## INSTRUCTION MANUAL



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## TYPE 3 S3 SAMPLING-PROBE UNIT



## SECTION 1

## CHARACTERISTICS

## General Information

The Tektronix Type 353 Sampling-Probe Unit is a dualtrace vertical channel plug-in unit for Tektronix Types 561A, 564 , and 567 Oscilloscopes. The Type 353 , operated with P6038 Direct Sampling Probes, has a basic risetime of 0.35 nsec or less when the signal source impedance is 50 ohms and the Noise-Risetime switch is at FAST RT. The LOW NOISE position of the switch gives the system a risetime of approximately 0.8 nsec . The P6038 sampling probe has a low-frequency input resistance of 100 k paralleled by about 2 pf capacitance. The system is capable of presenting accurate single- or dual-trace displays of repetitive high-speed signals with fractional-nanosecond risetime. By taking successive samples of a repetitive signal, each sample at a slightly later time with respect to the previous sample, the system reconstructs the signal on an equivalent time base.

## ELECTRICAL AND MECHANICAL CHARACTERISTICS

## Input Resistance

| Probe only | $100 \mathrm{k} \pm 1 \%$ |
| :--- | ---: |
| Probe and $10 \times$ Attenuator | $1 \mathrm{meg} \pm 1.5 \%$ |
| Probe and Response Normalizer | $100 \mathrm{k} \pm 1.5 \%$ |

## Ac Coupling Capacitor

| Capacitance $\quad 1000 \mathrm{pf}$ minimum, | 100 volts |
| :--- | ---: | ---: |
| Approximate low-frequency 3 db point: |  |
| Probe only | 1.5 kc |
| Probe and $10 \times$ Attenuator | 150 cycles |
| Probe and Response Normalizer | 1.5 kc |

## Maximum Signal Input

|  | Linear <br> (Dc <br> Peak | Display Plus <br> Ac) | Momentary D or Ac Peak Overload |
| :---: | :---: | :---: | :---: |
|  | Low Noise | Fast RT |  |
| Probe Only | $\pm 1.5 \mathrm{v}$ | $\pm$ | 10 v |
| Probe and $10 \times$ Attenuator | $\pm 15 \mathrm{v}$ | $\pm 30 \mathrm{~V}$ | 100 v |
| Probe and Response Normalizer | $\pm 1.5 \mathrm{v}$ | $\pm 3 \mathrm{r}$ | 10 v |
| Probe and Ac Coupling Capacitor | 1.5 va | c 3 V | ac 100 vdc |

## Input Capacitance

| Probe only | $2 \mathrm{pf} \pm 10 \%$ |
| :--- | ---: |
| Probe and $10 \times$ Attenuator | $1.8 \mathrm{pf} \pm 10 \%$ |
| Probe and Response Normalizer | $4 \mathrm{pf} \pm 10 \%$ |

## Signal Performance

See Table 1-1.

TABLE 1-1

| Input | Source Impedance | Risetime in nsec | Overshoot in \% | Noise in mv | Risetime in nsec | Overshoot in \% | Noise <br> in mv |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | FAST RISETIME |  |  | LOW NOISE |  |  |
| Probe Only | $50 \Omega$ | $\leq 0.35$ | 3 | $\leq 2$ | 0.8 | 2 | $\leq 0.5$ |
|  | *300 $\Omega$ | * 1.5 | * 0 | * $\leq 2$ | 1.7 | 0 | $\leq 2$ |
| Probe and | $50 \Omega$ | 0.38 | 5 | $\leq 2$ | 0.8 | 4 | $\leq 0.5$ |
| Coupling Capacitor | $300 \Omega$ | * 2.5 | * 0 | $* \leq 2$ | 3.0 | 0 | $\leq 2$ |
| Probe and $10 \times$ | $50 \Omega$ | 0.37 | 4 | 2 | 0.8 | 3 | 0.5 |
| Attenuator | $300 \Omega$ | * 1.5 | * 0 | * 2 | 1.7 | 0 | 0.5 |
| Probe and | $50 \Omega$ | * 1.5 | * 0 | * 2 | 1.7 | 0 | 2 |
| Response Normalizer | $300 \Omega$ | * 5 | * 0 | * 2 | 5 | 0 | 2 |

Risetime is $10 \%$ to $90 \%$.
Overshoot is peak aberration of first 1 nsec of a square pulse display.
Noise is for single-channel operation at unity loop gain; multiply figures by 1.5 for combined-trace operation.
*SMOOTHING control fully counterclockwise. Dot transient response less than unity.

## Deflection Factors

Calibrated steps of $5,10,20,50$, and $100 \mathrm{mv} /$ div. Accuracy at unity loop gain: $\pm 3 \%$ for all positions of MV/DIV switch with NORM-INV switch at NORM; $\pm 5 \%$ for all positions of the MV/DIV switch with NORM-INV switch at INV. A VARIABLE control with about a $3: 1$ range permits uncalibrated sensitivity increase, thus decreasing the deflection factor of each setting of the MV/DIV switch. Accuracy at full smoothing: $\pm 3 \%$ to $\pm 6 \%$ for all positions of the MV/DIV switch with NORM-INV switch at NORM; $\pm 5 \%$ to $\pm 8 \%$ for all positions of the MV/DIV switch with NORMINV switch at INV.

## Triggering

External to Timing Unit. Pretrigger must arrive at Timing Unit external trigger input connector about 60 nsec prior to arrival of signal at input to P6038 Probe when sweep rate is $1 \mathrm{nsec} / \mathrm{div}$ or faster. Pretrigger can arrive at Timing Unit more than 60 nsec ahead of signal to P6038 Probe when using slower sweep rates.

## Operating Modes

A Only, B Only, Dual-Trace, A + B, and A Vertical - B Horizontal (X-Y operation). The dual-trace switching frequency is one-half the sampling rate.

Rejection ratio for $A+B$ mode is $40: 1$ or better when each channel is driven with a 0.5 -volt flat-top pulse and the deflection factor is $50 \mathrm{mv} /$ div, each channel. At 100 $\mathrm{mv} / \mathrm{div}, \mathrm{A}+\mathrm{B}$, a 4 -division identical signal in each channel will produce an 8 -division display, $\pm 0.15$ division.

## Display

Normal or Inverted, permitting the addition or subtraction of dual-trace displays. Valuable in X-Y displays for observation of hysterisis loops, or for inverting the phase of signals into or out of an amplifier for phase comparison. Inverted operation can add an additional $2 \%$ error to the deflection factors.

## Smoothing

Each channel SMOOTHING control permits adjustment of the dot transient response. Clockwise rotation reduces time jitter and random noise. Valuable when operating at lowest deflection factors. The dot transient response can be made correct for source impedances from at least $50 \Omega$ to approximately $300 \Omega$ when the Noise-Risetime switch is at LOW NOISE; from about $50 \Omega$ to some higher value (dependent upon source capacitance) when the Noise-Risetime switch is at FAST RT.

## Dc Offset

The dc component of a signal may be offset up to $\pm 0.5$ volt (with a ten-turn control) to either bring a display back onto the crt, or to make an incremental measurement.

## Signal Outputs

Signal output jacks, A OUT and B OUT ( $\mathrm{A}+\mathrm{B}$ ) are provided. The signal output of each is 1 volt/div, $\pm 3 \%$, on a dc level of about +10 volts when the trace is centered vertically. Output impedance is 10 k .

## Trace Finder

Pushing the TRACE FINDER button reduces the vertical amplifier gain by 5 , allowing off-screen displays to be located and returned to view.

## Dot Slash

The sampling dot vertical stability is such that no slash is visible when triggering at a rate above about 150 cps . At a triggering rate of 50 cps , the dot slash will not exceed 0.2 division.

## Co-Channel Time Coincidence

Dual-trace display of a fastrise pulse will produce no more than a 60 -picosecond time difference between channels.

## Construction

Aluminum-alloy chassis with six plug-in subehassis. Photoetched anodized panel.

## Dimensions

Height $6 \frac{1}{4}$ inches, width $4 \frac{1}{4}$ inches, depth $12 \frac{1}{2}$ inches.

## Weight

$6 \mathrm{lbs}, 1 \mathrm{oz}$.

## Accessories

|  | Tektronix <br> Part No. |
| :--- | ---: |
| 2 - Instruction Manuals | $070-374$ |
| 2 — P6038 Probe Packages | $010-156$ |

Part No.

070-374
010-156

# OPERATING INSTRUCTIONS 

## CAUTION

## always turn off the oscilloscope power before inserting or removing plug-in UNITS.

## General Information

The Type 353 with P6038 Direct Sampling Probes is part of a wide-band, high input impedance, dual-channel servotype, slide-back sampling system. The sampled signal drives a rachet memory that sets the vertical dot position after each sample. The sampling principle is essentially that of an error signal device that corrects a memory output voltage each time a sample is taken. (See "Sampling Notes", Tektronix publication number 061-557.) An external trigger pick-off or other source of triggering signal is required by the associated timing unit.

A minimum deflection factor of about $2 \mathrm{mv} / \mathrm{div}$ at the P6038 Probe input may be employed to view low-level signals or portions of larger signals. The DC OFFSET control permits a large signal, $\pm 0.5$ volt from ground, to be examined in small detail at maximum sensitivity. The DC OFFSET will position any portion of the signal into view for small detail measurements.

At minimum deflection factors, random noise can be reduced by use of the SMOOTHING control. Smoothing will not significantly affect the display risetime, but will reduce noise if each sample taken represents only a small increment of the total signal amplitude.
The Type 353 includes circuits that operate the Type 6R1 Digital Unit for accurate voltage and time measurement of the display. The Type 3S3, Type 3T77, and Type 6R1 operated in a Type 567 Oscilloscope make up a high performance, automatic readout sampling oscilloscope.

## FUNCTIONS OF FRONT-PANEL CONTROLS AND CONNECTORS

Mode Switch-Selects one of five operational modes.
A ONLY: Only Channel A is displayed.
B ONLY: Only Channel B is displayed.
DUAL-TRACE: Both channels display separate signals simultaneously; switching between channels occurs at onehalf the sampling rate.
$\mathbf{A}+\mathbf{B}$ : Both channels are combined to display the algebraic sum or difference of two signals as a single trace. Channel B POSITION control positions the trace. Both channel DC OFFSET controls operate.
A VERT B HORIZ: Channel A controls the vertical deflection and Channel $B$ controls the horizontal deflection. Permits X-Y operation at full bandwidth.
POSITION Control (Both Channels) - Permits moving the trace about 10 divisions vertically.

MV/DIV Switch (Both Channels) - Selects the desired vertical deflection factor. For example, with the MV/DIV switch at 100, each major division of vertical deflection corresponds to 100 millivolts of applied signal. The P6038 10X Attenuator will change this example to $1 \mathrm{volt} / \mathrm{div}$.

VARIABLE Control (Both Channels) - At least a 3 to 1 range (uncalibrated) control to permit increased system gain at each position of the MV/DIV switch. Minimum deflection factor (maximum gain) is then about $2 \mathrm{mv} / \mathrm{div}$.
SMOOTHING Control (Both Channels) - Gain control in the Preamplifier that permits adjustment of the sampling system loop gain. With the Noise-Risetime switch at LOW NOISE, the loop gain can be set to unity for a source-impedance range from at least $50 \Omega$ to about $300 \Omega$. With the Noise-Risetime switch at FAST RT, the loop gain can be set to unity for a source-impedance range from at least $50 \Omega$ to some higher value depending upon the source capacitance at the tip of P6038 Probe.

Time jitter and/or amplitude noise may be objectionable when operating at minimum deflection factors or maximum sweep rates. This is important when making documentation photographs. Clockwise rotation of the SMOOTHING control reduces the loop gain of the automatic slide-back feedback system to allow random noise reduction. (See "Sampling Notes", pages 5 and 6, for additional information about using the SMOOTHING control.) When measuring signals at unknown source impedance, always start with the SMOOTHING control fully clockwise.

To test for proper position of the SMOOTHING control, switch the timing unit DOTS PER DIV switch between 100 and 10 , and observe the amount of display change. If the change is insignificant, the SMOOTHING control is not substantially affecting the dot transient response. The transient response will almost always be proper at 100 dots/div with the SMOOTHING control fully clockwise. See "Unity Loop Gain" near the end of this section.

Noise-Risetime Switch (Both Channels) - A switch that changes the conduction time of the probe sampling bridge at the time of each sample. The FAST RT position sets the bridge conduction time for a risetime of 0.35 nsec or less. The LOW NOISE position sets the bridge conduction time to about 0.8 nsec and reduces the sampling system display noise.
DC OFFSET Control (Both Channels) - Applies an internal signal offset voltage of -0.5 to +0.5 volt. May be used to effectively cancel a dc component in the presence of a small ac signal. Permits a chosen portion of the waveform to remain relatively fixed on the crt when the vertical deflection factor is changed. The DC OFFSET control will position any part of a +0.5 - to -0.5 -volt signal into view even when the MV/DIV switch is at 5 . The sampling system may overload off screen, but the display will not be distorted by such high-gain viewing of large signals. (The Digital Unit operates correctly for displays with the 0\% and $100 \%$ zones within the oscilloscope 8 -division graticule limits.)

NORM-INV Switch (Both Channels) - In the NORM position, the crt display has the same polarity as the applied signal, + up and - down. Placing one switch at NORM, the other at INV, and the mode switch to $A+B$ permits the difference of two signals to be presented as a single trace.

GAIN Control (Both Channels) - Permits adjustment of the display amplitude so the Type 353 output can match the deflection factor of various oscilloscopes. The GAIN control does not affect the amplitude of information sent to the digital unit operated in a Type 567 Oscilloscope.

TRACE-FINDER - The TRACE FINDER button reduces the overall vertical amplifier gain by 5 . Any off-screen display can then be found and the correct positioning action taken to restore it to view.

PROBE A - PROBE B - Each channel has its own P6038 Direct Sampling Probe. Probes may be disconnected and may be interchanged. If probes are interchanged, most internal adjustments require recalibration. Probe A is marked blue and Probe B is marked red for easy identification of proper probe location.

## Signal Outputs

The Type 353 has two auxiliary output signals (in addition to the regular vertical signals to the crt). The two output connectors are labeled A OUT and B OUT ( $\mathrm{A}+\mathrm{B}$ ). Signals at these connectors are 1 volt/div through 10 k , with about a +10 -volt level when the trace is centered. External loading of the signal output leads will not disturb normal sampling operations or the crt display. The two auxiliary outputs are for use by external analog paper recorders or oscilloscope monitors.

Operation at $\mathrm{A}+\mathrm{B}$ mode disconnects the signal to the A OUT connector and supplies the combined signal information to the B OUT $(A+B)$ connector.

## PRELIMINARY INSTRUCTIONS

Since the Type $3 S 3$ Sampling Unit is part of a complete sampling system, we suggest that you read the operating instructions section of the oscilloscope and Timing Unit instruction manuals before proceeding.

## Installing the Type 353

With the oscilloscope power off, turn the securing lock counterclockwise, then push the Type 353 as far into the cell as possible. Tighten the securing lock clockwise to complete the plug-in insertion.
To remove the plug-in, first turn off the power, then reverse the installation procedure.

## Using the P6038 Probe

The P6038 Probes can be used to signal trace directly within a test circuit, or can be inserted into special chassis or coaxial fittings. (The test-point jack provided with the probe adds about 0.6 pf capacitance to the probe input.)

The signal source impedance must be low when measuring pulses with risetime near the system limit.

The P6038 Probe can be compared with any standard oscilloscope probe. The bandwidth (risetime) is limited by internal circuitry and the source resistance-input capacitance time constant. However, the P6038 Probe input capacitance is quite low, nominally 2 pf , allowing a very fast response to low impedance signals.

The major difference between the P6038 Probe and a standard attenuator probe is the sampling circuit. A small signal is sent out the probe tip to the signal source at each sample. This can be reduced a factor of ten by using the 10X Attenuator. Normal sampling pulse kickout is less than 50 mv when the system is at equilibrium, and less than 5 mv using the 10X Attenuator. The kickout is not seen by the sampling system, and if more than about 0.33 -nsec delay cable is used between the signal source and the probe tip, the kickout is lost long before the next sample is taken.

## Source Impedance Sensitivity

The probe input is sensitive to both source resistance and capacitance, and the system dot transient response varies as the input circuit impedance is varied. The no-signal trace level will shift vertically as the signal source impedance is changed. This is caused by the small amount of kickout from the probe tip. It is impossible to select perfectly equal input bridge diodes, and their minor differences cause the small kickout signal when the system is at equilibrium. (The kickout pulse is a bit larger during the time the sampling bridge is responding to a change in signal level.)

The probe tip is not critically damped when measuring from very low impedance signal sources. The probe tip is a short length of wire between the very tip and the sampling bridge. The tip has about 2 nanohenries of inductance. Combined with the input capacitance of about 2 picofarads, the tip will ring when driven from an impedance under about $33 \Omega$. The ringing is obvious when the Noise-Risetime switch is at FAST RT and the probe sees an impedance less than $50 \Omega$. Ringing is a less serious problem when the switch is at LOW NOISE. For this reason the Characteristics section of this manual shows risetime figures for $50 \Omega$ operation.

## Response Normalizer

To make the probe input insensitive to source impedance, a special non-attenuating Response Normalizer is provided. Placing it on the tip of a probe lets the probe sampling gate "look into" a constant $300 \Omega$ source impedance during the time each sample is taken. Thus, there will be essentially no base-line trace shift due to different source impedances.

The Response Normalizer, however, adds about 2 pf capacitance to the probe input. The system risetime is now limited because the sampling bridge is fed through $300 \Omega$ in series with the signal source impedance. Without the normalizer, the probe input is 100 k paralleled by 2 pf , with a $0.35-\mathrm{nsec}$ risetime. With the normalizer, the probe input is 100 k paralleled by 4 pf , with a risetime of about 1.5 nsec . The advantage of the Response Normalizer is that its use eliminates the trace shift as the signal source impedance is changed.

Using the Response Normalizer on a 1 k source impedance signal produces about a 10 -nsec risetime display. This is due to the input time constant limiting the voltage rise rate to the probe input.

## 10X Attenuator

A second method for making the probe input insensitive to source impedance is to use the 10X Attenuator. This is particularly valuable when measuring signals greater than 0.8 volt peak-to-peak. Using the 10 X Attenuator on a 1 k source impedance signal produces between a 5 - and 6 -nsec rise-time display. Thus, the attenuator has less input capacitance than the Response Normalizer.

The 10X Attenuator is correctly frequency compensated as it leaves the factory. Each attenuator is color coded, and should be used with one probe only. See the P6038 Probe instruction manual for compensation procedure.

## Coax-To-Probe Adapters

Three special adapters for mating the P6038 Probe to coax systems are available. Their use is described here.


Fig. 2-1. Special GR-To-P6038 Adapter for connecting the P6038 Probe to a $50 \Omega$ line. (Part No. 017-076)

GR-To-P6038 Adapter. The P6038 Probe can be used at the end of an unterminated $50 \Omega$ system (System 5 of Table $2-1)$ with the correct precautions. Fig. 2-1 shows the GR-ToP(t. 138 Adapter. (Tektronix Part No. 017-076.)


Fig. 2-2. Using the VP-2.
(2) 100 -ohm Resistors


# Special Test <br> Jack (131-258) 

Fig. 2-3. Home-made $50 \Omega$ Termination for P6038 Probe. Make leads as short as possible.

BNC-To-P6038 Adapter. Identical in function to the GR-To-P6038 Adapter, but for cables fitted with BNC connectors. (Tektronix Part No. 103-038.)

Voltage Pickoff. Described as System 8 of Table 2-1 \{see Fig. 2-2), the Tektronix Voltage Pickoff Adapter VP-2 permits using the P6038 Probe to look at signals within a closed $50 \Omega$ system with negligible effect upon the signal. The P6038 Probe "looks into" $50 \Omega$ when using the VP-2. (Tektronix Part No. 017-077.)

Terminated $50 \Omega$ System. Fig. 2-3 shows a home-made adapter that can be made by those requiring the P6038 Probe to look at a terminated $50 \Omega$ system. It should be used with the Noise-Risetime switch at LOW NOISE to keep the input circuit overshoot (ringing) to a minimum. This special adapter is recommended over a BNC in-line $50 \Omega$ termination and the BNC-To-P6038 Adapter that will place extra capacitance at the probe tip. The VP-2 is superior to this special adapter.

## FIRST TIME OPERATION

The Type 353 is calibrated at the factory in a Type 567 Oscilloscope. It is designed to be operated in any Tektronix Type 561A, 564, or 567 Oscilloscope. There are small differences in power supply voltages and crt deflection factors between oscilloscopes that will be apparent in the operation of the Type 353 . Thus, before using the Type 353 for accurate measurements, do the following procedure each time the unit is operated in a different oscilloscope.
Connect the two P6038 Probes to the PROBE A and PROBE B connectors. Mate the probe color to the panel color.

## Balance and Gain Procedure

1. Turn on the oscilloscope power and set the Timing Unit controls for a free-running $10 \mathrm{nsec} /$ div trace at 100 dots/div.
2. Set the Type 353 controls:

| POSITION | Midrange |
| :--- | ---: |
| MV/DIV | 100 |
| VARIABLE | CALIB |
| NORM-INV | NORM |
| Mode | O ONLY |
| DC OFFSET | Five turns from either end |
| Noise-Risetime | FAST RT |
| SMOOTHING | Fully clockwise |

## Operating Instructions-Type 353

3. Place the Channel A probe tip into the 50 -ohm environment of Fig. 5-1. Center the trace and let the instrument warm up for 15 minutes.
4. Adjust the DC OFFSET control for no trace shift while turning the VARIABLE control through its range. Recenter the trace with the POSITION control. The DC OFFSET control must remain at this position through step 6.
5. Turn the SMOOTHING control through its range. If the trace moves more than one-half division, do the following.
a. Remove the oscilloscope left side panel and adjust the A Memory SMOOTHING BALANCE control for no trace shift when the SMOOTHING control is turned. (The SMOOTHING BALANCE control for Channel A is on the 2 nd subchassis from the front; the SMOOTHING BALANCE control for Channel B is on the 3rd subchassis.)
b. Return the SMOOTHING control fully clockwise. Check that the DC OFFSET control position has not changed (from step 4). Reposition the trace to the graticule center with the POSITION control.
6. Set the MV/DIV switch to 20 . Operate the Noise-Risetime switch between LOW NOISE and FAST RT. If the trace moves more than two divisions, do the following:
a. With the Noise-Risetime switch at LOW NOISE, recenter the trace by adjusting the A RISETIME BAL control, R175, located on the Gate Generator subchassis.
b. Set the Noise-Risetime switch to FAST RT and recenter the trace with the A BRIDGE BAL control, R185, also located on the Gate Generator subchassis. Repeat (a) and (b).
c. Set the MV/DIV switch to 5 and again perform steps (a) and (b). Final adjustment is when the Noise-Risetime switch can be at either position and the trace will not move more than one division for any position of the MV/DIV switch.
7A. Gain Adjustment - With Digital Unit
a. Set the Type 353 controls:

MV/DIV
VARIABLE
Noise-Risetime
CALIB
SMOOTHING
FAST RT
Counterclockwise
b. Touch the probe tip to the oscilloscope Amplitude Calibrator 0.5 -volt jack the calibrator must provide a $60-\mathrm{cps}$ square wave). Adjust the Timing Unit Recovery Time control until a square wave drifts slowly across the crt.
c. Set the Digital Unit to measure rising-slope voltage, with the A $100 \%$ ZONE SET control adjusted so the $100 \%$ intensified zone is at the graticule center. As the display drifts slowly the Digital Unit will indicate the pulse amplitude when the $100 \%$ intensified zone is at the pulse top. Adjust the Type 353 GAIN control so the display amplitude is the same as the digital readout value. The display vertical deflection factor is now within $3 \%$.

7B. Gain Adjustment - Without Digital Unit
a. Do steps 7A (a) and (b).
b. Adjust the GAIN control so the display amplitude is 5 divisions peak-to-peak. Do not adjust the internal DIGITAL GAIN control.
8. Repeat step 7 for Channel B. Replace oscilloscope side panel.

It is important that this procedure be completed each time the Type 353 is operated in a different oscilloscope.

The P6038 Probe(s) will now operate in balance for either LOW NOISE or FAST RT operation for source impedances from $50 \Omega$ up to about $300 \Omega$. The DC OFFSET control must be adjusted (as in the balance procedure) for each different source impedance if it is desired that the trace shift be minor when switching the Noise-Risetime switch. This type of operation is not always necessary, but can be of value when signal tracing and making a quick risetime measurement. See "Signal Searching-Signal Analyzing Suggestions" just ahead of Table 2-1.

## Dual-Trace Operation

The dual-trace feature of the Type 353 permits viewing signals into and out of an amplifier or signals of differing amplitude and time delay, but not signals of differing repetition rate or frequency unless harmonically related or otherwise synchronously coupled. A suggested system is illustrated in Fig. 2-4.

Use the following procedure for setting up the Type 353.

1. Set the Mode switch to DUAL-TRACE.
2. Set the MV/DIV switches to the approximate values for 3 or 4 divisions of display on each channel. If necessary, use the 10X Attenuator on the probe at the amplifier output.
3. Set the SMOOTHING controls fully clockwise.
4. Set the Noise-Risetime switches to FAST RT.
5. If the amplifier inverts the signal, you may wish to place one NORM-INV switch to NORM and the other to INV.
6. If a signal has a de component over 1 volt, be sure to ac-couple it at the input. The peak-to-peak input should not exceed 3 volts.

## Triggering the Sampling System

The Type 353 has no internal trigger takeoff system. Therefore, an external trigger signal must be applied to the Timing Unit. Two convenient trigger-signal sources are an in-line trigger takeoff system, such as available in the Tektronix Type 110, or an external trigger-output signal from a pulse generator such as the Tektronix Type 105, 107, or 111.

To complete the dual-trace operation, set the Type 3177 controls as follows:

1. Set the INT.-EXT. Triggering Source switch to EXT + or - , depending upon the polarity of the triggering signal.


Fig. 2-4. Pulse testing an amplifier.
2. Select a sweep rate to display two or three cycles of the signal. If unknown, start at $10 \mathrm{nsec} / \mathrm{div}$.
3. Set the DOTS/DIV switch to 100.
4. Set the DELAY control to midrange. It can be set later to properly position the waveform on the crt.
5. Set the RECOVERY TIME control fully counterclockwise.
6. Set the TRIGGER SENSITIVITY control for proper triggering, just counterclockwise of the free-run position.
7. The display should be a faithful reconstruction of the signal. If you have trouble obtaining a stable or properly triggered display, the problem may be either trigger signal amplitude too high or too low, trigger signal frequency too high or too low, or internal interference due to recovery time.

To find the cause, first check the position of the TRIGGER SENSITIVITY control, and/or turn the RECOVERY TIME control. If the TRIGGER SENSITIVITY control cannot stop the display (by turning it counterclockwise), the trigger-signal amplitude is too high. Or if a stable display cannot be obtained before the sweep free-runs, the trigger signal amplitude is too low.

If adjustment of the TRIGGER SENSITIVITY and RECOVERY TIME controls produces triggering, but it is jittery or confused, the trigger-signal frequency may be too high or too low.

Set the TIME/DIV switch to 1 nSEC, and if the display is other than the beginning of a waveform, the trigger-signal frequency is too high. In this case, a trigger-countdown device such as the Tektronix Type 280 is needed. External synchronization, using the Type 280, operates to 5000 mc .

Low-frequency sine-wave trigger-signal amplitude must be at least 16 mv peak-to-peak below about 250 mc . Additional
amplitude is needed when the triggering signal is below about 200 kc .

If confused triggering occurs in the form of multiple traces, try turning the RECOVERY TIME control while changing the position of the TIME/DIV switch.

A combination of recovery time and sweep rate can be found which will produce a stable display except at low frequencies. The object is to time the arrival of the trigger signal with respect to the recovery of the trigger circuits to prevent premature retriggering.

If making time or voltage measurements directly from the crt , it is usually best to align the display with the appropriate vertical or horizontal graticule markings. The graticule can then serve as a scale from which to make either time or amplitude measurements.

With the aid of the DC OFFSET control, any point on a waveform within $\pm 0.5$ volt of ground can be made to stay relatively fixed on the crt independent of vertical sensitivity. The POSITION control will then place that portion of the waveform wherever desired within the control limits. Remember: The POSITION control is approximately a +8 to - 8 -division control. The DC OFFSET is an input $\pm 0.5$ volt control.

To check that the system dot transient response is proper, set the DOTS/DIV switch of the Type $3 T 77$ to 10 . If the risetime or the peak-to-peak amplitude of the display are not altered, the system has correct dot transient response. If the signal repetition rate is fast enough, correct operation can occur with the SMOOTHING control clockwise and 100 dots/div.

## Unity Loop Gain (Correct Dot Response)

To set the sampling system loop gain to unity, set the Timing Unit DOTS/DIV switch to 10 and the TIME/DIV switch so the display pulse rise has only two or three dots. Turn the DELAY control slowly to "paint-in" the true pulse waveshape. Set the DOTS/DIV switch to 100. If the peak of the pulse is different than the "painted-in" pulse peak at 10 dots/div, adjust the SMOOTHING control until the manydot display and the "painted-in" 10 -dot display appear equal. This is the point where the loop gain is unity.

If the loop gain is greater than unity, the display will be either excessively noisy, tearing at the display beginning, or spread all over the crt. This is particularly true when operating at LOW NOISE.

If the loop gain is less than unity, the display amplitude will decrease for sine waves, and the amplitude of a fastrise pulse will be low at the end of the rise. This is particularly true when the Timing Unit is operating at 10 dots/ div. The sampling system can always be operated at something less than unity loop gain if there are 100 dots/div to correct for these display limits just described.

## Voltage Measurements

Vertical displacement of the crt trace is directly proportional to the voltage at the input to the P6038 Probe. The amount of displacement, for a given voltage, can be selected with the MV/DIV switch. To provide sufficient deflection for
best resolution, set the MV/DIV switch so the display spans a large portion of the graticule. Also, when measuring between points on a display, measure consistently from either the bottom or top of the trace so the width of the trace is not included in your measurements.

To make a voltage-difference measurement between two points on a display, proceed as follows:

1. Using the graticule as a scale, note the vertical deflection, in divisions, between the two points on the display. Make sure the VARIABLE control is in the CALIB position.
2. Multiply the divisions of vertical deflection by the numerical setting of the MV/DIV switch and the attenuation factor (if any) of an attenuator. The product is the voltage difference between the two points measured.

If desired, you can measure the instantaneous (or dc) voltage-to-ground of a signal. This is accomplished in the same general manner as described previously. However, with no signal applied, you must first establish a ground reference point on the crt. To do this, allow the Timing Unit to present a free-running trace, and install either the Response Normalizer or the 10X Attenuator to the probe tip. Then, vertically position the trace so that it is exactly aligned with one of the horizontal graticule lines. (This assumes no vertical shift in the trace base-line due to unequal duty cycle of an ac-coupled pulse train.) The actual graticule line selected will be largely determined by the polarity and amplitude of the applied signal. After this point, make no further adjustments with the POSITION or the DC OFFSET controls. Once the ground reference is established, apply the signal and measure the voltage in the same manner as described previously. Use the established ground reference as the point from which to make all measurements.

If the applied signal has a relatively high de level, the ground-reference point and the actual signal may be so far apart that one or both will not be in the viewing area of the graticule. In this case, refer to the description of the DC OFFSET control earlier in this section.

## Voltage Pickoff in Terminated Coax

The P6038 Probe can be used to look at the voltage signal in a terminated $50 \Omega$ coax line by using the Tektronix VP-2. The VP-2 is a specially designed Tee adapter that causes very little reflection in a closed coax system. (An ordinary coax Tee causes considerable reflections.) The VP-2 provides a $50 \Omega$ source impedance to the P6038 Probe (there is $25 \Omega$ in series with the tip inside the VP-2). Its use allows the P6038 Probe to observe signals on the coax center conductor while essentially not disturbing the information on its way to its normal load. Use of the VP-2 will degrade fast signal rise-time slightly.

A more accurate method of measuring voltage amplitude of a display (other than dc) is to use a Type 6R1 Digital Unit in a Type 567 Oscilloscope. See the Type 6R1 Instruction Manual for operating information. The Type 6R1 will measure the amplitude of displays whose peak-to-peak level is visible on the crt. It is not accurate if the peak-to-peak level extends outside an 8 -division graticule.

## Pulse Risetime Measurements

To make accurate measurement of a fast-rise pulse risetime, consider the following:

1. The oscilloscope crt alignment must be correct so that a free-running sweep is parallel to a horizontally scribed graticule line. See the note on alignment of the crt in the oscilloscope instruction manual.
2. The Timing Unit must be correctly calibrated. This can be checked quickly by inserting a $30-\mathrm{cm}$ air line (1-nsec delay) in series with the external triggering signal cable and noting the trace shift.
3. The signal source impedance must be low ( $50 \Omega$ ) to obtain the Type $353 / \mathrm{P} 60380.35-\mathrm{nsec}$ risetime performance.
4. If the signal repetition rate is low, and if you use 10 dots/div, the dot transient response must be checked and the SMOOTHING control correctly adjusted.
5. Calculate the signal true risetime from the following:

If the pulse signal is transported to the P6038 Probe through a short section of coaxial cable, and if the cable is as large as RG-8A/U exhibiting essentially no high-frequency attenuation in the form of "dribble-up", the pulsedisplay risetime $T_{r}$ is

TABLE 2-1
Type 353 P6038 Input Systems

| System | Advantages | Limitations | Accessories Required | Source Loading. See P6038 Instruction Manual, Input $R_{P}$ and $C_{p}$ Curves. | Precautions |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1. Probe only. | Convenient for most uses. | Trace shift with source impedance changes. <br> Dc and ac voltage. Ground clip will ring at high frequency. | Use ground clip provided or special adapter. | $100 \mathrm{k}+2 \mathrm{pf}$ plus C of adapter. | Dot transient response varies with signal source impedance. <br> Less than 50 mv sampling - pulse kickout into test circuit. |
| 2. Probe plus 10X Attenuator. | No trace shift with different source impedance. Can handle larger signals. Reduced sampling - pulse kickout. | Careful compensafion required. Loss of sensitivity. | Use ground clip provided or special adapter. | $1 \mathrm{meg}+1.8 \mathrm{pf}$ plus $C$ of adapter. | Compensate at beginning of each use. |
| 3. Probe and $A c$ Coupling Capacitor. | Dc voltage isolation. | Adds some C and $L$ to probe tip. | Use ground clip provided or special adapter. | $100 \mathrm{k}+3.5 \mathrm{pf}$ plus $C$ of adapter. | Degraded risetime to charge 3.5 pf . |
| 4. Probe and Response Normalizer. | Minimum trace shift with different source impedance. Full sensitivity. | Degraded risetime. | Use ground clip provided or special adapter. | $100 k$ + 4 pf. <br> $300 \Omega$ for $\approx 1 / 3$ <br> nsec.   | Input voltage limited to probe $V$ Max. |
| 5. Probe into unterminated coaxial cable. | Ro (of cable) as source $Z$ to probe. Full bandwidth to $2 T$ of cable, then reflections. Full sensitivity. | Input $Z$ remains $R_{\mathrm{O}}$ for only $2 T$ of cable. Ok for $50 \Omega$ systems only, and for pulses shorter than 2T of cable. | Adapter at cable end. Coaxial attenuator(s), such as 5X at source. Ac Coupler. | $\mathrm{R}_{\mathrm{O}}+2 \mathrm{pf}$ for 2 T of cable, then all of cable $C$ on source. | $100 \%$ reflection sent back to source. |
| 6. Terminated co$a x_{i}$ termination at probe tip. | $\mathrm{R}_{\mathrm{O}} / 2$ at probe tip without cable $2 T$ limit. Full bandwidth. $1 / 2$ sensitivity of system 5. | 2 pf of probe tip causes reflections. Probe tip rings. | Termination and adapter. Ac Coupler. | $\mathrm{R}_{\mathrm{O}}+2 \mathrm{pf} . \mathrm{R}_{\mathrm{O}}+$ 3.5 pf if Ac Coupler used. Plus adapter C. | Reflection of input C. Dc and ac loading on test point. Power limit of termination. |
| 7. Same as 6, with coaxial attenuator at termination. | Less reflection from 2-pf input. | Reduced signal. Probe tip rings. | Attenuators with correct fittings. | $\mathrm{R}_{\bigcirc}$ only. |  |
| 8. Tap into terminated coaxial system. | Permits signal to go to normal load. Dc or ac coupling without coaxial attenuators. | 2 pf load at tap point. 3.5 pf if Ac Coupler is used. | Special tap adapter such as Tektronix VP-2. | See probe or 10X Attenuator input curves, also P6038 Probe manual. | Reflection from probe 2 pf , or attenuator 1.8 pf . Use attenuator to stop probe kickout going to load. |

$$
T_{r}=\sqrt{\left(\text { Signal } T_{r}\right)^{2}+\left(\text { Scope } T_{r}\right)^{2}}
$$

| Transposing: |
| :--- |
| Signal $T_{r}$ |$=\sqrt{T_{r}^{2}-\left(\text { Scope } T_{r}\right)^{2} .}$

Signal Searching - Signal Analyzing Sugges-
tions

When signal tracing through a circuit and the crt display does not need to show waveshape details, the following suggestions may be of value:

1. Assemble the P6038 Probe 10X Attenuator and an Ac Coupler.
2. Set the Noise-Risetime switch to LOW NOISE and the SMOOTHING control fully clockwise.
3. Set the Timing Unit DOTS/DIV switch to 100 . Set other Timing Unit controls as required for proper triggering.
4. When signal tracing through a circuit, the Timing Unit DELAY control may have to be adjusted to restore the display to mid-crt if significant signal delay exists between test points.

To view precise waveshapes at a test point, obtain a display and then set the system loop gain (dot transient response) to unity, or as close to unity as the input circuit impedance will alow. See the paragraph at the end of "Triggering the Sampling System", in this section. Use as many dots/div as the signal repetition rate (display flicker) will allow.

## P6038 Input Systems

Table 2-1 is a quick reference guide for using the P6038 Probe most effectively. Not every situation is included, but many forms of input systems commonly used with directsampling probes are included. The letter " C " means capacitance, " T " means time, and " L " means inductance.

## SECTION 3

## CIRCUIT DESCRIPTION

## General Information

Most circuits in the Type $3 S 3$ are on plug-in subchassis. The main frame contains only the preamplifier circuits, controls, interconnections, and cables. You may wish to refer to the Tektronix publication "Sampling Notes", publication number 067-557, during the following discussion.

## Block Diagram

The Type $3 S 3$ simplified block diagram of Fig. 3-1 shows each circuit in block form, with all front-panel controls identified. Since the two channels are nearly identical, only the Channel A circuits are shown. A detailed block diagram is included with the schematics at the back of this manual.

External trigger information to the Timing Unit starts the sampling cycle. The Timing Unit sends command pulses to the Type 353 Gate Generator. The Gate Generator sends very short duration push-pull pulses to both P6038 Probes, and longer duration pulses to both Memory circuits. The
pulses from the Gate Generator first connect the signal to the preamplifiers, and then each preamplifier to its Memory.

Input signals arrive at the P6038 Probe sampling gate. The sampling gate is biased to conduction by the Gate Generator as command pulses arrive from the timing unit. The sampling gate output signal is a series of pulses, amplified by the preamplifier, and coupled through the MV/DIV switch to the Memory. The Memory input circuit is an Ac Amplifier that raises the signal level for the Memory. The Gate Generator biases a two-diode gate at the Memory input to conduction as the signal arrives.

The Memory amplifies and stores the signal. The Memory output is sent to the Inverter, and to the probe and input circuit to set the voltage equal to the signal at the time of the sample. The next sample only corrects for any signal change since the last sample.) The Memory output signal can be inverted by the unity gain Inverter. The output of both channels then pass to the Dual-Trace electronic switch where either or both are sent on to the Vertical Amplifier, and each is available for the oscilloscope Digital Unit.


Fig. 3-1. Type 353 simplified block diagram, Channel $B$ is essentially the same as Channel $A$.


Fig. 3-2. Simplified Channel A input.

## P6038 Probe

The Type 353 input is via the P6038 Probe shown in simplified form in Fig. 3-2. The probe is the heart of the sampling system where the 0.35 -nsec risetime performance is established. The input impedance is 100 k paralleled by about 2 pf .

Fig. 3-2 shows the probe sampling gate is normally reverse biased (about 4 to 5 volts). The relay contacts represent an equivalent method of applying forward bias to the sampling gate. If the relay is closed momentarily, the gate is forward biased and connects the signal to the Preamplifier. The duration of forward biasing is slightly less than 0.35 nsec ; so fast that the probe cable and Preamplifier shunt capacitance (Cs) limit the signal to the Preamplifier grid to about $2 \%$ of the input amplitude. Cs is stray input capacitance that increases the signal duration at the Preamplifier input. Because only about $2 \%$ of the signal
gets to the Preamplifier, the sampling efficiency is about $2 \%$.

## Gate Generator (Series A, Model II

The pulses that gate the sampling diodes into conduction are formed by a snap-off diode and clipping line, driven by a blocking oscillator, Q200. The blocking oscillator also drives the Memory input gates via the memory gate width amplifier, Q214.

The Gate Generator quiescent state is as follows: Q200 is held cut-off by reverse bias developed across D202. The emitter and base rest at +20 volts. The collector of Q200 rests slightly below ground due to about 20 ma of current flowing in the snap-off diode D200. The memory-gate amplifier Q214 is cut off with its base at about +0.3 volt due to the drop across D212.

As the positive trigger pulse arrives from the Timing Unit, the following action takes place:

The Timing Unit command pulse passes through coupling capacitor C209 and diode D207 to the collector of Q200. Q200 is a common-emmitter type blocking-oscillator. When the positive trigger pulse is received, signal current passes through the collector winding of T200. Signal current in the collector winding induces a voltage in the base winding that overcomes the back-bias at the base and turns the transistor on for a blocking-oscillator cycle. The fast current rise which then occurs in the collector of Q200 is directy coupled to the snap-off circuit. During turn-on, Q200 base-emitter junction is forward biased by the feedback winding of T200. C202 receives a charge that will aid in stopping any self oscillation after the trigger pulse is gone.
After the collector voltage of Q200 rises to the saturation point, the normal blocking-oscillator back swing tries to occur. At the same time the charge on C202 back-biases the base of Q200, allowing a quick return to equilibrium.

The quiescent condition of snap-off diode D200 is set by the SNAP-OFF CURRENT control, R205. The circuit typically carries about 20 ma of forward current through D200. This forward current assures that D200 has many carriers within its junction region. As the forward current is suddenly reversed, the carriers require a short time to clear out and open the diode in a normal reverse bias condition. Snap-off diode D200 is reverse biased by the pulse from Q200 but does not become a high impedance immediately.

As the pulse from Q200 arrives at D200, a high reverse current builds up in the clipping line and D200. As the carriers clear out of the D200 junction, the reverse current stops suddenly, sending a fast-rise voltage pulse into the $50 \Omega$ clipping line and toward each probe.


Fig. 3-3. Principle of snap-off diode action as SNAP-OFF CURRENT control is adjusted.

The blocking oscillator output pulse has a finite risetime. The snap-off diode reverse-cleanout delay is proportional to the forward bias applied (SNAP-OFF CURRENT adjustment). Thus, the interrogate pulse amplitude is set by the SNAP-OFF CURRENT control position. See Fig. 3-3.
The sharp step that appears at the clipping line input at snap-off is propagated down the line. The line acts as a balanced transmission line, terminated in a short circuit. The step travels to the short circuit in a finite time. When it reaches the short, it is reflected, equal in amplitude and opposite in polarity, back to the snap-off diode and the
probes. The reflection reverses the intial fast-pulse polarity, limiting the pulse duration to a very short time, and the snap-off diode returns to its normal forward bias condition. T160 balances the fast sampling pulses that are sent to the probe. The sampling pulse (Gate Generator output pulse to probes) is of triangular form with a duration greater than 1 nsec at its base and less than 0.35 nsec at the peak.

## Low Noise—Fast Risetime

The system risetime is altered by changing the peak value of the Gate Generator pulse that causes the sampling gates to conduct. The Type 353 uses a switch that changes the value of the bridge volts (reverse bias) instead of changing the pulse amplitude. By this method, the peak value of gate pulse is effectively changed as shown in Fig. 3-4, thus changing the length of time the sampling gates conduct and the system risetime.


Fig. 3-4. Two conditions of Low Noise-Fast Risetime switch, idealized waveforms.

When the Low Noise-Fast Risetime switch is at LOW NOISE, R181 and R189 are placed in parallel with the BRIDGE VOLTS control. This reduces the amount of sampling bridge reverse bias. The sampling diodes' balance changes slightly with a change of bridge volts. The combination of the BRIDGE BAL and RISETIME BAL controls allows each probe gate to be balanced for both bias conditions of the Low Noise-Fast Risetime switch.

## Memory Gate Width

The memory is allowed to receive signals only when a sample is taken. Because the feedback loop contains positive feedback, the output of the Preamplifier must be disconnected from the memory input while the feedback loop is shifting the level at the input to the Preamplifier. The Gate Generator subchassis has a memory gate driver that controls the memory gates.

Memory gate amplifier Q214 is normally biased to cut-off due to drop across D212 and current through the MEMORY GATE WIDTH control R215 and R213. Q214 collector rests at -12.2 volts. The collector current path is through the two windings of the two Memory gates, not through D216 and R216. As Q200 pulses, a third winding of T200 couples a negative signal through D212 to the base of Q214, causing Q214 to saturate. Q214 collector rises nearly to ground and its current flows through the two Memory gates. Car-
rier storage, variable by the MEMORY GATE WIDTH control, assures that Q214 will stay at saturation for typically $0.4 \mu \mathrm{sec}$. As the collector of Q214 falls, D216 and R216 critically damp the Memory gate transformers to prevent ringing.

## Sampler Controls

The Gate Generator subchassis contains nearly all internal adjustments that control the sampling efficiency and loop gain; they are: SNAP-OFF CURRENT, MEMORY GATE WIDTH, A BRIDGE VOLTS, $A$ and B BRIDGE BAL, and $A$ and B RISETIME BAL controls. Note that there is no B BRIDGE VOLTS control. The bridge bias volts of Channel B is fixed, and the A BRIDGE VOLTS control allows the bridge bias volts of Channel $A$ to be adjusted so both channels perform with the same risetime.

Two other controls in each channel affect the system operation. Each Memory subchassis has a LOOP GAIN and a SMOOTHING BALANCE control. Their functions are described with the Memory circuit description.

## Preamplifier

The Preamplifier consists of two cascaded amplifiers, V114A, and the combination of V114B, Q124, and Q123. VIl4A is a voltage amplifier with a variable plate load, the SMOOTHING control. V114B, Q124, and Q123 form an operational amplifier with a high voltage gain. The supply voltage for V114A, and the first two elements of the operational amplifier, is double decoupled from the +125 volt supply. The entire amplifier negative return is to the -12.2-volt supply, and the collector supply of Q123 is decoupled from the +20 -volt supply.

Preamplifier gain is best described as voltage input and current output. If the input grid of V114A receives 0.1 volt, its plate will drive 0.5 ma to the operational amplifier (if the SMOOTHING control is fully counterclockwise at full gain). The operational amplifier has a virtual ground input impedance due to the feedback from the emitter of Q123. The internal-loop of the operational amplifier drives the base of Q123 about 2 volts for each input 0.1 ma at the grid of V114B. (2 volts across R123 equals 0.1 ma through R123 to the grid of V114B.) With 0.1 -volt input, the preamplifier output will be 10 volts.

Sampling efficiency of the P6038-Type 353 is about $10 \%$ or less. Under ideal conditions, about $10 \%$ of the signal at the probe tip reaches the grid of V114A. Signal source capacitance, and/or operation for fastrise signals, can reduce the sampling efficiency to about $2 \%$. Thus, with a 1 -volt signal at the probe tip, the input signal to V114A can be between about 20 mv and 100 mv .

Signals from the probe are fast pulses, one each time a sample is taken. Right after the grid of V114A has responded to the signal, feedback from the Memory sets the input voltage level equal to the true signal value.

The bypass capacitor C 117 in the cathode circuit of V 114 A , and the coupling circuit between V114A and V114B, differentiate both the signal and the feedback, thus allowing the circuit to return to equilibrium before the next sample is taken.

Fast positive input signals turn on Q123 in normal forward bias fashion. Fast negative going signals may turn Q123 off faster than its emitter can fall, in which case DI23 conducts and drives the emitter negative at the signal rate.

The Preamplifier output is ac coupled to the Memory subchassis through a section of the MV/DIV switch. The system, including the Preamplifier output, the MV/DIV switch and the Ac Amplifier (Memory subchassis), is shown in Fig. 3-5.


Fig. 3-5. Simplified connections from Preamplifier output to (Memory) Ac Amplifier input. *R $=$ Parallel value of all other R260 and R261 resistors.

## AC Amplifier

The Input circuit of the Memory subchassis is a two-transistor operational amplifier with its gain controlled by the MV/DIV switch resistance in series with the base of Q304. The input signal from the Preamplifier always looks into a 1 k load. The series resistor, $\mathrm{R}_{\text {in }}$ of Fig. 3-5, sets the Ac Amplifier voltage gain according to $R_{f} / R_{\text {in }}$. When the MV/ DIV switch is at $5, \operatorname{R260E}(1 \mathrm{k})$ sets the voltage gain at 30 . When the MV/DIV switch is at 100, R260A (21 k) sets the voltage gain at 1.5. The resistor $R_{T}$ of Fig. $3-5$ has no significant effect upon the circuit because it is in parallel with the virtual ground input resistance of the Ac Amplifier.

The input of the Ac Amplifier rests about - 0.3 volt from ground which requires ac coupling of the $1 k$ resistance to ground of the MV/DIV switch (C261). Thus, the signal differentiation by Cl 23 and the 1 k value of the MV/DIV switch is accomplished at the voltage of the Ac Amplifier input.
The Ac Amplifier output is set by R313, the LOOP GAIN control. R313 is adjusted during calibration so the system loop gain (dot transient response) is correct for $50 \Omega$ source impedance signals at the tip of the P6038 Probe when the SMOOTHING control is fully counterclockwise and the Noise-Risetime switch is at FAST RT.

The signal pulses handled by the Ac Amplifier are about 0.5 to $1 \mu \mathrm{sec}$ in duration. The amplifier output voltage can


Fig. 3-6. Simplified memory gate.
change a maximum of about 2 volts in about $0.1 \mu \mathrm{sec}$. Normally the system causes the output pulses to be less than 1 volt, but if the display moves 8 divisions in one sample, the output pulse will be about 1.6 volts peak. The output impedance of the circuit is low enough to charge C315 during the time the Memory Gate conducts.

## Memory (Series B, Model 1)

A simplified schematic of the Memory circuit is shown in Fig. 3-6. Refer also to the Memory schematic at the back of this manual. The Gate Generator closes the Memory input gate diodes D342 and D343 at the correct time of each sampling cycle. The Memory circuit is a feedback amplifier (integrator) with input and feedback elements both capacitors. The input capacitor is C315, the feedback capacitor is C375. V353 is an input cathode follower, Q364 is the amplifier, and Q374 is an output emitter follower.

The input impedance at the grid of V353 acts as a virtual ground because as the input signal changes the grid voltage, the signal is amplified and applied back to the input as negative feedback to cancel the original change.

The action of the Memory is to transfer a charge from C315 to C375. The circuit between the Ac Amplifier output and the grid of $V 353$ looks like $200 \Omega$ and 510 pf in series (when the Memory gate is conducting). Thus, as a signal appears at the Ac Amplifier output, C315 is charged. C315
tries to couple the signal to the grid of V353, but feedback prevents the grid voltage from changing significantly; the result is for both C315 and C375 to receive a charge.

When the Memory gate is not conducting, the grid of V 353 has a very high impedance to ground, and at this time the only possible discharge path for C375 is by V353 grid current or stray leakage current. The grid current and total leakage current is so low that there is essentially no change in the output voltage between samples even when sampling at the low rate of 150 times a second.

The circuit elements between C315 and the grid of V353 serve several purposes:

1. D330 and D332 are amplitude-limiting diodes. They normally do not conduct.
2. D324 is a 6-volt Zener to provide back-bias for the gating diodes D342 and D343.
3. The resistors all aid in setting the input quiescent voltage level.
4. T339 is a pulse transformer that allows rapid turn-on of the gating diodes to connect the input circuit to V353.
5. C325 assures that both sides of D324 follow the signal equally.

Within the Memory amplifier:

1. C365 corrects for transistor phase shift.

## Circuit Description-Type

2. D362 is positive signal overload protection for Q364.
3. D372 assures that fast negative signals at the base of Q374 will be coupled to C375 and the output, even if Q374 is momentarily cut off.
4. The maximum positive swing of the output lead can be about +20 volts. The maximum negative output can be about -12 volts.

Between samples, the Ac Amplifier output returns to its quiescent level, and any C315 charge (that was gained at the last sample) is cancelled. At the next sample (if there is any change at the Preamplifier input), C315 will receive a new charge and can add to or subtract from the residual charge of C375. C315 is charged by the Ac Amplifier only when the memory gate is conducting.

## System Operation With No Signal

Items to remember when examining signals at various points between the Preamplifier output and the Memory output:

1. It is impossible to install perfectly balanced sampling gate diodes, so at each Gate Generator pulse there will be some small error signal sent into the system.
2. The Memory circuit does not retain a perfectly stable output voltage because C375 cannot hold a charge permanently.
3. The Memory output is coupled back to the Preamplifier input (with proper attenuation).
4. Theorerically, if there is no input at the sampling gate, there will be no Ac Amplifier signal, and the Memory output will be zero. The Memory output will be essentially zero, but there will always be a small pulse at the Ac Amplifier output.
5. The SMOOTHING BALANCE control (R355) sets the quiescent dc level at the Memory input and if incorrectly adjusted will cause an offset voltage that looks like a continuous signal. For example, assume the SMOOTHING BALANCE control is off by +1 mv . If the Memory amplifier internal gain is 500 (it isn't actually), the Memory output will now be off by -500 mv . The $-500-\mathrm{mv}$ feedback to the input bridge creates an error signal which will drive the Memory output nearly back to zero. After several dots the Memory output will stabilize near zero, but slightly off from zero to provide enough error signal to correct for the original 1 -mv error. Thus, a continuous minor error signal is amplified to place the output level near zero. If the Preamplifier gain is reduced by the SMOOTHING control, the Memory output must now be larger so the error signal fed into the Ac Amplifier is larger, restoring again the $-1-\mathrm{mv}$ correction at the Memory input. A trace shift seen when the SMOOTHING control is rotated is the increased Memory output to make up for the reduced amplifier gain. Thus, the Memory input balance control is called the SMOOTHING BALANCE because its effect is seen by rotation of the SMOOTHING control.


Fig. 3-7. DC OFFSET and MV/DIV circuit from Memory output to feedback and Inverter circuits.

## DC Offset

The Memory output of Q374 is fed to the Inverter circuit. It is also fed to a voltage divider of the MV/DIV switch that controls the feedback signal sent to the Preamplifier and Gate Generator. The feedback attenuator resistors (R348, A through D, Attenuator Switching diagram), set the feedback amplitude to keep the basic Memory output at 1 volt/division while the feedback voltage just matches the input signal.

The Dc Offset circuit adds a dc shift to the feedback loop. It includes a current cancelling system that prevents offset current from flowing in R348; see Fig. 3-7. Rotating the DC OFFSET control from one end to the other causes equal currents to be injected at both sides of the MV/DIV feedback
divider. The resulting voltage drop of $\pm 0.5$ volt across both R344 and R346 is the offset voltage sent to the Preamplifier and Gate Generator. The two points of offset injection assures there is essentially no offset current in R348 so that the offset system is not affected by changing the stetting of the MV/DIV switch.
The DC OFFSET control may be used to extend the range of the POSITION control for signals with a de component up to $\pm 0.5$ volt.

## Inverter (Series C, Model 1)

The Inverter includes two operational amplifiers for each channel. The function is to invert the display when the front-panel NORM-INV switch is in the INV position. When


Fig. 3-8. Interconnections for Inverter subchassis.

## Circuit Description-Type 353

the switch is in the NORM position, both amplifiers are used in cascade. Switching and interconnections are shown in Fig. 3-8 and on the Interconnector Diagram at the back of this manual.

Each amplifier has a current injection system at the transistor base for changing the de level of the output signal. The INVERTER ZERO control is the current injection of the first amplifier. It is used to set the input and output voltage equal (essentially zero). As an example, Q424 coliector rests at about +20 volts. Zener diode D424 lowers the voltage to near zero without attenuation. Then the INVERTER ZERO control injects a small current at the base of Q424 to alter the output voltage a bit to allow for variation in components and input voltage. Thus, the first amplifier can be switched in or out of the circuit without changing the vertical position of a centered display. The current injection of the second amplifier is the front-panel POSITION control. The output voltage of each second amplifier (Q434 and Q454) is at about +10 volts.

All four amplifiers are simple operational amplifiers. The gain is set by the ratio of the feedback resistance to the input resistance. Each stage has essentially 12.1 k input and feedback resistance. The signal input current is equal to the feedback current, and the base impedance of each transistor is then a virtual ground. Thus, the resistance of the current injection circuits just discussed does not affect the signal source impedance and therefore does not affect the stage gain.

The gain of the first amplifier (Q424 and Q444) may not be unity. The gain is set by the 12.5 k feedback resistor and the series value of R349 at the Memory output (1 k), R352 (VARIABLE control at CALIB, 10 k ), and the DIGITAL GAIN control. The total of these three resistors will be between about 11 k and about 13.5 k depending upon the Memory ouput at unity loop gain.

The gain of the second amplifier (Q434 and Q454) is unity when fed from the first amplifier. Channel A gain is set by R429 and R435. The gain of the second amplifier will be the same as the first amplifier when the NORM-INV switch is at INV because its source resistance is then the input system from the Memory.

The DIGITAL GAIN control allows setting the system gain, from the probe tip to the Inverter output, to the correct value for operation with a digital plug-in unit in the Type 567 Oscilloscope. It also affects the display amplitude, but the display amplitude is then adjusted to match the digital unit readout by the front-panel GAIN control.

Operational amplifiers can be used as signal adders. More than one input can be paralleled at the virtual ground base impedance of Q454. When the Mode switch is set to $A+B$, both channel signals enter the base of Q454 and are added. If one channel NORM-INV switch is at INV, then the signals subtract. Under this mode of operation, the Channel A POSITION control does not affect the display (see Fig. 3-8). Both switches operate, and the single-trace algebraic display is positioned by the Channel B POSITION control.

Output of both channel Inverters at Q434 and Q454 goes to three 10 k loads. They are the Dual Trace subchassis, the front-panel output terminal, and the digital unit.

Each output can work into a very low impedance because the feedback within the operational amplifier makes its collector output impedance very low.

## Dual Trace (Series D, Model 1)

The Dual Trace subchassis determines which channel is displayed, or that both are displayed. Because of the various modes of operation possible, both the A and B channels will be discussed.

The signal of both channels enter the emitter circuits of separate common-base stages Q514 and Q524 that have a single and shared collector load at the input to the Vertical Amplifier. Which channel is displayed is determined by the Mode switch and the conduction of Q545 or Q555. Q514 and Q524 always conduct the same current, and the signal is either passed to the Vertical Amplifier or bypassed to the clamping circuit of Q545 or Q555.

During single-channel displays (A ONLY, B ONLY, A + B or A VERT B HORIZ), only one clamping transistor conducts. Q555 conducts for the A ONLY and A VERT B HORIZ modes, Q545 conducts for the B ONLY and A + B modes, and Q545 and Q555 become a bistable multivibrator, triggered by Q570 for DUAL-TRACE operation.

The output voltages of the INVERTER subchassis rests at +10 volts and are 'modulated' by signal currents. Each Dual-Trace common-base stage has about 10 k between the Inverter and the emitter of the stage (front-panel GAIN control in series with R513). Thus, each common-base stage conducts 1 ma steady de and $100 \mu \mathrm{a} / \mathrm{div}$ signal current. Memory output is 1 volt/div; Inverter output is $1 \mathrm{volt} / \mathrm{div}$ into 10 k . Thus, signal current is 0.1 ma or $100 \mu \mathrm{a} / \mathrm{div}$ at the input to the common-base stages.)

Fig. 3-9 shows de current flow paths for the common-base amplifiers for A ONLY operation. Voltages for A ONLY operation are included on the Dual Trace Schematic. The transistor for the channel not displayed, Q514 of Fig. 3-9, does not saturate when its output is channeled through D516. It must not saturate or dual-trace switching transients would be sent back to the Inverter and cause excessive display noise. The combined voltage drops across D557 (at the collector of Q555) and D516 assure that the collector valtage of Q514 will always be negative with respect to its base, therefore not saturated. B ONLY operation current flow is the reverse of that shown in Fig. 3-9.

## Dual-Trace Operation

The Type 353 switches between channels at every sample when operated in the Dual-Trace mode. Q545 and Q555 operate as a nonsaturating bistable multivibrator that switches at the sampling rate. Basically its frequency is about 50 kc if the timing unit triggering signal is 100 kc or greater; less than 50 kc if the triggering signal is less than 100 kc .

The multivibrator is switched by triggers from the blanking oscillator Q570. The triggers are negative pulses from the grounded winding of T570, each time the blanking oscillator is triggered by the Gate Generator. The trigger pulses are ac coupled to the base of the off transistor (Q545 or Q555) to turn it on and cause the multivibrator to switch.


Fig. 3-9. Current flow of Dual Trace common base amplifiers for A ONLY operation.

## Blanking Oscillator

The blanking oscillator is active in all modes of operation to blank the oscilloscope crt each time a sample is taken and the display dot is moved. Thus it serves well as the blanking system for Dual-Trace operation.
The blanking oscillator is triggered into conduction by the memory gate width circuit of the Gate Generator. The Gate Generator pulse does not last long enough to properly blank the crt so the blanking oscillator pulse lasts about $4 \mu \mathrm{sec}$.

Before Q570 is triggered it is cut off by about +0.2 volts at the base. The collector voltage is -38 volts. As the positive trigger pulse arrives, the following takes place.

1. The trigger is transformer coupled (and inverted) to the base to turn on Q570.
2. Regenerative blocking oscillator action follows and the transistor saturates.
3. As the trigger signal stops, the base of $Q 570$ is negative due to stored charge in the emitter-base junction. R57l removes the stored charge slowly, allowing Q570 to come out of saturation slowly and prevent any back-swing of T570. Thus a steady blanking signal of about +38 volts is sent to the oscilloscope crt circuit.
4. At the time the trigger arrives, a sharp negative pulse is sent to the Dual-Trace multivibrator. If the MODE switch
is at DUAL-TRACE, the multivibrator will switch states. Otherwise the trigger has no effect.

## Digital Readout Channel Information

Digital Readout amplifier Q564 sends a +2 -volt steady signal to the Digital Plug-In Unit when the Type 353 displays Channel $A$ and $a-l$-volt steady signal when Channel $B$ is displayed. It also switches at the Dual-Trace switching rate.

## Vertical Amplifier (Series E, Model 1)

The Vertical Amplifier is composed of two operational amplifiers. The first, Q614, Q624 and Q634, has a gain of 110 volts output per ma input. The second, Q654, Q664, and Q674 has a voltage gain of -1 .

The output voltage of the Dual Trace subchassis and the input of the Vertical Amplifier is set by the emitter voltage of Q614. The base of Q614 is the collector load for the two common-base dual-trace amplifiers.

The input circuit of Q614 includes a $\div 5$ TRACE FINDER push button. The Trace Finder switches the Dual-Trace output from a direct connection to the base of Q614, to a $5: 1$ resistive divider R607 and R608. Since both sides of the divider are at -12.2 volts, no de current flows in the divider.

## Circuit Description-Type 353

The input voltage level of the Vertical Amplifier is a combination of two silicon junction drops, D612 and the emitter-base junction of Q614. The Vertical Centering circuit, R610 and R611, set the current at the base of Q614 so that zero current from the Dual Trace circuit centers the trace. The current path is from the emitter of Q634, through R619, D612, and the Vertical Centering resistance. The total current with the trace centered is about 1.8 ma , enough to make the voltage drop across D612 equal and opposite the forward voltage drop of the emitter-base junction of Q614.
In making voltage measurements within the Vertical

Amplifier, all but one (as listed in the schematics) remain very stable with a stable trace position. However, the voltage at the collector of Q614 drifts nearly 0.5 volt if the trace is moved from center to either the top or bottom of the graticule. The drift is due to a thermal change in D615, but since it is at the high-impedance collector of Q614, there is essentially no change in current drive to the emitter of Q624. The drift is normal and should not be considered.

The Vertical Amplifier push-pull output is about 185 volts peak-to-peak for 8 divisions of trace shift. The signal input current for 8 divisions of trace shift is slightly less than 1 ma .

## SECTION 4

## MAINTENANCE

## PREVENTIVE MAINTENANCE

## Calibration

The Type $3 S 3$ Plug-In Unit will not require frequent calibration. However, to insure that the unit is operating properly at all times we suggest that you check the calibration after each 500 -hour period of operation (or every six months if used intermittently). A complete step-by-step procedure for calibration of the unit and checking its operation is included in Section 5.
The accuracy of measurements made wth the Type 3S3/ P6038 Probe system depends not only on the accuracy of calibration, but also on the calibration of the associated oscilloscope. It is important for the oscilloscope to be in proper calibration.

## Visual Inspection

Troube can sometimes be found by a visual inspection of the unit or probe. For this reason, make a thorough visual check each time the instrument is calibrated or repaired. Look for such defects as loose or broken connections, damaged connectors, improperly seated tubes, scorched or burned parts, broken terminal strips, etc. The remedy for these troubles is apparent, except for heat-damaged parts. Heat damage is often the result of other, less apparent trouble. It is essential for you to determine the cause of overheating before replacing damaged parts.

## Tube or Transistor Checks

Tester checks on the tubes and transistors used in the Type $3 S 3$ is not recommended. Tube testers sometimes indicate a tube to be defective when that tube is operating satisfactorily in a circuit, or they may fail to indicate tube defects which affect the performance of the circuits. The same applies to similar tests made on transistors. The criterion for useability of a tube or transistor is whether or not it works properly in the circuit. If it does not, then it should be replaced. Unnecessary replacement is not only expensive but may also require needless recalibration of the instrumnt.

## COMPONENT REPLACEMENT

## General Information

The procedures for replacing most parts in the Type $3 S 3$ and P6038 Probe are easy. Detailed instructions for their removal are therefore not required. In some cases, however, additional information may help you. This information is contained in the following paragraphs. Because of the circuit configuration, it will be necessary to recalibrate portions of the circuit when certain parts are replaced. Refer to the Calibration section of this manual.

## Removal of Subchassis Circuit Boards

Most of the Type 353 circuitry is located on subchassis circuit boards. Each subchassis has a 22 -contact connector


Fig. 4-1. Subchassis location guide.
that mates with the main-frame cables. Maintenance is made easier by the use of a special subchassis extender and special extension cables that permit the unit to be operated outside of the oscilloscope (identified at the beginning of the calibration procedure). The Type 353 will operate correctly with any subchassis extended for testing.

Removal of a subchassis is accomplished by pressing sideways on the two tabs located at each side of the unit being removed. The removal tabs apply lifting pressure to the guides, aiding in disconnecting it from the interconnecting socket.
When installing a subchassis, note the letter located just to the right (front panel facing you) of the interconnecting socket that identifies which subchassis will operate in that location. The letter is identified on each schematic as a "series" letter (the Gate Generator is "Series A"). The series letter is both a circuit guide and a physical position guide, and mates with a letter on the top lip of each subchassis. See Fig. 4-1.
To replace a subchassis, apply heavy hand pressure to push the unit fully into position. Take care not to rotate small screwdriver adjustments, as that will change the calibration.

## Switches

Procedures for the removal of defective switches are, for the most part, obvious and only a normal amount of care is required. If a switch is removed, careful notation of the leads to the switch should be made to facilitate connecting the new switch.

Single wafers are not normally replaced on the switches used in the Type 353. If one wafer is defective, the entire switch should be replaced. Switches may be ordered from Tektronix either unwired or with the parts wired in place.

## Soldering Precautions

In the production of Tektronix instruments a special silverbearing solder is used to establish a bond to the ceramic terminal strips. This bond may be broken by repeated use of ordinary tin-lead solder, or by excessive heating of the terminal strip with a soldering iron. Occasional use of ordinary $60-40$ solder will not break the bond unless excessive heat is applied.

If you are responsible for the maintenance of Tektronix instruments, it is advisable to have a stock of solder containing about $3 \%$ silver. This type of solder is generally available locally, or it may be purchased from Tektronix in one-pound rolls; order by part number 251-514.

Because of the shape of the terminals of the ceramic terminal strips, we recommend a small wedge-shaped tip on your soldering iron. These tips allow you to apply heat directly to the solder in the terminals. It is important to use as little heat as possible while producing a full-flow joint.

The proper technique for soldering components in place requires: (1) use of long-nose pliers to hold the lead securely between the component and the point where heat is applied, allowing the pliers to serve as a heat sink; (2) use of a hot iron for a short time; and (3) careful manipulation of the leads to prevent breakage. Use a 50 -to 70 -watt iron when working on ceramic strips.

## Ceramic Terminal Strips

Damaged ceramic terminal strips are most easily removed by unsoldering all connections, then knocking the plastic
yokes out of the chassis. This can be done by using a plastic or hard-rubber mallet to hit the ends of the yoke protruding through the chassis. If space limitations prohibit use of the mallet directly, a plastic rod can be used between the mallet and the yoke of the strip. When the two yokes supporting the strip have been knocked out of the chassis, the strip and yokes can be removed as a unit. The spacers will probably come out with the yokes; if not, they can be removed separately.

Another way of removing the terminal strip is to cut off the side of the yoke holding the strip with diagonal cutters. This permits the strip to be removed from a difficult area where a mallet cannot be used. The remainder of the yokes and the spacers can be pulled out separately. Since a replacement strip is supplied with yokes already attached, the old yokes need not be salvaged. However, the old spacers can probably be used again.

When the damaged strip and yoke assembly has been removed, place the spacers into the holes in the chassis. Then set the ends of the yoke pins into the spacers. Press or tap lightly directly above the yokes to drive the yoke pins down through the spacers. Be certain that the yoke pins are driven completely through the spacers. Then cut off the portion of the yoke pin protruding past the spacers. (See Fig. 4-2.)


Fig. 4-2. Ceramic strip assembly.

## P6038 Probe

The P6038 Probe may need inspection if it is dropped or has otherwise been damaged. To inspect a probe, grasp the cable strain-relief about $3 / 4$ inch from the probe body, and rotate the probe body counterclockwise to remove it. About six complete turns will free the securing threads and allow the body to be withdrawn off the tip end.

The cable strain relief boot should not be forced back from its normal position, as a special tool is required to reinstall it.

The sampling gate diodes are snapped in place. If the probe has been dropped, one or more of the diodes may have slipped out of one of its clips. Fig. 4-3 shows the proper location of the diodes and their polarity. Replace a diode in its clips by applying pressure on the lead, not on the ceramic body. (Diodes can be broken by finger pressure on the body).

In the event a diode requires replacement, a selected set of four diodes is available by ordering Tektronix Part No. 152-144. The diodes come as two pairs. Each pair is to be


Fig. 4-3. Inside views of P6038 Probe.
placed side-by-side, either at the tip end, or at the cable end. Do not mix diode locations or diode sets. Diode set replacement requires complete recalibration.

If any other probe parts require replacement, send the probe to your nearest Tektronix Field Repair Center. Do not attempt any soldering, as a special positioning jig is required to set proper tolerance.

To replace the probe body, take care that the threads do not rub against any components or the cable foam; then reverse the above removal procedure. Gentle handling is important; the P6038 Probe is not intended for rugged use.

## TROUBLESHOOTING

## General Information

The Type 353 derives all of its operating voltages from the oscilloscope, and depends on the oscilloscope and the Timing Unit for its display. You must be sure that the oscilloscope is not the cause of trouble.

If trouble occurs in the Type 353 , try to isolate it by quick operational and visual checks. First check the settings of all controls. Then operate the controls to see what effects if any, they have on the trouble. The normal or abnormal operation of each control may help you to establish a trouble symptom. (The cause of trouble which occurs only in certain positions of a control can usually be determined immediately from the trouble symptoms.)

After the trouble symptoms are established, look first for simple causes of trouble. Check to see that the pilot light of the oscilloscope is on, feel for any irregularities in the operation of the controls, listen for any unusual sound, see that the tube heaters are lit, check all power supply voltages, and visually check the entire instrument. The type of trouble will generally indicate the checks to make.

In general, a troubleshooting procedure consists of two parts: circuit isolation and circuit troubleshooting. Since the Type 353 is a complex unit, consisting of many circuits, you should study each schematic carefully while reading the circuit description to help determine which circuit is defective. After isolating the circuit, you can then troubleshoot in the circuit to find the cause of the trouble.

Most troubles will be caused by tube or semiconductor failures. Therefore, when trouble has been isolated to a circuit, the tubes and/or semiconductors in that circuit should be checked first. Be sure to return tubes and transistors found to be good to their original sockets.
If replacing Q214 (Gate Generator), or Q570 (Dual Trace) use all four pins of the transistor so the case is grounded.

Switch wafers shown on the schematics are coded to indicate the position of the wafer on the switches. The number portion of the code refers to the wafer number on the switch assembly. Wafers are numbered from the front of the switch to the rear. The letters $F$ and $R$ indicate whether the front or the rear of the wafer is used to perform the particular switching function.

## Trouble Symptoms

1. A display that may appear as trouble to someone not familiar with sampling techniques can occur when triggering information stops arriving from the Timing Unit. Each display dot is the result of a pulse from the Timing Unit arriving at the Type 353 Gate Generator. If the information stops-even in the middle of a trace-sampling stops immediately. The spot does not extinguish, but it stops progressing across the crt horizontally and starts drifting up or down the crt and ultimately goes out of sight. This is normal, and is not to be confused with trouble. (It is the Memory drifting, without repeated correction.) Should the Timing Unit information begin again, the dot will return to the crt and the interrupted trace will be completed.
2. If the display appears to compress-or limit-at one end of the POSITION control range, set the DC OFFSET control to a position that allows operation with the POSITION control nearer its midrange. Then reduce the input signal to 1 volt or less, peak-to-peak. If the symptom continues, recalibration of the Type $3 S 3$ is necessary.
3. If the dots are spread all over the crt, the SMOOTHING control is too far clockwise and the system loop gain is much greater than unity. Turn the SMOOTHING control counterclockwise.

## Testing Precaution

When observing waveforms in the Type 353 circuitry, always make certain that the test oscilloscope frame is connected to the Type 353 frame. Then if you wish to look at fast pulses inside the Type 353 circuits that are differential in nature, observe the following. The Tektronix P6034 and P6035 signal probes, used on one sampling system to observe another (such as with a Type 3576 or Type $661 / 4 \mathrm{S1}$ ), can be used in a differential fashion singly. If the circuit being measured is not at ground potential, both the probe center conductor and ground return must be ac-coupled. The center conductor can be ac-coupled using a General Radio Type 874 - K in-line capacitor. The ground return can be accoupled (for fast signals) by use of a $0.001-\mu \mathrm{f}$ capacitor at the probe ground clip. Use short leads. If the test oscilloscope frame is not connected to the Type 353 frame, $60-$ cycle stray pickup between the chassis can damage components in the Type 353 .

## Circuit Isolation Technique

If one channel of the Type 353 has no trace but the other channel operates, or if there is a trace but no signal displayed, the following circuit isolation procedure may be of help.
Use a 15-mc bandwidth (or greater) test oscilloscope, such as a Tektronix Type 530A- or 540-Series with Type H or L Plug-In Unit and a 10X Probe.

1. Set the test oscilloscope controls:

| TRIGGERING MODE | AC |
| :--- | ---: |
| TRIGGER SLOPE | -INT (Fig. 4-4), |
|  | + INT (Fig. 4-5) |
| TIME/CM | $0.5 \mu \mathrm{sec} / \mathrm{cm}$ |
| VOLTS/CM | As in Figs. $4-4$ and $4-5$ |


$0.5 \mu \mathrm{sec} / \mathrm{cm} . \quad 1 \mathrm{v} / \mathrm{cm}$.

Fig. 4-4. Ac Amplifier oułpuf with conditions described in text.
2. Connect the two extension cables listed at the beginning of the calibration procedure to operate the Type 353 outside the oscilloscope.
3. Place the Memory subchassis of the channel with trouble on a subchassis extender board and turn on the oscilloscope.
4. Set the Type 3S3 controls:

| MV/DIV | 10 |
| :--- | ---: |
| POSITION | Centered |
| DC OFFSET | Centered |
| Noise-Risetime | FAST RT |
| SMOOTHING | Counterclockwise |



Fig. 4-5. Preamplifier outpul with conditions described in text.
5. Place the P6038 Probe of the problem channel into a $50 \Omega$ environment.
6. Free run the Timing Unit at $10 \mathrm{nsec} / \mathrm{div}$ and 100 dots/ div.
7. Set the NORM-INV switch midway between positions. If the trace does not appear the trouble is after the switch. If the trace appears, the trouble is before the switch. Set the switch to NORM and finish this procedure.
8. Short the feedback loop to ground with a short clip lead at terminal B (for Channel A) or terminal W (for Channel B) of J21. The trace should leave the crt. Grounding the feedback loop permits isolation of a problem circuit in front of the Memory.
9. Connect the test oscilloscope 10X Probe ground clip to the ground side of the LOOP GAIN control R313 (NOT to the chassis), and the probe tip to the junction of R315 and C315. Connecting the probe in any other way can cause the Ac Amplifier to oscillate. The test oscilloscope display will now be that of the Ac Amplifier output. If there is no trouble up to this point, the display will be similar to Fig. 4-4, but not necessarily the same amplitude or polarity. If there is trouble in the Ac Amplifier, there will be no signal.

Adjustment of the RISETIME BAL control should alter or even invert the polarity of the display. Note the position of the RISETIME BAL control and restore it. If the RISETIME BAL control does not change the display, the trouble is after the Ac Amplifier.
10. If there is no pulse in step 9, move the test oscilloscope probe to the Preamplifier output. Connect the probe ground clip to the chassis of the Preamplifier shield and the tip to the output side of Cl 23 (Channel A) or Cl 53 (Channel B).

If there is a pulse similar to Fig. 4-5, and it can be altered in the same manner as the Ac Amplifier pulse was altered in step 9, the trouble is not in the Preamplifier.
11. If the circuits up to the Memory Gate input are working, dc couple the test oscilloscope to the Memory output, terminal F of J 22 for Channel A and terminal F of J23 for Channel B.

Set the test oscilloscope for a free-running sweep at 0.5 $\mu \mathrm{sec} / \mathrm{cm}$ and the vertical deflection for 10 volts $/ \mathrm{cm}$. If the Memory output can be made to go through zero volts (with the RISETIME BAL control), and there is still no trace for the sampling system, the trouble is after the Memory. If the Memory output is locked at either +20 or -12 volts, the trouble is in the Memory.

The test oscilloscope can be made to display a sampled display if the Memory is operating properly. Externally trigger the test oscilloscope at a slow sweep rate. If the Type 3 S3 controls can be made to display a signal on the test oscilloscope, the trouble is in the Inverter, Dual Trace, or Vertical Amplifier, and each can be checked by normal signal tracing methods.

## RESISTOR CODING

The Type 353 uses a number of very stable metal film resistors identified by their gray background color and color coding.


Fig. 4-6. Standard EIA color code for metal film resistors.
If the resistor has three significant figures with a multiplier, the resistor will be EIA color coded. If it has four significant figures with a multiplier, the value will be printed on the resistor. For example, a 333 k resistor will be color coded, but a 333.5 k resistor will have its value printed on.

The color coding sequence is shown in Fig. 4-6, and Table 4-1.

TABLE 4-1

## Color Code Sequence

| COLOR | 1ST <br> SIG. <br> FIG. | 2ND <br> SIG. <br> FIG. | 3RD <br> SIG. <br> FIG. | MULTIPLIER | $( \pm) \%$ <br> TOLER- <br> ANCE |
| :--- | :---: | :---: | :---: | :--- | :---: |
| Black | 0 | 0 | 0 | 1 | - |
| Brown | 1 | 1 | 1 | 10 | 1 |
| Red | 2 | 2 | 2 | 100 | 2 |
| Orange | 3 | 3 | 3 | 1,000 | - |
| Yellow | 4 | 4 | 4 | 10,000 | - |
| Green | 5 | 5 | 5 | 100,000 | 0.50 |
| Blue | 6 | 6 | 6 | $1,000,000$ | 0.25 |
| Violet | 7 | 7 | 7 | $10,000,000$ | 0.10 |
| Grey | 8 | 8 | 8 | $100,000,000$ | 0.05 |
| White | 9 | 9 | 9 | $1,000,000,000$ | - |
| Gold |  |  |  | 0.1 | 5 |
| Silver |  |  |  | 0.01 | - |
| No Color |  |  |  |  | 10 |

## SECTION 5

## CALIBRATION

## Introduction

The following paragraphs outline a procedure for calibrating the Type 353 . The instrument should not require frequent recalibration, but occasional adjustments will be necessary when tubes and other components are changed. Also, a periodic recalibration is desirable from the standpoint of preventive maintenance.

Apparent troubles in the instrument are occasionally the result of improper calibration of one more circuits. Consequently, calibration checks should be an integral part of any troubleshooting procedure. Abnormal indications occurring during calibration checks will often aid in isolating troubles to a definite circuit or stage.

In the instructions that follow, the steps are arranged in the proper sequence for a complete calibration of the instrument. Each numbered step contains the information required to make one check or adjustment or a series of related checks or adjustments. The steps are arranged to avoid unnecessary repetition of checks or adjustments.

## EQUIPMENT REQUIRED

The following equipment is required to perform a complete calibration of the Type 353 with P6038 Probes.

1. A calibrated oscilloscope, preferably a Type 567 with a calibrated Type 3 T77 Sampling Sweep Unit and a Type 6RI Digital Unit. If a Type 567 is not available, a Type 561A or 564 (with a Type 3T77) may be used.
2. A precision voltmeter with an accuracy of at least $0.2 \%$ at 0.6 volt.
3. A $20,000 \Omega /$ volt voltmeter.
4. An ohmmeter.
5. Two flexible special interconnecting cables to go between the Type 353 and the oscilloscope power connectors. Tektronix Part No. 012-066.
6. A Tektronix Type 110 Pulse Generator and Trigger Takeoff System or equivalent.
7. A Tektronix Type 113 Delay Cable or equivalent.
8. A signal generator capable of delivering either square waves or sine waves. Square waves at 1 mc , sine waves at 50 mc , at least 10 volts peak-to-peak into 50 ohms. Tektronix Type 105 Square Wave Generator, or Type 190 Constant Amplitude Signal Generator recommended.
9. Two $50 \Omega$ coax cables, RG-8A/U, with GR connectors, 10-nsec signal delay. Tektronix Part No. 017-501.
10. A $50 \Omega$ coax cable, RG-8A/U, with GR connectors, 5nsec signal delay. Tektronix Part No. 017-502.
11. A $50 \Omega$ coax cable, RG-58A/U, with GR connectors, 2-nsec signal delay. Tektronix Part No. 017-505.
12. Two nonterminating GR-To-P6038 Adapters. Tektronix Part No. 017-076.
13. A GR-To-BNC Adapter. Tektronix Part No. 017-065.
14. Two $50 \Omega 2 \mathrm{X}$ attenuators with GR connectors, such as Tektronix 2XT Attenuator, Part No. 017-046.
15. A $50 \Omega 10 \mathrm{X}$ attenuator with $G R$ connectors, such as Tektronix 10XT Attenuator, Part No. 017-044.
16. A $50 \Omega$ end-line termination with $G R$ connector, such as Tektronix $50 \Omega$ End-Line Termination, Part No. 017-047.
17. A GR-T, $50 \Omega$ coax Tee. Tektronix Part No. 017-069.
18. A GR-To-UHF Adapter, for use with the signal generator, Tektronix Part No. 017-021.
19. An insulated, small-bit screwdriver, for making adjustments.
20. A $5 k$ potentiometer.
21. A $1 \mathrm{k}, 1$-watt, $20 \%$ resistor.
22. A clip lead about $21 / 2$ feet long.
23. A simple switch for use as shown in Fig. 5-5.
24. In case of electrical troubles: A test oscilloscope with at least a $15-\mathrm{mc}$ bandwidth, such as Tektronix Type 530A- or 540-Series, with Type H or L Plug-In Unit. A 10X Attenuator Probe, such as the Tektronix P6000 or P6006. A special (Type 353) subchassis extender board, Tektronix Part No. 012-069.
25. In case of calibration with a new P6038 Probe: A 50 -watt soldering iron with $1 / 8$ inch tip, some plain $60-40$ solder, and a pair of needle-nose pliers.

## PRELIMINARY PROCEDURE

Make a complete visual check of the instrument. If calibration is being done as a result of trouble, check for correct transistors, tubes, and sampler diodes, and that they are in their correct locations. P6038 sampler diodes have a red dot on their cathode end (see Fig. 4-2). Memory gate diodes have a red dot at their cathode end also. If replacing Q214 or Q570, check that all four leads are plugged into the socket.

Use an ohmmeter to check the resistance of each interconnecting plug lead to ground, as shown in Tables 5-1 and 5-2. The probes are not connected for resistance measurements.

Set the Type 353 front-panel controls as follows before making the resistance measurements:

| MV/DIV | 100 |
| :--- | ---: |
| POSITION | Midrange |
| DC OFFSET | Midrange (5 turns from one end) |
| NORM-INV | NORM |
| Mode | A ONLY |
| SMOOTHING | Clockwise |
| Noise-Risetime | FAST RT |
| GAIN | Midrange |

TABLE 5-1

| Resistance to ground at power connector Pll (Horizontal connector). All subchassis in place. |  |  |  |
| :---: | :---: | :---: | :---: |
| Pin No. | Circuit | Ohmmeter Range | Res. |
| 1 | open | X100 k | inf. |
| 2 | open | X100 k | inf. |
| 3 | open | X100 k | inf. |
| 4 | open | $\times 100 \mathrm{k}$ | inf. |
| 5 | ground | X10 | 0 |
| 6 | open | X100 k | inf. |
| 7 | open | X100 k | inf. |
| 8 | open | X100 k | inf. |
| 9 | ground | $\times 10$ | 0 |
| 10 | $+300 \mathrm{v}$ | $\mathrm{X1} \mathrm{k}$ | 10 k |
| 11 | (B) HORIZ | X10 | 0 |
| 12 | Lissajous switch | X10 k | 50 k |
| 13 | open | X100 k | inf. |
| 14 | open | X100 k | inf. |
| 15 | +125v | XI k | $3.5 \mathrm{k}-4 \mathrm{k}$ |
| 16 | -12.2v | X10 | $5 \Omega$ |
| 17 | Lower CRT | XI k | $5 \mathrm{k}-13 \mathrm{k}$ |
| 18 | Timing Unit Trigger In | X100 | 270 ת |
| 19 | braid for 18 | X100 k | 0 |
| 20 | +125v | X1 k | $3.5 \mathrm{k}-4 \mathrm{k}$ |
| 21 | Upper CRT | X10 k | $5 \mathrm{k}-13 \mathrm{k}$ |
| 22 | ground | X100 k | 0 |
| 23 | -100 v | X1k | 2.5 k |
| 24 | Blanking | X1 k | 6 k |

After making resistance measurements, connect the Type 353 to the oscilloscope with the two flexible extension cables. Connect the P6038 Probes to the correct PROBE A and PROBE $B$ connectors. Set the oscilloscope intensity control at about 2 o'clock. Turn on the power and let the system warm up for five minutes.

## CALIBRATION

## Calibration With Original P6038 Probes

Set the Type 353 controls as in the Preliminary Procedure. Set the Type 3 T77 controls as foilows:

| POSITION | Midrange |
| :--- | ---: |
| DOTS/DIV. | 100 |
| HORIZ. MAG. | X1 |
| TIME/DIV. | 5 nSEC |
| VARIABLE | CALIB. |
| DELAY | Fully counterclockwise |
| TRIGGER SENSITIVITY | Clockwise to free run |
| RECOVERY TIME | Fully counterclockwise |
| SWEEP MODE | NORMAL |
| Trigger Source | +EXT. |

TABLE 5-2

| Resistance to ground at P2, all subchassis in place. |  |  |  |
| :---: | :---: | :---: | :---: |
| Pin No. | Circuit | Ohmmeter Range | Res. |
| 1 | CH 'A' Sig Out | Xl k | 2k-6k |
| 2 | Open | X100 k | inf. |
| 3 | CH 'B' Sig Out | X1 k | $2 \mathrm{k}-6 \mathrm{k}$ |
| 4 | Open | X100 k | inf. |
| 5 | CH 'B' Dec. Unit Gnd | X100 k | inf. |
| 6 | CH 'A' Dec. Unit Gnd | $\times 100 \mathrm{k}$ | inf. |
| 7 | Dec. 5 | X100 k | inf. |
| 8 | Dec. 4 | X100 k | inf. |
| 9 | open | X100 k | inf. |
| 10 | open | X100 k | inf. |
| 11 | CH 'A' Switch Pulse | X1 k | 1 k |
| 12 | open | X100 k | inf. |
| 13 | 'V' Units | $\times 100 \mathrm{k}$ | inf. |
| 14 | open | X100 k | inf. |
| 15 | ' $M$ ' Units | X100 k | inf. |
| 16 | open | X100 k | inf. |
| 17 | open | X100 k | inf. |
| 18 | open | X100 k | inf. |
| 19 | open | X100 k | inf. |
| 20 | CH 'B' $\div 1,2,5$, Gnd | X100 k | inf. |
| 21 | CH ' $\mathrm{A}^{\prime} \div 1,2,5$, Gnd | X100 k | inf. |
| 22 | $\div 5$ | X100 k | inf. |
| 23 | $\div 2$ | X100 k | inf. |
| 24 | $\div 1$ | X100 k | inf. |

## 1. Initial Balance

a. Connect the Channel A P6038 Probe into the $50 \Omega$ system of Fig. 5-1.
b. Center the trace with the POSITION control. If the trace is off screen, push the TRACE FINDER button about half way in, so it is obvious the switch is between contacts. Adjust the VERT CENTERING control (R611), on the Vertical Amplifier subchassis so the trace


Fig. 5-1. P6038 Probe tip in 50-ohm system.
is at the graticule centerline. Release the TRACE FIND. ER button. If the trace is still off screen, push the TRACE FINDER button all the way in and bring the trace to the graticule centerline by adjusting the BRIDGE BAL control (R185) and/or the RISETIME BAL control (R175), on the Gate Generator subchassis.
c. Short the crt vertical deflection plates together with a screwdriver at the crt. (Be careful not to ground them to the crt shield.) Note the trace vertical position. Push the TRACE FINDER button half way in and adjust the VERT CENTERING control to place the trace at the vertical position noted when shorting the crt plates.
d. Use the $20,000 \Omega /$ volt meter, and set the DC OFFSET control for +12 volts at the rear contact (slider) of the control.

The DC OFFSET control must stay at this position through step 3.
e. Adjust the SMOOTHING BALANCE control (R335) on the A Memory subchassis while turning the front-panel SMOOTHING control back and forth. The SMOOTHING BALANCE control is correctly set when the trace moves no more than about 0.3 division vertically as the SMOOTHING control is turned from one end to the other (Noise-Risetime switch at FAST RT).
f. Repeat for Channel B. Then let the instrument warm up for another 10 minutes before making further adjustments.

## 2. Vertical Balance

a. Set the Type 353 controls:

| SMOOTHING | Fully clockwise |
| :--- | ---: |
| Noise-Risetime | LOW NOISE |
| POSITION | Midrange |
| MV/DIV | 100 |
| VARIABLE | CALIB |
| NORM-INV | NORM |
| Mode | A ONLY |
| DC OFFSET | As set in step 1 |
| A BRIDGE VOLTS | Midrange |
| (on Gate Generator subchassis) |  |

b. Continue to free run the Timing Unit sweep.
c. Place the Channel A P6038 Probe into the $50 \Omega$ environment of Fig. 5-1.
d. Set the Noise-Riseime switch to FAST RT and adjust the RISETIME BAL control (R175) for no trace shift when operating the Noise-Risetime switch between its two positions. (The trace position will not necessarily be at the graticule center.)
e. Set the MV/DIV switch to 20 . Adjust the BRIDGE BAL control (R185) for no trace shift when operating the Noise-Risetime switch between its two positions. You may adjust the POSITION control to keep the display on the crt.


Fig. 5-2. Type $\mathbf{1 1 0}$, Type 113 system for setting risetime.


Fig. 5-3. Risetime measurement using a Type 6R1 Digital Unit.
f. Repeat step 2 (d) with the MV/DIV switch at 20.
g. Repeat step 2 (e).
h. Repeat steps 2 (a) through 2 (g) for Channel B. Leave the probe as connected for step 3.

## 3. Inverter Zero Adjustment

a. Step 2 must be completed before doing this step.
b. Set Channel B NORM-INV switch to NORM and adjust the B INVERTER ZERO control (R441) so the trace is at the same position as when the NORM-INV switch is at INV. Operate the NORM-INV switch back and forth to be certain the B INVERTER ZERO control is properly adjusted.
c. Repeat for Channel A.

4A. Set Channel B Risetime-With Digital Unit
NOTE
Do not use the subchassis extender in this step.


Fig 5-4. Visual risetime measurement without a Digital Unit.
a. Set up the Type 110, Type 113 system as in Fig. 5-2.
b. Set the Type 110 controls:

| TAKEOFF-EXT. $50 \Omega$ | TAKEOFF |
| :--- | ---: |
| ATTENUATOR | $\div 1$ |
| INVERTER | +1 |
| AMPLIFIER 1 and 2 | X1 each |
| Output Selector | EXT. OUTPUT |
| VOLTAGE RANGE | 5.0 |
| AMPLITUDE | 30 |
| PULSE POLARITY | + |
| PULSE GENERATOR | ON |

c. Set the Type 6R1 Digital Unit controls:

| START SLOPE | FIRST + |
| :--- | ---: |
| TIMING START | B TRACE $10 \%$ |
| STOP SLOPE | FIRST + |
| TIMING STOP | B TRACE $90 \%$ |
| MODE | TIME |
| RESOLUTION | LO |
| DISPLAY TIME | Clockwise |
| CRT DISPLAY | B $100 \%$ ZONE SET (Fig. 5-3) |

d. Set the Type 353 controls:

| Mode | B ONLY |
| :--- | ---: |
| MV/DIV | 50 |
| VARIABLE | CALIB |
| Noise-Risetime | FAST RT |
| SMOOTHING | Fully Counterclockwise |
| POSITION | Midrange |
| DC OFFSET | Center display |

e. Set the Type $3 T 77$ for an externally triggered display at $0.5 \mathrm{nsec} /$ div. Adjust the Type 353 SNAP-OFF CURRENT control (R205) so the digital readout is 0.39 NS.
f. Set the Type 6R1 RESOLUTION switch to HI and the DISPLAY TIME control to midrange. After ten sweeps, the Type 6R1 readout will be the average of the ten sweeps. Set the Type 353 SNAP-OFF CURRENT control so the readout is between 0.394 and 0.402 NS .
The adjustment just completed gives the Type 3S3-P6038 a risetime slightly less than 0.35 nsec when the probe is driven from a pulse generator with a risetime of 50 psec or less.

## 4B. Set Channel B Risetime-Without A Digital Unit

## NOTE

Do not use the subchassis extender in this step.
a. Set up the Type 110 pulser system and the Type $3 \$ 3$ as in step 4A.
b. Set the Type $3 T 77$ for an externally triggered display of $0.1 \mathrm{nsec} /$ div by setting the TIME/DIV. switch to 1 nSEC and the HORIZ. MAG. to X10. The display should be similar to Fig. 5-4.
c. Adjust the Type 353 VARIABLE control until the display is 8 vertical divisions.
d. Adjust the Type 353 SNAP-OFF CURRENT control (R205) until the display risetime is between 0.39 and 0.40 nsec, $10 \%$ to $90 \%$.

## 5. Memory Gate Width and Loop Gain Adjustment

a. Leave the system as connected. Do this step through (d) on Channel B only.
b. Set the Type 3 T 77 controls for an externally triggered display at 1 nsec/div, X1 magnifier, and 10 dots/div. The display should have about 5 to 7 dots in the pulse rise.
c. Check that the Type 353 Noise-Risetime switch is at FAST RT and the SMOOTHING control is fully counterclockwise.
d. Slowly adjust the MEMORY GATE WIDTH control (R215) until the vertical distance between pulse-rise dots is maximum. The adjustment for maximum distance between dots may not coincide with maximum pulse amplitude; disregard pulse amplitude and adjust R215 watching the pulse rise only. If two maximums occur, set the control at the maximum that occurs nearest the counterclockwise end of rotation.
e. Set the Type $3 T 77$ for $2 \mathrm{nsec} / \mathrm{div}$ and 10 dots/div.
f. Adjust the LOOP GAIN control on the B Memory sub chassis for unity loop gain, so the pulse rise looks the same at both 10 and 100 dots/div.
g. Connect the Channel A P6038 Probe to display the Type 110 pulse as was just done with Channel B.
h. Adjust the LOOP GAIN control on the A Memory subchassis for unity loop gain. Set the Type $3 T 77$ for 100 dots/div.
i. Set the system up as at the beginning of step 1. Repeat the SMOOTHING BALANCE adjusments of step 1 (e) and 1 (f) so the trace does not shift vertically when the front-panel SMOOTHING controls are turned.

## 6. Set Channel A Risetime

a. Connect the Channel A P6038 Probe to the system of step 4. Use either step $4 A$ or $4 B$ depending on whether you are using a digital unit.
b. Adjust the A BRIDGE VOLTS control (R169) so that the Channel A risetime is the same as the Channel B risetime.
c. Repeat step 5 (e) for Channel A.

## 7. Vertical Balance

Repeat step 2 (a) through 2 (h) for both channels.


Fig. 5-5. Circuit used to set Type 353 dc gain.

## 8A. Vertical Gain and Digital Gain AdjustmentWith Digital Unit

a. Connect the Channel A P6038 Probe to the system shown in Fig. 5-5. Leave the switch open.
b. Set the Type 353 MV/DIV switch to 100 , the VARIABLE to CALIB, the Noise-Risetime switch to FAST RT, and the SMOOTHING control counterclockwise.
c. Position a free-running trace at -3 divisions.
d. Close the switch and set the 5 k potentiometer for exactly +0.6 volt, as read from the precision voltmeter.
e. Adjust the front-panel GAIN control until the display is exactly +3 divisions, a total of 6 divisions from zero volts to +0.6 volt. Make and break the connection several times to be certain of correct adjustment.
f. Connect a Type 105 or Type 190 to the SIG. IN FOR TRIG. TAKEOFF connector of the Type 110. Turn the Type 110 PULSE GENERATOR switch OFF.
g. Connect the GR 874-T of Fig. 5-5 to the Type 113 Delay Cable end so that the signal generator can be used to operate the Type 353 , and externally trigger the Type $3 T 77$ through the Type 110. The Type 110 trigger takeoff operates without the POWER switch ON. Remove the 2 X attenuator in the line to the Type 113.
h. Set the Type 105 to operate af 1 megacycle, or the Type 190 to operate at 50 megacycles. Adjust the output amplitude so a triggered display is exactly 6 divisions peak-to-peak. See Fig. 5-6. The signal generator output is now 0.6 volt peak-to-peak at the tip of the P6038 Probe.
i. Set the Type 6R1 to read Channel A voltage at LO resolution.
i. Adjust the Type 3S3 A DIGITAL GAIN control (R354) so the digital unit indicates 600 MV .
k. Adjust the front-panel GAIN control so the display is again exactly 6 divisions peak-to-peak. The display will move vertically as the GAIN control is turned; reposition using the POSITION control.
I. Repeat for Channel B.

8B. Vertical Gain and Digital Gain-Without a Digital Unit
a. Leave the Type 353 DIGITAL GAIN (A and $B$ ) controls as adjusted at the factory.
b. Do step $8 \mathrm{~A}(\mathrm{a})$ through 8 A (e) for both channels.

## 9. Smoothing Range Check

a. Connect a probe to the Type 110 pulser system.
b. Set the Type 353 Noise-Risetime switches to FAST RT. Obtain a display at unity loop gain and 10 dots/div.
c. Turn the SMOOTHING control fully clockwise. Set the Noise-Risetime switch to LOW NOISE. The display should show slightly less than unity loop gain. If the display tears, indicating greater than unity loop gain, repeat the Loop gain portion of step 5. There should be no display tearing when the SMOOTHING control is clockwise and the signal source impedance is $50 \Omega$.

(a) Type 105 at $1 \mathrm{mc}, 0.1 \mu \mathrm{sec} / \mathrm{div}$.

(b) Type 190 at $50 \mathrm{mc} .2 \mathrm{nsec} / \mathrm{div}$.

Fig. 5-6. Using a square wave or a sine wave to set DIGITAL GAIN.
d. Repeat for the other channel.

## 10. Noise Check

a. Place a probe into the Type 110 pulser system. Set the Type 353 MV/DIV switch to 100, VARIABLE to CALIB, Noise-Risetime switch to LOW NOISE, and the SMOOTHING control clockwise. Trigger the display and set the Type 110 so the digital unit indicates 300 MV .
b. Set the digital unit RESOLUTION switch to UNSCALED. The readout should still be 300 .
c. Turn the Type $3 S 3$ VARIABLE control clockwise until the unscaled digital unit reading is 600 .
d. Turn off the Type 110 pulser. Leave the probe connected to the Type 113. Free run the Timing Unit sweep. Set the Type 353 MV/DIV switch to 5, being careful not to move the VARIABLE control. The system deflection factor is now 0.5 mv per minor graticule division. The noise should be less than 1 minor division (less than 0.5 mv ).
e. Set the Noise-Risetime switch to FAST RT and the SMOOTHING control counterclockwise. Disregarding $10 \%$ of the noise peaks, the noise should be about 4 minor graticule divisions (about 1.5 to 2 mv ).
f. Repeat for the other channel.

NOTE
If the noise is significantly higher than these limits, look for trouble in one or more of the following possible causes.

## Possible Noise Causes

1. High energy radio frequency radiation in the vicinity of the sampling system.
2. A high degree of sampling bridge volts imbalance, such as a ratio of 5 to 1 or greater between the + and volts to one of the probes. This indicates defective sampling diodes. Details of the diode locations and Tektronix part numbers are in the maintenance section of this manual.

## 11. Final Check

a. Turn off the oscilloscope. Restore any subchassis mounted on the subchassis extender. Install the Type 353 inside the oscilloscope immediately. Do not let it cool.
b. Turn the oscilloscope on and let it warm up for 10 minutes with the side panels in place.
c. Run through a quick check of the balance of a freerunning trace, step 2.

## Recalibration With New P6038 Probe

A new P6038 Probe is either a currently used probe with a new set of sampling diodes, or a new probe never before used on your Type 353. If installing a new probe, be sure to place the correct color band on the probe body.

1. Install the new probe and perform all of the previous procedure.

## 2. Time Coincidence Check

a. Move the 2 X attenuator of the Type 110 pulser system to the output of the Type 113 Delay Cable. Install the side connection of a GR 874-T to the 2 X attenuator, and a GR-To-P6038 Adapter to each remaining Tee connection. Insert a P6038 Probe into each adapter.
b. Operate the pulser system and Type $3 T 77$ for an externally-triggered $0.2 \mathrm{nsec} /$ div display (TIME/DIV: . 2 nSEC; HORIZ. MAG: XI).
c. Set the Type 353 MODE switch to DUAL-TRACE and adjust the Type 3 T77 DELAY control so the dual display shows the pulse rise near the crt center. Carefully position the two displays to be the same vertically.
d. Set both MV/DIV switches to 20 so the top or bottom of the displays is well off the screen, the start is visible, and the pulse rises are essentially vertical.
Each minor horizontal division is 40 psec . If the two pulse-rise positions are more than 60 psec apart, record the difference and determine which rise is Channel A and which rise is Channel B.
e. Fig. 5-7 shows the location of an adjustable time system on the Gate Generator subchassis. For example, if Channel A display should need to be moved to the right 30 psec , move the red and green leads to T160 exactly one centimeter closer to the 22-pin connector. Use a small soldering iron and move both leads equally so they are parallel when moved. A total range of about 100 psec adjustment is available by moving the red and green leads of both channels in opposite directions.
If it is necessary to move the leads just described, be careful not to change the twist as you move them. (Take care not to alter the turns-per-inch of the redgreen leads located at D200, the snap off diode.)


Fig. 5-7. Gate Generator parts location for adjusting co-channel time coincidence.

# SECTION 6 <br> <br> PARTS LIST AND SCHEMATICS 

 <br> <br> PARTS LIST AND SCHEMATICS}

## PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix Field Office.
Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number including any suffix, instrument type, serial number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix Field Office will contact you concerning any change in part number.

ABBREVIATIONS AND SYMBOLS

| a or amp | amperes | mm | millimeter |
| :---: | :---: | :---: | :---: |
| BHS | binding head steel | meg or M | megohms or mega ( $10^{6}$ ) |
| C | carbon | met. | metal |
| cer | ceramic | $\mu$ | micro, or $10^{-6}$ |
| cm | centimeter | n | nano, or $10^{-9}$ |
| comp | composition | $\Omega$ | ohm |
| cps | cycles per second | OD | outside diameter |
| crt | cathode-ray tube | OHS | oval head steel |
| CSK | counter sunk | p | pico, or $10^{-12}$ |
| dia | diameter | PHS | pan head steel |
| div | division | piv | peak inverse voltage |
| EMC | electrolytic, metal cased | plstc | plastic |
| EMT | electroyltic, metal tubular | PMC | paper, metal cased |
| ext | external | poly | polystyrene |
| $f$ | farad | Prec | precision |
| F \& I | focus and intensity | PT | paper tubular |
| FHS | flat head steel | PTM | paper or plastic, tubular, molded |
| Fil HS | fillister head steel | RHS | round head steel |
| $g$ or G | giga, or $10^{9}$ | rms | root mean square |
| Ge | germanium | sec | second |
| GMV | guaranteed minimum value | Si | silicon |
| h | henry | S/N | serial number |
| hex | hexagonal | t or T | tera, or $10^{12}$ |
| HHS | hex head steel | TD | toroid |
| HSS | hex socket steel | THS | truss head steel |
| HV | high voltage | tub. | tubular |
| ID | inside diameter | $v$ or V | volt |
| incd | incandescent | Var | variable |
| int | internal | w | watt |
| $k$ or K | kilohms or kilo (10) | w/ | with |
| kc | kilocycle | w/o | without |
| m | milli, or $10^{-3}$ | WW | wire-wound |
| mc | megacycle |  |  |

SPECIAL NOTES AND SYMBOLS

X000
Part first added at this serial number.
000X Part removed after this serial number.
*000-000 Asterisk preceding Tektronix Part Number indicates manufactured by or for Tektronix, or reworked or checked components.

Use 000-000
Part number indicated is direct replacement.
Internal screwdriver adjustment.
Front-panel adjustment or connector.


FRONT AND ACCESSORIES



RIGHT SIDE


Parts List-Type 353

LEFT SIDE


LEFT SIDE





|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| REF. <br> NO. | PART NO. | SERIAL | $\frac{\text { NO. }}{\text { DISC. }}$ | $\mathbf{Q}$ <br> $\mathbf{T}$ <br> $\mathbf{Y}$. | DESCRIPTION |
| 1 2 <br> 3 <br> 4 <br> 5 <br> 6 <br> 7 <br> 8 <br> 9 <br> 10 | $441-509$ $210-583$ $210-940$ $210-046$ $136-095$ $\ldots 11-081$ $261-035$ $406-635$ $\ldots \ldots \ldots$ $213-035$ $210-438$ $210-259$ $213-055$ $179-794$ $136-161$ $211-081$ $2161-035$ $361-218$ 131 |  |  |  | CHASSIS, Gate Generator <br> Mounting Hardware For Pots: <br> NUT, hex, $1 / 4-32 \times 5 / 16$ inch <br> WASHER, $1 / 4$ ID $\times 3 / 8$ inch OD <br> LOCKWASHER, internal, . 400 OD $\times .261$ inch ID <br> SOCKET, 4 pin transistor <br> Mounting Hardware: (not included) <br> SCREW, $2-56 \times \frac{1}{16}$ inch RHS phillips <br> SPACER, transistor socket <br> BRACKET, pot mounting <br> Mounting Hardware: (not included) <br> SCREW, thread cutting, $4-40 \times 1 / 4$ inch PHS phillips <br> NUT, hex, $1-72 \times 5 / 32$ inch <br> LUG, solder, peewee <br> SCREW, thread cutting, $2-32 \times 3 / 16$ inch PHS phillips <br> CABLE, harness, Gate Generator <br> SOCKET, 3 pin transistor <br> Mounting Hardware: (not included) <br> SCREW, $2-56 \times \frac{1}{16}$ inch RHS phillips <br> SPACER, transistor socket <br> CONNECTOR, chassis mount, 22 pin <br> Mounting Hardware: (not included) <br> SCREW, $4-40 \times 5 / 8$ inch RHS <br> WASHER, $5 S \times 9 / 32$ inch <br> LOCKWASHER, internal, \#4 <br> NUT, hex, $4-40 \times 3 / 16$ inch <br> STRIP, ceramic, $7 / 16$ inch $\times 16$ notches <br> SPACER, nylon |

\begin{tabular}{|c|c|c|c|c|c|}
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& \hline 2 \\
& 3 \\
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& 1 \\
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\end{aligned}
$$

\] \& | Mounting Hardware For Pots: |
| :--- |
| NUT, hex, $1 / 4-32 \times 5 / 16$ inch |
| WASHER, $1 / 4$ ID $\times 3 / 8$ inch OD |
| LOCKWASHER, internal, 400 OD x. 261 inch ID |
| LUG, solder, $1 / 4$ inch |
| SOCKET, 3 pin transistor |
| Mounting Hardware For Each: (not included) |
| SCREW, $2-56 \times \frac{1}{16}$ inch RHS phillips |
| SPACER, transistor socket |
| HOLDER, toroid |
| SPACER, nylon |
| STRIP, ceramic, $7 / 16$ inch $\times 13$ notches |
| SPACER, nylon |
| CABLE, harness, Memory |
| SOCKET, 4 pin tube |
| Mounting Hardware: (not included) |
| SCREW, $2-56 \times 9 / 16$ inch RHS phillips |
| LUG, solder, peewee |
| TUBE, spacer, $1 / 4$ inch |
| LOCKWASHER, internal, \#2 |
| NUT, hex, $2-56 \times 3 / 16$ inch |
| CONNECTOR, chassis mount, 22 pin |
| Mounting Hardware: (not included) |
| SCREW, $4-40 \times 5 / 8$ inch RHS phillips |
| WASHER, $55 \times 9 / 32$ inch |
| LOCKWASHER, internal, \#4 |
| NUT, hex, $4-40 \times 3 / 16$ inch |
| CHASSIS, Memory | <br>

\hline
\end{tabular}





## ELECTRICAL PARTS

Values are fixed unless marked Variable.

## Tektronix

Ckt. No. Part No.
Description

## Capacitors

Tolerance $\pm 20 \%$ unless otherwise stated.
Tolerance of electrolytic capacitors as follows (with exceptions):

$$
\begin{aligned}
3 V-50 V & =-10 \%,+250 \% \\
51 V-350 V & =-10 \%,+100 \% \\
351 V-450 V & =-10 \%,+50 \%
\end{aligned}
$$

| C102 | 281-513 | 27 pf | Cer | 500 v |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C110 | 290-199 | $1 \mu \mathrm{f}$ | EMT | 150 v |  |
| C111 | 281-559 | . $0015 \mu \mathrm{f}$ | Cer | 500 v |  |
| C112 | 283-004 | . $02 \mu \mathrm{f}$ | Disc Type | 150 v |  |
| C117 | 283-051 | . $0033 \mu \mathrm{f}$ | Disc Type | 100 v | 5\% |
| C119 | 281-546 | 330 pf | Cer | 500 v | 10\% |
| C121 | 281-559 | . $0015 \mu \mathrm{f}$ | Cer | 500 v |  |
| C122 | 283-024 | . $1 \mu \mathrm{f}$ | Cer | 30 v |  |
| Cl 23 | 281-536 | . $001 \mu \mathrm{f}$ | Cer | 500 v | 10\% |
| Cl 26 | 290-106 | $10 \mu \mathrm{f}$ | EMT | 15 v |  |
| C127 | 281-559 | . $0015 \mu \mathrm{f}$ | Cer | 500 v |  |
| C129 | 283-003 | . $01 \mu \mathrm{f}$ | Disc Type | 150 v |  |
| C133 | 281-513 | 27 pf | Cer | 500 v |  |
| C140 | 290-199 | $1 \mu \mathrm{f}$ | EMT | 150 v |  |
| C141 | 281-559 | . $0015 \mu \mathrm{f}$ | Cer | 500 v |  |
| C142 | 283-004 | . $02 \mu \mathrm{f}$ | Disc Type | 150 v |  |
| C147 | 283-051 | . $0033 \mu \mathrm{f}$ | Disc Type | 100 v | 5\% |
| C149 | 281.546 | 330 pf | Cer | 500 v | 10\% |
| C151 | 281-559 | . $0015 \mu \mathrm{f}$ | Cer | 500 v |  |
| Cl52 | 283-024 | . $1 \mu \mathrm{f}$ | Cer | 30 v |  |
| C153 | 281-536 | . $001 \mu \mathrm{f}$ | Cer | 500 v | 10\% |
| C156 | 290-106 | $10 \mu \mathrm{f}$ | EMT | 15 v |  |
| C157 | $281-559$ | . $0015 \mu \mathrm{f}$ | Cer | 500 v |  |
| C158 | 283-563 | . $001 \mu \mathrm{f}$ | Mica | 500 v | 10\% |
| C159 | 283-003 | . $01 \mu \mathrm{f}$ | Disc Type | 150 v |  |
| C252 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C261 | 283-023 | . $1 \mu \mathrm{f}$ | Cer | 10 v |  |
| C281 | 283-023 | . $1 \mu \mathrm{f}$ | Cer | 10 v |  |
| C680 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C681 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C682 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C685 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C686 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C689 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C691 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C693 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C695 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C697 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C699 | 283-068 | . $01 \mu \mathrm{f}$ | Cer | 500 v |  |

S/N Range

## Diodes

| Ckt. No. | Tektronix Part No. | Description |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D123 | 152-008 | German | nium T12G |  |  |
| D153 | 152-008 | German | nium T12G |  |  |
| D252 | 152-060 | Zener | 1M20Z10/1N3027A | 20 v |  |
| D681 | 152-066 | Silicon | 1N3194 |  |  |
| D682 | 152-066 | Silicon | 1N3194 |  |  |
| D683 | 152-066 | Silicon | 1N3194 |  |  |
| D686 | 152-066 | Silicon | 1N3194 |  |  |
| D687 | 152-066 | Silicon | 1N3194 |  |  |
| D688 | 152-066 | Silicon | 1N3194 |  |  |

## Connectors

| P11 | $131-149$ | Connector, 24 pin |
| :--- | :--- | :--- |
| P12 | $131-149$ | Connector, 24 pin |
| J21 | $131-220$ | Connector, 22 pin |
| J22 | $131-220$ | Connector, 22 pin |
| J23 | $131-220$ | Connector, 22 pin |
|  |  |  |
| J24 | $131-220$ | Connector, 22 pin |
| J25 | $131-220$ | Connector, 22 pin |
| J26 | $131-220$ | Connector, 22 pin |
| J101 | $131-281$ | Connector, Bendix |
| J131 | $131-281$ | Connector, Bendix |

## Inductors

L110
L121
L127
L129
L140

1151
L157
L159

Q123
Q124
Q153
Q154
*120-183 Toroid, 9T
*120-183 Toroid, 9T
*120-183 Toroid, 9T
276-532 Core, Shield Bead
*120-183 Toroid, 9T
*120-183 Toroid, $9 T$
*120-183
276-532

151-103
151-103
151-103
151-103

Toroid, 97
Core, Shield Bead

## Transisfors

Planar Silicon
Planar Silicon
Planar Silicon
Planar Silicon

## Resisfors

Resistors are fixed, composition, $\pm 10 \%$ unless otherwise indicated.

| R102 | $321-327$ | 24.9 k | $1 / 8 \mathrm{w}$ | Prec | $1 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R103 | $321-450$ | 475 k | $1 / 8 \mathrm{w}$ | Prec | $1 \%$ |
| R104 | $315-103$ | 10 k | $1 / 4 \mathrm{w}$ |  | $5 \%$ |
| R110 | $315-101$ | $100 \Omega$ | $1 / 4 \mathrm{w}$ | $5 \%$ |  |
| R111 | $315-101$ | $100 \Omega$ | $1 / 4 \mathrm{w}$ | $5 \%$ |  |

Resistors (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Descri |  |  | S/N Range |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R115 | 315-122 | 1.2 k | $1 / 4$ w | Var |  | 5\% |  |
| R116 ${ }^{1}$ | 311-423 | 2.5 k |  |  |  | A SMOOTHING |  |
| R117 | 315-122 | 1.2 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R120 | 315-562 | 5.6 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R123 | 321-318 | 20 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R124 | 301-513 | 51 k | 1/2w |  |  | 5\% |  |
| R125 | 315-133 | 13 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R126 | 315-560 | $56 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R132 | 321-327 | 24.9 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R133 | 321-450 | 475 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R134 | 315-103 | 10 k | $1 / 4 \mathrm{w}$ | Var |  | 5\% |  |
| R140 | 315-101 | $100 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R141 | 315-101 | $100 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R145 | 315-122 | 1.2 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R146 ${ }^{2}$ | 311-423 | 2.5 k |  |  |  | B SMOOTHING |  |
| R147 | 315-122 | 1.2 k | 1/4w |  | Prec | $\begin{aligned} & 5 \% \\ & 5 \% \\ & 1 \% \\ & 5 \% \\ & 5 \% \end{aligned}$ |  |
| R150 | 315-562 | 5.6 k | $1 / 4$ w |  |  |  |  |
| R153 | 321-318 | 20 k | $1 / 8 \mathrm{w}$ |  |  |  |  |
| R154 | 301-513 | 51 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R155 | 315-133 | 13 k | $1 / 4 \mathrm{w}$ |  |  |  |  |
| R156 | 315-560 | $56 \Omega$ | 1/4 w |  |  | 5\% |  |
| R252 | 308-069 | 12 k | 8 w |  | WW | 5\% |  |
| R260A | 321-320 | 21 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R260B | 321-291 | 10.5 k | 1/8 w |  | Prec | 1\% |  |
| R260C | 321-252 | 4.12 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R260D | 321-223 | 2.05 k | 1/8 w |  | Prec | 1\% |  |
| R260E | 321-193 | 1 k | 1/8 w |  | Prec | 1\% |  |
| R261A | 321-197 | 1.10 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R261B | 321-199 | 1.15 k | 1/8w |  | Prec | 1\% |  |
| R261C | 321-207 | 1.40 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
|  |  | 2.10 k | 1/8 w |  | Prec | 1\% |  |
| R280A | 321-320 | 21 k | 1/8w |  | Prec | 1\% |  |
| R280B | 321-291 | 10.5 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R280C | 321-252 | 4.12 k | 1/8 w |  | Prec | 1\% |  |
| R280D | 321-223 | 2.05 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R280E | 321-193 | 1 k | 1/8w |  | Prec | $1 \%$ |  |
| R281A | 321-197 | 1.10 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R281B | 321-199 | 1.15 k | 1/8 w |  | Prec | 1\% |  |
| R281C | 321-207 | 1.40 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R281D | 321-224 | 2.10 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |  |
| R341 | 317-428 | 50 k |  | Var |  | A DC OFFSET |  |
| R342 | 323-414 | 200 k | 1/2w |  | Prec | 1\% |  |
| ${ }^{1}$ See footnote page 6-18. |  |  |  |  |  |  |  |
| ${ }^{2}$ See footr | 6-18. |  |  |  |  |  |  |

Resistors (Cont'd)


## Switches

Wired Unwired

| SW1801 | $311-423$ |  |
| :--- | :--- | :--- |
| SW240 | $311-423$ |  |
| SW260 | $260-550 * 262-610$ | Rotary |
| SW280 | $260-550 * 262-610$ | Rotary |
| SW355 | $260-447$ | Slide |

${ }^{1}$ SW180 and R116 furnished as a unit.
${ }^{2}$ SW240 and R146 furnished as a unit.

Switches (Cont'd)


## Parts List-Type 353

## Connectior

| Ckt. No. | Tektronix <br> Part No. |  |
| :--- | ---: | :--- |
| P21 | 131-218 | Connector |
|  |  |  |
|  |  |  |
|  |  |  |
| Q200 | $151-083$ | 2N964 |
| Q214 | $151-015$ | 2N1516 |

## Transformers

## Q214

151-015
2N1516

|  |  |  | Resis |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R160 | 315-101 | $100 \Omega$ | 1/4w |  |  | 5\% |
| R165 | 315-102 | 1 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |
| R167 | 315-102 | 1 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |
| R168 | 315-333 | 33 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |
| R169 | 311-078 | 50 k |  | Var |  | 'A' BRIDGE VOLTS |
| R171 | 322-469 | 750 k | $1 / 4 \mathrm{w}$ |  | Prec | 1\% |
| R172 | 321-440 | 374 k | 1/8w |  | Prec | 1\% |
| R174 | 321-625 | 5.88 k | 1/8w |  | Prec | 1\% |
| R175 | 311-171 | 5k |  | Var |  | 'A' RISETIME BAL |
| R176 | 321-625 | 5.88 k | $1 / 8 \mathrm{w}$ |  | Prec | 1\% |
| R 178 | 321-423 | 249 k | 1/8w |  | Prec | 1\% |
| R181 | 315-562 | 5.6 k | $1 / 4$ w |  |  | 5\% |
| R183 | 316-334 | 330 k | $1 / 4 \mathrm{w}$ |  |  |  |
| R185 | 311-382 | 1 meg |  | Var |  | 'A' BRIDGE BAL |
| R187 | 321-222 | 2 k | 1/8 W |  | Prec | $1 \%$ |
| R189 | 315-562 | 5.6 k | 1/4w |  |  | 5\% |
| R202 | 315-102 | 1 k | 1/4w |  |  | 5\% |
| R204 | 304-271 | $270 \Omega$ | 1 w |  |  |  |
| R205 | 311-380 | $500 \Omega$ |  | Var | WW | SNAP-OFF CURRENT |
| R207 | 315-222 | 2.2 k | $1 / 4 w$ |  |  | 5\% |
| R209 | 315-271 | $270 \Omega$ | 1/4w |  |  | 5\% |
| R213 | 315-622 | 6.2 k | $1 / 4 \mathrm{w}$ |  |  |  |
| R215 | 311-329 | 50 k |  | Var |  | MEMORY GATE WIDTH |
| R216 | 315-621 | $620 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |
| R217 | 315-100 | $10 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |
| R 220 | 315-101 | $100 \Omega$ | 1/4w |  |  | 5\% |
| R 225 | 315-102 | 1 k | $1 / 4$ w |  |  | 5\% |
| R227 | 315-102 | 1k | $1 / 4 \mathrm{w}$ |  |  | 5\% |
| R228 | 315-563 | 56 k | $1 / 4 w$ |  |  | 5\% |
| R231 | 322-469 | 750 k | $1 / 4 \mathrm{w}$ |  | Prec | 1\% |
| R232 | 321-440 | 374 k | 1/8w |  | Prec | 1\% |
| R234 | $321-625$ | 5.88 k | $1 / 8 w$ |  | Prec | 1\% |
| R235 | 311.171 | 5 k |  | Var |  | 'B' RISETIME BAL |
| R236 | 321.625 | 5.88 k | 1/8 w |  | Prec | 1\% |
| R238 | 321-423 | 249 k | 1/8 w |  | Prec | 1\% |


| Ckt. No. | Tekłronix Part No. | Description |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R241 | 315-562 | 5.6 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |
| R243 | 316-334 | 330 k | $1 / 4$ w |  |  |  |
| R245 | 311-382 | 1 meg |  | Var |  | 'B' BR |
| R247 | 321-222 | 2 k | 1/8 W |  | Prec | 1\% |
| R249 | 315-562 | 5.6 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |
|  | Transformers |  |  |  |  |  |
| $\begin{aligned} & \text { T160 } \\ & \text { T200 } \\ & \text { T220 } \end{aligned}$ | *120-316 | Toroid, |  |  |  |  |
|  | *120-314 | Toroid, |  |  |  |  |
|  | *120-316 | Toroid, |  |  |  |  |
|  | MEMORY (2 required) Series B |  |  |  |  |  |
|  | *605-018 | Comple |  |  |  |  |
|  | Capacitors |  |  |  |  |  |
| C306 | 283-026 | . $2 \mu \mathrm{f}$ | Cer |  | 25 v |  |
| C315 | 283-581 | 510 pf | Mica |  | 300 v | 5\% |
| C325 | 283-026 | . $2 \mu \mathrm{f}$ | Cer |  | 25 v |  |
| C332 | 283-068 | . $01 \mu \mathrm{f}$ | Cer |  | 500 v |  |
| C365 | 281-504 | 10 pf | Cer |  | 500 v | 10\% |
| C373 | 283-004 | . $02 \mu \mathrm{f}$ | Disc Type |  | 150 v |  |
| C375 | 283-579 | 100 pf | Mica |  | 500 v | 5\% |
| C383 | 290-026 | $5 \mu \mathrm{f}$ | EMT |  | 25 v |  |
| C385 | 290-106 | $10 \mu \mathrm{f}$ | EMT |  | 15 v |  |
| C386 | 283-004 | . $02 \mu \mathrm{f}$ | Disc Type |  | 150 v |  |

Model No.

5\%
'B' BRIDGE BAL
$1 \%$
$5 \%$

Transformers

Toroid, 4T
oroid, 4T-2T
Toroid, 4T

## Diodes

D324
D330
D332
D342
D343

D362
D372

152-008
152-008

131-218
131-218
152-016
152-071
152-071
*152-145

P23

Connector, 22 pin
Connector, 22 pin

Connectors
Zener RT-6
Germanium ED2007
Germanium ED2007
Matched pair

Germanium T12G
Germanium T12G
(A)

| Transistors |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. |  | Description |  |  |  | Model No. |
| Q304 | 151-085 | 2N741 |  |  |  |  |  |
| Q313 | 151-085 | 2N741 |  |  |  |  |  |
| Q364 | 151-103 | Planar Silicon |  |  |  |  |  |
| Q374 | 151-103 | Planar Silicon |  |  |  |  |  |
|  | Resistors |  |  |  |  |  |  |
| R301 | 301-185 | 1.8 meg | 1/2w |  |  | 5\% |  |
| R304 | 301-303 | 30 k | $1 / 2 \mathrm{w}$ |  |  | 5\% |  |
| R306 | 315-100 | $10 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R312 | 321-335 | 30.1 k | $1 / 8 \mathrm{w}$ |  | Prec | $1 \%$ |  |
| R313 | 311-066 | $500 \Omega$ | . 2 w | Var |  | LOOP GAIN |  |
| R315 | 315-101 | $100 \Omega$ | $1 / 4$ w |  |  | 5\% |  |
| R323 | 301-683 | 68 k | $1 / 2 \mathrm{w}$ |  |  | 5\% |  |
| R324 | 315-823 | 82 k | 1/4 w |  |  | 5\% |  |
| R326 | 301-363 | 36 k | $1 / 2 \mathrm{w}$ |  |  | 5\% |  |
| R328 | 315-202 | 2 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R329 | 315-202 | 2 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R334 | 315-221 | $220 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R335 | 311-328 | 1 k |  | Var |  | SMOOTHING | BALANCE |
| R336 | 301-303 | 30 k | 1/2w |  |  | 5\% |  |
| R339 | 315-621 | $620 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R351 | 315-101 | $100 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R353 | 301-473 | 47 k | 1/2w |  |  | 5\% |  |
| R362 | 315-223 | 22 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R364 | 301-563 | 56 k | $1 / 2 w$ |  |  | 5\% |  |
| R374 | 301-333 | 33 k | 1/2w |  |  | 5\% |  |
| R385 | 315-470 | $47 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |
| R386 | 307-053 | 3.3 ת | $1 / 2 \mathrm{w}$ |  |  | 5\% |  |

Transformer
*120-313 Toroid, 25T

Electron Tube

## Diodes

| Ckt. No. | Tektronix <br> Part No. |  | Description |
| :--- | ---: | ---: | ---: | ---: |

## Connector

P24
131-218
Connector, 22 pin

Transistors

| Q424 | $151-103$ |
| :--- | ---: |
| Q434 | $* 153-522$ |
| Q444 | $151-103$ |
| Q454 | $* 153-522$ |

Planar Silicon
Tek Spec, checked Planar Silicon Tek Spec, checked

## Model No.

## dUAL TRACE Series D



D515
D516
D525

131-218
152-141
152-141
152-141
152-008

152-008
152-071
152-008
Q514
Q524
Q545
Q555
Q564
Q570

Q514
Q524
Q545
Q555
Q564
Q570

| $151-076$ | 2N2048 |
| :--- | :--- |
| $151-076$ | 2N2048 |
| $151-071$ | 2N1305 |
| $151-071$ | 2N1305 |
| $151-040$ | 2N1302 |
| $151-063$ | PADT 35 |

R513
R514
R519
R523
R524

| $321-277$ | $7.5 k$ | $1 / 8 w$ |
| :--- | :--- | :--- |
| $323-351$ | $44.2 k$ | $1 / 2 w$ |
| $323-433$ | $316 k$ | $1 / 2 w$ |
| $321-277$ | $7.5 k$ | $1 / 8 w$ |
| $323-351$ | $44.2 k$ | $1 / 2 w$ |

## Diodes

## Connector

Connector, 22 pin

## Transistors

## Resistors

Model No. $500 \mathrm{v} \quad 10 \%$
350 v
350 V
350 v
500 v

1N3605
1N3605
1N3605
1N3605
Germanium T12G

Germanium T12G
Germanium ED2007
Germanium T12G

Transis
2N2048
2N2048
2N1305
2N1302
PADT 35

| $1 / 8 w$ | Prec | $1 \%$ |
| :--- | :--- | :--- |
| $1 / 2 w$ | Prec | $1 \%$ |
| $1 / 2 w$ | Prec | $1 \%$ |
| $1 / 8 w$ | Prec | $1 \%$ |
| $1 / 2 w$ | Prec | $1 \%$ |

Resistors (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Description |  | Model No |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R541 | 315-562 | 5.6 k | 1/4 w | 5\% |  |
| R544 | 301-821 | $820 \Omega$ | 1/2w | 5\% |  |
| R545 | 303-223 | 22 k | 1 w | 5\% |  |
| R546 | 315-124 | 120 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R547 | 315-223 | 22 k | $1 / 4$ w | 5\% |  |
| R548 | 315-223 | 22 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R549 | 301-683 | 68 k | $1 / 2 \mathrm{w}$ | 5\% |  |
| R551 | 315-562 | 5.6 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R555 | 303-223 | 22 k | 1 w | 5\% |  |
| R556 | 315-124 | 120 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R557 | 315-223 | 22 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R558 | 315-223 | 22 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R559 | 301-683 | 68 k | 1/2w | 5\% |  |
| R561 | 315-223 | 22 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R564 | 301-563 | 56 k | $1 / 2 \mathrm{w}$ | 5\% |  |
| R565 | 315-222 | 2.2 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R567 | 315-152 | 1.5 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R570 | 301-153 | 15 k | $1 / 2 \mathrm{w}$ | 5\% |  |
| R571 | 316-474 | 470 k | $1 / 4 \mathrm{w}$ |  |  |
| R572 | 315-103 | 10 k | $1 / 4 \mathrm{w}$ | 5\% |  |
| R574 | 315-222 | 2.2 k |  |  |  |
| R577 | 315-101 | $100 \Omega$ | $1 / 4 w$ | $5 \%$ |  |
| Transformer |  |  |  |  |  |
| T570 | *120-315 | Toroid, 4T-10T-15T |  |  |  |

## VERTICAL AMPLIFIER Series E

*605-021
Complete Board

## Capacitors

| C614 | $283-026$ | $.2 \mu \mathrm{f}$ | Cer | 25 v |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| C619 | $281-501$ | 4.7 pf | Cer | 500 v | $\pm 1 \mathrm{pf}$ |
| C621 | $283-068$ | $.01 \mu \mathrm{f}$ | Cer | 500 v |  |
| C642 | $290-199$ | $1 \mu \mathrm{f}$ | EMT | 150 v |  |
| C654 | $290-159$ | $2 \mu \mathrm{f}$ | EMT | 150 v |  |
| C662 | $283-068$ | $.01 \mu \mathrm{f}$ | Cer |  |  |

## Diodes

| D612 | $152-107$ | Silicon T160 |  |
| :--- | :--- | :--- | :--- |
| D615 | $152-100$ | Zener TM120Z5/1N3046B | 120 V |
| D632 | $152-008$ | Germanium T12G |  |
| D672 | $152-008$ | Germanium T12G |  |

## Connector

| Ckt. No. | Tektronix <br> Part No. |  |
| :--- | ---: | :--- |
| P26 | $131-218$ |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
| Q614 | $151-103$ | Planar Silicon |
| Q624 | $* 153-521$ | Tek Spec, checked |
| Q634 | $* 153-521$ | Tek Spec, checked |
| Q654 | $151-103$ | Planar Silicon |
| Q664 | $* 153-521$ | Tek Spec, checked |
| Q674 | $* 153-522$ | Tek Spec, checked |

## Resisfors












| VOLTAGE READINGS WERE OBTAINED |  |
| :---: | :---: |
| UNDER FOLLOWING CONDITIONS: |  |
| CONTROLS | SETTINGS |
| DC OFFSET | Balanced |
| Trace | Centered |

PROBE TERMINATED INTO $50 \Omega$
$C M D$
863
MEMORY
SERIES-B MODEL-1

(1) INTERCONNECTOR DIAGRAM
(3) PREAMPLIFIER



TYPE 353 PLUG-IN
A


CMD
863
DUAL TRACE
SERIES-D
MODEL-1


TYPE 353 PLUG-IN


CMD
863

VERTICAL AMPLIFIER
SERIES-E
MODEL-I

## PARIS IIST CORRECIIONS

## DUAL TRACE Series D

ADD:

| R680* | $308-298$ | $.560 \Omega$ | 3 w | WW | $5 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: |
| R682** | $308-230$ | 2.7 k | 3 w | WW | $5 \%$ |

* Added between pin 15 and pin 20 of connector Pll.
** Added between pin 6 and pin 10 of connector P11.

TYPE 3S3 - TENT. S/N 170
PARTS LIST CORRECTION

## CHANGE TO:

| R115 | $315-222$ | $2.2 k$ | $1 / 4 w$ | $5 \%$ |
| :--- | :--- | :--- | :--- | :--- |
| R127 | $315-432$ | $4.3 k$ | $1 / 4 w$ | $5 \%$ |
| R145 | $315-222$ | $2.2 k$ | $1 / 4 w$ | $5 \%$ |
| R157 | $315-432$ | $4.3 k$ | $1 / 4 w$ | $5 \%$ |

ADD:

|  | R122 | $315-182$ | 1.8 k | $1 / 4 \mathrm{w}$ |
| ---: | ---: | :--- | :--- | :--- |
| R152 | $315-182$ | 1.8 k | $1 / 4 \mathrm{w}$ | $5 \%$ |
| R188 | $316-185$ | 1.8 meg | $1 / 4 \mathrm{w}$ | $10 \%$ |
| R248 | $316-185$ | 1.8 meg | $1 / 4 \mathrm{w}$ | $10 \%$ |
| P J2l |  |  | SCHEMATIC CORRECTIONS |  |

PREAMPLIFIER INPUT CHANGES


CHANGES IN 'A' AND 'B' PREAMPLIFIER OUTPUT

TYPE 3S3

## PARTS LIST CORRECTIONS

## CHANGE TO:

| R252 | $308-023$ | 10 k | 10 w | ww | $5 \%$ |
| :--- | :--- | :--- | :--- | :--- | :---: |
| R374 | $301-302$ | 30 k | $1 / 2 \mathrm{w}$ | $5 \%$ | (MEMORY BOARD) |
| R433 | $315-152$ | 1.5 k | $1 / 4 \mathrm{w}$ | $5 \%$ | (INVERTER BOARD) |
| R453 | $315-152$ | 1.5 k | $1 / 4 \mathrm{w}$ | $5 \%$ | (INVERTER BOARD) |
|  |  |  |  |  |  |
| ADD |  |  |  |  |  |
|  |  |  |  |  |  |
| R373 | $315-132$ | 1.3 k | $1 / 4 \mathrm{w}$ | $5 \%$ | (MEMORY BOARD) |

## PARTS LIST CORRECTIONS

CHANGE TO:

| C200 | $281-504$ | 10pf | Cer | 500 v | (GATE GENERATOR BOARD) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R124 | $301-223$ | 22 k | $1 / 2 \mathrm{w}$ | $5 \%$ |  |
| R154 | $301-223$ | 22 k | $1 / 2 \mathrm{w}$ | $5 \%$ |  |
| R204 | $308-231$ | $220 \Omega$ | 3 w | $5 \%$ | (GATE GENERATOR BOARD) |

ADD:

| R127 | $315-562$ | 5.6 k | $1 / 4 \mathrm{w}$ | $5 \%$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R157 | $315-562$ | 5.6 k | $1 / 4 \mathrm{w}$ | $5 \%$ |  |
| R433 | $315-102$ | 1 k | $1 / 4 \mathrm{w}$ | $5 \%$ | (INVERTER BOARD) |
| R453 | $315-102$ | 1 k | $1 / 4 \mathrm{w}$ | $5 \%$ | (INVERTER BOARD) |

## SCHEMATIC CORRECTION



PART. PREAMP. DIAG.


PART. INVERTER DIAG.


PART. GATE GEN. DIAG.

