on checking tube and transistor operation is given under Troubleshooting.

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## Recalibration

To assure accurate measurements, check the calibration of this instrument after each 500 hours of operation or every six months if used infrequently. In addition, replacement of components may necessitate recalibration of the affected circuits. Complete instructions are given in the Calibration section.


Fig. 4-1. Location of lubrication holes in fan (right side).

The calibration procedure can also be helpful in localizing certain troubles in the instrument. In some cases minor troubles not apparent during normal use may be revealed and/or corrected by recalibration.

## CORRECTIVE MAINTENANCE

## General

Corrective maintenance consists of component replacement and instrument repair. Special techniques or procedures required to replace components in the Type 106 are described here.

## Obtaining Replacement Parts

Standard Parts. All electrical and mechanical part replacements for the Type 106 can be obtained through your local Tektronix Field Office or representative. However, many of the standard electronic components can be obtained locally in less time than is required to order them from Tektronix, Inc. Before purchasing or ordering replacement parts, consult the parts lists for value, tolerance and rating.

## NOTE

When selecting replacement parts, it is important to remember that the physical size and shape of a component may affect its preformance at high frequencies. All replacement parts should be direct replacements unless it is known that a different component will not adversely affect instrument performance.

Special Parts. In addition to the standard electronic components, some special parts are used in the Type 106. These parts are manufactured or selected by Tektronix, Inc. to meet specific performance requirements, or are manufactured for Tektronix, Inc. in accordance with our specifications. These special parts are indicated in the parts list by an asterisk preceding the part number. Most of the mechanical parts used in this instrument have been manufactured by Tektronix, Inc.

Ordering Parts. When ordering replacement parts from Tektronix, Inc., include the following information:

1. Instrument type.
2. Instrument serial number.
3. A description of the part (if electrical, include circuit number).
4. Tektronix Part Number.

## Soldering Techniques

## WARNING

Disconnect the instrument from the power source before soldering.

Ceramic Terminal Strips. Solder used on the ceramic terminal strips should contain about $3 \%$ silver. Ordinary tinlead solder can be used occasionally without damage to the ceramic terminal strips. Use a 40 - to 75 -watt soldering iron with a $1 / 8$-inch wide chisel-shaped tip. If ordinary solder is used repeatedly or if excessive heat is applied, the solder-to-ceramic bond may be broken.

A roll of $3 \%$ silver is mounted on the rear of the instrument. Additional silver solder should be available locally, or it can be purchased directly from Tektronix, Inc. Order by Tektronix Part No. 251-0514-00.

Observe the following precautions when soldering ceramic terminal strips.

1. Use a hot iron for a short time. Apply only enough heat to make the solder flow freely.
2. Maintain a clean, properly tinned tip.
3. Avoid putting pressure on the ceramic terminal strip.
4. Do not attempt to fill the terminal-strip notch with solder; use only enough solder to cover the wires adequately.
5. Clean the flux from the terminal strip with a fluxremover solvent.

Circuit Boards. Use ordinary 60/40 solder and a 35 - to 40 -watt pencil type soldering iron on the circuit boards. The tip of the iron should be clean and properly tinned for best heat transfer to the solder joint. A higher wattage soldering iron may separate the wiring from the base material.

The following technique should be used to replace a component on a circuit board. Most components can be replaced without removing the boards from the instrument.

1. Grip the component lead with long-nose pliers. Touch the soldering iron to the lead at the solder connection. Do not lay the iron directly on the board, as it may damage the board.
2. When the solder begins to melt, pull the lead out gently. This should leave a clean hole in the board. If not, the hole can be cleaned by reheating the solder and placing a sharp object such as a toothpick or pointed tool into the hole to clean it out.
3. If a wire extends beyond the solder joint, clip off the in the board. If the component is replaced while the board is mounted in the instrument, cut the leads so they will just protrude through the board. Insert the leads into the board until the component is firmly seated against the board. If it does not seat properly, heat the solder and gently press the component into place.
4. Apply the iron and a small amount of solder to the connection to make a firm solder joint. To protect heatsensitive components, hold the lead between the component body and the solder joint with a pair of long-nose pliers or other heat sink.
5. Clip the excess lead that protrudes through the board.
6. Clean the area around the soldered connection with a flux-remover solvent. Be careful not to remove information printed on the board.

Metal Terminals. When soldering metal terminals (e.g., switch terminals, potentiometers, tube or transistor socket contacts, etc.), ordinary $60 / 40$ solder can be used. The soldering iron should have a 40 - to 75 -watt rating with a $1 / 8$ inch wide chisel-shaped tip.

Observe the following precautions when soldering metal terminals:

1. Apply only enough heat to make the solder flow freely.
2. Apply only enough solder to form a solid connection. Excess solder may impair the function of the part.
3. If a wire extends beyond the solder joint, clip off the excess.
4. Clean the flux from the solder joint with a flux-remover solvent.

## Component Replacement

## WARNING

Disconnect the instrument from the power source before replacing components.

Removing the Cabinet. The Type 106 is held into the cabinet by the securing screw on the lower left cornet of the front panel. To remove the cabinet, loosen this screw and slide the instrument out of the cabinet.

## CAUTION

The cabinet of the Type 106 is designed to direct the flow of air through the instrument. Operation of the instrument for a prolonged period of time without the cabinet may cause the instrument to overheat and the thermal cutout to open more frequently.

Ceramic Terminal Strip Replacement. A complete ceramic terminal strip assembly is shown in Fig. 4-2. Replace-
ment strips (including studs) and spacers are supplied under separate part numbers. The old spacers may be re-used if they are not damaged.


Fig. 4-2. Ceramic terminal strip assembly.

To replace a ceramic terminal strip, first unsolder all connections. Then, the damaged strip can be pried or pulled loose from the chassis. If the spacers come out with the strip, remove them from the stud pins to be used for installation of the new strip.

After the damaged strip has been removed, place the undamaged spacers in the chassis holes. Then, carefully press the studs into the spacers until completely seated. If necessary, use a soft mallet and tap lightly, directly over the stud area of the strip.

Circuit Board Replacement. If a circuit board is damaged and cannot be repaired, the entire assembly including all soldered-on components, or the board only, can be replaced. Part numbers are given in the Mechanical Parts List for either the completely-wired board or the unwired board.

All connections are soldered to the circuit boards. Most of the components mounted on the boards can be replaced without removing the board from the instrument. Observe the soldering precautions given under Soldering Techniques in this section. However, if the board itself must be replaced, use the following procedure:

1. Unsolder all leads connected to the board. Observe the soldering precautions given in this section.
2. Remove the securing nut holding the connector and circuit board assembly to the front panel (see Fig. 4-3) and remove the assembly. Use a General Radio wrench designed for this purpose.
3. Loosen the two clamp screws (see Fig. 4-3).
4. Unsolder the connection between the connector and the board and separate the units. (See Connector Repair or Termination Replacement which follows to repair these parts.)
5. To replace the board, reverse the order of removal. Correct connection of the interconnecting leads is shown in Figs. 4-6 and 4-7.


Fig. 4-3. Removing the + and - Output circuit board assemblies.


Fig. 4-4. Exploded view of + and - Output connectors.

Connector Repair or Termination Replacement. Use the following procedure to repair the connector or replace the termination. Fig. 4-4 shows the connector and its parts.

1. Follow steps 1 through 4 of the procedure under Cir cuit Board Replacement.
2. Use a special General Radio jig to hold the inner contact of the connector. Then, remove the hex nut on the
outside of the termination. The disc termination can now be removed from the connector.
3. To completely disassemble the connector, remove the remaining hex nut.
4. The connector can be re-assembled by reversing the steps above.

Tube and Transistor Replacement. Tubes and transistors should not be replaced unless actually defective. If removed during routine maintenance, return them to their original sockets. Unnecessary replacement of tubes or transistors may affect the calibration of this instrument. Replacement tubes or transistors should be of the orginal type or a direct replacement. When tubes or transistors are replaced, check the calibration of that part of the circuit which may be affected.

Rotary Switches. Individual wafers or mechanical parts of rotary switches are normally not replaced. If a switch is defective, replace the entire assembly. Replacement switches can be ordered either wired or unwired; refer to the Electrial Parts List for the applicable part number.

When replacing a switch, it is recommended that the leads and switch terminals be tagged with corresponding identification tags as the leads are disconnected. Then, use the old switch as a guide for installing the new one. An alternative method is to draw a sketch of the switch layout and record the wire color at each terminal.

## TROUBLESHOOTING

## Introduction

The following information is provided to facilitate troubleshooting of the Type 106, if trouble develops. Information
contained in other sections of this manual should be used along with the following information to aid in locating the defective component.

## Troubleshooting Aids

Diagrams. Circuit diagrams are given on foldout pages in Section 9. The circuit number and electrical value of each component in this instrument as well as important voltages and waveforms are shown on the diagrams.

Component Numbers. The circuit number of each electrical part in this instrument is shown on the circuit diagram. Each main circuit is assigned a series of circuit numbers. Table 4-1 lists the main circuits in the Type 106 and the series of circuit numbers assigned to each. For example, using Table 4-1 a resistor numbered R134 is identified as being located in the Fast Rise Output circuit.

TABLE 4-1
Circuit Numbers

| Circuit Number <br> on Diagrams | Circuit |
| :---: | :--- |
| $1-99$ | Generator |
| $100-199$ | Fast Rise Output |
| $200-299$ | Power Supply |

Switch Wafer Identification. Switch wafers shown on the diagrams are coded to indicate the position of the wafer in the complete switch assembly The numbered portion of the code refers to the wafer number counting from the front or mounting end of the switch toward the rear. The letters $F$ and $R$ indicate whether the front or rear of the wafer performs the particular switching function. For example, a wafer designated $2 R$ indicates that the rear of the second wafer is used for this particular switching function.

Circuit Boards. Figs. $4-6$ and $4-7$ show the circuit boards used in the Type 106. Each electrical component on the boards is identified by its circuit number. Correct connection of the interconnecting leads is also shown. The boards are outlined on the diagrams with a blue line. These pictures used along with the diagrams will aid in locating the components mounted on the circuit boards.

TABLE 4-2

| SUPPLY | BACK- <br> GROUND <br> COLOR | 1st <br> STRIPE | 2nd <br> STRIPE | 3rd <br> STRIPE |
| :--- | :--- | :--- | :--- | :--- |
| A Supply | Tan | Violet | Green | Black |
| A +150 V | White | Brown | Brown | Green |
| A -150 V | Tan | Brown | Brown | Green |
| A -20 V | Tan | Brown | Red | Brown |
| -10 Volt | Tan | Brown | Black | Brown |
| +10 Volt | White | Brown | Black | Black |

Wiring Color-Code. All insulated wire used in the Type 106 is color-coded according to the EIA standard color-code (as used for resistors) to facilitate point-to-point circuit tracing. The widest color stripe identifies the first color of the code. Power-supply voltages can be identified by three color stripes and the following background color-code: white, positive voltage; tan, negative voltage. Table 4-2 shows the wiring color-code for the power-supply voltages
used in the Type 106. The remainder of the wiring in the Type 106 is color-coded with two or less stripes or has a solid background without stripes. The color-coding helps to trace a wire from one point in the instrument to another.
Resistor Color-Code. A number of precision metal-film resistors are used in this instrument. These resistors can be identified by their grey body color. If a metal-film resistor has a value indicated by three significant figures and a multiplier, it will be color-coded according to the EIA standard resistor color-code. If it has a value indicated by four significant figures and a multiplier, the value will be printed on the body of the resistor. For example, a $333 \mathrm{k} \Omega$ resistor will be color-coded, but a $333.5 \mathrm{k} \Omega$ resistor will have its value printed on the resistor body. The color-code sequence is shown in Fig. 4-5.

Composition resistors are color-coded according to the EIA standard resistor color-code.

## Troubleshooting Techniques

This troubleshooting procedure is arranged in an order which checks the simple trouble possibilities before proceeding with extensive troubleshooting. The first few checks assure proper connection, operation and calibration. If the trouble is not located by these checks, the remaining steps


Fig. 4-5. Color-coding of metal-film resistors.
aid in locating the defective circuit and component. When the defective component is located, it should be replaced following the replacement procedures given in this section.

1. Check Associated Equipment. Before proceeding with troubleshooting of the Type 106, check that the equipment used with the Type 106 is operating correctly. Check that the signal is properly connected and that the interconnecting cables are not defective. Also, check the power source.
2. Check Control Settings. Incorrect control settings can indicate a trouble that does not exist. If there is any question about the correct function or operation of any control, see the Operating Instructions section of this manual.
3. Check Instrument Calibration. Check the calibration of the instrument, or the affected circuit if the trouble exists in one circuit. The indicated trouble may only be a result

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of misadjustment, or may be corrected by calibration. Complete instructions are given in the Calibration section of this manual. Individual calibration steps can be performed out of sequence. However, if the step affects the calibration of other circuits in the instrument, a more complete calibration will be necessary.
4. Isolate Trouble to a Circuit. To isolate a trouble to a particular circuit, note the trouble symptom. The symptom often identifies the circuit in which the trouble is located. When trouble symptoms appear in more than one circuit, check all affected circuits. Methods of checking the circuits are given in steps 5 through 7.

Incorrect operation of all circuits often indicates trouble in the Power Supply. Check first for correct voltage of the individual supplies. However, a defective component elsewhere in the instrument can appear as a power-supply trouble and may also affect the operation of other circuits.

After the defective circuit has been located, proceed with steps 5 through 7 to locate the defective component(s). If the trouble has not been isolated to a circuit using the procedure described here, check voltages and waveforms as explained in step 6 to locate the defective circuit.
5. Visual Check. Visually check the circuit in which the trouble is located. Many troubles can be located by visual indications such as unsoldered connections, broken wires, damaged circuit boards or damaged components.
6. Check Voltages and Waveforms. Often the defective component can be located by checking for the correct voltage or waveform in the circuit. Typical voltages and waveforms are shown on the diagrams.

## NOTE

Voltages and waveforms given on the diagrams are not absolute and may vary slightly between instruments. To obtain operating conditions similar to those used to take these readings, see the first diagram page.
A. VOLTAGES. Voltage measurements should be taken with a 20,000 ohms/volt DC voltmeter. Accuracy of the voltmeter should be within $3 \%$ on all ranges. Be sure that the test prods are well insulated to prevent accidental shorting of components.
B. WAVEFORMS. Use a test oscilloscope which has the following minimum specifications:

Bandwidth: DC to 30 MHz

Deflection factor: 0.05 volts/division minimum
Input impedance: 1 Megohm paralleled by about 20 pF
7. Check Individual Components. The following procedures describe methods of checking individual components in the Type 106. Components which are soldered in place can be checked most easily by disconnecting one end. This eliminates incorrect measurements due to the effects of surrounding circuitry.
A. TUBES AND TRANSISTORS. The best check of tube and transistor operation is actual performance under operating conditions. If a tube or transistor is suspected of being defective, it can best be checked by substituting a new component or one which has been checked previously. However, be sure that circuit conditions are not such that a replacement tube or transistor might also be damaged. If substitute tubes or transistors are not available, a dynamic tester may be used (such as Tektronix Type 570 or Type 575). Static-type testers are not recommended since they do not check operation under simulated operating conditions.
B. DIODES. A diode can be checked for an open or shorted condition by measuring the resistance between terminals. With an ohmmeter scale having an internal source of about 1.5 volts, the resistance should be very high in one direction and very low when the leads are reversed.

## CAUTION

Do not use an ohmmeter scale that has a high internal current. High currents may damage the diode.
C. RESISTORS. Resistors can be checked with an ohmmeter. Check the Electrical Parts List for the tolerance of resistors used in this instrument. Resistors should be replaced if the measured value is outside the specified tolerance.
D. INDUCTORS. Check for open inductors by checking continuity with an ohmmeter. Shorted or partially shorted inductors can usually be found by checking the waveform response when high-frequency signals are passed through the circuit. Partial shorting often reduces high-frequency response (roll-off).
E. CAPACITORS. A leaky or shorted capacitor can best be detected by checking resistance with an ohmmeter on the highest scale. Do not exceed the voltage rating of the capacitor. The resistance reading should be high after initial charge of the capacitor. An open capacitor can best be detected with a capacitance meter, or by checking whether the capacitor passes AC signals.


Fig. 4-6A. + Oułpuł Amplifier circuit board (above SN 1190).


Fig. 4-6B. + Output Amplifier circuit board (SN 200 to 1189).


Fig. 4-7A. - Output Amplifier circuit board (above SN 1190).


Fig. 4-7B. - Output Amplifier circuit board (SN 200 to 1189).

## SECTION 5

## PERFORMANCE CHECK

## Introduction

This performance check procedure is provided to check the operation of the Type 106 without removing the cabinet. This precedure may be used for incoming inspection, instrument familiarization, reliability testing, calibration verification, etc.

If the instrument does not meet the performance requirements given in this procedure, internal checks and/or adjustments are required. See the Calibration section. All performance requirements given in this section correspond to those given in the Characteristics section.

## Recommended Equipment

The following equipment is recommended for a complete performance check. Specifications given are the minimum necessary to perform this procedure. All equipment is assumed to be calibrated and operating within the given specifications. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

1. Test oscilloscope. Frequency response, DC to 30 MHz ; minimum deflection factor, 20 millivolts/division; accuracy, within $\pm 3 \%$; must have 1 kHz amplitude calibrator output voltages of 1,5 and 50 volts and a dual-frace vertical system. Tektronix Type 545B Oscilloscope with Type 1A2 DualTrace Plug-In Unit recommended.
2. Sampling oscilloscope. Risetime, 0.35 nanoseconds; calibrated deflection factor, 10 millivolts/division minimum; calibrated sweep range, equivalent to 100 nanoseconds/division to 0.2 nanoseconds/division. Tektronix Type 661 Oscilloscope with Type 4S3 Sampling-Probe Dual-Trace Unit and Type 5T3 Timing Unit recommended.
3. Delay cable. Impedance, 50 ohms; electrical length, 60 nanoseconds; connectors, GR874. Tektronix Type 113 Delay Cable recommended.
4. Time-mark generator. Marker outputs, 1 microsecond to 1 second; marker accuracy, within $0.1 \%$. Tektronix Type 184 Time-Mark Generator recommended.
5. Cable. Impedance, 50 ohms; type RG-213/U; electrical length, five nanoseconds; connectors, GR874. Tektronix Part No. 017-0502-00.
6. Thru-line termination. Impedance, 50 ohms; wattage ratings, 1.0 watts; accuracy, $\pm 3 \%$; connectors, GR874 input with BNC female output. Tektronix Part No. 017-0083-00.
7. Adapter. Connectors, GR874 and BNC female. Tektronix Part No. 017-0063-00.
8. Cable (two). Impedance, 50 ohms; type, RG-58A/U; length, 42 inches; connectors, BNC. Tektronix Part No. 012-0057-01.
9. Termination. Impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, BNC. Tektronix Part No. 011-0049-00.
10. BNC T connector. Tektronix Part No. 103-0030-00.
11. Attenuator. Attenuation, $10 \times$; impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, GR874. Tektronix Part No. 017-0078-00.
12. VP-2 Voltage Pickoff. Tektronix Part No. 017-0077-00.
13. End-line termination. Impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, GR874. Tektronix Part No. 017-0081-00.

## PERFORMANCE CHECK PROCEDURE

## General

In the following procedure, control settings or test equipment connections should not be changed except as noted. If only a partial check is desired, refer to the preceding step(s) for setup information. Type 106 front-panel control titles referred to in this procedure are capitalized (e.g., AMPLITUDE).

The following procedure uses the equipment listed under Recommended Equipment. If equipment is substituted, control settings or setup may need to be altered to meet the requirements of the equipment used.

## Preliminary Procedure

1. Connect the Type 106 to a power source which meets the voltage and frequency requirements of this instrument.
2. Set the Type 106 controls as follows:

| REPETITION RATE RANGE | 1 kHz |
| :---: | :---: |
| MULTIPLIER | 10 (clockwise) |
| SYMMETRY | Midrange |
| AMPLITUDE | Counterclockwise |
| HI AMPLITUDE - FAST RISE | HI AMPLITUDE |
| $\begin{aligned} & + \text { TRANSITION AMPLI- } \\ & \text { TUDE } \end{aligned}$ | Counterclockwise |
| - TRANSITION AMPLITUDE | Counterclockwise |
| POWER | ON |

3. Allow at least five minutes warm up at $25^{\circ} \mathrm{C}, \pm 5^{\circ}$ for checking the instrument to the given accuracy.

## 1. Check Amplitude Control Range

a. REQUIREMENT- 0.5 volt or less to 12 volts or greater into 50 -ohm load. 7 volts or less to 120 volts or greater, unterminated.

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b. Connect the OUTPUT (HI AMPLITUDE) connector to the input of the test oscilloscope through the five-nanosecond GR cable and the 50 -ohm in-line termination.
c. Set the test oscilloscope vertical deflection to 0.1 volts/ division and the sweep rate to 50 microseconds/division.
d. CHECK—Test oscilloscope display amplitude for five divisions or less ( 0.5 volt or less).
e. Set the test oscilloscope vertical deflection to 2 volts/ division.
f. Turn the AMPLITUDE (HI AMPLITUDE) control fully clockwise.
g. CHECK—Test oscilloscope display amplitude for six divisions or greater ( 12 volts or greater).
h. Set the test oscilloscope vertical deflection to 20 volts/ division.
i. Remove the 50 -ohm in-line termination and connect the five-nanosecond cable to the test oscilloscope input using the GR-to-BNC adapter.
i. CHECK—Test oscilloscope display for 6 divisions minimum amplitude ( 120 volts or greater).
k. Turn the AMPLITUDE ( HI AMPLITUDE) control fully counterclockwise.
I. Set the test oscilloscope vertical deflection to two volts/ division.
m. CHECK—Test oscilloscope display for 3.5 divisions or less amplitude (seven volts or less).

## 2. Check Symmetry Range

a. REQUIREMENT-Duty cycle variable from $45 \%$ or less to $55 \%$ or greater.
b. Connect the OUTPUT (HI AMPLITUDE) connector to the input of the test oscilloscope through the five-nanosecond GR cable and the 50 -ohm in-line termination.
c. Set the AMPLITUDE (HI AMPLITUDE) control to midrange.


Fig. 5-1. Typical test oscilloscope display showing symmetry limits.
d. Set the SYMMETRY control fully clockwise.
e. Set the test oscilloscope sweep rate to display one complete cycle in 10 divisions (use variable control).
f. CHECK—Positive portion of square wave for duration of 5.5 divisions or more ( $55 \%$ duty cycle or more; see Fig. 5-1).
g. Set the SYMMETRY control fully counterclockwise.
$h$. If necessary, readjust the sweep rate to display one complete cycle in 10 divisions.
i. CHECK—Positive portion of square wave for duration of 4.5 divisions or less ( $45 \%$ duty cycle or less; see Fig. $5-1$ ).

## 3. Check Repetition Rate Accuracy

a. REQUIREMENT-Within $\pm 10 \%$ of indicated repetition rate
b. Connect the timemark generator output to the channel 2 input connector of the test oscilloscope through a 50 -ohm BNC cable and a 50 -ohm termination. Set the time-mark generator for .1 millisecond markers.
c. Set the AMPLITUDE (HI AMPLITUDE) control to midrange.
d. Set the test oscilloscope vertical deflection to display about two divisions of the signal on each channel in the alternate mode.
e. Using the Type 106, time-mark generator and test oscilloscope settings given in Table 5-1, check repetition rate accuracy within $\pm 10 \%$.
f. Disconnect all test equipment.

## 4. Check Synchronized Operation

a. REQUIREMENT-Output signal synchronizes with 2.5 to 50 volt input square wave.
b. Connect the test-oscilloscope amplitude calibrator to the SYNC INPUT connector and the channel 1 input connector through a BNC T connector and two 50 -ohm BNC cables.
c. Connect the OUTPUT (HI AMPLITUDE) connector to the channel 2 input connector through a five-nanosecond GR cable and a 50 -ohm in-line termination.
d. Set the REPETITION RATE RANGE switch to 100 Hz and the multiplier to about 7.
e. Set the test oscilloscope amplitude calibrator for five volts output and the sweep rate to 0.5 millisecond/divsion.
f. Set the test oscilloscope to trigger from channel 1 in the chopped mode.
g. CHECK-Test oscilloscope for stable display of the channel 2 waveform (readjust the MULTIPLIER if necessary).
h. Set the test oscilloscope amplitude calibrator for 50 volts output.
i. CHECK-Test oscilloscope for stable display of the channel 2 waveform.
j. Set the test oscilloscope amplitude calibrator for one volt output.

TABLE 5-1
Repetition Rate Accuracy

| REPETITION <br> RATE RANGE <br> Switch Setting | MULTIPLIER <br> Control <br> Setting | Time <br> Markers <br> Applied | Test <br> Oscilloscope <br> Sweep Rate | CRT Display <br> (Cycles/Marker <br> for $\pm 10 \%$ <br> accuracy) |
| :---: | :---: | :---: | :---: | :---: |
| 100 kHz | 10 | $10 \mu \mathrm{~s}$ | $1 \mu \mathrm{~s} / \mathrm{div}$ | $9-11$ |
| 100 kHz | 5 | $10 \mu \mathrm{~s}$ | $1 \mu \mathrm{~s} / \mathrm{div}$ | $4.5-5.5$ |
| 10 kHz | 9 | 0.1 ms | $10 \mu \mathrm{~s} / \mathrm{div}$ | $8.1-9.9$ |
| 10 kHz | 4 | 0.1 ms | $10 \mu \mathrm{~s} / \mathrm{div}$ | $3.6-4.4$ |
| 1 kHz | 8 | 1 ms | $0.1 \mathrm{~ms} / \mathrm{div}$ | $7.2-8.8$ |
| 1 kHz | 3 | 1 ms | $0.1 \mathrm{~ms} / \mathrm{div}$ | $2.7-3.3$ |
| 100 Hz | 7 | 10 ms | $1 \mathrm{~ms} / \mathrm{div}$ | $6.3-7.7$ |
| 100 Hz | 2 | 10 ms | $1 \mathrm{~ms} / \mathrm{div}$ | $1.8-2.3$ |
| 10 Hz | 6 | 0.1 s | $10 \mathrm{~ms} / \mathrm{div}$ | $5.4-6.6$ |
| 10 Hz | 1 | 0.1 s | $10 \mathrm{~ms} / \mathrm{div}$ | $0.9-1.1$ |

k. CHECK—Test oscilloscope for drift of the channel 2 waveform due to inadequate sync signal.
I. Disconnect all test equipment.

## 5. Check Trigger Output

a. REQUIREMENT—Amplitude, 0.1 volt positive and negative into 50 ohms.
Risetime, 50 nanoseconds or less, between 0 and 0.1 volt.
Delay Time, 50 nanoseconds or less.
b. Connect the TRIGGER OUTPUT connector to the channel 2 input connector of the test oscilloscope through a 50 ohm BNC cable and a 50 -ohm BNC termination.
c. Connect the OUTPUT (HI AMPLITUDE) connector to the channel 1 input of the test oscilloscope through a 50 ohm GR cable and a 50 -ohm in-line termination.
d. Set the test oscilloscope to display the channel 2 signal at a vertical deflection of 0.1 volt/division and a sweep rate of 10 microseconds/division.
e. Set the REPETITION RATE RANGE switch to 100 kHz and the MULTIPLIER control to 1 .
f. CHECK-Test oscilloscope display for positive and negative pulse amplitude of 1 division minimum ( 0.1 volt minimum; see Fig. 5-2A).
g. Set the test oscilloscope for a vertical deflection of 0.02 volts/division at a sweep rate of 50 nanoseconds/ division (use magnifier).
h. Position the display to observe the leading edge of the positive pulse.
i. CHECK-Test oscilloscope display for one division or less between the 0 and 0.1 volt levels of the trigger pulse ( 50 nanoseconds or less; see Fig 5-2B.
i. Set the test oscilloscope to trigger from channel 1 in the alternate mode.
k. Position the $50 \%$ points of both waveforms to the horizontal centerline.
I. CHECK—Test oscilloscope display for one division or less spacing between the $50 \%$ amplitude points of the two waveforms ( 50 nanoseconds or less; see Fig. 5-3C).
m. Disconnect all test equipment.

## 6. Check Hi Amplitude Output Into 50 ohms

a. REQUIREMENT—Risetime (terminated in 50 ohms), 12 nanoseconds or less.
Aberrations, $2 \%$ or less in first 100 nanoseconds following leading edge.
b. Connect the TRIGGER OUTPUT connector to the $1 \mathrm{M} \Omega$ external trigger input connector of the sampling system through a 50 -ohm BNC cable and a 50 -ohm BNC termination.
c. Connect the OUTPUT (HI AMPLITUDE) connector to the sampling-system vertical input through a $10 \times$ GR attenuator, five-nanosecond GR cable, 60-nanosecond delay line and the VP-2 voltage pickoff to the P6038 sampling probe. Terminate the output of the VP-2 with a 50 -ohm GR termination. Set the MULTIPLIER control to 10.
d. Set the sampling-system vertical deflection to 200 millivolts/division, time position range switch to one microsecond and magnify the sweep to five nanoseconds/division.
e. Set the triggering and time-position controls for a stable display of the first leading edge.
f. Set the AMPLITUDE (HI AMPLITUDE) control for a fivedivision display.
g. CHECK-Sampling system display for 2.4 divisions or less between the $10 \%$ and $90 \%$ points of the leading edge (12 nanoseconds or less; see Fig. 5-3A).
h. Set the sampling system sweep rate to 50 nanoseconds/ division and the vertical deflection to 20 millivolts/division. Reposition the top of the waveform onto the viewing area with the DC offset control.
i. CHECK—Sampling system display for aberrations $\pm$ one division or less in first two divisions following the leading edge ( $\pm 2 \%$ or less in first 100 nanoseconds; see Fig. 5-3B).


Fig. 5-2. Typical test oscilloscope display when checking TRIGGER OUTPUT; (A) amplitude, (B) risetime, (C) delay time.

## 7. Check + Fast Rise Output

a. REQUIREMENT-Minimum amplitude, 50 millivolts or less.

Maximum amplitude, 500 millivolts or more.

Risetime, one nanosecond or less.
Aberrations, + and $-2 \%$ or less in first five nanoseconds following leading edge.
b. Disconnect the five-nanosecond GR cable from the $10 \times$ attenuator and connect it to the + OUTPUT connector.
c. Set the HI AMPLITUDE - FAST RISE switch to FAST RISE.
d. Set the sampling system sweep rate to 10 nanoseconds/ division.
e. CHECK-Sampling system display for 2.5 division or less amplitude ( 50 millivolts or less).
f. Set the sampling system vertical deflection to 100 millivolts/division.
g. Set the + TRANSITION AMPLITUDE control fully clockwise.
h. CHECK-Sampling system display for five division or more amplitude ( 500 millivolts or more).
i. Set the + TRANSITION AMPLITUDE control for five divisions of vertical deflection.
i. Set the sampling-system time position range switch to 100 nanoseconds and magnify the sweep to one nanosecond/ division.
k. CHECK-Sampling system display for one division or less between the $10 \%$ and $90 \%$ points of the leading edge (one nanosecond or less; see Fig. 5-4A).
I. Set the sampling system vertical deflection to 10 millivolts/division. Reposition the top of the waveform onto the viewing area with the DC offset control.
m. CHECK—Sampling system display for aberrations $\pm$ one division or less in first five divisions following the leading edge $(+$ and $-2 \%$ or less in first five nanoseconds; see Fig. 5-4B).

## 8. Check - Fast Rise Output

a. REQUIREMENT-Minimum amplitude, 50 millivolts or less.

Maximum amplitude, 500 millivolts or more.

Risetime, one nanosecond or less.
Aberrations, + and $-2 \%$ or less in first five nanoseconds following leading edge.
b. Disconnect the five-nanosecond cable from the + OUTPUT connector and connect it to the - OUTPUT connector.
c. Set the sampling-system vertical deflection to 20 millivolts/division and the sweep rate to 10 nanoseconds/ division.
d. CHECK—Sampling system display for 2.5 division or less amplitude ( 50 millivolts or less).
e. Set the sampling system vertical deflection to 100 millivolts/division.
f. Set the - TRANSITION AMPLITUDE control fully clockwise.


Fig. 5-3. Typical sampling system display when checking OUTPUT (HI AMPLITUDE), (A) risetime, (B) aberrations in first 100 nanoseconds.


Fig. 5-4. Typical sampling system display when checking + OUTPUT; (A) risetime, (B) aberrations in first five nanoseconds.


Fig. 5-5. Typical sampling system display when checking - OUTPUT; (A) risetime, (B) aberrations in first five narroseconds.


Fig. 5-6. Typical sampling system display of irigger iitfer.
g. CHECK—Sampling system display for five division or more amplitude ( 500 millivolts or more).
h. Set the - TRANSITION AMPLITUDE control for five divisions of vertical deflection.
i. Set the sampling system time position range switch to 100 nanoseconds and magnify the sweep to one nanosecond/ division.
i. CHECK—Sampling system display for one division or less between the $10 \%$ and $90 \%$ points of the leading edge (one nanosecond or less; see Fig. 5-5A).
k. Set the sampling system vertical deflection to 10 millivolts/division. Reposition the top of the waveform onto the viewing area with the DC offset control.
I. CHECK—Sampling system display for aberrations $\pm$ one division or less in first five divisions following the leading edge ( + and $-2 \%$ or less in first five nanoseconds; see Fig. 5-5B).

## 9. Check Trigger Jitfer

a. REQUIREMENT-300 picoseconds or less.
b. Set the sampling system to magnify the sweep rate to 0.2 nanosecond/division and set the triggering controls for a stable display. Set the sampling system vertical deflection to 100 millivolts/division.
c. CHECK—Rotate the MULTIPLIER control throughout its range and check for 1.5 division or less jitter in the leading edge of the waveform ( 300 picoseconds or less; see Fig. 5-6).
d. Remove the five-nanosecond cable from the - OUTPUT connector and connect it to the + OUTPUT connector.
e. CHECK-Rotate the MULTIPLIER control throughout its range and check for 1.5 divisions or less jitter in the leading edge of the waveform ( 300 picoseconds or less).
f. Disconnect all test equipment.

This completes the performance check procedure for the Type 106. If the instrument has met all performance requirements given in this procedure, it is correctly calibrated and within the specified tolerances.

## SECTION 6

## CALIBRATION

## Introduction

Complete calibration information for the Type 106 is given in this section. This procedure calibrates the instrument to the performance requirements listed in the Characteristics section. The Type 106 can be returned to original performance standards by completion of each step in this procedure. If it is desired to merely touch up the calibration, perform only those steps entitled Adjust . . (D. A short-form calibration procedure is also provided in this section for the convenience of the experienced calibrator. The short-form procedure may be used as a calibration record or an index to the steps in the complete Calibration Procedure.

The Type 106 should be checked, and recalibrated if necessary, after each 500 hours of operation, or every six months if used infrequently, to assure correct operation and accuracy. The Performance Check section of this manual provides a complete check of instrument performance without making internal adjustments. Use the performance check procedure to verify the calibration of the Type 106 and determine if recalibration is required.

## EQUIPMENT REQUIRED

## General

The following equipment, or its equivalent, is required for complete calibration of the Type 106 (see Figs. 6-1 and 6-2). Specifications given are the minimum necessary for accurate calibration of this instrument. All test equipment is assumed to be correctly calibrated and operating within the given specifications. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

1. Variable autotransformer. Must be capable of supplying 200 volt-amperes over a range of 103.5 to 126.5 volts (207 to 253 volts for 230 -volt nominal line). (If autotransformer does not have an AC voltmeter to indicate output voltage, monitor output with an AC voltmeter with range of at least 135 or 270 volts, RMS). For example, General Radio WIOMT3W Metered Variac Autotransformer.
2. DC voltmeter. Minimum sensitivity, 20,000 ohms/volt; accuracy, checked to within $\pm 1 \%$ at $-150,-10,+10$ and +150 volts; range, 0 to 350 volts. For example, Simpson Model 262.
3. Test oscilloscope. Frequency response, DC to 30 MHz ; minimum deflection factor, 20 millivolts/division; accuracy, within $\pm 3 \%$; must have 1 kHz amplitude calibrator output voltages of 1,5 and 50 volts and a dual-trace vertical system. Tektronix Type 545B Oscilloscope with Type 1A2 Dual-Trace Plug-In Unit recommended.
4. $10 \times$ probe with BNC connector. Tektronix P6008 Probe recommended.
5. Sampling oscilloscope. Risetime, 0.35 nanoseconds; calibrated deflection factor, 20 millivolts/division minimum; calibrated sweep range, equivalent to 100 nanoseconds/division to 0.2 nanosecond/division. Tektronix Type 661 Oscilloscope with Type 4S3 Sampling-Probe Dual-Trace Unit and Type 5 T3 Timing Unit recommended.
6. Delay cable. Impedance, 50 ohms; electrical length, 60 nanoseconds; connectors, GR874. Tektronix Type 113 Delay Cable recommended.
7. Time-mark generator. Marker outputs, 1 microsecond to 1 second; marker accuracy, within $0.1 \%$. Tektronix Type 184 Time-Mark Generator recommended.
8. Cable. Impedance, 50 ohms; type RG-213/U; electrical length, five nanoseconds; connectors, GR874. Tektronix Part No. 017-0502-00.
9. Thru-line termination. Impedance, 50 ohms; wattage rating, 1.0 watts; accuracy, $\pm 3 \%$; connectors, GR874 input with BNC female output. Tektronix Part No. 017-0083-00.
10. Adapter. Connector, GR874 and BNC female. Tektronix Part No. 017-0063-00.
11. Cable (two). Impedance, 50 ohms; type, RG-58A/U; length, 42 inches; connectors, BNC. Tektronix Part No. 012-0057-01.
12. Termination. Impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, BNC. Tektronix Part No. 011-0049-00.
13. BNC T connector. Tektronix Part No. 103-0030-00.
14. Attenuator. Attenuation, $10 \times$; impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, GR874. Tektronix Part No. 017-0078-00.
15. VP-2 Voltage Pickoff. Tektronix Part No. 017-0077-00.
16. End-line termination. Impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, GR874. Tektronix Part No. 017-0081-00.
17. Insulated screwdriver. $11 / 2$-inch shaft, non-metallic. Tektronix Part No. 003-0000-00.
18. Screwdriver. 3-inch shaft. Tektronix Part No. 003-0192-00.

## CALIBRATION RECORD AND INDEX

This short-form calibration procedure is provided to aid in checking the operation of the Type 106. It may be used as a calibration guide by the experienced calibrator, or it may be used as a record of calibration. Since the step numbers and titles used here correspond to those used in the complete procedure, this procedure also serves as an index to


Fig. 6-1. Recommended calibration equipment. Items 1 through 12


(16)

(17)

(18)

Fig. 6-2. Recommended calibration equipment. Items 13 through 18.
locate a step in the complete Calibration Procedure. Performance requirements correspond to those given in the Characteristics section.

## Type 106, Serial No.

## Calibration Date

$\qquad$

## Calibration Technician

1. Adjust Amplitude Cal. Page 6-5.

12 -volts output amplitude or greater.2. Check Amplitude Control Range. Page 6-5.
0.5 volt or less, minimum, termination in 50 ohms. 7 volts or less to 120 volts or greater, unterminated.3. Check $A+150, A-150, A-20,+10$ and -10 Volt Power. Supplies. Page 6-6.
A +150 -Volt supply $\quad+150$ volts, $\pm 15$ volts
A -150 -Volt supply -150 volts, $\pm 15$ volts
A - 20-Volt supply $\quad-20$ volts, $\pm 2$ volts
+10 -Volt supply $\quad+10$ volts, $\pm 1.5$ volts
-10 -Volt supply $\quad-10$ volts, $\pm 1.5$ volts
4. Check A Supply Regulation. Page 6-6.

12-volt output amplitude (terminated in 50 ohms) $\pm 1.2$ divisions.
5. Check $A+150, A-150, A-20,+10$ and -10 Volt Supply Regulation. Page 6-7.

$$
\begin{array}{ll}
\text { A }+150 \text {-Volt supply } & \text { Within } \pm 15 \text { volts } \\
\text { A }-150 \text {-Volt supply } & \text { Within } \pm 15 \text { volts } \\
\text { A }-20 \text {-Volt-supply } & \text { Within } \pm 2 \text { volts } \\
+10 \text {-Volt supply } & \text { Within } \pm 1.5 \text { volt } \\
-10 \text {-Volt supply } & \text { Within } \pm 1.5 \text { volt }
\end{array}
$$

6. Check Power-Supply Ripple. Page 6-8.

| A supply | $\pm 0.75$ volt, peak to peak |
| :--- | :--- |
| A +150 -Volt supply | $\pm 0.75$ volt, peak to peak |
| A -150 -Volt supply | $\pm 0.75$ volt, peak to peak |
| A -20 -Volt supply | $\pm 0.75$ volt, peak to peak |
| +10 -Volt supply | $\pm 0.2$ volt, peak to peak |
| - 10 -Volt supply | $\pm 0.2$ volt, peak to peak |7. Adjust Symmetry Range. Page 6-10.

$45 \%$ to $55 \%$ change in duty cycle.8. Adjust Repetition Rate Multiplier. Page 6-11. Correct repetition rate at 1 and 10 . Correct knob position at 5.9. Adjust Bias Level. Page 6-12.
$50 \%$ duty cycle at 1 MHz .10. Check Repetition Rate Accuracy. Page 6-12. Within $\pm 10 \%$ of indicated repetition rate.11. Check Synchronized Operation. Page 6-12. Output signals synchronize with 5 and 50 volt input square wave.

## Calibration-Type

12. Check Trigger Output. Page 6-13.Amplitude, 0.1 volt.
Risetime, 50 nanoseconds or less, between 0 and 0.1 volt.
Delay time, 50 nanoseconds or less.13. Check Hi Amplitude Output Into 50 Ohms. Page 6-14.
Risetime (terminated in 50 ohms), 12 nanoseconds or less.
Aberrations, $\pm 2 \%$ or less in first 100 nanoseconds following leading edge.14. Adjust + Fast Rise Output and Check Operation. Page 6-14.
Minimum amplitude, 50 millivolts or less.
Maximum amplitude, 500 millivolts or more.
Risetime and aberrations, adjust for one nanosecond or less risetime with aberrations + and $-2 \%$ or less in first five nanoseconds following leading edge.15. Adjust - Fast Rise Output and Check Operation. Page 6-16.
Minimum amplitude, 50 millivolts or less.
Maximum amplitude, 500 millivolts or more.
Risetime and aberrations, adjust for one nanosecond or less risetime with aberrations + and $-2 \%$ or less in first five nanoseconds following leading edge.16. Check Trigger Jitter. Page 6-17.

300 picoseconds or less jitter in leading edge of + and - output square waves.

## CALIBRATION PROCEDURE

## General

The following procedure is arranged in a sequence which allows the Type 106 to be calibrated with the least interaction of adjustments and reconnection of equipment. However, some adjustments affect the calibration of other circuits within the instrument. In this case, it will be necessary to check the operation of other parts of the instrument. When a step interacts with others, the steps which need to be checked will be noted.

Any needed maintenance should be performed before proceeding with calibration. Troubles which become apparent during calibration should be corrected using the techniques given in the Maintenance section.

The Adjust . . . (1) steps in the following procedure provide a check of instrument performance, whenever possible, before the adjustment is made. The symbol (1) is used to identify the steps in which an adjustment is made. To prevent recalibration of other circuits when performing a partial calibration, readjust only if the listed tolerance is not met. However, when performing a complete calibration, best overall performance will be provided if each adjustment is made to the exact setting, even if the check is within the allowable tolerance.

In the following procedure, a test equipment setup picture is shown for each major group of adjustments and checks. Beneath each setup picture is a complete list of front-panel control settings for the Type 106. To aid in locating individual controls which have been changed during complete calibration, these control names are printed in bold type. If only a partial calibration is performed, start with the nearest setup picture preceding the desired portion. Type 106 frontpanel control titles referred to in this procedure are capitalized (e.g., AMPLITUDE). Internal adjustment titles are initial capitalized only (e.g., Amplitude Cal).

The following procedure uses the equipment listed under Equipment Required. If substitute equipment is used, control settings or setup may need to be altered to meet the requirements of the equipment used.

## Preliminary Procedure

1. Remove the cabinet from the Type 106.
2. Connect the autotransformer to a suitable power source.
3. Connect the Type 106 to the autotransformer output.
4. Set the autotransformer output voltage to 115 (or 230 volts).
5. Set the Type 106 POWER switch to ON. Allow at least five minutes warm up at $25^{\circ} \mathrm{C}, \pm 5^{\circ}$, before checking the instrument to the given accuracy.

## NOTES

- 
- 


## MAINTENANCE NOTE

CALIBRATION ADDENDUM
TYPE 106

Section 6 Calibration
Page 6-5 Step 1
CHANGE: Steps $1(d)$ and $I(e)$ to read:
d. CHECK--Test oscilloscope display amplitude for six divisions or greater (12 volts or greater, see Fig. 6-4A).
e. ADJUST--Amplitude Cal adjustment, R247 (see Fig. 6-4B) for a compromise setting to bring the terminated and unterminated voltage ranges within limits.

Page 6-9 Fig. 6-7.
CHANGE: Figure title to read:
Fig. 6-7. Typical test oscilloscope display of power-supply ripple (60-cycle line). Sweep rate, 5 milliseconds/division; vertical deflection, 0.2 volt/ division ( 0.02 volt/division with lox probe).

This insert is placed in its appropriate position in your Product Reference Book and printed on colored paper to expedite retrieval. In a standard manual, it will be filed at the back of the manual.


Fig. 6-3. Initial test equipment setup for steps 1 - 5 .

## Front-panel control settings

| REPETITION RATE |  |
| :--- | :--- |
| RANGE | 1 kHz |
| MULTIPLIER | 10 (clockwise) |
| SYMMETRY | Midrange |
| AMPLITUDE | Clockwise |
| HI AMPLITUDE - FAST |  |
| RISE | HI AMPLITUDE |
| + TRANSITION AMPLI- |  |
| TUDE | Midrange |
| - TRANSITION AMPLI- |  |
| TUDE | Midrange |
| POWER | ON |

## 1. Adjust Ampliłude Cal

a. Test equipment setup is shown in Fig. 6-3.
b. Connect the OUTPUT (HI AMPLITUDE) connector to the input of the test oscilloscope through the five-nanosecond GR cable and the 50 -ohm in-line termination.
c. Set the test oscilloscope vertical deflection to two volts/ division, input coupling to DC and the sweep rate to 50 microseconds/division.
d. CHECK—Test oscilloscope display for six divisions/ amplitude, $\pm 0.6$ division, ( 12 volts, $\pm 10 \%$; see Fig. $6-4 \mathrm{~A}$ ).
e. ADJUST—Amplitude Cal adjustment, R247 (see Fig. 6-4B) for exactly six divisions of deflection.
f. INTERACTION—Check all steps.

## 2. Check Amplitude Control Range

a. Turn the AMPLITUDE (HI AMPLITUDE) control fully counterclockwise.
b. Set the test oscilloscope vertical deflection to 0.1 volt/ division.
c. CHECK—Test oscilloscope display for five divisions or less amplitude ( 0.5 volt or less).
d. Remove the 50 -ohm in-line termination and connect the five-nanosecond cable to the test oscilloscope input using the GR-to-BNC adapter.
e. Set the test oscilloscope vertical deflection to two volts/ division.
f. CHECK—Test oscilloscope display for 3.5 divisions or less amplitude (seven volts or less).
g. Turn the AMPLITUDE ( HI AMPLITUDE) control fully clockwise.


Fig. 6-4. (A) Typical rest oscilloscope display when adjusting $A$ Supply oûpuł voliage, (B) location of Amplifude Cal adjusiment (right side).
h. Set the test oscilloscope vertical deflection to 20 volts/ division.
i. CHECK—Test oscilloscope display for 6 divisions or greater amplitude, ( 120 volts or greater).
i. Remove all cable to facilitate the next step.
3. Check $\mathbf{A}+150, \mathrm{~A}-150, \mathrm{~A}-20,+10$ and - 10 Volt Power Supplies
a. Connect the DC voltmeter between TP259 and TP249 (see Fig. 6-5A); connect the negative lead to TP249.
b. CHECK—Meter reading for +150 volts, $\pm 15$ volts.
c. Connect the DC voltmeter between TP229 and TP249 (see Fig. 6-5A); connect the negative lead to TP249.
d. CHECK-Meter reading for -150 volts, $\pm 15$ volts.
e. Connect the DC voltmeter between TP269 and TP249 (see Fig. 6-5A); connect the negative lead to TP249.
f. CHECK—Meter reading for -20 volts, $\pm 2$ volts.
g. Connect the DC voltmeter between the +10 -volt test point (emitter of Q213, see Fig. 6-5B) and chassis ground.
h. CHECK—Meter reading for +10 volts, $\pm 1.5$ volts.
i. Connect the DC voltmeter between the -10 -volt test point (emitter of Q217, see Fig. 6-5B) and chassis ground.
i. CHECK—Meter reading for -10 volts, $\pm 1.5$ volts.

## 4. Check A Supply Regulation

a. Connect the OUTPUT (HI AMPLITUDE) connector to the input of the test oscilloscope through the five-nanosecond GR cable and the 50 -ohm in-line termination.
b. Set the test oscilloscope vertical deflection to two volts/ division.


Fig. 6-5. (A) Location of A Supply, $A+150, A-150$ and $A-20$ volt fest points (right side), (B) location of +10 and -10 volt test points (bołtom side).
c. CHECK—Test oscilloscope display for $\pm 0.6$ division maximum change while varying the autotransformer output voltage between 103.5 and 126.5 volts ( 207 and 253 volts for 230 volts nominal).
5. Check $A+150, A-150, A-20,+10$ and - 10 Volt Supply Regulation
a. Connect the DC voltmeter between TP259 and TP249 (see Fig. 6-5A).
b. CHECK-Meter reading for $\pm 15$ volts maximum change while varying the autotransformer output voltage between 103.5 and 126.5 volts ( 207 and 253 volts for 230 volts nominal).
c. Connect the DC voltmeter between TP229 and TP249 (see Fig. 6-5A).
d. CHECK—Meter reading for $\pm 15$ volts maximum change while varying the autotransformer output voltage between
103.5 and 126.5 volts (207 and 253).
e. Connect the DC voltmeter between TP269 and TP249.
f. CHECK - Meter reading for $\pm 2$ volts maximum change while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).
g. Connect the DC voltmeter between the +10 volt test point (see Fig. 6-5B) and chassis ground.
h. CHECK-Meter reading for $\pm 1.5$ volt maximum change while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).
i. Connect the DC voltmeter between the -10 volt test point (see Fig. 6-5B) and chassis ground.
i. CHECK—Meter reading for $\pm 1.5$ volt maximum change while varying the autotransformer output voltage between 103.5 and 126.5 volts ( 207 and 253).
k. Disconnect all test equipment.

NOTES


Fig. 6-6. Test equipment setup for step 6.

## Front-panel control settings

| REPETITION RATE |  |
| :--- | :--- |
| $\quad$ RANGE | 1 kHz |
| MULTIPLIER | 10 (clockwise) |
| SYMMETRY | Midrange |
| AMPLITUDE | Counterclockwise |
| HI AMPLITUDE - FAST |  |
| $\quad$ RISE | HI AMPLITUDE |
| + TRANSITION AMPLI- | Midrange |
| TUDE |  |
| — TRANSITION AMPLI- | Midrange |
| TUDE | ON |

## 6. Check Power Supply Ripple

a. Test equipment setup is shown in Fig. 6-6.
b. Connect the $10 \times$ probe to the test oscilloscope input connector.
c. Set the test oscilloscope for a vertical deflection of 0.02 volt/division, AC coupled, at a sweep rate of five milliseconds/division.
d. Connect the probe tip to TP249 (see Fig. 6-5A). Connect the probe ground lead to chassis ground.
e. CHECK—Test oscilloscope display for 3.75 divisions maximum line-frequency ripple ( $\pm 0.75$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts ( 207 and 253 volts for 230 volts nominal). Fig. 6-7 shows a typical test oscilloscope display of power supply ripple.
f. Connect the probe tip to TP259 (see Fig. 6-5A). Connect the probe ground lead to chassis ground.
g. CHECK—Test oscilloscope display for 3.5 divisions maximum line-frequency ripple ( $\pm 0.75$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).
h. Connect the probe tip to TP229 (see Fig. 6-5A). Connect the probe ground lead to chassis ground.
i. CHECK—Test oscilloscope display for 3.5 divisions maximum line-frequency ripple ( $\pm 0.75$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).
j. Connect the probe tip to TP269 (see Fig. 6-5A). Connect the probe ground lead to chassis ground.
k. CHECK—Test oscilloscope display for 3.5 divisions maximum line-frequency ripple ( $\pm 0.75$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).


Fig. 6-6. Test equipment setup for step 6.

## Front-panel control settings

| REPETITION RATE |  |
| :--- | :--- |
| RANGE | 1 kHz |
| MULTIPLIER | 10 (clockwise) |
| SYMMETRY | Midrange |
| AMPLITUDE | Counterclockwise |
| HI AMPLITUDE - FAST |  |
| RISE | HI AMPLITUDE |
| + TRANSITION AMPLI- |  |
| TUNE | Midrange |
| - TRANSITION AMPLI- |  |
| TUNE | Midrange |
| POWER | ON |

## 6. Check Power Supply Ripple

a. Test equipment setup is shown in Fig. 6-6.
b. Connect the $10 \times$ probe to the test oscilloscope input connector.
c. Set the test oscilloscope for a vertical deflection of 0.02 volt/division, AC coupled, at a sweep rate of five milliseconds/division.
d. Connect the probe tip to TP249 (see Fig. 6-5A). Conneat the probe ground lead to chassis ground.
e. CHECK—Test oscilloscope display for 3.5 divisions maximum line-frequency ripple ( $\pm 0.75$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts ( 207 and 253 volts for 230 volts nominal). Fig. 6-7 shows a typical test oscilloscope display of power supply ripple.
f. Connect the probe tip to TP259 (see Fig. 6-5A). Conneat the probe ground lead to chassis ground.
g. CHECK—Test oscilloscope display for 3.5 divisions maximum line-frequency ripple ( $\pm 0.75$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).
h. Connect the probe tip to TP229 (see Fig. 6-5A). Connest the probe ground lead to chassis ground.
i. CHECK—Test oscilloscope display for 3.5 divisions maximum line-frequency ripple ( $\pm 0.75$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).
i. Connect the probe tip to TP269 (see Fig. 6-5A). Conneat the probe ground lead to chassis ground.
k. CHECK-Test oscilloscope display for 3.5 divisions maximum line-frequency ripple ( $\pm 0.75$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).

I. Connect the probe tip to the +10 volt point (see Fig. 6-5B). Connect the probe ground lead to chassis ground.
m . CHECK-Test oscilloscope display for one division maximum line-frequency ripple ( $\pm 0.2$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).
n. Connect the probe tip to the -10 volt test point (see Fig. 6-5B). Connect the probe ground lead to chassis ground.
o. CHECK-Test oscilloscope display for one division maximum line-frequency ripple ( $\pm 0.2$ volt) while varying the autotransformer output voltage between 103.5 and 126.5 volts (207 and 253).
p. Return the autotransformer output voltage to 115 (230) volts. (If the line voltage is about 115 (230) volts, the Type 106 can be connected directly to the line; otherwise leave the instrument connected to the autotransformer for the remainder of the procedure.)
q. Disconnect all test equipment.


Fig. 6-7. Typical test oscilloscope display of power-supply ripple ( 60 -cycle line). Sweep rate, 5 millisecond/division vertical deflecfion, 0.2 volt/division ( 0.002 volt/division and $10 \times$ probe).

NOTES

## Calibration-Type 106



Fig. 6-8. Inifial test equipment sefup for steps 7 - 12.

## Front-panel control settings

| REPETITION RATE |  |
| :--- | :--- |
| $\quad$ RANGE | 1 kHz |
| MULTIPLIER | 10 (clockwise) |
| SYMMETRY | Midrange |
| AMPLITUDE | Midrange |
| HI AMPLITUDE - FAST <br> RISE |  |
| + TRANSITION AMPLI- |  |
| TUDE | Midrange |
| - TRANSITION AMPLI- |  |
| TUDE | Midrange |
| POWER | ON |

## 7. Adjust Symmetry Range

a. Test equipment setup is shown in Fig. 6-8.
b. Connect the OUTPUT (HI AMPLITUDE) connector to the channel 2 input of the test oscilloscope through the fivenanosecond GR cable and the 50 -ohm in-line termination.
c. Set the test oscilloscope vertical deflection to display about four divisions and the sweep rate to display one complete cycle in 10 divisions (use variable time/division control).
d. CHECK - Test oscilloscope display for five-division duration of the positive portion of the square wave ( $50 \%$ duty cycle).
e. ADJUST - Symmetry Range adjustment, R9 (see Fig. 6-9A), for five-division duration of the positive portion.
f. Set the SYMMETRY control fully clockwise; reset the time/division controls for one complete cycle in 10 divisions.
g. CHECK—Test oscilloscope display for 5.5 divisions or more duration of the positive portion of the square wave ( $55 \%$ or more; see Fig. 6-9B).
h. Set the SYMMETRY control fully counterclockwise; reset the time/division controls for one complete cycle in 10 divisions.
i. CHECK - Test oscilloscope display for 4.5 division or less duration of the positive portion of the square wave ( $45 \%$ or less; see Fig. 6-9B).
i. Return the SYMMETRY control to midrange.


Fig. 6-9. (A) Location of Symmetry Range adjustment (right side), (B) fypical test oscilloscope display showing correct SYMMETRY control range.

## 8. Adjust Repetition Rate Multiplier

a. Connect the time-mark generator output to the channel 1 input connector of the test oscilloscope through a 50 -ohm BNC cable and a 50 -ohm BNC termination.
b. Set the time-mark generator for one-microsecond markers.
c. Set the AMPLITUDE (HI AMPLITUDE) control fully clockwise.
d. Set the REPETITION RATE RANGE switch to 100 kHz .
e. Set the test oscilloscope vertical deflection to display about two divisions of the signal on each channel in the alternate mode at a sweep rate of one microsecond/division.
f. CHECK - Test oscilloscope display for one cycle for each marker displayed (see Fig. 6-10A).
g. ADJUST - Rep Rate Multiplier Cal $(\times 10)$ adjustment, R6 (see Fig. 6-10B), for one cycle for each marker displayed.
h. Set the MULTIPLIER control fully counterclockwise to 1 .


Fig. 6-10. (A) Typical test oscilloscope display when adjusting repetition rate multiplier, (B) location of repetition rate multiplier (bottom side).
i. Set the test oscilloscope sweep rate to 10 microseconds/division.
j. Set the time-mark generator for 10 microsecond markers.
k. CHECK - Test oscilloscope display for one cycle for each marker displayed (see Fig. 6-10A).
I. ADJUST - Rep Rate Multiplier Cal ( $\times 1$ ) adjustment, R30 (see Fig. 6-10B), for one cycle for each marker displayed.
m . Recheck steps b through | as necessary for correct repetition rate.
n. Set the test oscilloscope sweep rate to 2 microseconds/ division.
o. Set the time-mark generator for one microsecond markers.
p. Set the MULTIPLIER control for exactly one cycle for each two markers displayed.
q. CHECK—MULTIPLIER control should be at 5 .
r. ADJUST-Loosen set screw in MULTIPLIER knob and reposition for correct indication.


Fig. 6-11. (A) Typical test oscilloscope display when adjusting bias level, ( $B$ ) location of bias level adjustment (right side).

## 9. Adjust Bias Level

a. Set the MULTIPLIER control fully clockwise.
b. Set the test oscilloscope sweep rate to $0.1 \mu \mathrm{~s} /$ division and the vertical mode switch to channel 2.
c. CHECK—Test oscilloscope display for $50 \%$ duty cycle (see Fig. 6-11A).
d. ADJUST-Bias Level adjustment R39 (see Fig. 6-11B) for 50\% duty cycle.
e. Set the REPETITION RATE RANGE switch to 1 kHz .

TABLE 6-1
Repetition Rate Accuracy

| REPETI- <br> TION <br> RATE <br> RANGE <br> Switch <br> Setting | MULTI- <br> PLIER <br> Control <br> Setting | Time <br> Markers <br> Applied | Test <br> Oscillo- <br> scope <br> Sweep <br> Rate | CRT Display <br> (Cycles/ <br> Marker for <br> $\pm 10 \%$ <br> accuracy) |
| :---: | :---: | :---: | :---: | :---: |
| 100 kHz | 10 | $10 \mu \mathrm{~s}$ | $1 \mu \mathrm{~s} /$ div | $9-11$ |
| 100 kHz | 5 | $10 \mu \mathrm{~s}$ | $1 \mu \mathrm{~s} / \mathrm{div}$ | $4.5-5.5$ |
| 10 kHz | 9 | 0.1 ms | $10 \mu \mathrm{~s} / \mathrm{div}$ | $8.1-9.9$ |
| 10 kHz | 4 | 0.1 ms | $10 \mu \mathrm{~s} /$ div | $3.6-4.4$ |
| 1 kHz | 8 | 1 ms | $0.1 \mathrm{~ms} /$ div | $7.2-8.8$ |
| 1 kHz | 3 | 1 ms | $0.1 \mathrm{~ms} /$ div | $2.7-3.3$ |
| 100 Hz | 7 | 10 ms | $1 \mathrm{~ms} /$ div | $6.3-7.7$ |
| 100 Hz | 2 | 10 ms | $1 \mathrm{~ms} / \mathrm{div}$ | $1.8-2.3$ |
| 10 Hz | 6 | 0.1 s | $10 \mathrm{~ms} / \operatorname{div}$ | $5.4-6.6$ |
| 10 Hz | 1 | 0.1 s | $10 \mathrm{~ms} / \mathrm{div}$ | $0.9-1.1$ |



Fig. 6-12. Typical test oscilloscope display when checking TRIGGER OUTPUT. (A) Amplitude, (B) risetime, (C) delay time.
f. Set the test oscilloscope sweep rate to $10 \mu \mathrm{~s} /$ division.
g. CHECK—Test oscilloscope display for $50 \%$ duty cycle.
h. ADJUST—Bias level adjustment, R39 for $50 \%$ duty cycle.
i. Recheck steps a through h. A compromise setting may be necessary to provide best duty cycle for both checks c and g .

## 10. Check Repetition Rate Accuracy

a. Set the test oscilloscope vertical Mode switch to Alt.
b. CHECK—Using the Type 106, time-mark generator and test oscilloscope settings given in Table 6-1, check repetition rate accuracy within $\pm 10 \%$.
c. Disconnect all test equipment.

## 11. Check Synchronized Operation

a. Connect the test oscilloscope amplitude calibrator to both the SYNC INPUT connector and the channel 1 input connector through a BNC T connector and two 50 -ohm BNC cables.
b. Connect the OUTPUT (HI AMPLITUDE) connector to the channel 2 input connector through a five nanosecond GR cable and a 50 -ohm in-line termination.
c. Set the REPETITION RATE RANGE switch to 100 Hz and the MULTIPLIER control to about 7.
d. Set the test oscilloscope amplitude calibrator for five volts output and the sweep rate to 0.5 millisecond/division.
e. Set the test oscilloscope to trigger from channel 1 in the chopped mode.
f. CHECK - Test oscilloscope for stable display of the channel 2 waveform (readjust the MULTIPLIER control if necessary).
g. Set the test oscilloscope amplitude calibrator for 50 volts output.
h. CHECK - Test oscilloscope for a stable display of the channel 2 waveform.
i. Set the test oscilloscope amplitude calibrator for one volt output.
i. CHECK - Test oscilloscope display for drift of the channel 2 waveform due to inadequate sync signal.
k. Disconnect all test equipment.

## 12. Check Trigger Oułpuł

a. Connect the TRIGGER OUTPUT connector to the channel 2 input connector of the test oscilloscope through a 50 ohm BNC cable and a 50 -ohm BNC termination.
b. Connect the OUTPUT (HI AMPLITUDE) connector to the channel 1 input connector of the test oscilloscope through a 50 -ohm GR cable and a 50 -ohm in-line termination.
c. Set the test oscilloscope to display the channel 2 signal at a vertical deflection of 0.1 volt/division and the channel 1 signal at a vertical deflection of 5 volts/division and a sweep rate of 10 microseconds/division.
d. Set the REPETITION RATE RANGE switch to 100 kHz and the MULTIPLIER control to 1 .
e. CHECK - Test oscilloscope display for positive and negative pulse amplitude of 1 division minimum ( 0.1 volt peak minimum; see Fig. 6-12A).
f. Set the test oscilloscope for a vertical deflection of 0.2 volt/division at a sweep rate of 50 nanoseconds/division (use magnifier).
g. Position the display to observe the leading edge of the positive pulse.
h. CHECK - Test oscilloscope display for one division or less between the 0 and 0.1 volt level of the trigger pulse ( 50 nanoseconds or less; see Fig. 6-12B).
i. Set the test oscilloscope to trigger from channel 1 in the alternate mode.
i. Position the $50 \%$ points of both waveforms to the horizontal centerline.
k. CHECK - Test oscilloscope display for one division or less spacing between the $50 \%$ amplitude points of the two waveforms ( 50 nanoseconds or less; see Fig. 6-12C).
I. Disconnect all test equipment.

## NOTES



Fig. 6-13. Inifial test equipmenł sełup for steps $13-16$.

## Front-panel control settings

| REPETITION RATE | 100 kHz |
| :--- | :--- |
| RANGE |  |
| MULTIPLIER | 10 (clockwise) |
| SYMMETRY | Midrange |
| AMPLITUDE | Midrange |
| HI AMPLITUDE - <br> FAST RISE | HI AMPLITUDE |
| + TRANSITION AMPLI- | Midrange |
| TUDE | MRANSITION AMPLI- |
| TUDE | Midrange |
| POWER | ON |

## 13. Check Hi Amplitude Output Into 50 Ohms

a. Test equipment setup is shown in Fig. 6-13.
b. Connect the TRIGGER OUTPUT connector to the $1 \mathrm{M} \Omega$ external trigger input connector of the sampling system through a 50 -ohm BNC cable and a 50 -ohm BNC termination.
c. Connect the OUTPUT (HI AMPLITUDE) connector to the sampling system vertical input through a $10 \times$ GR attenuator, five-nanosecond GR cable, 60-nanosecond delay line and the VP-2 voltage pickoff to the P6038 sampling
probe. Terminate the output of the VP-2 with a 50 -ohm GR termination.
d. Set the sampling system vertical deflection to 200 millivolts/division, time position range switch to one microsecond and magnify the sweep to five nanosecond/division.
e. Set the triggering and time position controls for a stable display of the first leading edge.
f. Set the AMPLITUDE (HI AMPLITUDE) control for a five division display.
g. CHECK - Sampling system display for 2.4 divisions or less betwen the $10 \%$ and $90 \%$ points of the leading edge (12 nanoseconds or less; see Fig. 6-14A).
h. Set the sampling system sweep rate to 50 nanoseconds/ division and the vertical deflection to 20 millivolts/division. Reposition the top of the waveform onto the viewing area with the DC offset control.
i. CHECK—Sampling system display for aberrations $\pm$ one division or less in first two divisions following the leading edge ( $\pm 2 \%$ or less in first 100 nanoseconds; see Fig. 614B).
14. Adjust + Fast Rise Output and Check Operation
a. Disconnect the five-nanosecond GR cable from the $10 \times$ attenuator and connect it to the + OUTPUT connector.
b. Set the HI AMPLITUDE - FAST RISE switch to FAST RISE.


Fig. 6-14. Typical sampling system display when checking OUTPUT (HI AMPLITUDE), (A) risetime, (B) aberrations in first 100 nanoseconds.


Fig. 6-15. Typical sampling system display when checking + OUTPUT; (A) minimum amplifude, (B) maximum ampliłude, (C) risetime and aberrations. (D) Location of C107 and C118 (bottom side).


Fig. 6-16. Typical sampling system display when checking - OUTPUT; (A) minimum amplifude, (B) maximum amplifude, (C) risetime and aberrations, (D) location of C127 and C138 (bottom side).
c. Set the sampling-system sweep rate to 10 nanoseconds/ division.
d. Set the + TRANSITION AMPLITUDE control fully counterclockwise.
e. CHECK—Sampling system display for 2.5 divisions or less amplitude ( 50 millivolts or less; see Fig. 6-15A).
f. Set the sampling system vertical deflection to 100 millivolts/division.
g. Set the + TRANSITION AMPLITUDE control fully clockwise.
h. CHECK - Sampling system display for five divisions or more amplitude ( 500 millivolts or more; see Fig. 6-15B).
i. Set the + TRANSITION AMPLITUDE control for five divisions of vertical deflection.
i. Set the sampling system time position range switch to 100 nanoseconds and magnify the sweep to one nanosecond/ division.
k. CHECK - Sampling system display for one division or less between the $10 \%$ and $90 \%$ points of the leading edge with $\pm 0.1$ division or less aberrations in the first five divi-
sions following the leading edge one nanosecond or less risetime with $\pm 2 \%$ or less aberrations in first five nanoseconds; see Fig. 6-15C).
I. ADJUST-C107 and C118 (see Fig. 6-15D) for optimum risetime and square corner at the top of the leading edge of the waveform. A compromise setting may be necessary to obtain one-nanosecond risetime with + and $-2 \%$ or less aberrations.

## 15. Adjust - Fast Rise Output and Check Operation

a. Remove the five-nanosecond cable from the + OUTPUT connector and connect it to the - OUTPUT connector.
b. Set the sampling system vertical deflection to 20 millivolts/division and the sweep rate to 10 nanoseconds/division.
c. Set the - TRANSITION AMPLITUDE control fully counterclockwise.
d. CHECK—Sampling system display for 2.5 divisions or less amplitude ( 50 millivolts or less; see Fig. 6-16A).
e. Set the sampling system vertical deflection to 100 millivolts/division.
f. Set the - TRANSITION AMPLITUDE control fully clockwise.
g. CHECK-Sampling system display for five divisions or more amplitude ( 500 millivolts or more; see Fig. 6-16B).
$h$. Set the - TRANSITION AMPLITUDE control for five divisions of vertical deflection.
i. Set the sampling system time position range switch to 100 nanoseconds and magnify the sweep to one nanosecond/division.
j. CHECK - Sampling system display for one division or less between the $10 \%$ and $90 \%$ points of the leading edge with $\pm 0.1$ division or less aberrations in the first five divisions following the leading edge (one nanosecond or less risetime with $\pm 2 \%$ or less aberrations in first five nanoseconds; see Fig. 6-16C).
k. ADJUST- Cl 27 and Cl 38 (see Fig. 6-16D) for optimum risetime and square corner at bottom of the leading edge of the waveform. A compromise setting may be necessary to obtain one-nanosecond risetime with + and $-2 \%$ or less aberrations.

## 16. Check Trigger Jitter

a. Insert the Type 106 into the cabinet.
b. Set the sampling system to magnify the sweep rate to 0.2 nanosecond/division and set the triggering controls for a stable display.
c. CHECK - Rotate the MULTIPLIER control throughout its range and check for 1.5 divisions or less jitter in the leading edge of the waveform ( 300 picoseconds or less; see Fig. 6-17).


Fig. 6-17. Typical sampling system display of trigger jitter.
d. Remove the five-nanosecond cable from the - OUTPUT connector and connect it to the + OUTPUT connector.
e. CHECK - Rotate the MULTIPLIER control throughout its range and check for 1.5 divisions or less jitter in the leading edge of the waveform ( 300 picoseconds or less).
f. Disconnect all test equipment.

This completes the calibration procedure for the Type 106. If the instrument has been completely calibrated to the tolerances given in this procedure, it will meet the performance requirements given in the Characteristics section of this Instruction Manual.

# SECTION 7 ELECTRICAL PARTS LIST 

Values are fixed unless marked Variable.

| Ckt. No. | Tektronix <br> Part No. | Description | S/N Range |
| :--- | ---: | :--- | ---: |
|  |  |  | Bulbs |
| B15 |  |  |  |
| B25 | $150-0027-00$ | Neon, NE-23 |  |
| B219 | $150-0027-00$ | Neon, NE-23 |  |
| B219 | $150-0052-00$ | Incandescent, $10 \mathrm{~V}, 40 \mathrm{~mA}$ (white lens) | $200-1169$ |
|  | $150-0065-00$ | Incandescent, $10 \mathrm{~V}, 40 \mathrm{~mA}$ (green lens) | $1170-\mathrm{up}$ |

## Capacitors

Tolerance $\pm 20 \%$ unless otherwise indicated.

†Only one $10 \mu \mathrm{~F}$ section is utilized.

${ }^{1}$ See Mechanical Parts List.

Diodes (Cont)
Tektronix
Ckt. No.
Part No.
Description

| D212 | 152-0199-00 | Rectifier bridge MDA 962-3 (Motorola) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| D213 | 152-0120-00 | Zener | 1N3020B | $1 \mathrm{~W}, 10 \mathrm{~V}, 5 \%$ |
| D216 | 152-0120-00 | Zener | 1N3020B | $1 \mathrm{~W}, 10 \mathrm{~V}, 5 \%$ |
| D222 | 152-0232-00 | Rectifier bridge assembly |  |  |
| D224 | 152-0101-00 | Zener | 1N3041B | $1 \mathrm{~W}, 75 \mathrm{~V}, 5 \%$ |
| D232 | 152-0232-00 | Rectifier bridge assembly |  |  |
| D233 | *152-0185-00 | Silicon | Replaceable | by IN3605 |
| D234 | *152-0185-00 | Silicon | Replaceable | by 1 N 3605 |
| D243 | *152-0185-00 | Silicon | Replaceable by | by IN3605 |
| D252 | 152-0232-00 | Rectifier bridge assembly |  |  |
| D255 | 152-0240-00 | Zener | UZ 5215 | $5 \mathrm{~W}, 150 \mathrm{~V}, 10 \%$ |
| D262 | 152-0199-00 | Rectifier bridge MDA 962 | 2-3 (Motorola) |  |
| D264 | 152-0060-00 | Zener | 1N3027A | $1 \mathrm{~W}, 20 \mathrm{~V}, 10 \%$ |

## Fuse

F201 159-0041-00 1.25 A, 3 AG, Slo-Blo

## Inductors

*131-0102-00
3 wire, male

## Plug

$* 108-0057-00$
$* 108-0057-00$
$276-0507-00$
$276-0507-00$
$276-0507-00$

$276-0507-00$
$276-0507-00$
$276-0507-00$
$8.8 \mu \mathrm{H}$
$\begin{array}{rl}* 108-0057-00 & 8.8 \mu \mathrm{H} \\ 276-0507-00 & \text { Core, Fer }\end{array}$
$\begin{array}{ll}\text { Core, Ferramic Suppressor } & \text { X635-up } \\ \text { Core, Ferramic Suppressor } & \text { X635-up }\end{array}$ X635-up
Core, Ferramic Suppressor
X635-up

X635-up
X635-up
X635-up

## Transistors

| *151-0195-00 | Silicon |
| ---: | :--- |
| 151-0169-00 | Silicon |
| *151-0108-00 | Silicon |
| $151-0190-00$ | Silicon |
| $151-0190-00$ | Silicon |

Replaceable by MPS 6515
2N3439
$\begin{array}{lr}\text { Replaceable by } 2 \mathrm{~N} 2501 & 200-634 \\ 2 \mathrm{~N} 3904 & 635-\mathrm{up} \\ 2 \mathrm{~N} 3904 & \end{array}$

2N3904
Replaceable by 2N2501 200-1189
2N4275
Selected from 2N3546
1190-up
200-1189
2N4258

Transistors (Cont)

| Ckt. No. | Tektronix Part No. |  | Description | S/N Range |
| :---: | :---: | :---: | :---: | :---: |
| Q115 | 151-0188-00 | Silicon | 2N3906 | X1190-up |
| Q124 | *151-0108-00 | Silicon | Replaceable by 2N2501 |  |
| Q134 | *151-0109-00 | Silicon | Selected from 2N918 | 200-929 |
| Q134 | *151-0223-00 | Silicon | 2N4275 | 930-up |
| Q135 | 151-0190-00 | Silicon | 2N3904 | X1190-up |
| Q213 | *151-0136-00 | Silicon | Replaceable by 2 N 3053 |  |
| Q217 | *151-0134-00 | Silicon | Replaceable by 2 N 2905 | 200-679 |
| Q217 | 151-0208-00 | Silicon | 2N4036 | 680-up |
| Q224 | 151-0150-00 | Silicon | 2N3440 |  |
| Q227 | 151-0150-00 | Silicon | 2N3440 |  |
| Q233 | *151-0136-00 | Silicon | Replaceable by 2 N 3053 |  |
| Q234 | 151-0150-00 | Silicon | 2N3440 |  |
| Q247 | *151-0196-00 | Silicon | Replaceable by 40256 | 200-777 |
| Q247 | 151-0201-00 | Silicon | 2N3739 | 778-1354 |
| Q247 | 151-0251-00 | Silicon | 2N4240 | 1355-up |
| Q257 | 151-0149-00 | Silicon | 2N3441 |  |
| Q267 | *151-0136-00 | Silicon | Replaceable by 2 N 3053 |  |

## Resistors

Resistors are fixed, composition, $\pm 10 \%$ unless otherwise indicated.

| R1 | 302-0105-00 | $1 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R2 | 315-0473-00 | $47 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R3 | 315-0104-00 | $100 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R4 | 315-0152-00 | $1.5 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R5 | 301-0275-00 | $2.7 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% | X698-up |
| R6 | 311-0408-00 | $20 \mathrm{k} \Omega$ |  | Var |  |  |  |
| R8 | 311-0353-00 | $25 \mathrm{k} \Omega$ |  | Var |  |  |  |
| R9 | 311-0256-00 | $300 \Omega$ |  | Var |  |  |  |
| R10 | 303-0203-00 | $20 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |  |
| R11 | 323-0168-00 | $549 \Omega$ | $1 / 2 \mathrm{~W}$ |  | Prec | 1\% |  |
| R12 | 315-0752-00 | $7.5 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R14 | 302-0330-00 | $33 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |  |  |
| R15 | 301-0131-00 | $130 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% | 200-1479X |
| R16 | 302-0330-00 | $33 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |  |  |
| R17 | 323-0406-00 | $165 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | Prec | 1\% |  |
| R20 | 303-0203-00 | $20 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |  |
| R21 | 323-0168-00 | $549 \Omega$ | $1 / 2 \mathrm{~W}$ |  | Prec | 1\% |  |
| R22 | 315-0752-00 | $7.5 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R24 | 302-0330-00 | $33 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |  |  |
| R25 | 301-0680-00 | $68 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |  |
| R26 | 302-0330-00 | $33 \Omega$ | 1/2W |  |  |  |  |
| R27 | 323-0406-00 | $165 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | Prec | 1\% |  |
| R30 | 311-0326-00 | $10 \mathrm{k} \Omega$ |  | Var |  |  |  |
| R31 ${ }^{2}$ | 311-0026-00 | $100 \mathrm{k} \Omega$ |  | Var |  |  |  |
| R34 | 301-0131-00 | $130 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% | X1480-up |
| R35 | 315-0392-00 | $3.9 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% | 200-634 |

${ }^{2}$ Furnished as a unit with SW17.

## INSTRUCTION MANUAL

## PARTS LIST ADDENDUM

ADD:

| R17B | $301-0206-00$ | $20 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ | $5 \%$ |
| :--- | ---: | ---: | :--- | :--- |
| R17C | $301-0226-00$ | $22 \mathrm{M} \varepsilon$ | $1 / 2 \mathrm{~W}$ | $5 \%$ |
| R17D | $301-0226-00$ | 22 M 8 | $1 / 2 \mathrm{~W}$ | $5 \%$ |
| R17E | $301-0915-00$ | 9.1 M 8 | $1 / 2 \mathrm{~W}$ | $5 \%$ |
| R27B | $301-0206-00$ | 20 M 8 | $1 / 2 \mathrm{~W}$ | $5 \%$ |
| R27C | $301-0226-00$ | 22 M 8 | $1 / 2 \mathrm{~W}$ | $5 \%$ |
| R27D | $301-0226-00$ | 22 M 8 | $1 / 2 \mathrm{~W}$ | $5 \%$ |
| R27E | $301-0915-00$ | 9.1 M 8 | $1 / 2 \mathrm{~W}$ | $5 \%$ |

This insert is placed in its appropriate position in your Product Reference Book and printed on colored paper to expedite retrieval. In a standard manual, it will be filed at the back of the manual.

## Resistors (Cont)

| Ckt. No. | Part No. |  | Description |  |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R35 | 301-0562-00 | 5.6 k $\Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% | 635-up |
| R36 | 315-0823-00 | $82 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% | 200-634 |
| R36 | 301-0473-00 | $47 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% | 635-up |
| R37 | 303-0273-00 | $27 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |  |
| R38 | 305-0303-00 | $30 \mathrm{k} \Omega$ | 2 W |  |  | 5\% |  |
| R39 | 311-0390-00 | $25 \mathrm{k} \Omega$ |  | Var |  |  |  |
| R42 | 316-0101-00 | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  | X430-up |
| R43 | 302-0393-00 | $39 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |  |  |
| R45 | 315-0681-00 | $680 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R46 | 315-0151-00 | $150 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R52 | 302-0472-00 | $4.7 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |  |  |
| R55 | 304-0271-00 | $270 \Omega$ | 1 W |  |  |  |  |
| R56 | 304-0100-00 | $10 \Omega$ | 1 W |  |  |  | 200-634X |
| R59 | 302-0104-00 | $100 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |  |  |
| R61 | 316-0330-00 | $33 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R62 | 301-0222-00 | $2.2 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |  |
| R63 | 316-0100-00 | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R71 | 316-0330-00 | $33 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R72 | 301-0222-00 | $2.2 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |  |
| R73 | 316-0100-00 | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R81 | 316-0330-00 | $33 \Omega$ | $1 / 4 W$ |  |  |  |  |
| R82 | 301-0222-00 | $2.2 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |  |
| R83 | 316-0100-00 | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R91 | 316-0330-00 | $33 \Omega$ | $1 / 4 W$ |  |  |  |  |
| R92 | 301-0222-00 | $2.2 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |  |
| R93 | 316-0100-00 | $10 \Omega$ | 1/4W |  |  |  |  |
| R99 | 308-0392-00 | $600 \Omega$ | 14 W |  | WW | 2\% |  |
| R101 | 302-0100-00 | $10 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |  |  |
| R102 | 303-0820-00 | $82 \Omega$ | 1 W |  |  | 5\% |  |
| R103 | 316-0102-00 | $1 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R105 | 316-0472-00 | $4.7 \mathrm{k} \Omega$ | $1 / 4 W$ |  |  |  |  |
| R107 | 316-0220-00 | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R114 | 301-0241-00 | $240 \Omega$ | $1 / 2 W$ |  |  | 5\% | 200-1189 |
| R114 | 301-0201-00 | $200 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% | 1190-up |
| R115 | 311-0587-00 | $5 \mathrm{k} \Omega$ |  | Var |  |  | 200-1189 |
| R115 | 311-0117-00 | $5 \mathrm{k} \Omega$ |  | Var |  |  | 1190-up |
| R116 | 315-0202-00 | $2 \mathrm{k} \Omega$ | 1/4 W |  |  | 5\% | X1190-1449 |
| R116 | 315-0182-00 | $1.8 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% | 1450-up |
| R119 | 307-0068-00 | $50 \Omega$ |  |  |  | 1\% |  |
| R121 | 302-0100-00 | $10 \Omega$ | 1/2W |  |  |  |  |
| R122 | 303-0820-00 | $82 \Omega$ | 1 W |  |  | 5\% |  |
| R123 | 316-0102-00 | $1 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R125 | 316-0472-00 | $4.7 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R127 | 316-0220-00 | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |  |
| R134 | 301-0241-00 | $240 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% | 200-1189 |
| R134 | 301-0201-00 | $200 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% | 1190-up |

Resistors (Cont)


## Switches

|  | Unwired | Wired |  |  |
| :--- | :--- | :--- | :--- | :--- |
| SW17 |  |  |  |  |
| SW201 | $260-0771-00$ | $* 262-0742-00$ | Rotary | REPETITION RATE RANGE |
| SW202 | $260-0199-00$ |  | Toggle | POWER |
| SW242 | $260-0675-00$ |  | Slide | HI5 -230 V |
|  | $260-0398-00$ |  | Toggle | HMPLITUDE FAST RISE |

${ }^{3}$ Furnished as a unit with R31.

Transformer
$\left.\begin{array}{llll} & \begin{array}{l}\text { Tektronix } \\ \text { Ckt. No. }\end{array} & \text { Part No. } & \text { Description }\end{array}\right]$ S/N Range

## Thermal Cutout

TK201 $260-0677-00$ Opens $158^{\circ} \mathrm{F}, \pm 5^{\circ}$; Closes $128^{\circ} \mathrm{F}, \pm 10^{\circ}$

TP229
TP249
TP259
TP269
344-0105-00 Clip, Test Point 344-0105-00 Clip, Test Point 344-0105-00 Clip, Test Point 344-0105-00 Clip, Test Point

## Test Points

V15

| V15 | $154-0212-00$ | 6EW6 |
| :--- | ---: | :--- |
| V25 | $154-0212-00$ | $6 E W 6$ |
| V64 | $154-0503-00$ | $7189 A$ |
| V74 | $154-0503-00$ | $7189 A$ |
| V84 | $154-0503-00$ | $7189 A$ |
|  |  |  |
| V94 | $154-0503-00$ | $7189 A$ |

## Electron Tubes

154-0503-00 7189A
V94

## FIGURE AND INDEX NUMBERS

Items in this section are referenced by figure and index numbers to the illustrations which appear on the pullout pages immediately following the Diagrans section of this instruction manual.

## INDENTATION SYSTEM

This mechanical parts list is indented to indicate item relationships. Following is an example of the indentation system used in the Description column.

```
Assembly and/or Component
    Detail Part of Assembly and/or Component
    mounting hardware for Detail Part
        Parts of Detail Part
        mounting hardware for Parts of Detail Part
mounting hardware for Assembly and/or Component
```

Mounting hardware always appears in the same indentation as the item it mounts, while the detail parts are indented to the right. Indented items are part of, and included with, the next higher indentation.

Mounting hardware must be purchased separaiely, unless otherwise specified.

## PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix, Inc. Field Office or representative.

Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number, instrument type or number, serial or model number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix, Inc. Field Office or representative will contact you concerning any change in part number.

Change information, if any, is located at the rear of this manual.

## ABBREVIATIONS AND SYMBOLS

For an explanation of the abbreviations and symbols used in this section, please refer to the page immediately preceding the Electrical Parts List in this instruction manual.

# INDEX OF MECHANICAL PARTS LIST ILLUSTRATIONS 

FIG. 1 FRONT
FIG. 2 CHASSIS
FIG. 3 CABINET
FIG. 4 ACCESSORIES

## SECTION 9 DIAGRAMS

The following symbols are used on the diagrams:

$$
\begin{aligned}
& \text { Screwdriver adjustment } \\
& \square \\
& \begin{array}{l}
\text { Front-panel control or connector } \\
\text { Clockwise control rotation in direction }
\end{array}
\end{aligned}
$$

## IMPORTANT

## Voltage and Waveform Conditions

Voltages measured with a 20,000 ohms/volt VOM. All readings in volts. Voltages are measured with respect to chassis ground unless otherwise noted.

Waveforms shown are actual waveform photographs taken with a Tektronix Oscilloscope Camera System and Projected Graticule. The test oscilloscope had the following characteristics: Minimum deflection factor, $0.05 \mathrm{volt} / \mathrm{division}(0.5 \mathrm{volt} / \mathrm{division}$ using $10 \times$ probe); frequency response, DC to 30 MHz . DC input coupling was used except as noted otherwise. To indicate true time relationship between signals, the test oscilloscope was externally triggered from the TRIGGER OUTPUT pulse.

Voltages and waveforms on the schematics (shown in blue) are not absolute and may vary between instruments because of differing component tolerances, internal calibration or front-panel control settings. Any apparent differences between voltage levels measured with the voltmeter and those shown on the waveforms are due to circuit loading of the voltmeter.

Voltages and waveforms were obtained under the following conditions unless otherwise noted on the individual diagrams:

Front-panel control settings

| REPETITION RATE RANGE | 1 kHz |
| :--- | :--- |
| MULTIPLIER | 10 |
| SYMMETRY | Midrange |
| AMPLITUDE | Clockwise |
| HI AMPLITUDE - FAST RISE | HI AMPLITUDE |
| + TRANSITION AMPLITUDE | Clockwise |
| - TRANSITION AMPLITUDE | Clockwise |
| POWER | ON |
| OUTPUT (connector) | Terminated in 50 ohms |
| + OUTPUT (connector) | Unterminated |
| - OUTPUT (connector) | Unterminated |

## Other conditions

Line voltage
Output cable
Output termination
115 volts
Five-nanosecond GR cable RG-213 V
50-Ohm in-line


# SECTION <br> DIAGRAMS 

The following symbols are used on the diagrams：


IMPORTANT

## Voltage and Waveform Conditions

Voltages measured with a 20,000 ohms／volt VOM．All readings in volts．Voltages are measured with respect to chassis ground unless otherwise noted．

Waveforms shown are actual waveform photographs taken with a Tektronix Oscilloscope Camera System and Projected Graticule．The test oscilloscope had the following characteristics：Minimum deflec－ tion factor， $0.05 \mathrm{volt} / \mathrm{division}(0.5 \mathrm{volt} / \mathrm{division}$ using $10 \times$ probe）； frequency response，DC to 30 MHz ．DC input coupling was used ex－ cept as noted otherwise．To indicate true time relationship between signals，the test oscilloscope was externally triggered from the TRIG－ GER OUTPUT pulse．

Voltages and waveforms on the schematics（shown in blue）are not absolute and may vary between instruments because of differing component tolerances，internal calibration or front－panel control set－ tings．Any apparent differences between voltage levels measured with the voltmeter and those shown on the waveforms are due to cir－ cuit loading of the voltmeter．

Voltages and waveforms were obtained under the following con－ ditions unless otherwise noted on the individual diagrams：

| Front－panel control settings |  |
| :--- | :--- |
| REPETITION RATE RANGE | 1 kHz |
| MULTIPLIER | 10 |
| SYMMETR | Midrange |
| AMPLITUDE | Clockwise |
| HI AMPLITUDE－FAST RISE | HI AMPLITUDE |
| ＋TRANSITION AMPLITUDE | Set for 500 millivolts output |
| －TRANSITION AMPLITUDE | Set for 500 millivolts output |
| POWER | ON |
| OUTPUT（connector） | Terminated in 50 ohms |
| ＋OUTPUT（connector） | Unterminated |
| －OUTPUT（connector） | Unterminated |
| Other conditions |  |
| Line voltage | 115 volts |
| Output cable | Five－nanosecond GR cable |
| Output termination | （RG－8A／U） |
| On－Ohm in－line |  |

The handwritten notes on this page are a complete history of electrical modifications. These notes are not on the schematics in the customer's Instruction Manual. Components whose values are changed by modification, are identified by an adjacent encircled starting serial number. When a component has been added or deleted --rather than changed to a new value --- the encircled serial number will be accompanied by the word "added" or "deleted". Cross reference to the modification and description can be made by scanning the "EFF. SN" column of the Modification Summary Index located in another section of this Reference Book.



The handwritten notes on this page are a complete history of electrical modifications. These notes are not on the schematics in the customer's Instruction Manual. Components whose values are changed by modification, are identified by an adjacent encircled starting serial number. When a component has been added or deleted -rather than changed to a new value --- the encircled serial number will be accompanied by the word "added" or "deleted". Cross reference to the modification and description can be made by scanning the "EFF. SN" column of the modification Summary Index located in another section of this Reference Book.

## 



Instruction Manual
Schematic Addendum


BEAVERTON

## MAINTENANCE NOTES

PROBLEM
After using the Type 106 at full output current, turning the AMPLITUDE control knob to a lower output current results (after a few minutes) in destruction of R 235 , a $3 \mathrm{k} 1 / 4 \mathrm{~W}$ resistor in the " A " regulator circuit.

When the AMPLITUDE control is turned counter-clockwise, Q233 is supposed to let the base of Q247 move towards the -10 volt supply. Icbo of Q247 (when Q247 is hot) is larger than the current through R237. If R237 is unable to pull the base of Q247 down, the comparator transistor, Q234, is turned on hard -- with eventual or immediate destruction of R235. D234 clamps the top of R235 to ground, while saturation of Q234 pulls the lower end of R235 to a negative voltage -possibly -100 volts.

SOLUTION
Change R237 from $22 \mathrm{k} 1 / 4 \mathrm{~W} \pm 10 \%$ resistor to $4.7 \mathrm{k} 1 / 4 \mathrm{~W} \pm 10 \%$. Part number of the new resistor is: 316-0472-00.

Modification 11468 will cover the change in production instruments.

Charles V. Sanford/cmh

Product Technica! Information 9-1-66

