## INSTRUCTION

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## WARRANTY

All Tektronix instruments are warranted against defective materials and workmanship for one year. Tektronix transformers, manufactured in our own plant, are warranted for the life of the instrument.

Any questions with respect to the warranty mentioned above should be taken up with your Tektronix Field Engineer.

Tektronix repair and replacement-part service is geared directly to the field, therefore all requests for repairs and replacement parts should be directed to the Tektronix Field Office or representative in your area. This procedure will assure you the fastest possible service. Please include the instrument Type and Serial or Model Number with all requests for parts or service.

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Serial number 2000 and up.


Serial number 1999 and below
Fig. 1-1. Type 556 Oscilloscopes.

## SECTION 1

## CHARACTERISTICS

Change information, if any, affecting this section is found at the rear of the manual.

## Introduction

The Type 556 Oscilloscope-is a versatile dual-beam laboratory type instrument providing accurate voltage and time measurements in the $D C$ to 50 MHz frequency range. Two complete horizontal and vertical deflection systems permit completely indepentent operation of the two beams.

The Upper Beam can display the signal from either the left or right vertical plug-in unit and may be controlled by either the A or B time base or an external signal. The Lower Beam displays the signal from the right plug-in and the sweep is controlled by the B time base or an external signal. The left and right plug-in compartments accept all letter series and 1 -series plug-ins.

Special circuits within the oscilloscope provide selection of an accurate, continuously-variable delay when using the

B sweep. The $B$ sweep may be delayed by the A sweep from $0.1 \mu \mathrm{~s}$ to 50 s (calibrated) after application of a trigger pulse. This feature permits the delayed $B$ sweep to expand a selected portion of the undelayed $A$ sweep, thereby providing precise time measurements and detailed observation of the signal. Both the delayed and undelayed sweeps can be presented simultaneously on the oscilloscope screen. The Upper Beam trace has an intensified zone indicating the portion of the signal being displayed by the B sweep and Lower Beam.

The instrument is designed to operate over an ambient temperature range of $0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$. Performance specifications that are given in the center column apply over this temperature range after a warmup time of 20 minutes. Supplemental information describing a characteristic or a feature is also included in this portion of the manual.

## VERTICAL AMPLIFIERS

| Characteristics | Performance Specification | Supplemental Information |
| :--- | :--- | :--- |
| Frequency Response | DC to $\geq 50 \mathrm{MHz}$ at 3 dB down with a l-series <br> plug-in unit having a risetime of 3.12 ns or less. | $\leq 6.25 \mathrm{~ns}$. Indicated risetime of 6.93 ns <br> with a Test Load Plug-In Unit (Tektronix <br> Part No. 067-0521-00) having a risetime <br> of 3 ns. |
| Risetime |  | $\leq 2.25 \%$ peak overshoot, rounding, ringing or <br> tilt. |
| Applies to all three vertical modes with <br> Test Load Plug-In Units. |  |  |
| Gain Change with Line Voltage <br> Change | $\leq 1 \%$ from 147 VAC peak to 178 VAC peak. |  |

## A \& B SWEEP GENERATORS

| Calibration Accuracy $5 \mathrm{~s} / \mathrm{cm}$ to $0.1 \mu \mathrm{~s} / \mathrm{cm}$ | $\pm 3 \%$ of displayed time between two points displayed within the middle 8 cm . |  |
| :---: | :---: | :---: |
| $\times 10$ Magnified Display | $\pm 5 \%$ of displayed time between any two points $\geq 1 \mathrm{~cm}$ apart displayed within the middle 8 cm . | Calibrated from 4 cm to 70 cm from sweep start. Extends fastest sweep rate to $10 \mathrm{~ns} / \mathrm{cm}$. |
| Variable Time/Cm Range | $\geq 2.5: 1$. | Extends slowest sweep to approximately $12.5 \mathrm{~s} / \mathrm{cm}$. |
| Sweep Length | $10.5 \mathrm{~cm} \pm 0.5 \mathrm{~cm}$ | At $1 \mathrm{~ms} / \mathrm{cm}$. |
| VARIABLE TIME DELAY |  |  |
| Delay Time Accuracy $5 \mathrm{~s} / \mathrm{cm}$ to $1 \mu \mathrm{~s} / \mathrm{cm}$ | $\pm 1 \%$ of indicated delay time $\pm 2 \%$ of A TIME/CM setting + fixed delay of $\leq 150 \mathrm{~ns}$ in system. | $1 \%$ of A TIME/CM setting corresponds to 1 minor division on the DELAY-TIME MULTIPLIER dial. |
| $0.5 \mu \mathrm{~s} / \mathrm{cm}$ to $0.1 \mu \mathrm{~s} / \mathrm{cm}$ | $\pm 1 \%$ of indicated delay time $\pm 5 \%$ of A TIME/CM setting + fixed delay of $\leq 150 \mathrm{~ns}$ in system. | For additional information refer to Fig. 2-10 in the Operation Instructions. |

## Characteristics-Type 556

| Characteristics | Performance Specification | Supplemental Information |
| :---: | :---: | :---: |
| Incremental Delay Time Accuracy <br> $5 \mathrm{~s} / \mathrm{cm}$ to $1 \mu \mathrm{~s} / \mathrm{cm}$ $\pm 1 \%$ of indicated incremental delay <br> time $\pm 4 \%$ of $\mathrm{T} \mid \mathrm{ME} / \mathrm{CM}$ setting. Incremental Delay Time is the difference <br> between two delay time readings. |  |  |
| $\overline{0.5} \mu \mathrm{~s} / \mathrm{cm}$ to $0.1 \mu \mathrm{~s} / \mathrm{cm}$ | $\pm 1 \%$ of indicated incremental delay time $\pm 7 \%$ of A TIME/CM setting. | For additional information refer to Page 2-24 in the Operating Instructions. |
| Short Term Jitter | $\leq 1$ part in 20,000 of the available delay time. |  |
| EXTERNAL HORIZONTAL AMPLIFIERS |  |  |
| Ext. Horizontal Deflection Factor | $\leq 0.1 \mathrm{~V} / \mathrm{cm}$ with DISPLAY MAG in $\times 10$ position. |  |
| Transient Response | $\pm 3 \%$ peak overshoot, rounding, ringing or tilt. |  |
| Variable Range | $\geq 10: 1$ |  |
| Frequency Response | DC to $\geq 400 \mathrm{kHz}$ at 3 dB down. VARIABLE control set fully cw. |  |
| Maximum Input Voltage | 50 V combined DC + peak AC. | With DISPLAY MAG in $\times 10$ position. |
| Input C |  | Approximately 65 pF . |
| A \& B TRIGGERING FEATURES |  |  |
| Characteristic | Feature |  |
| Source | Internal Normal (from left or right trigger pick-off circuit within the vertical amplifier), Internal Plug-In (from one of the channels in the left or right Type 1A1 or 1A2 Plug-In Unit), Line and External. |  |
| Coupling | Capacitive (AC), low-frequency reject (AC LF REJ), high-frequency reject (AC HF REJ) or direct (DC). |  |
| Slope | Triggering on positive-or-negative-going portion of triggering signal. |  |
| Mode: <br> Auto Stability | Free runs sweep in absence of a triggering signal; instrument can be triggered on signals $\geq 30 \mathrm{~Hz}$. |  |
| Triggered | Triggered at an adjustable level. |  |
| Jitter | $\leq 2 \mathrm{~ns}$. |  |
| LEVEL Control Range: Normal | $\geq \pm 2 \mathrm{~V}$. |  |
| $\times 10$ Increase | $\geq \pm 20 \mathrm{~V}$. |  |
| $\begin{aligned} & \text { External Trigger Input: } \\ & \text { R \& C } \end{aligned}$ | Approximately 1 megohm paralleled by approximately 35 pF . |  |
| Volts | 50 V maximum ( DC plus peak AC ). |  |

## A \& B TRIGGERING SENSITIVITY

| Trigger Coupling/Source |  | To 10 MHz | To 50 MHz |
| :---: | :---: | :---: | :---: |
| AC : <br> INT NORM |  | $\leq 2 \mathrm{~mm}$ display amplitude above 60 Hz . | $\leq 1 \mathrm{~cm}$ display amplitude. |
| EXT |  | $\leq 0.2 \mathrm{~V}$ above 60 Hz . | $\leq 0.4 \mathrm{~V}$. |
| AC LF REJ: <br> INT NORM | $\begin{aligned} & \geq 3 \mathrm{~cm} \text { display amplitude } \\ & \text { at } 30 \mathrm{~Hz} \text {. } \end{aligned}$ | $\leq 2 \mathrm{~mm}$ display amplitude above 2.5 kHz . | $\leq 1 \mathrm{~cm}$ display amplitude. |
| EXT | $\geq 3 \mathrm{~V}$ at 30 Hz . | $\leq 0.2 \mathrm{~V}$ above 2.5 kHz . | $\leq 0.4 \mathrm{~V}$. |
| AC HF REJ: <br> INT NORM | $\leq 2 \mathrm{~mm}$ display amplitude from 60 Hz to $60 \mathrm{kHz}, \geq 1 \mathrm{~cm}$ at 6 MHz . |  |  |
| EXT | $\leq 0.2 \mathrm{~V}$ from 60 Hz to 60 kHz , $\geq 1 \mathrm{~V}$ at 6 MHz . |  |  |
| DC |  | $\leq 3.5 \mathrm{~mm}$ display amplitude. | $\leq 2 \mathrm{~cm}$ display amplitude. |
| EXT |  | $\leq 0.2 \mathrm{~V}$. | $\leq 0.4 \mathrm{~V}$. |
| INT PLUG IN | Characteristics that apply for the EXT trigger input also apply to the Int Plug-In interconnection (pin 5 of plug-in connectors J 11 and J12). |  |  |

## AMPLITUDE CALIBRATOR

| Characteristic | Performance Specification | Supplemental Information |
| :--- | :--- | :--- |
| Voltage Accuracy | $\pm 2 \%$. |  |
| 5 mA Current Loop Accuracy | $\pm 2 \%$. |  |
| Repetition Rate | $1 \mathrm{kHz} \pm 25 \%$ |  |
| Duty Cycle | $45 \%$ to $55 \%$. | 70 pF load. |
| Risetime | One-half indicated voltage $\pm 2 \%$ when termi- | Applies to AMPLITUDE CALIBRATOR <br> switch positions from 0.2 mV to 0.2 V <br> nated into 50 ohms $\pm 0.1 \%$. |
| Terminated Voltage Accuracy |  |  |

## Z AXIS INPUTS

| Sensitivity |  | 10 V P to $P$ causes noticeable modula- <br> tion intensity. |
| :--- | :--- | :--- |
| Input $R$ at DC |  | 1 megohm $\pm 10 \%$. |

FRONT-PANEL OUTPUT SIGNALS

| A GATE | $\geq 8 \mathrm{~V}$ positive-going pulse. | With baseline at zero volts. Time coin- <br> cident with the A sweep. Maximum <br> current is 10 mA . Recommended load <br> resistance $\geq 1 \mathrm{k} \Omega$. |
| :--- | :--- | :--- |
| B GATE | $\geq 8 \mathrm{~V}$ positive-going pulse. | With baseline at zero volts. Time coin- <br> cident with the B sweep. Maximum <br> current is $10 \mathrm{~mA} . \quad$ Recommended load <br> resistance $\geq 1 \mathrm{k} \Omega$. |
| DLY'D TRIG | $\geq 7 \mathrm{~V}$ positive-going pulse into a $\geq 1 \mathrm{k} \Omega$ load. |  |
| A SAlse occurs at the end of the A sweep |  |  |
| delay period. |  |  |

## POWER SOURCE REQUIREMENTS

| For serial numbers 2000 and up |  |  |  |
| :---: | :---: | :---: | :---: |
| Regulating Range Selection: | AC RMS Range $\quad \leq 2 \%$ ic distortion put power | AC Peak Operating Range ( $>2 \%$ harmonis distortion ${ }^{1}$ ) | A Line Voltage Selector assembly facilities selection of a regulating range compatible with the actual line voltage. |
| $\begin{aligned} & 115 \text { Volts } \\ & \text { LO } \end{aligned}$ | 90 to 110 V | 127 to 156 V |  |
| M | 104 to 126 V | 147 to 178 V |  |
| HI | 112 to 136 V | 158 to 192 V |  |
| 230 Volts |  |  |  |
| LO | 180 to 220 V | 254 to 311 V |  |
| M | 208 to 252 V | 294 to 356 V |  |
| HI | 224 to 272 V | 316 to 384 V |  |

${ }^{1}$ Crest Factor $=\frac{\text { Peak } V}{\text { RMS } V}=$ between 1.30 and 1.414.

| Characteristic | Performance Specification | Supplemental Infromation |
| :---: | :---: | :---: |
| For serial numbers 100-1999 |  |  |
| Normal Line: | AC RMS Operating AC Peak Operating Range ( $\leq 2 \%$ harmon- Range ( $>2 \%$ harmonic distortion of the in- ic distortion ${ }^{1}$ ) put power waveform) |  |
| 115 VAC Nominal | 100 to 130 V | Normally wired at the factory for this voltage unless directed otherwise. |
| 230 VAC Nominal | 200 to 260 V V 284 to 366 V |  |
| Low Line: 104 VAC Nominal | 90 to $117 \mathrm{~V} \quad 127$ to 165 V |  |
| 208 VAC Nominal | 180 to 234 V 254 to 330 V |  |

## CRT AND DISPLAY

| Characteristic | $\quad$ Information |
| :--- | :--- |
| Tube Type | T5560-31-1. Dual-Beam, round, glass envelope. Tektronix Part No. 154-0500-00. |
| Phosphor | P31 standard. Others available on special order. |
| Accelerating Potential | Approximately $10 \mathrm{kV} ;$ gun potential is 2 kV. |
| Scan Area | $\geq 6 \mathrm{~cm}$ vertical by 10 cm horizontal per beam. Beams can be overlapped in a 4 cm area. |
| Graticule Type | Internal. 8 cm vertical by 10 cm horizontal. Each major division is $1 \mathrm{~cm} ;$ four corners are <br> omitted. |
| Graticule Illumination | Variable edge lighting. |
| Internal Unblanking | DC-coupled to CRT control grids from the Sweep Generators. |
| Orthogonality | Within $\pm 1 \%$. |
| Trace Rotation Range | Sufficient to align traces with their respective graticule lines. |
| Beam Finder | Limits traces within graticule area. |

## ELECTROMAGNETIC INTERFERENCE

Electromagnetic Interference

Meets interference specifications of MIL-I-6181D over the following frequency ranges: Radiated (with CRT mesh filter, cabinet covers and BNC connector covers installed)-150 kHz to 1 GHz ; conducted (power line) -150 kHz to 25 MHz .

## MECHANICAL CHARACTERISTICS

| Construction | Aluminum alloy chassis, panel and cabinet. Glass laminate etched circuit boards. |
| :--- | :--- |
| Finish | Anodized front panel. Blue vinyl-finished cabinet and rear panel. |
| Overall Dimensions: | Measured at maximum points; 15 inches high, $16-7 / \mathrm{s}$ inches wide, 24 inches deep. |
| ${ }^{2}$ Crest factor $=\frac{\text { Peak } \mathbf{V}}{\text { RMS V }}=$ between $\mathbf{1 . 3 0}$ and $\mathbf{1 . 4 1 4 .}$ |  |

## ENVIRONMENTAL CHARACTERISTICS

The Type 556 has been designed to operate over a temperature range of $0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$, altitude up to 15,000 feet. The non-operating storage temperature range is $-40^{\circ} \mathrm{C}$ to $+65^{\circ} \mathrm{C}$, altitude up to 50,000 feet. After storage at either extreme, the instrument must be allowed at least 4 hours time for all components to return to the ambient temperature range $0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$ before operating.

Further information on environmental test procedures may be obtained by contacting your local Tektronix Field Office or representative.

## ACCESSORIES

Standard accessories supplied with the Type 556 can be found on the last pullo-ut page of the Mechanical Parts List Illustrations. For optional accessories see the Tektronix, Inc. catalog.

# SECTION 2 OPERATING INSTRUCTIONS 

Change information, if any, affecting this section will be found at the rear of the manual.

## General

This section of the manual provides for the effective use of the instrument by describing the function and operation of the front panel controls and connectors, listing the first time and general operating instructions and presenting some basic applications.

## Nomenclature and Terminology

For reference and guidance, these terms are defined as they are used in this manual.

Alternate Mode-A time-sharing method of displaying the output signals of two or more channels with a single cathode ray tube beam. Channel switching is sequential and occurs at the end of the sweep.

Chopped Mode-A time-sharing method of displaying output signals of two or more channels with a single cathode ray tube beam, in sequence, at a rate not referenced to the sweep.

Chopping Rate-The rate at which channel switching occurs in Chopped Mode.

Chopping Transient Blanking-The process of blanking the indicating spot during the switching periods in Chopped Mode.

Dual-Beam Oscilloscope-An oscilloscope in which the cathode ray tube produces two separate electron beams that may be individually or jointly controlled.

Dual-Trace-A mode of operation in which a single beam in a cathode ray tube is shared by two signal channels.

Multi-Trace-A mode of operation in which a single beam in a cathode ray tube is shared by two or more signal channels.

Signal Channel-A signal amplifying circuit in a plug-in unit. With dual and multi-channel plug-ins, the channels are generally designated Channel 1 (or A) Channel 2 (B), etc.

## Power Requirements

This instrument may be operated with power from either a 115 -volt or a 230 -volt (nominal) power source. With proper positioning of the Line Voltage Selector connectors, the power supply circuit will provide correct DC voltages with adequate regulations with any line voltage within voltage limits of 90 to 136 volts RMS and 180 to 272 volts RMS and frequency limits of 50 to 60 Hz . The adjustable turns ratio design of the power transformer provides the means of making the instrument compatible with this wide range of power source voltages.

## SN 2000-up

A Line Voltage selector assembly is provided to facilitate changing the power transformer turns ratio (see Fig. 2-1). The assembly contains two line fuses and two movable pins and socket type connectors. The two-position connector is termed the Voltage Selector and the three-position connector is termed the Range Selector.
Table 2-1 lists the six Voltages and Range selector combinations and the line voltage ranges they should be used with. Before connecting the instrument to a power source, measure the power source line voltage and position the Voltage and Range selectors accordingly.

TABLE 2-1

| Voltage <br> Selector <br> position | Range <br> Selector <br> position | Will provide optimum <br> regulation for line <br> voltages from |
| :---: | :---: | :---: |
| 115 V | LO | 90 to 110 volts |
| 115 V | M | 104 to 126 volts |
| 115 V | HI | 112 to 136 volts |
| 230 V | LO | 180 to 220 volts |
| 230 V | M | 208 to 252 volts |
| 230 V | HI | 224 to 272 volts |

To change the power transformer from one regulating range configuration to another use the following procedure:

1. Disconnect the instrument from the power source.
2. Loosen the two captive screws and remove the cover. Since the line fuses are attached to the cover, they will be pulled from their holders with the cover.
3. To change nominal line selections, pull the Voltage Selector until its pins are free of the sockets, invert the selector and reseat the pins in the desired sockets.

## NOTE

115 -volt to 230 -volt plug adapters are not supplied with this instrument. If a suitable adapter is not available, it may be necessary to change the line-cord plug.
4. To change regulating range selections, pull the Range selector until its pins are free of the sockets, move it to the desired range position and seat the pin in the sockets.
5. Replace the assembly cover and the two line fuses. Press the cover firmly onto the assembly to seat the two fuses in their holders, then tighten the captive screws.
6. The indicating tabs on the selectors will be protruding through the covers to indicate the selected regulating range. Always check the position of these tabs before applying power to the instrument.

## SN 100-1999

Instruments with serial numbers 100-1999, unless tagged otherwise, are connected at the factory for operation at 115 volts (nominal). The power transformer has eight primary ferminals which are connected to solderless pin connectors on the Power board. These quick-change connectors make possible operation from four different nominal AC voltages: 104, 115,208 and $230 \mathrm{~V}, 50$ to 60 Hz . Fig. 2.2 illustrates the jumper and lead connections required for operalion on each of the slated line voltages. For 208 V and 230 V operation, the iwo unused jumpers can be stored on the unused pins of terminals J and T. All lead connections to the board that are not shown in Fig. 2.2 remain as they are.

No chango in fan connections is required when changing the connection on the beard as directed in the illustration.

## NOTE

Two metal tags (prinled on each side) are provided at the rear of the instrument to indicate the four nominal line vollages. If the primary wiring is changed, be sure to use the proper log to indicate the voltage for which the instrument is wired.

## Temperature considerations

To reduco operating temperalures, air is drawn in through the filter al the rear and blown forward through the instrument. For the most officient air circulation and heat dissipation, provide al least three inches elearance af the rear, Iwo inches at the sides and operate the instrumant with the side covers installed. If the fan becomes inoperative or the air circulation is obslrueted, the internal temparalures will axcesed a safo oporating lovel in a relativaly short pariod of lime. To pravant damago to the componenis from excossive lemperatures, a thermal cutoul switch is incorporalad in the power supply circuitry. This switch is designad to infarrupt power to tha instrument when the ambient femparaturo oxceeds aboul $140^{\circ} \mathrm{F}$.

## CAUTION

Since the thermal cutoul switch will resel when its ambient temperalure decreases to some level below its actuating temperalure, set the POWER switch to OFF bafora allempling to remedy the cause of the high temperature condition.

## CONTROLS AND CONNECTORS

Figure 2.3 shows the location of all the instrument operaping controls and connectors. A brial doseription of each typo of contral and connector is given in the following table. Controls with the same nomenclatures generally perform identical functions for their respective beams and a description for one is applicable to the other. Those controls with the same nomenclature, but with differences in their funcfions, are poinled oul and described as separale lype controls.

Some of the controls and connectors, particularly those with complex functions or mulliple applicalions, are described in greater defail under Gencral Operating Insiructions.

## A AND B TRIGGERING CONTROLS

Source
Selects triggering signal source, Two selecfor switches are combined under the no-
menclalure of SOURCE to provide this complex switching function. The selections of the two position selector switch are:
LEFT: From left plug-in or left verlical amplifier.
RIGHT: From right plug-in or right vertical amplifier. The selections of the four position selector switch are:

(A) Cover in place.

(B) Cover removed.

Fig. 2-1. Line Valiage Salector assembly; provided in Instuments with turial number 2000 and up.


Fig. 2-2. Posltions of the movable |umpar wires fblack on yellowl for the four nominal line valtage selections. This illusiration la applicable to 556 SN's 100 to 1999.

INT NORM: From trigger pickoff in the oscilloscope vertical amplifier for the triggering range is offered for triggering on higher amplitude signals. The sweep trigger circuit is most sensitive to small signals with the LEVEL control pushed in and set close to 0 .

| TRIGGER | Connector for applying an external trig- <br> INPUT |
| :--- | :--- |
|  | ger signal to the Sweep Trigger circuit |
| when its SOURCE switch is set to EXT. |  |

ger signal to the Sweep Trigger circuit when its SOURCE switch is set to EXT.
respective plug-in unit.

INT PLUG IN: From trigger pickoff in the respective plug-in unit. Applies to multitrace plug-in units with this capability.

LINE: Uses a line-frequency signal as a trigger.

EXT: From signal applied to the TRIGGER INPUT connector. Not affected by LEFTRIGHT switch.

COUPLING Determines method of coupling the triggering signal to the trigger circuit.

AC: Blocks the DC component and allows triggering to take place on the $A C$ component. With frequencies about 30 Hz and below, use the DC position.
AC LF REJ: Rejects $D C$ and progressively attenuates signal frequencies below about 2.5 kHz , allowing the trigger circuits to respond only to the higher frequencies.

AC HF REJ: Rejects DC, passes signals between 60 Hz and 60 kHz and progressively attenuates signals above 60 kHz .

DC: Permits triggering on both high and low (to DC ) frequency signals.

SLOPE Selects portion of triggering signal which will trigger the sweep.
+: Sweep triggers from positive-going portion of the triggering signal.
-: Sweep triggers from negative-going portion of the triggering signal.

LEVEL Selects the amplitude point on the triggering signal where sweep triggering occurs. When the knob is pulled out, greater

## DISPLAY

POSITION

DISPLAY MAG ing on signals with repetition rates higher than about 30 Hz . With no trigger signal or with a lower repetition rate, the time-base circuit free runs and provides a convenient reference trace.

TRIG: Permits normal triggering on all triggering signals. No trace occurs when the triggering signal is removed. OR
DELAY TIME

## A Sweep

A TIME/CM

## Upper Beam

Selects vertical (Y-axis) and horizontal (Xaxis) mode of operation for the Upper Beam.

LEFT PLUG-IN EXT: Left plug-in signal provides the vertical deflection while the signal applied to the UPPER BEAM EXT HORIZ IN connector provides the horizontal deflection.

LEFT PLUG-IN A: Left plug-in signal provides the vertical deflection and the $A$ TIME/CM switch sets the sweep rate of the Upper Beam.

LEFT PLUG-IN B: Left plug-in signal provides the vertical deflection and the $B$ TIME/CM switch sets the sweep rate of the Upper Beam.

RIGHT PLUG-IN A: Right plug-in signal provides the vertical deflection and the A TIME/CM switch sets the sweep rate of the Upper Beam.
RIGHT PLUG-IN B: Right plug-in signal provides the vertical deflection and the B TIME/CM switch sets the sweep rate of the Upper Beam.

RIGHT PLUG-IN EXT: Right plug-in signal provides the vertical deflection while the signal applied to the UPPER BEAM EXT HORIZ IN connector provides the horizontal deflection of the Upper Beam.

Controls horizontal position of Upper Beam trace. Single knob controls both coarse and fine adjustment of the beam position by means of a backlash coupling between the two sections of the control.

Expands the Upper Beam display to left and right of graticule center.

X1: Normal presentation of the display.
$\times 10$ : Horizontal length of Upper Beam display is magnified by 10 . The $\times 10$ light indicates that the display is magnified.

VARIABLE

Normally referred to as the A TIME/CM switch in this manual. Selects the sweep rate of the A sweep generator. Also selects the basic delay time (to be multiplied by the DELAY-TIME MULTIPLIER dial setting) for delaying the B sweep when the B MODE switch is set to DLY'D BY A.

Provides continuously variable sweep rate to at least 2.5 times the setting of the A TIME/CM switch. Sweep rate is calibrated when the control is set fully clockwise to
CALIBRATED. An UNCAL neon turns on
when the VARIABLE control is not in the
CALIBRATED position.

RESET $\quad$| When the RESET lamp is on, the A sweep |
| :--- |
| is ready to start when a trigger is received |
| (A MODE switch set to SINGLE SWEEP). |
| After a sweep is completed, the RESET |
| button must be pressed before another |
| sweep can be presented. |

A MODE $\quad$| Determines the A sweep generator operat- |
| :--- |
| ing mode. |

NORM: The A sweep is triggered from an internal or external signal as selected by the A TRIGGERING controls.

SINGLE SWEEP: The A sweep generator generates one sweep and then shuts off until reset.

## B Sweep

B TIME/CM

## VARIABLE <br> and <br> RESET

B MODE
Selects the sweep rate of the B sweep generator. Can be used to drive the Upper Beam, Lower Beam, or both beams, depending on the position of the DISPLAY switches.

Performs same functions for B sweep as corresponding control and pushbutton do for A sweep.

Determines the B sweep generator operating mode.

SINGLE SWEEP: The B sweep generator generates one sweep and then shuts off until reset

DLY'D BY A: B sweep circuit will not produce a sweep until a trigger pulse is received following the delay time selected by the A TIME/CM \{OR DELAY TIME) switch and the DELAY-TIME MULTIPLIER dial.

NORM: The B sweep is triggered from an internal or external signal as selected by the B TRIGGERING controls.

Lower Beam
DISPLAY Selects horizontal (X-axis) mode of operation for the Lower Beam.

RIGHT
PLUG-IN:

Right plug-in signal provides the vertical deflection and the A TIME/CM switch sets the sweep rate of the lower beam (not incorporated in instruments serial numbered 100-1999).

RIGHT PLUG-IN B: Right plug-in signal provides the vertical deflection and the

POSITION Performs same functions for Lower Beam and DISPLAY MAG

B TIME/CM switch sets the sweep rate of the Lower Beam.

RIGHT PLUG-IN EXT: Right plug-in signal provides the vertical deflection while the signal applied to the LOWER BEAM EXT HORIZ IN connector provides the horizontal deflection of the Lower Beam.

## Upper Beam and Lower Beam (for both beams where applicable)

INTENSITY Controls brightness of the display.

## CAUTION

Excessive intensity can permanently damage the phosphor on the CRT screen. Use the INTENSITY control to keep the beam brightness turned down below the level that causes a halo to form around the CRT spot or trace.

FOCUS Provides adjustment for a well-defined display. Used in conjunction with the INTENSITY and ASTIGMATISM controls.

CONTRAST (For Ppper Beam only in instruments SN 100-1999). Controls brightness of non-intensified portion of trace or display during delayed B sweep mode of operation.

ASTIGMATISM Used in conjunction with the INTENSITY and FOCUS controls for obtaining a welldefined display.

## Lower Portion of Front Panel

UPPER BEAM Controls amount of Upper Beam horizontal EXT HORIZ VAR ROTATION SEPARATION

TRACE Screwdriver adjustment to simultaneously

TRACE Varies the vertical position of the Upper deflection produced by voltage applied to the UPPER BEAM EXT HORIZ IN connector. Horizontal deflection factor is continuously variable from about 1 to $10 \mathrm{~V} / \mathrm{cm}$ with the Upper Beam DISPLAY switch set to either of the EXT positions and the DISPLAY MAG switch set to $\times 1$; from 0.1 to about $1 \mathrm{~V} / \mathrm{cm}$ when DISPLAY MAG switch is set to $\times 10$. align the traces of both beams with their respective horizontal center lines.

Beam with respect to the Lower Beam when the Upper Beam DISPLAY switch is set to any of the RIGHT PLUG-IN positions.

| SCALE ILLUM | Controls graticule illumination. |
| :---: | :--- |
| LOWER BEAM |  |
| EXT HORIZ | Same function as corresponding Upper <br> VAR |
| Beam horizontal deflection. |  |
| DELAY-TIME the Lower |  |
| MULTIPLIER | Works in conjunction with the A TIME/ <br> CM IOR DELAY TIME) switch. Provides <br> variable delay of the B sweep up to 10.00 <br> times the delay time indicated by the A |
| TIME/CM switch. |  |

BEAM FINDER Returns the displays of both beams to the screen when the button is pressed. Limits the horizontal and vertical amplifier dynamic ranges of both beams. Used to locate trace(s) which exceeds scan of display area.

## AMPLITUDE CALIBRATOR

Determines the peak-to-peak positive-fromground voltage available at the CAL OUT connector.

## NOTE

When working into an external 50 ohm load using the .2 VOLTS to 200 mVOLTS positions, output amplitude is one-half the indicated voltage.

5 mA Current
Provides 5 mA square-wave current from the calibrator circuit. The arrow shows direction of conventional current flow (i.e., positive to negative).

POWER Toggle switch: Applies line power to the low-voltage power transformer.

Light: Indicates that the AC line voltage is applied to the power transformer.

DLY'D TRIG Output connector which supplies a sharp positive-going trigger spike equal to or greater than 7 V at the end of the delay period as set by the A TIME/CM (OR DELAY TIME) switch and the DELAY-TIME MULTIPLIER control.

A GATE Output connector which supplies a posi-tive-going square-wave pulse equal to or greater than 8 V coincident with the A sweep. Pulse duration is approximately $10.5 \times$ the setting of the A TIME/CM switch when the (A) VARIABLE control is set to CALIBRATED.

B GATE Same as A GATE except applies to B TIME/CM switch and (B) VARIABLE control.

CAL OUT Output connector for the Amplitude Calibrator.

UPPER BEAM EXT HORIZ IN

Input connector for applying an external horizontal signal to the Upper Beam horizontal amplifier when the Upper Beam DISPLAY switch is set to either EXT posi-
tion. A positive voltage deflects the beam from left to right.

A SAWTOOTH Output connector which supplies a sawtooth voltage from the A sweep generator. Peak amplitude is equal to or greater than $9 \mathrm{~V} / \mathrm{cm}$. The sawtooth ramp is positivegoing from near ground.

B SAWTOOTH Same as A SAWTOOTH except applies to the B sweep generator output.

LOWER BEAM Same as UPPER BEAM EXT HORIZ IN EXT HORIZ IN except applies to the Lower Beam horizontal amplifier when the Lower Beam DISPLAY switch is set to EXT.

## Rear Panel (Upper and Lower Beam)

EXT CRT Input connector for intensity modulation CATHODE (Z-axis) of the display.

## CRT Cathode Selector

Toggle switch for the CRT cathode circuit. EXT CRT CATHODE: Normal operation with shorting cover connected. With shorting cover removed, CRT cathode can be intensity modulated with a 10 V or more signal applied to the EXT CRT CATHODE connector.

UPPER BEAM (LOWER BEAM) CHOPPED BLANKING: Permits blanking the Upper (Lower) Beam while the multi-trace plugin unit is switching from one channel to another during chopped mode of operation.

LINE VOLTAGE Facilitates changing the power transformer SELECTOR ASSEMBLY circuit configuration. The assembly contains a Voltage Selector, a Range Selector and two line fuses. (not incorporated in instruments SN 100-1999).

## SELECTION OF PLUG-IN UNITS

The Type 556 Oscilloscope is designed to use Tektronix letter-series and 1 -series plug-in units as the input stages for the two vertical deflection systems.

A plug-in unit installed in the left-hand compartment of the oscilloscope is identified as the "left plug-in". This unit provides vertical deflection for the Upper Beam only when the Upper Beam DISPLAY switch is set to the LEFT PLUG-IN positions. Similarly, the plug-in unit installed in the righthand compartment is referred to as the "right plug-in". This unit, however, provides vertical deflection for both beams simultaneously or for the Lower Beam only, depending on the settings of the DISPLAY switches.

The use of plug-in units as the vertical inputs permits changing the vertical characteristics of the oscilloscope to meet a wide range of application requirements. The particular plug-in units to be used must be selected to satisfy the requirements of your applications. In selecting the vertical plug-in units, consider the bandpass, risetime, deflection
factor, input RC characteristics and the number of inputs. Other plug-in units to consider are special purpose types such as differential amplifiers and comparators, operational amplifiers, spectrum analyzers, etc. Table 2-2 lists a wide variety of plug-in units that can be used with the instrument.

The Type 556 Oscilloscope should not be used without plug-in units installed or connected by extensions. Operating the instrument with a plug-in missing will not damage the oscilloscope, but will cause the vertical amplifier and the sweep generator on that side of the oscilloscope to be inoperative.

## TABLE 2-2

## VERTICAL PLUG-IN UNITS

(Plug-In/556 system bandwidth characteristics are at 3 dB down)

| Plug-In Unit Type | Calibrated Deflection Factor | Bandwidth | Risetime |
| :---: | :---: | :---: | :---: |
| For Wide-Band, Multiple Trace Applications |  |  |  |
| 1 Al DualTrace | $\begin{aligned} & 50 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 20 \mathrm{~V} / \mathrm{cm} \end{aligned}$ | DC to 50 MHz | 7 ns |
|  | $5 \mathrm{mV} / \mathrm{cm}$ | DC to 28 MHz | 12.5 ns |
|  | $500 \mu \mathrm{~V} / \mathrm{cm}$ | 2 Hz to 15 MHz | 23 ns |
| 1A2 DualTrace | $\begin{aligned} & 50 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 20 \mathrm{~V} / \mathrm{cm} \end{aligned}$ | DC to 50 MHz | 7 ns |
| CA DualTrace | $\begin{aligned} & 50 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 20 \mathrm{~V} / \mathrm{cm} \end{aligned}$ | DC to 24 MHz | 15 ns |
| $M$ FourTrace | $\begin{aligned} & 20 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 10 \mathrm{~V} \mathrm{~cm} \end{aligned}$ | DC to 20 MHz | 18 ns |
| High-Frequency Sampling Applications |  |  |  |
| 1S1 | $\begin{aligned} & 2 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 200 \mathrm{mV} / \mathrm{cm} \end{aligned}$ |  | 350 ps |
| 1S2 | $\begin{aligned} & 5 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 500 \mathrm{mV} / \mathrm{cm} \end{aligned}$ |  | 90 ps |
| For Wide-Band Applications |  |  |  |
| B | $\begin{aligned} & 50 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 20 \mathrm{~V} / \mathrm{cm} \end{aligned}$ | $\overline{D C}$ to 20 MHz | 18 ns |
|  | $\begin{aligned} & 5 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 20 \mathrm{mV} / \mathrm{cm} \end{aligned}$ | 2 Hz to 12 MHz | 30 ns |
| K | $\begin{aligned} & 50 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 20 \mathrm{~V} \end{aligned}$ | DC to 30 MHz | 12 ns |
| L | $\begin{aligned} & 50 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 20 \mathrm{~V} \end{aligned}$ | DC to 30 MHz | 12 ns |
|  | $\begin{aligned} & 5 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 2 \mathrm{~V} / \mathrm{cm} \end{aligned}$ | 3 Hz to 24 MHz | 15 ns |
| For High DC Sensitivity Applications |  |  |  |
| H WideBand | $\begin{aligned} & 5 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 20 \mathrm{~V} / \mathrm{cm} \end{aligned}$ | DC to 15 MHz | 23 ns |

For Differential Input Applications

| D High- <br> Gain | $1 \mathrm{mV} / \mathrm{cm}$ (to <br> $50 \mathrm{mV} / \mathrm{cm})$ | DC to 300 kHz | $0.18 \mu \mathrm{~s}$ |
| :---: | :--- | :--- | :--- |
| E Low- | $50 \mu \mathrm{~V} / \mathrm{cm} /$ to <br> Level | 0.06 Hz to 20 <br> $10 \mathrm{mV} / \mathrm{cm})$ | $6 \mu \mathrm{sHz}$ |
| G (to 60 kHz$)$ |  |  |  |
| Wide- <br> Band | $50 \mathrm{mV} / \mathrm{cm}$ to <br> $20 \mathrm{~V} / \mathrm{cm}$ | DC to 20 MHz | 18 ns |


| AA7 High- |
| :---: | :--- | :--- | :--- |
| Gain |$\quad$| $10 \mu \mathrm{~V} / \mathrm{cm}$ to |
| :--- |
| $10 \mathrm{~V} / \mathrm{cm}$ |$\quad$| DC to 500 kHz |
| :---: |
| Selectable |
| bandwidth |$\quad 0.7 \mu \mathrm{~s}$

For Integration, Differentiation, Function Generation, Linear and Non-Linear Uses

| 0 <br> Operational Amplifier | $\begin{aligned} & 50 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 20 \mathrm{~V} / \mathrm{cm} \end{aligned}$ | DC to 25 MHz | 14 ns |
| :---: | :---: | :---: | :---: |
| For Transducer and Strain Gage Uses |  |  |  |
| Q | $10 \mu$ strain/ div to 10,000 $\mu$ strain/div | DC to 6 kHz | $60 \mu \mathrm{~s}$ |
| For Displaying Simultaneously Delay, Rise, Storage, and Fall Times of Transistors |  |  |  |
| R TransistorRisetime | $\begin{aligned} & 0.5 \mathrm{~mA} / \mathrm{cm} \text { to } \\ & 100 \mathrm{~mA} / \mathrm{cm} \end{aligned}$ | DC to 30 MHz | 12 ns |

For Displaying Forward and Reverse Switching Characteristics of Semiconductor Diodes

| S Diode Recovery | 1 mA to 20 mA forward current, 0 mA to 2 mA reverse current | DC to 30 MHz | 12 ns |
| :---: | :---: | :---: | :---: |
| For Precise Amplitude Measurements Via |  |  |  |
| W <br> High-Gain Differential Comparator | $\begin{aligned} & 1 \mathrm{mV} / \mathrm{cm} \text { to } \\ & 50 \mathrm{~V} / \mathrm{cm} \end{aligned}$ | DC to 8 MHz at $1 \mathrm{mV} / \mathrm{cm}$, increasing to 23 MHz at $50 \mathrm{mV} / \mathrm{cm}$ | $\begin{aligned} & 44 \mathrm{~ns} \text { at } 1 \\ & \mathrm{mV} / \mathrm{cm}, 15 \\ & \mathrm{~ns} \text { at } 50 \\ & \mathrm{mV} / \mathrm{cm} \end{aligned}$ |

For Spectrum Analysis

| Plug-In Unit Type | Tuning Range |
| :---: | :---: |
| 1 L 5 | 10 Hz to 1 MHz |
| 1 L 10 | 1 MHz to 36 MHz |
| 1 L 20 | 10 MHz to 4200 MHz |
| 1 L 30 | 925 MHz to 10.5 GHz |

In addition, nine narrow-band spectrum analyzers covering frequencies between 10 MHz and 18.2 GHz are available on special order-contact your Local Tektronix Field Engineer or Field Office.

## FIRST TIME OPERATION

This procedure describes the basic turn-on precautions and demonstrates the function of the essential general operating controls.

1. Before connecting the instrument to a power source, set the POWER switch to OFF, turn both INTENSITY controls fully counterclockwise and inspect for a power transformer circuit configuration compatible with the actual power source voltage.
2. Install two vertical amplifier type plug-in units, or, if available, two Tektronix Calibration Fixtures, part number 067-0521-00.
3. Connect the instrument to the power source and turn the POWER switch to ON.
4. While waiting for instrument warmup, set the controls of both beams and the plug-in units as follows:

## $A$ and $B$ Triggering

A SOURCE
LEFT INT NORM
B SOURCE
COUPLING
SLOPE
MODE
LEVEL
$A$ and $B$ Sweep
A TIME/CM and B TIME/CM
. 5 SEC
VARIABLE
CALIBRATED
A MODE and B MODE
NORM

## Upper and Lower Beam

A DISPLAY
B DISPLAY
POSITION
DISPLAY MAG
AMPLITUDE CALIBRATOR
LEFT PLUG-IN A
RIGHT PLUG-IN B
Centered
$\times 1$
50 mVOLTS

## Rear Panel

CRT Cathode Selector
EXT CRT CATHODE

## Vertical Plug-In Units

| Position | Centered |
| :--- | :--- |
| Volts $/ \mathrm{Cm}$ | .05 |
| Input Selector | AC |

## Front Panel Adjustments

5. Apply a $50-\mathrm{mV}$ signal from the oscilloscope CAL OUT connector to both vertical plug-in units.
6. Turn the INTENSITY controls clockwise until the displays are of normal brightness.
7. Adjust the A and B Triggering LEVEL control to obtain stable displays.
8. Use the plug-in Position controls to position the displays to the center of their respective graticule viewing areas.
9. Use the Upper and Lower Beam horizontal POSITION controls to position th displays so they start at the left edge of the graticule.
10. Adjust the FOCUS and ASTIGMATISM conrols to obtain well-defined displays.
11. Set the plug-in unit Input Selector switches to Gnd or remove the signal. Check that the traces are parallel to their respective graticule center lines. If they are not, adjust the TRACE ROTATION control for best alignment of the traces with the graticule lines.
12. This completes the basic operation procedure for the Type 556. Instrument operation not explained here, or operation which needs further explanation is discussed under General Operating Information.

# GENERAL OPERATING INFORMATION 

## Light Filters

The mesh filter supplied with the Type 556 provides shielding against radiated EMI (electro-magnetic interference; formerly called RFI) from the face of the CRT. It also serves as a light filter to make the trace more visible under high ambient light conditions. The mesh filter and graticule cover are one unit (Tektronix Part No. 378-0572-00). To remove the filter, remove the four graticule nuts and then remove the graticule cover and mesh filter as a unit.

A tinted light filter is also provided. This filter minimizes light reflections from the face of the CRT to improve contrast when viewing the display under high ambient light conditions. If a light filter is needed and EMI shielding is not required, use the tinted filter to obtain least loss of beam brightness.

## NOTE

When using a light filter, avoid the tendency to set the beam intensities so high that they will burn the CRT phosphor.

A clear plastic faceplate protector is provided with the Type 556 for use when the mesh filter or the tinted filter are not used. The clear faceplate protector provides the best display for waveform photographs. It is also preferable for viewing high writing rate displays under low ambient light conditions.

The tinted filter or the faceplate protector should be used at all times to protect the CRT faceplate from scratches. The faceplate protector and the tinted filter are held in place by a graticule cover (Tektronix Part No. 200-0382-00). To remove the light filter or faceplate protector, remove the four graticule nuts and the graticule cover.

## Calibrated Graticule

The edge-lighted internal graticule is accurately marked with 8 vertical and 10 horizontal $1-\mathrm{cm}$ divisions. There are 2-mm sub-divisions marked on the vertical center line and the two horizontal center lines (one for each beam). One centimeter of each corner of the graticule is omitted so the graticule fits within the round CRT screen. The deflection factors of the CRT beams are calibrated to the graticule marks. Thus the marks provide a calibrated scale for making time and voltage measurements.

Each beam has a usable vertical scan area of 6 cm . The beams overlap in the center $4-\mathrm{cm}$ area of the graticule to permit superimposed displays.

## Beam Finder

The BEAM FINDER pushbutton provides a means of locating a display which overscans the viewing area either vertically or horizontally. When the BEAM FINDER button is pressed, the display is compressed within the graticule area. To locate and reposition an overscanned display, use the following procedure.

1. Press the BEAM FINDER button.

B. Center portion of rear panel.

Fig. 2-3. Control setup chart for Type 556 SN 2000 and up.

## Operating Instructions-Type 556



Fig. 2-4. Type 556 control setup chart for instruments with serial number 1999 and below.
2. While the BEAM FINDER button is held in, reduce the vertical deflection to less than 3 cm by adjusting the amplitude of the input signal or the deflection factor of the plug-in.
3. Adjust the POSITION controls of the plug-ins and the Type 556 to center the display within the beam viewing area.
4. Release the BEAM FINDER button; the display should appear within the viewing area.

## Output Signals

Several low-impedance signal outputs are available at the front panel of the Type 556 Oscilloscope. These are Delayed trigger pulse, a gate waveform from each time base, a sawtooth waveform from each time base, and an Amplitude Calibrator square wave. Typical waveforms are illustrated in Fig. 2-5.

In addition, some multi-trace vertical plug-in units provide an amplified single-channel signal output to be used as a reference for triggering oscilloscopes. Such units apply the single-channel signal to the Type 556 triggering circuits through internal wiring when the SOURCE switches are set to the PLUG IN position.

Use of the gate and sawtooth waveforms for triggering or driving external devices is illustrated in Fig. 2-6. In this application, the time base is usually set for a free-running sweep.

In addition to the sawtooth outputs on the front panel, there is an internal sawtooth voltage that is applied to pin 6 of both plug-in interconnecting jacks. For the left plug-in unit the sawtooth voltage originates from the A Sweep Generator; for the right plug-in unit the sawtooth voltage originates from the B Sweep Generator. These sawtooth voltages provide a standardized current ramp of $20 \mu \mathrm{~A} / \mathrm{cm}$ (nominal) via a standardizing resistor for use in driving plug-in spectrum analyzers requiring this signal source.

The internal current ramps can also be used to drive lowimpedance circuits, such as the minus input of an operational amplifier or the emitter of a transistor, with a positive-going linear ramp of current. The internal and external sawtooths from each sweep may not drive two circuits when both outputs are used at the same time, nor will the internal sawtooth successfully serve as a voltage signal source-especially at the faster sweep rates.

When pin 6 is not used, the high impedance of this sawtooth signal source prevents excessive cross-talk of the signal into the plug-in unit.

## Control Setup Chart

Fig. 2-3 and Fig. 2-4 show the front panel and a portion of the rear panel of the Type 556. If the controls of the plug-in unit being used are sketched in, the completed picture may be reproduced and used as a test setup record for special measurements, applications or procedures, or may be used as a training aid for familiarization with this oscilloscope.

## Vertical Controls

The vertical plug-in unit for each beam contains all the front-panel vertical positioning and deflection controls for that beam with the exception of the TRACE SEPARATION


Fig. 2-5. Output waveforms available at the front panel.
control. Refer to the instruction manuals of the particular plug-in units for operation of the vertical controls.

## CONNECTING TO THE SIGNAL SOURCE

Input signals that are to be displayed as vertical deflection on the CRT screen are applied to the input connectors on the two vertical plug-in units.


Fig. 2-6. Using the A GATE or A SAWTOOTH waveform to trigger or drive an external device. Sweep is usually free running.

## Use of Coaxial Cables

In general, coaxial cables should be used to connect the signal source to the vertical input. The use of coaxial cables nearly eliminates pickup from stray electromagnetic fields, and also eliminates radiation from the connecting cables by grounding the outside conductors. It is sometimes possible to use an unshielded input lead if the signal amplitude is high and if its frequency is low. When an unshielded lead is used, connect another lead between the oscilloscope chassis and the chassis of the signal source.

In high-frequency work it is usually necessary to terminate signal sources and connecting cables in their characteristic impedances. Unterminated connections result in signal reflections within the cables and cause distortion of the displayed waveforms. The input coaxial cable will often serve to terminate the signal source, and a termination placed at the input of the plug-in unit will provide sufficient termination for signal reflections. However, if the source impedance is considerably different from that of the connecting cable, the source end of the cable may also need to be terminated.

When connecting an input signal, the loading effect of the oscilloscope on the signal source must be considered. The resistance at the input of the vertical plug-in unit is usually 1 megohm which adequately limits low-frequency loading to a negligible value. However, at high frequencies, the input capacitance of the vertical plug-in and the distributed capacitance of the input cable become significant. Capacitive loading at high frequencies may be sufficient to adversely
affect both the displayed waveform and the operation of the signal source. Attenuator probes can be used to reduce capacitive and resistive loading to very small values.

## Use of Probes

In addition to reducing the load on the signal source, an attenuator probe also decreases the amplitude of the displayed waveform by the attenuation factor of the probe. This permits observation of signals beyond the normal amplitude limits of the oscilloscope and plug-in combination. Signal amplitudes, however, must be limited to the maximum allowable value of the probe being used.

Before a probe is used, it must be compensated to operate properly with the plug-in unit. Compensation of the probe is adjusted according to the procedure given in the instruction manual with the vertical plug-in unit and in the instructions accompanying the probe. In general, this adjustment is done by connecting the probe cable to one of the vertical inputs and observing several cycles of the calibrator waveform on the CRT screen. The compensating capacitor is then adjusted to provide minimum distortion of the top and leading corner of the square-wave signal (see Fig. 2-7).

## Trigger Source

INT. For most applications, the sweep can be triggered internally. In the INT positions of the SOURCE switch, the


Fig. 2-7. Probe compensation waveforms.
trigger signal is obtained from the vertical system. The SOURCE switch provides further selection of the internal trigger signal as follows:
(1) LEFT INT NORM; triggering is obtained from the left vertical amplifier. For single-trace displays this position provides the most convenient operation. However, for multitrace displays, special considerations must be made to provide the correct display. For further information refer to (3) LEFT INT PLUG IN and the plug-in instruction manual.
(2) RIGHT INT NORM; triggering is obtained from the right vertical amplifier. The information about single-trace and multi-trace displays given for the LEFT INT NORM position also applies for this position.
(3) LEFT INT PLUG IN; for a multi-trace plug-in unit in the left oscilloscope compartment that can supply a single-channel triggering signal through pin 5 of the interconnecting plug, such as the Tektronix Types 1A1 and 1A2 Dual-Trace Plug-In Units. This position is useful when operating the plugin unit in dual-trace chopped-mode operation since the triggering signal is the same as the applied signal and is free from the chopping rate switching transients. Also, this position is useful when operating the plug-in in dual-trace alternate operation to show true time relationship between input signals.
(4) RIGHT INT PLUG IN; same applications for (3) LEFT INT PLUG $\operatorname{IN}$ except this is for a multi-trace plug-in unit that is inserted in the right plug-in compartment of the oscilloscope.

LINE. The LINE position of the SOURCE switch connects the power-line frequency to the Sweep Trigger circuit. Line triggering is useful when the input signal is time-related to the line frequency. It is also useful for providing a stable display of a line-frequency component in a complex waveform.

EXT. An external signal connected to the TRIGGER INPUT connector can be used to trigger the sweep in the EXT position of the SOURCE switch. The external signal must be time-related to the displayed signal for a stable display. An external trigger signal can be used to provide a triggered display when the internal signal is too low in amplitude for correct triggering, or contains signal components on which it is not desired to trigger. It is also useful when signal
tracing in amplifiers, phase-shift networks, wave-shaping circuits, etc. The signal from a single point in the circuit can be connected to the TRIGGER INPUT connector through a signal probe or coaxial cable. The sweep is then triggered by the same signal at all times and allows amplitude, time relationship or waveshape changes of signals at various points in the circuit to be examined without resetting the triggering controls.

## Trigger Coupling

Four methods of coupling the trigger signal to the trigger circuits can be selected with the Triggering COUPLING switch. Each position permits selection or rejection of the frequency components of the trigger signal which will trigger the sweep.

AC. The $A C$ position blocks the $D C$ component of the trigger signal. Signals with low-frequency components below about 30 Hz will be attenuated. In general, AC coupling can be used for most applications. However, if the trigger signal contains unwanted frequency components or if the sweep is to be triggered at a DC level, one of the remaining COUPLING switch positions will provide a stable display.

The triggering point in the $A C$ position depends on the average voltage level of the trigger signal. If the trigger signals occur in a random fashion, the average voltage level will vary, causing the triggering point to vary also. This shift of the triggering point may be enough so it is impossible to maintain a stable display. In such cases, use DC coupling.

AC LF REJ. In the AC LF REJ position, DC is rejected and signals below about 2.5 kHz are attenuated. Therefore, the sweep will be triggered only by the higher-frequency components of the signal. This position is particularly useful for providing stable triggering if the trigger signal contains linefrequency components. Also, when operating multi-trace plug-in units in the alternate mode, the AC LF REJ position can provide a brighter display at the higher sweep rates. The smaller value coupling capacitor used in the sweep trigger circuit allows the circuit to recover faster, thus increasing its trigger-rate capability for triggering the sweep.

AC HF REJ. The AC HF REJ position passes all low-frequency signals between about 60 Hz and 60 kHz . $D C$ is


Fig. 2-8. Effects of Triggering LEVEL control and SLOPE switch.
rejected and signals outside the given range are attenuated. When triggering from complex waveforms, this position is useful for providing a stable display of low-frequency components.
DC. DC coupling can be used to provide stable triggering with low frequency signals which would be attenuated in the AC or AC HF REJ positions, or with low-repetition rate signals. The LEVEL control can be adjusted to provide triggering at the desired DC level on the waveforms. When using INT NORM triggering, the setting of the plug-in vertical Position control will affect the DC trigger level.

When the SOURCE switch is set to INT NORM, DC trigger coupling should not be used during alternate mode operation of a multi-trace plug-in unit. If used, the sweep will trigger on the DC level of the signal from one channel and then either lock out completely or free run on the signal from the other channel. Correct DC triggering on the first channel in this mode can be obtained if the SOURCE switch is set to the INT PLUG $\mathbb{N}$ position for a plug-in unit having an internal channel 1 output trigger.

## Trigger Slope

The Triggering SLOPE switch determines whether the trigger circuit responds on the positive-going or negative-going portion of the trigger signal. When the SLOPE switch is in the + (positive-going) position, the display will start with the positive-going portion of the waveform; in the - (nega-tive-going) position, the display will start with the negativegoing portion of the waveform (see Fig. 2-8). When several cycles of a signal appear in the display, the setting of the SLOPE switch will probably be unimportant. However, if only a certain portion of a cycle is to be displayed, correct setting of the SLOPE switch will provide a display which starts on the desired slope of the input signal.

## Trigger Mode

AUTO STABILITY. The automatic stability mode is generally the most convenient to use. It is particularly useful where a reference trace is needed in the absence of a trigger signal. To use this triggering mode, set the MODE switch to AUTO STABILITY and set the Triggering LEVEL control for proper triggering to obtain a stable display. When the triggering signal is removed, the sweep generator circuit will free run to present a reference trace on the CRT.

TRIG. The TRIG position of the MODE switch should be used if AUTO STABILITY position is undesirable or if the trigger signal has a very low repetition rate (below about 30 Hz ).

## Trigger Level

The Triggering LEVEL control determines the voltage level on the triggering waveform at which the sweep is triggered. When the LEVEL control is set in the + region, the trigger circuit responds at a more positive point on the trigger signal. When the LEVEL control is set in the - region, the sweep trigger circuit responds at a more negative point on the trigger signal. Fig. 2-8 illustrates this effect with different settings of the SLOPE switch.

To set the LEVEL control, first select the Triggering SOURCE, COUPLING and SLOPE switch positions. Then set the LEVEL control a few degrees either side of 0 (except for TRIG mode and DC coupling). If the display does not start at the desired point, adjust the LEVEL control for correct triggering.

In the DC position of the COUPLING switch, correct triggering may be obtained at any setting of the LEVEL control depending on the DC level of the trigger signal. To obtain correct triggering, set the LEVEL control fully counterclockwise. Then turn the LEVEL control clockwise until the display is triggered at the correct DC level.

When the LEVEL control is pulled outward its range is extended 10 times. The pulled outward position is useful for triggering on large amplitude signals. When the LEVEL control is pushed in, the range of the control is decreased and is most useful for signals of smaller amplitude.

## Free Run

To free run the sweep in the absence of trigger signals, set the Triggering MODE switch to AUTO STABILITY and the LEVEL control to any setting. A free running sweep is convenient when a reference trace is needed. If trigger signals are present, set the LEVEL control at either end of its range. This will allow the sweep to free run with the LEVEL control pushed in when the trigger amplitude is small, and with the LEVEL control pulled out when trigger amplitude is large. If it is desirable to free run the sweep in the presence of a larger input signal, set the SOURCE switch to some position not receiving input triggers; e.g., EXT.

With a free running sweep, one of the sweep generators can be used to initiate a gate or sawtooth signal to trigger or drive an external device under test. Fig. 2-6 illustrates this mode of operation using the A Gate or A Sawtooth and the Lower Beam. The signal applied to the device will then be synchronized with the sweep repetition rate of the sweep generator and will present a stable display on the CRT. Set the A TIME/CM switch and VARIABLE control to produce the desired repetition rate.

Another way to display the waveform of the A Gate, A Sawtooth, or the waveform from the external device is to apply the desired waveform to the Left Plug-In input connector. Next, set the Upper Beam DISPLAY switch to LEFT PLUG-IN B and use the B TIME/CM switch to obtain the desired display on the upper beam.

If the device has two output signals, apply the second signal from the device to the Right Plug-In input connector (see Fig. 2-6 dotted line). Set the Lower Beam DISPLAY switch to RIGHT PLUG-IN B. The two beams will then display the waveforms simultaneously. Similarly, more than two output signals from the external device may be displayed together by using both beams and multi-trace plug-in units.

## Selecting Sweep Rate

The $A$ and $B$ TIME/CM switches select calibrated sweep rates for their respective Sweep Generators. The VARIABLE control associated with the TIME/CM switch provides con-

## Operating Instructions-Type 556

tinuously variable sweep rates between the settings of the TIME/CM switch. Whenever the UNCAL light for either A or B is on, the sweep rate of either A or B Sweep Generator (or both if both UNCAL lights are on) is uncalibrated. The light is off when the associated VARIABLE control is set to the CALIBRATED position.

When making time measurements from the graticule, the area between the first-cm and ninth-em graticule lines provides the most linear time measurement (see Fig. 2-9). Therefore, the first and last centimeters of the display should not be used for making accurate time measurements. Position the display area to be timed so the timing area starts at the first centimeter graticule line. Set the TIME/CM switch so the end of the display timing area falls between the first and ninth cm graticule lines.


Fig. 2-9. Area of graticule used for obtaining accurate time measurements.

## Display Magnification

The displayed sweep is magnified ten times by setting the DISPLAY MAG switch from $\times 1$ to the $\times 10$ position. In the $\times 1$ position the center one-centimeter portion of the unmagnified display is the portion visible on the CRT in magnified form (see Fig. 2-10). Note that the display expands equally to each side from graticule center. Equivalent length of the magnified sweep is 100 cm . Thus, any $10-\mathrm{cm}$ portion of the display can be viewed by adjusting the horizontal POSITION control to bring the desired portion into the viewing area. The light located near the DISPLAY MAG switch is on whenever the switch is set to $\times 10$.

When the DISPLAY MAG switch is set to $\times 10$, the sweep rate is determined by dividing the TIME/CM switch setting by 10 . For example, if the TIME/CM switch is set to $.5 \mu \mathrm{SEC}$, the magnified sweep rate is $0.05 \mu \mathrm{~s} / \mathrm{cm}$. The magnified sweep rate must be used for all time measurements when the DISPLAY MAG switch is set to $\times 10$. The magnified sweep rate is calibrated when the UNCAL light is off.


Fig. 2-10. Operation of display magnifier.

## Using the Position Controls

The two beams have independent horizontal positioning. The Upper Beam horizontal POSITION control positions the Upper Beam display; the Lower Beam horizontal POSITION control positions the Lower Beam display. Clockwise rotation of either control causes the trace of the particular beam to move to the right on the CRT screen, and counterclockwise rotation moves the trace to the left. When the DISPLAY MAG switch is set to $\times 10$, the POSITION control has sufficient range to view any portion of the magnified display.

The POSITION control operates as a combination coarse and fine adjustment of the positioning by means of a backlash coupling between the two sections of the control. To position the trace or display horizontally, turn the POSITION control slightly past the point desired, then move the display to the final location. The fine adjustment section of the control operates only in the backlash of the coarse adjustment section. For example, to move the display to the right when the DISPLAY MAG switch is set to $\times 1$, rotate the POSITION control clockwise until the display is about 2 mm past the
desired location, then turn the control slightly counterclockwise for a fine adjustment of the display position.

## Single Sweep

When the signal to be displayed is non-repetitive, or if the signal is repetitive but varies in amplitude, shape or time so a stable display is difficult to obtain, use the single-sweep feature of the Type 556.

To use the single-sweep mode, first set the Triggering MODE switch to TRIG and then be sure to set the LEVEL control so the sweep trigger circuit will trigger on the event that is to be displayed. Using the Upper Beam controls as an example, set the A Triggering controls for proper triggering. Then set the A MODE switch to SINGLE SWEEP and press the RESET button. After the button is pressed, the next trigger pulse will initiate the sweep and a single trace will be presented by the Upper Beam.

After the sweep ends in the given example, the A Sweep Generator will be locked out until reset by pressing the RESET button once again. The RESET light located near the RESET button will light when the A Sweep Generator circuit has been reset and will go out after the sweep has been triggered.

## Delayed B Sweep

The delayed B sweep is operable in the DLY'D BY A (B sweep delayed by $A$ sweep) position of the B MODE switch. The A Sweep determines the time that the B Sweep is delayed. Sweep rate of the delayed portion is determined by the B TIME/CM switch.

When using DLY'D BY A mode of operation, the dualbeam display will appear similar to. Fig. 2-11. Referring to the Upper Beam display in the illustration, the amount of delay time between the start of the A Sweep and the intensified portion is determined by the setting of the A TIME/CM switch and the DELAY-TIME MULTIPLIER dial. Brightness level of the Upper Beam delaying A sweep, excluding the intensified portion, can be varied by rotating the CONTRAST control. (The brightness of the intensified portion can be changed by rotating the INTENSITY control.)

## NOTE

The OR DELAY TIME portion of the A TIME/CM OR DELAY TIME switch name as it appears on the front panel applies to delayed B sweep mode of operation. For simplicity, the switch is usually called $A$ TIME/CM in this manual.

Fig. 2-12 shows the DELAY-TIME MULTIPLIER dial. The outer numbers are major dial divisions and inner numbers are minor dial divisions. For example, the DELAY-TIME MULTIPLIER dial reading as shown in Fig. 2-12A is 3.55; 3 maor divisions and 55 minor divisions. This reading multiplied by the setting of the $A$ TIME/CM switch gives the calibrated delay time of the B Sweep (see Fig. 2-12B).

The intensified portion of the Upper Beam display is produced by the B Sweep. Time duration of this portion is governed by the setting of the B TIME/CM switch. The B TIME/CM switch should always be set for a sweep rate which is faster than the A TIME/CM switch setting. The Lower Beam
(as shown in Fig. 2-11) is used to display the intensified portion in magnified form for detailed examination.

The delayed B sweep is usually operated in two basic modes: (1) B sweep starts automatically after the delay time, and (2) B sweep starts only when triggered after the delay time.


Fig. 2-11. DLY'D BY A mode of operation. The intensified portion of the Upper Beam is expanded and displayed by the Lower Beam. A TIME/CM, 5 mSEC B TIME/CM, $50 \mu \mathrm{SEC}$.

Mode 1: B Sweep Starts Automatically After Delay Time. In this mode of operation the B sweep starts approximately 150 ns following the delay time (see Figs. $2-10$ and 2-13A). Since the delay time is the same for each sweep, the display will appear stable. Basically the setup is as follows:

1. Preset the right plug-in vertical deflection factor so the signal to be applied in step 2 will not overdrive the plugin unit but will produce an on-screen display.
2. Apply the signal to the right vertical plug-in unit.
3. Preset the DELAY-TIME MULTIPLIER control for a dial reading between 1.00 and 9.50 .
4. Set the A Triggering controls for normal internal triggering on the right plug-in signal.
5. Set these B Triggering controls as follows:
LEVEL
Fully clockwise and knob pulled outward
AUTO STABILITY


Flg. 2-12. $|A|$ DELAY-TIME MULTIPLIER dal. Reading shown is 3.35. IBI Delay ilma la calculated by multiplying the A TIME/CM sweop rale by the DELAY-TIME MULTIPLIER dial reading.
9. The Upper Beam display should have an intensified portion indicating the delayed 8 sweep time duration. If necessary, adjust the CONTRAST cenirol to show clearly the difference between the unintensified and iniensified portions. The Lower Beam should show a magnified display of the intensified portion (similar to Fig. 2-13A).
10. Turn the DELAY-TIME MULTIPLIER control and nole that the intensified portion moves smoothly along the Upper

Beam display. Thus, any portion of the Upper Beam display, except the extreme ends, can be magnified by the Lower Beam by controlling the slarting time of the B sweep with the DELAY-TIME MULTIPLIER contral. The dial readings indicate the number of major gralicule divisions between the beginning of the Upper Beam display and the intensified portion of the trace.

The degree of display magnification presented in this manner is equal to the ratio of the Upper Beam sweep rate to the Lower Beam sweep rate. For example, if the A TIME/ CM switch is sel 10.5 mSEC and the 日 TIME/CM switch is sel to $5 \mu \mathrm{SEC}$, the magnification is 100 limes.

If some signal other than the one applied to the right plugin unit is applied to the left plug-in unit and displayed by the Upper Beam, the intensified partion will still indicate the time relationship between the Iwo sweeps, but the Lower Beam will not be a magnified view of the Upper Beam display.

Mode 2: B sweep starts only when triggered after delay lime. This mode allows the B sweep to be triggerod by any triggaring ovent following the delay time (soc fig. 2.138). To demonsirale, sel up the Type 556 conirols in the same manner as described previously for Mode 1, except this information should be substifuted for slops 8 through 10.

Sot the B triggaring controls as follows:
Mode
SLOPE, COUPLING
SOURCE
LEVEL

Mode

SOURCE
LEVEL

## TRIG

As desired NORM INT, RIGHT
For proper triggering on right plug-in signal

Then furn the DELAY-TIME MULTIPLIER conlrol and nolice that the A sweep can be triggered by the appliad signal any lime after the delay time interval. The brightened portion of the Upper Beam display will jump from one Iriggaring paint on a cycle of the waveform to the same friggering point on the noxt cycle of the waveform as the DELAY-TIME MULTIPLIER control is turnod.

If no triggoring signal is appliad to the B swoep generator at the completion of the delay poriod, the Lowor Beam will be held off until a triggering pulso is received. The 8 MODE RESET lamp will light to indicato that tho sweep is ready to be triggered. Then, when the trigger signal appears, the 8 sweep generator will sweep and the RESET lamp will turn off. Thus, the time between the start of tha $A$ sweep and the starl of the B sweep will depend on tho occurrence of the B sweep triggering signal as well as on the sollings of the delay lime controls.

If separale triggaring signals are applied, the B sweep might occur at any time following the delay time period. Therefore the intensified portion of the Upper Beam display may appear any place past the delay lime period, or might not appear at all if there is no triggering signal.

## Delayed Trigger

To use the delayed Irigger pulses for triggering an external device, connect a coaxial cable from the DLY'D TRIG connector to the device under test and to the left plug-in Input connector. Connect the output signal from the device to the
right plug-in unit Input connector. Connect a coaxial cable from the A GATE to the B TRIGGER INPUT connector.

Set these controls as follows:

## A Triggering

MODE
LEVEL

AUTO STABILITY<br>Fully cw and knob pulled outward (to free run the A sweep)

## B Triggering

| MODE | TRIG |
| :---: | :--- |
| SLOPE, COUPLING | As desired |
| SOURCE | EXT |
| Upper Beam DISPLAY | LEFT PLUG-IN A |
| Lower Beam DISPLAY | RIGHT PLUG-IN B |
| A MODE \& B MODE | NORM |

The delayed triggered pulse is now triggering the device under test. One output pulse will occur for each A sweep, at a time determined by the setting of the DELAY-TIME MULTIPLIER control. To select the delay time, set the $A$ TIME/CM switch and the DELAY-TIME MULTIPLIER control so their product equals the desired delay time from $0.1 \mu \mathrm{~s}$ to 50 seconds (see Fig. 2-12B). Set the B Triggering LEVEL and the B TIME/CM switch to obtain a stable Lower Beam display of the device output waveform.

The Upper Beam is being used to monitor the delay trigger pulse. Each whole number on the DELAY-TIME MULTIPLIER dial represents 1 cm of pulse displacement from the left edge of the graticule. Since the DELAY-TIME MULTIPLIER control determines the time of occurrence of the delayed pulse, it can be used for positioning the Lower Beam display.

The A sweep generator can be either triggered or free run. If it is operated in a free run mode the repetition rate of the delayed trigger pulses will be the same as the repetition rate of the A Sweep Generator circuit at that particular setting of the A TIME/CM switch. (This rate can be varied from 0.02 Hz to about 70 kHz with the A TIME/CM switch.)

If the A sweep generator is operated in a triggered mode, an output delayed trigger pulse will occur after the A sweep generator has been triggered and has swept for the duration of the delay time period. The A sweep generator must complete its sweep and retrace before it can be triggered again. Thus the repetition rate of the delayed pulse output when the A sweep generator is triggered will depend on both the frequency of the triggering signal and the repetition rate of the A sweep generator circuit.

The Lower Beam can be used for displaying more than one cycle of the device output signal by setting the B TIME/ CM switch to a lower sweep rate than the A TIME/CM switch. The Lower Beam can also be used to expand a portion of the waveform if the B TIME/CM switch is set for a faster sweep rate than the A TIME/CM switch. Since the A GATE is triggering the B Sweep and the delayed trigger is triggering the device, the display can be positioned with the DELAY-TIME MULTIPLIER control.

## External Horizontal Deflection

To deflect one of the CRT beams horizontally with an externally-derived voltage signal, apply the external signal to the UPPER BEAM EXT HORIZ IN or LOWER BEAM EXT HORIZ IN connector and set the corresponding DISPLAY switch to EXT.

If the UPPER BEAM EXT HORIZ IN connector is used and the Upper Beam DISPLAY switch is set to LEFT PLUG-IN EXT position, the left plug in provides the vertical deflection and the external signal provides the horizontal deflection of the Upper Beam. If the Upper Beam DISPLAY switch is set to RIGHT PLUG-IN EXT, the right plug in deflects the Upper Beam vertically and the external signal deflects the Upper Beam horizontally.

The horizontal deflection factor can be varied from about $1 \mathrm{~V} / \mathrm{cm}$ to $10 \mathrm{~V} / \mathrm{cm}$ by means of the corresponding UPPER BEAM EXT HORIZ VAR or LOWER BEAM EXT HORIZ VAR control, when the appropriate DISPLAY MAG switch is set to $X 1$ and from about $0.1 \mathrm{~V} / \mathrm{cm}$ to $1 \mathrm{~V} / \mathrm{cm}$ when the appropriate DISPLAY MAG switch is set to $\times 10$.

Horizontal deflection with an external voltage signal provides low frequency $X-Y$ operation of the oscilloscope for comparing one function to another (e.g., Lissajous figures) or for making phase comparisons. However, this system is not intended for precise phase-angle measurements. The upper limit of the horizontal frequency response is 3 dB down at about 400 kHz ; therefore, $X-Y$ operation should be limited to signals below this frequency.

Time relationship of the $X-Y$ display may be provided through intensity modulation with 10 to 20 V timing pulses.

## Intensity Modulation

The two beams have separate EXT CRT CATHODE input connectors on the rear panel for application of intensity modulation signals.

To modulate one of the CRT beams, remove the connector cover from the EXT CRT CATHODE connector, check that the CRT Cathode Selector switch is set to the EXT CRT CATHODE position, and then apply a 10 to 50 V signal to the EXT CRT CATHODE connector. Positive-going voltage signals decrease the beam intensity and negative-going voltage increases the intensity from the level set by the appropriate INTENSITY control.

Intensity modulation can be used to relate other voltage information to the displayed signal without changing the shape of the waveform. Intensity time markers can be added to make time measurements more precise than those obtainable from the graticule marks. Identical signals applied to the two beams can be used to horizontally reference the two beams on the CRT screen or to correlate them in time.

## NOTE

Be sure to replace the connector grounding cover on the EXT CRT CATHODE connector when this input is not being used.


Fig. 2-13. Comparison of the two delayed-sweep modes. In each case the Upper Beam presentation represents the input to both vertical systems. The intensified portion of the Upper Beam display shows the part of the input wavefrom that is displayed by the lower Beam.

## Multi-Trace Operation Using Independent Deflection Systems

When the plug-in units are set for alternate-trace mode of operation, the oscilloscope supplies an alternate-trace sync pulse from each of its sweep generators for channel switching in multi-trace vertical plug-in units. The use of multitrace units in either alternate or chopped mode of operation provides simultaneous viewing of several input signals. All of, the traces resulting from one multi-trace unit will be displayed on one beam at the same sweep rate.
corresponding signal in that channel during alternate mode of operation. For chopped mode operation, triggering occurs

For multi-trace plug-in units that have a single-channel trigger pickoff circuit, the trigger from one channel is applied internally from the plug in to the Sweep Trigger circuit when the SOURCE switch is set to the LEFT INT PLUG IN or RIGHT INT PLUG-IN position, depending on which plug-in is selected. This permits internal triggering on only the one channel input signal, thus showing the time relationships of the multi-channel displayed waveforms.
For multi-trace units without a single-channel trigger output, each trace will be triggered on the waveform from the on the composite signal consisting of the signals in all the channels plus the chopping signal. If the time relationships of the signals are of interest, and external trigger signal can
be used, or the triggers can be derived from a time-related single input applied to the other beam.

Provision is included in the oscilloscope for blanking the between-channel switching transients when operating a multitrace plug-in unit in the chopped mode. During each sweep in this mode, a sequence of rapid switching occurs from one channel to the next, so that the signal in one channel is displayed for an instant, then the signal in the next channel. To blank the CRT beam during the period while the multitrace unit is switching from one channel to the next, set the CRT Cathode Selector switch to the UPPER BEAM CHOPPED BLANKING (or LOWER BEAM CHOPPED BLANKING) position. As mentioned previously, use single-channel or external triggering for best results. When not using chopped mode operation, be sure to return the CRT Cathode Selector switch to the EXT CRT CATHODE position.

## Multi-Trace Operation Using Interconnected Vertical Deflection Systems

When the Upper Beam DISPLAY switch is set to the RIGHT PLUG-IN A position and the right plug-in unit is set for alternate mode operation, the oscilloscope logic circuitry permits the signal in one channel to be displayed by both sweeps before the next channel can be displayed. To accomplish this, th logic circuitry supplies only one alternate-trace sync pulse for both sweeps. The logic circuit operates best when the B sweep is set to run at the same rate or faster than the $A$ sweep.

## NOTE

If different triggering sources are used to trigger the sweeps, the higher repetition-rate triggers should be applied to the B sweep when the B sweep is set to run faster than the A sweep.

## Operating Hints (When Upper Beam DISPLAY switch is set to RIGHT PLUG-IN A)

1. If the B MODE switch is set to NORM, the B Triggering MODE switch is set to TRIG and the B sweep is not triggered, the A sweep will lock out and cannot be triggered. No displays can be obtained until the B sweep is triggered or the B Triggering MODE switch is set to AUTO STABILITY. If the B MODE switch is set to SINGLE SWEEP, the B sweep cannot be triggered until the RESET button is pressed.
2. If the B MODE switch is set to DLY'D BY A and the right plug in is set for alternate-mode operation, proper operation can be obtained if the DELAY-TIME MULTIPLIER control is set to any setting higher than 0.20 and the $A$ and B Triggering controls are set as follows: RIGHT, INT NORM or INT PLUG IN, AC LF REJ, AUTO STABILITY: A LEVEL is set to trigger the A sweep, and B LEVEL is set fully clockwise.

If other control setting combinations are used, it is possible to obtain results that appear abnormal. Such apparent abnormal results might be: A or B sweep locks out, both sweeps lock out, shortened sweep lengths due to the sweeps reverting before completing their runup, only one channel displayed by each beam, unstable displays, etc.

## BASIC APPLICATIONS

The following information describes the procedure and technique for making basic measurements with the Type 556 Oscilloscope. There can be many variations of these applications but to describe clearly how a certain basic measurement is made, the procedures give the pertinent control settings and connectors used for both the oscilloscope and the plug in(s). For these applications, therefore, assume that two Type 1Al Dual-Trace Plug-In Units are used with the oscilloscope.

Familiarity with the operation of the instrument when used with the Type 1A1 or other similar plug-in units will permit these basic techniques to be adapted to the individual measurement requirements. As an aid to understanding how the oscilloscope operates internally, refer to Figs. 3-1 through $3-6$ in the Circuit Description section. These illustrations are simplified functional block diagrams of the vertical and horizontal deflection systems.

## Peak-to Peak Measurements-AC

To make a peak-to-peak voltage measurement, the Lower Beam and the right-side plug-in unit are used as an example in the following procedure:

1. Set the Lower Beam DISPLAY switch to RIGHT PLUGIN B.
2. Preset the Type 1 Al Channel 1 VOLTS/CM switch to a deflection factor which will allow the expected signal to be displayed without over-driving the vertical amplifier.
3. Set the Type 1A1 Input Selector switch to AC.
4. Apply the signal to the Type 1 Al Channel 1 Input connector.
5. Set the Channel 1 Volts/cm switch so the signal waveform is visible in the Lower Beam graticule viewing area.
6. Set the B Triggering controls as follows:

| LEVEL | Near O |
| :--- | :--- |
| MODE | AUTO STABILITY |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | NORM INT RIGHT |

7. Adjust the Channel 1 Vertical Position control so the downward excursion of the waveform coincides with one of the graticule lines below the Lower Beam graticule center line.
8. With the Lower Beam POSITION control, move the display horizontally so that one of the upper peaks of the signal lies near the vertical center line.

## NOTE

The B Triggering LEVEL control and SLOPE switch can be used to horizontally position a slow rise and fall waveform such as the sine wave shown in Fig. 2-14.
9. Measure the peak-to-peak vertical deflection in cm . Make sure the Channel 1 Variable control is in the Calibrated position.

## NOTE

This technique may also be used to make vertical measurements between two points on the waveform rather than peak to peak.
10. Multiply the distance measured in step 9 by the vertical attenuator switch setting. Also include the attenuation factor of the probe, if any.


Fig. 2-14. Measuring peak-to-peak voltage of a waveform.

Example. Assume a peak-to-peak vertical deflection of 4.6 cm (see Fig. 2-14) using a $10 \times$ attenuator probe and a vertical deflection factor of 0.5 volts per cm .
Using the formula:

$$
\begin{gathered}
\text { Volts } \\
\text { eak to Peak }
\end{gathered} \underset{\substack{\text { vertical } \\
\text { deflection } \mathrm{cm})}}{\text { in }} \times \underset{\text { factor }}{\text { volts } / \mathrm{cm}} \times \underset{\substack{\text { attenuation } \\
\text { factor }}}{ } \times \underset{\text { probe }}{ }
$$

Substituting the given values:

$$
\text { Volts Peak to Peak }=4.6 \times 0.5 \times 10=23 \text { volts. }
$$

## Instantaneous Voltage Measurements-DC

To measure the $D C$ level at a given point on a waveform, the following procedure uses the Lower Beam and the rightside plug-in unit as an example:

1. Set the Lower Beam DISPLAY switch to RIGHT PLUGIN B.
2. Preset the Type 1A1 Channel 1 Volts/cm switch to a deflection factor which will allow the expected signal and DC component to be displayed without over-driving the vertical amplifier.
3. Set the vertical plug-in Input Selector switch to Ground.
4. Set the A Triggering MODE switch to AUTO STABILITY and turn the LEVEL control fully clockwise.
5. Position the trace to a line of the graticule below the Lower Beam graticule center line. If the average signal volt-
age is negative with respect to ground, position the trace to a reference line above the Lower Beam graticule center line. Do not move the vertical plug-in Position control after this reference line has been established.

## NOTE

To measure a voltage level with respect to a voltage other than ground, make the following changes in step 5: set the plug-in Input Selector switch to $D C$, apply the reference voltage to the Input connector, and position the trace to the reference line.
6. Set the Input Selector switch to DC. The ground reference line, if used, can be checked at any time by switching to the ground position.
7. Connect the signal to the Input connector.
8. If the waveform is outside the viewing area, set the plug-in vertical attenuation switch so the waveform is visible.
9. Set the B Triggering controls for a stable display, and set the $B T I M E / C M$ controls to display the desired waveform.
10. Measure the distance in cm between the reference line and the point on the waveform at which the DC level is to be measured. For example, in Fig. 2-15 the measurement is made between the reference line and point $A$.


Fig. 2-15. Measuring Instantaneous DC voltage with respect to a reference.
11. Establish the polarity of the signal. Any signal-inverting switches on the plug in must be in the Normal position. If the waveform is above the reference line, the voltage is positive; below the line, negative.
12. Multiply the distance measured in step 10 by the vertical attenuation switch setting. Include the attenuation factor of the probe, if any.

Example. Assume that the vertical distance measured is 4.6 cm (see Fig. 2-15). The waveform is above the reference
line, using a $10 \times$ attenuator probe and an attenuator setting of 2 volts per cm .
Using the formula:

$\underset{\text { Voltage }}{\text { Instantaneous }}=4.6 \times+1 \times 2 \times 10$
The instantaneous voltage is +92 volts.

## Voltage Comparison Measurements

In some applications it may be necessary to establish a set of deflection factors other than those indicated by the vertical attenuator switch. This is useful for comparing signals to a reference voltage amplitude. To establish a new set of deflection factors based upon a specific reference amplitude, the Lower Beam and the right plug-in unit is used as an example in the following procedure:

1. Preset the Type 1 A1 Channel 1 Volts/cm switch to a deflection factor which will allow a signal of known value to be displayed within the graticule area.
2. Set the Lower Beam DISPLAY switch to RIGHT PLUG-IN B.
3. Apply the reference signal of known value to the Channel 1 Input connector.
4. With the Channel 1 Volts/cm switch and Variable control, adjust the display for an exact number of vertical cm divisions. Do not move the Variable control after obtaining the desired deflection.
5. Divide the amplitude of the reference signal (volts) by the product of the deflection in cm (established in step 4) and the vertical attenuator switch setting. This is the Deflection Conversion Factor.

$$
\begin{aligned}
& \text { Deflection } \\
& \text { Conversion }=\frac{\text { reference signal amplitude (volts) }}{\text { deflection }(\mathrm{cm}) \times \text { attenuator switch setting }} \\
& \text { Factor }
\end{aligned}
$$

6. To establish an Adjusted Deflection Factor at any setting of the vertical attenuation switch, multiply the attenuation switch setting by the Deflection Conversion Factor established in step 5.

$\underset{\text { Deflection }}{\text { Adiusted }}$| attenuator |
| :---: |
| sactor |
| switch |
| setting |$\times \underset{\text { Deflection }}{\text { Conversion }}$| Factor |
| :---: |

This adjusted Deflection Factor applies only to the right plug-in channel used and is correct only if the Variable vertical position control is not moved from the position set in step 4.
7. To determine the peak-to-peak amplitude of a signal compared to a reference, disconnect the reference and set the vertical attenuation switch to a deflection factor which will provide sufficient deflection to make the measurement. Do not move the vertical deflection Variable control.
8. Apply the signal to the Input connector, and measure the deflection. The amplitude may be determined by the following formula:

Example: Assume a reference signal amplitude of 30 volts, a vertical attenuator switch setting of 5 , and a deflection of 4 cm . Substituting these values in the Deflection Conversion Factor formula (step 5):
$\begin{aligned} & \text { Deflection } \\ & \text { Conversion } \\ & \text { Factor }\end{aligned}=\frac{30}{4 \times .5}=1.5$
Then, with an attenuator switch setting of 10, the Adjusted Deflection Factor (step 6) would be:

> Adjusted
> Deflection $=10 \times 1.5=15$ volts $/ \mathrm{cm}$
> Factor

To determine the peak-to-peak amplitude of an applied signal which produces a vertical deflection of 5 cm , use the Signal Amplitude formula (step 8):
$\underset{\text { Amplitude }}{\text { Signal }}=15 \times 5=75$ volts.

## Time Measurements

A. To measure time between two points on a waveform, the Lower Beam and the right plug-in unit are used as an example in the following procedure:

1. Preset the Type IA1 Channel Volts/cm switch to a deflection factor which will permit the signal to be displayed without over-driving the vertical amplifier.
2. Set the Lower Beam DISPLAY switch to RIGHT PLUGIN B.
3. Connect the signal to the Input connector of Channel 1.
4. Set the Volts/cm switch to display approximately 5 vertical cm of the signal.
5. Set the B Triggering controls to obtain a stable display.
6. Set the B TIME/CM switch to the fastest sweep rate that will display less than eight divisions between the desired time measurement points (see Fig. 2-16). See the topic entitled Selecting Sweep Rate in this section concerning the non-linearity of the first and last divisions of display.
7. Adjust the Vertical Position control to move the points between which the measurement is to be made to the Lower Beam graticule center line. This location of the waveform is desirable to permit accurate measurements using the $2-\mathrm{mm}$ markings of the center line.
8. Adjust the Horizontal Position control to move the starting point of the time measurement area to the first-cm graticule line.

## NOTE

The B Triggering LEVEL control and SLOPE switch can be used for horizontally positioning the waveform as explained previously.


Fig. 2-16. Measuring time duration between two points on a waveform.
9. Measure the horizontal distance between the time measurement points. The B TIME/CM VARIABLE control must be in the CALIBRATED position.
10. Multiply the distance measured in step 9 by the setting of the B TIME/CM switch. If sweep magnification is used, divide the result by 10 .
Example: Assume that the distance between the time measurement points is 5 cm (see Fig. 2-16) and the B TIME/CM switch is set to .1 mSEC with the magnifier off.

Using the formula:

$$
\text { Time Duration }=\frac{\begin{array}{c}
\text { horizontal } \\
\text { distance } \\
\text { (in } \mathrm{cm})
\end{array}}{\text { magnification }} \times \begin{gathered}
\text { TIME/CM } \\
\text { setting }
\end{gathered}
$$

Substituting the given values:

$$
\text { Time Duration }=\frac{5 \times 0.1 \mathrm{mS}}{1}
$$

The time duration is 0.5 milliseconds.
B. Time measurements between two time-related events may be made using a Dual-Trace plug-in such as the Type 1A1 and a single beam display of the Type 556.
To simplify procedure steps, assume that the Lower Beam will display Channels 1 and 2 of the right plug-in. Use the following procedure:

1. Set the Lower Beam DISPLAY switch to RIGHT PLUGINB.
2. Set the B Triggering controls for right plug-in internal triggering.
3. Preset the right plug-in Channel 1 and 2 Volts/cm switches for a deflection factor which will permit displays without over-driving the vertical amplifier.
4. Set the right plug-in Mode switch either to Chop or Alt. In general, the Chopped mode is more suitable for
low-frequency signals, and the Alternate mode is more suitable for high-frequency signals. More information on determining the correct mode is given under Multi-Trace Operation in this section.
5. Connect the reference signal to the Channel 1 input and the comparison signal to the Channel 2 input. The reference signal should precede the comparison signal in time. Use coaxial cables or probes which have equal time-delay characteristics to connect the signals to the input connectors.
6. Set both Volts/cm switches to display 4 or 5 vertical cm of the reference signal and the comparison signal.
7. Obtain a stable display with the B Triggering LEVEL control.
8. Set the B TIME/CM switch for a sweep rate which shows as much distance as possible (up to 8 cm ) between the two waveforms.
9. Adjust the Vertical Position controls of Channels 1 and 2 to center the points on each waveform between which the measurement is to be made on the Lower Beam center line.
10. Adjust the Horizontal POSITION control so the Channel 1 (reference) waveform crosses the horizontal center line at a vertical graticule line.
11. Measure the horizontal difference between the Channel 1 wavveform and the Channel 2 waveform (see Fig. 2-17).


Fig. 2-17. Measuring the time difference between two pulses using a dual-trace unit and a single beam.
12. Multiply the measured difference by the setting of the B TIME/CM switch. If sweep magification is used, divide the answer by 10 .

Example: Assume that the TIME/CM switch setting is 50 $\mu \mathrm{SEC}$, the DISPLAY MAG is set to $\times 10$ and the horizontal
difference between waveforms is 4.5 cm (see Fig. 2-17). Using the formula:

$$
\text { Time Delay }=\frac{\begin{array}{c}
\text { TIME/CM } \\
\text { setting }
\end{array} \times \begin{array}{c}
\text { horizontal } \\
\text { difference } \\
\text { (in } \mathrm{cm})
\end{array}}{\text { magnification }}
$$

Substituting the given values:

$$
\text { Time Delay }=\frac{50 \times 4.5}{10}
$$

The time delay is 22.5 microseconds.
C. Time-comparison measurements may also be made using both beams of the Type 556 and two single-channel vertical plug-ins. Time-related events can be displayed by both beams if the beams are both driven at the same sweep rate. It is generally advisable to use the same time base for driving both beams to reduce the overall error resulting from sweep rate tolerances.

Use the following procedure:

1. Set the AMPLITUDE CALIBRATOR switch to 1 VOLTS, the B TIME/CM switch to .5 mSEC , the Lower Beam DISPLAY switch to RIGHT PLUG-IN B, and both plug-in Vertical Attenvator switches to 0.05 volts $/ \mathrm{cm}$.
2. Set the Upper Beam DISPLAY switch to LEFT PLUG-IN B. Both beams will be used (in step 3 and following) to display two separate input signals on the same time base, and the A TIME/CM switch will have no effect on the Upper Beam display.
3. Connect the Calibrator signal to both Vertical Inputs and set the B Triggering controls so both displays are stable while triggering on the positive slope of the waveform.
4. With the two plug-in Vertical Position controls, superimpose the waveforms and position the $50 \%$ amplitude levels to one of the beam graticule center lines.
5. Adjust the Upper Beam and Lower Beam Horizontal POSITION controls so the rising portion at the start of each trace begins on the second vertical ( $1-\mathrm{cm}$ ) graticule line. Do not move either Horizontal POSITION control after the beams are thus registered.
6. Remove the Calibrator signal from the two Input connectors and connect the two time-related signals to be displayed. If necessary reset the plug-in vertical deflection factors so the displays do not overscan the viewing area and repeat step 4.

## NOTE

Since both Upper and Lower Beam displays are initiated by the input signal from the right plug in, it will be necessary to connect the first (reference) signal to the right plug-in Input connector. Also the two signals to be compared should be connected to the two plug-in connectors by cables or probes having the same delay characteristics.

Time-interval measurements can now be made. See Fig. 2-18.

## Delayed Sweep Time Measurements

The delayed sweep mode can be used to make accurate time measurements. Overall accuracy of the measurement will be affected by the following factors:


Fig. 2-18. Measuring the time difference between two pulses using single-channel units, both beams and the same time base.
a. Accuracy of the A Sweep Generator at the sweep rate used.
b. DELAY-TIME MULTIPLIER dial incremental accuracy.

The following measurement determines the time difference between two pulses displayed on the same trace. This application may also be used to measure time difference from two different sources (dual-frace) or to measure time duration of a single pulse.

1. Preset the plug-in vertical deflection factor to permit an on-screen display of the waveform to be measured.
2. Apply the signal to the right vertical plug-in unit.
3. Set the Upper Beam DISPLAY switch to RIGHT PLUG-IN A and the Lower Beam DISPLAY switch to RIGHT PLUG-IN B.
4. Set the B TIME/CM switch for a sweep rate about 10 times faster than that of the A TIME/CM switch.
5. Set the B MODE switch to DLY'D BY A. (Leave the $A$ MODE switch set to NORM).
6. Set the DELAY-TIME MULTIPLIER control for a dial reading between 1.00 and 9.50 .
7. Set the A Triggering controls for normal internal triggering on the right plug-in signa!.
8. Set these B Triggering controls as follows:

LEVEL Fully clockwise and knob pulled outward
MODE
AUTO STABILITY
9. The Upper Beam display should have an intensified portion indicating the delayed B sweep time duration. If necessary, adjust the CONTRAST control to show clearly the difference between the unintensified and intensified portions.

The Lower Beam should show a magnified display of the intensified portion of the Upper Beam display.
10. Turn the DELAY-TIME MULTIPLIER dial to move the intensified portion of the Upper Beam display to the first pulse so the first dial reading can be obtained. The exact point may be determined by positioning the magnified pulse (or the rising portion) to the vertical center line of the graticule, as viewed on the Lower Beam trace (see Fig. 2-19A). Note the reading on the DELAY-TIME MULTIPLIER dial.


Fig. 2-19. Measuring time difference using delayed sweep.
11. Advance the intensified portion of the display to the next pulse (see Fig. 2-19B), determining the exact position as in step 10. Note the reading on the DELAY-TIME MULTIPLIER dial.
12. Subtract the first reading from the second and multiply by the setting of the A TIME/CM switch. This is the time interval between the pulses.

Example: Assume the first dial reading is 3.28 and the second dial reading is 7.41 with the A TIME/CM switch set to 2 mSEC (see Fig. 2-17).
Using the formula:
Time Difference
(delayed sweep)

$$
\underset{\text { reading }}{\substack{\text { second dial }} \underset{\text { reading }}{\text { first dial }} \times \text { A TIME/CM }} \times \underset{\text { setting }}{\text { TIM }}
$$

Substituting the given values:

$$
\text { Time Difference }=(7.41-3.28) \times 2
$$

The time difference is 8.26 milliseconds.
13. If all possible tolerances are included, the formula should read:

$$
\underset{\text { Difference }}{\text { Dime }}=
$$

$$
\underset{\text { reading }}{2 \text { nd dial }}-\underset{\text { reading }}{\text { lst dial }} 1 \pm 0.01 \pm 0.04^{1} \times
$$

A TIME/CM setting
${ }^{1} \pm 0.07$ for 3 fastest A TIME/CM readings

## Delayed Sweep Magnification

The delayed sweep feature can be used to provide widerrange magnification than can be obtained by the use of the DISPLAY MAG switch position. The rate of either sweep is not actually increased; the magnification is the result of delaying the $B$ sweep an amount of time selected by the $A$ TIME/CM switch and the DELAY-TIME MULTIPLIER dial before the display is presented at the sweep rate selected by the B TIME/CM switch. At higher magification ranges, the Triggered Delayed Sweep Magnification procedure should be used.

For delayed sweep magification, use the following procedure:

1. Preset the right plug-in vertical deflection factor for an on-screen display.
2. Set the B Triggering MODE switch to AUTO STABILITY, turn the LEVEL control fully clockwise and pull the LEVEL knob outward.
3. Set the Upper Beam DISPLAY switch to RIGHT PLUGIN A.
4. Apply the signal to the Input connector of the right plug in.
5. Set the A Triggering controls for a stable display on the Upper Beam (SOURCE switch set to RIGHT).
6. Set the B MODE switch to DLY'D BY A.
7. Set the A TIME/CM switch to a setting which displays the complete waveform, and set the B TIME/CM switch to a setting 100 times faster. The Upper Beam display should show the complete waveform with an intensified portion. This intensified portion has a duration equal to the ratio of the B TIME/CM setting to the A TIME/CM setting, and is displayed on the Lower Beam in magnified form.

## NOTE

It may be necessary to adjust the front panel CONTRAST control in order to view the intensified portion of the Upper Beam display more easily.
8. The magnification can be calculated by dividing the $A$ TIME/CM setting by the B TIME/CM setting.

Example: The magnification of the display shown in Fig. $2-20$ with an A TIME/CM setting of $10 \mu \mathrm{SEC}$ and a B TIME/ CM setting of . $1 \mu \mathrm{SEC}$ is:

$$
\text { Magnification }=\frac{10 \times 10^{-6}}{.1 \times 10^{-6}}=100
$$



Fig. 2-20. Using delayed sweep for sweep magnification.

The magnification is 100 times.
The delayed sweep magnification method just described may produce too much jitter at high magnification ranges. Displaying the delayed sweep in a triggered mode provides a more stable display, since the delayed display is triggered at the same point each time. For a triggered delayed sweep display, use the following procedure:

1. Set up the display as given in steps 1 through 7 in the Delayed Sweep Magnification section.
2. With the DELAY-TIME MULTIPLIER dial, move a waveform peak of the magnified display to the vertical center line of the graticule.
3. Push the B Triggering LEVEL knob in and rotate the control slowly counterclockwise. At a point near the $O$ mark, the waveform peak on the magnified display will jump to the start of the B sweep, indicating that the B sweep is now triggered. Notice that rotation of the DELAY-TIME MULTIPLIER dial will cause the intensified portion of the Upper Beam display to jump from one peak to the next, while the delayed sweep display remains stable.
4. Measurement and magnification are as described under Delayed Sweep Magnification.

## Displaying Complex Signals Using Delayed Sweep

Complex signals often consist of a number of individual events of differing amplitudes. Since the trigger circuits are sensitive to changes in signal amplitude, a stable display can normally be obtained only when the sweep is triggered by the event(s) having the greatest amplitude. However, this may not produce the desired display of a lower amplitude event which follows the triggering event. The delayed sweep feature provides a means of delaying the start of the B sweep by a selected amount following the event which triggers the A Sweep Generator. Then, the part of the waveform which contains the information of interest can be displayed. Fig. 2-21 demonstrates this feature. Follow the operation under Delayed Sweep Magnification or Triggered Delayed Sweep Magnification to obtain a display in this mode.


Fig. 2-21. Displaying a complex signal using delayed sweep.

## Frequency Measurements

The frequency of a periodically-recurrent waveform can be determined as follows:

1. Measure the time duration of one cycle of the waveform as described in Time Measurements, step A.
2. The frequency of the signal is the reciprocal of the time duration of one cycle.

Example: The frequency of the signal shown in Fig. 2-22 which has a time duration of 1 ms is:

$$
\text { Frequency }=\frac{1}{.001}=1,000 \text { or } 1 \mathrm{kHz}
$$

## Risetime Measurements

Risetime measurements employ basically the same techniques as time-duration measurements. The main difference is in the points between which the measurement is made. The following procedure gives the basic method of measuring risetime between the $10 \%$ and $90 \%$ points of the waveform.


Fig. 2-22. Determining the frequency of a periodically recurrent waveform when the TIME/CM switch is set to .2 mSEC .

Falltime can be measured in the same manner on the trailing edge of the waveform.

1. Set the Lower Beam DISPLAY switch to RIGHT PLUG-IN B.
2. Preset the Type 1 A1 Channel 1 Volts/cm switch to a deflection factor which will allow the expected signal to be displayed without overdriving the vertical amplifier.
3. Apply the signal to the Channel 1 Input connector.
4. Set the Volts/cm switch and Variable control to produce a display an exact number of divisions in amplitude.
5. Center the display about the horizontal center line of the Lower Beam graticule area.
6. Set the B TIME/CM switch to the fastest sweep rate that will display less than eight divisions between the $10 \%$ and $90 \%$ points on the waveform. The TIME/CM VARIABLE control must be in the CALIBRATED position.
7. Determine the $10 \%$ and $90 \%$ points on the rising portion of the waveform. The figures given in Table 2-3 are for the points $10 \%$ up from the start of the rising portion and $10 \%$ down from the top of the rising portion ( $90 \%$ point).

TABLE 2-3

| Vertical Display (cm) | $10 \%$ and $90 \%$ points |
| :---: | :---: |
| 4 | 0.4 cm |
| 5 | $\frac{0.5 \mathrm{~cm}}{0.6 \mathrm{~cm}}$ |
| 6 |  |

8. Adjust the Horizontal POSITION control to move the $10 \%$ point of the waveform to the second cm graticule line. For example, with a $5-\mathrm{cm}$ vertical amplitude display as
shown in Fig. 2-23, the $10 \%$ point would be 0.5 cm up from the start of the rising portion.

NOTE
If the fastest sweep speed ( $10 \mathrm{~ns} / \mathrm{cm}$ ) is used, set the Triggering LEVEL control so the rising portion of the waveform starts at the fourth cm graticule line.
9. Measure the horizontal distance between the $10 \%$ and 90\% points.
10. Multiply the distance measured in step 9 by the setting of the TIME/DIV switch. If sweep magnification is used, divide this answer by 10 .

Example: Assume that the horizontal distance between the $10 \%$ and $90 \%$ points is 4 cm (see Fig. 2-23) and the TIME/ DIV switch is set to $1 \mu$ SEC with the DISPLAY MAG switch set to $\times 10$. Applying the time duration formula to risetime:

$$
\begin{aligned}
\begin{array}{c}
\text { Risetime } \\
\text { (Time Duration) }
\end{array} & \begin{array}{c}
\text { horizontal } \\
\text { distance } \\
(\text { in } \mathrm{cm})
\end{array}
\end{aligned} \times \begin{gathered}
\text { TIME/CM } \\
\text { setting }
\end{gathered}
$$

Substituting the given values:

$$
\text { Risetime }=\frac{2 \times 1}{10}=0.2 \text { microsecond. }
$$



Fig. 2-23. Measuring risetime.

## Delayed Trigger Generator

The B GATE output signal (available at the front-panel connector) can be used to trigger an external device at a selected delay time after the start of the A Sweep. The delay time of the B GATE output signal can be selected by the setting of the DELAY-TIME MULTIPLIER dial and A TIME/CM switch.

A Sweep Triggered Internally. When the A Sweep is triggered internally to produce a normal display, the delayed trigger may be obtained as follows:

1. Obtain a triggered display in the normal manner on the Upper Beam.
2. Set the B MODE switch to DLY'D BY A.
3. Select the amount of delay from the start of A Sweep by means of the DELAY-TIME MULTIPLIER dial, positioning the intensified portion of the Upper Beam display as desired.
4. Connect the B GATE signal to the external equipment.
5. The duration of the B GATE pulse is determined by the setting of the B TIME/CM switch.
6. The external equipment will be triggered at the start of the intensified portion if it responds to positive-going triggers, or at the end of the intensified portion if it responds to negative-going triggers.

A Sweep Triggered Externally. This mode of operation can be used to produce a delayed trigger with or without a corresponding display. Connect the external trigger signal to the A Triggering TRIGGER INPUT connector and set the A Triggering SOURCE switch to EXT. Obtain a triggered sweep of the Upper Beam. Then, follow the operation given under A Sweep Triggered Internally (steps 2 through 6) to obtain the delayed trigger.

## Normal Trigger Generator

Ordinarily, the signal to be displayed also provides the trigger signal for the oscilloscope. In some instances, it may be desirable to reverse this situation and have the oscilloscope trigger the signal source. This can be done by connecting the A GATE signal to the input of the signal source. Pull the A Triggering LEVEL knob outward, rotate the LEVEL control fully clockwise, set the A Triggering MODE to AUTO STABILITY, and adjust the A TIME/CM switch for the desired display. Since the signal source is triggered by a signal that has a fixed time relationship to the sweep, the output of the signal source can be displayed on the CRT as though the Type 556 were triggered in the normal manner.

## Multi-Trace Phase Difference Measurements

Phase comparison between two signals of the same frequency can be made using the dual-beam feature with singleinput plug-ins. This method of phase-difference measurement can be used up to the frequency limit of the vertical system provided both the A and B horizontal amplifiers are accurately calibratetd and are identical. To make the comparison, use the following procedure:

1. Set the AMPLITUDE CALIBRATOR switch to .1 VOLTS, the B TIME/CM switch to .5 mSEC , and both plug-in vertical attenuator switches to 0.05 volts $/ \mathrm{cm}$.
2. Set the Lower Beam DISPLAY switch to RIGHT PLUGINB.
3. Set the Upper Beam DISPLAY switch to LEFT PLUGIN B. Both beams will be used (in steps 4 and following) to display two separate input signals on the same time base, and rotation of the A TIME/CM switch will have no effect on the Upper Beam display.
4. Connect the Calibrator signal to both Vertical Inputs and set the B Triggering controls so both displays are stable while triggering on the positive slope of the waveform.
5. With the Vertical Position controls, superimpose and center the waveforms on the Lower Beam graticule center line.
6. Adjust the Upper and Lower Beam Horizontal POSITION controls so the start of each trace is on the first vertical $(0-\mathrm{cm})$ graticule line. Then, if necessary, slightly readjust one of the Horizontal POSITION controls so the rising portions of the square waves are superimposed in the center area of the graticule. Do not move either Horizontal POSITION control after the beams are thus registered.
7. Remove the calibrator signal from the two Input connectors, adjust both vertical attenuator switches to a deflecfion factor which will display the signals to be compared, and apply the two signals to the plug-in Inputs. (If the displays are not the desired size, reset the vertical attenuator switches).

## NOTE

Since both Upper and Lower Beam displays are initiated by the input signal from the right plug-in, it will be necessary to connect the first (reference) signal to the right plug-in Input connector. Also the signals to be compared should be connected to the plug-ins by means of cables or probes having the same delay characteristics.
8. With the B Triggering controls, obtain a stable display (both beams).
9. Set the B TIME/CM switch to a sweep rate which displays about one cycle of the waveform.
10. Turn the B TIME/CM VARIABLE control until one cycle of the reference signal (the right plug-in) occupies exactly 9 cm horizontally (see Fig. 2-24). Each cm then represents $40^{\circ}$ of the cycle ( $360^{\circ}$ divided by $9 \mathrm{~cm}=40^{\circ}$ per cm ). This is the phase factor.
11. Measure the horizontal difference between corresponding points on the waveform.
12. Multiply the measured distance (in cm ) by $40^{\circ}$ (phase factor) to obtain the exact amount of phase difference.

Example: Assume a horizontal difference is 0.6 cm with a phase factor of $40^{\circ}$ as shown in Fig. 2-24.

Using the formula:

$$
\begin{aligned}
\text { Phase Difference }=\underset{\text { horizontal }}{\text { difference }} \\
\text { (in } \mathrm{cm} \text { ) }
\end{aligned} \times \underset{\text { phase }}{\text { factor }}
$$

Substituting the values given:
Phase Difference $=0.6 \times 40^{\circ}$
The phase difference is $24^{\circ}$.
More Precise Phase Measurements. More precise phase measurements can be made by increasing the sweep rate
(without changing the B TIME/CM VARIABLE control setting). One of the easiest ways to increase the sweep rate is with the Lower Beam DISPLAY MAG switch. Delayed sweep magnification may also be used. The adjusted phase factor is determined by dividing the phase factor obtained previously by the increase in sweep rate.

Example: If the sweep rate were increased 10 times with the magnifier, the adjusted phase factor would be $40^{\circ}$ divided by $10=4^{\circ}$ per cm . Fig. $2-25$ shows the same signals used in Fig. 2-24 but with the Lower Beam DISPLAY


Fig. 2-24. Measuring phase difference.

MAG switch set to $\times 10$. With a horizontal difference of 6 cm , the phase difference is:

$$
\begin{aligned}
& \text { horizontal adjusted } \\
& \text { Phase Difference }=\text { difference } \times \text { phase } \\
& \text { (in } \mathrm{cm} \text { ) factor }
\end{aligned}
$$

Substituting the given values:
Phase Difference $=6 \times 4^{\circ}$
The phase difference is $24^{\circ}$.


# SECTION 3 <br> CIRCUIT DESCRIPTION 

Change information, if any, affecting this section is found at the rear of the manual.

## Introduction

This section of the manual contains a functional description of the instrument circuitry. A general discussion of display logic, with accompanying diagrams, preceeds the detailed functional circuit analysis.

## DISPLAY LOGIC

The display logic system used to connect deflection signals to the dual independent vertical and horizontal deflection circuits provides the instrument with a versatility that permits accommodation of diverse applications. The two beams may be deflected by signals from several sources. In general, the signal source options are as follows:

Upper Beam—Vertical deflection by signals from either plugin unit. Horizontal deflection by sweep signals from either A or B time base generator or by signals from an external source (EXT HORIZ IN).

Lower Beam-Vertical deflection by signals from the right plug-in only. Horizontal deflection by sweep signals from either A or B time base generator (Time-base B only for serial numbers 1999 and below) or by signals from an external source.

Table 3-1 lists some typical applications with examples of signal source selections. The figure number listed with an
application refers to the illustration that shows the major circuit interconnections for the selected signal source opions.

## FUNCTIONAL BLOCK DIAGRAMS

To provide a basis for this discussion, six functional block diagrams (Fig. 3-1 through 3-6) are used to demonstrate how the major circuit blocks are connected when a particular operating mode is set up. There are many other combinations that can be shown, depending on the setting of the controls and the plug-in units used, but these six modes are intended to provide the fundamental information needed for quickly analyzing the internal operation of the Type 556 before studying the individual circuits in detail.

## First Basic Mode (Fig. 3-1)

In this mode of operation the Type 556 is operating as two completely independent systems. A signal applied to the left plug-in unit is coupled to the Left Vertical Input Amplifier. At this point a portion of the signal is taken off to provide normal internal push-pull triggering signals to the A Sweep Trigger circuit. This circuit converts the triggering of the A Sweep Generator.
With the Upper Beam DISPLAY switch set to LEFT PLUGIN A, the sawtooth from the A Sweep Generator is applied to the Upper Beam Horizontal Amplifier. This amplifier provides push-pull drive to the Upper Beam horizontal deflection plates.

TABLE 3-1

| Application | Signal Source Selection |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Upper Beam |  | Lower Beam |  |
|  | Vertical | Horizontal | Vertical | Horizontal |
| Two indepent display sys- <br> tems. Fig. 3-1. | Left | A sweep | Right | B sweep |
| Signals from one plug-in <br> displayed at two sweep <br> rates. Figs. 3-2, 3-4 and 3-6. | Right | A sweep | Right | B sweep |
| Signals from two plug-ins <br> displayed at a common <br> sweep rate. | Left | B sweep | Right | B sweep |
| Dual X-Y displays. | Left | External | Right | External |
| Combined X-Y and Y-T <br> (time-basel displays. Fig. <br> 3-3. | Right | External | Right | B sweep |
| Dual multi-trace displays. <br> Fig. 3-5. | Right | A sweep | Right | B sweep |
| B sweep delayed by A <br> sweep. Fig. 3-6. | Right | A sweep | Right | B sweep |



Going back to the Left Vertical Input Amplifier block, the left vertical signal is also applied to the Diode Switching circuit. With the Upper Beam DISPLAY switch set as given, the Diode Switching circuit connects the signal to the left vertical Delay Line. Any signal from the right plug-in is blocked by the "off" diodes in the Diode Switching circuit.

The Delay Line is a specially braided 186 -ohm line which delays the application of the left plug-in signal to the Left Vertical Output Amplifier for 170 ns. This amount of delay provides time for unblanking the Upper Beam and starting the horizontal sweep before the vertical signal reaches the Upper Beam vertical deflection plates. Thus, it is possible to display the leading edge of a single fast-rising pulse. The Delay Line has a constant characteristic impedance along its length and requires no adjustment.

The signal applied to the right plug-in drives the Lower Beam deflection plates and B Sweep Trigger in the same manner as described for the Upper Beam system. In like manner, the B Sweep Trigger circuit triggers the B Sweep Generator. The sawtooth output is applied to the Lower Beam Horizontal Amplifier which in turn is used to drive the Lower Beam horizontal deflection plates.

## Second Basic Mode (Fig. 3-2)

This mode shows the Type 556 operating as two interconnected vertical deflection systems with independent horizontal deflection systems. The main advantage of this mode is that only one probe need be used for coupling the signal to the Type 556, and yet maximum flexibility is obtained in displaying the signal on both beams. Use of one probe will minimize circuit loading of the device under test as compared to using separate probes at the same test point.

The vertical signal to be displayed by both beams is applied to the right plug-in. At the Right Vertical Input Amplifier the signal is taken off in the usual manner for application to the A and B Sweep Trigger circuits. The trigger circuits trigger their respective Sweep Generator circuits. The A Sweep Generator and Upper Beam Horizontal Amplifier circuits drive the Upper Beam horizontal deflection plates. Similarly, the B Sweep Generator and Lower Beam Horizontal Amplifier circuits drive the Lower Beam horizontal deflection plates. The sweep rate for the one beam can be controlled independent of the other. Thus, the displays shown in Fig. 3-2, for example, can be obtained by setting one sweep rate twice as fast as the other.
Also, from the Right Vertical Input Amplifier the signal goes through a Crossover Amplifier to the Diode Switching circuit. With the Upper Beam DISPLAY switch set to RIGHT PLUG-IN $A$, the diodes for the right plug-in signal are turned on and the signal goes through the left vertical Delay Line and Left Vertical Output Amplifier to the Upper Beam vertical deflection plates. The signal from the left plug-in is blocked by the "off" diodes in the Diode Switching circuit.

To provide a vertical display on the Lower Beam, the right plug-in signal goes through the Right Vertical Input Amplifier, right vertical Delay Line and Right Vertical Output Amplifier to the Lower Beam vertical deflection plates.

Since the left plug-in is not used in this mode for display purposes, it can be used to amplify a low-amplitude triggering signal for application to the A and B Sweep Trigger
circuits. To use this trigger, set the $A$ and $B$ Triggering SOURCE switches to LEFT, INT, NORM.

## Third Basic Mode (Fig. 3-3)

Under the conditions given in Fig. 3-3, the Type 556 is operating as two interconnected vertical systems and two independent horizontal deflection systems. In this mode, however, the Upper Beam Horizontal Amplifier is driven externally to obtain an Upper Beam X-Y display of the right plug-in and external horizontal input signals. The Lower Beam is used in a conventional manner to display the right plug-in signal amplitude against time.

Since the A Sweep Trigger and A Sweep Generator circuits are not used to obtain the displays, these circuits can be used for other purposes, if desired. For example, the A Sweep Generator block shows that its output signals are available. In addition, the left plug-in and Left Vertical Input Amplifier blocks are available for other uses as mentioned in the Second Basic Mode description.

## Fourth Basic Mode (Fig. 3-4)

Fig. 3-4 shows the Type 556 operating as two interconnected vertical and horizontal deflection systems. Here the right plug-in signal is applied to the vertical deflection plates of both beams and the B Sweep circuit is used to provide dual-beam horizontal deflection.

Horizontal deflection of the beams can be controlled individually by using the DISPLAY MAG switches. To obtain the displays shown, the Upper Beam DISPLAY MAG switch is set to $\times 1$ and the Lower Beam DISPLAY MAG switch is set to $\times 10$.

As described previously, the blocks that are not used for obtaining the displays can be used for other purposes.

## Fifth Basic Mode (Fig. 3-5)

In this mode of operation the Type 556 is operating as two interconnected vertical deflection systems. The dual-trace right plug-in unit provides the vertical deflection for both beams. Both Sweep Generators and Horizontal Amplifiers provide independent horizontal deflection drive for their respective beams.

With the dual-trace unit operating in the alternate mode, the Alternate Trace Logic circuit is used to produce one alternate sync pulse per slower sweep. For example, assume that both Sweep Generators are triggered simultaneously by the right plug-in channel 1 signal and both sweeps have started. Also, assume that the A Sweep is set to run several times slower than B Sweep. Under these conditions, the B Sweep Generator will generate several sweeps while the $A$ Sweep is still running up. But, each time the B Sweep resets no alternate sync pulses are produced during the A Sweep runup.

As soon as the A Sweep ends, however, the A Sweep Inhibit gate keeps the A Sweep from starting again until the B Sweep can reset once again. As the B Sweep resets, the combined condition of A Sweep off and B Sweep resetting causes the Alternate Trace circuit to produce one alternate sync pulse that is applied to the dual-trace unit. The



Fig. 3-3. The Type 556 operating as two interconnected vertical deflection systems and two completely independent horizontal deflection systems. Upper Beam Horizontal Amplifier is driven externally to obtain an X-Y display and the Lower Beam is driven by the B Sweed.



Circuit Description-Type 556

## Circuit Description-Type 556

alternate sync pulse switches the plug-in unit to channel 2. Both sweeps start again and deflect their respective beams so a dual-beam display of channel 2 is obtained.

If the B Sweep is the slower sweep, the A Sweep will run only once and is locked out by the A Sweep Inhibit gate until the B Sweep resets. Since the A Sweep is the only one which is locked out in each case, best results are obtained by running the B Sweep at the same rate or faster than the A Sweep. This same operating characteristic applies if a singlechannel plug-in unit is used.

As shown in Fig. 3-5, the A and B Triggering switches are set to RIGHT, INT, PLUG-IN. In these positions the channel 1 trigger is applied from the right plug-in to both Sweep Trigger circuits and the internal triggering signal from the Left and Right Vertical Input Amplifiers are not used. Thus, use of the channe! 1 trigger permits the channel 1 input signal to be used as the time reference for channel 2.

If the dual-trace unit is set for chopped-mode operation, (not shown in Fig. 3-5) the plug-in sends chopped blanking pulses via the Chopped Blanking Amplifier and CRT Cathode Selector switches to the CRT cathodes to blank out the traces during the channel-switching intervals.

## Sixth Basic Mode (Fig. 3-6)

For the conditions given in Fig. 3-6, the Type 556 is operating as two interconnected vertical deflection systems with the right plug-in signal displayed by both beams. The horizontal deflection systems are operating independently since each beam is driven by its respective Sweep Generator and Horizontal Amplifier. In this (Delayed B Sweep) mode of operation, where the B MODE switch is set to DLY'D BY A and the B Triggering is automatic, the B Sweep starts automatically after the A Sweep delay time.

If the right plug-in triggering signals from the Right Vertical Amplifier are applied to the B Sweep Trigger circuit and the B Triggering controls are set for triggered operation, the B Sweep will not start automatically after the delay time but must be triggered by a right plug-in internal triggering signal. Once triggered, the B Sweep will run. Delay time is determined by the A TIME/CM switch in the A Sweep Generator circuit and the DELAY-TIME MULTIPLIER control in the Delay Pickoff circuit. To prevent the A Sweep from running again until the B Sweep can reset, the B Gate is applied to an Inverter stage in the Alternate Trace Logic circuit. The inverted B Gate is used as an A Sweep Inhibit gate to lock out the A Sweep. When the sweeps reset, the A Sweep will run again when triggered by the right plug-in signal and the cycle is repeated.
Referring to Fig. 3-6 again, this same mode of operation can be changed easily to single-sweep B delayed mode by setting the A MODE switch to SINGLE SWEEP. When triggered, the A Sweep will run only once, the B Sweep will run automatically after the delay time and the sweeps will not start again until the A MODE RESET button is pressed and the A Sweep is triggered to repeat the cycle.

## CIRCUIT ANALYSIS

The following circuit analysis of the Type 556 is keyed to detailed block diagrams that are provided in this portion
of the manual. These diagrams give the names of the individual stages and show how they are connected together to form a major circuit. The major circuits from which the detailed block diagrams are derived, are shown on the schematic diagrams located on the pullout pages in the Diagrams section.

Each schematic diagram has been assigned a reference diagram number in a diamond frame; for example, Left Vertical Amplifier $\langle 1$. These numbers are used throughout the detailed block and schematic diagrams as references to point out where a circuit on one diagram ties into the circuit on another diagram. When reading through the description, refer to the schematic diagrams for electrical values of components, voltages, waveforms and other detailed information as needed.

As supplemental information to the detailed blocks provided in this section, there are two more block diagrams provided on pullout pages in the Diagrams section. These diagrams show the interrelationship of blocks throughout the vertical and horizontal systems.

## LEFT VERTICAL AMPLIFIER

## Input Cathode Follower, V3

The push-pull output of the left plug-in, with a fixed DC level of about +67.5 V , is applied to the Input Cathode Follower V3 stage (see Fig. 3-7) via pins 1 and 3 of the plugin connector Jll .

Letter-series plug-in units, when inserted into the oscilloscope, actuate the transient-response compensation switch SW105. This switch connects a series network, C100 and R100, across the input to V3A and V3B. The network compensates for the slight difference in transient response that exists between the letter- and 1 -series vertical plug-in units. Since the switch is mechanically actuated by the plug-in, no attention on the part of the operator is required.

Resistors R1 and R101, connected in series with the grids of $V 3 A$ and $V 3 B$, are parasitic suppressors. $V 3 A$ and $V 3 B$ are two halves of a 12AT7 twin-triode tube. The cathodes of the tube are returned to ground through the DC BALANCE control R5. This control adjusts the bias voltages of V3A and V3B so that the CRT trace will come to graticule center with V3A and V3B grids connected together.

The heaters of V3 and V661 (see Heater Wiring diagram) are part of a series heater circuit which receives power from the $+100-\mathrm{V}$ DC supply. V3 and V661 heaters drop the voltage 25 V to provide 75 V at 150 mA to the remaining portion of the heater string located in the left plug-in unit. The DC voltage supply to the plug-in heaters eliminates hum modulation of the cathodes and stablizes the tube gain.

Protection diodes D4 and D104 prevent V3 cathodes from going below +61 V . This voltage is set by a 39 V zener, D6, connected between the anodes of the diodes and the +100 V supply. D4 and D104 are normally back-biased, but if the cathode voltages should attempt to decrease below +61 V , the diodes will conduct and clamp the cathodes, thus preventing any further decrease in cathode voltage. Zener D6 is also connected to a voltage divider network. At the junction of R6 and R7 the voltage is about +50 V which is used as the low-impedance voltage source for the Diode Switch-


Circuit Description-Type 556


Fig. 3-7. Partial block diagram of Left Vertical Amplifier.
ing stage to be described later. Diodes D8, D108, D9 and D109 (for SN 100-1999, D7, D8, and D108) provide protection for certain transistors in the stages that follow.

## Signal Input Emitter Follower, Q3 and Q103

The push-pull left plug-in signal from the Input C. F. stage is applied to the Signal Input E. F. (Q3, Q103) stage. For signal purposes, this stage is an emitter follower since the output is taken from its emitters. However, the collector circuits operate in a cascode configuration with the Trigger Pickoff Amplifiers (Q74, Q174).

To compensate for variations between plug-in units in output DC level from the nominal +67.5 V , the output from the Trigger DC Collector Current Regulator stage (Q83, Q84) is applied to R9 and R109 in the emitter circuit of Q3 and Q103. Further details about the regulator stage are described later.

## Trigger Pickoff Amplifier, Q74 and Q174

To obtain a push-pull triggering signal which is always available for normal internal triggering purposes when the SOURCE switch is set to LEFT, INT, NORM, the signal must be taken off ahead of the Diode Switching stage. This is accomplished by connecting the Trigger Pickoff Amplifier (Q74, Q174), in a cascode configuration with the Input E. F. stage.

The push-pull internal trigger output from Q74 and Q174 is applied to the Trigger Pickoff E.F. stage.

## Trigger Pickoff Emitter Follower, Q73 and Q173

This stage provides low-impedance drive for the $A$ and $B$ Triggering SOURCE switches. When the SOURCE switches are set to LEFT, INT, NORM, the normal internal triggering signal with its regulated DC output level is coupled to the $A$ and $B$ Sweep Trigger circuits for use in triggering the $A$ and B Sweep Generator circuits.

## Left Trigger Current Regulator, Q83 and Q84

The regulator stage consisting of Q83 and Q84 with associated circuitry acts as a series bootstrap element that automatically regulates the common-mode DC collector currents so that collector voltage levels are held constant. This is particularly important when using the DC coupling mode of triggering. When using this mode, the DC levels at the collectors of Q74 and Q174 must be held at a nominal value to maintain proper DC levels at the emitters of Q73 and Q173 for application to the Sweep Trigger circuits.

If the plug-in output $D C$ level is more or less than +67.5 V , this common-mode voltage change from the nominal value of of 67.5 V tends to cause a current change through $\mathrm{Q} 3, \mathrm{Q} 103$, Q74 and Q174. This current change tends to change the voltage at the collectors of Q74 and Q174. As a result, an error signal is developed at the junction of L77 and L177.

The error signal is applied to the base of Q83. This transistor operates as an emitter follower for the error signal which is then applied to the base of Q84. Transistor Q84 and associated circuitry acts as a series-element regulator in the emitter circuit of Q3 and Q103 comparing the error signal voltage to the +100 V supply. By resetting the emitter voltages of Q3 and Q103, current through the transistors is the same as if the plug-in output level were +67.5 V .

The regulating action of Q83 and Q84 causes the voltage at the junction of L 77 and L 177 to remain constant so the collector voltage of Q74 and Q174 are maintained at a nominal level for application to the bases of Q73 and Q173. Thus, with the plug-in unit Position control centered so the voltages at pins 1 and 3 of $\mathrm{Jl1}$ are equal, the voltage at the emitters of Q73 and Q173 should be about +50 V .

The zener diode drop across D87 is used as a reference voltage for the bases of Q74 and Q174. Thus, the bases move up and down in phase with the junction of R9 and R109, but 12 volts removed by D87.

## Delay Line Driver Amplifier, Q14 and Q114

The balanced Delay Line Amplifier stage, Q14 and Q114, is a push-pull stage which is actually connected in cascode with Q44 and Q144. An adjustable vertical GAIN control R12 is provided in the emitter circuit. Gain is adjusted by controlling the amount of degeneration. Variable capacitor C10 is adjusted to vary the time constant sufficiently to optimize the transient response.

The RC networks in the collectors of Q14 and Q114 are thermal time constant compensations. The push-pull signal from this stage provides signal current drive for the Diode Switching circuit and delay line.

In the LEFT PLUG-IN positions of the Upper Beam DISPLAY switch, the Left Amplifier Current Regulator, Q93 and Q94, provides a regulated current via R14 and R114 to the emitters of Q14 and Q114.

## Diode Switching Circuit

Fig. 3-8 shows the operation of the Diode Switching circuit. This circuit permits passage of either the left or right plug-in signals to the Upper Beam vertical deflection plates. The Upper Beam DISPLAY switch is used to control the switching of the diodes.
The LEFT and RIGHT positions of the Upper Beam DISPLAY switch shown in Fig. 3-8 correspond to these frontpanel positions: LEFT is any of the LEFT PLUG-IN positions and RIGHT corresponds to the RIGHT PLUG-IN positions. Assume the Upper Beam DISPLAY switch is set to the LEFT position. +72 V is applied from the collector circuit of Q94 (see Fig. 3-7) to the cathode junctions of D17 and D117 to turn these diodes off and turn on diodes D15 and D115. As a result the left plug-in signal passes through diodes D15 and D115 to the left-vertical delay line.

On the other hand, +50 V is applied to the cathode junctions of D19 and D119 to turn these diodes on and turn off diodes D16 and D116. Thus, diodes D16 and D116 prevent the right plug-in signal from being applied to the left-vertical delay line.

If the Upper Beam DISPLAY switch is set to the RIGHT position, just the opposite occurs. +50 V is applied to D17 and D117 and +72 V is applied from the collector circuit of Q94 to D19 and D119. Hence, all the previously on diodes are turned off and the off diodes are turned on. The left pulg-in signal is blocked by D15 and D115; D16 and D116 pass the right plug-in signal to the left-vertical delay line.

## Right Plug-In Crossover E. F., Q23 and Q123

The right plug-in signal from the Signal Input E. F. (Q203, Q403) in the Right Vertical Amplifier circuit is applied at all times through 93 -ohm coaxial cables to the Right Plug-In Crossover E. F. (Q23, Q123). Termination for the cable is provided by R20 and R120. Purpose of the emitter follower stage is to isolate the impedance of the cables from the input impedance of the Delay Line Driver Amplifier circuit. The input impedance of the right Plug-In Crossover, E. F. stage depends upon settings of the gain and peaking adjustments.

## Right Plug-In Crossover Amplifier, Q34 and Q134

This stage is very similar to the Delay Line Driver Amplifier Q14 and Q114 described earlier. In the emitter circuit a CROSSOVER GAIN control R34 is provided to adjust the gain of the stage so the vertical deflection factor of the right plug-in signal amplitude to the Upper Beam vertical deflection plates is the same as that from the left plug-in unit.

Variable capacitors C19, C30 and C31 with R31 are adjusted for optimum transient response. These adjustments vary the high-frequency peaking in the emitter circuit.

In the RIGHT PLUG-IN positions of the Upper Beam DISPLAY switch, a regulator current is fed from the Left Amplifier Current Regulator (Q93, Q94) through the switch via R36 and R136 to the emitters of Q34 and Q134. In the LEFT PLUG-IN positions of the Upper Beam DISPLAY switch, R37 provides "keep alive" current for diodes D19 and D119.

## Left Vertical Delay Line

Output from the left or right Delay Line Driver stages is applied through the Left Vertical Delay Line to the Output Driver Amplifier (Q44, Q144). The Delay Line delays the signal about 170 ns to give the Sweep Generator circuit time to initiate a sweep before the vertical signal reaches the Upper Beam vertical deflection plates.

R41-C41 and R141-C141 provide the output termination for the Delay Line; R18 provides the reverse termination. The center-tapped inductors, L18 and L118, at the input to the Delay Line and the collector-base capacitance of the delay line transistors form a T -section matching network. Impedance of the network can be varied by adjusting Cl 7 in the LEFT PLUG-IN positions of the Upper Beam DISPLAY switch and C19 in the RIGHT PLUG-IN positions.

## Output Driver Amplifier, Q44 and Q144

This stage forms the other portion of the cascode amplifier with the Delay Line Driver Amplifier Q14 and Q114. Net-


Fig. 3-8. Partial block-and-circuit diagram of Left and Right Vertical Amplifiers. The diodes are located in the Diode Switching circuit of the Left Vertical Amplifier.


Fig. 3-9. Partial block diagram of Left and Right Vertical Output Amplifiers.
works C42-R42 and R142-C142 are temperature compensations for Q44 and Q144. L43 and L143 are adjustable Tcoils for high-frequency peaking.

Zener D144 limits the base-collector voltage to about 22 V for protection purposes. Any change in DC level at the anode of DI44 due to a change from nominal in output DC level of the plug-in is applied to the Left Amplifier Current Regulator, Q93 and Q94. D146 supplies base voltage to Q44 and Q144.

A TRACE SEPARATION control R182 is switched into the emitters of Q44 and Q144 when the Upper Beam DISPLAY switch is set to the RIGHT PLUG-IN positions allowing the Upper Beam to be positioned independently of the Lower Beam.

## Left Amplifier Current Regulator, Q93 and Q94

This stage regulates the DC collector levels of Q44 and Q144 to compensate for any change in plug-in unit DC output level from the nominal value of +67.5 V .

For regulating purposes, if the $D C$ level at the junction of R90 and R91 tends to change due to a change in current through Q44 and Q144, an error signal is developed and applied to the base of Q93. The emitter output from Q93 is applied to the base of Q94. Transistor Q94 serves as a DC current series regulator to control the emitter current of Q14 and Q114 when the Upper Beam DISPLAY switch is set to any of the LEFT PLUG-IN positions.

In the RIGHT PLUG-IN positions of the switch, the regulating current is applied to the Right Plug-In Crossover Amplifier (Q34 and Q134).

With the Upper Beam DISPLAY switch set to RIGHT PLUGIN A, the right plug-in vertical Position control positions both beams simultaneously but cannot position one beam with respect to the other. However, the latter situation is solved by adding a TRACE SEPARATION control, R182, in the Q94 collector circuitry. The control varies the DC current through R180 more than through R184, or vice versa, so that the control acts as a vertical positioning control for the Upper Beam.

The positioning currents are applied via the Upper Beam DISPLAY switch through R40 and R140 to the emitter input circuit of Q44 and Q144. When the Upper Beam DISPLAY switch is set to any of the LEFT PLUG-IN positions these positioning currents are disconnected from R40 and R140 so the TRACE SEPARATION control has no effect on the Upper Beam. The control is disconnected at this time because the left plug-in Position control provides the normal vertical positioning range for the Upper Beam.

## Output E. F., Q43 and Q143

This stage is an emitter follower for either the left or right plug-in signals from the Output Driver Amplifier (Q44, Q144), depending on the position of the Upper Beam DISPLAY switch.


Fig. 3-10. Block diagram of the A Sweep Trigger.

To trace the signal, assume the Upper Beam DISPLAY switch is set to the LEFT PLUG-IN positions. The push-pull left plug-in signal is applied to the bases of Q43 and Q143 and the output signal at the emitters is used to drive the lower part (Q54, Q154) of the hybrid Output Amplifier stage.

## Output Amplifier Q54, Q154, V64 and V164

The Output Amplifier stage operates in a hybrid cascode configuration to drive the Upper Beam vertical deflection plates and to raise the DC output level from about +50 V at the bases of the transistors to about +176 V at the deflection plates.

L64 and L164 are T-coils that provide high-frequency peaking in the stage. Other high-frequency compensation adjustments are HF COMP 1 (R52), HF COMP 2 (R54), C51, C53, C54 and C55.

The BEAM FINDER button, when pressed, disconnects R150 and R151 limiting the emitter current to Q54 and Q154. This restricts the dynamic operating range of the transistors limiting the trace to the Upper Beam display area. The BEAM FINDER switch SW155 also connects R62 and R162 in shunt
with Q54 and Q154 maintaining current through V64 and V164 essentially constant, so that the average CRT deflection plate potential does not change. The BEAM FINDER switch SW1 55 performs a similar function in the Right Vertical Amplifier circuit. This same switch is used in the Upper and Lower Beam Horizontal Amplifier circuits to restrict the horizontal deflection simultaneously with the vertical deflection.

The +10 V in the emitter circuit of Q54 and Q154 is a supply voltage obtained from zener D442 in the Q244-Q444 emitter circuit of the Right Vertical Amplifier. This voltage goes to terminals $A B$ in the Power Supply circuit for distribution to relay coils L1125 (Upper Beam Horizontal Amplifier) and L1225 (Lower Beam Horizontal Amplifier).
In the grid circuit of V64 and V164 there is an 8608 BIAS adjustment R69. This adjustment sets the collector voltage rcross Q54 and Q154 for correct thermal characteristics.

## RIGHT VERTICAL AMPLIFIER

This circuit is the same as the Left Vertical Amplifier except for the crossover amplifier and TRACE SEPARATION control circuitry which have already been described.

## A SWEEP TRIGGGER〈3

## Trigger Source

The triggering signal source is selected with the SOURCE switch SW515. Six sources are available and they are all shown being applied to the SOURCE switch block in Fig. 3-10. The SOURCE switch block lists all the SOURCE switch positions. Each position is shown with its corresponding signal source.

## Trigger Coupling

The COUPLING switch offers a means of accepting or rejecting certain frequency components of the triggering signal. In the AC and AC LF REJ positions, the DC component of a push-pull signal is blocked by coupling capacitors C501 and C502, and C525 or C526. In the AC position, frequency components below about 30 Hz will be attenuated. In the AC LF REJ position, frequency components below about 1.6 kHz will be attenuated.

The AC HF REJ position attenuates high-frequency components of the triggering signal. The signals are AC-coupled and are attenuated below about 60 Hz and above about 100 kHz . In the DC position, the push-pull normal internal triggering signal is DC-coupled to the triggering circuit via dividers R504-R505 and R520-R521. The no-signal DC level at the input to the dividers with the plug-in Position control centered is about +50 V . At the output of the dividers the voltage is about zero.

## Trigger Level

The A Triggering LEVEL control R518 applies a DC voltage to one grid or the other of V534, depending on the position of the SLOPE switch. Purpose of the LEVEL control is to set the DC push-pull current through Q544 and Q554 to a point where the trigger signal current will cause tunnel diode D555 to switch states. Switching of the tunnel diode to its high state always occurs on the positive-going rising portion of the waveform at Q554 collector.

With the SLOPE switch set to + and the LEVEL control pushed inward as shown on the A Sweep Trigger schematic diagram, voltage range of the control at the grid of V534B is about $\pm 2 \mathrm{~V}$ when measured using a DC-coupled oscilloscope having a 10 -megohm input loading. When the control is pulled outward to the $\times 10$ RANGE INCREASE position, R511 is bypassed and the voltage range is about $\pm 20 \mathrm{~V}$. If the LEVEL control knob is properly positioned on the shaft, the knob should point to 0 when voltage at the grid of V534B is zero.

## Trigger Slope

The + and - positions of the SLOPE switch SW520 provide a means of inverting or not inverting the single-ended signal which is applied to the anode of D555. This is accomplished by switching the triggering signal at the grids of V534.

In the + position of the SLOPE switch, a positive-going incoming single-ended triggering signal applied to the junction of R526 and R528 will be applied to the grid of V534A. The signal will have the same polarity when applied to D555.

If the SLOPE switch is set to -, the signal will be applied to the grid of V534B and will be inverted when applied to D555 so D555 can switch on the falling (positive-going) portion of the displayed waveform. This is done so the positivegoing trigger at the output of the A Sweep Trigger can be made to occur during either a positive-going or a negativegoing portion of the triggering signal.

## Trigger Comparator V534

The Trigger Comparator circuit consists of a cathodecoupled vacuum tube pair, V534A and V534B. In operation, the circuit is a push-pull amplifier which drives a Trigger Output Amplifier Q544 and Q554.

The A TRIGGER LEVEL CENTERING control R545 in the plate circuit of V534 is adjusted so the base voltages on Q544 and Q554 are equal when V534 grid voltages are zero. Coil L547 is energized when the COUPLING switch SW510 is set to the AC HF REJ position. The coil closes SW547 contacts to connect C547 across V534 output and limit the high-frequency push-pull response of the circuit.

## Trigger Outpuł Amplifier, Q544 and Q554

Push-pull signals from V534 are applied to the Trigger Output Amplifier stage, Q544 and Q554. The push-pull input signals are converted to single-ended output signals at the collector of Q554 for application to tunnel diode D555.

## Tunnel Diode Trigger Regenerator D555

For discussion purposes, assume these conditions: The SLOPE switch is set to + , the LEVEL control is set in the + region, and the current through D555 is such that the tunnel diode is in its low state (see Fig. 3-11 for the characteristic


Fig. 3-11. Tunnel diode characteristics.
curve of a tunnel diode). When a positive-going trigger is applied to the grid of V534A, the trigger is negative-going at the base of Q554. Collector current of Q554 increases and this increased current flows through D555, causing D555 to switch to its high state. The sudden switching of D555 to its high state causes the tunnel diode to produce a positivegoing trigger having a uniform amplitude and a fast rise for application to the Sweep Gate Tunnel Diode D565 and to the A Auto Multivibrator stage, Q605 and Q615.

When the positive-going trigger at the base of Q554 returns to the original starting level, decreased current through Q554 resets the tunnel diode to its low state. R553 and the A TRIGGER SENSITIVITY control R556 sets the load and bias on D555 so the tunnel diode has a small hysteresis but not small enough to switch states on internal noise or to selfoscillate.

## B SWEEP TRIGGER

The B Sweep Trigger is similar to the A Sweep Trigger in every respect except the B Sweep Trigger drives the B Sweep Generator.

## A SWEEP GENERATOR and A SWEEP TIMING SWITCH



## General

The A Sweep Generator produces seven simultaneous output signals controlled by four input signals (see Fig. 3-12). There are two more input signals but these control only a portion of the A Sweep Generator circuit when certain Upper Beam DISPLAY switch positions are used. The input signals are:

1. For triggered-sweep operation, a positive-going trigger from D555 in the A Sweep Trigger.
2. For autostability operation, a DC threshold level determined by the A Auto Multivibrator circuit, Q605 and Q615.
3. For single sweep operation, a positive-going reset pulse generated by operating the RESET button.
4. For RIGHT PLUG-IN A operation, a positive-going inhibit gate from the Alternate Trace Logic and Blanking Circuit.
5. In RIGHT PLUG-IN A, DLY'D BY A operation, a positivegoing trace brightening pulse (restored to normal intensity during B sweep) from R799 in the B Sweep Generator circuit. This pulse controls the Upper Beam unblanking circuitry only. In addition, there is a positive-going inhibit gate coming from the Alternate Trace Logic and Blanking circuit.
6. In RIGHT PLUG-IN operation, a negative-going B gate during B sweep from Q763 and Q773 in the B Sweep Generator circuit. This gate pulse controls the Upper Beam unblanking circuitry only.

The output signals are:

1. Positive-going unblanking pulse applied to the CRT Circuit Upper Beam control grid.
2. Positive-going gate signal to the A GATE connector on the front panel.
3. Negative-going gate signal during the A Sweep to D1024 in the Alternate Trace Logic and Blanking circuit.
4. Positive-going $A$ sawtooth signal to the Upper Beam Horizontal Amplifier via the Upper Beam DISPLAY switch.
5. Positive-going A sawtooth signal to the Delay Pickoff circuit.
6. Positive-going A sawtooth signal to pin 6 of Ill. Used for driving a left plug-in spectrum analyzer capable of utilizing this signal.
7. Positive-going $A$ sawtooth signal to the front-panel $A$ SAWTOOTH connector.
8. Positive-going $A$ sawtooth signal to the Lower Beam Horizontal Amplifier, via the Lower Beam DISPLAY switch.

To simplify the operational description of each stage shown in Fig. 3-12, the description initially assumes that the condiions are as follows:

1. The front-panel controls are set as follows:

A Triggering

Upper Beam DISPLAY

## A MODE

 ready to be triggered by a triggering pulse from D555.3. The description for each stage begins with the stage in its quiescent state; i. e., the A Sweep Generator circuit is ready to be triggered. Then, the discussion proceeds to describe the operation as D555 triggers the sweep. Refer to Figs. 3-12, 3-13, 3-14 and the appropriate schematic iagrams when following the description. Other modes of operation, but only those of most importance where the input signal directly affects the stage, are briefly described last. All signal amplitudes and voltages stated in the text are approximate.

## A Gate Tunnel Diode D565

During quiescence, tunnel diode D565 is in its low state. Bias current is set by R561, D562 and R563 connected to the +100 V supply.

To switch D565 to its high state, a positive-going trigger from D555 is required. The trigger is coupled through C560 to L560 and D561. C560 and L560 form a differentiating network to provide a very narrow trigger pulse to D565. Diode D560 clamps the junction of L560 and R560 at about +0.5 V .

Upon application of the trigger pulse, D565 switches to its high state and the A Sweep Generator circuit produces a sawtooth. At a point determined by the A SAWTOOTH AMPL control R678, the Holdoff Multi changes state, V625A returns D565 to its low state and holds D565 in the low state until holdoff capacitor C675 discharges to a point where V625A will allow D565 to accept another trigger. The output signal from D565 is a $350-\mathrm{mV}$ positive-going gate applied to the base of Q564. Duration of the gate is equal to the ramp time of the sawtooth.


Fig. 3-12. Block diagram of the A Sweep Generator circuit.


Fig. 3-13. Illustration showing time relationship of waveforms in the $A$ Sweep Generator circuit starting at the quiescent voltage levels.

When the A Triggering MODE switch is set to AUTO STABILITY, and triggers from D555 are absent, the A Auto Multivibrator stage (Q605, Q615) sets the DC threshold level of D565 so the sweep cycle can be repeated to obtain a free-running sweep.

## A Gate Amplifier Q564

In its quiescent state, Q564 is cut off. When a trigger is applied to D565 and the tunnel diode switches to its high state, D565 drives Q564 into saturation. Q564 remains
saturated until D565 returns to the low state. The voltage waveform at Q564 collector is a 10.5 V negative-going gate applied to the bases of Q563 and Q573. Duration of the gate is equal to the ramp time of the sawtooth.

## A Gate Emitter Follower and Amplifier Q563

The 10.5 V negative-going gate from Q564 collector is applied to the bases of Q563 and Q573. The following discussion describes the A Gate Emitter Follower Q563 stage. In its quiescent state, Q563 is cut off. When the gate is


Fig. 3-14. Time-related waveforms showing how the CONTRAST control varies the non-intensified DC level of the A Sweep unblanking pulse.
applied, Q563 is driven into saturation until the gate ends. The emitter waveform from this stage has the same polarity as the input and the amplitude is about 9 volts. Purpose of the stage is to provide a fast-rise negative-going low-impedance drive to the following circuits (see Fig. 3-12).

1. When the Upper Beam DISPLAY switch is set to LEFT PLUG-IN A or RIGHT PLUG-IN A, the 9-V negative-going gate is applied to the Upper Beam Unblanking Amplifier V574A. The gate is then amplified and inverted for use in unblanking the Upper Beam.
2. The $9-V$ negative-going gate is applied to D1024 in the Alternate Trace Logic and Blanking circuit to provide drive to the logic circuit and then (during gate turn off) to produce an alternate-trace sync pulse that can be used by the left plug-in multi-trace unit.
3. The 9-V negative-going gate is applied to Disconnect Diode D640 to turn off the diode so a sweep sawtooth can be generated.
4. The waveform at the collector of Q563 is a positivegoing 14-V + gate source for driving the grid circuit of V583A so this waveform is available at the A GATE connector every time the sweep runs. Diode D570 clamps the collector of Q563 so the gate cannot go higher than the diode bias above ground for the duration of the gate.

## A Gate Emitter Follower Q573

Transistor Q573 with associated components is connected in a complementary circuit with Q563. The purpose of Q573
is to provide a fast-rise positive-going gate at the end of the sweep through its emitter follower action.

In its quiescent state, Q573 is conducting. When the gate is applied to its base, Q573 is driven into cutoff and remains in this state until the gate terminates. When the gate ends, Q573 is quickly turned on and this completes the cycle. The fast turn-on of Q573 is necessary for driving V1043A to obtain the proper alternate-trace sync pulse amplitude.

## Disconnect Diode D640

Disconnect Diode, D640, is forward-biased and quiescently conducting current through Q573, R640 and R660. When tunnel diode D565 is triggered and switches to its high state, the 9-V negative-going gate from transistors Q563 and Q573 is applied to D640. The gate reverse biases D640 and the current through D640 is interrupted, and the Miller circuit generates a sawtooth. When the sweep terminates and the negative-going gate at Q563 emitter returns to its quiescent level, D640 is forward biased again, thus completing the cycle. Diode D641 is a protection diode for D640 and is normally not conducting.

## Miller Sweep Generator V661 and A Sweep Timing Switch

In its quiescent state V661 is conducting heavily. When the negative-going gate reverse biases Disconnect Diode D640, timing capacitor C660 begins to charge through the timing resistor R660 and the VARIABLE control R662 (see A

Sweep Timing Switch diagram; more details about this diagram are given later).

As C660 begins to charge, a negative-going change in voltage occurs at the grid of V661, is amplified by a factor of about 200 and appears as a positive-going voltage at the plate of the tube. This amplified change is coupled back through V673A, D675 and D681 to the output side of timing capacitor C660. The coupled-back change tends to oppose any change at the grid side of the timing capacitor. This feedback action continues throughout the sawtooth rise, limiting the total negative excursion at the grid of V661 to less than 1 V .

With the grid of V661 held at nearly constant voltage level, the voltage across the timing resistor R660 remains essentially unchanged. Current through the resistor is therefore constant and the timing capacitor charges linearly. The resulting voltage change at the cathode of V673A, and hence, the output end of C660, is a linear positive-going sawtooth (about 105 V in amplitude at $1 \mathrm{~ms} / \mathrm{cm}$ ) that is capable of driving the following circuits:

1. Via LEFT PLUG-IN A and RIGHT PLUG-IN A positions of the Upper Beam DISPLAY switch to the base of Q1135 in the Upper Beam Horizontal Amplifier.
2. Via RIGHT PLUG-IN A position of the Lower Beam DISPLAY switch to the base of Q1235 in the Lower Beam Horizontal Amplifier.
3. To the grid of V904A in the Delay Pickoff circuit.
4. To pin 6 of the left plug-in jack Jll in the Plug-In Jack Details circuit, for use by Spectrum Analyzer plug-in units that are wired to accept this signal.
5. A sample sawtooth the grid of V625 in the Holdoff Multivibrator circuit (A Sweep Generator circuit).
6. A sawtooth to grid of V673B in the Second A Sawtooth C. F. (A Sweep Generator circuit).

The sweep rate (the rate at which the spot moves across the face of the CRT) is determined by the rate at which the timing capacitor and timing resistor permit the Miller Sweep Generator to run up. By means of the A TIME/CM switch SW660 (see A Sweep Timing Switch diagram), both the size of the capacitor being charged and the charging current can be selected to cover a wide range of sawtooth slopes (sweep rates). Note that SW660 is connected so that switching 8 capacitors and 6 resistors provides 24 different sweep rates, from $5 \mathrm{~s} / \mathrm{cm}$ to $0.1 \mu \mathrm{~s} / \mathrm{cm}$ without magnification. The A TIME/CM switch also selects the proper holdoff capacitor and discharge resistor for the sweep rate in use.

Adjustable capacitors $\mathrm{C} 660 \mathrm{G}, \mathrm{C} 660 \mathrm{H}$, and C 660 J are adjusted to obtain correct sweep timing at the fastest sweep rates.

Continuously variable uncalibrated sweep rates are provided by R662 and SW662 (mounted on and actuated by R662). When SW662 is switched to the uncalibrated position, the switch removes the short from around R662 and turns on the UNCAL neon B663. By turning VARIABLE control R662, the charging time of the timing capacitor selected by the $A$ TIME/CM switch may be increased by at least 2.5 times the calibrated rate, thus providing continuously variable sweep rates.

## First A Sawtooth Cathode Follower V673A

The First A Sawtooth Cathode Follower V673A stage isolates the output shunt capacitances and load from the circuitry associated with the Miller tube V661. The 105 volt positive-going sawtooth waveform at the grid of V673A produces the same waveform at the cathode for distribution to all points as described earlier.

Neon B670 is a protection device that prevents V673A grid from becoming too positive with respect to the cathode during warmup time when the oscilloscope is first turned on. The neon does not glow when the oscilloscope has warmed up.

Bootstrap capacitor C668 improves the operation of the Miller Sweep Generator circuit in developing rapidly rising runup waveforms. To make the output sawtooth signal start at about zero volts, zener diode D675 is used to overcome the difference between V673A cathode voltage level and the desired level at the junction of D681 and R681.

To allow the A Sweep Generator circuit to reset quickly when the sawtooth has terminated, diode D681 is backbiased during the sweep retrace time to disconnect the diodecathode circuitry from V673A cathode circuit. Diode D681 is normally conducting during the sawtooth runup and remaining portion of the holdoff period. C681 and R681 form a compensation network. C681 is adjusted to obtain best sweep linearity at the start of the sweep sawtooth when calibrating the fastest sweep rates.

## Clamp Emitter Follower Q643 and Clamp Diode D677

In their quiescent state, Q643 and D677 are conducting to provide a DC feedback loop. This assures stable quiescent conditions. When tunnel diode D565 is triggered and the 9-V negative-going gate from the emitter of Q563 is applied to the emitter of Q643, transistor Q643 cuts off and diode D677 is reverse biased. These are the conditions while the sawtooth is generated.

## Second A Sawtooth Cathode Follower V673B

The sawtooth output from the cathode circuit of V673A is applied to the grid of V673B in the Second A Sawtooth Cathode Follower stage. The purpose of this stage is to make the sawtooth available at the front-panel A SAWTOOTH connector while isolating the external loading from the internal sawtooth voltage.

## Holdoff Multivibrator V625

The Holdoff Multivibrator V625 circuit prevents D565 from being triggered during the retrace interval. That is, the holdoff circuit allows a finite time for the Miller Sweep Generator circuit to reach a steady-state condition after the completion of a sweep.

Due to the many modes of operation of this stage, each mode is described separately as follows:

1. Quiescent State-Conditions: (Assume the A MODE switch is set to NORM). V625A is conducting and V625B is
cut off. V625A cathode resets at about +12 V . Diodes D614, D616, D624, D635 and D678 are reverse-biased; D627 and D629 are conducting.
2. D565 Triggered-When tunnel diode D565 is triggered, the Miller Sweep Generator produces the positive-going sawtooth as explained earlier. At a certain point on the sawtooth ramp (about zero volts on the sample appearing at the wiper arm of the A SAWTOOTH AMPL control R678), diode D678 conducts and holdoff capacitor C675 charges. The sawtooth continues to rise and is coupled through D678 to the grid circuit of V625B.
When the rising sawtooth voltage reaches about +14 V at D678 cathode (see Fig. 3-13), V625B conducts, V625A cuts off and V625A cathode drops from +12 V to about -1 V. D616 conducts and D565 is driven to its low state but cannot be triggered while V625A is cut off. The sweep terminates, the retrace interval begins, D678 reverse-biases, and C675 begins to discharge resistors R637 and R639 for the SEC and MSEC positions of the A TIME/CM switch.

During the sweep retrace and holdoff time the holdoff capacitor continues discharging without interruption and holds V625B in conduction while the Miller Sweep Generator circuit resets and reaches its steady-state condition. As long as V625B is conducting, V625A is cut off and D565 cannot be triggered.

Finally, C675 becomes discharged to a point where V625B cuts off and V625A conducts. V625A cathode rises from - 1 V to +12 V , D616 reverse-biases and this completes the holdoff circuit cycle. D565 is ready to be triggered once again.
Holdoff time is determined by the size of the holdoff capacitor and resistors R637, R639. The A TIME/CM switch SW660 is used to change the time constant of the holdoff circuit simultaneously with the change of timing capacitors and resistors. In the $\mu \mathrm{SEC}$ positions of the A TIME/CM switch, R637 and R639 are shunted by R675 to speed up C675 discharge.

The A SAWTOOTH AMPL control R678 determines sweep length by controlling the voltage level at which the saw-tooth-ramp sample starts, since the end of the sample is always fixed by the point at which $V 625 B$ conducts.
3. Single-Sweep Operation-Assume these beginning conditions: A MODE switch SW625 is set to SINGLE SWEEP, no triggers are applied to D565, and the RESET button is not pressed. Diode D635 is conducting and holding V625B in conduction and V625A is cut off. Under these conditions, the sweep circuit cannot be triggered. However, if the RESET button is pressed, a positive-going pulse will be applied through D624 to the cathode of V625B sufficient to cut off V625B so the multivibrator switches states; i. e., V625B cuts off and V625A conducts. Now the sweep is ready to start when D565 is triggered.
4. Right Plug-In Multi-Trace Unit Set For AlternateMode of Operation-Conditions: A MODE and B MODE switches are set to NORM, Upper Beam DISPLAY switch SWI 85 is set to RIGHT PLUG-IN A, the right plug-in is set for multi-trace alternate mode of operation (see Fig. 3-5), and the B sweep is set for a slower sweep rate than the A sweep. With no triggers applied to D565, V625A is conducting and V625B is cut off.

When triggers are applied to D565 and D765 (in the B Sweep Generator circuit), both sweeps start. As the A sweep sawtooth reaches the point where V625B conducts and V625A cuts off, D565 resets to its low state and the A sweep terminates. At this point, a 10 volt positive-going inhibit gate (from D1008 and D1010 in the Alternate Trace Logic circuit), is applied to the grid of V625B. This inhibit gate, equal in duration to the time difference between the end of the $A$ sweep and the end of the slower-running $B$ sweep, holds V625B in conduction, preventing D565 from being triggered.
Then, as the B sweep ends, the inhibit pulse ends simultaneously with the B gate sweep and allows holdoff capacitor C675 to discharge to the point where V625B cuts off and V625A conducts, D565 is now ready to be triggered once again.

The purpose of the inhibit gate is to lock out the A sweep until the $B$ sweep terminates. Then, the combined action of $A$ sweep in its locked-out condition and the B sweep resetting causes the Alternate Trace Logic circuit to produce one alternate sync pulse for switching the plug-in to the next channel. Then, the cycle is repeated as both beams display the signal in the second channel. To summarize the action, the Alternate Trace Logic circuit allows the plug-in to switch channels only when the slower sweep has completed its runup.

If the $B$ sweep is set faster than the $A$ sweep, the $B$ sweep cycle is repeated until the A sweep ends, then the inhibit gate occurring at this time and lasting until the B sweep ends keeps the A sweep locked out until the B sweep resets. The Alternate Trace Logic circuit does not produce any alternate sync pulses while the $A$ sweep is running up but, as explained eariler, the combined condition of locked-out A sweep and the $B$ sweep going through its resetting action causes only one alternate sync pulse to be produced.
5. B Sweep Delayed-By-A Mode of Operation-Conditions: A MODE switch is set to NORM, B MODE switch is set to DLY'D BY A and the Upper Beam DISPLAY switch is set to RIGHT PLUG-IN A (similar to Fig. 3-6). Assume that the B sweep is set to last longer than the A sweep, and both sweeps have ended.

With no triggers applied to D565, V625A is conducting and V625B is cut off. When a trigger is applied to D565, the A sweep starts running up. At a certain point on the sawtooth ramp, (determined by the setting of the DELAY-TIME MULTIPLIER control) a delayed trigger from the Delay Pickoff circuit is applied to the B Sweep Generator circuit.

Assume that the $B$ sweep starts automatically upon application of the delayed trigger. The B Sweep runs up and simultaneously generates a negative-going B gate. The B Gate Inverter circuit Q1004 (see Alternate Trace Logic \& Blanking diagram) inverts the gate so it is positive-going and about 10 V in amplitude. This $+10-\mathrm{V}$ gate is now referred to as an inhibit gate. This gate is applied to the grid circuit of V625B. When the A sweep ends and V625B goes into conduction, V625A cuts off and resets D565 to its low state.

The inhibit gate holds V625B in conduction until the A sweep ends and Holdoff Capacitor C675 discharges to a point that causes V625B to cut off and V625A to conduct. Thus, the inhibit gate holds the A sweep locked out until the B sweep ends to prevent the intensified portion of the Upper Beam display from extending into the start of the A sweep.
6. B Single-Sweep Mode of Operation-This mode is similar to B Sweep Delayed-By-A mode, except that the B MODE switch is set to SINGLE SWEEP. The DELAY-TIME MULTIPLIER control and delayed trigger are not used in this Mode. With the Upper Beam DISPLAY switch set to RIGHT PLUGIN A, the Holdoff Multivibrator operates as in the previously described mode; that is, the inhibit gate locks out the A sweep until the B sweep ends.

## Reset Lamp Driver Q619 and Reset Lamp B619

The Reset Lamp Driver Q619 circuit with B619 is mainly used for single-sweep operation, so this mode is described first.

Assume these conditions: The A MODE switch SW625 is set to SINGLE SWEEP, no triggers are applied to D565 and the RESET button is not pressed. Under these conditions, D635 holds V625B in conduction when the sweep ends and V625A is cut off. The cathode of V625A will be at -1 V. This voltage, applied to the base circuit of Q619, holds Q619 cut off and B619 is turned off.

When the RESET button is pressed, C622 charges quickly toward +10 V , resulting in a positive-going pulse which is applied through D624 to the cathode of V625B. The pulse is sufficient to turn off V625B and V625A conducts. The cathode of V625A rises from -1 V to +12 V , Q619 conducts, B619 turns on, and D565 is ready to accept a trigger.

When D565 is triggered, the negative-going gate at the emitter of Q563 turns off Q619 and B619; also, as described earlier, disconnect diode D640 is reverse-biased and the sawtooth is generated. When the sawtooth drives V625E into conduction, V625A cuts off and the sweep is terminated. This ends the cycle of operation until the RESET button is pressed again.
If the A MODE switch is set to the NORM position, the RESET button is disconnected and D635 anode is connected to ground. Thus, toward the end of the sweep, holdoff capacitor C675 is able to discharge to a point where V625B cuts off, V625A conducts and the sweep ends. Transistor Q619 conducts, B619 turns on and D565 is ready to be triggered. When D565 is triggered, Q619 and B619 turn off and the cycle of operation is repeated. It is normal for 8619 to stay on when the sweep duty cycle is low (sweep holdoff time is relatively long).

## A Auto Multivibrator, Q605 and Q615

Transistors Q605 and Q615 with associated circuit components form a triggered monostable multivibrator that has two modes of operation when the A Triggering MODE switch SW505 is set to AUTO STABILITY. The two modes are: (1) non-triggered, and (2) triggered. Mode 1 is described first because it is the normal state of the multivibrator.

Mode 1 (Non-triggered). Transistor Q605 is conducting and Q615 is cut off. C611 has charged to approximately 25 V , determined mostly by Zener diode D612. Diode D614 is conducting and its current adds to the current through D565. This extra current causes D565 to be held at a threshold level that enables the Holdoff Multivibrator to switch

D565 to its high state at the end of each sweep holdoff period. Thus, the A Sweep Generator will go into a free-running mode when trigger signals are absent.

Mode 2 (Triggered). Assume that all the conditions given for Mode 1 are present and $100-\mathrm{Hz}$ or faster triggers are applied to T555 from D555. (Ignore for the moment that these same triggers are also applied to D565.) Under these conditions, the multivibrator will be triggered and will run through its natural period. For the following discussion the period is the minimum time that it takes for the multivibrator to be triggered, switch states, and then return to its original triggerable state.

Differential triggers from the secondary of T555 are applied to the base of Q605. Only the negative-going portion of one of the triggers actually triggers the multivibrator, so this is the only portion discussed here. The negative-going trigger feeds through the base-emitter junction of Q605, drives Q615 into saturation and Q605 cuts off. The collector of Q605 rises exponentially as C604 charges through R604 and R605. Finally, a point is reached where the decreasing charge current lowers the base of Q615, causing this transistor to cut off and Q605 to conduct. This completes the first half-cycle.

With Q605 conducting and Q615 cut off, C604 goes through its recovery time and C611 starts charging through R610 and R611. C604 exponential discharge current raises the base of Q615 to a point that will enable one of the triggers, feeding through the base emitter junction of Q605, to drive Q615 into saturation and Q605 will cut off. As Q615 goes into saturation, C611 is quickly discharged through the low impedance of Q615. Thus, the natural period for the multivibrator is short enough to limit the charge time of C611 well below the threshold level so zener D612 never breaks down, D614 never conducts, and D565 returns to its low state. The A Sweep Generator will stop free running when if (sweep generator) completes its cycle. From this point on, as long as triggers are applied to D565 from D555, these same triggers will trigger the sweep.

As Q605 is turning on and Q615 is turning off, D604 conducts to limit the negative-going swing on the base of Q615 to about -0.6 V or less. The negative-going swing is developed by the drop in collector voltage as Q605 turns on and by C604 as it starts its recovery.

As Q615 is driven into saturation, D602 conducts to assure rapid turn on Qf Q615 and to clamp its emitter.

If the triggers from D555 are slowly decreased in repetition rate from 100 Hz toward 30 Hz , the period of the multivibrator will be longer and C611 will change further. As a result, C611 charge will approach the threshold level for D565.

If the time between triggers is reduced to longer than 50 ms (trigger repetition rate slower than 30 Hz ), Q615 will remain in its cut off condition for a time sufficient to allow C611 to charge to the level mainly determined by D612. When this point is reached, D614 conducts and D565 returns to the threshold level that enables the A Sweep Generator to free run.

When the A Triggering MODE switch is set to the TRIG position, the switch grounds the collector of Q615 and disables the automatic stability feature of the Type 556.

## Upper Beam Unblanking Amplifier V574A

When the Upper Beam DISPLAY switch SWI 85 is set to the LEFT PLUG-IN A or RIGHT PLUG-IN A positions and the B MODE switch SW825 is set to NORM or SINGLE SWEEP, an unblanking pulse is generated for use in driving the Upper Beam CRT control grid circuit so that the Upper Beam is unblanked during the A sweep time. The unblanking pulse is initiated when tunnel diode D565 switches to its high state and produces a 9-V negative-going gate at the Q563 emitter (see Fig. 3-14A).
The $9-\mathrm{V}$ negative-going gate at the emitter of Q563 is connected through the Upper Beam DISPLAY switch to the control grid circuit of V574A. The gate rapidly drives V574A into cutoff and the plate rises from +49 V to about +129 V (see Fig. 3-14B). Thus, a positive-going pulse about 80 V in amplitude is produced at the plate and applied to the grid of V583B. When the sweep ends, D565 is driven into its low state, V574A resumes conduction, and the $80-\mathrm{V}$ unblanking pulse is terminated.
Diode D574 is forward biased during the time V574A is in a quiescent state. The feedback loop established with D574 conducting provides a stable quiescent voltage level at the cathode of V573B. The negative-going gate signal that is applied to the V574A grid to generate the unblanking signal, also reverse biases D574 and interrupts the fedback loop.
When a negative-going gate signal is applied to V574's grid, its plate voltage will rise until D799 is forward biased. Diode D799 is located in the B sweep generator circuit. When the B MODE switch is set to either NORM or SINGLE SWEEP, the voltage at the cathode of D799 is established at approximately +127 VDC by D796 and its associated circuitry. The V574A plate voltage rise is clamped at approximately +129 volts. When the B MODE switch is set to DLY'D BY A, the reference voltage at the cathode of D799 may be varied by the conduction of Q794.
When the B MODE switch is set to DLYD BY A, +100 VDC is applied to the Upper Beam CONTRAST contiol, R793 and to the Lower Beam CONTRAST control, R853. With the +100 volts applied to R793, the bias of Q794 may be adjusted to reduce the amplitude of the Upper Beam unblanking signal (diminishing the trace brightness levell, except during the time when a B gate signal from the plate of V783A is applied to the base of Q794. The B gate signal overrides the effect of the $D C$ voltage from R793, and the Upper Beam unblanking signal is returned to its normal amplitude. Returning the Upper Beam intensity to normal during B sweep time (Upper Beam DISPLAY set to A) permits viewing the amount of delay between the start of the $A$ sweep and the $B$ sweep.
With a B delayed by $A$ application where the $A$ sweep is displayed on the Lower Beam, R853 may be used to adjust the bias of Q854 to provide a contrast in the Lower Beam intensity between the $A$ and $B$ sweep times.

Since the instruments with serial numbers 100-1999 do not have the capability of displaying the $A$ sweep on the Lower Beam, only the Upper Beam CONTRAST control is incorporated. The contrast circuitry for these instruments is described as follows:

Set the B MODE switch to the DLY'D BY A position and assume the following conditions: Upper Beam DISPLAY switch
is set to RIGHT PLUG-IN A, Lower Beam DISPLAY switch is set to RIGHT PLUG-IN B, the B sweep is operating faster than the A sweep, and the DELAY-TIME MULTIPLIER dial is set for a reading of about 3.00 . Using these conditions to describe the unblanking pulse shown in Fig. 3-14C, the A sweep unblanking pulse will be produced in the usual manner, except V574A plate DC level at cutoff is controlled two ways:

1. The B MODE switch SW825 connects one end of the CONTRAST control R796 to +100 V , D796 is forward biased and D799 is reverse biased when the B sweep is not running. Thus, the CONTRAST control, rather than D799, determines the plate DC level during V574A cutoff when the B sweep is not running.
2. However, when the B sweep runs, its unblanking pulse is applied to the base circuit of Q793. The unblanking pulse causes D799 to conduct, D796 reverse biases, and V574A plate $D C$ level is clamped at +129 V for the duration of the B unblanking pulse.

Thus, the CONTRAST control varies the non-intensified portions of the $A$ unblanking pulse and the B unblanking pulse is used to restore the intensified portion of the A unblanking pulse to its normal (original) level. That is, if the Upper Beam INTENSITY control setting was set for suitable trace brightness during normal A sweep operation, the intensified portion reaches this same level during A Intensified by B operation.
When the Upper Beam DISPLAY switch SW185 is set to the LEFT PLUG-IN B or RIGHT PLUG-IN B positions and the B MODE switch SW825 is set to any position, the B sweep unblanking pulse is applied via the Upper Beam DISPLAY switch to the control grid circuit of V574A. The pulse is used to unblank the CRT Upper Beam during the B sweep in the same manner described for normal A sweep operation.
When the Upper Beam DISPLAY switch is set to either of the EXT positions, V574A grid is grounded through R574 and R575 to unblank the Upper Beam for external horizontal input operation.

## A Sweep Unblanking Cathode Follower V583B

The $80-\mathrm{V}$ positive-going unblanking pulse at the plate of V574A is applied to the grid of V583B in the A Sweep Unblanking C. F. stage. The output pulse obtained at V583B cathode is the same as the input but at slightly lower amplitude (about 76 V ). This 76 volt pulse is coupled from V583B cathode through a network (in the CRT Circuit) to the CRT Upper Beam control grid. The unblanking pulse turns on (unblanks) the beam during the sweep time.
Capacitor C583 connected from the cathode of V583B to the plate circuit of V574A is a bootstrap capacitor. At the instant the unblanking pulse goes positive, the bootstrap capacitor helps to drive the plate of V574A positive. This action assures rapid turn-on of the beam at the start of the sweep.
Diode D581, connected from the cathode of V583B to the plate circuit of V 574 A , is a bootstrap diode. D581 turns on the instant the unblanking pulse goes negative to help drive the cathode of V583B downward. This action assures rapid turnoff of the beam at the end of the sweep.

## Circuit Description-Type 556

## A + Gate Cathode Follower V583A

The 14 volt positive-going pulse at the collector of Q563 is used by the A +Gate Cathode Follower V583A to provide a + gate waveform to the A GATE front-panel connector on the Type 556.

In its quiescent state, the control grid of V583A rests at about -4.4 volts. When the sweep runs, the 14 V pulse at Q563 collector is applied to divider resistor R586 and R587. Amplitude of the pulse at the junction of R586 and R587 is about 13 volts. The pulse drives the grid from -4.4 V to about +8.6 V . The output waveform at the cathode rises from ground to about 11 V for application to the front panel A GATE connector.

## B SWEEP GENERATOR and B SWEEP TIMING SWITCH



The B Sweep Generator and B Sweep Timing Switch circuit operation is the same as the corresponding circuits used in the A sweep except as follows:

1. There is no inhibit gate applied to the Holdoff Multivibrator circuit V825, but similar action takes place in this circuit when the B MODE switch SW825 is set to the DLY'D BY A position. In this position of the switch +10 V is applied to the grid circuit of V825B. This holds the V825B section of the multivibrator in conduction after the $B$ sweep ends so the next B sweep cannot be generated until a delayed trigger pulse switches the multivibrator.

The delayed trigger is a 10 V short-duration positive-going pulse obtained from Q933 in the Delay Pickoff circuit. The pulse is generated at a predetermined time during each $A$ sweep. When the pulse is applied via the B MODE switch to the junction of C823 and R822, and through D824 to the cathode of V825B, the pulse drives V825B into cutoff and causes the multivibrator to switch states. V825B is now cut off, V825A is conducting, and the B sweep is ready to be triggered in either of two ways.
(a) If the B Triggering MODE switch SW705 is set to the AUTO STABILITY position and there is no trigger from the B Sweep Trigger circuit, the B Auto Multivibrator circuit (Q805 and Q815) sets D765 threshold level so the B sweep starts immediately.
(b) If the B Triggering MODE switch is set to the TRIG position, a trigger from the B Sweep Trigger circuit applied to D765 will trigger the sweep. The B sweep will run once, lock out, and will not reset until the next delayed trigger arrives.
2. The B SAWTOOTH SLOPE adjustment R861 (see B Sweep Timing Switch diagram) permits adjusting the B sawtooth slope to match the A sawtooth slope.

Instruments SN 100-1999 have these additional differences in their $A$ and $B$ circuits.
3. Diode D778 with emitter follower Q799 provides the clamping action for V774A plate when V774A is driven into cutoff by the B gate. Thus, the plate voltage level during cutoff is about +128 V and this is essentially the same level as described earlier when D578 clamped the plate of V574A in the A Sweep Generator circuit.
4. The B Sweep Unblanking Cathode Follower V783B applies the trace brightening pulse through Q793 to V574A plate circuit located in the A Sweep Generator circuit. For further information about the operation of Q793 with associated circuitry containing D799, D796 and the CONTRAST control R796, refer to the Upper Beam Unblanking Amplifier V574A description.

## DELAY PICKOFF

Refer to Figs. 3-6 and 3-15, and the Delay Pickoff schematic diagram during the following discussion.

The Delay Pickoff circuit generates a 10 volt short-duration positive-going pulse that is delayed from the start of the $A$ sweep by an amount determined by the settings of the $A$ TIME/CM (OR DELAY TIME) switch and the DELAY-TIME MULTIPLIER dial. The comparator in the delay pickoff circuit continuously monitors the sawtooth ramp voltage from the A Sweep Generator circuit and compares the ramp voltage with a DC voltage level established by the DELAY-TIME MULTIPLIER dial.
When the ramp voltage biases V904A into conduction, the comparator switches tunnel diode D905 to its high state. The tunnel diode generates a trigger pulse that is delayed from the start of the A sweep by the time it takes the ramp voltage to rise to a value approximately equal to the voltage established by the DELAY-TIME MULTIPLIER dial setting.

The trigger pulse from the tunnel diode is applied via T905 to a monostable Delayed Trigger Multivibrator so the trigger is regenerated into a fast-rise, high-amplitude, short-duration delayed trigger. The delayed trigger is applied internally via the B MODE switch to the B Holdoff Multivibrator V825 for use in the delayed B sweep mode of operation. The trigger is also applied to the DLY'D TRIG front-panel connector where it is always available.

Assume the Type 556 circuits are set for these conditions:

1. The $B$ sweep is set to run faster than the $A$ sweep.
2. The $B$ MODE switch is set to DLY'D BY A.
3. The A Sweep Generator has reset and is ready to be triggered.
4. The B Sweep Miller circuit has run up and reset, D765 is in its low state but cannot be triggered because the $B$ MODE switch is applying +10 V to the grid circuit of V825B. The +10 V holds this half of the multivibrator in conduction to lock out the B sweep. (Only a delayed trigger can make the multivibrator switch states so that the B sweep can be triggered as mentioned earlier.)
5. The DELAY-TIME MULTIPLIER control is set for a dial reading of 3.00 . This is equal to 30 volts on the 105 -volt $A$ sweep sawtooth ramp; or, 3 cm from the start of the sweep having a total length of 10.5 cm .

With the A Sweep ready to be triggered, the quiescent conditions for all stages in the Delay Pickoff circuit are as follows:
(a) V904B, Q908 and Q924 are conducting.
(b) V904A and Q933 are cut off.
(c) D905 is in its low-voltage state.


Fig. 3-15. Block diagram of Delay Pickoff circuit.

## Constant Current Transistor Q908, Delay Pickoff Comparator V904 and Delayed Trigger Pulse Generator D905

Transistor Q908 is a constant-current source for V904A and V904B to keep the current through the Comparator relatively constant despite the large voltage swings applied to the grids. The base of Q908 is connected to ground and its collector rests at +34 volts. Emitter resistor R908 sets the current through Q908 and the Comparator at about 5 mA .

When the A sweep starts, the sawtooth ramp voltage is applied to the grid of V904A and the voltage selected by the wiper arm of the DELAY-TIME MULTIPLIER control R915 is applied to the grid of V904B. Assume the ramp voltage is increasing at the rate of $10 \mathrm{~V} / \mathrm{ms}$. Then, 3 ms after the sweep starts, the voltage on the grid of V904A will rise 30 V and will be equal to the voltage at the grid of V 904 B as set by the DELAY-TIME MULTIPLIER control.

At the point where V904A and B grids are equal, V904A conducts and draws current through R907 and tunnel diode D905. An increase in current through R907 results in a decrease through R909 and this push-pull current action causes D905 to switch to its high state. When D905 switches, a sharp trigger is developed in the primary of T905 and inductively coupled into the secondary. The dots above T905 windings on the schematic diagram indicate the + polarity end of the windings. To obtain a negative-going trigger to drive the base of Q924, the trigger is taken off at the negative end of the secondary winding.

When the sweep ends, V904A cuts off and returns D905 to its low state.
The Type 556 is calibrated so the major dial markings of the DELAY-TIME MULTIPLIER control correspond to the graticule divisions by correct adjustment of the DELAY START R918 and DELAY STOP R914 controls.

To eliminate ground-loop currents due to the remote location of the Delay Pickoff circuit, the coaxial shield of the cable from the A Sweep Generator is used as an isolated (from chassis) ground. The shield is connected to ground in the Delay Pickoff circuit through R900. V904B grid is referenced to the same isolated ground through C911.

## Delay Trigger Multivibrator Q924 and Q933

The sharp negative-going trigger from T905 secondary is applied to the base of Q924. Transistor Q924 increases its conduction and Q933 turns on for the duration of the pulse. A fast positive-going trigger, rising from zero to +10 V , is produced at the emitter of Q933. This trigger is applied via the B MODE switch to the cathode circuit of V825B in the B Holdoff Multivibrator stage. The trigger causes V825B to cut off. V825A conducts to allow D765 to be triggered by the next trigger from the B Sweep Trigger or the B Auto Multivibrator (Q805 and Q815) to set D765 threshold level, depending on the settings of the B Triggering controls.
In addition, the trigger is applied to the DLY'D TRIG connector J935 on the front panel of the Type 556. This trigger is available for use in externally triggering other equipment.


Fig. 3-16. Block diagram of Alternate Trace Logic and Blanking circuits for Type 556 instruments with serial number 2000 and up.


Fig. 3-17. Block diagram of Alternate Trace Logic and Blanking circuit for Type 556 instruments with serial numbers 100 to 1999.

## ALTERNATE TRACE LOGIC \& BLANKING

## Introduction

For this discussion, refer to the Alternate Trace Logic \& Blanking schematic diagram (Fig. 3-16 and Fig. 3-17).

The Alternate Trace Logic \& Blanking circuit can be divided into five smaller circuits according to purpose as follows:

1. B Gate Inverter Q1004. Purpose of this stage is to invert the negative-going $B$ gate so the gate can serve as an inhibit gate for the A sweep during delayed-by-A and singlesweep operation. The inhibit gate locks out the A sweep until the B sweep ends to prevent the intensified portion of the Upper Beam display from folding over during right plugin A display mode of operation.
2. Alternate Trace Multivibrator, Q1015 and Q1025. This stage provides the logic to operate a right plug-in multitrace unit in the alternate mode during dual-beam operation. The sequence for proper logic is: Channel 1 (or A) signal is displayed simultaneously by both beams and then channel 2 (or B) signal is displayed by both beams, and so on.
3. Alternate Trace Sync Pulse Emitter Follower Q1033. This stage provides alternate trace sync pulse drive from D1014 and D1024 or Q1015 and Q1025 to V1063A.
4. Alternate Trace Sync Pulse Amplifiers, V1043A and V1063A. These stages amplify the alternate-trace sync pulses that are used to switch the channels in multi-trace plugin units operating in the alternate mode. Channel switching occurs during the sweep retrace time.
5. Chopped Blanking Amplifiers, V1043B and V1063B. These stages amplify the chopped-blanking pulses coming from the multi-trace units operating in the chopped mode. These pulses blank the beams during the plug-in switching time from one channel to the next. Thus, the switching portions of the chopped display are not visible at normal settings of the INTENSITY controls.

## B Gate Inverter Q1004

Operating conditions for this stage are: B MODE switch set to DLY'D BY A or SINGLE SWEEP, Upper Beam DISPLAY switch set to RIGHT PLUG-IN A, and the Lower Beam DISPLAY switch set to RIGHT PLUG-IN B. Assume the DELAYTIME MULTIPLIER control and the B TIME/CM switch are set so the delayed $B$ sweep terminates after the $A$ sweep ends. Using these conditions while the B sweep is running, the 9 volt negative-going B gate from the Gating Emitter Follower Q763 in the B Sweep Generator circuit is applied through R1001 to the base of Q1004.

At the collector of Q1004 the gate pulse is a positive-going pulse about 10 V in amplitude. The pulse, now referred to as the inhibit gate, is applied through D1008 to the grid circuit of V625B in the A Holdoff Multivibrator stage of the A Sweep Generator circuit. When the A sweep ends, the inhibit gate holds the A sweep locked out until the B sweep ends.

If the right plug-in is a multi-trace unit that is set for alternate mode of operation, diodes D1014 and D1024 provide
the logic for producing one alternate trace sync pulse per last sweep to end. To accomplish this logic, +100 V is applied to the collector circuits of Q1015 and Q1025 to disable the multivibrator stage and reverse bias D1021. As a result, diodes D1014 and D1024 are forward biased to permit the diodes to follow the DC levels of the incoming $A$ and $B$ gates.

When both sweeps are running concurrently, the gate from the last sweep that terminates is used to generate the alter-nate-trace sync pulse. For example, assume both sweeps are running; the DC level at the junction of D1014 and D1024 anodes will be at about the +1 V level and will remain at this level until the last sweep ends. As the last sweep ends, the positive-going portion of the $D C$ level as it moves from +1 V to +10 V is used to generate the alternate-trace sync pulse required for switching the channels in the right plug-in multi-trace unit. Thus, for multi-trace delayed-sweep operation from the right plug-in unit operating in the alternate mode, there is always one $A$ sweep and one $B$ sweep per one alternate-trace sync pulse.

## Alternate Trace Logic Multivibrator, Q1015 and Q1025

To establish the operating conditions for describing this circuit, assume the A and B MODE switches are set to NORM, the Upper Beam DISPLAY switch is set to RIGHT PLUG-IN A and the Lower Beam DISPLAY switch is set to RIGHT PLUG. IN B. Under these conditions, diodes D1024 and D1014 are reverse biased and not used; D1021 is always conducting.

Assume further that the sweeps have been triggered and are now running concurrently. With these conditions Q1025 is conducting and Q1015 is cut off. Diodes D1010, D1013 and D1028 are reverse biased; D1018 is conducting and clamps Q1015 collector at about -0.25 V. Diode D1023 is slightly forward biased and the collector of Q1025 is resting at about +10 V .

Assume the $A$ sweep is ending first. As the $A$ sweep ends and the A gate terminates (goes from +1 V to +10 V ), the positive-going rise of this pulse is coupled through C1023 and D1023 to the base of Q1025. Transistor Q1025 is driven into cutoff and its collector is clamped at about +0.25 V by D1028.

With Q1025 cut off, the multivibrator action turns on Q1015, D1018 reverse biases and D1010 conducts to apply an inhibit gate to the A Holdoff Multivibrator stage. Thus, the A sweep is locked out and only the termination of the B gate can remove the inhibit gate and allow the A sweep to reset to its triggerable level; i. e., V625B is cut off and V625A is conducting in the A Holdoff Multivibrator stage to enable D565 to be triggered.

Assume the B sweep is now ending after the A sweep has ended. At the instant the $B$ sweep ends, the $B$ gate terminates and goes from +1 V to +10 V . The terminating B gate becomes a positive-going pulse when coupled through Cl 013 and this pulse drives Q1015 into cutoff. D1018 clamps the collector of Q1015 at -0.25 V . The multivibrator action causes Q1025 to conduct and D1028 reverse biases. As Q1015 goes into cutoff, D1010 is reverse biased and the inhibit gate is terminated to allow the A sweep to reset to its triggerable level. This completes one cycle of the multivibrator operation.

The signal generated at Q1025 collector is applied to the base of Q1033. The only portion of the signal that is used to produce an alternate-trace sync pulse is the portion generated when Q1025 turns on the instant the B sweep ends. This coincides with the combined condition of the A sweep locked out and the B sweep resetting. While the B sweep resets, the A sweep is allowed to reset and the alternatetrace sync pulse switches the right plug-in to the next channel. Thus, comparing this mode of operation to the operation of the B Gate Inverter stage previously described, the logic of the multivibrator circuit operation is such that the B sweep can run several times while there is only one A sweep and there will be only one alternate-trace sync pulse as shown in Fig. 3-18.

For the duration of the A sweep Q1025 is conducting and Q1015 is cut off. The positive-going portion of the B gate pulses, coupled through C1013 and D1013, will not basetrigger Q1015 because the transistor is already cut off. For the opposite situation, each time the $B$ gate starts, the nega-tive-going portion of the $B$ gate pulses fail to reach the base of Q1015 because D1013 will not pass these pulses. As a result, Q1015 remains in cutoff while Q1025 is conducting and no alternate-trace sync pulses are generated while the A sweep is running.

## Alternate Trace Sync Pulse Emitter Follower Q1033

This stage operates in conjunction with the B Gate Inverter and multivibrator stages to provide low-impedance sync pulse drive to V1063A.

## Right Alternate Trace Sync Amplifier V1063A

With the Upper Beam DISPLAY switch set to RIGHT PLUG. IN A and the Lower Beam DISPLAY switch set to RIGHT PLUG-IN B, the alternate-trace sync pulse is applied to the grid circuit of V1063A. Coupling capacitor C1061 with R1060 forms a differentiating network for shaping the sync pulse. Diode D1062 clamps the negative-going portion of the pulse so only the positive-going portion is used as the sync pulse.

Both the cathode and plate circuits are completed through the switch connections in the right multi-trace plug-in unit operating in the alternate mode. In general, V1063A conducts only when the positive-going portion of the differential pulse is applied to the grid and the plug-in is operating in the alternate mode. V1063A is inoperative when operating in other modes. When V1063A is conducting, the alternatetrace sync pulse is either an amplified negative-going pulse when taken from the plate via pin 16 of $\mathrm{Jl2}$, or is a small positive-going pulse when taken from the cathode via pin 8 of J 12 , if the tube is connected to operate as a cathode follower.

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## Left Alternate Trace Sync Pulse Amplifier V1043A

When the Upper Beam DISPLAY switch is set to LEFT PLUGIN EXT or LEFT PLUG-IN A position, the A gate from the A Gate Emitter Follower Q563 is applied via the DISPLAY switch and C1041 to the grid circuit of V1043A. The function of the Left Alternate Trace Sync Pulse Amplifier stage is to provide an alternate-trace sync pulse via pin 8 or 16 of Jll to the left plug-in multi-trace unit during the sweep retrace time when the plug-in is operating in the alternate mode.
Operation of this stage is similar to the Right Alternate Trace Sync Pulse Amplifier stage. The sync pulse from V1043A is used to switch the channels in the left plug-in unit during the sweep retrace.

## Lower Beam Chopped Blanking Amplifier V1063B

To avoid displaying the channel-switching portion of the vertical chopping signal when using a right plug-in multitrace unit in the chopped mode, the beam is blanked during switching time between channels by the signal generated in the multi-trace unit. The negative-going chopped blanking pulses are connected to the junction of C1071 and R1065 through pin 16 of J12 of the right vertical interconnecting plug. The pulses are coupled through C1071 to the grid of the Lower Beam Chopped Blanking Amplifier tube V1063B. The signal is amplified and the inverted pulses are applied through the LOWER BEAM CHOPPED BLANKING position of the CRT Cathode Selector switch SW 1345 (see CRT Circuit diagram) to the Lower Beam CRT cathode.
Note that the pulses applied to the junction of C1071 and R1065 are also applied through C1065 and a coaxial cable to the Upper Beam DISPLAY switch. When the switch is set to any of the RIGHT PLUG-IN positions, the negative-going chopped blanking pulses from the right plug-in unit are applied through the switch and coupled through Cl051 to the grid of the Upper Beam Chopped Blanking tube V1043B for the purpose of blanking the Upper Beam display during the chopped-mode switching time between channels.

## Upper Beam Chopped Blanking Amplifier V1043B

This amplifer serves the same purpose as the one for the Lower Beam; i. e., to provide chopped-mode blanking of the Upper Beam during chopped-mode switching between channels. When the Upper Beam DISPLAY switch is set to any of the RIGHT PLUG-IN positions, the chopped blanking pulses from the right plug-in are amplified by V1043B for application to the Upper Beam CRT cathode. The pulses to the CRT cathode are applied via the UPPER BEAM CHOPPED BLANKING position of the CRT Cathode Selector switch SW1395 (see CRT Circuit diagram).

When the Upper Beam DISPLAY switch is set to any of the LEFT PLUG-IN positions, the left plug-in chopped blanking pulses are used to blank the chopped-mode switching portion of the Upper Beam display. This occurs, of course, when the left plug-in is operating in the chopped mode. These pulses from the left plug-in are applied through pin 16 of 11 and


Fig. 3-18. Time-related waveforms showing how the A Sweep is locked out until the B Sweep ends. Note that only one alternate-trace sync pulse per slower sweep is generated for switching the channels in the right plug-in unit.
through C1051 to the grid of V1043B for amplification. The amplified and inverted pulses are applied through the UPPER BEAM CHOPPED BLANKING position of the CRT Cathode Selector SW1395 to the Upper Beam cathode of the CRT.

## UPPER BEAM HORIZONTAL AMPLIFIER

The DC-coupled Upper Beam Horizontal Amplifier circuit (see Fig. 3-19) consists of Operational Amplifier Q1135, Q1145, Paraphase Amplifier Q1154-Q1164, push-pull Output

Amplifier V1174-V1184, Capacitance Driver V1194, and Externat Horizontal Amplifier V1104.

The input signal for the Horizontal Amplifier is selected by the Upper Beam DISPLAY switch SW185. In the EXT positons the external signal, applied to the UPPER BEAM EXT HORIZ IN connector, is selected to drive the Upper Beam horizontal deflection plates. In the A positions of the switch the positive-going $A$ sweep sawtooth provides the horizontal deflection, in the $B$ positions the positive-going $B$ sweep sawtooth provides the horizontal deflection.


Fig. 3-19. Block diagram of the Upper Beam Horizontal Amplifier circuit.

## Input Amplifier Q1135

The input signal selected by the Upper Beam DISPLAY switch, along with the DC positioning current from the horizontal POSITION controls R1136A and R1136B, is connected to the base of Q1135 in the Input Amplifier stage. This stage works together with Input Emitter Follower stage Q1145 to form an operational amplifier whose gain can be adjusted by the $\times 10$ CAL control R1146 in the negative feedback loop. The Input Amplifier stage has a low input impedance and is current driven.

Horizontal positioning is provided by the POSITION controls, R1136A and R1136B. These controls are driven by the same shaft and they set the DC level of the input signal. Backlash coupling is used between the two sections of the POSITION control so both a coarse adjustment, R1136A, and a fine adjustment, R1136B, can be obtained by turning only one POSITION knob. Fine adjustment of the horizontal position is provided by R 1136 B operating in a $60^{\circ}$ arc provided by the backlash coupling arrangement.

Negative feedback from the emitter of Q1145 to the base of Q1135 keeps the output impedance of the two stages low. The $\times 10 \mathrm{CAL}$ adjustment provides a means of adjusting the amount of feedback, thereby controlling the gain when the DISPLAY MAG switch SW1120 is set to $\times 10$.

## Input Emitter Follower Q1145

The composite signal output (DC-positioning and signal current) from the collector of Q1135 is applied to a compensated divider network R1141, R1142 and C1141. The divider output is applied to the base of Q1145. Transistor Q1145 and associated components is an emittter follower, but the negative feedback to Q1135 makes the two transistors function as an operational amplifier. The output signal at the emitter of Q1145 is applied through D1151 to the base of Q1154. Diode D1151 is a protection diode. Resistor R1153 provides a bootstrap arrangement to restore the linearity of the sawtooth ramp. Zener D1144 sets the collector voltage at +25 V .

## Paraphase Amplifier, Q1154 and Q1164

Transistors Q1154 and Q1164 with associated circuitry form a paraphase amplifier that converts the single-ended signal from the emittter of Q1145 into a push-pull output. The signal from Q1154 to Q1164 is coupled through the common emitter circuit. Gain of the stage is set by placing the DISPLAY MAG switch SW1120 to the $\times 1$ position and adjusting the $\times 1$ CAL control R1167 for proper $1 \mathrm{mSEC} / \mathrm{CM}$ sweep timing.

When the DISPLAY MAG switch SW1120 is set to the $\times 10$ position, coil L1125 is energized to close its relay contacts (SW1125 on the Upper Beam Horizontal Amplifier diagram). These same contacts are closed when the Upper Beam DISPLAY switch SW1185 is set to either of the EXT positions. The contacts connect R1166 across the emitter resistors to decrease the emitter resistance of the stage and increase the display magnification by 10 . To provide a front-panel indication that the DISPLAY MAG switch is set to $\times 10$, SW1120 completes the circuit for B1120 so the incandescent lamp will turn on.

If switching the DISPLAY MAG switch between $\times 1$ and $\times 10$ causes a horizontal shift of the display, SWP/MAG REGIS control R1168 can be adjusted to prevent display shift.

Variable capacitor Cl 165 is adjusted for proper $0.1 \mu \mathrm{sec}$ sweep timing when the DISPLAY MAG switch is set to $\times 10$. Diode D1160 sets the base of Q1164 at about +0.5 V .

## Output Amplifier V1174A and V1184A

The ramp voltage outputs from the collectors of Q1154 and Q1164 are applied to the control grids of V1174A and V1184A in the Output Amplifier stage. These two triodes amplify the ramp voltages, then the output is applied to the Output Cathode Followers, V1174B and V1184B.

To maintain the desired linearity at high sweep rates, part of the output is bootstrapped by the cathode followers through small variable capacitors C1172 and C1182. Diode D1182 conducts when the sweep resets to quickly return the beam to the left edge of the graticule.

BEAM LOCATE switch SW155, located in the cathode circuit of V1174A and V1184A, is a pushbutton switch. When pressed, the switch removes the short-circuit across R1179 to increase the common-cathode resistance and limit the current in the stage. The decrease in current limits the dynamic range of the stage so an off-screen display will appear on screen and the display location can be determined. B1178 is a protection neon that turns on during warm-up of the Type 556, thus limiting the grid-to-cathode voltages at that time.

## Output Cathode Followers, V1174B and VI184B

The Output Cathode Follower stage, V1174B and V1184B, provides a low impedance push-pull drive to the Upper Beam horizontal deflection plates. Variable capacitors C1174 and C1184, together with stray capacitance across R1174 and R1184, form an adjustable high frequency feed-back network to obtain proper sweep waveshapes at high sweep rates.

Neons B1173 and B1183 limit grid-to-cathode voltage during the Type 556 warm up.

## Capacitance Driver, V1194

The cathode of V 1174 B drives the left-hand deflection plate and, during the sweep, the cathode voltage should go linearly in a negative direction. At high sweep rates, when V1174B tries to drive the left-hand deflection plate negative, the deflection-plate capacitance and the output capacitance of cathode follower V1174B tend to distort the ideal linear ramp voltage into an RC discharge curve. To overcome this tendency toward non-linearity, the positive-going ramp voltage at the cathode of V1184B is applied through C1193 to the control grid of Capacitance Driver tube V1194.
The positive-going voltage on the grid of V1194 forces it into heavy conduction. The current supplied through the tube provides extra current to the cathode of V 1174 B and helps to discharge the capacitance in the V1174B output circuit. Since the CRT beam is blanked during the return trace, there is no need for a similar current driver for the cathode of V1184B.

## External Horizontal Amplifier V1104

External signals for use in providing horizontal deflection of the Upper Beam are applied to the UPPER BEAM EXT HORIZ IN connector. In the $\times 1$ position of the Upper Beam DISPLAY MAG switch SW1120, the signal is applied through the switch contacts and a compensated $10 \times$ attenuator to the grid of V1104A. The signal is attenuated $10 \times$ because the Paraphase Amplifier stage, Q1154 and Q1164, is already set for $\times 10$ display magnification regardless of the Upper Beam DISPLAY MAG switch position. When the Upper Beam DISPLAY switch is set to either of the EXT positions, coil L1125 is energized, closing SWll25 relay contacts to provide the $\times 10$ amplifer gain regardless of the DISPLAY MAG positions. Thus, to obtain a normal ( $\times 1$ ) display, the XI attenuator is used to reduce the amplitude of the signal by a factor of ten.

When the DISPLAY MAG switch is set to $\times 10$, the signal is coupled directly (without attenuation) through the switch contacts to the grid of V1104A and the resulting horizontal deflection will appear as a $\times 10$ magified display.
V1104A and V1104B form a cathode follower groundedgrid amplifier and the gain is controlled by adjusting the value of a coupling resistor connected in the cathode circuit. In this circuit, the variable coupling resistor is the UPPER BEAM EXT HORIZ VAR control R1108 which provides at least a $10: 1$ range of adjustment. The output of V 1104 B is applied through the DISPLAY switch to the base of Q1135.

Quiescent current through V1104B is adjusted with the EXT HORIZ DC BAL control R1110 to match the current through V1104A. With R1110 properly adjusted, there is no DC current flow in R1108 and R1105 with no signal applied. Thus, the UPPER BEAM EXT HORIZ VAR 1-10 control can be rotated without causing any horizontal shift in the position of the beam.

Variable capacitor C1115 provides a means of frequencycompensating the divider that is formed when the plate circuit of V1104B is connected to base circuit of Q1135.

## LOWER BEAM HORIZONTAL AMPLIFIER

Except for differences in signal source selections, the Lower Beam Horizontal Amplifier circuit operates the same as the Upper Beam Horizontal Amplifier circuit. The signal source selections for the Lower Beam Horizontal Amplifier are: RIGHT PLUG-IN A, RIGHT PLUG-IN B and EXT.

Instruments with serial numbers 100-1999 do not have the RIGHT PLUG-IN A signal selection.

## CRT CIRCUIT

The CRT in the Type 556 has two sets of vertical deflection plates and two sets of horizontal deflection plates, operated independently of each other. The CRT circuit consists of similar control circuits for the Upper Beam and the Lower Beam. The CRT Circuit consists of two major circuits that are similar to each other and controlled independently. One circuit is the Lower Beam and the other is the Upper Beam. However, the Lower Beam section contains additional circuits that control both beams. These are the high-voltage
delay ${ }^{1}$ and post-acceleration circuits. Fig. 3-20 is a block diagram that shows the Lower Beam CRT Circuit and those adjustments that are common to both beams. The CRT requires an accelerating potential of about 10,000 volts for both beams. Approximately 1850 volts of this is supplied by the CRT negative supply circuits and the remaining 8150 volts is provided by the Lower Beam post-acceleration circuit.

The - 1850 volt supply for each beam consists of an oscillator, step-up transformer, rectifier and voltage regulator circuits. The description of these circuits refers to the Lower Beam section only but can be applied to the Upper Beam as well. Since the Lower Beam section contains additional circuits that affect both beams, these circuits are included in the description.

## High-Voltage Oscillator V1300, Error Amplifier (V774B and V774C), and CRT Control-Grid Rectifier D1332

V1300 with associated circuitry comprises the high-voltage oscillator. V774B and V774C with their associated components are the error amplifiers. Output of the High-Voltage Oscillator is through T1301.
The High-Voltage Oscillator is a modified Armstrong circuit which operates at a frequency of about 35 kHz , determined mainly by the primary winding inductance of T1301 and the capacitance of Cl 303 . Amplitude of the oscillator signal, and thus the amplitude of the rectified DC voltage is adjusted by changing the voltage on the control grid of V1300. This votage is controlled by the HIGH VOLTAGE adjustment R1332, through the Error Amplifier stage.
Transformer T1301 steps up the oscillator signal to the required voltage outputs. Diode D1332 provides half-wave rectification to produce the -1850 V . This negative DC high voltage is filtered by $\mathrm{Cl} 330, \mathrm{C} 1333, \mathrm{C} 1334$ and R 1339 . Then it is applied to the CRT cathode and to a high-resistance voltage divider. The divider includes the FOCUS control R1336 and the HIGH VOLTAGE control R1332. When the HIGH VOLTAGE control R1332 is properly adjusted, the voltage at TP1 340 is -1850 volts.

A portion of the -1850 V is fed back to the oscillator from the junction of R1331 and R1334 through the Error Amplifier stage for amplitude regulation. By comparing this voltage with the ground reference voltage at the cathode of V774C, any tendency of the rectified voltage to become more negative, for instance, would decrease the current through V774C and cause V774B grid to go less negative. This, in turn, would increase the current through V774B and R1302. With increased current through the resistors, the voltage at the control grid of V1300 goes more negative and thus would decrease the oscillator output amplitude to bring the rectifier output back to the correct value.

## High Voltage Delay Q1334

The High Voltage Delay circuit consists of Q1334 and associated components. Purpose of this circuit is to gradually increase the high voltage while the instrument is warming up and the Lower Beam CRT circuit is stabilizing. The action of the delay circuit permits the Lower Beam to reach normal brightness at a slower rate than the Upper Beam.
${ }^{1}$ Added in Type 556 SN 2000 and up.

## Circuit Description-Type 556



Fig. 3-20. Partial block diagram of CRT circuit showing the LowerBeam section and those adjustments that are common to both beams.

When the instrument is first furned on, Q1334 goes into saturation; D1334 and D1325 are reverse biased. The base current of Q1334 and the high-resistance path of R1323, R1325, R1326 and R1328 allow C1325 to change slowly. The change current keeps Q1334 froward biased and in saturation until the current begins to decrease as Cl 325 approaches full change. In about 20 seconds C1325 charge current has decreased to the point where D1325 becomes biased and Q1334 starts to come out of saturation.

As Q1334 comes out of saturation and starts to turn off, C1331 begins to charge. Charge current flows through the emitter-base junction of Q1334, and through resistors R1323, R1328 and R1329. As C1331 approaches full charge and the current decreases, Q1334 turns off and D1334 becomes biased. During the time that C 1331 has been charging, the voltage level at the junction of R1330, R1331 and R1333 rises slowly, this action causes V774C grid voltage to go slowly less negative. Current through V774C increases, cur-
rent through V 774 B decreases and V 1300 control grid voltage goes less negative. As a result, the oscillator output amplitude is increased gradually as C 1331 changes. Finally, when C1331 becomes fully charged, the voltages at TP1340 and the post-acceleration anode reach their normal level.

Total delay time is about 40 seconds. When the instrument is turned off, protection diode D1334 limits Q1334 emitter-to-base junction reverse bias by allowing C 1325 to discharge through the diode.

## Post-Acceleration Supply

A half-wave voltage tripler circuit, V1322, V1232 and V1342, rectifies the output from the associated secondary winding of T 1301 to provide the dual-beam CRT post-acceleration potential of +8150 volts. Regulation of this voltage is provided through the transformer by regulation of the HighVoltage Oscillator V1300 output. Ground return for this supply is through the resistive helix inside the CRT to pin 9, through the R1392-R1393 divider resistors and to the $+225-\mathrm{V}$ and $+100-\mathrm{V}$ supplies.

## CRT Control-Grid and Unblanking Circuit

As stated eariler, D1322 rectifies the high voltage from T1301 secondary winding (terminals 6 and 9). This rectified voltage provides the DC bias source for the CRT control grid. The front-panel Lower Beam INTENSITY control R1319 provides a means for manually adjusting the bias voltage applied to the Lower Beam CRT control grid and thus control the magnitude of the beam current. The range of the INTENSITY control varies the grid from about - 1950 to - 1870 volts.

As the control grid negative voltage is decreased (made less negative), the beam intensity is increased.

At the slower sweep rates the sweep unblanking signal from V783B in the B Sweep Generator circuit is applied through R1316, R1317, R1318, R1319 and R1320 to drive the Lower Beam control grid. The INTENSITY control R1319 is normally set so the Lower Beam does not light the phosphor of the CRT screen except during the positive portion of the sweep unblanking waveform.

At the fastest sweep rates, the stray capacitance of the floating control grid circuit makes it difficult for the grid to rise fast enough to unblank the CRT within the required time. A network consisting of R1316 and R1320 isolates the capacitive loading. By this arrangement, the fast leading edge of the unblanking pulse is coupled through C1321 and C1323 to the control grid of the CRT. For short-duration unblanking pulses such as those occurring at the fastest sweep rates, the DC levels on the rectifier D1322 and the associated secondary winding of Tl 301 are not appreciably affected. Longer unblanking pulses such as those that occur at the slower sweep rates, charges the stray capacitance in the control grid circuit through R1316. This pulls the floating grid up and holds the grid at the unblanked potential for the duration of the unblanking pulse.

## CRT Circuit Controls and Connectors

Optimum size and shape of the upper beam as it is accelerated to the screen is obtained by adjusting the front-panel

FOCUS and ASTIGMATISM controls. The FOCUS control R1366 provides the correct voltage for the second anode (focus ring) of the Upper Beam elements. Proper voltage for the third anode is obtained by adjusting the ASTIGMATISM control R1344. In order to obtain optimum spot size and shape, both the FOCUS and ASTIGMATISM controls are adjusted to provide the proper electronic lens configuration in the region of the second and third anodes. Spot intensity is adjusted by means of the front-panel INTENSITY control R1319. Varying the INTENSITY control changes the voltage on the CRT control grid, which in turn varies the density of the electron stream. Internal CENTER GEOM R1342 and EDGE GEOM R1391 controls adjust the isolation and edge shield voltages to minimize bowing of the display. The frontpanel TRACE ROTATION control, R1390A and R1390B, permits minor adjustment in trace orientation. By adjusting the TRACE ROTATION control, the traces for both beams can be made parallel with the horizontal center lines on the internal graticule.

## Lower Beam CRT Controls

The EXT CRT CATHODE BNC connector on the rear panel of the Type 556 provides an input for externally modulating the Lower Beam CRT cathode. The connector is normally grounded by a grounding cover. To intensity modulate the display from an external source, the grounding cover is disconnected from the BNC connector, the CRT Cathode Selector switch SW1345 is set to the EXT CRT CATHODE position, and the modulating signal is coupled to the Lower Beam CRT cathode through C1347.

When the Type 556 is used with multi-channel vertical plug-in units that provide multi-trace chopped blanking pulses, the blanking pulses are applied to the CRT Cathode Selector switch SW1345. With the plug-in unit operating in the chopped mode and SW1345 set to the LOWER BEAM CHOPPED BLANKING position, a positive pulse of about 20 volts amplitude is applied through Cl 347 to the cathode of the Lower Beam. At normal intensity levels, this pulse is sufficient to cut off the CRT during the time the channels in the plug-in unit are switched.

## Upper Beam CRT Circuit

Except for the dual-beam post-acceleration supply and the high-voltage delay circuit included in the Lower Beam section, the Upper Beam CRT circuit is the same. For the Upper Beam, there is an additional signal which is combined with the unblanking pulse for controlling the trace unblanking levels. This additional signal, as explained earlier in the Upper Beam Unblanking Amplifier V574A description, restores the beam to its normal intensity level for the duration of the $\mathbf{E}$ sweep when using delayed-sweep mode of operation. This intensity level is referred to in this manual as the intensified portion of the Upper Beam display.

In delayed-sweep mode of operation, the front-panel CONTRAST control (see B Sweep Generator circuit) is used to control the brightness of the non-intensified portions of the trace and the INTENSITY control R1369 is used to set the overall level including the intensified portion of the display.

## POWER SUPPLY and HEATER WIRING



## General

The low-voltage power supply provides the operating power for the instrument from four regulated supplies: - 150 $\mathrm{V},+100 \mathrm{~V},+225 \mathrm{~V}$ and +350 V . Electronic regulation is used to provide stable output voltages. Each supply is fuseprotected against overloads.

An unregulated +6 volt supply is provided to operate the Reset Lamp Driver stages Q619 and Q819, and for powering the incandescent indicator lights B619 and B819. Unregulated 6.3 V and 12.6 V RMS AC voltages are provided for operating the tube filiments (including the dual-beam CRT), POWER pilot light and graticule lamps.. The 6.3 V is also the line triggering source for the A and B Sweep Trigger circuits.

All of the power-supply DC regulator circuits operate similarly. A sensing circuit compares a sample of the output voltage against a fixed reference voltage. Any difference between the output voltage and the reference produces an error signal which is amplified and applied to the series regulator transistors, causing the regulators to correct for the error and return the output to the proper value. Fig. 3-21 is a block diagram of the Power Supply circuit (Fig. 3-22 for SN 100-1999).

## Power Transformer

The power transformer T1401 is enclosed in a special metal shield to reduce the effects of electromagnetic interference in the other circuits. The transformer windings ar shown schematically on the Power Supply diagram in Section 9.

When line voltage is applied to the instrument, the current path through the primary circuit is through line filter FL1400, POWER switch SW1402, thermal cutout TK1404, fuse F1401 or flses F1401 and F1402, and through both primary windings. When the instrument is configurated for a 115 volts (nominal) application, only fuse Fl 401 is used, with a 230 volts (nominal) application, fuse F1402 is added to the circuitry.

To provide optimum voltage regulation and correct DC voltage levels with any applied line voltage within the ranges of 90 to 136 VAC and 180 to 272 VAC , the primary is constructed as two identical windings, each with three taps to permit selection of different turns ratios. The desired transformer turns ratio is selected by positioning the Voltage and Range Selectors (located in the Line Voltage Selector Assembly). The two windings are connected in parallel when the Voltage Selector is set to 115 V and in series when the selector is set to 230 V . The position of the Range Selector (LO, M, HI) determines which taps on the two windings are selected.

For instruments with serial numbers 100-1999, the transformer primary circuit configuration is as follows:

One winding connects to terminals 1 and 3, the other connects to terminals 2 and 4. There are two more windings which may be used as voltage bucking or aiding windings. These are connected to terminals 5 and 6 for one winding and terminals 7 and 8 for the other winding. These windings
along with the two main primary windings may be used to allow the instrument to run on nominal line voltages of 104, 115,208 , and 230 volts, depending upon how all the windings are connected. Square pin connectors on a power circuit board simplify the connections of leads and connectors when changing line-voltage operation.
Thermal cutout switch TK1404 is provided to protect the instrument from excessive heating. When its ambient temperature exceeds approximately $140^{\circ} \mathrm{F}$, the thermal cutout switch will open the transformers primary circuit, Since the switch will close when its ambient temperature drops below its opening temperature, and restore line voltage to the primary, always set the POWER switch to OFF before attempting to remedy an overheated instrument condition.

The fan must be operative when power is applied to the instrument to adequately circulate the cooling air. Since the fan motor is connected across one of the primary windings. power is applied to the fan motor when it is applied to the primary windings and the fan rotation speed is not affected by changes to the transformers turns ratio.

The transformers output windings are the voltage source for five full wave rectifier circuits and one 6.3 VAC circuit.

## DC VOLTAGE SUPPLIES SN 2000-up

## -150 Volts Supply

A block diagram of this circuit is shown in Fig. 3-20. The - 150 Volts Supply circuit contains a rectifier in the form of a diode bridge (D1482) connected to one of the secondary windings of T1401; a variable resistance network that contains the -150 volts output level adjustment R1498; a comparator circuit (Q1484 and Q1494) that senses any change in the output voltage level with respect to ground and two emitter followers (Q1504 and Q1513) that connects the output of the comparator circuit to 2 series regulator (Q1517). The series regulator circuit (Q1517) provides the necessary voltage compensations to maintain the output level at -150 volts.
Q1484 and Q1494 with their associated circuitry form the voltage comparator circuit. The constant plate to cathode voltage of glow discharge tube. V1482 is used to fix the voltage at the base of Q1484 with respect to the negative side of the rectifier bridge or output of the -150 supply. The base of Q1494 is connected to a variable resistance network that includes the -150 volts adjustment R1498. Since this resistance network is connected between the -150 supply circuits output and ground, the Q1494 base voltage level set by R1498 is referenced to ground. With the base voltage of Q1484 fixed with respect to the output voltage and the base voltage of Q1494 following any change in output voltage with respect to ground, the division of currents through Q1484 and Q1494 will vary with any output voltage change in respect to ground. The changes in the division of currents through the two transistors will cause voltage changes in both collector circuits, but only the voltage changes, or error signals, developed in the Q1494 collector circuit are coupled by the emitter follower circuits to the series regulator circuit.

During instrumnt calibration, the - 150 volts adjustment, R1498, is set to establish a division of currents through Q1484 and Q1494. This produces a Q1494 collector voltage which sets the Q1504, Q1515 and Q1517 bias voltages, producing


Fig. 3-21. Block diagram of Power Supply circuit and partial circuit of Heater Wiring for the Type 556 SN 2000 and up.


Fig. 3-22. Block diagram of Power Supply circuit and partial circuit of Heater Wiring for the Type 556 SN 100 to 1999.
a Q1517 collector to emitter drop which equals the difference between the rectifier output voltage and 150 volts. When the regulator circuitry is adjusted to produce -150 volts for a given rectifier output, any change in output voltage with respect to ground causes a bias change on Q1494 of opposite polarity to the output voltage, and of about one half the amplitude. For example, if the -150 volts output began to increase toward -151 volts, the voltage at the emitter of Q1494 would become more negative by approximately the unit of voltage change (due to the constant voltage across V1482), while the voltage at the base of Q1414 would become more negative by approximately one-half the unit of voltage change (due to the voltage divider action of the resistance network), resulting in an increase in forward bias of approximately one-half the unit of voltage change.

Q1504 and Q1513 with their associated circuitry form two emitter follower circuits. Error signals developed in the collector circuit of Q1494 are coupled to the base of Q1517 via these two emitter followers. The two emitter followers provide isolation between the error sensing circuit and the series regulator. The associated circuitry is configured to provide error signal limiting for regulator circuit protection and to provide phase shifting to prevent self-inflicted regulator circuit oscillations.

Q1517 and shunt resistor R1519 form a series regulator circuit. The circuit functions as a variable resistance in series with the -150 volt load circuits. Any change in the rectifier output voltage, whether due to line voltage or load current changes, is compensated by an equal change in voltage across the series regulator circuit.

Since the compensating changes in voltage across the series regulator are reactions to changes in the output voltage with respect to ground, there is a temporary change in output voltage during the regulator circuit reaction time. Filter capacitors Cl 498 and Cl 499 , connected between the -150 volts output and ground, suppresses the effects of these voltage changes to a level negligible to the operation of the instrument.

Fuse 1482 will open when the current through it exceeds approximately .75 amperes. Since an excessive current must be present for a finite interval before F1 482 will open, R1517 is provided to limit surge currents through Q1517 to a level within the transistor's dissipation capabilities.

## +100 Volt Supply

The input to the +100 V supply is the output of the secondary winding connected to terminals 13 and 14 on the power transformer Tl 401 and the silicon diode bridge D1452. In addition to its other loads, the +100 V supply provides current to the +225 V supply and then through the 225 V supply to the 350 V supply. Also, the +100 V supply must provide a total current of 300 mA to two series strings of filaments (see the Heater Wiring diagram). The plug-in units become part of the series filament string. If the plug-in units are removed while the oscilloscope is operating, the +100 V supply is capable of remaining within its dissipation limits despite the 300 mA change in load.

The configuration of the +100 Volt Supply regulator circuit and its reaction to a change in output voltage is similar to the -150 Volts supply regulator circuit.

Q1454 with its associated circuitry forms the error sensing circuit. The base of Q1454 is connected to a resistance network that includes the +100 volt output adjustment R1459. Since R1459 is connected between the +100 Volt output and the regulated -150 Volt output, any change in the +100 volts with respect to the -150 Volts is applied as a change signal to the base of Q1454. D1450 provides thermal compensation for Q1454 and reference to ground.
Q1463 and Q1464 with their associated circuitry form a circuit similar in configuration and function to the circuit formed by Q1504 and Q1513 in the - 150 Volt supply circuit.

Q1467 and Q1477 are connected in parallel and with the shunt resistors R1476, R1477 and R1478 form the series regulator circuit.

Fuse F1478 and current limiting resistors R1464 and R1469 protect the circuit from excessive currents.

## +225 Volt Supply

The AC output of the secondary windings between terminals 15 and 16 is rectified by diode bridge D1432 and added to the +100 volt supply output to produce the +225 volts supply.

The +225 volts supply is similar in configuration and operation to the +100 volts supply. Q1434 with its associated circuitry forms the error sensing circuit. D1430 provides +100 reference and temperature compensation for Q1434 and R1430 is the +225 Volt output adjustment. Q1443 and Q1444 with their associated circuitry form the emitter follower circuits. Q1447 with the two shunt resistors R1445 and R1446 form the series regulator circuit. The regulating circuit is protected by fuse F1446 and current limiting resistors R1442 and R1443.

## +350 Volt Supply

The AC output of the secondary windings between terminals 19 and 20 is rectiifed by diode bridge D1412 and added to the +225 volts supply through the series regulator (Q1427) to produce the +350 Volt supply.

Q1414 with its associated circuitry forms the error sensing circuit. The base of Q1414 is connected to the junction of two equal value resistors. Since these two resistors are connected between the +350 Volts output and the -150 Volt output, about one-half the amplitude of any change in the +350 Volts with respect to the regulated -150 Volts is applied to the base of Q1414.
Q1424 with its associated circuitry forms an emitter follower circuit that provides isolation between the error sensing circuit and the series regulator circuit. The output of Q1424 is the signal drive for Q1427 in the series regulator circuit.

Q1427 and shunt resistor R1427 form the series regulator circuit. Current limiting for Q1427 is provided by R1429.

In the event of a circuit malfunction, the +350 V supply circuitry is protected from excessive currents by F1424 and the output supply voltage is prevented from decreasing substantially below the +250 volts supply level by D1440.

The power supply circuits in instruments SN 100-1999 are configurated similarly to the circuits described above. They produce the same output supply voltages and the supply
voltages and are regulated in essentially the same manner. In general, components in the two power supply configurations that have the same circuit designations, provide the same or a similar function. The notable circuit differences are, the transistors used in the four series regulator circuits are PNP germanium instead of NPN silicon; modified Darlington amplifiers instead of emitter follower circuits connect the output of the error sensing circuits to the series regulators in the $-150,+100$ and +250 Volt supplies and a voltage amplifier instead of an emitter follower connects the error sensing circuit to the series regulator in the +350 Volt supply.

## CALIBRATOR 17

The Calibrator circuit in the Type 556 is a 1 kHz squarewave generator (see Fig. 3-23 and the Calibrator schematic) that provides both voltage and a 5 mA current output to the front-panel connectors. The voltage output is taken from the CAL OUT connector on the front panel, where either a square wave or a steady +100 V DC reference voltage is available.

By rotating the AMPLITUDE CALIBRATOR switch SW1630, the amplitude of the square wave output may be varied from 0.2 mV to 100 V peak to peak. The current output is applied to the loop marked 5 mA , with the arrow indicating conventional current flow. When the AMPLITUDE CALIBRATOR switch is set to the 100 V DC position, the loop has 5 mA DC flowing through it. When the switch is set to the $5 \mathrm{~mA} \Omega$ position, the current through the link is in the form of a $1 \mathrm{kHz}, 5 \mathrm{~mA}$ square wave.

## CAUTION

The loop is designed for use with a snap-on current probe and does not unplug.

## Calibrator Multivibrator, V1605A and V1605B

The square-wave generator is an astable multivibrator using two sections of a three-section tube. V1605A and V1605B are the multivibrator sections with the pentode section (V1605A) connected as a triode. The value of the plate load resistor R1605 is relatively lower than the value of V1605B plate load resistor R1615 so the current drawn through the sections during conduction will be nearly the same and constant current will be drawn from the -150 V supply.

When the amplitude calibrator is turned on, the multivibrator cathodes are returned through R1602 and R1601 to the -150 V supply. Capacitor Cl 602 bypasses any fast switching transients that may appear at the cathodes. The plate of V1605A operates from the +100 V supply while the plate of V 1605 B operates from the +225 V supply. The plate of V1605B swings from about -2 volts to about +143 volts. The output voltage from the plate of V1605B is coupled through R1620 and the CAL AMPL control R1628 to the grid of the cathode follower section, V1605C.

## Calibrator Output Cathode Follower V1605C

The Calibrator Multivibrator stage switches the Calibrator Output Cathode Follower section, V1605C, between cutoff and conduction. During the negative portion of the multivibrator output waveform, the grid of V1605C is driven well below cutoff and its cathode rests at ground potential. During the positive portion of the waveform, V1605C is driven into conduction and the cathode potential is +100 V , set accurately by the CAL AMPL control R1628, the clamping action of D1620, and the precise setting of the +100 V supply.

Accurate adjustment of the CAL AMPL control is made by setting the AMPLITUDE CALIBRATOR switch SW 1630 to 100 V DC and then adjusting R1628 for exactly +100 V output at


Fig. 3-23. Block diogram of the Calibrator circuit.
the CAL OUT connector. With the switch set to 100 V DC, the Calibrator Multivibrator stage is disabled because the cathode return circuit is disconnected from -150 V . Diode D1620 conducts and clamps the junction of R1620 and R1628 at about 0.6 V higher than the +100 V supply voltage. Thus, V1605C is held in conduction at the same level as that obtained when the multivibrator is operating and V1605B plate is at its most positive level. With V1605C grid held at a constant $D C$ level and with the +100 V supply previously adjusted for proper output, the CAL AMPL control R1628 can be easily adjusted for exactly +100 V output at the CAL OUT connector.

The network consisting of $\mathrm{R} 1622, \mathrm{R} 1624$ and Cl 624 prevents any ringing on the rising portion of the square wave.

## Output Divider Resistors

Cathode-follower section V1605C has a precision divider network for its cathode resistor. With the CAL AMPL control properly adjusted so the signal amplitude at the cathode
of V 1605 C is exactly 100 V peak to peak, the divider network accurately divides the basic 100 V square wave to lower amplitudes in multiples of 1,2 or 5 and provides an accurate 50 -ohm output resistance when the AMPLITUDE CALIBRATOR switch is set to .2 VOLTS and below. If the 50 -ohm output is terminated into a 50 -ohm external load, the peak voltage across the external termination will be one-half that indicated by the switch setting.
The $100 \mathrm{~V} D C$ is available for use as a reference when the AMPLITUDE CALIBRATOR switch is set to 100 V DC. If the switch is set to the 5 mA position, an accurate 5 mA square wave is fed through the current loop. The accuracy of this current is established by the accurate $20 \mathrm{k} \Omega$ series resistance of divider resistors R1632 through R1640.

The 0.25 ohm resistor R1654, connected in series with the output divider resistors R1647 and R1650, minimizes possible ground current effects on the calibrator voltage accuracy; i. e., ground currents that may exist between the oscilloscope chassis and the chassis of some other device that is driven by the Amplitude Calibrator.

# SECTION 4 <br> MAINTENANCE 

Change information, if any, affecting this section is found at the rear of the manual.

## Introduction

This section of the manual contains maintenance informafion for use in preventive maintenance, corrective maintenance, and troubleshooting procedures for the Type 556.

## PREVENTIVE MAINTENANCE

## General

Preventive maintenance consists of cleaning, visual inspection, lubrication, etc. Preventive maintenance performed on a regular basis will help prevent instrument failure and will improve reliability of this instrument. The severity of the environment to which the Type 556 is subjected will determine the frequency of maintenance required.

We recommend servicing and recalibration after each 500 hour period of operation, or more frequently if the instrument is usually operated under adverse conditions such as a high temperature or a dusty or corrosive atmosphere. Even if the instrument is used only occasionally, it should be serviced and recalibrated at least once every six months.

## Exterior Cleaning

Loose dust accumulated on the outside of the Type 556 can be removed with a soft cloth or small paint brush. The paint brush is particularly useful for dislodging dirt on and around the front-panel controls. Dirt which remains can be removed with a soft cloth dampened in a mild solution of water and detergent. Abrasive cleaners should not be used.

Clean the light filter, faceplate protector and CRT face with a soft, lint-free cloth dampened with denatured alcohol.

## CAUTION

Avoid the use of chemical cleaning agents which might damage the plastics used in this instrument. Some chemicals to avoid are benzene, toluene, xylene, acetone or similar solvents.

## Removal of Panels

The side panels on the Type 556 may be easily removed for access to the internal circuitry. The panels are held in place by slot-head fasteners that can be released with a broad-blade screwdriver or a small coin. Turn each fastener $1 / 4$ turn counterclockwise to free the panel. The top and bottom panels are held in place by Phillips-head screws.

For further acces to the internal circuitry of the Type 556 any of the corner rail angles can be removed by using a Phillips screwdriver.

In addition to providing dust protection and proper shielding, the side, top and bottom panels enable the cooling air
to be directed through the filter and fan for proper air circulation throughout the interior of the instrument. The panels should not be removed except during maintenance and calibration.

## Interior Cleaning

Dust in the interior of the instrument should be removed occasionally due to its electrical conductivity under highhumidity conditions. The best way to clean the interior is to blow off the accumulated dust with dry, low-velocity air. Remove any dirt which remains with a soft paint brush or a cloth dampened with a mild detergent and water solution. A cotton-tipped applicator is useful for cleaning in narrow spaces or for cleaning ceramic terminal strips and circuit boards.

The high-voltage circuits, particularly parts located in the high-voltage compartment and the area surrounding the postdeflection anode connector, should receive special attention. Excessive dust or dirt in these areas may cause high-voltage arcing and result in improper instrument operation.

## Air Filter

The air filter should be visually checked every few weeks and cleaned or replaced if dirty. For cleaning, remove the filter from the rear of the instrument. Wash it in the same manner as a synthetic sponge, rinse and let dry. When the filter is thoroughly dry, coat with fresh air-filter adhesive (available from air conditioner suppliers or order Tektronix Part No. 006-0580-00). Let the adhesive dry thoroughly before re-installing the filter.

If desired, the filter may be replaced by ordering from your local Tektronix Field Office or Representative. The part number is 378-0034-01.

## Visual Inspection

The Type 556 should be inspected occasionally for such defects as broken connections, broken or damaged ceramic strips, improperly seated transistors or tubes, damaged circuit boards and heat-damaged parts.

The remedy for most visible defects is obvious; however, care must be taken if heat-damaged parts are located. Overheating is usually only a symptom of trouble. For this reason, it is essential to determine the actual cause of overheating before the heat-damaged part is replaced; otherwise, the damage may be repeated.

## Transistor and Tube Checks

Periodic checks of the transistors and tubes in the Type 556 are not recommended. The best check of transistor or tube
performance is its actual operation in the instrument. More details on checking transistor and tube operation is given under Troubleshooting.

## Lubrication

The reliability of potentiometers, rotary switches and other moving parts can be increased if they are kept properly lubricated. Use a cleaning-type lubricant (such as Tektronix Part No. 006-0218-00) on shaft bushings and switch contacts. Lubricate switch detents with a heavier grease (such as Tektronix Part No. 006-0219-00). Potentiometers should be lubricated with a lubricant which will not affect electrical characteristics (such as Tektronix Part No. 006-0220-00). Do not overlubricate. A lubrication kit containing the necessary lubricants and instructions is available from Tektronix. Order Tektronix Part No. 003-0342-00.

The fan bearings are sealed and do not require lubrication.

## CORRECTIVE MAINTENANCE

## General

Corrective maintenance consists of component replacement and instrument repair. Special techniques or procedures required to replace components in this instrument are described here.

## Obtaining Replacement Parts

Standard Parts. All electrical and mechanical part replacements for the Type 556 can be obtained through your local Tektronix Field Office or representative. However, many of the standard electronic components can be obtained locally in less time than is required to order them from Tektronix, Inc. Before purchasing or ordering replacement parts, consult the Parts List for value, tolerance and rating.

## NOTE

When selecting replacement parts, it is important to remember that the physical size and shape of a component may affect its performance at high frequencies. All replacement parts should be direct replacements unless it is known that a different component will not adversely affect instrument performance.

Special Parts. In addition to the standard electronic components, some special parts are used in the Type 556 . These parts are manufactured or selected by Tektronix, Inc. to meet specific performance requirements, or are manufactured for Tektronix, Inc. in accordance with our specifications. These special parts are indicated in the Parts List by an asterisk preceding the part number. Most of the mechanical parts used in this instrument have been manufactured by Tektronix, Inc. Order all special parts directly from your Tektronix Field Office or representative.

Ordering Parts. When ordering replacement parts from Tektronix, include the following information:

1. Instrument Type.
2. A description of the part (if electrical, include circuit number).
3. Tektronix Part Number.
4. Instrument Serial Number.

## Soldering Techniques

## WARNING

Disconnect the instrument from the power source before soldering.
To solder or unsolder any small or short-lead component:

1. Use needle-nosed pliers to act as a heat sink between the soldering point and the component;
2. Use a moderately hot iron for a short period of time;
3. Manipulate your tools with care to avoid damage to small components;
4. Use only enough solder to make a good bond.

Due to the presence of normal stray fields and capacitance within the instrument, the locations of some components in the Type 556 are important to the operation of the system. Be sure to install replacement components in the exact positions occupied by the original parts.

After soldering any connection, clip off the excess length of the soldered leads. Be sure that these ends are not dropped into the instrument where they could cause electrical shorting.


Fig. 4-1. Soldering aid for use with bare wires.

Fig. 4-1 illustrates a handy tool for holding bare wires in place while soldering. It can be made from a short length of wooden dowel or thermoset plastic, with one end shaped as a wedge.
When soldering to a wafer-type switch, do not let the solder flow around and beyond the rivet on the switch terminal. The spring tension of the switch contact may be destroyed by excess solder and the switch will need to be replaced.

Circuit Boards. Use ordinary $60 / 40$ solder and a 35 - to 40- watt pencil type soldering iron on the circuit boards. The tip of the iron should be clean and properly tinned for best heat transfer to the solder joint. A higher wattage
soldering iron may separate the etched wiring from the base material.

The following technique should be used to replace a component on a circuit board.

1. Grip the component lead with long-nose pliers. Touch the soldering iron to the lead at the solder connection. Do not lay the iron directly on the board, as it may damage the board.
2. When the solder begins to melt, pull the lead out gently. This should leave a clean hole in the board. If not, the hole can be cleaned by reheating the solder and placing a sharp object such as a toothpick or pointed tool into the hole to clean it out.
3. Bend the leads of the new component to fit the holes in the board. If the component is replaced while the board is mounted in the instrument, cut the leads so they will just protrude through the board. Insert the leads into the board until the component is firmly seated against the board. If it does not seat properly, heat the solder and gently press the component into place.
4. Apply the iron and a small amount of solder to the connection to make a firm solder joint. To protect heat-sensitive components, hold the lead between the component body and the solder joint with a pair of long-nose pliers or other heat sink.
5. Clip the excess lead that protrudes through the board.
6. Clean the area around the soldered connection with a flux-remover solvent to maintain good environmental characteristics. Be careful not to remove information printed on the board.

Ceramic Terminal Strips. Solder used on the ceramic terminal strips should contain about $3 \%$ silver. Ordinary tinlead solder can be used occasionally without damage to the ceramic terminal strips. Use a 40 - to 75 -watt soldering iron with a $1 / 8$ inch wide chisel-shaped tip. If ordinary solder is used repeatedly or if excessive heat is applied, the solder-toceramic bond may be broken.

A small roll of $3 \%$ silver solder is mounted near the Lower Beam high-voltage compartment on the right side of the instrument. Additional silver solder should be available locally or it can be purchased directly from Tektronix; order by Tektronix Part No. 251-0514-00.

Observe the following precautions when soldering ceramic terminal strips:

1. Use a hot iron for a short time. Apply only enough heat to make the solder flow freely.
2. Maintain a clean, properly tinned tip.
3. Avoid putting pressure on the ceramic terminal strip.
4. Do not attempt to fill the terminal-strip notch with solder; use only enough solder to cover the wires adequately.
5. Clean the flux from the terminal strip with a fluxremover solvent to maintain good environmental characteristics.

Metal Terminals. When soldering metal terminals (for example, switch terminals, potentiometers, etc.), ordinary

60/40 solder may be used. The soldering iron should have a 40 - to 75 -watt rating with a $1 / 8$ inch wide chisel-shaped tip.

Observe the following precautions when soldering metal terminals:

1. Apply only enough heat to make the solder flow freely.
2. Apply only enough solder to form a solid connection. Excess solder may impair the function of the part.
3. If a wire extends beyond the solder joint, clip off the excess.
4. Clean the flux from the solder joint with a flux-remover solvent to maintain good environmental characteristics.

## Ceramic Strip Replacement

To replace a damaged ceramic terminal strip, first unsolder all connections, then pry the mounting studs attached to the strip out of the chassis. If prying is not satisfactory, remove the studs by tapping on the ends protruding from the reverse side of the chassis. Still another way to remove a ceramic strip is to use diagonal cutters and cut off one side of each stud. The remainder of the studs can then be pulled out after the strip has been removed.

If the nylon spacers do not come out with the studs, they may be left in the chassis or pulled out separately. The spacers, if not damaged, can be used with the new ceramic strip assembly. Replacement strips are supplied with mounting studs attached, so it is not necessary to salvage the old studs.

When the damaged strip and stud assembly have been removed, place the spacers into the mounting holes in the chassis and press the mounting studs of the new strip assembly into the spacers. It may be necessary to tap lightly or apply some pressure to the ceramic strip to make the studs seat all the way down into the spacers. To avoid damage to the terminal strip use a soft-tipped tool for tapping, and apply force only to the portion of the strip directly above the mounting studs. Fig. $4-2$ shows the assembled terminal strip. Cut off the excess length of the mounting studs extending beyond the ends of the spacers. Resolder all components and wires in place as they were previously arranged (note the soldering techniques described earlier).


Fig. 4-2. The assembled ceramic strip.

## Component Replacement

Transistor and Tube Replacement. Transistors and tubes should not be replaced unless actually defective. If they are removed during routine maintenance, return them to their original sockets. Unnecessary replacement of transistors or tubes may affect the calibration of this instrument. When transistors or tubes are replaced, check the operation of that part of the circuit which may be affected.

Fuse Replacement. Table 4-1 shows the ratings of the fuses used in this instrument. Refer to Figs. 4-3 and 4-4 for the locations.

TABLE 4-1
Fuse Replacement

| Fuse Circuit <br> No. | Circuit | Rating |
| :---: | :---: | :---: |
| F1401 | 115 VAC | $10 \mathrm{~A} \mathrm{Slo-Blo}$ |
| F1402 | 230 VAC | 5 A Slo-Blo |
| F1424 | +350 VDC | 0.75 A Fast |
| F1446 | +225 VDC | 1.5 A Fast |
| F1478 | +100 VDC | 1 A Fast |
| F1482 | -150 VDC | 0.75 A Fast |

Rotary Switch Replacement. Individual wafers or mechanical parts of rotary switches normally are not replaced. If a switch is defective, replace the entire assembly. Replacement switches can be ordered either wired or unwired; refer to the Parts List for the applicable part numbers.

## Circuit Board Assembly Replacement

If a circuit board is damaged and cannot be repaired, a circuit board without components may be obtained; or, if desired, a unit completely wired with components mounted may be obtained by the normal ordering procedure.

All electrical connections to the folowing circuit boards are made with push-on pin conectors: A Sweep Trigger Switch, B Sweep Trigger Switch, A Sweep Trigger, B Sweep Trigger and Power. The push-on connectors to these boards are easily removed. Once the wires are disconnected, removal is a matter of removing the mounting screws and lifting out the board. To reinstall or replace these boards, use the illustrations (see Fig. 4-11 through 4-16 in this section as a guide for reconnecting the wires to the board.

The A Triggering switch circuit board (consisting of five individual lever switches wired to the circuit board) may be removed as an assembly, and the switch to be replaced may be soldered to the board, using the soldering techniques suggested previously. The same procedure is used for the replacement or removal of the B Triggering switch circuit board assembly.

All electrical connections to the High Voltage Delay board* are soldered. Two 40- to 75 -watt soldering irons are required to remove this board from the ceramic strip slots.

## Cathode-Ray Tube Replacement

Use the following procedure to replace the CRT:
*Added in Type 556 5/N 218 and up. Some instruments were modified out of sequence.

## Removal (See Fig. 4-5)

1. At the rear of the instrument, remove the four cap nuts securing the air filter housing. Remove the housing and air filter.
2. Remove the four screws securing the fan assembly. The fan assembly is hinged to allow easy access to the interior of the instrument.
3. Disconnect the CRT socket.
4. Disconnect the lead clips from the deflection pin connectors on the neck of the CRT. The leads to the Lower Beam may be reached through the fan assembly opening.

## CAUTION

Be careful to avoid bending the deflection pin connectors.
5. Disconnect the high voltage anode lead.

## NOTE

The two wires through the shield near the high voltage anode connector are the leads to the beam rotator coil and should not be removed.
6. At the front of the instrument, remove the four nuts securing the graticule cover. Remove the graticule cover, the light filter (if used), and the clear plastic face plate protector.
7. Remove the plastic ring which holds the light guide to the perimeter of the face plate, and remove the light guide.

ठ. Loosen the CRT clamp until the CRT can be slid forward and removed.

## Replacement

1. Insert the CRT from the front of the instrument with the high voltage anode connector about $90^{\circ}$ counterclockwise from a directly upward position.
2. Replace the leads going to the Lower Beam deflection pin connectors one at a time starting with the red (on white) lead and rotating the CRT clockwise as the other leads are replaced. The color code on the CRT shield indicates the correct connections for the deflection pin connectors.
3. Temporarily replace the face plate protector and graticule cover and screw down the knurled retaining nuts.
4. Position the CRT so that the face plate is touching the face plate protector and the vertical graticule lines are parallel to the sides of the instrument.
5. Tighten the CRT neck clamp to 4 inch-pounds ( $\pm 2$ inch-pounds) of torque.

## CAUTION

Do not exceed 4 inch-pounds of torque under any condition when tightening the CRT neck clamp.
6. Replace the CRT socket and the remaining deflection pin connectors.
7. Connect the high voltage anode connector.
8. Remove the graticule cover and the face plate protector, and install the light guide and plastic hold-down ring.


Fig. A-3. Powar Supply fuie locailans, botiam vlaw.


Fig. 4-4. Lacalion of line fuses.

## Mainfenance-Type 556



Fig. 4-3 Inalpument rear vlew, CRT ieplacement (filior houslng removed).
9. Replace the facoplate protector, light filter (if used), and the graticule cover, screwing down the graticule nuts.
10. The four wing nuls securing the CRT shield assembly to the back panel may be loosened to permit adjusiment of the shield so the CRT faceplate will bo exacily parallol with the front panel of tho insirument.
11. Adjust the BEAM ROTATION control before beginning the recalibration proceduro.

## NOTE

After the replacement of any electrical camponent, it will be necessary to check the calibration of the circuit involved. If other circuits are closely related, as indicated on the schematic diagrams and in Table 4-5, their calibration should also be checked. Since the low voltage supplies affect all circuils, the entire instrument will need recalibrafion if work has been done on the power supplies or if a power transformer has been replaced.

## Power Transformer Replacement

Use the following procedure to replace the low vollago power transformer:

## WARNING

Remove the power source plug from the rear of the instrument before aftempting to replace the transformer.

1. Disconnect all transformer-lead pin connectors from the powar circuit board, including the white wire going from the hinged power-chassis to terminal A (ground) on the power circuif board.
2. Loosen the two knurled faslening screws sufficiently to allow the hinged power chassis to swing away from the instrument.
3. To clear the way for sliding out the transformer (see Step 8] loosen the power supply cables by forcing them out of the two plastic clamps and removing the screws in two other plastic clamps (see Fig. 4.6).


Fig. A.6. Powar tianiformer replacemant tphata taken with hinged power chassla awung opanl.


Fig. 4-7. CRT filament lead lacalions ILower Beaml.
4. Remove bolh vertical plug-ins from the instrument.
5. Remove the two screwe holding the right plug-in transient response compensation switch (Fig. 4.6). The switch can now be dropped slightly to clear the power Iransformer mounting brackets.
6. Remove 4 power fransformer mounting brackel screws (2 in each plug-in compartment).


Fig 4-8. CRT Illament lead lecailoni IUpper Baml.
7. Unsolder 2 wires from each high voliage compariment, as shown in Fig. 4.7 for tho Lower Beam, and Fig. 4.8 for the Upper Beam. Thase wires aro the filament leads to the CRT and are color coded as shown on Fig. 4-7 and 4.8.
8. The Iransformer can now be slid out of the instrumani, using the slack created by loosaning the cables (as described in slop 3).

## CAUTION

The CRT and Power Transformer are isolaled by a special melal having unique shielding properties. Also, ather painted shields inside the instrument are made of this special metal. Deforming these shialds by culting, bending, or subjecting them to sevare mechanical shocks will destroy the magnetic shielding properties of the melal.
9. The new Iransformar may be installad by reversing the procedures. Refer to the color coding information shown in Figs. 4.7, 4.8 and 4-15.

## TROUBLESHOOTING

## Introduction

The following information is provided to facilitale troubleshooling of the Type 556. Information contained in other sections of this manual should be used in conjunction with the following information to aid in locating the defective componenl.

## Troubleshooting Aids

Diagrams. Circuit diagrams are shown on foldoul pages in Section 9. The circuip number and electrical value of each
component in this instrument are indicated on the diagrams. Important voltages and waveforms are also shown.

Component Numbering. Each main circuit in the instrument is assigned a series of circuit numbers. Table 4-2 lists

TABLE 4-2
Circuit Numbered Location

| Circuit No. | Diagram |
| :---: | :---: |
| 1-189 | Left Vertical Amplifier |
| 200-479 | Right Vertical Amplifier |
| 500-565 | 'A' Sweep Trigger |
| 566-695 | 'A' Sweep Generator \& Timing Switch |
| 700-765 | 'B' Sweep Trigger |
| $766-895$ | 'B' Sweep Generator \& Timing Switch |
| 900-945 | Delay Pickoff |
| 1000-1079 | Alternate Trace Logic and Blanking |
| 1100-1199 | Upper Beam Horizontal Amplifier |
| 1200-1299 | Lower Beam Horizontal Amplifier |
| 1300-1399 | Cathode-Ray Tube Circuit |
| 1400-1519 | Power Supply |
| 1525-1545 | Heater Wiring |
| 1550-1599 | Plug-in Jack Details |
| 1600-1659 | Calibrator |

the main circuits in the Type 556 and the series of circuit numbers assigned to each. For example, a resistor numbered R930 is identified as a component in the Delay Pickoff circuit.

Switch Wafer Identification. Switch wafers shown on the diagrams are coded to indicate the position of the wafer in the complete switch assembly. The numbered portion of the code refers to the wafer number counting from the front, or mounting end of the switch, toward the rear. The letters ' $F$ ' and ' $R$ ' indicate whether the front or the rear of the wafer performs the particular switching function. For example, a wafer designated $2 R$ indicates that the rear of the second wafer is used for this particular switching function.

Circuit Boards. Figs. 4-11 through $4-16$ show the individual boards, with the circuit numbers for each component identified for each board. The circuit board sections of the diagrams are outlined in blue, to aid in locating components.

Wiring Color Code. All insulated wire used in the Type 556 is color-coded according to the EIA standard color code (as used for resistors) to facilitate circuit tracing. The widest color stripe identifies the first color of the code. Power supply voltages can be identified by three color stripes and the following background color code: white, positive voltage; tan, negative voltage. Table $4-3$ shows this wiring color code (with exceptions) for the power supplies in the Type 556. The remainder of the wiring in the Type 556 is color coded, vary-


Fig. 4-9. Color coding of metal-film resistors.
ing from a solid color and no stripes, to a solid color and one or more stripes, as an aid in point-to-point circuit tracing.

TABLE 4-3
Power Supply Wiring

| Supply | Back- <br> ground <br> Color | 1st <br> Stripe | 2nd <br> Stripe | 3rd <br> Stripe |
| :---: | :---: | :---: | :---: | :---: |
| -150 V | Tan | Brown | Green | Brown |
| $+6 \mathrm{~V}^{1}$ | White | Blue |  |  |
| $+10 \mathrm{~V}^{1}$ | White | Brown |  |  |
| +100 V | White | Brown | Black | Brown |
| +225 V | White | Red | Red | Brown |
| +350 V | White | Orange | Green | Brown |

${ }^{1}$ Exception: Color code partially conforms to EIA standard.
Resistor Color Code. A number of precision metal-film resistors are used in this instrument. These resistors can usually be identified by their gray body color. If a metalfilm resistor has a value indicated by three significant figures and a multiplier, it will be color coded according to the EIA standard resistor color code. If it has a value indicated by four significant figures and a multiplier, the value will be printed on the body of the resistor. For example, a $333 \mathrm{k} \Omega$ resistor will be color coded, but a $333.5 \mathrm{k} \Omega$ resistor will have its value printed on the resistor body. The color code sequence is shown in Fig. 4-9.

Composition resistors are color coded according to the EIA standard resistor color code.

## Troubleshooting Techniques

This troubleshooting procedure is arranged in an order which checks the simple trouble possibilities before proceeding with extensive troubleshooting. The first few checks assure proper connection, operation and calibration. If the trouble is not located by these checks, the remaining steps aid in locating the defective component. When the defective component is located, it should be replaced following the replacement procedures given in this section.

## NOTE

> Check all fuses. Often a blown fuse cannot be detected by visual means. The ratings and locations of fuses are shown in Table 4-1 and Figs. $4-3$ and 4-4.

1. Check Associated Equipment. Before proceeding with troubleshooting of the Type 556, check that the equipment used with the Type 556 is operating correctly. Check that the signal is properly connected and that the interconnecting cables or probes are not defective. Also, check the power source.
2. Check Control Settings. Incorrect control settings can indicate a trouble that does not exist. For example, incorrect setting of the A or B TIME/CM VARIABLE controls appears as an uncalibrated sweep; incorrect setting of the Triggering controls appears as a defective sweep or trigger circuit; incorrect setting of the Variable Volts/cm controls appears as incorrect gain, etc. If there is any question about the correct function
or operation of any control, see the Operating Instructions section of this manual.

Incorrect operation of all eircuits often indicates trouble in the Low Voltage Power Supply. Check first for correct adjustment of the individual supplies. However, a defective component elsewhere in the instrument can appear as a power supply trouble and may affect the operation of other circuits.

Table 4-4 lists the tolerances of the power supplies in the Type 556. If a power supply voltage is within the listed tolerance, the supply can be assumed to be working correctly. If outside the tolerance, the supply may be misadjusted or operating incorrectly. Use the procedure given in the Calibration section to adjust the power supplies.

TABLE 4-4
Power Supply Tolerances

| Voltage | Tolerance |
| :---: | :---: |
| -150 V | $\pm 1.5 \mathrm{~V}$ |
| +100 V | $\pm 1.0 \mathrm{~V}$ |
| +225 V | $\pm 0.625 \mathrm{~V}$ |
| +350 V | $\pm 10.5 \mathrm{~V}$ |

${ }^{2}$ Measured between +100 and +225 V.
3. Check Instrument Calibration. Check the calibration of the instrument, or the affected circuit if the trouble exists in one circuit. The indicated trouble may only be a result of misadjustment or may be corrected by calibration. Complete instructions are given in the Calibration section of this manual. Individual calibration steps can be performed out of sequence. However, if the circuit affects the calibration of other circuits in the instrument, a more complete calibration will be necessary. General Information in the Calibration section describes how calibration steps which interact are noted.
4. Isolate trouble to a particular circuit. The Type 556 incorporates a significant feature in its design that greatly simplifies the isolation of a trouble to a particular circuit. This feature is the built-in versatility of the instrument which incorporates two independent vertical and horizontal deflection systems (with the exception of the low voltage and CRT circuits). The vertical input circuits are mounted in plugin units that can be quickly replaced or extended to facilitate isolation and troubleshooting. In addition, the time base circuits can be switched by front panel controls so the Upper Beam can be operated by either the A or B time base generator, and the Lower Beam by the B Time Base generator.
An example using the front-panel controls is as follows: Supposing the A Sweep Generator is suspect because the sweep will not trigger. Since the A Sweep Trigger is connected to the A Sweep Generator, the A Sweep Trigger circuit could also be at fault. To substitute these circuits, set the Upper Beam DISPLAY switch to LEFT PLUG-IN B and the B Triggering SOURCE switch to LEFT INT NORM. Now the B Sweep Trigger and B Sweep Generator can be used to check whether an Upper Beam display can be obtained.

Another example using the front-panel controls is as follows (but this time a coaxial paich cord is also used): Suppose the Lower Beam Horizontal Amplifier is suspect. In this case the Lower Beam DISPLAY switch can be set to RIGHT PLUG-IN

TABLE 4-5
Circuit Interconnections

|  |  | Pwr. Sup. | $\begin{gathered} \text { Htr. } \\ \text { Wrg. } \end{gathered}$ |  | R <br> Vert. <br> Amp. | A Swp. Trig. | A <br> Swp. <br> Gen. | B <br> Swp. <br> Trig. | B <br> Swp. <br> Gen. | $\begin{aligned} & \text { Dly. } \\ & \text { P. O. } \end{aligned}$ | Alt. Trace Logic \& Blkg. | Upr. Beam Horiz. Amp. | Lwr. Beam Horiz. Amp. | CRT Circuit |  | Calib. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | Upr. Beam | Lwr. Beam |  |
| Power Supply |  | X | X | $X$ | $X$ | $X$ | X | X | $X$ | X | X | $X$ | X | X | $X$ | $X$ |
| Heater | Wiring | X | X | $X$ | X | X | X | X | X | X | X | X | $X$ | X | X | $X$ |
| Left Ve Amplifi |  | X | X | X | X | X |  |  |  |  |  |  |  | X |  |  |
| Right V <br> Amplifi | $\begin{aligned} & \text { ertical } \\ & \hline \end{aligned}$ | X | X | X | X |  |  | X |  |  |  |  |  |  | X |  |
| A Swee Trigger |  | X | X | X |  | X | X |  |  |  |  |  |  |  |  |  |
| A Swee Genera |  | X | X |  |  | X | X |  |  | X | X | X |  |  |  |  |
| $\begin{aligned} & \text { B Swee } \\ & \text { Trigger } \\ & \hline \end{aligned}$ |  | X | X |  | X |  |  | X | X |  |  |  |  |  |  |  |
| B Swee Genera |  | X | X |  |  |  |  | X | X | X | X |  | X |  |  |  |
| Delay Pickoff |  | X | X |  |  |  | X |  | X | X |  |  |  |  |  |  |
| Alterna Logic Blankin | e Trace and | X | X |  |  |  | X |  | X |  | X |  |  |  |  |  |
| Upper zontal | Beam HoriAmplifier | X | X |  |  |  | X |  |  |  |  | X |  | X |  |  |
| Lower zontal | Beam HoriAmplifier | X | X |  |  |  |  |  | X |  |  |  | X |  | X |  |
| CRT | Upper Beam | X | X | X |  |  |  |  |  |  |  | X |  | X | X |  |
| Circuit | Lower Beam | X | X |  | X |  |  |  |  |  |  |  | X | X | X |  |
| Calibra |  | X | X |  |  |  |  |  |  |  |  |  |  |  |  | X |

EXT and a patch cord can be connected from the A SAWTOOTH connector through an attenuator to the LOWER BEAM EXT HORIZONTAL IN connector. Now the A sweep can be used to drive the Lower Beam Horizontal Amplifier to check whether a normal trace can be obtained.

Thus the system can usually be used to check for the isolation of a trouble to a particular circuit. If one beam is operating properly, it can be used to signal-trace the defective circuit.

The Type 556 can be used to signal-trace all of its own circuits except:

1. Lower Beam CRT Circuit.
2. Alternate-Trace Lagic Circuit (Q1004, Q1015, and Q1025).

## 3. Power Supply Circuit.

The signal-tracing is done in the following manner:
The Upper Beam side of the oscilloscope is used to signaltrace all of the Lower Beam circuits except the Lower Beam CRT circuit. The Upper Beam can also be used to check ripple in the Low Voltage Power Supply (when the supplies are regulating) and to signal-trace the Calibrator circuit.

The Lower Beam side of the oscilloscope can be used to signal-trace all of the Upper Beam circuits and the Delay Pickoff circuit.

For checking the Lower Beam CRT and Alternate-Trace Logic circuits, a test oscilloscope is required. The test oscilloscope should have a frequency response of $D C$ to 10 MHz or higher and a minimum deflection factor of $0.05 \mathrm{~V} / \mathrm{cm}$ when using a $10 \times$ probe. To show time relationship in the AlternateTrace Logic Circuit, the test oscilloscope should be externally triggered by the A GATE signal from the Type 556.

The Type 556 contains 15 main circuits. The normal interconnections between these circuits is given in Table 4-5 to aid in circuit isolation. Since the table lists only the main circuits, all interconnections may not be indicated.

To isolate a trouble to a circuit, note the trouble symptom. The symptom often identifies the circuit in which the trouble is located. For example, poor focus of both beams indicates that the CRT circuit (includes high voltage) is probably at fault. When trouble symptoms appear in more than one circuit, or if the trouble is not located in the circuit which indicates the trouble, Table 4-5 may aid in locating the cause of the trouble. To use the table, find the vertical line which shows the circuit(s) affected. Check the first circuit listed in the left column. If this circuit is not the source of the trouble, check the next circuit listed in the left column
which interacts, etc. Methods of checking the defective circuits after they have been located are given in steps 5 through 8.

The pin connectors used to connect the circuit boards to the instrument provide a convenient means of circuit isolation. For example, a short in a power supply can be isolated to the Low-Voltage Power Supply by disconnecting pin connectors for that voltage at the boards.
After the defective circuit has been located, proceed with steps 5 through 8 to locate the defective component(s). If the trouble has not been isolated to a circuit using the procedure described here, check the voltages and waveforms as explained in step 7 to locate the defective circuit.
5. Check Circuit Board connections. If the trouble is isolated to a circuit board that has push-on connectors, check the connectors on the circuit board for correct connection. Figs. 4-11 through 4-16 shows the correct connections for each of these boards.
6. Visual Check. Visually check the circuit in which the trouble has been located. Many troubles can be located by visual indications such as broken wires, damaged circuit boards or damaged components.
7. Check Voltages and Waveforms. Often the defective components can be located by checking for the correct voltage or waveform in the circuit. Typical voltages and waveforms are given on the Schematic Diagrams.

## NOTE

Voltages and waveforms given on the diagrams may vary slightly between instruments. To obtain operating conditions similar to those used to take readings, see the IMPORTANT note on the foldout portion to the left of the Vertical Block Diagram. In addition, refer to the diagram for the circuit being checked.

## CAUTION

When troubleshooting the circuits, be sure the probe tip or test prods can be used in tight places without causing an accidental short circuit. If care is not used, a short circuit can cause damage to several semiconductors; particularly in the vertical amplifiers.

The waveforms on the schematic diagrams are shown in three configurations, depending on whether the Upper Beam section, the Lower Beam section, or a separate test oscilloscope is used to obtain the particular waveform. The Type 556 graticule is shown with its eight vertical divisions, whereas the separate test oscilloscope is shown with six vertical divisions. The waveforms obtained with the Upper Beam display are shown in the upper part of the eight-division graticule and the Lower Beam displays are located in the lower portion of the graticule. The displays obtained by using the separate test oscilloscope are generally near the center of the six vertical divisions graticule. See the illustrations, Fig. 4-10.

Voltage measurements should be taken with a $20,000 \mathrm{ohm} /$ volt DC meter. Accuracy of the voltmeter should be within $3 \%$ on all ranges. The test prods should be well insulated to avoid shorting of components adjacent to the test point.


Fig. 4-10. Waveform source identification.
8. Check Individual Components. The following procedures describe methods for checking individual components in the Type 556. Components which are soldered in place can be checked more easily by disconnecting one end. This eliminates incorrect measurements due to the effects of surrounding circuitry.

Transistors and Tubes. The best check of transistor or tube operation is a performance check under actual operating conditions. If a transistor or tube is suspected of being defective, it can best be checked by substituting a new component or one which has been checked previously. However, be sure that circuit conditions are not such that the replace-

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ment transistor or tube might also be damaged. If substitute transistors or tubes are not available, a dynamic tester may be used (such as Tektronix Type 570 or 575). Static type testers are not recommended, however, since they do not check operation under simulated operating conditions.

## NOTE

Two small access plates have been provided inside each plug in compartment to allow easy inspection or replacement of the A and B Sweep Generator tubes V625 and V825.

## CAUTION

Care should be exercised when replacing plasticcased transistors, as two types of lead configurations are manufactured. If in doubt as to the correct lead nomenclature, refer to the manufacturer's basing diagrams. Some transistors have the lead code ( $E, B, C$ ) marked on the case. All transistor sockets in this instrument are wired for the lead configuration used in metal-cased transistors.

Diodes. A diode (excluding the tunnel diodes, zener diodes and the silicon diodes in the CRT circuit) usually can be checked for an open or shorted condition by measuring the resistance between terminals. With an ohmmeter scale having an internal source of about 1.5 volts, the resistance should
be very high in one direction and very low when the leads are reversed.

## CAUTION

Do not use an ohmmeter scale that has a high internal current. High currents may damage the diode. Do not measure tunnel diodes with an ohmmeter; use a dynamic tester (such as Tektronix Type 575 Transistor-Curve Tracer).

Resistors. Resistors can be checked with an ohmmeter. Check the Electrical Parts List for the tolerance of the resistors used in this instrument. Resistors normally do not need to be replaced unless the measured value varies widely from the specified value.

Inductors. Check for open inductors by checking continuity with an ohmmeter. Shorted or partially shorted inductors can usually be found by checking the waveform response when high-frequency signals are passed through the circuit. Partial shorting often reduces high-frequency response (rolloff).

Capacitors. A leaky or shorted capacitor can best be detected by checking resistance with an ohmmeter on the highest scale. Do not exceed the voltage rating of the capacitor. The resistance reading should be high after initial charge of the capacitor. An open capacitor can best be detected with a capacitance meter or by checking whether the capacitor passes $A C$ signals.

NOTES

## NOTES

## SECTION 5

## PERFORMANCE CHECK

Change information, if any, affecting this section is found at the rear of the manual.

## Introduction

This section of the manual provides a means of rapidly checking the performance of the Type 556. It is intended to check the calibration of the instrument without the need for performing the complete Calibration Procedure. The Performance Check does not provide for the adjustment of any internal controls. Failure to meet the requirements given in this procedure indicates the need for internal checks or adjustments, and the user should refer to the Calibration Procedure in this manual.

## Recommended Equipment

The following equipment is recommended for a complete performance check. Specifications given are the minimum necessary to perform this procedure. All equipment is assumed to be calibrated and operating within the original specifications. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

For the most accurate and convenient performance check, special calibration fixtures are used in this procedure. These calibration fixtures are available from Tektronix, Inc. Order by part number through your local Tektronix Field Office or representative.

1. Test oscilloscope. Bandwidth, DC to $10 \mathrm{MHz}_{i}$ minimum deflection factor, 0.005 volts/division; $1 \times$ and $10 \times$ probes. Tektronix Type 531A Oscilloscope recommended, with Type $W$ plug-in.
2. $10 \times$ probe with BNC connector. Tektronix Type P6006 recommended. Part No. 010-0128-00.
3. $1 \times$ probe with BNC connector. Tektronix Type P6028 recommended. Part No. 010-0120-00.
4. Time-mark generator. Marker outputs, 5 seconds to 0.1 microsecond; sine-wave output at 50 MHz . Tektronix Type 184 recommended.
5. Constant-amplitude sine-wave generator. Frequencies, 50 kHz and 350 kHz up to $\geq 50 \mathrm{MHz}$; output amplitude, at least 1 volt; amplitude accuracy, $\pm 5 \%$ into $50 \Omega$ load. Tektronix Type 191 recommended.
6. Test load and pulser unit. Tektronix Calibration Fixture, Part No. 067-0521-00 (2 required).
7. Amplitude calibrator. Amplitude accuracy, within $0.25 \%$; signal amplitude, 0.1 volt to 100 volts; output signal, 1 kHz square-wave and $+D C$; must have mixed display feature. Tektronix Calibration Fixture 067-0502-00 recommended.
8. Variable autotransformer. Must be capable of supplying 1 kVA over a voltage range of 90 to 130 VAC $(182$ to 260 volts for 230 -volt nominal line). If autotransformer does not have an AC voltmeter (RMS), monitor the output with a voltmeter having a range of at least 130 volts (or 260 volts). For
example, General Radio W10MT3W Metered Variac Autotransformer.
9. Plug-in preamplifiers with dual-channel inputs, vertical deflection sensitivity to 5 millivolts $/ \mathrm{cm}$. Tektronix Type 1A1 or equivalent, 2 required. Include one 18 -inch $50 \Omega$ cable (Tektronix Part No. 012-0076-00).
10. Low-frequency sine-wave signal generator, 30 Hz to $60 \mathrm{kHz}, 1$ volt output, Heathkit Model 1G-72 or equivalent.
11. Current probe. Sensitivity, 1 milliamp/division; accuracy within 3\%. Tektronix P6019 Current Probe with Type 134 Amplifier recommended.
12. 3-wire power socket assembly (required only if autotransformer is equipped with a single output power socket). Tektronix Part No. 136-0102-00.
13. 3 -wire power cable 20 inches long (required only if autotransformer is equipped with a single output power socket). Tektronix Part No. 161-0014-00.
14. Precision 50 -ohm termination. For example, Tektronix Calibration Fixture Part No. 067-0515-00.
15. 50 -ohm terminations; accuracy, $3 \%$; BNC connectors. Tektronix Part No. 011-0049-00; two required.
16. BNC T connector. Tektronix Part No. 103-0030-00.
17. Adapter. Connectors, GR to BNC jack. Tektronix Part No. 017-0063-00.
18. Cable. Impedance, 50 ohm; type, RG58A/U; length, 42 inch; connectors, BNC. Tektronix Part No. 012-0057-00. Four required.
19. Patch cord, 18 inch with BNC plug-jack terminals on each end. Tektronix Part No. 012-0087-00.

## PERFORMANCE CHECK PROCEDURE

## General

In the following procedure, test equipment connections or control settings should not be changed except as noted. If only a partial check is desired, refer to the preceding step(s) for setup information.

The following procedure uses the equipment listed under "Recommended Equipment". If substitute equipment is used, control settings or setup must be altered to meet the requirements of the equipment used.

## Preliminary Procedure

1. Install the test load units in the oscilloscope plug-in compartments.
2. Connect the Type 556 to the autotransformer and connect the autotransformer to a line voltage within the regulating range of the oscilloscope power supplies.

## Performance Check-Type 556

3. Set the Type 556 Upper and Lower Beam INTENSITY controls fully counterclockwise.
4. Set the Type 556 POWER switch to $O N$ and set the autotransformer for 115 VAC (or 230 VAC ).
5. Allow 20 minutes for instrument warmup. Meanwhile, set the remaining controls as follows:

| A Triggering Controls |  |
| :---: | :---: |
| SOURCE | NORM INT LEFT |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Clockwise, pushed in |
| Upper Beam Controls |  |
| DISPLAY | LEFT PLUG-IN A |
| POSITION | Mid-range |
| DISPLAY MAG | $\times 1$ |
| FOCUS | Adjust for best display |
| ASTIGMATISM | Adjust for best display |
| CONTRAST | Clockwise |
| UPPER BEAM EXT HORIZ VAR 10-1 | Clockwise |
| A Sweep Controls |  |
| A TIME/CM | 0.5 mSEC |
| VARIABLE | CALIBRATED |
| A MODE | NORM |
| B Triggering Controls |  |
| SOURCE | NORM INT RIGHT |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Clockwise, pushed in |
| Lower Beam Controls |  |
| DISPLAY | RIGHT PLUG-IN B |
| POSITION | Mid-range |
| DISPLAY MAG | $\times 1$ |
| FOCUS | Adjust for best display |
| ASTIGMATISM | Adjust for best display |
| CONTRAST | Clockwise |
| LOWER BEAM EXT HORIZ VAR 10-1 | Clockwise |
| B Sweep Controls |  |
| B TIME/CM | 0.5 mSEC |
| VARIABLE | CALIBRATED |
| B MODE | NORM |
| SCALE ILLUMINATION | Adjusted to illuminate graticule lines |
| TRACE SEPARATION | Mid-range |
| DELAY-TIME MULTIPLIER | 1.00 |
| AMPLITUDE CALIBRATOR | OFF |


| Rear Panel Controls |  |
| :--- | :--- |
| Upper Beam CRT Cathode | EXT CRT CATHODE |
| Selector |  |
| Lower Beam CRT Cathode <br> Selector | EXT CRT CATHODE |

Test Load Units (both)

| Test Function | Low Load |
| :--- | :--- |
| Variable | mid-range |
| Amplitude | mid-range |
| Vertical Position | mid-range |
| Repetition Rate | Low |

## 1. Check Amplitude Calibrator Operation

a. Requirement-Voltage accuracy, $\pm 2 \%$; terminated voltage accuracy, one-half of indicated voltage $\pm 2 \%$; repetition rate, $1 \mathrm{kHz} \pm 25 \%$; duty cycle, 45 to $55 \%$; risetime, 1.5 microseconds or less.
b. Set the AMPLITUDE CALIBRATOR to 100 VDC, and connect a $50 \Omega$ cable from the CAL OUT connector to the Standard Amplitude Calibrator Unknown Input connector.
c. Set the test oscilloscope time/cm switch to 50 microsecond.
d. Set the Type $W$ plug-in unit as follows:

| Input Atten | 100 |
| :--- | :--- |
| Channel A Ac-Dc-Gnd | Dc |
| Channel B Ac-Dc-Gnd | Gnd |
| Millivolts/cm | 10 |
| Display | A-Vc |
| Vc Range | +1.1 |
| Comparison Voltage (Vc) | 10.00 |
| NOTE |  |

Familiarity with the operation of the Type $W$ plug-
in unit is a prerequisite to the use of this procedure.
e. Set the Standard Amplitude Calibrator to 100 Volts + DC Mixed, and connect a 50 -ohm cable from the Output connector to the Type $W$ Channel A input connector.
f. Adjust the test oscilloscope for a free-running display. With correct adjustment of the Type $W$, the display will be on or near the reference level established by the Comparison Voltage.
g. Check-Separation of the display traces (see Fig. 5-1) not more than $2 \mathrm{~cm}( \pm 2 \%)$. A single trace indicates that the AMPLITUDE CALIBRATOR voltage and the Standard Amplitude Calibrator voltage are equal.
h. Set instrument controls as indicated in Table 5-1, checking for tolerances as shown.
i. Change the AMPLITUDE CALIBRATOR to .2 VOLTS, and the Standard Amplitude Calibrator to 1 Volts.
i. Insert the precision termination (listed under Recommended Equipment, item 14) between the Type 556 CAL OUT connector and the 50 -ohm cable, using adapters as necessary.

TABLE 5-1
Calibrator Amplitude Accuracy Check

| AMPLITUDE CALIBRATOR | Standard Amplitude Calibrator |  | Millivolts/cm | W control | gs <br> Comparison Voltage ( Vc ) | Tol. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Input Atten |  | Vc Range |  |  |
| 100 V DC | $\begin{aligned} & 100 \text { Volts } \\ & +D C \end{aligned}$ | 100 | 10 | +1.1 | 10.000 | 2 cm |
| 100 VOLTS | 100 Volts (square wave) | 100 | 10 | +1.1 | 10.000 | 2 cm |
| 50 | 50 | 100 | 5 | +1.1 | 5.000 | 2 cm |
| 20 | 20 | 100 | 2 | $+1.1$ | 2.000 | 2 cm |
| 10 | 10 | 10 | 10 | +1.1 | 10.000 | 2 cm |
| 5 | 5 | 10 | 5 | +1.1 | 5.000 | 2 cm |
| 2 | 2 | 10 | 2 | +1.1 | 2.000 | 2 cm |
| 1 | 1 | 1 | 10 | +1.1 | 10.000 | 2 cm |
| . 5 | . 5 | 1 | 5 | +1.1 | 5.000 | 2 cm |
| . 2 | . 2 | 1 | 2 | +1.1 | 2.000 | 2 cm |
| . 1 | . 1 | 1 | 1 | +1.1 | 1.000 | 2 cm |
| 50 mVOLTS | 50 mV | 1 | 1 | +1.1 | 0.500 | 1 cm |



Vertical sensitivity, 1 volt/cm.

Fig. 5-1. Amplitude Calibrator accuracy check.
k. Change the Type $W$ Comparison Voltage (Vc) dial to 1.000 .

1. Check-Separation of display traces not more than 2 cm .
m . Remove the Standard Amplitude Calibrator signal, and remove the precision termination.
n. Change the Type $W$ Vc Range switch to 0.
o. Connect an 18 -inch 50 -ohm cable (furnished with the Type 1A1, see item 9) from the CAL OUT connector to the Type W Channel A input connector, set the Input Atten switch to 100 , and the Millivolts/cm to 5 .
p. Set the AMPLITUDE CALIBRATOR switch to 2 VOLTS
q. Set the test oscilloscope time/cm to 0.2 milliseconds, and obtain a stable display.
r. Check-l cycle of the displayed waveform between 3.75 cm and 6.25 cm in length.
s. With the vertical deflection factor of the plug-in unit at 0.5 volts $/ \mathrm{cm}$, obtain a stable display at a sweep rate of 0.1 milliseconds $/ \mathrm{cm}$.
t. With the test oscilloscope positioning control, move the display so that the rising portion of the display coincides with the $1-\mathrm{cm}$ vertical graticule line.
u. Change the display length with the time $/ \mathrm{cm}$ variable control, so that one cycle of the display is 8 cm long.
v. Check-Falling portion of the waveform not more than 4 mm either side of the graticule center vertical line (duty cycle 45 to $55 \%$ ).
$w$. Return the variable time/cm control to the calibrated position.
$x$. Change the AMPLITUDE CALIBRATOR to 5 VOLTS.
y. Adjust the display amplitude to 5 cm with the Variable Millivolts/cm control.
z. Set the test oscilloscope time/cm to 0.2 microseconds, and adjust the triggering level control to display the full rising portion of the waveform.
aa. Adjust the horizontal and vertical Position controls simultaneously so that the $10 \%$ point of the rising portion of the waveform crosses an intersection of a vertical and a horizontal graticule line (see Fig. 5-2).
ab. Measure the horizontal distance between the $10 \%$ and $90 \%$ points on the rising portion of the waveform.
ac. Check-Risetime 1.5 microseconds or less.
ad. Change the test oscilloscope vertical deflection factor to 10 volts $/ \mathrm{cm}$.
ae. Change the AMPLITUDE CALIBRATOR to 100 VOLTS.
af. Adjust the display as in steps $(z)$ and (aa), with an amplitude of 5 cm .


Fig. 5-2. Typical display, amplitude calibrator risetime. Indicated risetime is $\mathbf{0 . 8}$ microseconds.
ag. Check-Risetime 1.5 microseconds or less.
ah. Remove the 50 -ohm cable.

## 2. Check 5 mA Current Loop

a. Requirement- 5 mA current indication in current loop.
b. Connect the Type 134 Amplifier and P6019 Currentmeasuring Probe to the vertical input of the test oscilloscope.
c. Set the Type 134 Amplifier attenuator to $2 \mathrm{~mA} /$ div.
d. Change the test oscilloscope vertical deflection Volts/ cm switch to 50 millivolts $/ \mathrm{cm}$.
e. Clip the probe to the current loop on the front panel of the Type 556.
f. Rotate the AMPLITUDE CALIBRATOR switch through all positions, noting that no waveform is displayed at any position except the 5 mA setting.
g. Check-Display amplitude of approximately 2.5 cm at the 5 mA switch position.
h. Remove the Type 134 Amplifier and Current-measuring Probe.

## 3. Check Trace Rotation

a. Requirement-Traces can be adjusted parallel to the horizontal graticule lines.
b. Position the Upper and Lower Beam traces to their respective graticule center horizontal lines with the traces starting at the $0-\mathrm{cm}$ graticule lines.
c. With a small screwdriver, adjust the TRACE ROTATION control.
d. Check-Traces can be adjusted parallel to the horizontal graticule lines.

## 4. Check Beam Finder Operation

a. Requirement-Overscanned display returns to the display area when the BEAM FINDER button is depressed.
b. Depress the BEAM FINDER button and hold in this position.
c. Rotate first the right and left vertical position controls fully clockwise and counterclockwise, and then the Upper Beam and Lower Beam POSITION controls, while observing the position of both displays.
d. Check-Both displays should remain within the graticule viewing areas while the BEAM FINDER button is depressed.

## 5. Check Geometry

a. Requirement-Alignment of markers with the vertical graticule lines within 1 mm .
b. Remove both Test Load units, and in their places install Type 1Al plug-in units.
c. Apply 1 -millisecond markers from the time-mark generator (item 4 of Recommended Equipment) through a BNC T connector, two $50 \Omega$ cables and $50 \Omega$ terminations to the Type 1 Al vertical inputs of both plug-ins.
d. Check that the $A$ and $B$ TIME/CM switches are set to .5 mSEC .
e. Adjust both plug-in variable volts/cm controls so that the displays over-scan both Upper and Lower Beam respective graticule areas.
f. Pull the A and B LEVEL control knobs outward and adjust the $A$ and $B$ Triggering controls for stable displays on both beams.
g. Adjust both plug-in vertical position controls so that the time-mark base line is below the viewing areas for the two beams.
h. Adjust the Upper and Lower Beam POSITION controls so that the first time marks for both beams are superimposed at the left-hand $(0-\mathrm{cm})$ vertical graticule line.
i. Adjust the A and B TIME/CM VARIABLE controls for one time mark per cm on both displays. Time marks will now be superimposed over the entire graticule area.
i. Check-Maximum deviation of the traces from vertical graticule lines should not exceed 1 mm . See Fig. 5-3 for examples of geometry adjustment.
k. Disconnect the marker signals and position the Lower Beam trace to the bottom graticule line. Check for vertical trace deviation (bowing or tilt) of not more than 1 mm .
I. Position the Upper Beam trace to the top graticule line and check for vertical trace deviation (bowing or tilt) of not more than 1 mm .
m. Set the $A$ and $B$ TIME/CM VARIABLE controls to CALIBRATED.

## 6. Check Focus and Astigmatism Control Operation

a. Requirement--Sharp, well-defined display.
b. Apply 100 -microsecond markers to both plug-in unit vertical inputs.

(A) Poor Geometry

(B) Good Geomelry

Fig. 5-3. Typical CRT displays showing (A) poor geometry adjustment; (B) good geometry adjustment.
c. Adjust both plug-in unit vertical position controls so that the time-mark base lines are below the viewing areas for the beams.
d. Check-Well-defined markers with optimum settings of the FOCUS and ASTIGMATISM controls. (When making the check, the INTENSITY controls can be set so one display at a time is viewed.)

## 7. Check Upper and Lower Beam Scan Areas

a. Requirement-6 $\times 10 \mathrm{~cm}$ scan area for each beam.
b. Change both $A$ and $B$ TIME/CM switches to .1 mSEC .
c. Set the time-mark generator for 1-microsecond markers.
d. Turn the Upper Beam INTENSITY control so that the Upper Beam display is no longer visible.
e. Adjust the right plug-in vertical deflection factor so that the raster produced by the markers over-scans the Lower Beam graticule area.
f. Check-The scan area equals or exceeds $6 \times 10 \mathrm{~cm}$.
g. Extinguish the Lower Beam display with the INTENSITY control and turn the Upper Beam INTENSITY control to produce a display on the Upper Beam.
h. Check-The Upper Beam scan area equals or exceeds $6 \times 10 \mathrm{~cm}$.

## 8. Check CRT Orthogonality

a. Requirement-Angle between horizontal and vertical traces 90 degrees $\pm 1 \mathrm{~mm}$.
b. Set the A TIME/CM switch to 1 mSEC .
c. Set the time-mark generator for 1 -millisecond and 0.1 millisecond markers.
d. Adjust the A Triggering controls for a stable display.
e. Position an Upper Beam 1-millisecond marker at the intersection of a vertical graticule line and the horizontal graticule line 3 cm below the Upper Beam graticule center horizontal line.
f. Check—The adjacent 0.1 millisecond marker should not cross the Upper Beam graticule center vertical line at the point 3 cm above the Upper Beam graticule center horizontal line.
g. Repeat steps (b) through (f) for the Lower Beam.
h. Disconnect the time markers.

## 9. Check Vertical Amplifier DC Balance-Right and Left

a. Requirement-Traces within 1 cm of graticule center line with common-mode input.
b. Replace the Type 1 Al plug-ins with two test load units. Allow at least three minutes for the Type 556 to stabilize.
c. Set the test load unit Test Function switches to Common Mode.
d. Check-Upper and Lower Beams traces within 1 cm of the respective center lines of the Upper and Lower Beam graticule areas.

## 10. Check Trace Separation Range

a. Requirement-The TRACE SEPARATION control should have sufficient range to superimpose the Upper Beam trace on the Lower Beam trace within the center $4-\mathrm{cm}$ area of the graticule.
b. Change the Upper Beam DISPLAY switch to RIGHT PLUG-IN A.
c. Change the right plug-in unit Test Function to Low Load.
d. Using the right plug-in unit Vertical Position control, position the Lower Beam trace to coincide with the horizontal graticule line located $1-\mathrm{cm}$ below the Lower Beam graticule center horizontal line.
e. Using the TRACE SEPARATION control, position the Upper Beam trace so it is superimposed on the Lower Beam trace.
f. Check-The TRACE SEPARATION control should have sufficient range to superimpose the Upper Beam trace on the Lower Beam trace within the center $4-\mathrm{cm}$ area of the graticule.

## 11. Check Vertical Amplifier Gain

a. Requirement-Vertical deflection accuracy $\pm 3 \%$.
b. Set the controls as follows:

| A Triggering Controls |  |
| :---: | :---: |
| SOURCE | LEFT INT NORM |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Clockwise, knob pulled outward |
| Upper Beam DISPLAY | LEFT PLUG-IN A |
| Upper Beam DISPLAY MAG | $\times 1$ |
| A TIME/CM | . 1 mSEC |
| A VARIABLE | CALIBRATED |
| B Triggering Controls |  |
| SOURCE | RIGHT INT NORM |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Clockwise, knob pulled outward |
| Lower Beam DISPLAY | RIGHT PLUG-IN B |
| Lower Beam DISPLAY MAG | $\times 1$ |
| B TIME/CM | . 1 mSEC |
| B VARIABLE | CALIBRATED |
| B MODE | NORM |
| TRACE SEPARATION | Centered |

Test Load Units (both)
Test Function
Gain Set
c. Set both test load unit Test Function switches to Gain Set.
d. Connect a $50 \Omega$ cable from the Standard Amplitude Calibrator Output connector to the left test load unit Ext Input connector.
e. Check that both $A$ and $B T M E / C M$ switches are set to .1 mSEC .
f. Set the Standard Amplitude Calibrator to supply a $100-\mathrm{V}$ square-wave output.
g. Center the Upper Beam free-running display in the Upper Beam viewing area.
h. Change the B Triggering MODE switch to TRIG. The Lower Beam will no longer be visible.
i. Check-Display amplitude of $4 \mathrm{~cm} \pm 1.2 \mathrm{~mm}$.
i. Remove the calibrator signal from the left plug-in unit and instead, connect the signal to the right plug-in test load Ext Input connector.
k. Change the B Triggering MODE switch to AUTO STABILITY and the A Triggering MODE switch to TRIG. The Lower Beam display will now be the only one visible.
I. Center the Lower Beam free-running display in the Lower Beam viewing area.
m. Check-Display amplitude of $4 \mathrm{~cm} \pm 1.2 \mathrm{~mm}$.
n. Return the A Triggering MODE switch to AUTO STABILITY, and change the Upper Beam DISPLAY switch to RIGHT PLUG-IN A. Both beam displays will again be visible.
o. Decrease the Lower Beam INTENSITY control (counterclockwise rotation) until the Lower Beam display is no longer visible.
p. Use the TRACE SEPARATION control to center the Upper Beam free-running display in the Upper Beam viewing area.
q. Check—Display amplitude of $4 \mathrm{~cm} \pm 1.2 \mathrm{~mm}$.

## 12. Check Vertical Amplifier Compression/Ex-pansion-Left, Right, and Crossover

a. Requirement-No more than 0.5 mm amplitude change in 2 cm signal.
b. Equipment setup remains as in step 11. Change the Standard Amplitude Calibrator to a $50-\mathrm{V}$ square-wave output and apply the signal to the left plug-in unit.
c. Set the Upper Beam DISPLAY switch to LEFT PLUG-IN $A$ and center the $2-\mathrm{cm}$ display in the Upper Beam viewing area. Note the display amplitude.
d. With the left test load unit Vertical Position control, move the 2 cm display to the top 2 cm of the graticule.
e. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$.
f. Move the Upper Beam display so it is centered in the Lower Beam viewing area.
g. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$ with respect to the amplitude noted in step (c).
h. Change the A Triggering MODE switch from AUTO STABILITY to TRIG. The Upper Beam display will now disappear.
i. Apply the Standard Amplitude Calibrator signal to the right plug-in unit.
i. Increase the Lower Beam INTENSITY control (clockwise rotation) until the Lower Beam display is visible.
k. Center the 2 cm display in the Lower Beam viewing area. Note the display amplitude.

1. With the right test load Vertical Position control, move the 2 cm display so it is centered in the Upper Beam viewing area.
m . Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$.
n. Move the 2 cm display to the bottom 2 cm of the graticule.
o. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$ with respect to the amplitude noted in step (k).
p. Return the A Triggering MODE switch to AUTO STABILITY.
q. Set the Upper Beam DISPLAY switch to RIGHT PLUG-IN A. The Upper and Lower Beam displays will now be visible. Decrease the intensity of the Lower Beam display.
r. Using the right test load Vertical Position control, center the Upper Beam 2 cm display in the Upper Beam viewing area. Note the display amplitude.
s. Move the 2 cm display to the top 2 cm of the graticule. Use the right test load Vertical Position control to move the display.
t. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$.
u. Use the right test load Vertical Position control to move the display so it is centered in the Lower Beam viewing area.
v. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$ with respect to the amplitude noted in step (r).

## 13. Check Common Mode Rejection

a. Requirement-Not more than 3 mm vertical deflection with common mode input of 1 volt.
b. Set the Standard Amplitude Calibrator to 1 volt squarewave output.
c. Connect a BNC T connector to the Standard Amplitude Calibrator Output connector. Using $50 \Omega$ cables, apply the signal to both test load Ext Input connectors.
d. Set both the right and left test load unit Test Function switches to Common Mode.
e. Change the Upper Beam DISPLAY switch to LEFT PLUGIN A and increase the intensity of the Lower Beam trace to normal brightness.
f. Check-The signal amplitude on both beam displays not to exceed 3 mm .
g. Change the Upper Beam DISPLAY switch to RIGHT PLUG-IN A.
h. Check-The signal amplitude on the Upper Beam display not to exceed 3 mm .
i. Remove the Standard Amplitude Calibrator signal from both test load unit inputs.

## 14. Check Trace Drift with Line Voltage Change

a. Requirement-Vertical drift of the Upper or Lower Beam trace not to exceed 2 mm with change in line voltage.
b. Set the controls as follows:

## A Triggering Controls <br> SOURCE <br> COUPLING <br> LEFT INT NORM <br> AC

SLOPE
MODE
LEVEL
Upper Beam DISPLAY
A TIME/CM
B Triggering Controls
SOURCE
COUPLING
SLOPE
MODE
LEVEL
Lower Beam DISPLAY
B TIME/CM
Test Load Unit (both)
Test Function
Test Oscilloscope
Time/cm
Type W
AC-DC-GND (A)
AC-DC-GND (B)
Input Atten
Millivolts/cm
Display
Vc Range
Autotransformer
$+$
AUTO STABILITY
Clockwise, knob pushed in
LEFT PLUG-IN A
1 mSEC

RIGHT INT NORM
AC
$+$
AUTO STABILITY
Clockwise, knob pushed in
RIGHT PLUG-IN B 1 mSEC

Gain Set

5 milliseconds

DC
GND
100
50
A-Vc
0
115 (RMS)

## NOTE

The following procedure applies only to a Type 556 connected to a nominal 115 -volt 3 -wire power source. For an instrument connected to other than a nominal 115 -volt source, a procedure and test fixtures adapted to local conditions will be required; for example, a 230 -volt source will require an autotransformer with the higher output, an isolation transformer for the test oscilloscope, power sockets, etc.
c. Connect the 20 -inch power cord between the autotransformer and the power socket assembly, and connect the Type 556 power cord to the power socket assembly.

NOTE
The short power cord and the socket assembly (items 12 and 13 of Recommended Equipment) are used only to provide convenient measurement terminals with a minimum of hazard. If the autotransformer used is equipped with more than one output socket, the cord and socket assembly may be eliminated.
d. Connect a $1 \times$ probe to the test oscilloscope input connector.
e. Connect the probe ground lead to the ground pin of one of the sockets in the power socket assembly.
f. With the probe tip, determine which of the two remaining socket contacts is the neutral contact, and connect the probe tip to this contact.
g. Change the Type $W$ Millivolts/cm switch to 20 . The vertical deflection sensitivity should now be 2 volts $/ \mathrm{cm}$.
h. Measure the peak voltage of the waveform, as shown in Fig. 5-4.
i. Set the Type W Comparison Voltage (Vc) dial to 178 plus the reading obtained in step (h).


Fig. 5-4. Illustrating measurement of voltage drop in neutral wire. Probe connected between grounding pin and neutral wire; Type $W$ Time/cm, 5 milliseconds; vertical sensitivity, 2 volts/cm.

Example: If the reading obtained in step (h) was 2.4 volts, the dial should be set to 180.4.
i. With the right and left plug-in units vertical position controls, adjust the Upper and Lower Beam traces to their respective graticule center horizontal lines.
k. Set the Vc Range to +11 .
I. Change the Millivolts/cm switch to 10 .
m. Move the probe tip from the neutral contact to the high-voltage or "hot" contact in the power socket assembly.
$n$. Adjust the autotransformer output until the tips of the waveforms shown on the test oscilloscope reach the reference line established previously by the Type W. (See Fig. 5-5 for typical display). The test oscilloscope is now indicating 178 peak VAC at the autotransformer output, or 126 volts RMS.
o. Wait two minutes to allow the Type 556 to stabilize, and observe the position of the Upper and Lower Beam traces.
p. Check-Vertical drift of either trace should not exceed 2 mm upward or downward.
q. Return the autotransformer output to 115 volts.
r. Allow about 2 minutes at the 115 -volt setting of the autotransformer, then recheck that the Upper and Lower Beam traces are on their respective center horizontal graticule lines.
s. Set the Type W Comparison Voltage (Vc) dial to 141.4 plus the reading obtained in step ( h ).
t. Adjust the autotransformer output until the tips of the waveform shown on the test oscilloscope reach the reference


Fig. 5-5. Illustrating method of peak line voltage measurement; Trpe $W$ plug-in vertical deflection factor $1 \mathrm{~V} / \mathrm{cm}$; sweep rate 5 milliseconds/cm.
line established previously by the Type $W$. The test oscilloscope is now indicating 141.4 peak VAC at the autotransformer output, or 100 volts RMS.
u. Wait two minutes to allow the Type 556 to stabilize, and observe the position of the Upper and Lower Beam traces.
v. Check-Vertical drift of either trace should not exceed 2 mm upward or downward.
w. Return the autotransformer setting to 115 volts, disconnect the probe, and return the Type W Vc Range switch to 0 .

## 15. Check Alternate Trace Operation

a. Requirement-Trace alternation at all sweep rates.
b. Connect the BNC T connector to the Type 556 CAL OUT connector. Connect two $50 \Omega$ cables from the T connector to the Ext Input connectors on the right and left test load units.
c. Set the AMPLITUDE CALIBRATOR to 10 VOLTS, and set the Test Function switches on both Test Load units to Alternate.
d. Check-Two traces on the Upper Beam display, with the calibrator signal appearing on only one trace.
e. Rotate the A TIME/CM switch through all positions from 1 mSEC to $.1 \mu \mathrm{SEC}$ checking for two traces on the Upper Beam display for all positions. Return the A TIME/CM switch to 1 mSEC .
f. Repeat steps (d) and (e) for the Lower Beam, checking for two traces in all positions of the B TIME/CM switch from 1 mSEC through . $1 \mu \mathrm{SEC}$.
g. Change the Upper Beam DISPLAY switch to LEFT PLUGINB.
h. Rotate the B TIME/CM switch through all positions from 1 mSEC to $.1 \mu \mathrm{SEC}$.
i. Check--Two traces displayed by each beam in all positions of the B TIME/CM switch.
i. Change the Upper Beam DISPLAY switch to RIGHT PLUG-IN A.
k. Rotate the A TIME/CM and B TIME/CM switches through all positions from 1 mSEC to $.1 \mu \mathrm{SEC}$, keeping the A and B TIME/CM settings the same.

## NOTE

With the Upper Beam DISPLAY switch in the RIGHT PLUG-IN A position, a multiple trace will appear on both displays for some of the switch positions. This condition is normal.
I. Check-Two traces on each beam at all positions of the TIME/CM switches.
m. Change the Upper Beam DISPLAY switch to RIGHT PLUG-IN B.
n. Rotate the B TIME/CM switch through all positions from 1 mSEC to $.1 \mu \mathrm{SEC}$.
o. Check-Two traces displayed by each beam at all settings of the TIME/CM switches from 1 mSEC through $.1 \mu \mathrm{SEC}$.
p. Remove the AMPLITUDE CALIBRATOR signal from both plug-ins.

## 16. Check Multi-Trace Chopping Transient Blanking

a. Requirement-Blanking of switching transients.
b. Change both test load unit Test Function switches to Chopped.
c. Set the Upper Beam DISPLAY switch to LEFT PLUG-IN A.
d. Set both TIME/CM switches to $5 \mu \mathrm{SEC}$.
e. Adjust the A and B Triggering LEVEL controls for stable displays on both beams.
f. Change the Upper Beam CRT Cathode Selector switch (on rear panel) to UPPER BEAM CHOPPED BLANKING.
g. Check-Disappearance of fast chopping transients (vertical lines) on the Upper Beam display.
h. Change the Lower Beam CRT Cathode Selector switch (on rear panel) to LOWER BEAM CHOPPED BLANKING.
i. Check-Disappearance of fast chopping transients on the Lower Beam display.
i. Repeat steps ( f ) and ( g ) with the Upper Beam DISPLAY switch in the LEFT PLUG-IN B, RIGHT PLUG-IN A, and RIGHT PLUG-IN B positions.

## NOTE

With the Upper Beam DISPLAY switch in the RIGHT PLUG-IN A position, the A Triggering SOURCE switch should be changed to RIGHT for that one position only.
k. Reset both CRT Cathode Selector switches to EXTERNAL CRT CATHODE.
I. Disconnect the coaxial cables and BNC T connector.

## 17. Check External Trigger Sensitivity

a. Requirement-Stable displays with 0.2 -volt input at 1 kHz .
b. Remove the test load units and in their place install the Type 1A1 plug-in units.
c. Set the controls as follows:

| A Triggering Controls |  |
| :---: | :---: |
| SOURCE | EXT |
| COUPLING | $A C$ |
| SLOPE | $+$ |
| MODE | TRIG |
| LEVEL | Centered, knob pushed in |
| Upper Beam DISPLAY | LEFT PLUG-IN A |
| Upper Beam DISPLAY MAG | $\times 1$ |
| A TIME/CM | 1 mSEC |
| A VARIABLE | CALIBRATED |
| A MODE | NORM |
| B Triggering Controls |  |
| SOURCE | EXT |
| COUPLING | AC |
| SLOPE | + |
| MODE | TRIG |
| LEVEL | Centered, knob pushed in |
| Lower Beam DISPLAY | RIGHT PLUG-IN B |
| Lower Beam DISPLAY MAG | $\times 1$ |
| B TIME/CM | ? mSEC |
| B VARIABLE | CALIBRATED |
| B MODE | NORM |

d. Connect a BNC T and two $50 \Omega$ cables from the Standard Amplitude Calibrator output connector to the input connector of the right plug-in unit, and the B Triggering TRIGGER INPUT connector.
e. Set the right plug-in unit vertical deflection switch to 1 volt/cm and the Input Selector switch to DC.
f. Set the Standard Amplitude Calibrator to 0.2 volts, square wave output.
g. Check-Stable display may be obtained with adjustment of the B Triggering LEVEL control.
h. Change the Standard Amplitude Calibrator to 50 millivolts.
i. Check-No stable display may be obtained with adjustment of the LEVEL control.
i. Change the two $50 \Omega$ cables from the right plug-in unit input connector and the B Triggering TRIGGER INPUT connector to the left plug-in unit input connector and the A Triggering TRIGGER INPUT connector.
k. Set the left plug-in unit vertical deflection switch to 1 volt/cm and the Input Selector switch to DC.
I. Set the Standard Amplitude Calibrator to 0.2 volts, square-wave output.
m . Check-A stable display may be obtained with adjustment of the A Triggering LEVEL control.
n. Change the Standard Amplitude Calibrator to 50 millivolts.

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o. Check-No stable display may be obtained with adjustment of the LEVEL control.

## 18. Check Triggering Level Control Ranges

a. Requirement-EXT, at least $\pm 2$ volts; $\times 10$, at least $\pm 20$ volts.
b. Change the right and left plug-in unit vertical attenuation switches to 5 volts $/ \mathrm{cm}$.
c. Set the Standard Amplitude Calibrator to 2 volts, +DC in the mixed mode.
d. Turn the A Triggering LEVEL control fully clockwise.
e. Check-Display not triggered, demonstrating that the control has moved the DC level of the Triggering circuit beyond the positive 2 -volt signal amplitude.
f. Change the Standard Amplitude Calibrator to -DC output.
g. Set the A Triggering SLOPE switch to - .
h. Turn the A Triggering LEVEL control fully counterclockwise.
i. Check-Display not triggered, demonstrating that the control has moved the level of the triggered circuit beyond the amplitude of the negative 2 -volt input signal.
i. Set the Standard Amplitude Calibrator for 20 volts output.
k. Pull out the A Triggering LEVEL control knob (PULL FOR $\times 10$ RANGE INCREASE).
I. Check-Display not triggered.
m. Change the Standard Amplitude Calibrator to $+D C$.
$n$. Set the A Triggering SLOPE switch to + .
o. Turn the A Triggering LEVEL control fully clockwise.
p. Check-Display not triggered.
q. Change the Standard Amplitude Calibrator output from the A Triggering TRIGGER INPUT connector to the B Triggering TRIGGER INPUT connector, and from the left plug-in unit vertical input connector to the right plug-in unit vertical input connector.
r. Pull out the B Triggering LEVEL control knob, and turn the control fully clockwise.
s. Check—Display not triggered.
t. Set the Standard Amplitude Calibrator for -DC output.
u. Set the B Triggering SLOPE switch to - .
v. Turn the B Triggering LEVEL control fully counterclockwise.
w. Check-Display not triggered.
$x$. Set the Standard Amplitude Calibrator for 2 volts output, and push the LEVEL control knob in.
y. Check-Display not triggered.
z. Change the Calibrator output to $+D C$.
aa. Change the B Triggering SLOPE switch to + , and turn the LEVEL control fully clockwise.
ab. Check-Display not triggered.
ac. Push in the A Triggering LEVEL control knob and disconnect the Standard Amplitude Calibrator signal.

## 19. Check Internal Triggering-Lower Beam

a. Requirement-Correct triggering with the following trigger coupling conditions and signal inputs:

b. Set the B Triggering SOURCE switch to RIGHT INT NORM the MODE switch to AUTO STABILITY, and the B TIME/CM switch to $.2 \mu \mathrm{SEC}$.
c. Set the constant-amplitude generator for a $10-\mathrm{MHz}$ signai, apply the signal through a $50 \Omega$ cable and $50 \Omega$ termination to the right plug-in unit, and adjust the plug-in unit vertical controls to display a signal 2 mm in amplitude.
d. Check-Stable displays can be obtained on the Lower Beam with the B Triggering COUPLING switch in the AC and AC LF REJ positions. The LEVEL control may be adjusted as necessary to obtain a stable display.

## NOTE

If desired, set the B Triggering MODE switch to TRIG when performing the "check" steps in this procedure (step 19). Use the AUTO STABILITY position between the "check" steps when setting up the display amplitude.
e. Change the generator frequency to 50 MHz .
f. Set the B Triggering COUPLING switch to AC, and the Lower Beam DISPLAY MAG switch to $\times 10$.
g. Adjust the amplitude of the display to 1 cm .
h. Check-Stable displays may be obtained with adjustment of the LEVEL control.
i. Remove the constant amplitude generator signal from the right plug-in connector and connect the output of the lowfrequency signal generator through a coaxial cable to the same connector.
j. Set the $B$ Triggering COUPLING switch to AC HF REJ, the B TIME/CM switch to $50 \mu \mathrm{SEC}$, and return the Lower Beam DISPLAY MAG switch to $\times 1$.
k. Set the generator frequency to 60 kHz and adjust the display amplitude to 2 mm .
I. Check-Stable display may be obtained with adjustment of the LEVEL control.
m . Replace the low-frequency signal generator with the constant amplitude generator; set the generator frequency
to 6 MHz . Set the Type 556 B TIME/CM switch to $.5 \mu \mathrm{SEC}$, and the display amplitude to 1 cm .
n. Check-No stable display with adjustment of the LEVEL control.
o. Change the B Triggering SOURCE switch to PLUG-IN INT and the COUPLING switch to AC.
p. Set the right plug-in Variable Volts/cm control to Calib and set the generator amplitude control for 4 mm display on the Lower Beam.
q. Check-Stable display may be obtained while adjusting the LEVEL control.
r. Remove the constant-amplitude generator signal from the right plug-in input connector, and connect the output of the low-frequency signal generator to the same connector.
s. Set the generator output for 60 Hz sine waves.
t. Set the B TIME/CM switch to 5 mSEC so several cycles of the waveform are displayed. and set the B Triggering SOURCE switch to RIGHT INT NORM. Adjust the plug-in unit vertical attenuator for a display 2 mm in amplitude.
u. Check-Stable displays may be obtained on the Lower Beam with the $B$ Triggering COUPLING switch in the AC and AC HF REJ positions. The LEVEL control may be adjusted as necessary to obtain stable displays.
v. Increase the display amplitude to 3.5 mm .
w. Change the B Triggering COUPLING switch to DC.
x. Check-Stable displays may be obtained while adjusting the LEVEL control.
y. Change the generator to 30 Hz , and B TIME/CM switch to 10 mSEC , and adjust the display amplitude to 3 cm .
z. Change the $B$ Triggering COUPLING switch to $A C$ LF REJ.
aa. Check-No stable displays may be obtained while adjusting the LEVEL control.
ab. Change the generator frequency to 2.5 kHz , set the $B$ TIME/CM switch to 1 mSEC , and adjust the amplitude of the display to 2 mm .
ac. Check-Stable displays may be obtained with adjustment of the LEVEL control.

## 20. Check Internal Triggering-Upper Beam

a. Requirement-Correct triggering with the following trigger coupling conditions and signal inputs:
$\mathrm{AC}: \quad 2 \mathrm{~mm} 60 \mathrm{~Hz}$ to 10 MHz , increasing to 1 cm at 50 MHz .
AC LF REJ: $\geq 3 \mathrm{~cm}$ at $30 \mathrm{~Hz}, 2 \mathrm{~mm} 2.5 \mathrm{kHz}$ to 10 MHz , increasing to 1 cm at 50 MHz .
AC HF REJ: 2 mm 60 Hz to 60 kHz , increasing to 1 cm at 6 MHz .
DC: $\quad 3.5 \mathrm{~mm} \mathrm{DC}$ to 10 MHz , increasing to 2 cm at 50 MHz .
b. Set the A Triggering SOURCE switch to LEFT INT NORM, and the MODE switch to AUTO STABILITY.
c. Change the low-frequency generator output signal to the left plug-in unit input connector, and adjust the signal amplitude to 2 mm on the Upper Beam display.
d. Set the A TIME/CM switch to 1 mSEC .
e. Set the A Triggering COUPLING switch to AC LF REJ.
f. Check-Stable displays may be obtained on the Upper Beam while adjusting the LEVEL control.

## NOTE

If desired, set the A Triggering MODE switch to TRIG when performing the "check" steps in this procedure (step 20). Use the AUTO STABILITY position between the "check" steps when setting up the display amplitude.
g. Change the generator frequency to 30 Hz , and change the A TIME/CM switch to 10 mSEC .
h. Adjust the signal amplitude to 3 cm .
i. Check-No stable display while adjusting the LEVEL control.
i. Change the generator frequency to 60 Hz , and the $A$ TIME/CM switch to 5 mSEC .
k. Adjust the signal amplitude to 2 mm .
I. Check-Stable displays may be obtained with the COUPLING switch in AC, and AC HF REJ, while adjusting the LEVEL control.
m . Increase the amplitude of the display to 3.5 mm .
n. Change the COUPLING switch to DC.
o. Check-Stable displays may be obtained while adjusting the LEVEL control.
p. Remove the low-frequency signal, and connect the con-stant-amplitude signal generator output through a 50 ohm cable and 50 -ohm termination to the left plug-in unit vertical input connector.
q. Set the generator frequency to 10 MHz .
r. Set the A TIME/CM switch to $.2 \mu$ SEC, and adjust the left plug-in controls so the display is 2 mm in amplitude.
s. Check--Stable displays may be obtained on the Upper Beam with the A Triggering COUPLING switch in the AC and AC LF REJ positions. The LEVEL control may be adjusted as necessary to obtain a stable display.
t. Change the generator frequency to 50 MHz .
u. Set the A Triggering COUPLING switch to AC, and the A TIME/CM switch to $.2 \mu \mathrm{SEC}$.
v. Change the DISPLAY MAG switch to $\times 10$, and adjust the amplitude of the display to 1 cm .
w. Check-Stable displays may be obtained with adjustment of the LEVEL control.
x. Remove the constant amplitude generator signal from the left plug-in connector and connect the output of the lowfrequency signal generator through a coaxial cable to the same connector.
y. Set the A Triggering COUPLING switch to AC HF REJ, the A TIME/CM switch to $50 \mu \mathrm{SEC}$, and return the Upper Beam DISPLAY MAG switch to $\times 1$.
z. Set the generator frequency to 60 kHz and adiust the display amplitude to 2 mm .
aa. Check-Stable displays may be obtained with adjustment of the LEVEL control.

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ab. Replace the low-frequency signal generator with the constant amplitude generator; set the generator frequency to 6 MHz . Set the Type 556 A TIME/CM switch to $15 \mu \mathrm{SEC}$, and the display amplitude to 1 cm .
ac. Check-No stable display with adjustment of the LEVEL control.
ad. Change the A Triggering SOURCE switch to PLUG-IN INT and the COUPLING switch to AC.
ae. Set the left plug-in Variable Volts/cm control to Calib and set the generator amplitude control for a 4 mm display on the Upper Beam.
af. Check-Stable displays may be obtained while adjusting the LEVEL control.

## 21. Check Crossover Triggering

a. Requirement-A stable display with a 2 mm signal at 10 MHz .
b. Set the Upper Beam DISPLAY switch to RIGHT PLUG-IN A, the A Triggering SOURCE to RIGHT INT NORM, the MODE switch to TRIG, and the A TIME/CM switch to $.2 \mu \mathrm{SEC}$.
c. Set the B Triggering LEVEL fully clockwise, the MODE switch to AUTO STABILITY, the COUPLING switch to AC and the B TIME/CM switch to $.2 \mu \mathrm{SEC}$.
d. Set the constant-amplitude signal generator to supply a 10 MHz signal and connect the signal to the right plug-in unit input connector. Adjust the right plug-in unit controls to display a signal 2 mm in amplitude on the Upper Beam.
e. Check-Stable display on the Upper Beam while adjusting the A Triggering LEVEL control.
f. Remove the generator signal.

## 22. Check Auto Stability Operation

a. Requirement-Sweep triggering at 30 Hz ; free-running display with no signal.
b. Connect a 30 Hz sine-wave signal from a low-frequency generator to the right plug-in unit input connector and set the B TIME/CM switch to 10 mSEC .
c. Adjust the plug-in unit for a display 1 cm in amplitude.
d. Rotate the $B$ Triggering LEVEL control from a fully counterclockwise position through 0 to the full clockwise position.
e. Check-Triggered (stable) display near the 0 position, and a free-running display in the remainder of the rotation area.
f. Remove the generator signal from the right plug-in unit connector and apply the signal to the left plug-in unit input connector.
g. Set the A Triggering SOURCE switch to LEFT INT NORM, MODE switch to AUTO STABILITY, Upper Beam DISPLAY switch to LEFT PLUG-IN A and the A TIME/CM switch to 10 mSEC .
h. Use steps (c) and ( $d$ ) as a guide to check the A Triggering AUTO STABILITY operation.
i. Check-Triggered (stable) display near the 0 position, and a free-running display in the remainder of the rotation area.
i Remove the generator signal.

## 23. Check Line Trigger and LF Reject Operation

a. Requirement-Line triggering, must produce stable display of correct polarity; Slope, changes display polarity when switched; Low-Frequency Reject operation, does not trigger at line frequency.
b. Connect a $10 \times$ probe to the right plug-in unit input connector.
c. Preset the right plug-in unit vertical deflection to a factor ( $100 \mathrm{~V} / \mathrm{cm}$ with $10 \times$ probe) that will permit an onscreen display when the signal in step (e) is applied.
d. Set the B TIME/CM switch to 5 mSEC .
e. Set the B Triggering SOURCE switching LINE RIGHT, and connect the probe tip to the oscilloscope line voltage source.
f. Check-Stable display with adjustment of the LEVEL control.
g. Change the SLOPE switch from + to - .
h. Check-Correct trigger polarity with the change of the SLOPE switch.
i. Change the SOURCE switch to NORM INT RIGHT.
i. Check-Stable display with adjustment of the LEVEL control.
k. Change the COUPLING switch to AC LF REJ.
I. Check--No stable display with adjustment of the LEVEL control.
$m$. Return the COUPLING switch to $A C$ and remove the probe.

## 24. Check A and B Single Sweep Operation

a. Requirement-Sweep triggers with the same Triggering LEVEL control settings as in AUTO STABILITY; sweep locks out until reset.
b. Set the Standard Amplitude Calibrator to 1 volt squarewave output and apply the signal to the left plug-in unit input connector.
c. Set the left plug-in unit vertical deflection switch to 1 volt $/ \mathrm{cm}$ and set the A TIME/CM switch to .5 mSEC .
d. With the variable volts $/ \mathrm{cm}$ control, adjust the Upper Beam display amplitude for 5 mm , and adjust the A Triggering controls for a stable display.
e. Change the A MODE switch to SINGLE SWEEP, the A Triggering MODE switch to TRIG and remove the Standard Amplitude Calibrator signal from the left plug-in unit input connector.
f. Depress the A sweep RESET button, and note that the single-sweep indicator light is lit.
g. Re-apply the Standard Amplitude Calibrator signal to the input connector.
h. Check-The sweep runs once, and the indicator light is extinguished.
i. Use steps (c) through (g) as a guide for the B sweep, the right plug-in unit and Type 556 front-panel control settings.
i. Check-The B sweep runs once, and the indicator light is extinguished.
k. Return the A and B MODE switches to NORM, and remove the Standard Amplitude Calibrator signal.

## 25. Check Basic Timing-A Sweep

a. Requirement-Sweep rate $\pm 3 \%$ of displayed time, $\times 1$; $\pm 5 \%$ of displayed time, $\times 10$.
b. Remove the Type 1A1 units and install Test Load units in their place.
c. Set controls as follows:

A Triggering Controls
SOURCE LEFT INT NORM
COUPLING AC
SLOPE +
MODE AUTO STABILITY
LEVEL
Upper Beam DISPLAY
Upper Beam DISPLAY MAG $\times 1$
A TIME/CM 1 mSEC
A VARIABLE CALIBRATED
A MODE
NORM
B Triggering Controls
SOURCE
COUPLING
SLOPE
MODE
LEVEL
Lower Beam DISPLAY
Lower Beam DISPLAY MAG
B TIME/CM
B VARIABLE
B MODE
Test Load Units (both)
Test Function
Low Load
d. Connect a BNC T connector, two $50 \Omega$ cables and two $50 \Omega$ terminations from the fime-mark generator to both Test Load unit Ext Input connectors.
e. Set the time-mark generator for 1 -millisecond and 100 microsecond markers.
f. Adjust the A and B Triggering controls for stable displays in the Upper and Lower Beam graticule viewing areas.
g. Set the Upper Beam DISPLAY MAG switch to $\times 10$.
h. Check-One 100 -microsecond marker/cm $\pm 5 \%$ or $\pm 4 \mathrm{~mm}$.

## NOTE

When checking sweep timing, or when making time measurements from the graticule, the area between the first-cm and ninth-cm graticule lines provides the most linear measurement. Therefore the $0-\mathrm{cm}$ to $1-\mathrm{cm}$ and the $9-\mathrm{cm}$ to $10-\mathrm{cm}$ areas of the display should not be used for making accurate time measurements. See Fig. 2-7 in Selecting Sweep Rate, Section 2 of this manual.
i. Change the Upper Beam DISPLAY MAG switch to $\times 1$.
i. Check—One 1 -millisecond marker/cm, $\pm 3 \%$ or 2.4 mm .

## 26. Check Upper Beam Sweep Magnifier Registration

a. Requirement-No more than 0.5 cm shift when switching the DISPLAY MAG switch from $\times 10$ to $\times 1$.
b. Set the Upper Beam DISPLAY MAG switch to $\times 10$ and position the start of the trace to the graticule center vertical line.
c. Change the DISPLAY MAG switch to $\times 1$.
d. Check-No more than 0.5 cm shift of the start of the trace as the DISPLAY MAG switch is changed from $\times 10$ to $\times 1$.
e. Check that Lower Beam DISPLAY MAG switch is set to $\times 1$.

## 27. Check A Sweep Length

a. Requirement-Sweep length $10.5 \mathrm{~cm} \pm 5 \mathrm{~mm}$.
b. Set the time-mark generator for 1 -millisecond and 500microsecond markers. Position the display to start at the $0-\mathrm{cm}$ graticule line.
c. Check-The 22nd marker (counting the marker at the $0-\mathrm{cm}$ graticule line) is just visible at the right hand edge of the graticule.
d. Return the DISPLAY MAG switch to $\times 10$.

## 28. Check B Sweep Sawtooth Slope

a. Requirement-One 100 -microsecond marker/cm on the Upper Beam display.
b. Set the Upper Beam DISPLAY switch to LEFT PLUG-IN B.
c. Set the time-mark generator for 1-millisecond and 100 microsecond markers.
d. Check-One 100-microsecond marker/cm on the Upper Beam display.
e. Return the DISPLAY MAG switch to $\times 1$.

## 29. Check B Sweep Length

a. Requirement-Sweep length $10.5 \mathrm{~cm} \pm 5 \mathrm{~mm}$.
b. Set the time-mark generator for 1 -millisecond and 500 microsecond markers.
c. Check-The 22nd marker (counting the marker at the $0-\mathrm{cm}$ graticule line) is just visible at the right-hand edge of the graticule.

## 30. Check Basic Timing-B Sweep

a. Requirement-Sweep rate $\pm 3 \%$ of displayed time, $\times 1$; $\pm 5 \%$ of displayed time, $\times 10$.
b. Set the Lower Beam DISPLAY switch to $\times 10$, and position the display for optimum viewing.
c. Set the time-mark generator for 1 -millisecond and 100 microsecond markers.
d. Check-One 100 -microsecond marker $/ \mathrm{cm}, \pm 5 \%$ or 4 mm .
e. Change the Lower Beam DISPLAY MAG switch to $\times 1$.
f. Check-One 1-millisecond marker/cm, $\pm 3 \%$ or 2.4 mm .

## 31. Check Lower Beam Sweep Magnifier Registration

a. Requirement-No more than 0.5 cm shift in the display when changing the DISPLAY MAG switch from $\times 10$ to $\times 1$.
b. Set the Lower Beam DISPLAY MAG switch to $\times 10$ and position the start of the trace to the graticule center vertical line.
c. Change the DISPLAY MAG switch to $\times 1$.
d. Check-No more than 0.5 cm shift of the start of the trace as the DISPLAY MAG switch is changed from $\times 10$ to $\times 1$.
e. Return the DISPLAY MAG switch to $\times 1$ and disconnect the time-markers from the Type 556.

## 32. Check Delay-Time Multiplier Dial Setting

a. Requirement-Counterclockwise reading, $0.20 \pm 2$ minor divisions; clockwise reading, $10.20 \pm 4$ minor divisions.
b. Rotate the DELAY-TIME MULTIPLIER dial fully counterclockwise until it hits the stop.

## NOTE

If dial is reset, delayed-sweep calibration will be changed and it will be necessary to perform a recalibration of the A sweep (steps 45 through 48 in the Calibration Procedure).
c. Check-Dial reading of $0.20, \pm 2$ minor divisions.
d. If the dial reading is not 0.20 (within $\pm 2$ minor divisions), loosen the knob setscrew and reposition the knob so that the fully counterclockwise position reading is correct.
e. Rotate the DELAY-TIME MULTIPLIER dial fully clockwise.
f. Check-Dial reading of $10.20, \pm 4$ minor divisions.

## 33. Check Delay Start and Stop

a. Requirement-Intensified portion of the display starts at the 2 nd and 10th markers with the DELAY-TIME MULTIPLIER
dial set to $1.00 \pm 10$ minor divisions, and $9.00 \pm 10$ minor divisions, respectively, with a difference of 800 minor divisions $\pm 8$ minor divisions between the two dial readings.
b. Set controls as follows:

| A Triggering Controls |  |
| :--- | :--- |
| $\quad$ SOURCE | RIGHT INT NORM |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Near 0, knob pushed in |
| Upper Beam DISPLAY | RIGHT PLUG-IN A |
| Upper Beam DISPLAY MAG | $\times 1$ |
| A TIME/CM | 1 mSEC |
| A VARIABLE | CALIBRATED |
| A MODE | NORM |
| B Triggering Controls |  |
| SOURCE | RIGHT INT NORM |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Fully clockwise, knob |
|  | pulled outward |
| Lower Beam DISPLAY | RIGHT PLUG-IN B |
| Lower Beam DISPLAY MAG | $\times 1$ |
| B TIME/CM | $10 \mu S E C$ |
| B VARIABLE | CALIBRATED |
| B MODE | NORM |
| Test Load Units (both) |  |
| Test Function | Low Load |

c. Connect a $50 \Omega$ cable from the time-mark generator through a $50 \Omega$ termination to the right test load unit Ext Input connector.
d. Set the time-mark generator for 1-millisecond markers.
e. Adjust the A Triggering controls for a stable display on the Upper Beam.
f. Adjust the TRACE SEPARATION and right test load unit Variable and Vertical Position controls for convenient viewing of the Upper and Lower Beam displays.
g. Change the $B$ MODE switch to DLY'D BY A.

## NOTE

Adiustment of the Upper Beam INTENSITY and CONTRAST controls may be necessary for optimum viewing of the intensified portion of the display.
h. Adjust the DELAY-TIME MULTIPLIER dial so that the intensified portion of the Upper Beam display starts at the 2nd marker.
i. Check-The dial reading should be $1.00 \pm 10$ minor divisions.
i. Adjust the DELAY-TIME MULTIPLIER dial so that the intensified portion of the Upper Beam display starts at the 10th marker.
k. Check-The dial reading should be $9.00 \pm 10$ minor divisions.
I. Check-The difference obtained between the dial readings obtained in steps (i) and (k) should be 800 minor divisions $\pm 8$ minor divisions.

## 34. Check Delay-Time Multiplier Incremental Linearity

a. Requirement-Deviation of DELAY-TIME MULTIPLIER readings between adjacent major dial divisions not more than $\pm 2$ minor divisions from 1.00 to 9.00 .
b. Set the DELAY-TIME MULTIPLIER dial to 8.00 .
c. Rotate the dial as necessary to position the delayed pulse to start at the $0-\mathrm{cm}$ graticule line.
d. Check—Deviation of dial reading from 8.00 should be not more than $\pm 2$ minor divisions on the dial as compared to the deviation from 9.00 of the previous dial reading. For example, if the dial reading from 9.00 is 9.04 , the reading from 8.00 should be $8.04 \pm 2$ minor divisions.
e. Repeat check at all major divisions from 8.00 to 1.00 .

## 35. Check Delay-Time Jitter

a. Requirement-Jitter not more than 0.5 cm .
b. Change the B TIME/CM switch to $1 \mu \mathrm{SEC}$.
c. Set the DELAY-TIME MULTIPLIER dial to 10.00 approximately, centering the magnified pulse near the center of the graticule.
d. Check—Jitter not more than 0.5 cm .
e. Set the DELAY-TIME MULTIPLIER dial to 1.00 approximately, centering the magnified waveform near the center of the graticule.
f. Check-Jitter not more than 0.5 cm .

## 36. Check Horizontal Amplifier 50 MHz Com-pensation-Upper Beam

a. Requirement-Timing accuracy $\pm 5 \%$ (or $\pm 4 \mathrm{~mm}$ ) 4 cm from sweep start to 70 cm from sweep start.
b. Set the controls as follows:

A Triggering Controls

SOURCE
COUPLING
SLOPE
MODE
LEVEL
Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A VARIABLE
A MODE
B Triggering Controls
SOURCE
COUPLING

RIGHT INT NORM
AC
$+$
AUTO STABILITY
Near 0, knob pushed in
RIGHT PLUG-IN A
$\times 1$
$0.1 \mu$ SEC
CALIBRATED
NORM

RIGHT INT NORM
$A C$

SLOPE
MODE
LEVEL
Lower Beam DISPLAY Lower Beam DISPLAY MAG
B TIME/CM
B VARIABLE
B MODE
DELAY-TIME MULTIPLIER
$+$
AUTO STABILITY
Fully clockwise, knob pulled outward
RIGHT PLUG-IN B
$\times 10$
$1 \mu$ SEC
CALIBRATED
NORM
1.00

Test Load Units (both)
Test Function
Low Load
c. Change the B MODE switch to SINGLE SWEEP (this disables the B sweep).
d. Set the time-mark generator for $50 \mathrm{MHz}(20 \mathrm{~ns})$ sinewave output.
e. Connect a 10 -microsecond trigger signal from the timemark generator Trigger Output connector through a $50 \Omega$ cable and $50 \Omega$ termination to the Upper Beam TRIGGER INPUT connector.
f. Set the A Triggering SOURCE switch to EXT and adjust the LEVEL control to obtain a stable display.
g. Position the display so the Upper Beam waveform starts at the $0-\mathrm{cm}$ graticule line. (Turn up the INTENSITY control temporarily to see the start of the waveform for proper positioning.)
h. Change the Upper Beam DISPLAY MAG switch to $\times 10$.


Fig. 5-6. Typical display, high-speed sweep timing, showing peak of a sine wave at the $4-\mathrm{cm}$ graticule line, see step $36(k)$.
i. Position the sine waves to align with the vertical graticule lines.
j. Check-One cycle $/ 2 \mathrm{~cm}$, Upper Beam display. The $1-\mathrm{cm}$ and $9-\mathrm{cm}$ sine-wave peaks should coincide with their respective graticule lines. Tolerance is $\pm 5 \%$ or $\pm 4 \mathrm{~mm}$. Position the display 10 cycles to the left and recheck timing accuracy.


Fig. 5-7. Typical display showing 4th cm sine wave of Fig. 5-6 repositioned to the $1-\mathrm{cm}$ graticule line, as in step 36 (I).
k. Position the display so the Upper Beam waveform starts at the $0-\mathrm{cm}$ graticule line. (Turn up the INTENSITY control temporarily to check that the waveform is properly positioned. See Fig. 5-6.)
I. Adjust the A Triggering LEVEL control so a sine-wave peak (top or bottom) falls on the $4-\mathrm{cm}$ graticule vertical line. Note that sine-wave peak and position it to the $1-\mathrm{cm}$ graticule vertical line. (See Fig. 5-7.)
m. Check-One cycle/ 2 cm , Upper Beam display; 1-cm, 5 cm and $9-\mathrm{cm}$ sine-wave peaks should coincide with their respective graticule vertical lines (see Fig. 5-8). Tolerance is $\pm 5 \%$ or $\pm 4 \mathrm{~mm}$.
n. Change the Upper Beam DISPLAY MAG switch to $\times 1$ and reposition the display to start at the $0-\mathrm{cm}$ graticule vertical line.


Fig. 5-8. Typical display, correct high speed sweep timing and linearity.

## 37. Check Timing and Delaying Sweep Accu-racy-A Sweep

a. Requirement-A Sweep accuracy, $\pm 3 \%$ or $\pm 2.4 \mathrm{~mm}$; delaying sweep, within 8 minor divisions of the DELAY-TIME MULTIPLIER dial for each position of the A TIME/CM switch.
b. Change the B MODE switch to DLY'D BY A, and check that the Lower Beam DISPLAY switch is set to $\times 10$.
c. Check-Using Table 5-2 as a guide, check the A Sweep CRT displayed accuracy with respect to the $1-\mathrm{cm}$ and $9-\mathrm{cm}$ graticule vertical lines. Tolerance should be within $\pm 3 \%$ or $\pm 2.4 \mathrm{~mm}$. In addition, check the delayed sweep accuracy using the DELAY-TIME MULTIPLIER dial. Tolerance should be within 8 minor divisions for each A TIME/CM switch position. The technique for checking the three fastest sweep rates using the DELAY-TIME MULTIPLIER dial is as follows:

For the $0.1 \mu$ SEC A TIME/CM switch position, the basic technique is described in steps 48s through 48aa of the Calibration Procedure. For the $0.2 \mu \mathrm{SEC}$ switch position the technique is similar to the 0.1 position, but 16 markers must be counted on the Lower Beam display when rotating the

TABLE 5-2
Timing and Delaying Sweep Accuracy-A Sweep

| A TIME/CM | B TIME/CM | Time Mark <br> Generator | Check <br> Upper Beam <br> Display |
| :---: | :---: | :---: | :---: |
| $0.1 \mu \mathrm{SEC}$ | $0.1 \mu \mathrm{SEC}$ | $0.1 \mu \mathrm{~s}$ | 1 marker $/ \mathrm{cm}$ |

${ }^{1}$ Use CONTRAST control to check display.
${ }^{2}$ Lower Beam DISPLAY MAG switch is set to $X 10$. (For the remaining $B$ TIME/CM switch positions, the switch is set to $X 1.1$
"Set the A Triggering SOURCE switch to RIGHT INT NORM and the MODE switch set to TRIG.


Fig. 5-9. Typical displays, Delay Start and Stop adjustments check.
dial from 1.00 to 9.00 . Check dial reading from 9.00 at intercept point. For the $0.5 \mu \mathrm{SEC}$ switch position, set the A Triggering SOURCE switch to RIGHT INT NORM, the Lower Beam DISPLAY MAG switch to $X 1$ and use a similar technique to that described in steps 48 c through 48 f of the Calibration Procedure

For the A TIME/CM switch position from $1 \mu \mathrm{SEC}$ to 5 SEC, use a similar technique for checking delaying sweep accuracy to that used when checking the Delay Start and Stop adjustments (step 33) and as shown in Fig. 5-9.

## 38. Check B Sweep Crossover Compensation

a. Requirement-Timing accuracy $\pm 3 \%$, Upper Beam display.
b. Set the Type 556 and plug-in unit controls as follows:

A Triggering Controls

| SOURCE | RIGHT INT NORM |
| :--- | :--- |
| COUPLING | AC |
| SLOPE | + |
| MODE | TRIG |

LEVEL
Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A VARIABLE
A MODE
B Triggering Controls
SOURCE
COUPLING
SLOPE
MODE
LEVEL
Lower Beam DISPLAY
Lower Beam DISPLAY MAG
B TIME/CM
B VARIABLE
B MODE
Test Load Units (both)
Test Function

Fully clockwise, knob pushed in
RIGHT PLUG-IN B
$\times 1$
1 mSEC
CALIBRATED
NORM

RIGHT INT NORM
AC
$+$
AUTO STABILITY
Near 0, knob pushed in
RIGHT PLUG-IN B
$\times 1$
. $1 \mu$ SEC
CALIBRATED
NORM
c. Set the time mark generator for 0.1-microsecond markers.
d. Remove the $10-\mu$ s trigger signal from the Upper Beam TRIGGER INPUT connector and apply the signal to the Lower Beam TRIGGER INPUT connector.
e. Set the B Triggering SOURCE switch to EXT and check that the Upper Beam DISPLAY switch is set to RIGHT PLUGINB.
f. Check—One marker/cm, Upper Beam display, $\pm 2.4$ mm.

## 39. Check Horizontal Amplifier $\mathbf{5 0} \mathbf{~ M H z}$ Com-pensation-Lower Beam

a. Requirement-Timing accuracy $\pm 5 \%$ (or $\pm 4 \mathrm{~mm}$ ) from the $1-\mathrm{cm}$ to $9-\mathrm{cm}$ graticule vertical lines.
b. Change the Upper Beam DISPLAY switch to LEFT PLUGIN A.
c. Set the time-mark generator for 50 MHz ( 20 ns ) sinewave output.
d. Adjust the B Triggering LEVEL control to obtain a stable display.
e. Position the display so the Lower Beam waveform starts at the $0-\mathrm{cm}$ graticule line. (Turn up the INTENSITY control temporarily to see the start of the waveform for proper positioning.)
f. Change the Lower Beam DISPLAY MAG switch to $\times 10$.
g. Position the sine waves to align with the graticule vertical lines.
h. Check-One cycle/2cm, Lower Beam display. The 1cm and $9-\mathrm{cm}$ sine-wave peaks should coincide with their

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respective graticule vertical lines. Tolerance is $\pm 5 \%$ or $\pm 4 \mathrm{~mm}$. Position the display 10 cycles to the left and recheck timing accuracy.
i. Position the display so the Lower Beam waveform starts at the $0-\mathrm{cm}$ graticule vertical line. (Turn up the INTENSITY control temporarily to check that the waveform is properly positioned. Use Fig. 5-6 as a guide.)
i. Adjust the B Triggering LEVEL control so a sine-wave peak (top or bottom) falls on the $4-\mathrm{cm}$ graticule vertical line. Note the sine-wave peak and position it to the $1-\mathrm{cm}$ graticule line. (Use Fig. 5-7 as a guide.)
k. Check—One cycle/ 2 cm , Lower Beam display; $1-\mathrm{cm}, 5$ cm and $9-\mathrm{cm}$ sine-wave peaks should coincide with their respective graticule lines. Tolerance is $\pm 5 \%$ or $\pm 4 \mathrm{~mm}$.

## 40. Check Timing Accuracy-B Sweep

a. Requirement-Timing accuracy $\pm 3 \%$ ( 2.4 mm ).
b. Change the B Triggering MODE switch to TRIG, the SOURCE switch to INT NORM and the Lower Beam DISPLAY MAG switch to $\times 1$.
c. Disconnect the trigger signal from the Lower Beam TRIGGER INPUT connector.
d. Check-Using Table 5-3 as a guide, check the B sweep CRT displayed accuracy with respect to the $1-\mathrm{cm}$ and $9 . \mathrm{cm}$ graticule vertical lines. Tolerance should be within $\pm 3 \%$ or $\pm 2.4 \mathrm{~mm}$.

TABLE 5-3

| B TIME/CM | Time Mark Generator | Check Lower Beam Display |
| :---: | :---: | :---: |
| $0.1 \mu \mathrm{SEC}$ | $0.1 \mu \mathrm{~s}$ | 1 marker/cm |
| $0.2 \mu$ SEC | $0.1 \mu \mathrm{~s}$ | 2 markers/cm |
| $0.5 \mu$ SEC | $0.5 \mu \mathrm{~s}$ | 1 marker/cm |
| $1 \mu \mathrm{SEC}$ | $1 \mu \mathrm{~s}$ | 1 marker/cm |
| $2 \mu \mathrm{SEC}$ | $1 \mu \mathrm{~s}$ | 2 markers/cm |
| $5 \mu$ SEC | $5 \mu \mathrm{~s}$ | 1 marker/cm |
| $10 \mu$ SEC | $10 \mu \mathrm{~s}$ | $1 \mathrm{marker} / \mathrm{cm}$ |
| $20 \mu$ SEC | $10 \mu \mathrm{~s}$ | 2 markers/cm |
| $50 \mu$ SEC | $50 \mu \mathrm{~s}$ | 1 marker/cm |
| 0.1 mSEC | 0.1 ms | 1 marker/cm |
| 0.2 mSEC | 0.1 ms | 2 markers/cm |
| 0.5 mSEC | 0.5 ms | 1 marker/cm |
| 1 mSEC | 1 ms | 1 marker/cm |
| 2 mSEC | 1 ms | 2 markers/cm |
| 5 mSEC | 5 ms | 1 marker/cm |
| 10 mSEC | 10 ms | 1 marker/cm |
| 20 mSEC | 10 ms | 2 markers/cm |
| 50 mSEC | 50 ms | 1 marker/cm |
| 0.1 SEC | 0.1 s | 1 marker/cm |
| 0.2 SEC | 0.1 s | 2 markers/cm |
| 0.5 SEC | 0.5 s | 1 marker/cm |
| 1 SEC | 1 s | 1 marker/cm |
| 2 SEC | 1 s | 2 markers/cm |
| 5 SEC | 5 s | 1 marker/cm |

## 41. Check Variable Time/cm Range

a. Requirement-At least 2.5:1 reduction in $A$ and $B$ Sweep rates.
b. Set the Upper Beam DISPLAY switch to RIGHT PLUG-IN A.
c. Set the B TIME/CM to 1 mSEC .
d. Set the A and B Triggering MODE switches to AUTO STABILITY.
e. Check that the A Triggering SOURCE switch is set to RIGHT INT NORM.
f. Set the time-mark generator for 10 -millisecond markers.
g. Adjust the A and B Triggering LEVEL controls to obtain stable Upper and Lower Beam displays. Markers on both beams will appear at the $0-\mathrm{cm}$ and $10-\mathrm{cm}$ graticule vertical lines.
h. Rotate the A and B TIME/CM VARIABLE controls fully counterclockwise; the UNCAL lights should be on.
i. Check-Horizontal distance between markers should be 4 cm or less, both displays.
i. Return both VARIABLE controls to CALIBRATED; the UNCAL lights should be off.

## 42. Check Trigger Delay

a. Requirement-Trigger delay equal to or less than 150 nanoseconds.
b. Preset the Type 556 controls as follows:

```
B MODE
DLY'D BY A
A and B TIME/CM
A Triggering
B Triggering
DELAY-TIME MULTIPLIER
\(A\) and \(B\) TIME/CM
A Triggering
B Triggering
DELAY TIME MULTIPLIER
```

c. Set the time-mark generator for 1-microsecond marker output.
d. Adjust the A triggering LEVEL control to obtain a stable display.
e. With the Upper and Lower Beam POSITION controls, position both traces to start at the $0-\mathrm{cm}$ graticule vertical line.
f. Turn the DELAY-TIME MULTIPLIER dial counterclockwise while adjusting the TRACE SEPARATION and right plug-in Vertical Position controls until the marker on the Lower Beam display is superimposed on the Upper Beam marker.
g. Check-Dial reading difference from 10.00 equal to or less than 150 nanoseconds. (One minor dial division equals one nanosecond.)
h. Disconnect the marker signal from the right plug-in unit.

## 43. Check External Horizontal Amplifier DC Balance-Upper Beam

a. Requirement-No more than $\pm 5 \mathrm{~cm}$ horizontal shift of the left edge of the display as the UPPER BEAM EXT HORIZ VAR 1-10 control is rotated.
b. Set the controls as follows:

A Triggering Controls

| SOURCE | LEFT EXT |
| :--- | :--- |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |

LEVEL
Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A VARIABLE
A MODE
B Triggering Controls
SOURCE
COUPLING
SLOPE
MODE
LEVEL
Lower Beam DISPLAY
Lower Beam DISPLAY MAG
B TIME/CM
B VARIABLE
B MODE
AUTO STABILITY
Near 0, knob pushed in
LEFT PLUG-IN EXT
$\times 10$
1 mSEC
CALIBRATED
NORM

RIGHT EXT
AC
$+$
AUTO STABILITY
Near 0, knob pushed in
RIGHT PLUG-IN EXT
$\times 10$
1 mSEC
CALIBRATED
NORM
Test Load Units (both)
Test Function Low Load
c. Set the Standard Amplitude Calibrator to supply a 0.5 volt square wave signal.
d. Connect the signal through a BNC T connector to the A Triggering TRIGGER INPUT connector and the UPPER BEAM EXT HORIZ IN connector.
e. Connect a patch cord from the A SAWTOOTH connector to the left test load unit Ext Input connector.
f. Rotate the UPPER BEAM EXT HORIZ VAR 1-10 control fully clockwise.
g. Adjust the left test load unit Variable control to display 4 or 5 cycles of the waveform in the Upper Beam graticule area.
h. Position the left edge of the display to the center vertical line of the graticule.
i. Rotate the UPPER BEAM EXT HORIZ VAR $1-10$ control from fully clockwise to fully counterclockwise, then fully clockwise.
i. Check-No more than $\pm 5 \mathrm{~cm}$ horizontal shift of the left edge of the display as the VAR 1-10 control is rotated.
k. Return the VAR $1-10$ control fully clockwise.

## 44. Check External Horizontal Amplifier Variable Control Range-Upper Beam

a. Requirement-At least a 10:1 ratio of horizontal deflection control.
b. Position the left edge of the display to the $2-\mathrm{cm}$ graticule line.
c. Check -5 cm or more of horizontal deflection.
d. Rotate the UPPER BEAM EXT HORIZ VAR 1-10 control fully counterclockwise.
e. Check-Horizontal deflection equal to or less than 10\% of the deflection noted in step (c).
f. Return the VAR 1-10 control fully clockwise.

## 45. Check External Horizontal Amplifier $\times 10$ Compensation-Upper Beam

a. Requirement-Front corner of waveform showing no more than $3 \%$ overshoot, rolloff, or ringing.
b. Check-Front corner of waveform should be similar to Fig. 5-10, showing no more than $3 \%$ overshoot, rolloff, or ringing.


Fig. 5-10. Typical display, External Horizontal Amplifier Compensation check.

## 46. Check External Horizontal Amplifier $\times 1$ Compensation-Upper Beam

a. Requirement-Front corner of waveform showing no more than $3 \%$ overshoot, rolloff, or ringing.
b. Change the DISPLAY MAG switch to $\times 1$.
c. Change the Standard Amplitude Calibrator output to 5 volts. Note amount of horizontal deflection because this information will be checked for step 47 (b).
d. Check-Front corner of waveform similar to Fig. 5-10, and showing no more than $3 \%$ overshoot, rolloff, or ringing.

## 47. Check Magnifier $\times 1-\times 10$ Ratio Accu-racy-Upper Beam

a. Requirement-Ratio of $10: 1$, withia $3 \%$.
b. Measure the horizontal deflection of the display observed in step 46(c).
c. Change the Standard Calibrator output to 0.5 volts.
d. Change the DISPLAY MAG switch to $\times 10$.
e. Check-Horizontal deflection of the display should be within $3 \%$ of the display noted in step 46 (c).
f. Set the Upper Beam INTENSITY control so the display is not visible.

## 48. Check External Horizontal Amplifier DC Balance-Lower Beam

a. Requirement-No more than $\pm 5 \mathrm{~cm}$ horizontal shift of the left edge of the display as the LOWER BEAM EXT HORIZ VAR 1-10 control is rotated.
b. Move the Standard Amplitude Calibrator signal to the LOWER BEAM EXT HORIZ IN connector, and to the B Triggering EXT TRIGGER INPUT connector.
c. Move the patch cord to connect the B SAWTOOTH connector to the right test load unit Ext Input connector.
d. Rotate the LOWER BEAM EXT HORIZ IN VAR 1-10 fully clockwise.
e. Adjust the right test load unit Variable control to display 4 or 5 cycles of the waveform in the Lower Beam graticule area.
f. Position the left edge of the display to the center vertical line of the graticule.
g. Rotate the LOWER BEAM EXT HORIZ VAR 1-10 from fully clockwise to fully counterclockwise, then fully clockwise.
h. Check-No more than $\pm 5 \mathrm{~cm}$ horizontal shift of the left edge of the display as the VAR 1-10 control is rotated.
i. Return the VAR 1-10 control fully clockwise.

## 49. Check External Horizontal Amplifier Variable Control Range-Lower Beam

a. Requirement-Horizontal deflection control ratio of at least 10:1.
b. Position the left edge of the display to the $2-\mathrm{cm}$ graticule vertical line.
c. Check-Horizontal deflection of the display 5 cm or more.
d. Rotate the LOWER BEAM EXT HORIZ VAR $1-10$ control fully counterclockwise.
e. Check-Horizontal deflection equal to or less than $10 \%$ of the deflection noted in step (c).
f. Return the VAR 1-10 control fully clockwise.

## 50. Check External Horizontal Amplifier $\times 1$ and $\times 10$ Compensation-Lower Beam

a. Requirement-Front corner of waveform showing no more than $3 \%$ overshoot, rolloff, or ringing.
b. Check-Front corner of waveform similar to Fig. 5-10, and showing no more than $3 \%$ overshoot, rolloff, or ringing.
c. Change the DISPLAY MAG to $\times 1$.
d. Change the Standard Amplitude Calibrator output to 5 volts. Note amount of horizontal deflection because this information will be needed for step 51 (b).
e. Check-Front corner of waveform similar to Fig. 5-10, and showing no more than $3 \%$ overshoot, rolloff, or ringing.

## 51. Check Magnifier $\times 1-\times 10$ Ratio Accuracy —Lower Beam

a. Requirement-Ratio of 10:1, within 3\%.
b. Measure the horizontal deflection of the display noted in step 50 (d).
c. Change the Standard Calibrator output to 0.5 volts.
d. Change the DISPLAY MAG switch to $\times 10$.
e. Check-Horizontal deflection of the display should be within $3 \%$ of the deflection noted in step 50 (b).
f. Reduce the Lower Beam intensity. Remove the Standard Calibrator signal and the patch cord.
g. Return the $A$ and $B$ Triggering SOURCE switches to NORM INT, and both DISPLAY MAG switches to $\times 1$.
h. Set the Upper Beam DISPLAY switch to LEFT PLUG-IN A and the Lower Beam DISPLAY switch to RIGHT PLUG-IN B.

## 52. Check Z Axis Operation-Upper and Lower Beams

a. Requirement-Noticeable intensity modulation with 10 volt input signal.
b. Set the AMPLITUDE CALIBRATOR to 10 VOLTS.
c. Check that both CRT Cathode Selector switches (on rear panell are set to EXT CRT CATHODE.
d. Adjust the INTENSITY controls of both beams for normal viewing.
e. Remove the two BNC shorting-type caps (on rear panel) from the BNC connectors.
f. Connect a $50 \Omega$ cable from the CAL OUT connector to the Upper Beam BNC conector on the rear panel.
g. Check that the A and B TIME/CM switches are set to 1 mSEC.
h. Check-_Upper Beam CRT display for noticeable intensity modulation (see Fig. 5-11). (INTENSITY setting may have to be reduced to view trace modulation.)
i. Move the CAL OUT signal to the Lower Beam BNC connector.


Fig. 5-11. Typical display, intensity modulation (Z Axis Operation).
i. Check-Lower Beam CRT display for intensity modulation, as in step (h).
k. Remove the AMPLITUDE CALIBRATOR signal and replace both BNC caps.

## 53. Check A Sweep Sawtooth Amplitude

a. Requirement-Sawtooth waveform amplitude equal to or greater than 94.5 volts for a $10.5-\mathrm{cm}$ A Sweep.
b. Set controls as follows:

| A Triggering Controls |  |
| :--- | :--- |
| SOURCE | LEFT INT NORM |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Fully clockwise, knob |
|  | pushed in |
| Upper Beam DISPLAY | LEFT PLUG-IN A |
| Upper Beam DISPLAY MAG | $\times 1$ |
| A TIME/CM | 1 mSEC |
| A VARIABLE | CALIBRATED |
| A MODE | NORM |
| B Triggering Controls |  |
| SOURCE |  |
| COUPLING | RIGHT INT NORM |
| SLOPE | AC |
| MODE | + |
| LEVEL | AUTO STABILITY |
|  | Fully clockwise, knob |
| Lower Beam DISPLAY | pushed in |
| Lower Beam DISPLAY MAG | RIGHT PLUG-IN B |
| B TIME/CM | $\times 1$ |
| B VARIABLE | 1 mSEC |
| B MODE | CALIBRATED |
| MORM |  |

Test Load Units (both)
Test Function
Test Oscilloscope
Time/cm Low Load
c. Connect a $10 \times$ probe to the test oscilloscope vertical amplifier input connector.
d. Set the test oscilloscope vertical deflection switch to 5 volts $/ \mathrm{cm}$.
e. Connect the probe tip to the A SAWTOOTH connector, and adjust the test oscilloscope triggering for a stable display.
f. Check-Test oscilloscope display amplitude of 94.5 volts or more (equal to or greater than 9 volts per cm for the A sweep).

## 54. Check B Sweep Sawtooth Amplitude

a. Requirement-Sawtooth waveform amplitude equal to or greater than 94.5 volts for a $10.5-\mathrm{cm}$ B sweep.
b. Move the probe tip to the B SAWTOOTH connector.
c. Check-Test oscilloscope display amplitude of 94.5 volts or more (equal to or greater than 9 volts per cm for the B sweep).

## 55. Check A Sweep Gate Amplitude

a. Requirement-Gate waveform amplitude 10 volts or more.
b. Connect the probe tip to the A GATE connector.
c. Change the test oscilloscope vertical deflection switch to 0.5 volts $/ \mathrm{cm}$.
d. Check-Gate waveform amplitude 10 volts or more.

## 56. Check B Sweep Gate Amplitude

a. Requirement-Gate waveform amplitude 10 volts or more.
b. Move the probe tip to the B GATE connector.
c. Check-Gate waveform amplitude 10 volts or more.

## 57. Check Delayed Trigger Waveform Amplitude

a. Requirement-Delayed trigger pulse amplitude 7 volts or more.
b. Change the test oscilloscope time/cm switch to 1 microsecond.
c. Check that the vertical deflection switch is set to 0.5 volts $/ \mathrm{cm}$.
d. Move the probe tip to the DLY'D TRIG connector.
e. Rotate the A TIME/CM switch through all positions.
f. Check-Delayed trigger pulse amplitude 7 volts or more.

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## NOTE

Adjustment of the test oscilloscope intensity control may be necessary to observe the pulse at the slower sweep rates.
g. Remove the probe.

## 58. Check Vertical Amplifier Transient Response

a. Requirement-Waveform showing $\leq 2.25 \%$ peak overshoot, rolloff, or ringing.
b. Set the controls as follows:

| A Triggering Controls |  |
| :---: | :---: |
| SOURCE | LEFT INT NORM |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Near 0, knob pushed in |
| Upper Beam DISPLAY | LEFT PLUG-IN A |
| Upper Beam DISPLAY MAG | $\times 1$ |
| A TIME/CM | . 1 mSEC |
| A VARIABLE | CALIBRATED |
| A MODE | NORM |
| B Triggering Controls |  |
| SOURCE | RIGHT INT NORM |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Near 0, knob pushed in |
| Lower Beam DISPLAY | RIGHT PLUG-IN B |
| Lower Beam DISPLAY MAG | $\times 1$ |
| B TIME/CM | . 1 mSEC |
| B VARIABLE | CALIBRATED |
| B MODE | NORM |
| Test Load Units (both) |  |
| Test Function | + Pulse |
| Pulse Repetition Rate | Low |

c. Adjust the right plug-in unit Vertical Position control to move the Lower Beam below the viewing area.
d. With the left plug-in unit Vertical Position control, center the display within the Upper Beam viewing area.
e. Adjust the amplitude of the display to 5 cm with the left plug-in unit Amplitude control. Use the left plug-in unit Vertical Position control to keep the display centered within the Upper Beam viewing area.
f. Check—Upper Beam CRT display for flat top.
g. Change the left plug-in unit Pulse Repetition Rate control to Med.
h. Change the A TIME/CM switch to $.1 \mu \mathrm{SEC}$.
i. Set the Upper Beam POSITION control so the rising portion of the pulse is located near the center of the graticule.
i. With the left plug-in unit Vertical Position control, move the waveform so the front corner is located 3 cm above the Upper Beam graticule center horizontal line. Note the appearance of the front corner of the waveform.
k. Using the left plug-in unit Vertical Position control, move the flat top portion of the display 3 cm below the Upper Beam graticule center horizontal line.
I. Check-For no change in front corner of the waveform. Allowable front corner change is $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$.
m. Change the left plug-in unit Test Function switch to -Pulse, and the Type 556 A Triggering SLOPE switch to -. The waveform will now appear as a negative-going pulse.
n. Repeat step (i) through (I) but position the lower leading corner of the waveform to the same points described in the steps.
o. Check-Change in front corner of the waveform should be $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$.
p. Change the left plug-in unit Test Function switch to +Pulse, and the Type 556 A Triggering SLOPE switch to +.
q. Adjust the left plug-in unit Vertical Position control to move the Upper Beam display below the viewing area.
r. Repeat steps (d) and (e) for the right plug-in unit and Lower Beam.
s. Check--Lower Beam CRT display for flat top.
t. Repeat steps ( $\mathbf{g}$ ) through ( $k$ ) for the right plug-in unit and Lower Beam.
u. Check-For no change in front corner of the waveform. Allowable front corner change is $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$.
v. Repeat steps ( m ) and ( n ) for the right plug-in unit and Lower Beam.
w. Check-Change in front corner of the waveform should be $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$.
x. Change the right plug-in unit Test Function switch to + Pulse, and the Type 556 B Triggering SLOPE switch to + .
y. Change the A Triggering SOURCE switch to RIGHT INT NORM, and the Upper Beam DISPLAY switch to RIGHT PLUGIN A.
z. With the TRACE SEPARATION and right plug-in unit Vertical Position controls, position the rising portion of the displays near their respective graticule centers.
aa. Set the Lower Beam INTENSITY control so the Lower Beam is not visible.
ab. Check—Upper Beam CRT display for optimum square corner and flat top, with peak overshoot, rolloff, or ringing $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$. See Fig. $5-12$ for a typical display.

## 59. Check Vertical Amplifier Risetime-Crossover

a. Requirement-Risetime of the $10 \%$ to $90 \%$ portion of the rising portion should be 6.93 nanoseconds or less with the test load unit pulse risetme of 3 nanoseconds. Fig. 5.13 shows a typical display.

(A) Upper Beam

(B) Lower Beam

Fig. 5-12. Typical displays, high frequency compensations correctly adjusted.


Fig. 5-1 3. Correct positioning of Upper Beam waveform for risetime check.


Fig. 5-14. Correct positioning of Lower Beam waveform for risetime check.

## NOTE

When performing steps 59 through 61, take into consideration sweep timing error, if any, and/or geometry and orthogonality in the area where the measurement is made.
b. Set the Upper Beam DISPLAY MAG switch to $\times 10$.
c. With the TRACE SEPARATION and Upper Beam POSITION controls, position the Upper Beam $5-\mathrm{cm}$ display so that the $10 \%$ point on the rising portion of the waveform crosses the intersection of the Upper Beam graticule center horizontal line with the graticule center vertical line. Fig. 5-13 shows the correct positioning of the display.
d. Check—Risetime of the $10 \%$ to $90 \%$ portion of the pulse risetime should be 6.93 nanoseconds or less.

## 60. Check Vertical Amplifier Risetime-Left

a. Requirement-Risetime of the $10 \%$ to $90 \%$ portion of the rising portion should be 6.93 nanoseconds or less with the test load unit pulse risetime of 3 nanoseconds.
b. Change the A Triggering SOURCE switch to LEFT INT NORM.
c. Change the Upper Beam DISPLAY to LEFT PLUG-IN A.
d. With the left test load unit Vertical Position and Upper Beam POSITION controls, position the $5-\mathrm{cm}$ display so that the $10 \%$ point on the rising portion of the waveform is at the same point as in step 59 (c).
e. Check-Risetime of the $10 \%$ to $90 \%$ portion of the pulse rise should be 6.93 nanoseconds or less.

## 61. Check Vertical Amplifier Risetime-Right

a. Requirement-Risetime of the $10 \%$ to $90 \%$ portion of the rising portion should be 6.93 nanoseconds or less with the test load unit pulse risetime of 3 nanoseconds.

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b. Check that the B TIME/CM switch is set to $.1 \mu \mathrm{SEC}$.
c. Set the Lower Beam DISPLAY MAG switch to $\times 10$.
d. Rotate the left plug-in unit Vertical Position control so that the Upper Beam display is below the viewing area, and increase the Lower Beam INTENSITY so that the Lower Beam display is visible.
e. Position the $5-\mathrm{cm}$ Lower Beam display so that the $10 \%$
point on the rising portion crosses the intersection of the $1-\mathrm{cm}$ horizontal graticule line and the graticule center vertical line. See Fig. 5-14 for correct display positioning.
f. Check-Risetime of the $10 \%$ to $90 \%$ portion of the rising portion should be 6.93 nanoseconds or less with the test load unit pulse risetime of 3 nanoseconds. Fig. 5-14 shows a typical display.

# SECTION 6 CALIBRATION 

Change information, if any, affecting this section is found at the rear of the manual.

## Introduction

This calibration procedure can be used either for complete calibration of the Type 556 to return it to original performance, or as an operational check of the instrument performance. Completion of every step in this procedure will return the Type 556 to its original standards. If a complete calibration of the instrument is not desired, refer to the "Calibration Index" for the page location of individual step instruction.

## General Information

The calibration of the Type 556 should be checked at regular intervals to insure that it is operating properly and accurately. (See the Maintenance section of this manual for the recommended recalibration interval.) In addition, certain portions of the instrument must be recalibrated after tubes or transistors have been changed or repairs have been made. A complete procedure is provided in this section for checking the calibration of the Type 556, and for making adjustments when necessary.

In the instructions that follow, the steps are arranged in convenient sequence to avoid unnecessary repetition. If a complete recalibration is not needed, individual steps may be performed separately only if those steps do not affect any other adjustments.

Important information and preliminary settings of controls are given at the beginning of the calibration procedure. Any controls that are not mentioned are not critical during that portion of the procedure. Test equipment used in a particular step should remain connected at the end of the step unless instructions state otherwise. If only part of the procedure is being performed, it may be necessary to check back to the last major setup change to determine the test equipment connections and setting of controls.

Internal controls should not be preset unless the instrument has been repaired or is known to be seriously out of adjustment. If repairs have been made, preset internal controls to mid-range in the affected circuits.

> NOTE
> Certain adjustments is some circuits interact with adjustments in other circuits in the instrument. Refer to the schematic diagrams; if in doubt about the effect of an adjustment on other circuits, check the calibration of all closely associated circuits.

If adjustments are made on the power supplies, the calibration of the entire instrument should be checked. In particular, the sweep rates and vertical deflection factors will be affected.

## RECOMMENDED EQUIPMENT <br> (see Figs. 6-1 through 6-3)

## General

The following equipment or its equivalent is recommended for complete calibration of the Type 556. Specifications given are the minimum necessary for accurate calibration of this instrument. All test equipment is assumed to be correctly calibrated and operating within the orginal specifications. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

## Special Test Equipment

For the quickest and most accurate calibration, special calibration fixtures are used where necessary. All calibration fixtures listed under "Recommended Equipment" can be obtained from Tektronix, Inc. Order by part number through your local Tektronix Field Office or representative.

1. Test oscilloscope. Bandwidth, DC to $10 \mathrm{MHz}_{\text {; }}$ minimum deflection factor, 0.005 volts/division; $1 \times$ and $10 \times$ probes. Tektronix Type 531A Oscilloscope recommended, with Type W plug-in.
2. $10 \times$ probe with BNC connector. Tektronix Type P6006 recommended. Part No. 010-0128-00.
3. $1 \times$ probe with BNC connector. Tektronix Type P6028 recommended. Part No. 010-0120-00.
4. Time-mark generator. Marker outputs, 5 seconds to 0.1 microsecond; sine-wave output at 50 MHz . Tektronix Type 184 recommended.
5. Constant-amplitude sine-wave generator. Frequencies, 50 kHz and 350 kHz up to $\geq 50 \mathrm{MHz}$; output amplitude, at least 1 volt; amplitude accuracy, $\pm 5 \%$ into $50 \Omega$ load. Tektronix Type 191 recommended.
6. Test load and pulser unit. Tektronix Calibration Fixture, Part No. 067-0521-00 (2 required).
7. Precision DC voltmeter. Accuracy, within $\pm 0.05 \%$; meter resolution $50 \mu \mathrm{~V}$; range, 0.1 to 500 volts. For example, Fluke Model 801 B .
8. Amplitude calibràtor. Amplitude accuracy, within $0.25 \%$; signal amplitude, 0.1 volts to 100 volts; output signal, 1 kHz square-wave and $+D C_{i}$ must have mixed display feature. Tektronix Calibration Fixture 067-0502-00 recommended.
9. DC voltmeter. Minimum sensitivity, $20,000 \Omega /$ volt; accuracy checked to within $1 \%$ at -1850 volts. For example, Simpson Model 262.

fig. 6-1. Recammanded calibration equipment. Itams 1 through 12.


Fig. 6-2. Recommended calibration equipment. Ifoms 13 through 23.

## Calibration-Type 556



Fig. 6-3. Adjustment tools.
10. Variable autotransformer. Must be capable of supply1 kVA over a voltage range of 90 to 130 VAC ( 182 to 260 volts for 230 -volt nominal line). If autotransformer does not have an AC voltmeter (RMS), monitor the output with a voltmeter having a range of at least 130 volts (or 260 volts). For example, General Radio W10MT3W Metered Variac Autotransformer.
11. Plug-in preamplifiers with dual channel inputs, vertical deflection sensitivity to 5 millivalts $/ \mathrm{cm}$. Tektronix Type 1 Al or equivalent, 2 required. Include one 18 -inch $50 \Omega$ cable (Tektronix Part No. 012-0076-00) supplied with the plug-in unit.
12. Low-frequency sine-wave signal generator, 30 Hz to 60 kHz , 1 volt output, Heathkit Model 1G-72 or equivalent.
13. Current probe. Sensitivity, 1 milliamp/division; accuracy, within $3 \%$. Tektronix P6019 Current Probe with Type 134 Amplifier recommended.
14. 3-wire socket assembly (required only if autotransformer is equipped with a single output power socket). Tektronix Part No. 136-0102-00.
15. 3 -wire power cable 20 inches long (required only if autotransformer is equipped with a single output power socket). Tektronix Part No. 161-0014-00.
16. Precision 50 -ohm termination. For example, Tektronix Calibration Fixture Part No. 067-0515-00.
17. Termination (two). Impedance, 50 ohm; accuracy, $\pm 3 \%$; connectors, BNC. Tektronix Part No. 011-0049-00.
181. $5 \times$ attenuator. Impedance, 50 ohm; accuracy, $\pm 3 \%$; connectors, BNC. Tektronix Part No. 011-0060-00.
191. $10 \times$ attenuator. Impedance, 50 ohm; accuracy, $\pm 3 \%$; connectors, BNC. Tektronix Part No. 011-0059-00.
20. BNC T connector. Tektronix Part No. 103-0030-00.
21. Adapter. Connectors, GR to BNC jack. Tektronix Part No. 017-0063-00.
22. Cable (four). Impedance, $50 \Omega$; type, RG58A/U; length, 42 inch; connectors, BNC. Tektronix Part No. 012-0057-00.
23. Patch cord, 18 inch with BNC plug-in jack terminals on zach end. Tektronix Part No. 012-0087-00.

Adjustment tools (see Fig. 6-3)

| Description | Tektronix <br> Part No. |
| :--- | :---: |
| a. Insulated screwdriver (1 $1 / 2$ <br> metallic | $003-0000-00$ |
| b. Screwdriver, 3 inch shaft, non- | $003-0192-00$ |
| c. Tuning rod, 5 inch | $003-0301-00$ |
| d. Tuning tool |  |
| Handle <br> Insert, for $5 / 64$ inch (ID) hex cores | $003-0307-00$ |
| IItems 18 and 19 are needed if a generator does not have an out- <br> put amplitude control. |  |

## CALIBRATION RECORD AND INDEX

This Abridged Calibration Procedure is provided to aid in checking the operation of the Type 556. It may be used as a calibration guide by the experienced calibrator, or it may be used as a calibration record. Since the step numbers and titles used here correspond to those used in the complete Calibration Procedure, the following procedure serves as an index to locate a step in the complete Calibration Procedure. Characteristics are those listed in the Characteristics section of the Instruction Manual.

Type 556, Serial No.
Calibration Date

```
1. Adjust Power Supply (Page 6-9)
    Adjust \(-150 \mathrm{~V}, \pm 1.5 \mathrm{~V}\)
    Adjust \(+100 \mathrm{~V}, \pm 1 \mathrm{~V}\)
    Adjust \(+225 \mathrm{~V}, \pm 0.625 \mathrm{~V}\) (measured between +100 V
        and +225 V )
    Check \(+350 \mathrm{~V}, \pm 10.5 \mathrm{~V}\)
```

2. Check Power Supply Ripple and Regulation (page 6-10)

Low Load at High Line
Maximum Ripple (Peak-to-Peak)

| -150 V | 5 mV |
| :--- | ---: |
| +100 V | 5 mV |
| +225 V | 10 mV |
| +350 V | 15 mV |

3. Check Power Supply Ripple and Regulation (page 6-12)

High Load at Low Line
Maximum Ripple (Peak-to-Peak)

| -150 V | 5 mV |
| :--- | ---: |
| +100 V | 5 mV |
| +225 V | 10 mV |
| +350 V | 15 mV |

4. Adjust High Voltage-Lower Beam (page 6-12)

Adjust $-1850 \mathrm{~V}, \pm 55 \mathrm{~V}$.
5. Adjust High Voltage-Upper Beam (page 6-12)

Adjust $-1850 \mathrm{~V}, \pm 55 \mathrm{~V}$.
6. Adjust Amplitude Calibrator (page 6-14)

Voltage accuracy, $\pm 2 \%$.
7. Check Terminated Voltage (page 6-15)

Accuracy, $1 / 2$ indicated $V \pm 2 \%$ when terminated in $50 \Omega$.
8. Check Repetition Rate (page 6-15)

Rate $1 \mathrm{kHz} \pm 25 \%$.
9. Check Duty Cycle (page 6-15)

Duty cycle, 45 to $55 \%$.
10. Check Risetime (page 6-16)

Risetime, $\leq 1.5$ microseconds.11. Check 5 mA Current Loop (page 6-16)

5 mA through probe loop.
12. Check Horizontal Deflection/Graticule Alignment (page 6-16)
Trace parallel to horizontal graticule lines.13. Check Beam Finder Switch Operation (page 6-17) Over-scanned display returned to viewing area.14. Adjust Geometry (page 6-18) Best overall geometry.15. Adjust Focus and Astigmatism (page 6-19) Sharp, well-defined displays.16. Check Upper and Lower Beam Scan Areas (page 6-19)
$\geq 6 \mathrm{~cm} \times 10 \mathrm{~cm}$ per beam, except for graticule corners.17. Check CRT Orthogonality (page 6-20)
$90^{\circ} \pm 1^{\circ}$.18. Adjust Vertical Amplifier DC Balance-Left (page 6-20)
Trace centering with balance control.19. Adjust Vertical Amplifier DC Balance-Right (page 6-21)
Trace centering with balance control.20. Check Trace Separation Range (page 6-21) Trace superimposition within the center $4-\mathrm{cm}$ area of the graticule.21. Adjust Vertical Amplifier Gain (page 6-22) Correct vertical deflection.22. Check Vertical Amplifier Compression/Expansion (page 6-23) $\leq 0.5 \mathrm{~mm}$ compression/expansion with 2 cm signal.23. Check Common Mode Rejection (page 6-23)

Display amplitude $\leq 3 \mathrm{~mm}$ with common-mode input of 1 volt to test load unit.24. Check Trace Drift with Line Voltage Change (page 6-24)
$\leq \pm 2 \mathrm{~mm}$ within line voltage change limits.25. Check Alternate-trace Operation (page 6-26) Trace alternation at all sweep rates.26. Check Multi-trace Chopping Transient Blanking (page 6-26)
Blanking of switching transients in the chopped mode.27. Adjust External Triggering-A and B Sweeps (page 6-27)
Correct trigger operation; see Calibration Procedure.28. Check B Triggering Level Control Ranges (page 6-28) Normal, $\geq \pm 2 \mathrm{~V} ; \times 10$ range increase, $\geq \pm 20 \mathrm{~V}$.29. Check $A$ Triggering Level Control Ranges (page 6-29) Normal, $\geq \pm 2 \mathrm{~V} ; \times 10$ range increase, $\geq \pm 20 \mathrm{~V}$.30. Check Internal Triggering-Lower Beam (page 6-30) Correct triggering with minimum deflections.
$\square$ 31. Check Internal Triggering-Upper Beam (page 6-31) Correct triggering with minimum deflections.32. Check Crossover Triggering (page 6-31)

Correct triggering with minimum deflections.33. Check Auto Stability Operation (page 6-32)

Sweep triggering at 30 Hz .
Sweep free-runs with no signal.34. Check Line Trigger and LF Reject Operation (page 6-32)
Triggering at line frequency; no triggering at low frequencies.
35. Check A and B Single Sweep Operation (page 6-32) Sweeps trigger with same trigger level as in AUTO STABILITY; sweeps lock out until reset.
36. Adjust Basic Timing-A Sweep (page 6-33)

Sweep timing within $\pm 3 \%$ of indicated sweep rate at $\times 1$ and $\pm 5 \%$ at $\times 10$.37. Adjust Upper Beam Sweep Magnifier Registration (page 6-34) $\leq 0.5 \mathrm{~cm}$ shift when switching from magnified to normal sweep.
$\square$ 38. Adjust A Sweep Sawtooth Amplitude (pages 6-34) Sweep length $10.5 \mathrm{~cm} \pm 0.5 \mathrm{~cm}$ at 1 millisecond $/ \mathrm{cm}$.39. Adjust B Sweep Sawtooth Slope (page 6-34)

Timing adjustment to match the B sweep generator to the A sweep generator.40. Adjust B Sweep Sawtooth Amplitude (page 6-35) Sweep length $10.5 \mathrm{~cm} \pm 0.5 \mathrm{~cm}$ at 1 millisecond $/ \mathrm{cm}$.41. Adjust Basic Timing-B Sweep (page 6-35)

Sweep timing within $\pm 3 \%$ of indicated sweep rate at $\times 1$ and $\pm 5 \%$ at $\times 10$.42. Adjust Lower Beam Sweep Magnifier Registration (page 6-35) $\leq 0.5 \mathrm{~cm}$ shift when switching from magnified to normal sweep.
43. Adjust Lower Beam A Sweep Gain (page 6-36)

Sweep timing within $\pm 5 \%$ of indicated sweep rate. This step is not applicable to 556 instruments with serial numbers 100 to 1999.44. Adjust A and B Sawtooth Currents (page 6-36) Sawtooth current waveforms at plug-in unit connectors, pin 6.45. Check Delay-Time Multiplier Dial Setting (page 6-37) Counterclockwise setting, $00.20, \pm 2$ minor divisions; clockwise setting, 10.20, $\pm 4$ minor divisions.46. Adjust Delay Start and Stop (page 6-38) Correct adjustment, $\pm 8$ minor divisions.47. Check Delay-Time Multiplier Incremental Linearity (page 6-39)
$\pm 2$ minor divisions from 1.00 to 9.00 major dial divisions.
48. Check Delay-Time Jitter (page 6-39)

Jitter $\leq 0.5 \mathrm{~cm}$.49. Adjust Timing-A Sweep (page 6-40) Sweep timing within $\pm 3 \%$ of indicated sweep rate.
50. Adjust Horizontal Amplifier 50 MHz compensationsUpper Beam (page 6-42)
Timing accuracy $\pm 5 \%$ (or $\pm 4 \mathrm{~mm}$ ) 4 cm from sweep start to 70 cm from sweep start.
51. Check Timing and Delaying Sweep Accuracy-A Sweep (page 6-43)
A Sweep accuracy, $\pm 3 \%$ or 2.4 mm ; delaying sweep, within 8 minor divisions of the DELAY-TIME MULTIPLIER dial for each position of the A TIME/CM switch.52. Adjust Timing-B Sweep (page 6-44)

Sweep timing within $\pm 3 \%$ of indicated sweep rate.
53. Adjust C882-B Sweep Crossover Compensation (page 6-44)
Timing accuracy, $\pm 3 \%$, Upper Beam display.
54. Adjust Horizontal Amplifier 50 MHz CompensationLower Beam (page 6-45)
Timing Accuracy $\pm 5 \%$ (or $\pm 4 \mathrm{~mm}$ ) 4 cm from sweep start to 70 cm from sweep start.
55. A Sweep Crossover Compensation (page 6-46) Tolerance, $\pm 3 \%$ or $\pm 2.4 \mathrm{~mm}$.
This step is not applicable to 556 instruments with serial numbers 100 to 1999.
56. Check Timing Accuracy-B Sweep (page 6-46)

Timing accuracy within $\pm 3 \%$ of indicated sweep rate.57. Check Variable Time/cm Range (page 6-46) $\geq 2.5: 1$ reduction in $A$ and $B$ Sweep rates.58. Check Trigger Delay (page 6-46)

Trigger delay $\leq 150$ nanoseconds.59. Adjust External Horizontal Amplifier DC BalanceUpper Beam (page 6-47)
$\leq \pm 5 \mathrm{~cm}$ horizontal shift of the left edge of the display as the UPPER BEAM EXT HORIZ VAR $1-10$ control is rotated.60. Check External Horizontal Amplifier Variable Control Range-Upper Beam (page 6-48)
$\geq 10: 1$ ratio of horizontal deflection control.61. Adjust External Horizontal Amplifier $\times 10$ Compensa-tion-Upper Beam (page 6-49)
$\leq 3 \%$ overshoot, rolloff, or ringing.62. Adjust External Horizontal Amplifier $\times 1$ Compensa-tion-Upper Beam (page 6-49) $\leq 3 \%$ overshoot, rolloff, or ringing.63. Check Magnifier $\times-1 \times 10$ Ratio Accuracy-Upper Beam (page 6-49)
Ratio of $10: 1$, within $3 \%$.64. Adjust External Horizontal Amplifier DC BalanceLower Beam (page 6-49)
$\leq 5 \mathrm{~cm}$ horizontal shift of the left edge of the display as the LOWER BEAM EXT HORIZ VAR 1-10 control is rotated.
65. Check External Horizontal Amplifier Variable Control Range-Lower Beam (page 6-50) $\geq 10: 1$ ratio of horizontal deflection control.66. Adjust External Horizontal Amplifier $\times 1$ and $\times 10$ Compensations-Lower Beam (page 6-50) $\leq 3 \%$ overshoot, rolloff, or ringing.67. Check Magnifier $\times 1-\times 10$ Ratio Accuracy-Lower Beam (page 6-50)
Ratio of $10: 1$, within $3 \%$.
68. Check Z Axis Operation-Upper and Lower Beams (page 6-50)
Intensity modulation with 10 -volt signal.69. Check A Sweep Sawtooth Amplitude (page 6-50) $\geq 94.5 \mathrm{~V}$ for a 10.5 cm A sweep.70. Check B Sweep Sawtooth Amplitude (page 6-52) $\geq 94.5 \mathrm{~V}$ for a 10.5 cm B sweep.71. Check A Sweep Gate Amplitude (page 6-52) Waveform amplitude $\geq 10 \mathrm{~V}$.72. Check B Sweep Gate Amplitude (page 6-52) Waveform amplitude $\geq 10 \mathrm{~V}$.73. Check Delayed Trigger Waveform Amplitude (page 6-52)
Pulse amplitude $\geq 7 \mathrm{~V}$.74. Adjust 8608 Bias Control (page 6-52)

Front corner waveform change $\leq 2.25 \%$ overshoot, rolloff, or ringing.75. Adjust Vertical Amplifier High Frequency Compensa-tions-Left (page 6-53) $\leq 2.25 \%$ overshoot, rolloff, or ringing.76. Adjust Vertical Amplifier High Frequency Compensa-tions-Crossover (page 6.55) $\leq 2.25 \%$ overshoot, rolloff, or ringing.77. Adjust Vertical Amplifer High Frequency Compensa-tions-Right (page 6-55)
$\leq 2.25 \%$ overshoot, rolloff, or ringing.78. Check Vertical Amplifier Risetime-Right (page 6-56) $\leq 6.93$ nanoseconds with test load unit.79. Check Vertical Amplifier Risetime-Crossover (page 6-56)
$\leq 6.93$ nanoseconds with test load unit.
80. Check Vertical Amplifier Risetime—Left (page 6-56) $\leq 6.93$ nanoseconds with test load unit.
81. Check High Frequency Triggering (page 6-57) Stable displays with 50 MHz signals.

## CALIBRATION PROCEDURE

## General

In the following calibration procedure, a test equipment setup is shown for each major setup change. Complete control seitings are listed following the picture. To aid in locating individual controls which have been changed during a major calibration step, these controls are listed at the beginning of the step. If only a partial calibration is performed, start with the nearest major setup preceding the desired portion.

## NOTE

When performing a complete recalibration best performance will be obtained if each adjustment is made to the exact setting, even if the Check is within the allowable tolerance.
The following procedure uses the equipment listed under "Recommended Equipment". If substitute equipment is used, control settings or setup must be altered to meet the requirements of the equipment used.

## Preliminary Procedure

1. Remove the side, bottom, and top covers from the Type 556.
2. Connect the autotransformer (if used) to a suitable power source.
3. Connect the Type 556 power cord to the autotransformer output (or directly to the power source).
4. Install two test load units in the Type 556.
5. Preset the Type 556 and test load unit controls as follows:


Fig. 6.4. Inlilal test selup for power supply valtage adusiment.

Type 556
A Triggoring Controls
SOURCE
COUPLING
SLOPE
MODE
level

Upper Beam Controls
DISPLAY
POSITION
DISPLAY MAG
INTENSITY
FOCUS
ASTIGMATISM
CONTRAST
UPPER BEAM EXT
HORIZ VAR 1-10

A Sweep Controls

| A TIME/CM | .5 mSEC |
| :--- | :--- |
| VARIABLE | CALIBRATED |
| A MODE | NORM |

B Triggering Conirols SOURCE
COUPLING
SLOPE
MODE
LEVEL

Lower Beam Controls DISPLAY POSITION DISPLAY MAG INTENSITY FOCUS ASTIGMATISM CONTRAST LOWER BEAM EXT HORIZ VAR 1.10

B Sweep Controls
B TIME/CM
VARIABLE

B MODE
SCALE ILLUMINATION
TRACE SEPARATION
DELAY-TIME MULTIPLIER
AMPLITUDE CALIBRATOR
POWER

NORM INT, RIGHT
AC
$+$
TRIG
Clockwisa, knob pushed in

RIGHT PLUG•IN B
Mid-range
$\times 1$
0

0
0
Clockwise
Clockwise
.5 mSEC
CAlibrated
NORM
0
Mid-range
1.00

OFF
Off

Rear Panel Controls

| Upper Beam CRT | EXT CRT CATHODE |
| :--- | :--- |
| Cathode Selector |  |
| Lower Beam CRT <br> Cathode Selector | EXT CRT CATHODE |

Test Load Vertical Plug-In Units (both units)

| Test Function | Low Load |
| :--- | :--- |
| Variable | Mid-range |
| Amplitude | Mid-range |
| Vertical Position | Mid-range |
| Repetition Rate | Low |

6. Set the autotransformer for 115 VAC , turn the POWER switch to ON and allow 20 minutes for instrument warmup.

## 1. Adjust Power Supply Voltages

a. The initial test equipment setup is shown in Fig. 6-4.
b. Set the precision DC voltmeter (item 7 of Recommended Equipment) to the -150 volt range.
c. Connect the voltmeter negative lead to the output end of fuse F1482 (Fig. 6-4), and connect the positive lead to chassis ground.
d. Check—A reading of -150 volts, $\pm 1.5$ volts.
e. Adjust R1498 (Fig. 6-4) for a reading of -150 volts.
f. Set the voltmeter to the 100 -volt range. Connect the positive meter lead to fuse F1478 ( Fig. 6-4), and connect the negative lead to chassis ground.
g. Check-A reading of +100 volts, $\pm 1.00$ volt.
h. Adjust R1459 (Fig. 6-4) for a reading of +100 volts.
i. Set the voltmeter to the +125 volt range.
i. Connect the negative meter lead to the +100 -volt fuse F1478, and connect the positive meter lead to the +225 -volt fuse F1446 (Fig. 6-4).
k. Check—A reading of +125 volts, $\pm 0.625$ volts.

1. Adjust R1439 (Fig. 6-4) for a meter reading of +125 volts.
m . Set the meter to the +350 -volt range, and connect the positive meter lead to fuse F1424 (Fig. 6-4).
n . Connect the negative meter lead to the oscilloscope chasis ground.
o. Check-A meter reading of +350 volts, $\pm 10.5$ volts.
p. Disconnect the meter leads.

## NOTES

## Calibration-Type 556



Fig. 6-5. Iniflal tait selup for chesking powar aupply fipple and regulailon.

## 2. Check Power Supply Ripple and RegulationLow Load at High Line Voltage <br> NOTE

The following procedure applios only to a Type 556 connacted to a nominal 115 -volt 3 -wire power source. For an instrument connected to other than a nominal 115 -volp source, a procedure and test fixtures adaplad to local conditions will be required; for example, a 230 -volt source will require an autolransformer with the higher output, an isolation transformer for the test oscilloscope, power sockets, etc.
a. Tho initial test setup is shown in Fig. 6-5. Type 556 controls remain as in Step 1; other conirol seltings are as follows:

Test Load Unit (bolh)
Test Function
Low Load
Test Oscilloscope
Time/cm
5 milliseconds
Type W

| AC.DC-GND [A] | DC |
| :--- | :--- |
| AC-DC-GND (B] | GND |
| Input Allen | 100 |
| Millivolis/cm | 50 |


| Display | A.Ve |
| :--- | :--- |
| Ve Range | 0 |
| Aulotransformer | 134 (RMS] |

b. Connact the 20 -inch power cord between the autalrans. formar and the power sockal assambly, and connoct tha Type 556 power cord to the powar sackat asembly, as shown in Fig. 6-5.

## NOTE

The short power cord and the socket assembly (items 14 and 15 of Recommended Equipment) are used only to provide convenient measurement terminals with a minimum of hazard. If the aulotransformer used is equipped with more than one oulput socket, the cord and sockel assembly may be eliminated.
c. Connect a $1 \times$ probe to the test oscilloscope input connector.
d. Connect the probe ground lead to the ground pin of one of the sockats in the power socket assembly.
e. With the probe lip, determine which of the two remaining socket contacts is the neutral contact, and connect the probe tip to this socket conlact.
f. Change the Type $W$ Millivalts/cm switch to 20 . The vertical deflection sensitivily should now be 2 volts/cm.


Fig. 6-6. Illustrating measurement of voltage drop in neutral wire. Probe connected between grounding pin and neutral wire; Type W Time/cm, 5 milliseconds; vertical sensitivity, 2 volts/cm.
g. Measure the peak voltage of the waveform, as shown in Fig. 6-6.
h. Set the Type $W$ Comparison Voltage (Vc) dial to 178 plus the voltage reading obtained in step (g).

Example: If the reading obtained in step (g) was 2.4 volts, the dial should be set to 180.4 .
i. Set the Ve Range to +11 .
i. Change the Millivolt/cm switch to 10.
k. Move the probe tip from the neutral contact to the highvoltage or "hot" contact in the power socket assembly.
I. Adjust the autotransformer output until the tips of the waveforms shown on the test oscilloscope reach the reference line established previously by the Type W. (See Fig. 6-7 for typical display). The test oscilloscope is now indicating 178 peak VAC at the autotransformer output, or 126 volts RMS (RMS $\times 1.414=$ Peak).
m. Change the Vc Range to 0 , and the $A C-D C-G N D$ switch to AC.
n. Remove the probe tip and ground lead from the power socket contacts, connect the probe tip to the Type $556+100-$ volt fuse (output end), and connect the probe ground lead to the chassis ground.

## CAUTION

When the Type $W$ is used with the AC-DC-GND switch in the AC coupling position, the Input Atten switch must be set (steps $q, t$, and $w$ that follow) so that input voltages applied internally to the $W$ unit amplifier are attenuated to 15 volts or less


Fig. 6-7. Illustrating method of peak line voltage measurement; Type $W$ plug-in vertical deflection factor $1 \mathrm{~V} / \mathrm{cm}$; sweep rate 5 milliseconds/cm.
until the input coupling capacitor is charged. Failure to observe this precaution when connecting the probe to the Type 556 power supply fuses may result in damage to Type $W$ components.
o. Change the Input Atten switch to 1, and the Millivolts/ cm to 5 .
p. Check-Ripple amplitude not to exceed 5 millivolts/cm (See Table 6-1).

TABLE 6-1
Power Supply Ripple Tolerances

| Power Supply | Ripple (Peak-to-Peak) |
| :---: | :---: |
| -150 | 5 millivolts |
| +100 | 5 millivolts |
| +225 | 10 millivolts |
| +350 | 15 millivolts |

Remove the probe tip, and change the Input Atten to 100.
r. Connect the probe to the -150 -volt fuse, and change the Input Atten to 1.
5. Check-Ripple amplitude not more than 5 millivolts.
t. Remove the probe tip, and change the Input Atten to 100.
u. Connect the probe to the +225 -volt fuse, and change the Input Atten to 1.
v. Check-Ripple amplitude not more than 10 millivolts.


Fig. 6-8. Typical test oscilloscope display of power supply ripple, -150 volt supply ( 60 cycle line). Vertical deflection, 0.005 volts/cm; sweep rate, 5 milliseconds/cm; low load condition.
w. Remove the probe, and change the Input Atten to 100 .
$x$. Connect the probe to the +350 -volt fuse, and change the Input Atten to 1.
y. Check—Ripple amplitude not more than 15 millivolts.
z. Disconnect the probe and ground lead from the Type 556.

## NOTE

With the Type 556 power supply regulation circuits operating normally, the DC regulated voltages will not deviate from the specified tolerances when the line voltage is varied between the lower and upper voltage limits. This is due to the use of transistors in the regulating circuits; therefore a check of the ripple amplitudes present will be an accurate check of the limits of regulation. For this reason the normal monitoring of the $D C$ voltages has been omitted from the procedure.

## 3. Check Power Supply Ripple and RegulationHigh Load at Low Line Voltage

a. Change Input-A AC-DC-GND to $D C$, the Input Atten to 100, and the Millivolts/cm to 20.
b. Change both test load unit Test Function switches to High Load and set the AMPLITUDE CALIBRATOR switch to 100 V DC.
c. Set the autotransformer output to approximately 100 volts, as shown on the RMS meter.
d. Repeat steps 2 (d), (e), and (g).
e. Set the Comparison Voltage (Vc) dial to 141.1 plus the reading obtained in step (g).
Example: If the peak reading obtained in step ( $g$ ) was 3.0 volts, set the dial to 144.4 .
f. Repeat steps 2 (i), (i), and (k).
g. Adjust the autotransformer output until the tips of the waveforms shown on the test oscilloscope reach the reference line established previously by the Type W . The test oscilloscope is now indicating 141.4 volts peak $A C$ at the autotransformer output, or 100 volts RMS.
h. Repeat steps $2(\mathrm{~m})$ through (z).
i. Return the autotransformer output to 115 volts.

## 4. Adjust High Voltage-Lower Beam

a. Set the $D C$ voltmeter (item 9 of Recommended Equipment) to the high voltage range.
b. Connect the meter leads from the high voltage test point to chassis ground, as shown in Fig. 6-10.


Fig. 6-9. Typical display showing ripple on +350 -volt supply ( 60 cycle line). Vertical deflection, 0.005 volts $/ \mathrm{cm}$; sweep rate, 5 milliseconds/cm; high load condition.
c. Check—A meter reading of -1850 volts $\pm 55$ volts.
d. Adjust High Voltage control R1332 for a meter reading of -1850 volts. Fig. $6-10$ shows the controi location.

## 5. Adjust High Voliage-Upper Beam

a. Connect the meter leads from the high voltage test point to chassis ground, as shown in Fig. 6-11.
b. Check-A meter reading of -1850 volts, $\pm 55$ volts.
c. Adjust High Voltage control R1382 for a meter reading of -1850 volts. Fig. 6-11 shows the control location.
d. Remove the meter leads.


Fig. 6-10. Tast setup for adjusting high veliage—lowar geam.


Fig. 6-11. Tasl ratup for adusiling high voliage——Upper Baam.

## NOTES



Pig. 6-12, Tast selup for Amplitude Callbralar adjualmant.

## 6. Adjust Amplitude Calibrator

a. Tost oquipment selup as shown in Fig. 6-12.
b. Connect a 50 n cable from the Type 556 CAL OUT connector to the Standard Amplitude Calibrator Unknown Input connector. Check that the Type 556 AMPLITUDE CALI. BRATOR switch is sol to 100 VDC .
c. Connect a $50 \Omega$ cable from tho test ascilloscope vertical input connector to the Output connector on the Standard Amplituda Calibrator. Set the Standard Amplitude Calibrator 10 100 Volls, $+D C$, Mixed.
d. Set the test oscilloscope input for AC coupling, and the vertical deflection factor to 1 volr $/ \mathrm{cm}$.
e. Set the test oscilloscopo controls for a free-running display centered on the graticule.
f. Check-Amplitude of display not more than 2 cm . See Fig. 6.14 for a lypical display.
g. Adjust R1628 (Fig. 6.13) lo reduce the display amplitude to zero.
h. Turn tho Type 556 POWER switch off.
i. Connect a shori jumper wire with insulated elips bolween the paints shown in Fig. 6-13. Care should be used to avoid louching adjacent components or leads with the jumper terminal clips.


[^1]
## NOTE

The jumper wire applies - 150 volts to the grid of V1605B, cutting it off and placing the cathode of V1605C at +100 volts for convenient checking of the AMPLITUDE CALIBRATOR switch divider network.

TABLE 6-2
Amplitude Calibrator Adjustment

| AMPLITUDE <br> CALIBRATOR <br> VOLTS | Standard <br> Calibrator <br> Volts | Test Oscilloscope |  |
| :---: | :---: | :---: | :---: |
| 100 | 100 | V/cm AC | Deflection <br> (max) |
| 50 | 50 | 0.5 | 0 cm <br> (adjusted) <br> 2 cm |
| 20 | 20 | 0.2 | 2 cm |
| 10 | 10 | 0.1 | 2 cm |
| 5 | 5 | 0.05 | 2 cm |
| 2 | 2 | 0.02 | 2 cm |
| 1 | 1 | 0.01 | 2 cm |
| .5 | 0.5 | 0.005 | 2 cm |
| .2 | 0.2 | 0.005 | 0.8 cm |
| .1 | 0.1 | 0.005 | 0.4 cm |



Vertical sensifivity, 1 volt/cm.

Fig. 6-14. Typical display, Amplitude Calibrator adjusłment.
i. Turn the POWER switch to ON.
k. Set the AMPLITUDE CALIBRATOR and Standard Amplitude Calibrator switches as shown in Table 6-2, checking for the deflection tolerances listed.

## 7. Check Terminated Voltage Accuracy

a. Set the Type 556 AMPLITUDE CALIBRATOR to .2 VOLTS and the Standard Amplitude Calibrator to 0.1 V .
b. Insert the precision $50 \Omega$ termination (item 16 listed under Recommended Equipment) between the Type 556 CAL

OUT connector and the $50 \Omega$ cable, using adapters as necessary.
c. With the test oscilloscope vertical deflection switch at 0.005 volts $/ \mathrm{cm}$, note a deflection of 0.4 cm or less.
d. Remove the Standard Amplitude Calibrator signal and the precision termination.
e. Turn off the Type 556 POWER switch, remove the jumper wire, and turn the POWER switch ON.

## 8. Check Amplitude Calibrator Repetition Rate

a. Set the AMPLITUDE CALIBRATOR to 1 VOLTS.
b. Connect an 18 -inch $50 \Omega$ cable (this cable is furnished with the Type 1A1) from the CAL OUT connector to the test oscilloscope vertical input.
c. Set the vertical deflection factor of the test oscilloscope plug-in to 0.5 volts/ cm and obtain a stable display at a sweep rate of 0.2 milliseconds $/ \mathrm{cm}$.
d. Check-1 cycle of the displayed waveform between 3.75 cm and 6.25 cm in length.

## 9. Check Amplitude Calibrator Duty Cycle

a. Set the AMPLITUDE CALIBRATOR switch to 2 VOLTS.
b. With the vertical deflection factor of the plug-in at 0.5 volts $/ \mathrm{cm}$, obtain a stable display at a sweep rate of 0.1 milliseconds/cm.
c. With the horizontal positioning control, move the display so that the rising portion of the display coincides with the $1-\mathrm{cm}$ vertical graticule line.
d. With the time/cm variable control, change the sweep rate so that one cycle of the calibrator signal is exactly 8 cm long.
e. Check-Falling portion of the waveform not more than 4 mm either side of the graticule center vertical line (duty cycle 45 to $55 \%$ ).

## 10. Check Amplitude Calibrator Risetime

a. Change the variable time/cm control to the calibrated position.
b. Set the AMPLITUDE CALIBRATOR to 5 VOLTS.
c. Set the vertical deflection factor to 0.5 volts $/ \mathrm{cm}$, and adjust the display for a 5 cm vertical deflection with the variable volts/cm control.
d. Set the test oscilloscope time $/ \mathrm{cm}$ to 0.2 microseconds, and adjust the triggering level control to display the full rising portion of the waveform.
e. Adjust the horizontal and vertical positioning controls simultaneously so that the $10 \%$ point of the rising portion of the waveform crosses an intersection of a vertical and a horizontal graticule line (see Fig. 6-15).


Fig. 6-15. Typical display, amplitude calibrator risetime. Indicated risetime is 0.8 microseconds.
f. Measure the horizontal distance betwaen the $10 \%$ and $90 \%$ points on the rising partion of the waveform.
G. Chack-Risatime 1.5 microseconds or less.
h. Change the test oscilloscope vertical deflection factor to 10 volis/cm.
i. Change the AMPLITUDE CALIBRATOR swith to 100 VOLTS.
¡. Adjust the display as a slep (e), with an amplitude of 5 cm .
k. Check-Risatimo 1.5 microsecands or less.
I. Remove the $50 \Omega$ cable.

## 11. Check 5 mA Current Loop

a. Connact the Typo 134 Amplifier and P6019 Curranlmeasuring Probo to the vartical input of the test oscilloscopa.
b. Sol the Type 134 Amplifier allenuator to $2 \mathrm{~mA} / \mathrm{div}$.
c. Change the test oscilloseopo vertical deflection switch to 50 millivolis $/ \mathrm{cm}$.
d. Clip the probe to the current loop on the front panel of tho Type 556.
e. Rotate the AMPLITUDE CALIBRATOR switch through all positions, noting that no waveform is displayod at any position except the 5 mA setting.
6. Check-Display amplifude of approximately 2.5 cm al the 5 mA switch position.
g. Remove the Type 134 Amplifier and Current-measuring Probe.


Pig. 6-16. tacalion of trace calallan call lest polnit.

## 12. Check Horizontal Deflection/Graticule Alignment

## NOTE

The following staps $|a|$ through $|g|$ are to be performed only if the CRT has been replaced.
a. Set the voltmater (item 9 of Recommended Equipmont) to the 10 VDC scale.
b. Connoct the volimetor leads across the traco rolation cail test points (see Fig. 6.16).
c. With a small scrowdriver, adjust the TRACE ROTATION control lin the conler of tho TRACE SEPARATION knob) for a reading of 0 on the volimalor.
d. Set the A and B Triggering MODE switchos to AUTO STABILITY. Adjust the Upper and Lower Beam INTENSITY, FOCUS and ASTIGMATISM controls to obtain woll-dofined tracos.
e. Position the slart of the $A$ and $B$ sweeps to the intersection of the $0-\mathrm{cm}$ gralicule lina with the Upper and Lower Beam graticule horizontal conlor lines.
f. Noto where the traces intersect the 101 h cm graticule line.
g. Check-Maximum of 0.5 cm vertical deviation of each trace at the intersection of the trace with the 10 th cm graticule line.
h. Adjust the TRACE ROTATION control for best alignment of the traces with the graticule horizontal lines. Remove the meter leads.

## 13. Check Beam Finder Switch Operation

a. Perform steps 12 (d) and 12 (e) if these steps have not already been performed.
b. Depress the BEAM FINDER button and hold in this position.
c. Rotate first the right and left vertical position controls fully clockwise and counterclockwise, and then the Upper Beam and Lower Beam POSITION controls, while observing the position of both displays.
d. Check-Both displays should remain within the graticule viewing areas while the BEAM FINDER button is depressed.

## NOTES

## Calibration-Type 556



Pig. 6-17. Teif salup for Geomairy adjuaimanl.

## 14. Adjust Geometry

a. Remove both Test Load unils, and in thoir place install Typa $|A|$ plug-in unils. The last equipment solup is shown in Fig. 6.17.
b. Apply 1 -millisacond markers from the lime-mark gonerator [item 4 of Recommanded Equipment) Through a BNC T conneclor, two $50 \Omega$ cables and $50 \Omega$ Ierminalions to the Typa IAl vertical inputs of both plug-ins.
c. Check that the A and B TIME/CM switches are set to .5 mSEC .
d. Adjust both plug-in variable volis/cm controls so that the displays over-scan both Upper and Lower Beam respecliva graticule areas.
e. Pull the A and 8 LEVEL conlrol knobs oulward and adjust tho A and B Triggering controls for slable displays on bolh beams.
f. Adjust both plug.in vertical position controls so thal the time-mark base line is below the viewing ared for both beams.
g. Adjust the Upper and Lower Beam POSITION controls so that the first time marks for both beams are superimposed at the left-hand $|0 . \mathrm{cm}|$ vertical graticule line.
h. Pre-adjust Sawiooth Amplitude conlrols R678 and R878 for approximataly 10.5 cm sweep langits. (Seo fig. 6-33 and 6.36 for tho locations of R678 and R878).
i. Adjust the $A$ and B TIME/CM VARIABLE controls for one lime mark por cm on both displays. Time marks will now be superimposed ovar tho antira graticule area.
i. Check-Maximum deviation of the Iracos from verlical graticule lines should not exceed 1 mm. See Fig. 6.18 for examplas of geometry adjustment.
k. Adjus! Geometry conirals R1391 and R1342 for minimum bowing of the marker tracos. (Seo Fig. 6-19 for R1391 and R1342 locations].
I. Interaction-Remove the time-mark signals and racheck tho TRACE ROTATION control adjusiment.
m. Position the Lower Beam trace to the boltom graticule line and check for verlical traca deviation (bowing or bilt] of not more than 1 mm .
n. Position the Uppar Beam Irace to the top graticule line and check for vertical Irace deviation [bowing or tilt] of not more than 1 mm .
o. Set the $A$ and $B$ TIME/CM VARIABLE controls 10 CALIBRATED.

(A) Poor Geometry

(B) Good Geometry

Fig. 6-18. Yypleal CRT diaplayi showing (A) poor geometry adjustmenti (B) good geometry adjuitment.

## 15. Adjust FOCUS and ASTIGMATISM

a. Apply 100 -microsecond lime marks to both plug-in Vertical inpuls.
b. Adjust both plug-in vertical position controls so that the lima-mark base line is below the viewing area for both beams.
c. Adjust the Upper and Lower Beam FOCUS and ASTIG. MATISM controls for sharp, well focussed displays on both beams.


Fig. 6-19. Locallon af Edge and Cemiar gameliy adjusimanis.
16. Check Upper and Lower Beam Scan Areas
a. Chango both $A$ and $B$ TIME/CM switches to .1 mSEC.
b. Set the lime-mark generator for 1-microsecond markers.
c. Turn the Upper Beam INTENSITY conirol so that the Upper Beam display is no longer visible.
d. Adjust the right plug-in vertical deflection factor so that the raster produced by the markers over-scans the Lower Beam graticule area.
e. Check-The scan area equals or exceeds $6 \times 10 \mathrm{~cm}$.

## Calibration-Type 556



Fig. 6-20. Vertical amplifier DC balance and galn aduatmanis daft ilde vlewl.
f. Extinguish the Lower Beam display with the INTENSITY control and turn the Upper 8cam INTENSITY control 10 produce a display on the Upper Beam.
g. Chack-Tho Uppar Bcam scan aroa equals or axcoods $6 \times 10 \mathrm{~cm}$.

## 17. Check CRT Orthogonality

a. Set the A TIME/CM switch 101 mSEC .
b. Set the time-mark ganerator for 1 -millisacond and 0.1 . millisecond markers.
c. Adjust the A Triggering controls for a slable display.
d. Position an Upper Beam I-millisecond marker at the intersection of a vertical gralicula line and the horizontal graticula lina 3 cm bolow the Uppor Bcam gralicule center horizontal lino.
e. Check-The adjacent 0.1 millisecond marker should not cross the Upper Beam graticule center vertical line at the point 3 cm above the Upper Beam graticule center horizontal line.
f. Repeat sleps (a) through (e) for the Lower Beam.
g. Disconnect the time markers.

## 18. Adjust Vertical Amplifier DC Balance- O Left

a. Remove the Type 1 A1 vertical plug-in unils and in their place install the test load units. Allow at least three minutes warm-up time.
b. Set the controls as follows:

## 19. Adjust Vertical Amplifier DC BalanceRight

a. Check-Deviation of the Lower Beam trace from its graticule center horizontal line should not exceed 0.5 cm .
b. Adjust DC Balance control R205 (see Fig. 6-21) to center the trace on the Lower Beam graticule center horizontal line.

## 20. Check Trace Separation Range

a. Change the Upper Beam DISPLAY switch to RIGHT PLUG-IN A.
b. Change the right plug-in unit Test Function switch to Low Load.
c. Using the right plug-in unit Vertical Position control, position the Lower Beam trace to coincide with the horizontal graticule line located 1 cm below the Lower Beam graticule center horizontal line.
d. Using the TRACE SEPARATION control, position the Upper Beam trace so it is superimposed on the Lower Beam trace.
e. Check-The TRACE SEPARATION control should have sufficient range to superimpose the Upper Beam trace on the Lower Beam trace within the center $4-\mathrm{cm}$ area of the graticule.

NOTES


Pig. 6-22. Equipmant satup for vartieal amplifier galn adusimenti,

## 21. Adjust Vertical Amplifier Gain

o. The equipment selup for this siep is shown in Fig. 6.22.
b. Set the controls as follows:

A Triggaring Conirols

SOURCE
COUPLING
SLOPE
MODE
LEVEL

Uppor Bcam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A VARIABLE
A MODE

8 Triggering Controls
SOURCE
COUPLING
SLOPE
MODE
LEVEL

## LEFT INT NORM

## AC

$+$
AUTO STABILITY
Clockwise, knob pulled oulward
LEFT PLUG.IN A
$\times 1$
. 1 mSEC
CAlibrated
NORM

RIGHT INT NORM
AC
$+$
AUTO STABILITY
Clockwise, knob pulled oulward
owor 8eam DISPLAY
Lowor Bcom DISPLAY MAG
B TIME/CM
B VARIABLE
B MODE
TRACE SEPARATION

Test Load Unir (both)
Tas! Function

RIGHT PLUG.IN B
$\times 1$
. 1 mSEC
CAlIbRATED
NORM
Centered

Gain Sat
c. Set boih test load unit Test Function switches to Gain Sat.
d. Connect a $50 \Omega$ cable from the Standard Amplitude Calibrator Output connector to the left test load unit Ext Input connector.
e. Check that both $A$ and $B T I M E / C M$ switches are set to 1 mSEC .

1. Set the Standard Amplifude Calibrator Io supply a $100 \cdot \mathrm{~V}$ square-wave oulput.
g. Center the Upper Beam free-running display in the Upper Beam viewing area.
h. Change the B Triggering MODE switch to TRIG. The Lower Beam will no longer be visible.
i. Check—Display amplitude of 4 cm .
i. Adjust GAIN R12 (see Fig. 6-20) for a display amplitude of exactly 4 cm .
k. Remove the calibrator signal from the left plug-in unit and instead, connect the signal to the right plug-in test load Ext Input connector.
2. Change the B Triggering MODE switch to AUTO STABILITY and the A Triggering MODE switch to TRIG. The Lower Beam display will now be the only one visible.
m . Center the Lower Beam free-running display in the Lower Beam viewing area.
n. Check-Display amplitude of 4 cm .
o. Adjust GAIN R212 (see Fig. 6-21) for a display amplitude of exactly 4 cm .
p. Return the A Triggering MODE switch to AUTO STABILITY, and change the Upper Beam DISPLAY switch to RIGHT PLUG-IN A. Both beam displays will again be visible.
q. Decrease the Lower Beam INTENSITY control (counterclockwise rotation) until the Lower Beam display is no longer visible.
r. Use the TRACE SEPARATION control to center the Upper Beam free-running display in the Upper Beam viewing area.
s. Check-Display amplitude of 4 cm .
t. Adjust CROSSOVER GAIN R34 see Fig. 6-20) so that the Upper Beam display amplitude is exactly 4 cm .

## 22. Check Vertical Amplifier Compression/Ex-pansion-Left, Right and Crossover

a. Equipment setup remains as in Step 21. Change the Standard Amplitude Calibrator to a $50-\mathrm{V}$ square-wave output and apply the signal to the left plug-in unit
b. Set the Upper Beam DISPLAY switch to LEFT PLUG-IN A and center the 2 cm display in the Upper Beam viewing area. Note the display amplitude.
c. With the left test load unit Vertical Position control, move the $2-\mathrm{cm}$ display to the top 2 cm of the graticule.
d. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$.
e. Move the Upper Beam display so it is centered in the Lower Beam viewing area
f. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$ with respect to the amplitude noted in step (b).
g. Change the A Triggering MODE switch from AUTO STABILITY to TRIG. The Upper Beam display will now disappear.
h. Apply the Standard Amplitude Calibrator signal to the right plug-in unit.
i. Increase the Lower Beam INTENSITY control (clockwise rotation) until the Lower Beam display is visible.
i. Center the $2-\mathrm{cm}$ display in the Lower Beam viewing area. Note the display amplitude.
k. With the right test load Vertical Position control, move the $2-\mathrm{cm}$ display so it is centered in the Upper Beam viewing area.
I. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$.
m . Move the $2-\mathrm{cm}$ display to the bottom 2 cm of the graticule.
n. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$ with respect to the amplitude noted in step (j).
o. Return the A Triggering MODE switch to AUTO STABILITY.
p. Set the Upper Beam DISPLAY switch to RIGHT PLUGIN A. The Upper and Lower Beam displays will now be visible. Decrease the intensity of the Lower Beam display.
q. Using the right test load Vertical Position control, center the Upper Beam 2-cm display in the Upper Beam viewing area. Note the display amplitude.
r. Move the $2-\mathrm{cm}$ display to the top 2 cm of the graticule. Use the right test load Vertical Position control to move the display.
s. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$.
t. Use the right test load Vertical Position control to move the display so it is centered in the Lower Beam viewing area.
u. Check-The change in display amplitude not to exceed $\pm 0.5 \mathrm{~mm}$ with respect to the amplitude noted in step (q).

## 23. Check Common Mode Rejection

a. Set the Standard Amplitude Calibrator to 1 volt squarewave output.
b. Connect a BNC T connector to the Standard Amplitude Calibrator Output connector. Using $50-\Omega$ cables, apply the signal to both test load Ext Input connectors.
c. Set both the right and left test load unit Test Function switches to Common Mode.
d. Change the Upper Beam DISPLAY switch to LEFT PLUGIN A and increase the intensity of the Lower Beam trace to normal brightness.
e. Check-The signal amplitude on both beam displays not to exceed 3 mm .
f. Change the Upper Beam DISPLAY switch to RIGHT PLUG-IN A.
g. Check-The signal amplitude on the Upper Beam display not to exceed 3 mm .
h. Remove the Standard Amplitude Calibrator signal from both test load unit inputs.


Fig. ©-23. Inilal last selup for chacking trace difi with line voltage change.
24. Check Trace Drift with Line Voltage Change
a. The test selup is shown in Fig. 6-23.
b. Sel the controls as follows:

A Triggering Controls
SOURCE
COUPLING
SLOPE
MODE
LEVEL
Upper Beam DISPLAY
A TIME/CM
B Triggering Conirols
SOURCE
COUPLING
SLOPE
MODE
LEVEL
Lower Beam DISPLAY
B TIME/CM
LEFT INT NORM
AC
+
AUTO STABILITY
Clockwise, knob pushed in
LEFT PLUG.IN A
I mSEC
RIGHT INT NORM
AC
+
AUTO STABILITY
Clockwise, knob pushed in
RIGHT PLUG-IN B
1 mSEC

Gain Sot

5 milliseconds
Type W

| AC-DC-GND $\|A\|$ | DC |
| :--- | :--- |
| AC-DC-GND $(B)$ | GND |
| Inpul Allen | 100 |
| Millivolis/em | 50 |
| Display | A-Vc |
| Vc Range | 0 |
| Autolransformer | 115 (RMS) |

## NOTE

The following procedure applies only to a Type 556 connected to a nominal 115 -valt 3 -wire power source. For an instrument connected to other than a nominal 115 -volf source, a procedure and lest fixtures adapted to local conditions will be required; for example, a 230 -volt source will require an autotransformer with the higher output, an isolation transformer for the lest oscilloscope, power sockets, etc.
c. Connect the 20 -inch power cord between the autotransformer and the power socket assembly, and connect the Type 556 power cord to the power socket assembly, as shown in Fig. 6-23.

## NOTE

The short power cord and the socket assembly (items 14 and 15 of Recommended Equipment) are used only to provide convenient measurement terminals with a minimum of hazard. If the autotransformer used is equipped with more than one output socket, the cord and socket assembly may be eliminated.
d. Connect a $1 \times$ probe to the test oscilloscope input connector.
e. Connect the probe ground lead to the ground pin of one of the sockets in the power socket assembly.
f. With the probe tip, determine which of the two remaining socket contacts is the neutral contact, and connect the probe tip to this contact.
g. Change the Type $W$ Millivolts/cm switch to 20 . The vertical deflection sensitivity should now be 2 volts $/ \mathrm{cm}$.
h. Measure the peak voltage of the waveform, as shown in Fig. 6-24.


Fig. 6-24. Illustrating measurement of voltage drop in neutral wire. Probe connected between grounding pin and neutral wire; Type $W$ Time/cm, 5 milliseconds; vertical sensitivity, 2 volts/cm.
i. Set the Type W Comparison Voltage (Vc) dial to 178 plus the reading obtained in step ( h ).

Example: If the reading obtained in step ( h ) was 2.4 volts, the dial should be set to 180.4 .
j. With the right and left plug-in unit vertical position controls, adjust the Upper and Lower Beam traces to their respective graticule center horizontal lines.
k. Set the Vc Range to +11 .
I. Change the Millivolts/cm switch to 10.
m. Move the probe tip from the neutral contact to the highvoltage or "hot" contact in the power socket assembly.
n. Adjust the autotransformer output until the tips of the waveforms shown on the test oscilloscope reach the reference line established previously by the Type W. (See Fig. 6-25 for typical display). The test oscilloscope is now indicating 183 peak VAC at the autotransformer output, or 130 volts RMS.


Fig. 6-25. Illustrating method of peak line voltage measurement; Type $W$ plug-in vertical deflection factor $1 \mathrm{~V} / \mathrm{cm}$; sweep rate 5 milliseconds/cm.
o. Wait two minutes to allow the Type 556 to stabilize, and observe the position of the Upper and Lower Beam traces.
p. Check-Vertical drift of either trace should not exceed 2 mm in the upward or downward direction.
q. Return the autotransformer output to 115 volts.
r. Allow about 2 minutes at the 115 -volt setting of the autotransformer, then recheck that the Upper and Lower Beam traces are on their respective center horizontal graticule lines.
s. Set the Type W Comparison Voltage (Vc) dial to 141.4 plus the reading obtained in step (h).
t. Adjust the autotransformer output until the tips of the waveform shown on the test oscilloscope reach the reference line established previously by the Type W. (See Fig. 6-25 for typical display). The test oscilloscope is now indicating 147 peak VAC at the autotransformer output, or 104 volts RMS.
u. Wait two minutes to allow the Type 556 to stabilize, and observe the position of the Upper and Lower Beam traces.
v. Check—Vertical drift of either trace should not exceed 2 mm in the upward or downward direction.
w. Return the autotransformer setting to 115 volts, disconnect the probe, and return the Type $W$ Vc Range switch to 0 .

## 25. Check Alternate Trace Operation

a. Connect the BNC T connector to the Type 556 CAL OUT connector. Connect two $50 \Omega$ cables from the $T$ connector to the Ext Input connectors on the right and left test load units.
b. Set the AMPLITUDE CALIBRATOR to 10 VOLTS, and set the Test Function switches on both Test Load units to Alternate.
c. Check-Two Traces on the Upper Beam display, with the calibrator signal appearing on only one trace.
d. Rotate the A TIME/CM switch through all positions from 1 mSEC to $.1 \mu \mathrm{SEC}$, checking for two traces on the Upper Beam display for all positions.
e. Repeat steps (c) and (d) for the Lower Beam, checking for two traces in all positions of the B TIME/CM switch from 1 mSEC through . $1 \mu \mathrm{SEC}$.
f. Change the Upper Beam DISPLAY switch to LEFT PLUGIN B.
g. Rotate the B TIME/CM switch through all positions from 1 mSEC to $.1 \mu \mathrm{SEC}$.
h. Check-Two traces displayed by each beam in all positions of the $B$ TIME/CM switch.
i. Change the Upper Beam DISPLAY switch to RIGHT PLUG-IN A.
i. Rotate the A TIME/CM and B TIME/CM switches through all positions from 1 mSEC to $.1 \mu \mathrm{SEC}$, keeping the A and B TIME/CM settings the same.

## NOTE

With the Upper Beam DISPLAY switch in the RIGHT PLUG-IN A position, multiple traces will appear on both displays for some of the switch positions. This condition is normal.
k. Check-Two traces on each beam at all positions of the TIME/CM switches.
I. Change the Upper Beam DISPLAY switch to RIGHT PLUG-IN B.
m. Rotate the B TIME/CM switch through all positions from 1 mSEC to $.1 \mu \mathrm{SEC}$.
n. Check-Two traces displayed by each beam at all settings of the TIME/CM switches from 1 mSEC through . 1 $\mu$ SEC.

## SN 2000-up only

o. Set the Lower Beam DISPLAY switch to A.
p. Rotate the A TIME/CM and B TIME/CM switches through all positions from 1 mSEC to $.1 \mu \mathrm{SEC}$, keeping the A and $B$ TIME/CM settings the same.
q. Check-Two traces on each beam at all positions of the TIME/CM switches.
r. Return the Lower Beam DISPLAY switch to B.
s. Remove the AMPLITUDE CALIBRATOR signal from both plug-ins.

## 26. Check Multi-Trace Chopping Transient Blanking

a. Change both test load unit Test Function switches to Chopped.
b. Set the Upper Beam DISPLAY switch to LEFT PLUG-IN A.
c. Set both TIME/CM switches to $5 \mu \mathrm{SEC}$.
d. Adjust the A and B Triggering LEVEL controls for stable displays on both teams.
e. Change the Upper Beam CRT Cathode Selector switch (on rear panel) to UPPER BEAM CHOPPED BLANKING.
f. Check-Disappearance of fast chopping transients (vertical lines) on the Upper Beam display.
g. Repeat steps (e) and ( $f$ ) with the Upper Beam DISPLAY switch in the LEFT PLUG-IN B, RIGHT PLUG-IN A, and RIGHT PLUG-IN B positions.

## NOTE

With the Upper Beam DISPLAY switch in the RIGHT PLUG-IN A positioin, the A Triggering SOURCE switch should be changed to RIGHT for that one position only.
h. Change the Lower Beam CRT Cathode Selector switch (on rear panel) to LOWER BEAM CHOPPED BLANKING.
i. Check-Disappearance of fast chopping transients on the Lower Beam display.

## SN 2000-up only

i. Set the Lower Beam DISPLAY switch to A and repeat steps (h) and (i).
k. Return the Lower Beam DISPLAY switch to B.
I. Reset both CRT Cathode Selector switches to EXTERNAL CRT CATHODE.
m. Disconnect the coaxial cables and BNC T connector.


Fig. 6-26. Equipment selup for exiarnal triggeting adjuitmenis.

## 27. Adjust External Triggering- $A$ and $B$ Sweeps

a. Remove the Test Load units and in thair place install the Type IA1 plug-in units. Test equipment selup is shown in Fig. 6-26.
b. Sot Controls as follows:

## A Triggering Controls

| SOURCE | EXT |
| :--- | :--- |
| COUPLING | AC |

SLOPE
MODE
LEVEL
Upper Beam DISPLAY
Upper Geam DISPLAY MAG
A TIME/CM
A Variable
A MODE
B Triggering Controls
SOURCE
EXT
COUPLING
AC
SLOPE +

MODE
LEVEL
Lowor Beam DISPLAY
Lower Bcam DISPLAY MAG
8 TIME/CM
B VARIABLE
B MODE

## TRIG

Cenlerad, knob pushed in RIGHT PLUG•IN 8
$\times 1$
1 mSEC
CAlIBRATED
NORM
c. Disable the B Triggaring LEVEL control by connecling a short jumper wire from chassis ground to connecting pin $Y$ on the 8 Triggering Switch circuit board. See Fig. 6-27.
d. Sol the Standard Amplifuda Calibrator to 2 volis.
e. Connect a BNC T and two 50 § cables from the Standard Amplitude Calibrator output connector to the inpul connector of the right plug-in, and the B Triggering TRIGGER INPUT connector.
f. Set the right plug-in vertical deflection switch to 1 voli/cm.
g. Place the right plug-in Input Selector switch to DC.
h. Set the test oscilloscope vertical deflection switch to 20 millivalis $/ \mathrm{cm}$, and the time/cm switch to 0.2 milliseconds.
i. Connect the 10X probe tip to the junction of R755 and R756. Fig. $6-28$ shows the connecting point for the probe tip.

## Calibration-Type 556



Flg. 6-27. Illustrailng method af connecilig jumpar wire lo adjusi riggoring.
i. Adjust the test oscilloscope triggering controls for a stable display.
k. Change the Standard Calibrator to 0.1 volts.

## NOTE

The signal amplitudes given in steps 27 (k), (0), (v) and (z) are used as calibration adjusiment aids only and therefore will not be the same as those given in the Characleristics section.
I. Check-Stable Lower Beam displays in both the + and - posilions of tho SLOPE switch.
m. Adjusi Triggor Sansitivily R756 and B Trigger Leval Centaring R745 to oblain the correct slable display on the lest oscilloscope as shown in fig. 6-29. The locations of R756 and R745 are shown in Fig. 6-28.
n. Adjust R756 counterclockwise slowly until tho Lower Beam display disappears, then clockwiso unlit the display reappears and remains slable.
o. Change the Standard Amplituda Calibrator to 50 millivolis.
p. Check-No stable display on the Lower Beam in either position of the SLOPE switch.
q. Remove the lest probe from the B Triggering circuit and connect it to the corresponding point in the A Triggering circuit, as in step (c) and (i). See Fig. 6.27. Remove the jumper wire from the B Triggering circuit and connect it between chassis ground and pin $Y$ on the A Trigger Switch board. (Use Fig. 6.27 as a guide to illustrate corresponding conneclions.)
r. Change the two $50 \Omega$ cables from the right plug-in inpur connector and the B Triggering TRIGGER INPUT connector to the left plug-in input connector and the A Triggering TRIGGER INPUT connector.
s. Set the Standard Calibrator io 2 volis.
t. Set the left plug-in vertical deflection switch 101 volifom and the Input Selector switch to DC.
u. Adjust the test oscilloscope triggering controls for a stable display.
v. Change the Slandard Calibrator to 0.1 volts.
w. Check-Stable Upper Eeam displays in both the + and - positions of the SLOPE switch.
x. Adjust Trigger Sensitivity R556 and Trigger Level Centering R545 for a stable display on the test oscilloscope as in step (m). The locations of R556 and R545 are shown in Fig. 6.30.


Flg. 6-28. Exiernal trlggering adjuitment locatons, B iweap.
y. Adjust R556 slowly countorclockwise until the Upper Bcam display disappoars, then slowly clockwise until the dis. play reappears and ramains stable.
z. Change the Standard Amplifude Calibrator to 50 millivolts.
oa. Check-No stable display on the Upper Beam in the + or - positions of the SLOPE switch.
ab. Remove the test probe and jumper wire.
ac. Remove the Siandard Amplitudo Calibrator Signal.

## 28. Check B Triggering LEVEL Control Ranges

a. Connect a $10 \times$ probe from the test oscilloscope pin A (to grid of V7348) on the B trigger switch board |see Fig. 6-28]. Check that the B Triggering SLOPE switch is sot to + .


Fig. 6-29. Triggar adusimant wavaforma.
b. Set the test oscilloscope vertical deflection switch to 0.2 volis/cm, DC coupling.
c. Rotate the B Triggering LEVEL control fully clockwise and counlerclockwise.


Fig. 6-30. Extarnal irlgeeping adjustment locations, $\mathbf{A}$ iweep.
d. Check-Control range must be $\pm 2$ volis minimum from center position.
e. Set the lest oscilloscope vertical daflection switch to 2 volis/cm.
f. Pull B Triggering LEVEL contral out to obtain a $\times 10$ ranga increase.
g. Check-Conirol rango musi bo $\pm 20$ volis minimum from cenier position.
h. Push the LEVEL knob in and remove the test probe.

## 29. Check A Triggering LEVEL Control Ranges

a. Connect the $10 \times$ probe to pin A (10 grid of V5348) on the A trigger switch board (seo Fig. 6-30). Chack that the Type 556 A Triggering SLOPE switch is sol io + . Sot the test oscilloscope vertical dofloction switch to $0.2 \mathrm{Volis} / \mathrm{cm}$.
b. Rotate the A Triggering LEVEL control fully clockwise and counterclockwise.
c. Check-Conirol range must bo $\pm 2$ volis minimum from the center position.
d. Set the test oscilloscope vertical deflection switch to 2 volis/cm.
e. Pull the $\mathbf{A}$ Triggering LEVEL conirol out to oblain $\times 10$ range increase.
f. Check-Control range must be $\pm 20$ volis minimum from the center position.
g. Push the LEVEL knob in and remove the probe.

## Calibration-Type 556



Fig. 6-31. Tasi $\operatorname{celup}$ for checking Inletnal Irlggar.

## 30. Check Internal Triggering-Lower Beam

a. The test equipment selup is shown in Fig. 6-31.
b. Sol the 8 Triggering SOURCE switch 10 RIGHT INT NORM, the MODE switch to AUTO STABILITY, and the B TIME/CM switch to $.2 \mu \mathrm{SEC}$.
c. Set the constant-amplitude generator for a 10 MHz signal, and adjust the plug-in unit vertical conirols to display a signal 2 mm in amplitude.
d. Check-Stable displays can be oblained on the Lower Beam with the B Triggering COUPLING switch in the AC and AC LF REJ positions. The LEVEL control may be adjustod as necessary to oblain a stable display.

## NOTE

If desired, sel the B Triggering MODE switch to TRIG when performing the "Check" sleps in this procedure (step 30). Use the AUTO STABILITY position between the "Check" steps when selling up the display amplifude.
e. Remove the constant amplitude generator signal from the right plug-in connector and connect the outpul of the lowfrequency signal generalor through a coaxial cable to the same connector.
f. Set the Type 556 B Triggering COUPLING switch to AC HF REJ and the B TIME/CM switch to $50 \mu \mathrm{SEC}$. Set the
genaralor trequency 1060 kHz and adjusi the display amplilude to 2 mm .
g. Check-Stable display may be oblained with adjusiment of the LEVEL control.
h. Replace the low-frequancy signal generator with the constant amplitude generator; sel the ganerator frequency to 6 MHz . Sol the Type 556 B TIME/CM switch $10.5 \mu \mathrm{SEC}$, and the display amplifude to 1 cm .
i. Check—No stablo display with adjustment of tho LEVEL control.
i. Change the B Triggering SOURCE switch to PLUG-IN INT and the COUPLING switch to AC.
k. Set the right plug-in Variable Volts/em conirol 10 Calib, the Volts/em switch to 0.05 , and set the generator amplitude conlrol for a display on the Lower Beam.

1. Check-Stable display may be oblained while adjusting the LEVEL control.
m . Remove the constant-amplitude generator signal from the right plug-in unit input connector, and connect the output of the low-frequency signal generalor to the same conneclor.

ก. Set the generator output for $60 . \mathrm{Hz}$ sine waves.
o. Set the B TIME/CM switch to 5 mSEC so several cycles of the waveform are displayed, and set the B Triggering SOURCE switch to RIGHT INT NORM. Adjust the plug-in unit verlical attenuation for a display 2 mm in amplitude.
p. Check-Stable displays may be obtained on the Lower Beam with the B Triggering COUPLING switch in the AC and AC HF REJ positions. The LEVEL control may be adjusted as necessary to obtain stable displays.
q. Increase the display amplitude to 3.5 mm .
r. Change the B Triggering COUPLING switch to DC.
s. Check-Stable displays may be obtained while adjusting the LEVEL control.
t. Change the generator to 30 Hz , the B TIME/CM switch to 10 mSEC , and adjust the display amplitude to 3 cm .
u. Change the B Triggering COUPLING switch to AC LF REJ.
v. Check-No stable displays may be obtained while adjusting the LEVEL control.
w. Change the generator frequency to 2.5 kHz , set the B TIME/CM switch to 1 mSEC , and adjust the amplitude of the display to 2 mm .
x. Check-Stable displays may be obtained with adjustment of the LEVEL control.

## 31. Check Internal Triggering-Upper Beam

a. Set the A Triggering SOURCE switch to LEFT INT NORM, the MODE switch to AUTO STABILITY.
b. Change the low-frequency generator output signal to the left plug-in unit input connector, and adjust the signal amplitude to 2 mm on the Upper Beam display.
c. Set the A TIME/CM switch to 1 mSEC.
d. Set the A Triggering COUPLING switch to AC LF REJ.
e. Check-Stable displays may be obtained on the Upper Beam while adjusting the LEVEL control.

## NOTE

If desired, set the A Triggering MODE switch to TRIG when performing the "Check" steps in this procedure (Step 31). Use the AUTO STABILITY position between the "Check" steps when setting up the display amplitude.
f. Change the generator frequency to 30 Hz , and change the A TIME/CM switch to 10 mSEC .
g. Adjust the signal amplitude to 3 cm .
h. Check-No stable display while adjusting the LEVEL control.
i. Change the generator frequency to 60 Hz , and the $A$ TIME/CM switch to 5 mSEC .
i. Adjust the signal amplitude to 2 mm .
k. Stable displays may be obtained with the COUPLING switch in AC and AC HF REJ, while adjusting the LEVEL control.
I. Increase the amplitude of the display to 3.5 mm .
m. Change the COUPLING switch to DC.
n. Check--Stable displays may be obtained while adjusting the LEVEL control.
o. Remove the low-frequency signal, and connect the constant-amplitude signal generator output through a 50 ohm cable and 50 ohm termination to the left plug-in unit vertical input connector.
p. Set the generator frequency to 10 MHz .
q. Set the A TIME/CM switch to $.2 \mu \mathrm{SEC}$ and adjust the left plug-in unit controls so the display is 2 mm in amplitude.
r. Check-Stable displays may be obtained on the Upper Beam with the A Triggering COUPLING switch in the AC and AC LF REJ positions. The LEVEL control may be adjusted as necessary to obtain a stable display.
s. Remove the constant amplitude generator signal from the left plug-in connector and connect the output of the lowfrequency signal generator through a coaxial cable to the same connector.
t. Set the A Triggering COUPLING switch to AC HF REJ and the A TIME/CM switch to $50 \mu$ SEC. Set the generator frequency to 60 Hz and adjust the display amplitude to 2 mm .
u. Check--Stable displays may be obtained with adjustment of the LEVEL control.
$v$. Replace the low-frequency signal generator with the constant amplitude generator; set the generator frequency to 6 MHz . Set the Type 556 A TIME/CM switch to $.5 \mu \mathrm{SEC}$, and the display amplitude to 1 cm .
w. Check-No stable display with adjustment of the LEVEL control.
x. Change the A Triggering SOURCE switch to PLUG-IN INT and the COUPLING switch to AC.
$y$. Set the left plug-in Variable Volts/cm control to Calib, the Volts/cm switch to 0.05 , and set the generator amplitude control to obtain a 4 -mm display on the Upper Beam.
z. Check-Stable displays may be obtained while adjusting the LEVEL control.

## 32. Check Crossover Triggering

a. Set the Upper Beam DISPLAY switch to RIGHT PLUG-IN A, the A Triggering SOURCE to RIGHT INT NORM, the MODE switch to TRIG and the A TIME/CM switch to $.2 \mu \mathrm{SEC}$.
b. Set the B Triggering LEVEL fully clockwise and MODE switch to AUTO STABILITY the COUPLING switch to AC and the B TIME/CM switch to $.2 \mu \mathrm{SEC}$.
c. Set the constant-amplitude signal generator to supply a 10 MHz signal and connect the signal to the right plug-in unit input connector. Adjust the right plug-in unit controls to display a signal 2 mm in amplitude on the Upper Beam.
d. Check-Stable display on the Upper Beam while adjusting the A Triggering LEVEL control.
e. Remove the generator signal.

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## 33. Check Auto Stability Operation

a. Connect a 30 Hz sine-wave signal from a low-frequency generator to the right plug-in input connector and set the B TIME/CM switch to 10 mSEC .
b. Adjust the plug-in for a display 1 cm in amplitude.
c. Rotate the B Triggering LEVEL control from a fully counterclockwise position through 0 to the fully clockwise position.
d. Check-Triggered (stable) display near the 0 position, and a free-running display in the remainder of the rotation area.
e. Remove the generator signal from the right plug-in connector and apply the signal to the left plug-in input connector.
f. Set the A Triggering SOURCE switch to LEFT INT NORM, MODE switch to AUTO STABILITY, Upper Beam DISPLAY switch to LEFT PLUG-IN A and the A TIME/CM switch to 10 mSEC .
g. Use steps (b) through (d) as a guide to check the A Triggering AUTO STABILITY operation.
h. Remove the generator signal.

## 34. Check Line Trigger and LF Reject Operation

a. Connect a $10 \times$ probe to the right plug-in input connector.
b. Preset the right plug-in vertical deflection to a factor $(100 \mathrm{~V} / \mathrm{cm}$ with $10 \times$ probe) that will permit an on-screen display when the signal in step (d) is applied.
c. Set the $B$ TIME/CM switch to 5 mSEC .
d. Set the B Triggering SOURCE switch to LINE RIGHT, and connect the probe tip to the oscilloscope line voltage source.
e. Check-Stable display with adjustment of the LEVEL control.
f. Change the SLOPE switch from + to - .
g. Check-Correct trigger polarity with the change of the SLOPE switch.
h. Change the SOURCE switch to NORM INT RIGHT.
i. Check-Stable display with adjustment of the LEVEL control.
i. Change the COUPLING switch to AC LF REJ.
k. Check-No stable display with adjustment of the LEVEL control.
I. Return the COUPLING switch to $A C$ and remove the probe.

## 35. Check A and B Single Sweep Operation

a. Set the Standard Amplitude Calibrator to 1 volt squarewave output and apply the signal to the left plug-in input connector.
b. Set the left plug-in vertical deflection switch to 1 volt $/ \mathrm{cm}$ and set the A TIME/CM switch to .5 mSEC .
c. With the variable volts/cm control, adjust the Upper Beam display amplitude for 5 mm , and adjust the A Triggering controls for a stable display.
d. Change the A MODE switch to SINGLE SWEEP, the A Triggering MODE switch to TRIG and remove the Standard Amplitude Calibrator signal from the left plug-in input connector.
e. Depress the A sweep RESET button, and note that the single-sweep indicator light is lit.
f. Re-apply the Standard Amplitude Calibrator signal to the input connector.
g. Check-The sweep runs once, and the indicator light is extinguished.
h. Use steps (b) through (f) as a guide for the B sweep, the right plug-in and Type 556 front-panel control settings.
i. Check-The B sweep runs once, and the indicator light is extinguished.
i. Return the A and B MODE switches to NORM, and remove the Standard Amplitude Calibrator signal.

## NOTES



Fig. 6-32. Equipment seiup for bailc Ilming procedurai-A and B swepa.

## 36. Adjust Basic Timing-A Sweep

a. Removo the Typo |A| units and inslall Test Load units in their place. Tho test equipment solup is shown in Fig. 6.32
b. Sel controls as follows:

A Triggering Controls
SOURCE
COUPLING
SLOPE
MODE
LEVEL
Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A Variable
A MODE
B Triggering Controls
SOURCE
COUPLING
SLOPE

LEFT INT NORM
AC
$+$
AUTO STABILITY
Near 0 , knob pushed in LEFT PLUG-IN A $\times 1$
1 mSEC
CALIBRATED
NORM

RIGHT INT NORM
AC
$+$

MODE
LEVEL
Lower Beam DISPLAY
Lower Beam DISPLAY MAG
B TIME/CM
8 VARIABLE
B MODE

Test Load Units (both)
Test Function Low Load
c. Connect a BNC T connector, two $50 \Omega$ cables and iwo $50 \Omega$ terminations from the time-mark generator to both Test Load unit Ext Input connectors.
d. Set the time-mark generator for 1 -millisecond and 100 microsecond markers.
e. Adjust the A and B Triggering controls for stable displays in the Upper and Lower Beam graticule viewing areas.
f. Set the Upper Beam DISPLAY MAG switch to $\times 10$.
g. Check-One 100 -microsecond marker/em.


Fig. 6-33. Adjusiment lecalion for $A$ iwesp basic ilming and awlaoth amplitude.

## NOTE

When adjusting or checking sweep timing, or when making lime measuraments from the graticule, the area befween the firstem and ninth-cm graticula lines provides the most linear measurement. Therefore the $0 . \mathrm{cm}$ to $1-\mathrm{cm}$ and the $9-\mathrm{cm} 1010-\mathrm{cm}$ areas of the display should not be used for making accu. rale lime measurements. See Fig. 2-7 in Selecting Swoop Rate, Section 2 of this manual.
h. Adjust R1146 (seo Fig. 6.33) for one 100 -microsocond markar/cm.
i. Chango the Upper Beam DISPLAY MAG switch to $X 1$.
i. Chack-One 1-millisecond marker/cm.
k. Adjusi R1167 for one 1-millisacond marker/cm. See Fig. 6 -33; R1167 is localed adjacent to the X10 CAL coniral R1146.

1. Interaction-Repcat steps (f) through (k) for accurale adjusiment, as necessary.

## 37. Adjust Upper Beam Sweep Magnifier (O) Registration

a. Set the Upper Beam DISPLAY MAG switch to $\times 10$ and position the slart of the trace to the graticule center vertical line.
b. Change the DISPLAY MAG switch to $\times 1$.
c. Check-No shift of the start of the trace as the DISPLAY MAG switch is changed from $\times 10$ to $\times 1$.
d. Adjust R1168 (Fig. 6-34) to position the start of the trace to the graticule center line.
e. Repeat steps (a) through (d] until there is no shift of the start of the trace as the DISPLAY MAG switch is changed from $\times 10$ to $\times 1$.
f. Check that the Lower Beam DISPLAY MAG switch is set to $\times 1$.

## 38. Adjust A Sweep Sawtooth Amplifude (I)

a. Set the time-mark generator for 1 -millisecond and 500 . microsecond markers. Position the display to start at the $0 . \mathrm{em}$ graticule line.
b. Check-The 22nd marker (counting the marker at the $0 . \mathrm{cm}$ graticule linel is just visible at the right hand edge of the graticule.
c. Adjust R678 |see Fig. 6.33) so that the irace ends as the 22nd marker becomes visible. The sweep lengith is 10.5 cm .
d. Relurn the DISPLAY MAG switch to $\times 10$.


Fig. 6-34. Adualmant localon for Upper Beam swas magnifiar englatialion.

## 39. Adjust B Sweep Sawtooth Slope

a. Set the Uppar Bcam DISPLAY swith to LEFT PLUG-IN B.
b. Set the time-mark generator for 1 -millisecond and 100 . microsacond markers.
c. Check—One 100 -microsecond marker/em on the Upper Beam display.
d. Adjust R861 (sea Fig. 6-35) for one 100 -microsecond marker/cm.
e. Return the DISPLAY MAG switch $10 \times 1$.


Fig. B-35. Adjuiment locallon for s swap sowiooth ilope.

## 40. Adjust B Sweep Sawtooth Amplifude (1)

a. Sap the time-mark genarator for 1 -millisecond and 500 . microsacond markers.
b. Chack-The 22nd marker (counting the marker at the $0 . \mathrm{cm}$ graticula line) is jusi visible at the right-hand edgo of the graticule.
c. Adjust B Sawioolh Amplitude control R878 (see Fig. 6 636) so the trace onds as the 22 nd marker becomes visible (sweop lenglh is 10.5 cm ).

## 41. Adjust Basic Timing-B Sweep

a. Set tho Lowor Beam DISPLAY switch to $\times 10$, and position the display for optimum viewing.
b. Set the time-mark ganarator for 1 -millisecond and 100 . microsecond markers.
c. Chack-One 100 -microsecond markar/cm.
d. Adjust 81246 (soo Fig. 6-36) to oblain one 100 -micro. socond marker/cm.
e. Change the Lower Bcam DISPLAY MAG switch $10 \times 1$.
f. Check-One 1 -millisacond marker/em.
g. Adjust R1267 to obtain one 1-millisacond marker/cm. 81267 is located on the same bracket adjacent to the $\times 10$ adjustmant (see Fig. 6-36).
h. Inferaction-Repeat sleps (a) through (g) for accurate adjustment as necessary.

## 42. Adjust Lower Beam Sweep Magnifier () Registration

a. Set the Lower Beam DISPLAY MAG switch $10 \times 10$ and position the start of the trace to the graticule center verlical line.
b. Change the DISPLAY MAG switch to $\times 1$.


Fig. 6-36. Adjuitment location for basic Ifming and Bwap ampllfude.
c. Check-No shift of the starl of the irace as tho DIS. PLAY MAG switch is changed from $\times 10$ 10 $\times 1$.
d. Adjust R1268 SWP/MAG REGIS (soo Fig. 6-53) to position the starl of the trace to the graticule conter line.
e. Repeat sleps (a) through (d) until there is no shift of the start of the trace as tho DISPLAY MAG switch is changed from $\times 1010 \times 1$.
f. Refurn the DISPLAY MAG switch to $\times 1$ and disconnect the lime-markers from the Typo 556.


Fig. 6-37. lacalion of lower beam $A$ iweep gain adjusiment for serial numbered inilruments 2000 and up.

fig. 6-38, Equipment selup for $A$ and B sawlooth current adust.

## 43. Adjust Lower Beam A Sweep Gain (SN2000-up only)

a. Sot tho Uppar Boam DISPLAY switch to LEFT PLUG-IN A.
b. Set the $A$ TIME/CM switch to 1 mSEC .
c. Set the Lower Beam DISPLAY switch to A.
d. Sel the Lower Beam DISPLAY MAG switch $10 \times 10$.
e. Chack-Ono 100 -microsecond marker/cm.
f. Adjust R683 (see fig. 6-37) to oblain one 100 -micro. second marker/cm.

## 44. Adjust A and B Sawtooth Currents

a. The equipment setup is shown in fig. 6-38.
b. Set the Standard Amplitude Calibrator for a 2 -volt square-wave oulput signal.
c. Set the test oscilloscope/plug-in verlical deflection switch 10 0.05 volis $/ \mathrm{cm}$.
d. Set the test oscilloscope Time/Cm switch to 1 millisecond/cm.
a. Connect the $10 \times$ Probe tip to tha Slandard Calibrator Oulput and if necossary, adjust the lest oscilloscope variable valis $/ \mathrm{cm}$ for a dofloction of exactly 4 cm .
f. Remove the probe tip from the Standard Calibralor conneclor and connect it to the junction of R685 and the A SAW. TOOTH CURRENT adjusiment R684 (see Fig. 6.39A).
g. Set the test oscilloscope Timo/Cm switch to 5 mSEC .
h. Check---Display amplifude of 4 cm .
i. Adjust R684 for a $4 . \mathrm{cm}$ display on the test oscilloscope. It may be necessary to chango tho A TIME/CM swilch to a sweep rate which will display sevaral sawlooth cyeles for a more convenient amplifude measuramont. See Fig. 6-39A for R684 localion.
i. Change the probe from the junction of R684 and R685 to the junction point for R885 and B SAWTOOTH CURRENT adjusiment R884 (see Fig. 6-398).
k. Check-Display amplifude of 4 cm .
I. Adjust R884 \{see Fig. 6.39 B | for a $4-\mathrm{cm}$ display on the test oscilloscope.
m. Remove the probe.


Flg, 6-39. A and B awloath current adjuiment and last palnt lacaflons.

## 45. Check Delay-Time Multiplier Dial Setting

a. Rotale the DELAY.TIME MULTIPLIER dial fully counterclorkwiso until it hits the slop.

## NOTE

If dial is resel, dalayed-swaep calibration will be changed and if will be necassary to perform a recalibration of the $A$ sweep, which follows in steps 46 through 49.
b. Check-Dial reading of $0.20, \pm 2$ minor divisions.
c. If the dial reading is not 0.20 [within $\pm 2$ minor divisions), loosen the knob selscrew and reposition the knob so that the fully counterclockwise position reading is correct.
d. Rotate the DELAY-TIME MULTIPLIER dial fully clockwise.
e. Chack—Dial reading of $10.20, \pm 4$ minor divisions.

NOTES


Fig. 6-40. Tat ielup for adfailing Delay Stan and stop.
46. Adjust Delay Start and Stop
a. The test selup is shown in Fig. 6.40.
b. Sol controls as follows:

A Triggering Conirols
SOURCE
COUPLING
SLOPE
MODE
LEvEL
Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A VARIABLE
A MODE
B Triggering Controls
SOURCE
COUPLING
SLOPE
MODE
LEVEL

RIGHT INT NORM
AC
$+$
AUTO STABILITY
Near O, knob pushed in RIGHT PLUG.IN A $\times 1$
1 mSEC
CALIBRATED
NORM

RIGHT INT NORM
AC
$+$
AUTO STABILITY
Fully clockwise, knob pulled outward
(1)

Lower Beam DISPIAY
Lower Beam DISPLAY MAG
B TIME/CM
B Variable
B MODE

Test Load Unils (both)
Tasi Function

RIGHT PLUG.IN B
$\times 1$
$10 \mu \mathrm{SEC}$
CAlibrated
NORM

Low Load
c. Connect a $50 \Omega$ cable from the time-mark generator through a $50 \Omega$ termination to the right test load unit Ext Input connector.
d. Sel the time-mark genarator for 1 -millisocond markers.
e. Adjust the A Triggering controls for a slable display on the Upper Bcam.
f. Adjust the TRACE SEPARATION and right test load unit Variable and Vertical Position controls for convenient viewing of the Upper and Lower Beam displays.
g. Change the B MODE switch to DLY'D BY A.
h. Set the DELAY-TIME MULTIPLIER dial to 1.00 .


Fig. 6.41. Delay Start and Siop Adust locations.

## NOTE

Adjusiment of the Upper Boam INTENSITY and CONTRAST controls may be necessary for optimum viewing of the intelnsified portion of the display.
i. Check-Iniensified partion of the Upper Beam display siarls at the 2nd marker (soe Fig. 6.42A).
i. Adjus) DELAY START R918 (Fig. 6.41) so that the inten. sified portion of the display starls at the 2nd marker (preliminary adjusimeni).
k. Set the DELAY-TIME MULTIPLIER dial to 9.00 .
I. Chack-Intensified portion of display staris at the 101 h markar (sae Fig. 6.428).
m. Adjust DELAY STOP 8914 (see Fig. 6.41) so that the intensified portion of the display starts at the 10 th marker.
$n$. Set the DELAY-TIME MULTIPLIER dial to 1.00 .
o. Chack-The rising partion of tha dalayed pulse (dis. played on Lower Beam) starts at the $0 . \mathrm{cm}$ graticule line.
p. Readjust DELAY START R918 so that the rising portion of the delayed pulse slarls at the $0 . \mathrm{cm}$ graticule line.
q. Sot the DELAY-TIME MULTIPLIER dial to 9.00 .
r. Check-The rising portion of the delayed pulse starts at the $0 . \mathrm{cm}$ graticule line.
s. Readjust DELAY STOP R914 so that the rising portion of the delayed pulse starls at the $0 . \mathrm{cm}$ graticule line
t. Interaction-Repeat sleps ( $n$ ) through (s) and readjust if necessary.

## 47. Check Delay-Time Mulfiplier Incremental Linearity

a. Set the DELAY-TIME MULTIPLIER dial to 8.00 .


Fig. 6-42. Yypleal displayi, Dalay Slart and Stop adualmente.
b. Rotate the dial as necossary to position the delayed pulse to slart af the $0 . \mathrm{cm}$ graticule line.
c. Chack-Daviation of dial reading from 8.00 should bo not moro than $\pm 2$ minor divisions of the dial.
d. Repeat check at all major dial divisions from 8.00 10 1.00.

## 48. Check Delay-Time Jiffer

a. Change the B TIME/CM switch to $1 \mu S E C$.
b. Set tho DELAY.TIME MULTIPLIER dial to 10.00 approximately, centering the magnified pulse near the center of the graticule.
c. Check-Jitter not more than 0.5 cm .
d. Set the DELAY-TIME MULTIPLIER dial to 1.00 approximately, centering the magnified waveform near the center of the graticule.
e. Check-Jitter not more than 0.5 cm .


Fig. 6.43. Test safup for Swaep Timing-A and B.
49. Adjust Timing-A Sweep
a. The tost solup is shown in Fig. 6.43.
b. Sot controls as follows:

A Triggering Conirols SOURCE
COUPLING
SLOPE
MODE
LEVEL
Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A VARIABLE
A MODE
B Triggering Controls
SOURCE
COUPLING
SLOPE
MODE
LEVEL

RIGHT INT NORM
AC
$+$
AUTO STABILITY
Near 0, knob pushed in RIGHT PLUG.IN A
$\times 1$
$10 \mu \mathrm{SEC}$
CALIBRATED
NORM

RIGHT INT NORM
$A C$
$+$
AUTO STABILITY
Fully clockwise, knob pulled outward

Lowar Beam DISPLAY
Lowor Beam DISPLAY MAG
B TIME/CM
B VARIABLE
B MODE
DELAY-TIME MULTIPLIER
Test Load Unit (both]

| Tos! Function | Low Load |
| :---: | :--- |
| Time-Mark Genoralor | 10 microsoconds |

## NOTE

Throughout the timing procedure the dalayed sweep display on the Lower Beam is used as an aid in making accurate timing adjustments. Fig. 6-44 illustrates the correct method of positioning the delayed sweep display in relation to the delaying or A sweep. The use of a consistent method of positioning will result in a high degree of timing accuracy.
c. Set the time-mark generator for 10 -mierosecond marker output and adjust the Type 556 A Triggering conlrols for a stable display.
d. Adjust the CONTRAST and INTENSITY conirols so that the intensified portion of the Upper Beam display can be easily distinguished from the rest of the display.
e. Set the DELAY.TIME MULTIPLIER dial so that the 2 nd marker on the Upper Beam display is fully intensified to the marker tip, similar to the waveform shown in Fig. 6-44. The dial reading will be on or near 1.00; note the reading. Also note the position of the Lower Beam display markers.
f. Rolate the DELAY-TIME MULTIPLIER dial to move the intensified partion of the display to the 10ih marker, and set the dial to read 8.00 divisions plus the reading noted in slep (e).

Example: if the dial reading in step (e) is 1.03 , the new selting should be 9.03 exactly.
g. Check-The 10 th marker is iniensified to the marker lip, similar to the waveform shown in Fig. 6.44.


Pig. B.44. Malhad af adjusting Hming as dascribed In slap 49 (e).
h. Adjust C660G (Fig. 6-45) so that the 10 th marker is fully iniensifiad, and tho Lower Beam display markers aro pasilionod as in slop (a).
i. Inleraction-Repeat sleps $\{\mathrm{a})_{\text {, ( }}(\mathrm{f})$ ( g ), and ( h ) as needad.
i. Change the A TIME/CM switch to $1 \mu \mathrm{SEC}$, and the B TIME/CM to $0.1 \mu$ SEC. Set the time-mark generator for 1 . microsecond marker oulput.
k. Repeat stops (e and $\}$ ).
I. Cheek-Tho tenth marker is intensified to the marker tip.
m. Adjust C660H (Fig. 6-45) so that the renth marker is intensified to the marker tip, and the delayed sweep display is positioned the same as in the 1.00 setting of the DELAY TIME MULTIPLIER dial.
n. Interaction-Repeat the check of the 1.00 dial selling and the adjusiment at the 9.00 dial setting unil no furiher adjustment is necessary.


Fig. 6-45. Adjusimani locatlonis for A swap iming, lop view af Type 356.
o. Connect a 10 -microsecond triggar signal from the timemark generator Trigger Outpul connector through a 50 -ohm cable and 50 -ohm termination to the Upper Beam TRIGGER INPUT connector and set the A triggering SOURCE swith to EXT.
p. Change the A TIME/CM switch $100.5 \mu \mathrm{SEC}$ and check that the time-mark generator is set to supply 1 -microsecond marker output to tho right plug.in.
q. Check-One $1 \mu \mathrm{SEC}$ marker per 2 cm (disregard the first marker.)
r. Preadjusi C660J (Fig. 6.45) for ono $1 \mu$ SEC marker $/ 2 \mathrm{~cm}$.
s. Change tho $A$ TIME/CM switch $100.1 \mu \mathrm{SEC}$ and the limo-mark genorator to supply 0.1 -microsecond markers.
+. Check-One marker per em, Upper Beam display.
u. Preadjust C861 (Fig. 6-45) for one markar/cm.
v. Intaraction-C660」 and C681 adjustments interact; repeal slaps ( p ) through ( U ) as necessary.
w. Set the DELAY TIME MULTIPLIER dial to 1.00 .
$x$. Adjust the CONTRAST control so the intensified portion of the Upper Beam display can be viewed. Use the Upper Beam POSITION control to position the peak of the first intensified pulse to the $1-\mathrm{cm}$ vertical graticule line.
$y$. Set the Lower Beam DISPLAY MAG switch to $\times 10$ and use the Lower Beam POSITION control to position the $50 \%$ level on the rising portion of the marker pulse to an intercept point. For example, al the point where 5 h cm verlical graticule line and 2 nd cm horizonial line from bothom of graticule meet as shown in Fig. 6-46.
z. Set the dial to 9.00 , but, while doing so, be sure to count eight markers (not counting the one displayed at 1.00] displayed by the Lower Beam as these markers move to the left past the intercept point. Then, os the dial is set to 9.00 , the $50 \%$ level on the rising portion of the eighth marker should be al the intercept point.


Fig. 6-46. Pypical display obialnad ta Illusitate Iniercepl palni with dial at 1.00.
aa. Check-8th marker at intercept point.
ab. Readjust C660J (Fig. 6.45) to position the eighth marker at the intercept point.
ac. Change CONTRAST control and, if desired, the INTEN. SITY control so all of the Upper Beam display is visible. Reposition the Upper Beam display so tho 2nd marker is located af the $1 . \mathrm{cm}$ verlical graticule line.
ad. Check-One markor/em, Upper Beam display.
ae. Roadjust C681 \{Fig. 6-45) for one marker per cm.

## NOTE

If the linearity from the 1st 10 2nd marker is exceedingly poor, check the position of the slugs in Cl174 and Cl184 (Fig. 6-471. The slugs should normally be positioned about five turns above the malal wiper contacts. If the slugs are readjusted so they are five turns out, repeat step (ae).

## 50. Adjust Horizontal Amplifier 50 MHz Compensation-Upper Beam

a. Change the 8 MODE switch to SINGLE SWEEP (this disables the B sweop.]
b. Sal the time-mark genoralor for $50 \mathrm{MHz}[20 \mathrm{~ns}]$ sine wave oulput.
c. Ghange the Upper Beam DISPLAY MAG switch to $\times 10$.
d. Position the sine wavos to align with the vertical graticule lines.
e. Check-One cycle/2 cm, Upper Beam display.
f. Adjust Cl 193 (sec Fig. 6.47) for maximum sweep expansion.
g. Adjust C 1182 (see Fig. 6-47) for maximum sweep expansion.
h. Adjust C1172 (see Fig. 6-47) for maximum sweep expansion.
i. Repeat sleps ( ( inrough ( h ) in the same order.
i. Position the display so the Upper Beam waveform starts al the $0 . \mathrm{cm}$ graticule line. Turn up the INTENSITY control lemporarily to check that the waveform is properly pasitioned. See Fig. 6-48A.
k. Adjust the A Triggering LEVEL control so a sine-wave peak (lop or boltom) falls on the $4 . \mathrm{cm}$ graticule line. Note that sine-wave peak and position it to the $1-\mathrm{cm}$ graticule line. (See Fig. 6.48B).

fig. 6.47, High-spesd awaep cempeniallen adjusiment, A swep.
I. Check-One cycle/2 cm, Upper Beam display; $1 . \mathrm{cm}$, $5 . \mathrm{cm}$ and $9 . \mathrm{cm}$ sine-wave poaks should coincide with their rospoctivo graticulo linos (soo Fig. 6.48C). Toleranco is $=-5 \%$ or $\pm 4 \mathrm{~mm}$.
m. Adjusi C1165 (seo Fig. 6.47) for 1 cycle $/ 2 \mathrm{~cm}$ and so the sine-wave peaks at tho $1 . \mathrm{cm}$ and $9 . \mathrm{cm}$ lacalions coincide with their respoctive graticule lines.
n. If the center sine-wave pack dees not coincide with the $5-\mathrm{cm}$ graticule line, readjust C1174 and C1184 until proper coincidence of $1 . \mathrm{cm}$ and $5 . \mathrm{cm}$ peaks is oblained.
0. Readjust C 165 until the $1-\mathrm{cm}$ and $9-\mathrm{cm}$ sine-wave peaks coincide with their respective graticule lines.
p. If Cl 165 is readjusled, repeat stops (n) and (I) for proper linearity of sine-wave peak alignment with the $1 . \mathrm{cm}, 5-\mathrm{cm}$ and $9 . \mathrm{cm}$ graticule lines (see Fig. 6.48 C ).


Fig. 6-48. Typical displays, high-speed sweep timing. Waveform (A) shows lop paak of a slne wave af the $4-\mathrm{cm}$ graticula line, wavoform $|B|$ shows display properly positioned, and wavoform (C) shows correct high-speed sweep tlming and linearity.


Fig. 6.49. Adusimant lecalion: for B awaep ilming, top view of Typa 556.
q. Change the Upper Beam DISPLAY MAG switch io $\times 1$.
r. Reposition the Uppor Beam display to start at the $0 . \mathrm{cm}$ graticule lines.
s. Change the Upper Beam DISPLAY MAG switch to $\times 10$.
t. Check-One cycle/2 cm, Upper Beam display. The 1 cm and $9 . \mathrm{cm}$ sine-wove peaks should coincide with their respective graticule lines. Tolerance is $\pm 5 \%$ or $\pm 4 \mathrm{~mm}$.
U. If the $9 . \mathrm{cm}$ sino-wavo paak talls long with respect to the graticula line, readjust C1172 for proper timing, If the $9 . \mathrm{cm}$ sine-wave peak falls shori, repeak steps (i) through (i). If the sweep timing is correct, position the display 10 cyeles to the lath. Repear step (t) and then go to slep (y).
v. Change the Upper Boam DISPIAY MAG switch $10 \times 1$ and reposition the display 10 start at the $0 . \mathrm{cm}$ graticule lino.
w. Set the time-mark generator for 0.1-microsecond marker output.
x. Chack-Ono marker/em, Upper Beam display.
y. Readjust C681 for one marker/em.

## 51. Check Timing and Delaying Sweep Accuracy -A Sweep

a. Change the B MODE switch to DLY'D BY A, and check that the Lower Beam DISPLAY switch is set to $\times 10$.
b. Check—Using Table 6-3 as a guide, check the A Sweep CRT displayed accuracy with respect to the $1-\mathrm{cm}$ and $9 . \mathrm{cm}$ graticule lines. Tolerance should be within $\pm 3 \%$ or $\pm 2.4$ mm . In addition, check the delayed sweep accuracy using the DELAY-TIME MULTIPLIER dial. Tolerance should be within B minor divisions for each A TIME/CM switch position. The rechnique for checking the three fastest sweep rates using the DELAY-TIME MULTIPLIER dial is as follows:

For the 0.1 رLSEC A TIME/CM switch position, the basic lechnique is described in sleps 49s through 49a0. For the 0.2 ${ }_{\mu} \mathrm{SEC}$ switch position the technique is similar to the 0.1 position, but 16 markers must be counted on the Lower Beam

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display when rotating the dial from 1.00 to 9.00 . Check dial reading from 9.00 at intercept point. For the $0.5 \mu \mathrm{SEC}$ switch position, set the A Triggering SOURCE switch to RIGHT INT NORM, the Lower Beam DISPLAY MAG switch to $X 1$ and use a similar technique to that described in steps 49 c through 49f.

For the A TIME/CM switch position from $1 \mu \mathrm{SEC}$ to 5 SEC , use a similar technique for checking delaying sweep accuracy to that used when setting up the Delay Start and Stop adjustments (step 46) and as shown in Fig. 6-43.

TABLE 6-3
Timing and Delaying Sweep Accuracy-A Sweep

| A TIME/CM | B TIME/CM | Time Mark <br> Generator | Check Upper <br> Beam <br> Display |
| :---: | :---: | :---: | :---: |
| $0.1 \mu \mathrm{SEC}^{3}$ | $0.1 \mu \mathrm{SEC}^{+}$ | $0.1 \mu \mathrm{~s}$ | 1 marker $/ \mathrm{cm}$ |
| $0.2 \mu \mathrm{SEC}^{2}$ | $0.1 \mu \mathrm{SEC}^{4}$ | $0.1 \mu \mathrm{~s}$ | 2 markers $/ \mathrm{cm}$ |
| $0.5 \mu \mathrm{SEC}^{5}$ | $0.1 \mu \mathrm{SEC}$ | $0.5 \mu \mathrm{~s}$ | 1 marker $/ \mathrm{cm}$ |
| $1 \mu \mathrm{SEC}^{3}$ | $0.1 \mu \mathrm{SEC}$ | $1 \mu \mathrm{~s}$ | 1 marker $/ \mathrm{cm}$ |

${ }^{2}$ Use CONTRAST control to check display.

## ${ }^{3}$ Previously adjusted.

${ }^{4}$ Lower Beam DISPLAY MAG switch is set to $\times 10$. (For the remaining B TIME/CM switch positions, the switch is set to $\times 1.1$
${ }^{5}$ Previously adjusted. Set the A Triggering SOURCE switch to RIGHT INT NORM and the MODE switch to TRIG.

## 52. Adjust Timing-B Sweep

a. Set the Type 556 and plug-in controls as follows:

A Triggering Controls

| SOURCE | RIGHT INT NORM |
| :--- | :--- |
| COUPLING | AC |
| SLOPE | + |
| MODE | TRIG |
| LEVEL | Fully clockwise, knob <br> pushed in |

Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A VARIABLE
A MODE

B Triggering Controls SOURCE
COUPLING
SLOPE
MODE
LEVEL
Lower Beam DISPLAY
Lower Beam DISPLAY MAG
B TIME/CM
B VARIABLE
B MODE
Test Load Unit (both)
Test Function
b. Set the time mark generator for 10 -microsecond markers.
c. Position the Lower Beam display so the markers coincide with the graticule lines.
d. Check-One marker/cm, Lower Beam display.
e. Adjust C860G (see Fig. 6-49) to obtain 1 marker/cm.
f. Change the B TIME/CM switch to $1 \mu \mathrm{SEC}$.
g. Set the time-mark generator for 1-microsecond markers.
h. Check—One marker/cm, Lower Beam display.
i. Adjust C 860 H (see Fig. 6-49) to obtain 1 marker $/ \mathrm{cm}$.
i. Change the B TIME/CM switch to $0.5 \mu \mathrm{SEC}$.
k. Check-One marker $/ 2 \mathrm{~cm}$, Lower Beam display.
I. Adjust C860J (see Fig. 6-49) for one marker per 2 cm .
m . Change the B TIME/CM to $0.1 \mu \mathrm{SEC}$.
n . Set the time-mark generator for 0.1 -microsecond markers.
o. Remove the $10 \mu \mathrm{SEC}$ trigger signal from the Upper Beam TRIGGER INPUT connector and apply the signal to the Lower Beam TRIGGER INPUT connector.
p. Set the B Triggering SOURCE switch to RIGHT EXT.
q. Check-One marker/cm, Lower Beam display.
r. Adjust C881 (see Fig. 6-50) to obtain one marker/cm.
s. Interaction-C881 and C860J adjustments interact; set the time-mark generator for 1 -microsecond markers and repeat steps (i) through (r) until no further adjustment is necessary.

## 53. Adjust C882-B Sweep Crossover Compensation

a. Change the Upper Beam DISPLAY switch to RIGHT PLUG-IN B.
b. Check-One marker/cm, Upper Beam display.
c. Adjust C882 (see Fig. 6.50) for one marker/em on the Upper Beam display.

## 54. Adjust Horizontal Amplifier 50 MHz Compensation-Lower Beam

a. Change the Upper Beam DISPLAY swith to LEFT PLUG. IN A.
b. Set the time mark generalor for $50 \mathrm{MHz}(20 \mathrm{~ns})$ sinewave output.
c. Chango the Lower Beam DISPLAY MAG switch to $\times 10$.
d. Position the sine waves to align with the vertical graticule lines.
e. Check-One cycle/2 cm, Lower Beam display.
f. Adjust Cl 293 (see fig. 6-50) for maximum sweep oxpansion.
g. Adjust C 1282 (see Fig. 6-50) for maximum sweep expansion.
h. Adjus! C1272 (sce Fig. 6-50) for maximum sweop expansion.
i. Repeat steps ( $\ddagger$ through $\{\mathrm{h}$ ) in the same order.
i. Position the display so the Lower Beam waveform staris af the $0 . \mathrm{cm}$ graticule line. (Tuen up the INTENSITY conlrol lemporarily to check thap the wavaform is properly positionod. Uso Fig. 6.48A as aguide).
k. Adjust the B Triggering LEVEL control so a sine-wave peak flop or bottomp falls on the $4 . \mathrm{cm}$ graticule line. Note that sine-wava poak and position it to the $1 . \mathrm{cm}$ graticule line. (Use fig. 6.48B as aguida).
I. Chock-One cycle/2 cm, Lower Beam display; $1 . \mathrm{cm}, 5$. cm and $9 . \mathrm{cm}$ sine-wave peaks should coincide with their respectivo graticule lines. Tolerance is $\pm 5 \%$ or $\pm 4 \mathrm{~mm}$.


Fig. 6-50. High-speed swaep compansation ad|usiments-B swaep.
m. Adjusi Cl 265 (see Fig. 6.50 ) for 1 cycle $/ 2 \mathrm{~cm}$ and so the sine-waves peaks at $1-\mathrm{cm}$ and $9-\mathrm{cm}$ locations coincide with their respective graticule lines.
$n$. If the center sine-wave peak does not caincide with the $5-\mathrm{cm}$ graticule line, readjust C 1274 and C 1284 until proper coincidence of $1 . \mathrm{cm}$ and $5 . \mathrm{cm}$ peaks is obtained.
o. Readjust Cl 265 until the $1 . \mathrm{cm}$ and $9-\mathrm{cm}$ sine-wave peaks coincide with their respective graticule lines.
p. If Cl 265 is readjusted, repear steps ( n ) and ( 0 ) for proper lincarity of sine-wave peak alignment with the $1-\mathrm{cm}, 5$ cm and $9 . \mathrm{cm}$ graticule lines (Use Fig. 6.48C as a guide.)
q. Change the Lower Beam DISPLAY MAG switch to $\times 1$.
r. Reposition the Lower Beam display to slart at the $0 . \mathrm{cm}$ graticule line.
s. Change the Lower Beam DISPLAY MAG switch to $\times 10$.

1. Check-One cycle/2 cm, Lower Beam display. The $1-\mathrm{cm}$ and $9 . \mathrm{cm}$ sine-wave peaks should coincide with their respactive graticule lines. Tolerance is $\pm 5 \%$ or $\pm 4 \mathrm{~mm}$.


Fig. 6-51. Location of sweap crosiovar adjusimant for satial numbered instrumatis 2000 and up.
u. If the $9-\mathrm{em}$ sine-wave falls long with respect to the graticule line, readjust C 1272 for proper liming. If the $9-\mathrm{cm}$ sine-wave peak falls short, repeat steps (f) through (i). If the sweop timing is correct, position the display 10 cycles to the left. Repeat step (1) and then go to step (V).
v. Change the Lower Beam DISPLAY MAG switch to $\times 1$ and reposition the display to start at the $0-\mathrm{cm}$ graticule line.
w. Set the time-mark generator for 0.1-microsecond marker outpur.
x. Check-One marker/em, Lower Beam display.
y. Readjust C881 for one marker/em.

## 55. Adjust-A Sweep Crossover Compensa- (1) tion (SN 2000-up only)

a. Set the Lower Beam DISPLAY switch to A.
b. Set the Upper Beam DISPLAY switch to LEFT PLUG-IN A.
c. Set the time mark generator for 0.1 microsecond markers and connect the output to the left plug-in.
d. Set the Lower Beam DISPLAY MAG switch to $\times 1$.
e. Adjust C683 (see Fig. 6-51) to obtain a 1 marker/cm display on the lower beam. Tolerance: within $\pm 3 \%$ or $\pm 2.4 \mathrm{~mm}$.
f. Set the time mark generator for $50 \mathrm{MHz}(20 \mathrm{nSEC})$ sine wave output.
g. Set the Lower Beam DISPLAY MAG switch to $\times 10$.
h. Check $-1 \mathrm{~Hz} / \mathrm{cm}$ display on the lower beam. Tolerance: $\pm 5 \%$ or $\pm 4 \mathrm{~mm}$.

## 56. Check Timing Accuracy-B Sweep

a. Change the B Triggering MODE switch to TRIG and the SOURCE switch to INT NORM.
b. Disconnect the trigger signal from the Lower Beam TRIGGER INPUT connector.

TABLE 6-4
Timing Accuracy-B Sweep

| B TIME/CM | Time Mark Generator | Check Lower Beam Display |
| :---: | :---: | :---: |
| $0.1 \mu \mathrm{SEC}^{6}$ | $0.1 \mu \mathrm{~s}$ | 1 marker/cm |
| $0.2 \mu \mathrm{SEC}$ | $0.1 \mu \mathrm{~s}$ | 2 markers/cm |
| $0.5 \mu \mathrm{SEC}^{\text {6 }}$ | $0.5 \mu \mathrm{~s}$ | 1 marker/cm |
| $1 \mu \mathrm{SEC}^{\text {c }}$ | $1 \mu \mathrm{~s}$ | 1 marker/cm |
| $2 \mu \mathrm{SEC}$ | $1 \mu \mathrm{~s}$ | 2 markers/cm |
| $5 \mu$ SEC | $5 \mu \mathrm{~s}$ | 1 marker/cm |
| $10 \mu \mathrm{SEC}^{6}$ | $10 \mu \mathrm{~s}$ | 1 marker/cm |
| $20 \mu$ SEC | $10 \mu \mathrm{~s}$ | 2 markers/cm |
| $50 \mu$ SEC | $50 \mu \mathrm{~s}$ | 1 marker/cm |
| 0.1 mSEC | 0.1 ms | 1 marker/cm |
| 0.2 mSEC | 0.1 ms | 2 markers/cm |
| 0.5 mSEC | 0.5 ms | 1 marker/cm |
| $1 \mathrm{mSEC}^{6}$ | 1 ms | 1 marker/cm |
| 2 mSEC | 1 ms | 2 markers/cm |
| 5 mSEC | 5 ms | 1 marker/cm |
| 10 mSEC | 10 ms | 1 marker/cm |
| 20 mSEC | 10 ms | 2 markers/cm |
| 50 mSEC | 50 ms | 1 marker/cm |
| 0.1 SEC | 0.1 s | 1 marker/cm |
| 0.2 SEC | 0.1 s | 2 markers/cm |
| 0.5 SEC | 0.5 s | 1 marker/cm |
| 1 SEC | 1 s | 1 marker/cm |
| 2 SEC | 1 s | 2 markers/cm |
| 5 SEC | 5 s | 1 marker/cm |

${ }^{\text {a }}$ Previously adjusted.
c. Check-Using Table 6-4 as a guide, check the B sweep CRT displayed accuracy with respect to the $1-\mathrm{cm}$ and $9-\mathrm{cm}$ graticule lines. Tolerance should be within $\pm 3 \%$ or $\pm 2.4$ mm .

## 57. Check Variable Time/cm Range

a. Set the Upper Beam DISPLAY switch to RIGHT PLUGIN A.
b. Set the B TIME/CM to 1 mSEC .
c. Set the A and B Triggering MODE switches to AUTO STABILITY.
d. Check that the A Triggering SOURCE switch is set to RIGHT INT NORM.
e. Set the time-mark generator for 10 -millisecond markers.
f. Adjust the A and B Triggering LEVEL controls to obtain stable Upper and Lower Beam displays. Markers on both beams will appear at the $0-\mathrm{cm}$ and $10-\mathrm{cm}$ graticule lines.
g. Rotate the A and B TIME/CM VARIABLE controls fully counterclockwise; the UNCAL lights should be on.
h. Check-Horizontal distance between markers should be 4 cm or less, both displays.
i. Return both VARIABLE controls to CALIBRATED; the UNCAL lights should be off.

## 58. Check Trigger Delay

a. Preset the Type 556 controls as follows:

| B MODE | DLY'D BY A |
| :--- | :--- |
| A and B TIME/CM | $.1 \mu S E C$ |
| A Triggering | TRIG, + , AC, NORM INT, |
|  | RIGHT |
| B Triggering | AUTO STABILITY, +,$+ A C$, |
|  | NORM INT, RIGHT, |
|  | LEVEL control fully |
|  | clockwise with knob |
|  | pulled outward |
|  | 10.00 |

b. Set the time-mark generator for 1-microsecond marker output.
c. Adjust the A triggering LEVEL control to obtain a stable display.
d. With the Upper and Lower Beam POSITION controls, position both traces to start at the $0-\mathrm{cm}$ graticule line.
e. Turn the DELAY-TIME MULTIPLIER dial counterclockwise while adjusting the TRACE SEPARATION and right plug-in Vertical Position controls until the marker on the Lower Beam display is superimposed on the Upper Beam marker.
f. Check-Dial reading difference from 10.00 equal to or less than 150 nanoseconds. (One minor dial division equals one nanosecond.)

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g. Set the Upper Beam DISPLAY switch to RIGHT PLUG-IN B.

fig. 6-52. Horisontal Amplliter Adjuitment and Compeniallon.
h. Set the Lower Beam DISPLAY switch to RIGHT PLUG-IN A.
i. Sot the B TIME/CM switch to $10 \mu$ SEC.
i. Set the time-mark ganarator for 1-millisacond markars and connect the oulput to the right plug-in.
k. Check-Turn the DELAY-TIME MULTIPLIER dial both directions; the intensified portion of the Lower beam should move as the dial is furned.
I. Chock-Rolate the Lower Beam CONTRAST control and observe its effect on the intensity of the lower beam. Tho intensified portion should remain al tho same level while the romainder is varied by the control sotting.
m . Disconnect the markar signal from the right plug-in unit.

## 59. Adjust External Horizontal Amplifer DC Balance-Upper Beam

a. The initial tost seup is shown in Fig. 6-52.
b. Set the conirols as follows:

```
A Triggering Controls
    SOURCE
    COUPLING
    LEFT EXT
    AC
    +
    AUTO STABILITY
    Near 0, knob pushed in
```

Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A VARIABLE
A MODE
B Triggering Controls SOURCE
COUPLING
SLOPE
MODE
LEVEL.
Lower Beam DISPLAY
Lower Beam DISPLAY MAG
B TIME/CM
B Variable
8 MODE
Test Load Unir (both)
Test Function

LEFT PLUG-IN EXT
$\times 10$
1 mSEC
CALIBRATED
NORM

RIGHT EXT
AC
$+$
AUTO STABILITY
Near 0, knob pushed in RIGHT PLUG-IN EXT
$\times 10$
1 mSEC
CALIBRATED
NORM
c. Set the Standard Amplitude Calibrator to supply a 0.5 . volt square-wave signal.
d. Connect the signal through a BNC T connector to the A Triggering TRIGGER INPUT connector and the UPPER BEAM EXT HORIZ IN connector.
e. Connect a parch cord from the A SAWTOOTH connector to the left lest load unit Ext Input connector.

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Fig. 6-53. Adiuatment locations, Exiernal Horizonial Amplifiar DC Delance.
f. Rotate the UPPER BEAM EXT HORIZ VAR $1-10$ control fully clockwise.
g. Adjust the left test load unit Variable control to display 4 or 5 cycles of the waveform in the Upper Beam gralicule area.
h. Position the lefl edge of the display to the center vertical line of the graticule.
i. Rotate the UPPER BEAM EXT HORIZ VAR $1-10$ conlrol from fully clockwise to fully counicrelockwise, then fully clock. wise.
i. Check-No horizontal shift of the left edge of the display as the VAR 1.10 control is rolated.
k. Adjust EXT HORIZ DC BAL R1110 (Fig. 6.53A) while rotaling the VAR $1-10$ control, until there is no shift of the display.

(A) Upper Beam (left side)

(B) Lower Beam (right side)
fig. 6-54. Locations of External Horizantal Amplifier compensalion adjuilments.

1. Return the VAR $1-10$ conirol fully clockwise.
2. Check External Horizontal Amplifier Variable Control Range—Upper Beam
a. Position the left edge of the display to the $2-\mathrm{cm}$ graticule line.
b. Check -5 cm or more of horizontal deflection.
c. Rotate the UPPER BEAM EXT HORIZ VAR $1-10$ control fully counterclockwise.
d. Check-Horizontal deflection equal to or less than 10\% of the deflection noted in step (b).
e. Relurn the VAR 1-10 conlrol fully clockwise.

(A) C1115 mis-adjusted

(B) CIII5 mis-adjusted

(C) C1115 correctly adjusted

Fig. 6-55. Horizontal Amplifier $\times 1-\times 10$ Compensation-Upper Beam.
61. Adjust External Horizontal Amplifier $\times 10$ Compensation-Upper Beam
a. Check--Front corner of waveform similar to Fig. 6-55C, and showing no more than $3 \%$ overshoot, rolloff, or ringing.
b. Adjust C1115 (Fig. 6-54A) for best front corner and flat top.

## 62. Adjust External Horizontal Amplifier $\times 1$ Compensation-Upper Beam

a. Change the DISPLAY MAG switch to $\times 1$.
b. Change the Standard Amplitude Calibrator output to 5 volts.
c. Check-Front corner of waveform similar to Fig. 6-55C, and showing no more than $3 \%$ overshoot, rolloff, or ringing.
d. Adjust Cl100B(Fig. 6-54A) for the best front corner of
the waveform.

## 63. Check Magnifier $\times 1-\times 10$ Ratio Accuracy -Upper Beam

a. Measure the horizontal deflection of the display observed in step 62 (d).
b. Change the Standard Calibrator output to 0.5 volts.
c. Change the DISPLAY MAG switch to $\times 10$.
d. Check-Horizontal deflection of the display should be within $3 \%$ of the display noted in step 62 (d).
e. Set the Upper Beam INTENSITY control so the display is not visible.

## 64. Adjust External Horizontal Amplifier DC Balance-Lower Beam

a. Move the Standard Amplitude Calibrator signal to the
OWER BEAM EXT HORIZ IN connector, and to the B TrigLOWER BEAM EXT HORIZ IN connector, and to the B Triggering EXT TRIGGER INPUT connector.
b. Move the patch cord to connect the B SAWTOOTH connector to the right test load unit Ext Input connector. c. Rotate the LOWER BEAM EXT HORIZ IN VAR 1-10 fully clockwise.
d. Adjust the right test load unit Variable control to display. 4 or 5 cycles of the waveform in the Lower Beam graticule area.
e. Position the left edge of the display to the center vertical line of the graticule.
f. Rotate the LOWER BEAM EXT HORIZ VAR $1-10$ from fully clockwise to fully counterclockwise, then fully clockwise.
g. Check-No horizontal shift of the left edge of the display as the VAR 1-10 control is rotated.
h. Adjust EXT HORIZ DC BAL R1210 (Fig. 6-53B) while
rotating the VAR $1-10$ control, until there is no horizontal shift
h. Adjust EXT HORIZ DC BAL R1210 (Fig. 6-53B) while
rotating the VAR $1-10$ control, until there is no horizontal shift of the display.
i. Return the VAR 1-10 control fully clockwise.
©

d. Adjust the right test load unit Variable control to display. .



Fig. 6-56. Typical display, intensity modulation (Z Axis Operation).

## 65. Check External Horizontal Amplifier Variable Control Range-Lower Beam

a. Position the left edsye of the display to the $2-\mathrm{cm}$ graticule line.
b. Check-Horizontal deflection of the display 5 cm or more.
c. Rotate the LOWER BEAM EXT HORIZ VAR $1-10$ control fully counterclockwise.
d. Check-Horizontal deflection equal to or less than 10\% of the deflection noted in step (b).
e. Return the VAR 1 -IO control fully clockwise.

## 66. Adjust External Horizontal Amplifier (1) $\times 1$ and $\times 10$ Compensation-Lower Beam

a. Check-Front corner of waveform similar to Fig. 6-55C and showing no more than $3 \%$ overshoot, rolloff, or ringing.
b. Adjust C1215 (Fig. 6-54B) for best front corner and flat top.
c. Change the DISPLAY MAG to $\times 1$.
d. Change the Standard Amplitude Calibrator output to 5 volts. Note amount of horizontal deflection because this inf ormation will be needed for step 67(a).
e. Check-Front corner of waveform similar to 6-55C, and showing no more than $3 \%$ overshoot, rolloff, or ringing.
f. Adjust Cl 200 B (Fig. 6-54B) for the best front corner of the waveform.

## 67. Check Magnifier $\times 1-\times 10$ Ratio Accuracy —Lower Beam

a. Measure the horizontal deflection of the display observed in step 66d.
b. Change the Standard Amplitude Calibrator output to 0.5 volts.
c. Change the DISPLAY MAG switch to $\times 10$.
d. Check-Horizontal deflection of the display should be within $3 \%$ of the deflection noted in step 66d.
e. Reduce the Lower Beam intensity. Remove the Standard Calibrator signal and the patch cord.
f. Return the $A$ and $B$ Triggering SOURCE switches to NORM INT, and both DISPLAY MAG switches to $\times 1$.
g. Set the Upper Beam DISPLAY switch to LEFT PLUG-IN A and the Lower Beam DISPLAY switch to RIGHT PLUG-IN B.

## 68. Check Z Axis Operation-Upper and Lower Beams

a. Set the AMPLITUDE CALIBRATOR to 10 VOLTS.
b. Check that both CRT Cathode Selector switches (on rear panel) are set to EXT CRT CATHODE.
c. Adjust the INTENSITY controls of both beams for normal viewing.
d. Remove the two BNC shorting-type caps (on rear panel) from the BNC connectors.
e. Connect a $50 \Omega$ cable from the CAL OUT connector to the Upper Beam BNC connector on the rear panel.
f. Check that the A and B TIME/CM switches are set to 1 mSEC.
g. Check-Upper Beam CRT display for noticeable intensity modulation (see Fig. 6-56). (INTENSITY setting may have to be reduced to view trace modulation.)
h. Move the CAL OUT signal to the Lower Beam BNC connector.
i. Check-Lower Beam CRT display for intensity modulation, as in step (g).
j. Remove the AMPLITUDE CALIBRATOR signal and replace both BNC caps.

## 69. Check A Sweep Sawtooth Amplitude

a. The initial test setup and control settings are shown in Fig. 6-57.
b. Set controls as follows:


Fig. 6-57. Teit equlpment selup for checking axiernal waveforme.

| A Triggering Controls |  |
| :---: | :---: |
| SOURCE | LEFT INT NORM |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| level | Fully clockwiso, knob pushod in |
| Upper Beam DISPLAY | LEFT PLUG-IN A |
| Upper Beam DISPLAY MAG | $\times 1$ |
| A TIME/CM | 1 mSEC |
| A Variagle | CALIBRATED |
| A MODE | NORM |
| B Triggering Conirols |  |
| SOURCE | RIGHT INT NORM |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |
| LEVEL | Fully clockwise, knob pushed in |

Lower Beam DISPLAY
Lower Beam DISPLAY MAG
B TIME/CM
B VARIABLE
B MODE

Tost Load Units |both)
Test Function
Low Load

Tos: Oscilloscopo
Time/cm
5 milliseconds
c. Connect a $10 \times$ probe to the test oscilloscope vertical amplifier input connector.
d. Sel the test oseilloscopa veltical daflection switch lo 5 valis $/ \mathrm{cm}$.
e. Connect the probe tip to the A SAWTOOTH connector, and adjust the test oscilloscope triggering for a siable display.
f. Check—Sawlooth waveform amplifude $\geq 94.5$ volts for a 10.5 cm A sweep.

## 70. Check B Sweep Sawfooth Amplitude

a. Move the probe tip to the B SAWTOOTH connector.
b. Check_Sawtooth waveform amplitude $\geq 94.5$ valts for a 10.5 cm B sweep.

## 71. Check A Sweep Gate Amplitude

a. Connect the probe tip to the A GATE connector.
b. Change the test oscilloscope vertical deflection switch to 0.5 volts/cm.
c. Check-Gate waveform amplitude 10 volis or more.

## 72. Check B Sweep Gate Amplitude

a. Move the probe tip to the B GATE connector.
b. Check-Gaie waveform amplitude 10 volts or more.

## 73. Check Delayed Trigger Waveform Amplifude

a. Change the test oscilloscope time/cm switch to 1 microsecand.
b. Check that the verlical deflection swith is sel to 0.5 volis/cm.
c. Move the probe tip to the DLYD TRIG connector.
d. Rotale the A TIME/CM switch through all positions.
e. Chack—Dolayad triggor pulso amplifuda 7 volis or moro. NOTE
Adjusiment of the lest oscilloscope intensily control may be necessary to observe the pulse at the slower sweep rates.
f. Remove the probe.

## 74. Adjust 8606 Bias

## NOTE

The 8608 BIAS adjustmenis performed in this step affect the adjustments in step 75 through 77 bul the opposite is not true. Once slep 74 has been compleled, any aberrations that appear in the waveforms as a result of performing the step can be removed by performing slops 75 through 77 withoul affecting the 8608 BIAS adjusiments.
a. Set the controls as follows:

A Triggering controls

| SOURCE | LEFT INT NORM |
| :--- | :--- |
| COUPLING | AC |
| SLOPE | + |
| MODE | AUTO STABILITY |

LEVEL
Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM

LEFT INT NORM

AUTO STABILITY
Near 0, knob pushed in LEFT PLUG.IN A $\times 1$
. 1 mSEC


Flg. 6-58, Varilcal Amplifier high-frequency compensation odusle meni locallons, lelf sidei lofi bollom rall removed.

| A Variable | CAlibrated |
| :---: | :---: |
| A MODE | NORM |
| B Triggering conirols |  |
| SOURCE | RIGHT INT NORM |
| COUPLING | $A C$ |
| SLOPE | $+$ |
| MODE | AUTO STABILITY |
| LEVEL | Near O, knob pushed in |
| Lower Bcam DISPLAY | RIGHT PLUG-IN B |
| Lowor Bcam DISPLAY MAG | $\times 1$ |
| B TIME/CM | . 1 mSEC |
| B VARIABLE | CALIBRATED |
| B MODE | NORM |
| Test Load Units [both) |  |
| Test Function | + Pulse |
| Pulse Repelition Rale | Low |

b. Adjust the right plug-in Vertical Position conirol to move the Lower Beam below the viewing area.
c. With the left plug-in Vertical Position control, center the display within the Upper Beam viewing area.
d. Adjust the amplitude of the display to 5 cm with the left plug-in Amplitude control. Use the left plug-in Vertical Position control to keep the display centered within the Upper Beam viewing area.


Fig. 6.59. Vertical Amplifler high-frequancy companialion adjuslmant locallons, ilghi side.
e. Check-Upper Beam CRT display for flat iop.
f. Adjust R69 (soo Fig. 6-58) so the front portion of the displayed waveform flat lop is rolled off slighlly. Readjust R69 so the front pertion of the llat lop just becomes flat.
g. Change the loft plug-in Pulso Repetition Rato control to Med.
h. Change the $A$ TIME/CM switch to $.1 \mu S E C$.
i. Set the Upper Beam POSITION control so the rising portion of the pulse is located near the center of the graticule.
i. With the left plug-in Vertical Position control, move the waveform so the fronl-corner is located 3 cm above the Upper Beam graticule centor horizontal line. Note the appearance of the front corner of tho waveform.
k. Using the left plug-in Vertical Position conirol, move the flat top portion of the display 3 cm below the Upper Beam gralicule center horizontal line.
I. Check-For no change in frant corner of the waveform. Allowable front corner change is $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$.
m. Change the left plug-in Test Function switch to -Pulse, and the Type 556 A Triggering SLOPE switch to - The waveform will now appear as a negative going pulse.
n . Repeat slep (i] through (l) but position the lower leading corner of the waveform to the same points described in the steps.
o. Check-Chango in front corner of the waveform should be $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$.
p. Readjust 869 slightly so the front-corner change is within the limits stated in slep (o).
q. Change the leff plug-in Test Function switch to +Pulse، and the Type 556 A Triggering SLOPE switch to + .
r. Adjust the left plug-in Vertical Position control to move the Upper Beam display below the viewing area.
s. Repeat sleps (c) and (d) for the right plug-in unit and Lower Beam.
t. Check—Lower Beam CRT display for flat top.
u. Adjust R259 (see Fig. 6-59) so the front portion of the display waveform flat top is rolled off slightly. Readjust R259 so the front-portion of the flat top jusi becomas flat.
v. Repeat steps (g) through (k) for the right plug-in unit and Lower Beam.
w. Check-for no change in front corner of the waveform. Allowabla front cornor chango is $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$.
$x$. Repeat steps ( m ) and ( n ) for the right plug-in unit and Lower Beam.
y. Check-Change in front corner of the waveform should bo $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$.
z. Readjust R259 slightly so the froni-corner change is within the limils slated in slep (y).
aa. Change the right plug - in Test Function switch 10 +Pulso, and the Typo 556 日 Triggering SLOPE switch $10+$.

## 75. Adjust Vertical Amplifier High Frequency (1) Compensations-Left

a. Set the controls as follows:

A Triggering conirols

SOURCE
COUPLING
SLOPE
MODE
LEVEL
Upper Beam DISPLAY
Upper Beam DISPLAY MAG
A TIME/CM
A Variable
A MODE

## LEFT INT NORM

AC
$+$
AUTO STABILITY
Near 0. knob pushed in LEFT PLUG.IN A $\times 1$
$.1 \mu \mathrm{SEC}$
CAlIbRATED
NORM


Fig. 6.60. Leff and Right Verical Amplifier high-frequancy compensalion adusimeni localans tiop vlow of the Instrument).

B Triggering contrals

SOURCE
COUPLING
SIOPE
MODE
LEVEL
Lower Boom DISPLAY
Lowor Beam DISPLAY MAG
B TIMEJCM

- VARIABLE

B MODE
Tost Load Unils (both)
Test function
Pulse Repetition Rate

RIGHT INT NORM
$A C$
$+$
AUTO STABILITY
Near 0, knob pushod in RIGHT PLUG.IN B $\times 1$
. $1 \mu$ SEC
CALIBRATED
NORM

+ Pulso
Med
b. Set the right plug-in Vartical Position control so the Lower Beam display is positioned bolow tho gralicule viewing area.
c. Set the left plug-in Vertical Position control so tho Upper Bcam display is positioned info view. Position the top conner of the pulse near the verlical centerline and about 1.5 cm above the Upper 8cam horizontal center line.
d. Check-Upper Beam CRT display for optimum square corner and flal top, with peak overshool, rolloff, or ringing not to exceed $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$. See Fig. 6.61 A for a typical display.
e. Adjust left amplifier compensalions as shown in Table 6-5. Adjustment locations are shown in Fig. 6-58 and Fig. 6.60.

TABLE 6-5

| Adjustment | Area of Waveform Affecled (approximate distance from leading edge near lop corner ${ }^{7}$ of waveforml |
| :---: | :---: |
| Left Amplifier |  |
| 143 | Leading edge (adjust with L143). |
| 1143 | Leading edge (adjust with L43]. |
| 164 | 10 nanoseconds (adjust with L164). |
| 1164 | 10 nanoseconds (adjus! with L64). |
| R52 HF Comp 1 | Adjusis damping of slowest ringing component. |
| R54 HF Comp 2 | Adjusis damping of foslest ringing component. |
| C10 | Leading edge to 5 nanoseconds. |
| C17 | 330 nanoseconds (termination bump). |
| C51 | Leval of major front portion. Adjusi at sweep rale of 10 microseconds/ cm. |
| C53 | Leading edge to 20 nanoseconds. |
| C54 | Leading edge 105 nanoseconds. |
| C55 | 101030 nanoseconds. |
| Crossovar Amplifiar R31 | Adjust with C 30 for minimum ringing. |
| C19 | 330 nanosoconds (formination bump]. |
| C30 | Adjust with R31 for minimum ringing. |
| C31 | Leading edge to 75 nanoseconds. |
| C32 | Leval of major front portion. Adjusl al sweep rale of 10 microsecands/ cm . |
| Right Amplifier L254 | 10 nanosaconds (adjust with L454.). |
| 1454 | 10 nanosaconds (adjusi with L254). |
| L224 | Leading edge (adjust with L424). |
| 1424 | Leading edge (adjust with L224). |
| R242 HF Comp 1 | Adjusls damping of slowest ringing component. |
| R244 HF Comp 2 | Adjusls damping of faslest ringing component. |
| C210 | Leading edge to 5 nanoseconds. |
| C218 | 330 nanoseconds (termination bump). |
| C241 | Lavel of major front portion. Adjust al sweop rale of 10 microseconds/ cm . |
| C242 | Leading edge to 20 nanoseconds. |
| C244 | Leading edge to 5 nanoseconds. |
| C245 | 101030 nanoseconds. |

For positiva-golng pulse waveform; near boltom corner when vlewing a negalive-going pulse wavaform.


Fig. 6-61. Typical displays, high-frequency compensations correctly adjusted.

If the pulse waveform does not meet the requirements outlined in step (d) and re-adjustments are indicated, minimum adjustments of C51, C53, C54, C55, C10, R52 and R54 may be sufficient. However, if the CRT display indicates that the circuit is seriously misadjusted, adjust R52 and R54 for minimum ringing, and then proceed with small adjustments to the capacitors.

Each resistor and capacitor time-constant network affects a different portion of the waveform; however, each adjustment interacts with all other adjustments. Close observation of the waveform while switching the DISPLAY MAG from $\times 1$ to $X 10$ and vice versa as the adjustments are made will result in a square corner and flat top as illustrated in Fig. 6-61 (A) and (B). Also see Fig. 6-62 for an example of misadjustment.

## 76. Adjust Vertical Amplifier High Frequency Compensations-Crossover

a. Change the A Triggering SOURCE switch to RIGHT INT


Fig. 6-62. Example of misadjustment of C244, right vertical amplifier; sweep speed 100 nanoseconds/cm.

NORM, and the Upper Beam DISPLAY switch to RIGHT PLUGIN A.
b. Adjust the amplitude of the Upper Beam display to 5 cm with the right test load unit Amplitude control. Use the TRACE SEPARATION and right plug-in Vertical Position controls to position the rising portion of the displays near their respective graticule centers.
c. Set the Lower Beam INTENSITY control so the Lower Beam is not visible.
d. Check-Upper Beam CRT display for optimum square corner and flat top, with peak overshoot, rolloff, or ringing not to exceed $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$. See Fig. 6-61A for a typical display.
e. Adjust crossover amplifier compensations as indicated in Table 6-5.

## 77. Adjust Vertical Amplifier High Frequency © Compensations-Right

a. Set the Lower Beam INTENSITY control so the Lower Beam display is visible and decrease the Upper Beam INTENSITY control to remove the Upper Beam display.
b. Check that the Lower Beam display is located in the center of the Lower Beam graticule area, with the rising porfion of the waveform near the center vertical line.
c. Check-Lower Beam CRT display for optimum square corner and flat top, with peak overshoot, rolloff, or ringing not to exceed $\leq 2.25 \%$ of 50 mm or $\leq 1.125 \mathrm{~mm}$. See Fig. 6-61B for a typical display.
d. Adjust right amplifier compensations as indicated in Table 6-5.


Fig. 6-63. Hllustrating method of risetime measurement.

## 78. Check Vertical Amplifier Risetime—Right

a. Check that the B TIME/CM switch is set to . $1 \mu \mathrm{SEC}$.
b. Set the Lower Beam DISPLAY MAG to $\times 10$.
c. Position the $5-\mathrm{cm}$ Lower Beam display so that the $10 \%$ point on the rising portion crosses the intersection of the $1-\mathrm{cm}$
horizontal graticule line and the vertical graticule center line. See Fig. 6-63B for correct display positioning.
d. Check-Risetime of the $10 \%$ to $90 \%$ portion of the rising portion should be 6.93 nanoseconds or less with the test load unit pulse risetime of 3 nanoseconds. Fig. $6-63 \mathrm{~B}$ shows a typical display.

## NOTE

When performing steps 78 through 80 , take into consideration sweep timing error, if any, and/or geometry and orthogonality in the area where the measurement is made.

## 79. Check Vertical Amplifier Risetime-Crossover

a. Decrease the Lower Beam INTENSITY so that the Lower Beam display disappears, and increase the Upper Beam INTENSITY control so the Upper Beam display becomes visible. Set the Upper Beam DISPLAY MAG switch to $\times 10$.
b. With the TRACE SEPARATION and Upper Beam POSITION controls, position the Upper Beam 5-cm display so that the $10 \%$ point on the rising portion of the waveform crosses the intersection of the Lower Beam graticule horizontal center line with graticule vertical center line. Fig. 6-63A shows the correct positioning of the display.
c. Check-Risetime of the $10 \%$ to $90 \%$ portion of the pulse rise should be 6.93 nanoseconds or less.

## 80. Check Vertical Amplifier Risetime-Left

a. Change the A Triggering SOURCE switch to LEFT INT NORM.
b. Change the Upper Beam DISPLAY to LEFT PLUG-IN A.
c. With the left test load unit Vertical Position and Upper Beam POSITION controls, position the $5-\mathrm{cm}$ display so that the $10 \%$ point on the rising portion of the waveform is at the same point as in step 79 (b).
d. Check-Risetime of the $10 \%$ to $90 \%$ portion of the pulse rise should be 6.93 nanoseconds or less.

## NOTES

## PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix, Inc. Field Office or representative.

Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number, instrument type or number, serial or model number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix, Inc. Field Office or representative will contact you concerning any change in part number.

## SPECIAL NOTES AND SYMBOLS

$\times 000$ Part first added at this serial number
$00 \times$ Part removed after this serial number
*000-0000-00 Asterisk preceding Tektronix Part Number indicates manufactured by or for Tektronix, Inc., or reworked or checked components.

Use 000-0000-00 Part number indicated is direct replacement.
(1) Screwdriver adjustment.

Control, adjustment or connector.

ABBREVIATIONS AND SYMBOLS

| A or amp | amperes | $\stackrel{ }{L}$ | inductance |
| :---: | :---: | :---: | :---: |
| $A C$ or ac | alternating current | $\lambda$ | lambda-wavelength |
| AF | audio frequency | >> | large compared with |
| $\alpha$ | alpha-common-base current amplification factor | $<$ | less than |
| AM | amplitude modulation | LF | low frequency |
| $\approx$ | approximately equal to | Ig | length or long |
| $\beta$ | beta-common-emitter current amplification factor | LV | low voltage |
| BHB | binding head brass | M | mega or $10^{6}$ |
| BHS | binding head steel | m | milli or $10^{-3}$ |
| BNC | baby series " N " connector | MS: or meg | megohm |
| $\times$ | by or times | $\mu$ | micro or $10^{-6}$ |
| C | carbon | mc | megacycle |
| C | capacitance | met. | metol |
| cap. | capacitor | MHz | megahertz |
| cer | ceramic | mm | millimeter |
| cm | centimeter | ms | millisecond |
| comp | composition | - | minus |
| conn | connector | mtg hdw | mounting hardware |
| $\sim$ | cycle | n | nano or $10^{-9}$ |
| $\mathrm{c} / \mathrm{s}$ or cps | cycles per second | no. or \# | number |
| CRT | cathode-ray tube | ns | nanosecond |
| csk | countersunk | OD | outside diameter |
| $\Delta$ | increment | OHB | oval head biass |
| dB | decibel | OHS | oval head steel |
| dBm | decibel referred to one milliwatt | $\Omega$ | omega-ohms |
| DC or dc | direct current | $\omega$ | omega-angular frequency |
| DE | double end | p | pico or $10^{-12}$ |
|  | degrees | / | per |
| ${ }^{\circ} \mathrm{C}$ | degrees Celsius (degrees centigrade) | \% | percent |
| ${ }^{\circ} \mathrm{F}$ | degrees Fahrenheit | PHB | pan head brass |
| ${ }^{\circ} \mathrm{K}$ | degrees Kelvin | ¢ | phi-phase angle |
| dia | diameter | $\pi$ | pi-3.1416 |
| $\div$ | divide by | PHS | pan head steel |
| div | division | + | plus |
| EHF | extremely high frequency | $\pm$ | plus or minus |
| elect. | electrolytic | PIV | peak inverse voltage |
| EMC | electrolytic, metal cased | plste | plastic |
| EMI | electromagnetic interference (see RFI) | PMC | paper, metal cased |
| EMT | electrolytic, metal tubular | poly | polystyrene |
| $\stackrel{\varepsilon}{\varepsilon}$ | epsilon-2.71828 or \% of errar | prec | precision |
| $\geq$ | equal to or greater than | PT | paper, tubular |
| $\leq$ | equal to or less than | PTM | paper or plastic, fubular, molded |
| ext | external | pwr | pawer |
| F or f | farad | Q | figure of merit |
| F \& 1 | focus and intensity | RC | resistance capacitance |
| FH8 | flat head brass | RF | radia frequency |
| FHS | flat head steel | RFI | radio frequency interference (see EMI) |
| Fil HB | fillister head brass | RHB | round head brass |
| Fil HS | fillister head steel | $\rho$ | rho-resistivity |
| FM | frequency madulatian | RHS | round head steel |
| ft | feet or faot | r/min or rpm | revolutians per minute |
| G | giga or $10^{9}$ | RMS | root mean square |
| g | acceleration due to gravity | s or sec. | secand |
| Ge | germanium | SE | single end |
| GHz | gigahertz | Si | silicon |
| GMV | guaranteed minimum value | SN or S/N | serial number |
| GR | General Radio | $<$ | small compared with |
| $>$ | greater than | ${ }_{T}^{\text {T }}$ | tera or $10^{12}$ |
| H or h | henry | TC | temperature compensated |
| h | height or high | TD | tunnel diode |
| hex. | hexagonal | THB | truss head brass |
| HF | high frequency | ${ }^{0}$ | theta-angular phase displacement |
| HHB | hex head brass | thk | thick |
| HHS | hex head steel | THS | truss head steel |
| HSB | hex socket brass | tub. | tubular |
| HSS | hex socket steel | UHF | ultro high frequency |
| HV | high valtage | $\checkmark$ | volt |
| Hz | hertz (cycles per second) | VAC | volts, alternating current |
| 10 | inside diameter | var | variable |
| IF | intermediote frequency | VDC | volts, direct current |
| in. | inch or inches | VHF | very high frequency |
| incd | incandescent | VSWR | voltage standing wave ratio |
| $\infty$ | infinity | W | watt |
| int | internal | $w$ | wide ar width |
| $\boldsymbol{J}$ | integral | w/ | with |
| k | kilohms or kila ( $10^{3}$ ) | w/o | without |
| k $\Omega$ | kilohm | WW | wire-wound |
| kc | kilocycle | xmfr | transfarmer |
| kHz | kilohertz |  |  |

# SECTION 7 ELECTRICAL PARTS LIST 

Values are fixed unless marked Variable.


## Capacitors

Tolerance $\pm 20 \%$ unless otherwise indicated.

| C2 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C10 | 281-0060-00 | 100 | 829 | 2-8 pF, Var | Cer |  |  |
| C10 | 281-0036-00 | 830 |  | 3-12 pF, Var | Cer |  |  |
| Cl 3 | 281-0513-00 |  |  | 27 p F | Cer | 500 V |  |
| Cl 6 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| Cl 7 | 281-0005-00 |  |  | 1.5-7 pF, Var | Cer |  |  |
| C19 | 281-0012-00 |  |  | 7-45 pF, Var | Cer |  |  |
| C20 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C26 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C30 | 281-0060-00 |  |  | 2-8 pF, Var | Cer |  |  |
| C31 | 281-0029-00 |  |  | 1.5 .7 pF , Var | Cer |  |  |
| C32 | 281-0005-00 |  |  | $1.5-7 \mathrm{pF}$, Var | Cer |  |  |
| C39 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C41 | 281-0572-00 |  |  | 6.8 pF | Cer | 500 V | $\pm 0.5 \mathrm{pF}$ |
| C42 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |


| Capacitors (cont) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Serial/Model <br> Eff | No. Disc |  | Desc |  |  |
| C47 | 281-0510-00 |  |  | 22 pF | Cer | 500 V |  |
| C49 | 281-0630-00 |  |  | 390 pF | Cer | 500 V | 5\% |
| C50 | 281-0528-00 | 100 | 829 | 82 pF | Cer | 500 V | 10\% |
| C50 | 281-0523-00 | 830 |  | 100 pF | Cer | 350 V |  |
| C51 | 281-0063-00 |  |  | 9-35 pF, Var | Cer |  |  |
| C52 | 281-0513-00 |  |  | 27 pF | Cer | 500 V |  |
| C53 | 281-0063-00 |  |  | 9.35 pF , Var | Cer |  |  |
| C54 | 281-0063-00 |  |  | 9-35 pF, Var | Cer |  |  |
| C55 | 281-0060-00 |  |  | 2.8 pF , Var | Cer |  |  |
| C56 | 281-0504-00 | X830 |  | 10 pF | Cer | 500 V | 10\% |
| C58 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C60 | 283-0000-00 | X830 |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C65 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C70 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C71 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C81 | 281-0592-00 |  |  | 4.7 pF | Cer |  | $\pm 0.5 \mathrm{pF}$ |
| C82 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C87 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C90 | 281-0523-00 |  |  | 100 pF | Cer | 350 V |  |
| C91 | 281-0592-00 |  |  | 4.7 pF | Cer |  | $\pm 0.5 \mathrm{pF}$ |
| C93 | 283-0079-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 250 V |  |
| C94 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C99 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C100 | 281-0601-00 |  |  | 7.5 pF | Cer | 500 V | $\pm 0.5 \mathrm{pF}$ |
| C106 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C110 | 281-0550-00 | X830 |  | 120 pF | Cer | 500 V | 10\% |
| C113 | 281-0513-00 |  |  | 27 pF | Cer | 500 V |  |
| C115 | 281-0513-00 |  |  | 27 pF | Cer | 500 V |  |
| C116 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C139 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C141 | 281-0572-00 |  |  | 6.8 pF | Cer | 500 V | $\pm 0.5 \mathrm{pF}$ |
| C142 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C148 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C158 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C160 | 283-0000-00 | X830 |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C170 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C187 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C202 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C207 | 281-0550-00 | X830 |  | 120 pF | Cer | 500 V | 10\% |
| C210 | 281-0060-00 | 100 | 829 | $2-8 \mathrm{pF}$, Var | Cer |  |  |
| C210 | 281-0036-00 | 830 |  | 3-12 pF, Var | Cer |  |  |
| C213 | 281-0513-00 |  |  | 27 pF | Cer | 500 V |  |
| C216 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C218 | 281-0005-00 |  |  | 1.5-7 pF, Var | Cer |  |  |
| C222 | 281-0572-00 |  |  | 6.8 pF | Cer | 500 V | $\pm 0.5 \mathrm{pF}$ |

Capacitors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc | Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C225 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C230 | 281-0510-00 |  |  | 22 pF | Cer | 500 V |  |
| C231 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C239 | 281-0630-00 |  |  | 390 pF | Cer | 500 V | 5\% |
| C240 | 281-0528-00 | 100 | 829 | 82 pF | Cer | 500 V | 10\% |
| C240 | 281-0523-00 | 830 |  | 100 pF | Cer | 350 V | 10\% |
| C241 | 281-0063-00 |  |  | 9.35 pF , Var | Cer |  |  |
| C242 | 281-0063-00 |  |  | 9.35 pF , Var | Cer |  |  |
| C243 | 281-0513-00 |  |  | 27 pF | Cer | 500 V |  |
| C244 | 281-0063-00 |  |  | $9-35 \mathrm{pF}$, Var | Cer |  |  |
| C245 | 281-0060-00 |  |  | 2-8 pF, Var | Cer |  |  |
| C246 | 281-0504-00 | X830 |  | 10 pF | Cer | 500 V | 10\% |
| C248 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C250 | 283-0000-00 | X830 |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C255 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C260 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C261 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C271 | 281-0592-00 |  |  | 4.7 pF | Cer |  | $\pm 0.5 \mathrm{pF}$ |
| C272 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C277 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C280 | 281-0523-00 |  |  | 100 pF | Cer | 350 V |  |
| C281 | 281-0592-00 |  |  | 4.7 pF | Cer |  | $\pm 0.5 \mathrm{pF}$ |
| C283 | 283-0079-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 250 V |  |
| C284 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C289 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C297 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C400 | 281-0601-00 |  |  | 7.5 pF | Cer | 500 V | $\pm 0.5 \mathrm{pF}$ |
| C413 | 281-0513-00 |  |  | 27 pF | Cer | 500 V |  |
| C414 | 281-0513-00 |  |  | 27 pF | Cer | 500 V |  |
| C416 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C422 | 281-0572-00 |  |  | 6.8 pF | Cer | 500 V | $\pm 0.5 \mathrm{pF}$ |
| C425 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C448 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C450 | 283-0000-00 | X830 |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C460 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C500 | 283-0002.00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C501 | 283-0092-00 |  |  | $0.03 \mu \mathrm{~F}$ | Cer | 200 V | +80\%-20\% |
| C502 | 283-0032-00 |  |  | 470 pF | Cer | 500 V | 5\% |
| C504 | 281-0603-00 |  |  | 39 pF | Cer | 500 V | 5\% |
| C508 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C512 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C520 | 283-0095-00 |  |  | 56 pF | Cer | 200 V | 10\% |
| C525 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C526 | 281-0523-00 |  |  | 100 pF | Cer | 350 V |  |
| C528 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |

Capacitors (cont)

| Ckt. No. | Tektronix Part No. | Seri Eff | No. Disc |  | Desc |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C547 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C552 | 281-0580-00 |  |  | 470 pF | Cer | 500 V | 10\% |
| C558 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C560 | 281-0503-00 |  |  | 8 pF | Cer | 500 V | $\pm 0.5 \mathrm{pF}$ |
| C561 | 281-0508-00 |  |  | 12 pF | Cer | 500 V |  |
| C567 | 283-0026-00 |  |  | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C574 | 281-0518-00 |  |  | 47 pF | Cer | 500 V |  |
| C577 | 283-0077-00 |  |  | 330 pF | Cer | 500 V | 5\% |
| C578 | 281-0504-00 | X2000 |  | 10 pF | Cer | 500 V | 10\% |
| C581 | 281-0543-00 |  |  | 270 pF | Cer | 500 V | 10\% |
| C583 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C584 | 281-0504-00 | 100 | 1999X | 10 pF | Cer | 500 V | 10\% |
| C586 | 281-0523-00 | 100 | 1999 | 100 pF | Cer | 350 V |  |
| C586 | 281-0540-00 | 2000 |  | 51 pF | Cer | 500 V | 5\% |
| C589 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C604 | 283-0026-00 |  |  | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C611 | 290-0187-00 |  |  | $4.7 \mu \mathrm{~F}$ | Elect. | 35 V |  |
| C614 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C622 | 281-0543-00 |  |  | 270 pF | Cer | 500 V | 10\% |
| C631 | 281-0513-00 |  |  | 27 pF | Cer | 500 V |  |
| C635 | 281-0518-00 |  |  | 47 pF | Cer | 500 V |  |
| C637 | 281-0523-00 |  |  | 100 pF | Cer | 350 V |  |
| C643 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C648 | 281-0523-00 |  |  | 100 pF | Cer | 350 V |  |
| $\begin{aligned} & \text { C660A } \\ & \text { C660B } \end{aligned}$ |  |  |  | $\begin{aligned} & 10 \mu \mathrm{~F} \\ & 1 \mu \mathrm{~F} \end{aligned}$ |  |  |  |
| C660C | *295-0099-00 |  |  | $0.1 \mu \mathrm{~F}$ |  | Capacitor |  |
| C660D |  |  |  | $0.01 \mu \mathrm{~F}$ |  |  |  |
| C660E |  |  |  | 997.5 pF |  |  |  |
| C660F | 281-0574-00 |  |  | 82 pF | Cer | 500 V | 10\% |
| C660G | 281-0010-00 |  |  | 4.5-25 pF, Var | Cer |  |  |
| $\mathrm{C660H}$ | 281-0007-00 |  |  | 3-12 pF, Var | Cer |  |  |
| C660J | 281-0007-00 |  |  | 3-12 pF, Var | Cer |  |  |
| C666 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C668 | 281-0528-00 |  |  | 82 pF | Cer | 500 V | 10\% |
| C673 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C674 | 283-0010-00 |  |  | $0.05 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C675A | 285-0576-00 |  |  | $1 \mu \mathrm{~F}$ | PTM | 100 V | 10\% |
| C675B | 285-0633-00 |  |  | $0.22 \mu \mathrm{~F}$ | PTM | 100 V | 10\% |
| C675C | 285-0636-00 |  |  | $0.022 \mu \mathrm{~F}$ | PTM | 200 V |  |
| C675D | 285-0543-00 |  |  | $0.0022 \mu \mathrm{~F}$ | MT | 400 V |  |
| C675E | 281-0550-00 |  |  | 120 pF | Cer | 500 V | 10\% |
| C676 | 281-0550-00 |  |  | 120 pF | Cer | 500 V | 10\% |
| C681 | 281-0010-00 |  |  | 4.5-25 pF, Var | Cer |  |  |

Capacitors (cont)

| Ckt. No. | Tektronix Part No. | $\begin{aligned} & \text { Seri } \\ & \text { Eff } \end{aligned}$ | No. Disc |  | Desc |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C683 | 281-0010-00 | X2000 |  | 4.5-25 pF, Var | Cer |  |  |
| C688 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C696 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C698 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C699 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C700 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C701 | 283-0092-00 |  |  | $0.03 \mu \mathrm{~F}$ | Cer | 200 V | +80\%-20\% |
| C702 | 283-0032-00 |  |  | 470 pF | Cer | 500 V | 5\% |
| C704 | 281-0603-00 |  |  | 39 pF | Cer | 500 V | 5\% |
| C708 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C712 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C720 | 283-0095-00 |  |  | 56 pF | Cer | 200 V | 10\% |
| C725 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C726 | 281-0523-00 |  |  | 100 pF | Cer | 350 V |  |
| C728 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C747 | 283-0028-00 |  |  | $0.0022 \mu \mathrm{~F}$ | Cer | 50 V |  |
| C752 | 281-0580-00 |  |  | 470 pF | Cer | 500 V | 10\% |
| C758 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C760 | 281-0503-00 |  |  | 8 pF | Cer | 500 V | $\pm 0.5 \mathrm{pF}$ |
| C761 | 281-0508-00 |  |  | 12 pF | Cer | 500 V |  |
| C767 | 283-0026-00 |  |  | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C774 | 281-0518-00 |  |  | 47 pF | Cer | 500 V |  |
| C777 | 283-0077-00 |  |  | 330 pF | Cer | 500 V | 5\% |
| C778 | 281-0504-00 | X2000 |  | 10 pF | Cer | 500 V | 10\% |
| C781 | 281-0543-00 |  |  | 270 pF | Cer | 500 V | 10\% |
| C783 | 283-0020-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C784 | 281-0504-00 | 100 | 1999X | 10 pF | Cer | 500 V | 10\% |
| C786 | 281-0523-00 | 100 | 1999 | 100 pF | Cer | 350 V |  |
| C786 | 281-0504-00 | 2000 |  | $51 \mu \mathrm{~F}$ | Cer | 500 V | 5\% |
| C789 | 283-0002-00 | 100 | 1999 | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C789 | 283-0000-00 | 2000 |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C795 | 283-0002-00 | X2000 |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C796 | 283-0002-00 | 100 | 1999X | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C797 | 283-0002-00 | 100 | 1999X | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C799 | 281-0573-00 | 100 | 1999X | 11 pF | Cer |  | 10\% |
| C804 | 283-0026-00 |  |  | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C811 | 290-0187-00 |  |  | $4.7 \mu \mathrm{~F}$ | Elect. | 35 V |  |
| C813 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C823 | 281-0543-00 |  |  | 270 pF | Cer | 500 V | 10\% |
| C831 | 281-0513-00 |  |  | 27 pF | Cer | 500 V |  |
| C835 | 281-0518-00 |  |  | 47 pF | Cer | 500 V |  |
| C837 | 281-0523-00 |  |  | 100 pF | Cer | 350 V |  |
| C840 | 281-0542-00 | X330 |  | 18 pF | Cer | 500 V | 10\% |
| C843 | 283-0000-00 |  |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C848 | 281-0523-00 |  |  | 100 pF | Cer | 350 V |  |

## Electrical Parts List-Type 556



Capacitors (cont)

| Ckt. No. | Tektronix Part No. | Serial/Model No. Eff Disc |  | Descrip |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1074 | 281-0508-00 |  | 12 pF | Cer | 500 V |  |
| C1100B | 281-0031-00 |  | 3-12 pF, Var | Cer |  |  |
| C1100D | 281-0602-00 |  | 68 pF | Cer | 500 V | 5\% |
| C1110 | 283-0001-00 | X2000 | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1112 | 283-0001-00 |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1115 | 281-0010-00 |  | 4.5-25 pF, Var | Cer |  |  |
| C1117 | 281-0547-00 |  | 2.7 pF , | Cer | 500 V | 10\% |
| C1141 | 281-0549-00 |  | 68 pF | Cer | 500 V | 10\% |
| C1144 | 283-0002-00 |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| $\mathrm{Cl146}$ | 281-0549-00 |  | 68 pF | Cer | 500 V | 10\% |
| C1165 | 281-0022-00 |  | $8-50 \mathrm{pF}, \mathrm{Var}$ | Cer |  |  |
| C1169 | 283-0001-00 |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1172 | 281-0022-00 |  | $8-50 \mathrm{pF}, \mathrm{Var}$ | Cer |  |  |
| C1174 | 281-0053-00 |  | 0.35-1.37 pF, Var | Cer |  |  |
| C1176 | 283-0001-00 |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1182 | 281-0022-00 |  | $8-50 \mathrm{pF}, \mathrm{Var}$ | Cer |  |  |
| C1184 | 281-0053-00 |  | 0.35-1.37 pF, Var | Cer |  |  |
| C1186 | 283-0001-00 |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1190 | 283-0002-00 |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| Cl 193 | 281-0036-00 |  | 3-12 pF, Var | Cer |  |  |
| C1195 | 283-0000-00 |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1197 | 285-0628-00 |  | $0.033 \mu \mathrm{~F}$ | PTM | 300 V |  |
| C1200B | 281-0007-00 |  | 3-12 pF, Var | Cer |  |  |
| C1200D | 281-0602-00 |  | 68 pF | Cer | 500 V | 5\% |
| C1210 | 283-0001-00 | X2000 | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1212 | 283-0001-00 |  |  |  | 500 V |  |
| C1215 | 281-0010-00 |  | 4.5-25 pF, Var | Cer |  |  |
| C1217 | 281-0547-00 |  | 2.7 pF | Cer | 500 V | 10\% |
| Cl241 | 281-0549-00 |  | 68 pF | Cer | 500 V | 10\% |
| C1244 | 283-0002-00 |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1246 | 281-0549-00 |  | 68 pF | Cer | 500 V | 10\% |
| C1265 | 281-0022-00 |  | 8-50 pF, Var | Cer |  |  |
| C1269 | 283-0001-00 |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1272 | 281-0022-00 |  | 8-50 pF, Var | Cer |  |  |
| C1274 | 281-0053-00 |  | 0.35-1.37 pF, Var | Cer |  |  |
| C1276 | 283-0001-00 |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1282 | 281-0022-00 |  | 8-50 pF, Var | Cer |  |  |
| C1284 | 281-0053-00 |  | 0.35-1.37 pF, Var | Cer |  |  |
| C1286 | 283-0001-00 |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1290 | 283-0002-00 |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1293 | 281-0036-00 |  | 3-12 pF, Var | Cer |  |  |
| C1295 | 283-0000-00 |  | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1297 | 285-0628-00 |  | $0.033 \mu \mathrm{~F}$ | PTM | 300 V |  |
| C1300 | 285-0526-00 |  | $0.1 \mu \mathrm{~F}$ | MT | 400 V |  |
| C1302 | 281-0523-00 |  | 100 pF | Cer | 350 V |  |

Capacitors (cont)

| Ckt. No. | Tektronix Part No. | Seria Eff | No. Disc |  | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cl 303 | 283-0621-00 |  |  | $0.0027 \mu \mathrm{~F}$ | Mica | 1000 V | 5\% |
| C1305 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1311 | 281-0544-00 |  |  | 5.6 pF | Cer | 500 V | 10\% |
| C1314 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1315 | 285-0622-00 |  |  | $0.1 \mu \mathrm{~F}$ | PTM | 100 V |  |
| C1316 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1321 | 283-0116-00 |  |  | 820 pF | Cer | 500 V | 5\% |
| C1322 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\% - $20 \%$ |
| C1323 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1325 | 285-0576-00 |  |  | $1 \mu \mathrm{~F}$ | PTM | 100 V | 10\% |
| C1326 | 281-0556-00 |  |  | 500 pF | Cer | 10,000 V |  |
| C1327 | 283-0096-00 |  |  | 500 pF | Cer | 20,000 V |  |
| C1328 | 283-0556-00 |  |  | 500 pF | Cer | $10,000 \mathrm{~V}$ |  |
| C1329 | 283-0071-00 |  |  | $0.0068 \mu \mathrm{~F}$ | Cer | 5000 V |  |
| C1330 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1331 | 283-0059-00 |  |  | $1 \mu \mathrm{~F}$ | Cer | 25 V | +80\%-20\% |
| C1332 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1333 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1334 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1342 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1347 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\% - $20 \%$ |
| C1352 | 281-0523-00 |  |  | 100 pF | Cer | 350 V |  |
| C1353 | 283-0621-00 |  |  | $0.0027 \mu \mathrm{~F}$ | Mica | 1000 V | 5\% |
| C1355 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1361 | 281-0544-00 |  |  | 5.6 pF | Cer | 500 V | 10\% |
| C1364 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1365 | 285-0622-00 |  |  | $0.1 \mu \mathrm{~F}$ | PTM | 100 V |  |
| C1366 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\% - $20 \%$ |
| C1371 | 283-0116-00 |  |  | 820 pF | Cer | 500 V | 5\% |
| C1372 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\% - $20 \%$ |
| C1373 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\% - $20 \%$ |
| C1376 | 285-0526-00 |  |  | $0.1 \mu \mathrm{~F}$ | MT | 400 V |  |
| C1378 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1382 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1383 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1384 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1391 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1392 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1397 | 283-0082-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 4000 V | +80\%-20\% |
| C1400 | *285-0672-00 | X2047 |  | $0.1 \mu \mathrm{~F}$ | MT | 600 V | +5\%-15\% |
| C1404 | 285-0718-00 |  |  | $3.75 \mu \mathrm{~F}$ | PTM |  | 10\% |
| C1412 | 290-0173-00 |  |  | $200 \mu \mathrm{~F}$ | Elect. | 250 V |  |
| C1413 | 290-0303-00 | X2000 |  | $5 \mu \mathrm{~F}$ | Elect. | 300 V | +75\%-10\% |
| C1414 | 283-0067-00 | 100 | 1999X | $0.001 \mu \mathrm{~F}$ | Cer | 200 V | 10\% |
| C1421 | 285-0566-00 | 100 | 1999 | $0.022 \mu \mathrm{~F}$ | PTM | 200 V | 10\% |
| C1421 | 285-0572-00 | 2000 |  | $0.1 \mu \mathrm{~F}$ | PTM | 200 V |  |

Capacitors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc | Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1424A, B, C, D | 290-0294-00 |  |  | $10 \times 10 \times 20 \times 40 \mu \mathrm{~F}$ | Elect. | 300/400 | /400 V |
| C1426A,B,C,D | 290-0294-00 |  |  | $10 \times 10 \times 20 \times 40 \mu \mathrm{~F}$ | Elect. | 300/400 | /400 V |
| C1432 | 290-0169-00 |  |  | $400 \mu \mathrm{~F}$ | Elect. | 250 V |  |
| C1433 | 285-0572-00 |  |  | $0.1 \mu \mathrm{~F}$ | PTM | 200 V |  |
| C1434 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1435 | 290-0303-00 |  |  | $5 \mu \mathrm{~F}$ | Elect. | 300 V | +75\%-10\% |
| C1436 | 290-0266-00 |  |  | $290 \mu \mathrm{~F}$ | Elect. | 15 V |  |
| C1437 | 283-0001-00 | 100 | 1999X | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1448 | 285-0519-00 |  |  | $0.047 \mu \mathrm{~F}$ | MT | 400 V |  |
| C1450 | 285-0526-00 |  |  | $0.1 \mu \mathrm{~F}$ | MT | 400 V |  |
| C1451 | 290-0169-00 |  |  | $400 \mu \mathrm{~F}$ | Elect. | 250 V |  |
| C1452 | 290-0169-00 |  |  | $400 \mu \mathrm{~F}$ | Elect. | 250 V |  |
| C1453 | 285-0572-00 |  |  | $0.1 \mu \mathrm{~F}$ | PTM | 200 V |  |
| C1454 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1458 | 290-0303-00 |  |  | $5 \mu \mathrm{~F}$ | Elect. | 300 V | $+75 \%-10 \%$ |
| C1462 | 285-0519-00 |  |  | $0.047 \mu \mathrm{~F}$ | MT | 400 V |  |
| C1482 | 290-0180-00 |  |  | $300 \mu \mathrm{~F}$ | Elect. | 250 V |  |
| C1488 | 283-0067-00 | 100 | 1999 | $0.001 \mu \mathrm{~F}$ | Cer | 200 V | 10\% |
| C1488 | 283-0001-00 | 2000 |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1498 | 290-0214-00 |  |  | $10 \mu \mathrm{~F}$ | Elect. | 250 V |  |
| C1499 | 290-0214-00 |  |  | $10 \mu \mathrm{~F}$ | Elect. | 250 V |  |
| C1500 | 283-0001-00 |  |  | $0.005 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1501 | 285-0572-00 |  |  | $0.1 \mu \mathrm{~F}$ | PTM | 200 V |  |
| C1507 | 285-0519-00 |  |  | $0.047 \mu \mathrm{~F}$ | MT | 400 V |  |
| C1530 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1540 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1550 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1552A, B, C | 290-0072-00 |  |  | $20 \times 20 \times 40 \mu \mathrm{~F}$ | Elect. | 475 V |  |
| C1553 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1556 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1559 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1562 | 290-0012-00 |  |  | $2 \times 40 \mu \mathrm{~F}$ | Elect. | 250 V |  |
| C1563 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| Cl 580 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1582A, B, C | 290-0072-00 |  |  | $20 \times 20 \times 40 \times \mu \mathrm{F}$ | Elect. | 475 V |  |
| C1583 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1586 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1589 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1592 | 290-0012-00 |  |  | $2 \times 40 \mu \mathrm{~F}$ | Elect. | 250 V |  |
| C 1593 | 283-0068-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1602 | 285-0572-00 |  |  | $0.1 \mu \mathrm{~F}$ | PTM | 200 V |  |
| C1604 | 283.0002.00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |
| C1605 | 283-0524-00 |  |  | 750 pF | Cer | 500 V | 5\% |
| C1615 | 283-0524-00 |  |  | 750 pF | Cer | 500 V | 5\% |
| C1616 | 283-0002-00 |  |  | $0.01 \mu \mathrm{~F}$ | Cer | 500 V |  |

Capacitors (cont)

| Ckt. No. | Tektronix <br> Part No. | Serial/Model <br> Eff | No. <br> Disc |  | Description |
| :--- | ---: | :--- | :--- | :--- | :--- |
| C1624 | $285-0572-00$ |  | $0.1 \mu \mathrm{~F}$ | PTM | 200 V |
| C1640 | $281-0525-00$ |  | 470 pF | Cer | 500 V |
| C1650 | $281-0523-00$ |  | 100 pF | Cer | 350 V |



Diodes (cont)

| Ckt. No. | Tektronix Part No. | Seria Eff | No. Dise | Description |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D561 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D562 | *152-0075-00 |  |  | Germanium | Tek Spec |
| D565 | *152-0125-00 |  |  | Tunnel | Selected TD3A |
| D570 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D574 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D578 | *152-0061-00 | 100 | 1999X | Silicon | Tek Spec |
| D581 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D589 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |
| D602 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D604 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D612 | 152-0119-00 |  |  | Zener | 1N969A 0.4 W, $22 \mathrm{~V}, 10 \%$ |
| D614 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D616 | *152-0153-00 |  |  | Silicon | Replaceable by 1N4244 |
| D624 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D627 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D629 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D635 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D640 | *152-0161-00 |  |  | GaAs | Tek Spec |
| D641 | *152-0165-00 |  |  | Silicon | Selected from 1N3579 |
| D675 | 152-0118-00 |  |  | Zener | 1N3033 $1 \mathrm{~W}, 36 \mathrm{~V}, 20 \%$ |
| D677 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D678 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D681 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D690 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D755 | 152-0154-00 |  |  | Tunnel | TD253 10 mA |
| D760 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D761 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D762 | *152-0075-00 |  |  | Germanium | Tek Spec |
| D765 | *152-0125-00 |  |  | Tunnel | Selected TD3A |
| D770 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D774 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D778 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D781 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D788 | *152-0061-00 | X2000 |  | Silicon | Tek Spec |
| D789 | *152-0061-00 | X2000 |  | Silicon | Tek Spec |
| D790 | *152-0061-00 | $\times 2000$ |  | Silicon | Tek Spec |
| D792 | *152-0185-00 | $\times 2000$ |  | Silicon | Replaceable by 1N3605 |
| D796 | *152-0185-00 | 100 | 1999 | Silicon | Replaceable by 1N3605 |
| D796 | 152-0147-00 | 2000 |  | Zener | $1 \mathrm{~N} 971 \mathrm{~B} 0.4 \mathrm{~W}, 27 \mathrm{~V}, 5 \%$ |
| D797 | 152-0147-00 | 100 | 1999X | Zener | 1 N971B $0.4 \mathrm{~W}, 27 \mathrm{~V}, 5 \%$ |
| D799 | *152-0185-00 | 100 | 1999 | Silicon | Replaceable by 1N3605 |
| D799 | *152-0061-00 | 2000 |  | Silicon | Tek Spec |
| D802 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D804 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D812 | 152-0119-00 |  |  | Zener | 1N969A 0.4 W, $22 \mathrm{~V}, 10 \%$ |


| Diodes (cont) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Serial/Model Eff | No. Disc |  | Description |
| D814 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D816 | *152-0153-00 |  |  | Silicon | Replaceable by 1N4244 |
| D824 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D827 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D829 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D835 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D838 | *152-0185-00 | X2000 |  | Silicon | Replaceable by 1N3605 |
| D840 | *152-0161-00 |  |  | GaAs | Tek Spec |
| D841 | *152-0165-00 |  |  | Silicon | Selected from 1N3579 |
| D850 | *152-0061-00 | X2000 |  | Silicon | Tek Spec |
| D852 | *152-0185-00 | X2000 |  | Silicon | Replaceable by 1 N 3605 |
| D856 | 152-0147-00 | X2000 |  | Zener | 1N971B 0.4 W, $27 \mathrm{~V}, 5 \%$ |
| D859 | *152-0061.00 | X2000 |  | Silicon | Tek Spec |
| D875 | 152-0118-00 |  |  | Zener | 1N3033 1 W, $36 \mathrm{~V}, 20 \%$ |
| D877 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D878 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D881 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D890 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D905 | 152-0081-00 |  |  | Tunnel | 1 N 37142.2 mA |
| D1008 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1010 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1013 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1014 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1018 | *152-0075-00 |  |  | Germanium | Tek Spec |
| D1021 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1023 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1024 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1028 | *152-0075-00 |  |  | Germanium | Tek Spec |
| D1042 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1062 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1144 | 152-0022-00 |  |  | Zener | 1M25Z5 I W, $25 \mathrm{~V}, 5 \%$ |
| D1151 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1160 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1182 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D1244 | 152-0022-00 |  |  | Zener | 1M25Z5 $1 \mathrm{~W}, 25 \mathrm{~V}, 5 \%$ |
| D1251 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1260 | *152-0185-00 |  |  | Silicon | Replaceable by 1N3605 |
| D1282 | *152-0061-00 |  |  | Silicon | Tek Spec |
| D1303 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |
| D1322 | 152-0192-00 |  |  | Silicon | 7701-5X Varo |
| D1332 | 152-0192-00 |  |  | Silicon | 7701-5X Varo |
| D1334 | *152-0165-00 |  |  | Silicon | Selected from 1N3579 |
| D1335 | *152-0165-00 |  |  | Silicon | Selected from 1N3579 |
| D1372 | 152-0192-00 |  |  | Silicon | 7701-5X Varo |
| D1379 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |


| Diodes (cont) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Serial/Model Eff | No. Disc |  | Description |
| D1382 | 152-0192-00 |  |  | Silicon | 7701-5X Varo |
| D1412A, B, C, ${ }^{\text {(4) }}$ | 152-0066-00 |  |  | Silicon | 1N3194 |
| D1414 | *152-0107-00 |  |  | Silicon | Replaceable by 1N647 |
| D1416 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |
| D1420 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |
| D1424 | 152-0066-00 | 100 | 1999X | Silicon | 1N3194 |
| D1425 | 152-0066-00 | X2000 |  | Silicon | 1N3194 |
| D1429 | *152-0107-00 | 100 | 1999X | Silicon | Replaceable by 1N647 |
| D1430 | *152-0107-00 |  |  | Silicon | Replaceable by 1N647 |
| D1431 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |
| D1432A,B,C,D (4) | 152-0066-00 |  |  | Silicon | 1N3194 |
| D1433 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |
| D1434 | 152-0066-00 |  |  | Silicon | 1N3194 |
| D1435 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |
| D1436 | 152-0066-00 |  |  | Silicon | 1N3194 |
| D1440 | 152-0066-00 |  |  | Silicon | 1N3194 |
| D1443 | 152-0066-00 | 100 | 1999X | Silicon | 1N3194 |
| D1444 | *152-0107-00 | 100 | 1999X | Silicon | Replaceable by 1N647 |
| D1449 | *152-0107-00 |  |  | Silicon | Replaceable by 1 N647 |
| D1450 | *152-0107-00 |  |  | Silicon | Replaceable by 1N647 |
| D1 451 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1 N647 |
| D1452A,B,C,D (4) | *152-0198-00 |  |  | Silicon | MR-1032A (Motorola) |
| D1453 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1 N647 |
| D1455 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |
| D1464 | *152-0107-00 |  |  | Silicon | Replaceable by 1N647 |
| D1466 | *152-0107-00 | 100 | 1999X | Silicon | Replaceable by 1N647 |
| D1469 | *152-0107-00 | 100 | 1999X | Silicon | Replaceable by 1N647 |
| D1472 | 152-0066-00 | 100 | 1999X | Silicon | 1N3194 |
| D1 482A,B,C,D (4) | 152-0066-00 |  |  | Silicon | 1N3194 |
| D1501 | *152-0107-00 | X2000 |  | Silicon | Replaceable by 1N647 |
| D1515 | *152-0107-00 |  |  | Silicon | Replaceable by 1N647 |
| D1517 | *152-0107-00 | 100 | 1999X | Silicon | Replaceable by 1N647 |
| D1620 | *152-0061-00 |  |  | Silicon | Tek Spec |
|  |  |  |  |  |  |
| FL1 400 | 119-0071-00 | 100 | 1999 | 275 V AC |  |
| FL1 400 | 119-0135-00 | 2000 | 2046 | 275 V AC |  |
| FL1400 | 119-0135-00 | 2047 |  | 275 V AC |  |

## Fuses

10 A 3AG Slo-Blo
5 A 3AG Slo-Blo 0.75 A 3AG Fast-Blo 1.5 A 3AG Fast-Blo

1 A 3AG Fast-Blo 0.75 A 3AG Fast-Blo

## Connectors

| Ckt. No. | Tektronix <br> Part No. | Serial/Model <br> Eff |
| :--- | ---: | :--- |
| N11 | No. |  |
| Disc |  |  |


| L 18 | $* 108-0396-00$ |
| :--- | ---: |
| L 22 | $276-0554-00$ |
| L 40 | $* 119-0069-00$ |
| L 43 | $* 114-0211-00$ |
| L 64 | $* 114-0213-00$ |

Inductors

| L 77 | $* 108-0056-00$ |
| :--- | ---: |
| L 118 | $* 108-0396-00$ |
| L 122 | $276-0554-00$ |
| L 143 | $* 114-0211-00$ |
| L 164 | $* 114-0213-00$ |


| $0.14 \mu \mathrm{H}$ |  |
| :--- | :--- |
| Core, Toroid Ferrite |  |
| Delay Line |  |
| $250-370 \mathrm{nH}$, Var | Core $276-0506-00$ |
| $5-10 \mu \mathrm{H}$, Var | Core $276-0506-00$ |
|  |  |
| $1.2 \mu \mathrm{H}$ |  |
| $0.14 \mu \mathrm{H}$ |  |
| Core, Toroid Ferrite |  |
| $250-370 \mathrm{nH}$, Var | Core $276-0506-00$ |
| $5-10 \mu \mathrm{H}$, Var | Core $276-0506-00$ |
|  |  |
| $1.2 \mu \mathrm{H}$ |  |
| $0.14 \mu \mathrm{H}$ |  |
| Delay Line |  |
| $250-370 \mathrm{nH}$, Var |  |
| $5-10 \mu \mathrm{H}$, Var | Core $276-0506-00$ |
|  |  |
| $1.2 \mu \mathrm{H}$ |  |
| $0.14 \mu \mathrm{H}$ |  |
| $250-370 \mathrm{nH}$, Var |  |
| $5-10 \mu \mathrm{H}$, Var | Core $276-0506-00$ |
| $1.2 \mu \mathrm{H}$ | Core $276-0506-00$ |

Coil, Reed
Core, Ferramic Suppressor
$2.2 \mu \mathrm{H}$
$1.1 \mu \mathrm{H}$
Coil, Reed

Inductors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc | Description |
| :---: | :---: | :---: | :---: | :---: |
| L752 | 276-0507-00 |  |  | Core, Ferramic Suppressor |
| L755 | *108-0147-01 |  |  | $2.2 \mu \mathrm{H}$ |
| L760 | *108-0215-00 |  |  | $1.1 \mu \mathrm{H}$ |
| 11125 | *108-0355-00 |  |  | Coil, Reed |
| L1225 | *108-0355-00 |  |  | Coil, Reed |
| 11346 | *108-0016-00 |  |  | $29 \mu \mathrm{H}$ |
| L1390 | *108-0296-00 |  |  | Beam Rotator |
| 11396 | *108-0016-00 |  |  | $29 \mu \mathrm{H}$ |
| LR44 | *108-0397-00 | 100 | 829 | $1.2 \mu \mathrm{H}$ (wound on a $24 \Omega, 1 / 2 \mathrm{~W}, 5 \%$ resistor) |
| LR44 | *108-0454-00 | 830 |  | $1.1 \mu \mathrm{H}$ (wound on a $24 \Omega, 1 / 2 \mathrm{~W}, 5 \%$ resistor) |
| LR144 | *108-0397-00 | 100 | 829 | $1.2 \mu \mathrm{H}$ (wound on a $24 \Omega, 1 / 2 \mathrm{~W}, 5 \%$ resistor) |
| LR144 | *108-0454-00 | 830 |  | $1.1 \mu \mathrm{H}$ (wound on a $24 \Omega, 1 / 2 \mathrm{~W}, 5 \%$ resistor) |
| LR228 | *108-0397-00 | 100 | 829 | $1.2 \mu \mathrm{H}$ (wound on a $24 \Omega, 1 / 2 \mathrm{~W}, 5 \%$ resistor) |
| LR228 | *108-0454-00 | 830 |  | $1.1 \mu \mathrm{H}$ (wound on a $24 \Omega, 7 / 2 \mathrm{~W}, 5 \%$ resistor) |
| LR428 | *108-0397-00 | 100 | 829 | $1.2 \mu \mathrm{H}$ (wound on a $24 \Omega, 1 / 2 \mathrm{~W}, 5 \%$ resistor) |
| LR428 | *108-0454-00 | 830 |  | $1.1 \mu \mathrm{H}$ (wound on a $24 \Omega, 1 / 2 \mathrm{~W}, 5 \%$ resistor) |

## Transistors

| Q44 | $* 151-0185-00$ |
| :--- | ---: |
| Q54 | $151-0160-00$ |
| Q73 | $151-0190-00$ |
| Q74 | $* 151-0188-01$ |
| Q83 | $151-0190-00$ |

Q123
Q134
Q143
Q144
Q154

Q173
Q174
Q203
Q214
Q224

151-0087-00
151-0190-00
151-0087-00
*151-0185-00
*151-0185-00
*151-0109-00
*151-0185-00
*151-0109-00
*155-0185-00
$151-0160-00$
*151-0109-00
*151-0185-00
*151-0109-00
*155-0185-00

$151-0160-00$
$* 151-0109-00$
$* 151-0185-00$
$* 151-0109-00$
$*$
*155-0185-00
$151-0160-00$
$* 151-0109-00$
$* 151-0185-00$
$* 151-0109-00$
$*$
*155-0185-00
$151-0160-00$
*151-0109-00
*151-0185-00
*151-0109-00

* $155-0185-00$
$151-0160-00$
*151-0185-00
*151-0185-00
*151-0109-00
*151-0185-00
*151-0109-00
*151-0185-00

51-0188-01

151-0190-00
*151-0188-01
*151-0185-00
*151-0185-00
*151-0185-00

Germanium
Germanium
Silicon
Germanium Silicon

| Germanium | Selected from 2N2929 |
| :--- | :--- |
| Silicon | 2N3137 |
| Silicon | 2N3904 |
| Silicon | Replaceable by 2N3251 |
| Silicon | 2N3904 |
|  |  |
| Silicon |  |
| Silicon | 2N1131 |
| Silicon | 2N3904 |
| Germanium | 2N1131 |
| Germanium | Selected from 2N2929 |
|  | Selected from 2N2929 |

Silicon
Germanium Silicon Germanium Silicon

Silicon
Silicon Germanium Germanium Germanium

Selected from 2N2929 Selected from 2N2929 Selected from 2N918 Selected from 2N2929 Selected from 2N918

Selected from 2N2929 2N3137
2N3904
Replaceable by 2 N 325
2N3904

2N1131
2N3904

Selected from 2N2929
Selected from 2N2929

Selected from 2N918 Selected from 2N2929 Selected from 2N918 Selected from 2N2929 2N3137

2N3904
Replaceable by 2 N 3251
Selected from 2N2929
Selected from 2N2929
Selected from 2N2929

Transistors (cont)

| Ckt. No. | Tektronix Part No. | Seri <br> Eff | No. Disc | Description |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q233 | *151-0109-00 |  |  | Silicon | Selected from 2N918 |
| Q244 | 151-0160-00 |  |  | Silicon | 2N3137 |
| Q263 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q264 | *151-0188-01 |  |  | Silicon | Replaceable by 2N3251 |
| Q273 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q274 | 151-0087-00 |  |  | Silicon | 2N1131 |
| Q283 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q284 | 151-0087-00 |  |  | Silicon | 2N1131 |
| Q403 | *151-0185-00 |  |  | Germanium | Selected from 2N2929 |
| Q414 | *151-0185-00 |  |  | Germanium | Selected from 2N2929 |
| Q424 | *151-0185-00 |  |  | Germanium | Selected from 2N2929 |
| Q433 | *151-0109-00 |  |  | Silicon | Selected from 2N918 |
| Q444 | 151-0160-00 |  |  | Silicon | 2N3137 |
| Q463 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q464 | *151-0188-01 |  |  | Silicon | Replaceable by 2N3251 |
| Q544 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q554 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q563 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q564 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q573 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q605 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q615 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q619 | *151-0154-00 |  |  | Silicon | Replaceable by 2N2924 |
| Q643 | *151-0188-01 |  |  | Silicon | Replaceable by 2N3251 |
| Q744 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q754 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q763 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q764 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q773 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q779 | *151-0188-01 | 100 | 1999X | Silicon | Replaceable by 2N3251 |
| Q793 | *151-0188-01 | 100 | 1999X | Silicon | Replaceable by 2 N 3251 |
| Q794 | 151-0190-00 | X2000 |  | Silicon | 2N3904 |
| Q805 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q815 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q819 | *151-0154-00 |  |  | Silicon | Replaceable by 2 N 2924 |
| Q843 | *151-0188-01 |  |  | Silicon | Replaceable by 2 N3251 |
| Q854 | 151-0190-00 | X2000 |  | Silicon | 2N3904 |
| Q908 | 151-0150-00 |  |  | Silicon | 2N3440 |
| Q924 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q933 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q1004 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q1015 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q1025 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q1033 | 151-0190-00 |  |  | Silicon | 2N3904 |
| Q1135 | *151-0121-00 |  |  | Silicon | Selected from 2N3118 |

Transistors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc | Description |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q1145 | *151-0096-00 |  |  | Silicon | Selected from 2N1893 |
| Q1154 | 151-0063-00 | 100 | 1999 | Germanium | 2N2207 |
| Q1154 | *151-0133-00 | 2000 |  | Silicon | Selected from 2N3251 |
| Q1164 | 151-0063-00 | 100 | 1999 | Germanium | 2N2207 |
| Q1164 | *151-0133-00 | 2000 |  | Silicon | Selected from 2N3251 |
| Q1235 | *151-0121-00 |  |  | Silicon | Selected from 2N3118 |
| Q1245 | *151-0096-00 |  |  | Silicon | Selected from 2N1893 |
| Q1254 | 151-0063-00 | 100 | 1999 | Germanium | 2N2207 |
| Q1254 | *151-0133-00 | 2000 |  | Silicon | Selected from 2N3251 |
| Q1264 | 151-0063-00 | 100 | 1999 | Germanium | 2N2207 |
| Q1264 | *151-0133-00 | 2000 |  | Silicon | Selected from 2N3251 |
| Q1334 | *151-0192-00 |  |  | Silicon | Replaceable by MPS 6521 |
| Q1414 | *151-0096-00 |  |  | Silicon | Selected from 2N1893 |
| Q1424 | 151-0188-00 |  |  | Silicon | 2N3906 |
| Q1427 | *151-0158-00 | 100 | 1999 | Germanium | Replaceable by DTG 2400 |
| Q1427 | 151-0218-00 | 2000 |  | Silicon | 2N4348 |
| Q1434 | *151-0136-00 |  |  | Silicon | Replaceable by 2 N 3053 |
| Q1443 | *151-0096-00 |  |  | Silicon | Selected from 2N1893 |
| Q1444 | *151-0149-00 |  |  | Silicon | Selected from 2N3441 |
| Q1447 | *151-0158-00 | 100 | 1999 | Germanium | Replaceable by DTG 2400 |
| Q1447 | 151-0218-00 | 2000 |  | Silicon | 2N4348 |
| Q1454 | *151-0136-00 |  |  | Silicon | Replaceable by 2 N3053 |
| Q1463 | *151-0096-00 |  |  | Silicon | Selected from 2N1893 |
| Q1464 | *151-0149-00 |  |  | Silicon | Selected from 2N3441 |
| Q1467 | *151-0158-00 | 100 | 1999 | Germanium | Replaceable by DTG 2400 |
| Q1467 | 151-0218-00 | 2000 |  | Silicon | 2N4348 |
| Q1477 | *151-0158-00 | 100 | 1999 | Germanium | Replaceable by DTG 2400 |
| Q1477 | 151-0218-00 | 2000 |  | Silicon | 2N4348 |
| Q1484 | 151-0151-00 |  |  | Silicon | Replaceable by 2N930 |
| Q1494 | 151-0151-00 |  |  | Silicon | Replaceable by 2N930 |
| Q1504 | *151-0096-00 |  |  | Silicon | Selected from 2N1893 |
| Q1513 | *151-0149-00 |  |  | Silicon | Selected from 2N3441 |
| Q1517 | *151-0158-00 | 100 | 1999 | Germanium | Replaceable by DTG 2400 |
| Q1517 | 151-0218-00 | 2000 |  | Silicon | 2N4348 |

## Resistors

Resistors are fixed, composition, $\pm 10 \%$ unless otherwise indicated.

| R1 | 315-0220-00 |  |  | $22 \Omega$ | 1/4 W |  | 5\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R2 | 315-0101-00 | 100 | 829 | $100 \Omega$ | $1 / 4 W$ |  | 5\% |
| R2 | 308-0301-00 | 830 |  | $10 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R3 | 315-0101-00 | X830 |  | $100 \Omega$ | $1 / 4 W$ |  | 5\% |
| R4 | 305-0682-00 |  |  | $6.8 \mathrm{k} \Omega$ | 2 W |  | . $5 \%$ |


| Resisfors (cont) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Serial/Model Eff | No. Disc | Description |  |  |  |
| R5 | 311-0395-00 |  |  | $2.5 \mathrm{k} \Omega$, Var |  |  |  |
| R6 | 323-0206-00 |  |  | $1.37 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R7 | 308-0329-00 |  |  | $4 \mathrm{k} \Omega$ | 3 W | WW | 2\% |
| R8 | 305-0153-00 |  |  | $15 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R9 | 321-0129-00 |  |  | $215 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R10 | 315-0101-00 | X830 |  | $100 \Omega$ | $1 / 4 W$ |  | 5\% |
| R11 | 315-0471-00 |  |  | $470 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R12 | 311-0433-00 |  |  | $100 \Omega$, Var |  |  |  |
| R13 | 315-0300-00 |  |  | $30 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R14 | 323-0118-00 |  |  | $165 \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R16 | 321-0114-00 |  |  | $150 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R18 | 321-0123-00 |  |  | $187 \Omega$ | 1/8W | Prec | 1\% |
| R20 | 321-0094-00 |  |  | $93.1 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R22 | 321-0093-00 |  |  | $90.9 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R23 | 301-0242-00 |  |  | 2.4 k $\Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R24 | 315-0101-00 |  |  | $100 \Omega$ | 1/4W |  | 5\% |
| R25 | 315-0431-00 |  |  | $430 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R26 | 308-0306-00 |  |  | $3.26 \mathrm{k} \Omega$ | 3 W | WW | 2\% |
| R30 | 315-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R31 | 311-0463-00 |  |  | $5 \mathrm{k} \Omega$, Var |  |  |  |
| R32 | 321-0287-00 | 100 | 829 | $9.53 \mathrm{k} \Omega$ | 1/8W | Prec | 1\% |
| R32 | 315-0223-00 | 830 |  | $22 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R33 | 315-0300-00 |  |  | $30 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R34 | 311-0433-00 |  |  | $100 \Omega$, Var |  |  |  |
| R35 | 315-0471-00 |  |  | $470 \Omega$ | $1 / 4 W$ |  | 5\% |
| R36 | 321-0129-00 |  |  | $215 \Omega$ | 1/8W | Prec | 1\% |
| R37 | 303-0393-00 |  |  | $39 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R39 | 321-0107-00 |  |  | $127 \Omega$ | $1 / \mathrm{W}$ | Prec | 1\% |
| R40 | 315-0432-00 |  |  | $4.3 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R41 | 321-0092-00 |  |  | $88.7 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R42 | 321-0114-00 |  |  | $150 \Omega$ | 1/8W | Prec | 1\% |
| R43 | 321-0143-00 |  |  | $301 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R44 | 316-0220-00 |  |  | $22 \Omega$ | $1 / 4 W$ |  |  |
| R45 | 308-0291-00 |  |  | $2 \mathrm{k} \Omega$ | 3 W | WW | 5\% |
| R46 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |
| R47 | 308-0304-00 |  |  | $1.5 \mathrm{k} \Omega$ | $3 W$ | WW | 1\% |
| R48 | 323-0239-00 |  |  | $3.01 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R49 | 315-0153-00 | 100 | 829 | $15 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R49 | 315-0123-00 | 830 |  | $12 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R50 | 321-0221-00 | 100 | 829 | $1.96 \mathrm{k} \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R50 | 321-0213-00 | 830 |  | $1.62 \mathrm{k} \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R52 | 311-0442-00 |  |  | $250 \Omega$, Var |  |  |  |
| R54 | 311-0433-00 |  |  | $100 \Omega$, Var |  |  |  |
| R55 | 321-0201-00 |  |  | $1.21 \mathrm{k} \Omega$ | 1/8W | Prec | 1\% |
| R56 | 323-0051-00 |  |  | $33.2 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |


| Resistors (cont) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tekłronix Part No. | Serial/Model No. |  |  | Description |  |  |
| R58 | 301-0470-00 |  |  | $47 \Omega$ | 1/2W |  | 5\% |
| R59 | 303-0472-00 |  |  | $4.7 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R60 | 315-0473-00 |  |  | $47 \mathrm{k} \Omega$ | $1 / 4 W$ |  | 5\% |
| R62 | 308-0077-00 |  |  | $1 \mathrm{k} \Omega$ | 3 W | WW |  |
| R64 | *310-0631-00 |  |  | $1 \mathrm{k} \Omega$ | 3 W | Prec | 1\% |
| R65 | 315-0270-00 | 100 | 829 | $27 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R65 | 315-0390-00 | 830 |  | $39 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R66 | 315-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R67 | 323-0341-00 |  |  | $34.8 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R68 | 323-0350-00 | 100 | 829 | $43.2 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R68 | 323-0348-00 | 830 |  | $41.2 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R69 | 311-0326-00 |  |  | $10 \mathrm{k} \Omega$, Var |  |  |  |
| R70 | 315-0221-00 |  |  | $220 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R71 | 305-0152-00 |  |  | $1.5 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R72 | 316-0220-00 |  |  | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R73 | 315-0820-00 |  |  | $82 \Omega$ | 1/4W |  | 5\% |
| R74 | 315-0820-00 |  |  | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R75 | 308-0329-00 |  |  | $4 \mathrm{k} \Omega$ | 3 W | WW | 2\% |
| R77 | 323-0170-00 |  |  | $576 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R78 | 308-0406-00 |  |  | $1.2 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R79 | 315-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  | 5\% |
| R80 | 324-0327-00 |  |  | $24.9 \mathrm{k} \Omega$ | 1 W | Prec | 1\% |
| R81 | 323-0295-00 |  |  | $11.5 \mathrm{k} \Omega$ | 1/2W | Prec | 1\% |
| R82 | 307-0107-00 |  |  | $5.6 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R83 | 302-0473-00 |  |  | $47 \mathrm{k} \Omega$ | $1 / 2 W$ |  |  |
| R84 | 315.0100-00 |  |  | $10 \Omega$ | 1/4W |  | 5\% |
| R85 | 305-0821-00 |  |  | $820 \Omega$ | 2 W |  | 5\% |
| R87 | 305-0391-00 |  |  | $390 \Omega$ | 2 W |  | 5\% |
| R88 | 315-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R89 | 303-0682-00 |  |  | $6.8 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R90 | 308-0253-00 |  |  | $1.32 \mathrm{k} \Omega$ | 3 W | WW | 5\% |
| R91 | 323-0291-00 |  |  | $10.5 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R92 | 324-0327-00 |  |  | $24.9 \mathrm{k} \Omega$ | 1 W | Prec | 1\% |
| R93 | 315-0120-00 |  |  | $12 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R94 | 316-0100-00 |  |  | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R95 | 302-0473-00 |  |  | $47 \mathrm{k} \Omega$ | 1/2 W |  |  |
| R96 | 316-0100-00 |  |  | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R97 | 305-0821-00 |  |  | $820 \Omega$ | 2 W |  | 5\% |
| R99 | 305-0471-00 |  |  | $470 \Omega$ | 2 W |  | 5\% |
| R100 | 315-0820-00 |  |  | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R101 | 315-0220-00 |  |  | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R102 | 316-0474-00 | 100 | 829 | $470 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R102 | 308-0301-00 | 830 |  | $10 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R104 | 305-0682-00 |  |  | $6.8 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R106 | 315-0100-00 |  |  | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |


| Resistors (cont) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Serial/Model Eff | No. Disc | Description |  |  |  |
| R108 | 321-0123-00 |  |  | $187 \Omega$ | 1/8W | Prec | 1\% |
| R109 | 321-0129-00 |  |  | $215 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R110 | 315-0101-00 | X830 |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R113 | 315-0300-00 |  |  | $30 \Omega$ | $1 / 4 W$ |  | 5\% |
| R114 | 323-0118-00 |  |  | $165 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R115 | 303-0393-00 |  |  | $39 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R116 | 321-0114-00 |  |  | $150 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R120 | 321-0094-00 |  |  | $93.1 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R122 | 321-0093-00 |  |  | $90.9 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R125 | 315-0431-00 |  |  | $430 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R133 | 315-0300-00 |  |  | $30 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R136 | 321-0129-00 |  |  | $215 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R139 | 321-0107-00 |  |  | $127 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R140 | 315-0432-00 |  |  | $4.3 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R141 | 321-0092-00 |  |  | $88.7 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R142 | 321-0114-00 |  |  | $150 \Omega$ | 1/8W | Prec | 1\% |
| R143 | 321-0143-00 |  |  | $301 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R144 | 316-0220-00 |  |  | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R145 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R146 | 301-0123-00 |  |  | $12 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R147 | $317.0511-00$ | X830 |  | $510 \Omega$ | 1/8W |  | 5\% |
| R148 | 323-0239-00 |  |  | $3.01 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R150 | 308-0218-00 |  |  | $150 \Omega$ | 3 W | WW | 5\% |
| R151 | 308-0337-00 |  |  | $200 \Omega$ | 7 W | WW | 5\% |
| R153 | 305-0202-00 |  |  | $2 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R156 | 323-0051-00 |  |  | 33.2 ת | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R158 | 301-0470-00 |  |  | $47 \Omega$ | $1 / 2 W$ |  | 5\% |
| R159 | 303-0472-00 |  |  | $4.7 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R160 | 315-0473-00 |  |  | $47 \mathrm{k} \Omega$ | $1 / 4 W$ |  | 5\% |
| R162 | 308-0077-00 |  |  | $1 \mathrm{k} \Omega$ | 3 W | WW |  |
| R164 | *310-0631-00 |  |  | $1 \mathrm{k} \Omega$ | 6 W | Prec | 1\% |
| R165 | 315-0270-00 | 100 | 829 | $27 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R165 | 315-0390-00 | 830 |  | $39 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R166 | 315-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R167 | 305-0822-00 | 100 | 829 | $8.2 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R167 | 305-0432-00 | 830 |  | $4.3 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R170 | 315-0221-00 |  |  | $220 \Omega$ | $1 / 4 W$ |  | 5\% |
| R172 | 316-0220-00 |  |  | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R173 | 315-0820-00 |  |  | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R174 | 315-0820-00 |  |  | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R175 | 308-0329-00 |  |  | $4 \mathrm{k} \Omega$ | 3 W | WW | 2\% |
| R177 | 323-0170-00 |  |  | $576 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R180 | 323-0329-00 |  |  | $26.1 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R182 ${ }^{1}$ | 311-0595-00 |  |  | $10 \mathrm{k} \Omega$, Var |  |  |  |

${ }^{1}$ Furnished as a unit with R1390A,B.

Resistors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc | Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R184 | 323-0329-00 |  |  | 26.1 k $\Omega$ | 1/2W | Prec | 1\% |
| R187 | 302-0100-00 |  |  | $10 \Omega$ | $1 / 2 W$ |  |  |
| R201 | 315-0220-00 |  |  | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R202 | 315-0101-00 | 100 | 829 | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R202 | 308-0301-00 | 830 |  | $10 \mathrm{k} \Omega$ | $3 W$ | WW | 1\% |
| R203 | 315-0101-00 | X830 |  | $100 \Omega$ | $1 / 4 W$ |  | 5\% |
| R204 | 305-0682-00 |  |  | 6.8 k | 2 W |  | 5\% |
| R205 | 311-0395-00 |  |  | 2.5 k $\Omega$, Var |  |  |  |
| R206 | 302-0683-00 |  |  | $68 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R207 | 315-0101-00 | X830 |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R209 | 321-0129-00 |  |  | $215 \Omega$ | 1/8W | Prec | 1\% |
| R211 | 315-0471-00 |  |  | $470 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R212 | $311-0433-00$ |  |  | $100 \Omega$, Var |  |  |  |
| R213 | 315-0300-00 |  |  | $30 \Omega$ | $1 / 4 W$ |  | 5\% |
| R214 | 323-0118-00 |  |  | $165 \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R216 | 321-0122-00 |  |  | $182 \Omega$ | 1/8W | Prec | 1\% |
| R218 | 321-0123-00 |  |  | $187 \Omega$ | 1/8W | Prec | 1\% |
| R222 | 321-0092-00 |  |  | $88.7 \Omega$ | 1/8W | Prec | 1\% |
| R224 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R225 | 321-0114-00 |  |  | $150 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R226 | 321-0143-00 |  |  | $301 \Omega$ | 1/8W | Prec | 1\% |
| R230 | 308-0304-00 |  |  | $1.5 \mathrm{k} \Omega$ | $3 W$ | WW | 1\% |
| R233 | 323-0239-00 |  |  | $3.01 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R234 | 316-0220-00 |  |  | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R235 | 308-0291-00 |  |  | $2 \mathrm{k} \Omega$ | 3 W | WW | 5\% |
| R239 | 315-0153-00 | 100 | 829 | $15 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R239 | 315-0123-00 | 830 |  | $12 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R240 | 321-0221-00 | 100 | 829 | $1.96 \mathrm{k} \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R240 | 321-0213-00 | 830 |  | $1.62 \mathrm{k} \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R242 | 311-0442-00 |  |  | $250 \Omega$, Var |  |  |  |
| R244 | 311-0433-00 |  |  | $100 \Omega$, Var |  |  |  |
| R245 | 321-0201-00 |  |  | $1.21 \mathrm{k} \Omega$ | 1/8W | Prec | 1\% |
| R246 | 323-0051-00 |  |  | $33.2 \Omega$ | 1/2W | Prec | 1\% |
| R248 | 301-0470-00 |  |  | $47 \Omega$ | $1 / 2 W$ |  | 5\% |
| R249 | 303-0472-00 |  |  | $4.7 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R250 | 315-0473-00 |  |  | $47 \mathrm{k} \Omega$ | $1 / 4 W$ |  | 5\% |
| R252 | 308-0077-00 |  |  | $1 \mathrm{k} \Omega$ | 3 W | WW |  |
| R254 | *310-0631-00 |  |  | $1 \mathrm{k} \Omega$ | 6 W | Prec | 1\% |
| R255 | 315-0270-00 | 100 | 829 | $27 \Omega$ | $1 / 4 W$ |  | 5\% |
| R255 | 315-0390-00 | 830 |  | $39 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R256 | 315-0470-00 |  |  | $47 \Omega$ | $1 / 4 W$ |  | 5\% |
| R257 | 323-0341-00 |  |  | $34.8 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R258 | 323-0350-00 | 100 | 829 | $43.2 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R258 | 323-0348-00 | 830 |  | $41.2 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R259 | 311-0326-00 |  |  | $10 \mathrm{k} \Omega$, Var |  |  |  |

## Electrical Parts List-Type 556

Resistors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc |  | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R260 | 315.0221-00 |  |  | $220 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R261 | 305-0152-00 |  |  | $1.5 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R262 | 316-0220-00 |  |  | $22 \Omega$ | $1 / 4 W$ |  |  |
| R263 | 315-0820-00 |  |  | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R264 | 315-0820-00 |  |  | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R265 | 308-0329-00 |  |  | 4 k ת | $3 W$ | WW | 2\% |
| R267 | 323-0170-00 |  |  | $576 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R268 | 308-0406-00 |  |  | $1.2 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R269 | 315-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R270 | 324-0327-00 |  |  | $24.9 \mathrm{k} \Omega$ | 1 W | Prec | $1 \%$ |
| R271 | 323-0295-00 |  |  | $11.5 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R272 | 307-0107-00 |  |  | $5.6 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R273 | 302.0473-00 |  |  | $47 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R274 | $316-0100.00$ |  |  | $10 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R275 | 305-0821-00 |  |  | $820 \Omega$ | 2 W |  | 5\% |
| R277 | 305-0391-00 |  |  | $390 \Omega$ | 2 W |  | 5\% |
| R278 | 315-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  | 5\% |
| R279 | 303-0682-00 |  |  | 6.8 k $\Omega$ | 1 W |  | 5\% |
| R280 | 308-0253-00 |  |  | $1.32 \mathrm{k} \Omega$ | 3 W | WW | 5\% |
| R281 | 323-0291-00 |  |  | $10.5 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R282 | 324-0327-00 |  |  | $24.9 \mathrm{k} \Omega$ | 1 W | Prec | 1\% |
| R283 | 315-0120-00 |  |  | $12 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R284 | 316-0100-00 |  |  | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R285 | 301-0473-00 |  |  | $47 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R286 | 316-0100-00 |  |  | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R287 | 305-0821-00 |  |  | $820 \Omega$ | 2 W |  | 5\% |
| R289 | 303-0511-00 |  |  | $510 \Omega$ | 1 W |  | 5\% |
| R297 | 302-0100-00 |  |  | $10 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R400 | 315-0820-00 |  |  | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R401 | 315-0220-00 |  |  | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R402 | 316-0474-00 | 100 | 829 | $470 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R402 | 308-0301-00 | 830 |  | $10 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R404 | 305-0682-00 |  |  | $6.8 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R407 | 315-0101-00 | X830 |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R409 | 321-0129-00 |  |  | $215 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R413 | 315-0300-00 |  |  | $30 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R414 | $323-0118-00$ |  |  | $165 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R416 | 321-0122-00 |  |  | $182 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R422 | 321-0092-00 |  |  | 88.7 ת | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R423 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R424 | 301-0123-00 |  |  | $12 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R425 | 321-0114-00 |  |  | $150 \Omega$ | 1/8 W | Prec | 1\% |
| R426 | 321-0143-00 |  |  | $301 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R427 | 317-0511-00 | X830 |  | $510 \Omega$ | $1 / 8 \mathrm{~W}$ |  | 5\% |
| R433 | 323-0239-00 |  |  | $3.01 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |

Resistors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc | Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R434 | 316-0220-00 |  |  | $22 \Omega$ | $1 / 4 W$ |  |  |
| R440 | 308-0218-00 |  |  | $150 \Omega$ | 3 W | WW | 5\% |
| R441 | 308-0337-00 |  |  | $200 \Omega$ | 7 W | WW | 5\% |
| R442 | 308-0405-00 |  |  | $70 \Omega$ | 3 W | WW | 5\% |
| R443 | 305-0202-00 |  |  | $2 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R446 | 323-0051-00 |  |  | $33.2 \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R448 | 301-0470-00 |  |  | $47 \Omega$ | $1 / 2 W$ |  | 5\% |
| R449 | 303-0472-00 |  |  | $4.7 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R450 | 315-0473-00 |  |  | $47 \mathrm{k} \Omega$ | $1 / 4 W$ |  | 5\% |
| R452 | 308-0077-00 |  |  | $1 \mathrm{k} \Omega$ | 3 W | WW |  |
| R454 | *310-0631-00 |  |  | $1 \mathrm{k} \Omega$ | 6 W | Prec | 1\% |
| R455 | 315-0270-00 | 100 | 829 | $27 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R455 | 315-0390-00 | 830 |  | $39 \Omega$ | 1/4 W |  | 5\% |
| R456 | 315-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R457 | 305-0822-00 | 100 | 829 | $8.2 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R457 | 305-0432-00 | 830 |  | $4.3 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R460 | 315-0221-00 |  |  | $220 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R462 | 316-0220-00 |  |  | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R463 | 315-0820-00 |  |  | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R464 | 315-0820-00 |  |  | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R465 | 308-0329-00 |  |  | $4 \mathrm{k} \Omega$ | 3 W | WW | 2\% |
| R467 | 323-0170-00 |  |  | $576 \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R500 | 302-0101-00 |  |  | $100 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R501 | 315-0244-00 |  |  | $240 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R502 | 315-0244-00 |  |  | $240 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R504 | 321-1433-01 |  |  | $320 \mathrm{k} \Omega$ | 1/8W | Prec | 1/2\% |
| R505 | 322-1479-01 |  |  | $965 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ | Prec | 1/2\% |
| R508 | 315-0244-00 |  |  | $240 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R510 | 315-0394-00 |  |  | $390 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R511 | 301-0625-00 |  |  | $6.2 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R512 | 315-0105-00 |  |  | $1 M \Omega$ | 1/4W |  | 5\% |
| R514 | 301-0135-00 |  |  | $1.3 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R516 | 315-0334-00 |  |  | $330 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R518 ${ }^{2}$ | 311-0426-00 |  |  | $300 \mathrm{k} \Omega$, |  |  |  |
| R520 | 321-1433-01 |  |  | $320 \mathrm{k} \Omega$ | 1/8W | Prec | 1/2\% |
| R521 | 322-1479-01 |  |  | $965 \mathrm{k} \Omega$ | 1/4W | Prec | 1/2\% |
| R526 | 322-0481-00 |  |  | $1 \mathrm{M} \Omega$ | $1 / 4 \mathrm{~W}$ | Prec | 1\% |
| R528 | 315-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R531 | 315-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R533 | 316.0221-00 |  |  | $220 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R536 | 315-0470-00 |  |  | $47 \Omega$ | $1 / 4 W$ |  | 5\% |
| R538 | 316.0221-00 |  |  | $220 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R541 | 308-0262-00 |  |  | $15 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R543 | 308-0206-00 |  |  | $7.5 \mathrm{k} \Omega$ | 5 W | WW | 5\% |

${ }^{2}$ Furnished as a unit with SW518.

| Resistors (cont) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Serial/Model Eff | No. Disc | Description |  |  |  |  |
| R544 | 301-0202-00 | 100 | 597 | $2 \mathrm{k} \Omega$ | $1 / 2 W$ |  |  | 5\% |
| R544 | 315-0202-00 | 598 |  | $2 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R545 | $311.0442-00$ |  |  | $250 \mathrm{k} \Omega$, Var |  |  |  |  |
| R547 | $316-0104-00$ |  |  | $100 \mathrm{k} \Omega$ | $1 / 4 W$ |  |  |  |
| R548 | 317-0220-00 |  |  | $22 \Omega$ | $1 / 8 \mathrm{~W}$ |  |  | 5\% |
| R549 | 308-0313-00 |  |  | $20 \mathrm{k} \Omega$ | 3 W | WW |  | 1\% |
| R550 | 317-0220-00 |  |  | $22 \Omega$ | $1 / 8 W$ |  |  | 5\% |
| R552 | 315-0100-00 |  |  | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R553 | 321-0047-00 |  |  | 30.1 ת | $1 / 8 \mathrm{~W}$ | Prec |  | 1\% |
| R554 | 308-0320-00 |  |  | $15.6 \mathrm{k} \Omega$ | 3 W | WW |  | 1\% |
| R555 | 323-0350-00 |  |  | $43.2 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec |  | 1\% |
| R556 | 311-0597-00 |  |  | $50 \Omega$, Var |  |  |  |  |
| R557 | 323-0370-00 |  |  | $69.8 \mathrm{k} \Omega$ | 1/2W | Prec |  | 1\% |
| R558 | 323-0140-00 |  |  | $280 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec |  | 1\% |
| R559 | 315-0560-00 |  |  | $56 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R560 | 316-0224-00 |  |  | $220 \mathrm{k} \Omega$ | 1/4W |  |  |  |
| R561 | 323-0326-00 |  |  | $24.3 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec |  | 1\% |
| R562 | 307-0115-00 |  |  | $7.5 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R563 | 321-0245-00 |  |  | $3.48 \mathrm{k} \Omega$ | 1/8W | Prec |  | 1\% |
| R564 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R565 | 301-0393-00 |  |  | $39 \mathrm{k} \Omega$ | 1/2W |  |  | 5\% |
| R566 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R567 | 315-0202-00 |  |  | $2 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R568 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R569 | 315-0103-00 |  |  | $10 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R570 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R571 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R572 | 301-0753-00 | 100 | 1999 | $75 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |
| R572 | 301-0623-00 | 2000 |  | $62 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |
| R574 | 301-0133-00 |  |  | $13 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |
| R575 | 316.0101.00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |  |
| R576 | 301-0474-00 |  |  | $470 \mathrm{k} \Omega$ | $1 / 2 W$ |  |  | 5\% |
| R577 | 301-0163-00 |  |  | $16 \mathrm{k} \Omega$ | $1 / 2 W$ |  |  | 5\% |
| R578 | 316.0101.00 | 100 | 1999 | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R578 | 303-0243-00 | 2000 |  | $24 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R579 | 302-0104-00 | 100 | 1999 | $100 \mathrm{k} \Omega$ | 1/2W |  |  |  |
| R579 | 303-0513-00 | 2000 |  | $51 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R580 | 315-0561-00 |  |  | $560 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R581 | *310-0577-00 |  |  | $14 \mathrm{k} \Omega$ | 3 W | ped $7 \mathrm{k} \Omega$ ) | Prec | 1\% |
| R582 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R583 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |  |
| R584 | 303-0243-00 | 100 | 1999 | $24 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R584 | 315-0201-00 | 2000 |  | $200 \Omega$ | 1/4W |  |  | 5\% |
| R585 | 303-0513-00 | 100 | 1999 | $51 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R585 | 315-0242-00 | 2000 |  | $2.4 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |

Resistors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc | Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R586 | 323-0318-00 |  |  | $20 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R587 | 323-0419-00 |  |  | 226 k , | $1 / 2 W$ | Prec | 1\% |
| R588 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R589 | 316-0101-00 | 100 | 1999 | $100 \Omega$ | $1 / 4 W$ |  |  |
| R589 | 308-0432-00 | 2000 |  | $30 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R590 | 316-0101-00 | 100 | 1999X | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R591 | 316-0472-00 | 100 | 1999X | $4.7 \mathrm{k} \Omega$ | $1 / 4 W$ |  |  |
| R600 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 W$ |  |  |
| R602 | 303-0513-00 |  |  | $51 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R604 | 301-0303-00 |  |  | $30 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R605 | 301-0912-00 |  |  | $9.1 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R607 | 302-0103-00 |  |  | $10 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R610 | 301-0393-00 |  |  | $39 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R611 | 302-0471-00 |  |  | $470 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R613 | 301-0752-00 |  |  | $7.5 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R614 | 302-0152-00 |  |  | $1.5 \mathrm{k} \Omega$ | 1/2W |  |  |
| R616 | 301-0203-00 |  |  | $20 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R617 | 301-0274-00 |  |  | $270 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R618 | 315-0203-00 |  |  | $20 \mathrm{k} \Omega$ | $1 / 4 W$ |  | 5\% |
| R619 | 315-0120-00 |  |  | $12 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R621 | 302-0221-00 |  |  | $220 \Omega$ | 1/2W |  |  |
| R622 | 316-0226-00 |  |  | $22 \mathrm{M} \Omega$ | $1 / 4 W$ |  |  |
| R623 | 301-0183-00 |  |  | $18 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R624 | 315-0394-00 |  |  | 390 k ת | $1 / 4 W$ |  | 5\% |
| R625 | 324-0339-00 |  |  | $33.2 \mathrm{k} \Omega$ | 1 W | Prec | 1\% |
| R627 | 308-0268-00 |  |  | $22 \mathrm{k} \Omega$ | 5 W | WW | 1\% |
| R629 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |
| R631 | 323-0368-00 |  |  | $66.5 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R632 | 323-0399-00 |  |  | $140 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R634 | 323-0275-00 |  |  | $7.15 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R635 | 302-0562-00 |  |  | $5.6 \mathrm{k} \Omega$ | 1/2W |  |  |
| R636 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |
| R637 | 301-0754-00 |  |  | $750 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R639 | 301-0226-00 |  |  | $22 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R640 | 315-0202-00 |  |  | $2 \mathrm{k} \Omega$ | $1 / 4 W$ |  | 5\% |
| R641 | 303-0823-00 |  |  | $82 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R643 | 316-0272-00 |  |  | $2.7 \mathrm{k} \Omega$ | $1 / 4 W$ |  |  |
| R645 | 305-0243-00 |  |  | $24 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R647 | 316-0153-00 |  |  | $15 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R648 | 316-0122-00 |  |  | $1.2 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R660A |  |  |  | $7 \mathrm{M} \Omega$ | 1/2W |  | 1\% |
| R660B $\}$ | *312-0641-00 | 100 | 599 | $2.8 \mathrm{M} \Omega$ | $1 / 2 W$ |  | 1\% |
| R660C |  |  |  | $1.4 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 1\% |


${ }^{3}$ Furnished as a unit with SW662.

Resistors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc |  | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R712 | 315-0105-00 |  |  | $1 M \Omega$ | $1 / 4 W$ |  | 5\% |
| R714 | 301-0135-00 |  |  | $1.3 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R716 | 315-0334-00 |  |  | $330 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R718 ${ }^{4}$ | 311-0426-00 |  |  | $300 \mathrm{k} \Omega$, Var |  |  |  |
| R720 | 321-1433-01 |  |  | $320 \mathrm{k} \Omega$ | 1/8W | Prec | 1/2\% |
| R721 | 322-1479-01 |  |  | 965 k | $1 / 4 W$ | Prec | 1/2\% |
| R726 | 322-0481-00 |  |  | $1 \mathrm{M} \Omega$ | $1 / 4 W$ | Prec | 1\% |
| R728 | 315-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R731 | 315-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R733 | 316-0221-00 |  |  | $220 \Omega$ | $1 / 4 W$ |  |  |
| R736 | 315-0470-00 |  |  | $47 \Omega$ | $1 / 4 W$ |  | 5\% |
| R738 | 316-0221-00 |  |  | $220 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R741 | 308-0262-00 |  |  | 15 k ת | 5 W | WW | 5\% |
| R743 | 308-0206-00 |  |  | $7.5 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R744 | 301-0202-00 | 100 | 597 | $2 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R744 | 315-0202-00 | 598 |  | $2 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R745 | 311-0442-00 |  |  | $250 \Omega$, Var |  |  |  |
| R747 | 316-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R748 | 317-0220-00 |  |  | $22 \Omega$ | 1/8W |  | 5\% |
| R749 | 308-0313-00 |  |  | $20 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R750 | 317-0220-00 |  |  | $22 \Omega$ | 1/8W |  | 5\% |
| R752 | 315-0100-00 |  |  | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R753 | 321-0047-00 |  |  | 30.1 ת | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R754 | 308-0320-00 |  |  | $15.6 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R755 | 323-0350-00 |  |  | $43.2 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R756 | 311-0597-00 |  |  | $50 \Omega$, Var |  |  |  |
| R757 | 323-0370-00 |  |  | 69.8 k $\Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R758 | 323-01 40-00 |  |  | $280 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R759 | 315-0560-00 |  |  | $56 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R760 | 316-0224-00 |  |  | $220 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R761 | 323-0326-00 |  |  | $24.3 \mathrm{k} \Omega$ | 1/2W | Prec | 1\% |
| R762 | 307-0115-00 |  |  | $7.5 \Omega$ | $1 / 4 W$ |  | 5\% |
| R763 | 321-0245-00 |  |  | $3.48 \mathrm{k} \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R764 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |
| R765 | 301-0393-00 |  |  | $39 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R766 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |
| R767 | 315-0202-00 |  |  | $2 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R768 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R769 | 315-0103-00 |  |  | $10 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R770 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R771 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |
| R772 | 301-0753-00 | 100 | 1999 | $75 \mathrm{k} \boldsymbol{\Omega}$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R772 | 301-0623-00 | 2000 |  | $62 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R774 | 301-0133-00 |  |  | 13 k , | $1 / 2 \mathrm{~W}$ |  | 5\% |

[^2]| Resistors (cont) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Serial/Model <br> Eff | No. Disc | Description |  |  |  |  |
| R775 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R776 | 301-0474-00 |  |  | $470 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |
| R777 | 301-0163-00 |  |  | $16 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |
| R778 | 302-0104-00 | 100 | 1999 | $100 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |  |
| R778 | 303-0243-00 | 2000 |  | $24 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R779 | 302-0102-00 | 100 | 1999 | $1 \mathrm{k} \Omega$ | 1/2W |  |  |  |
| R779 | 303-0513-00 | 2000 |  | $51 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R780 | 315-0561-00 |  |  | $560 \Omega$ | $1 / 4 W$ |  |  | 5\% |
| R781 | *310-0577-00 |  |  | $14 \mathrm{k} \Omega$ | 3 W | ed $7 \mathrm{k} \Omega$ ) | Prec | 1\% |
| R782 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R783 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |  |
| R784 | 303-0243-00 | 100 | 1999 | $24 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R784 | 315-0201-00 | 2000 |  | $200 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R785 | 303-0513-00 | 100 | 1999 | $51 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R785 | 315-0242-00 | 2000 |  | $2.4 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R786 | 323-0318-00 |  |  | $20 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec |  | 1\% |
| R787 | 323-0419-00 |  |  | 226 k $\Omega$ | $1 / 2 \mathrm{~W}$ | Prec |  | 1\% |
| R788 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R789 | 316-0101-00 | 100 | 1999 | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R789A | 301-0224-00 | 2000 |  | $220 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |
| R789B | 308-0432-00 | 2000 |  | $30 \mathrm{k} \Omega$ | 3 W | WW |  | 1\% |
| R790 | 316-0101-00 | 100 | 1999 | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R790 | 315-0152-00 | 2000 |  | $1.5 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R791 | 316-0472-00 | 100 | 1999 | $4.7 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R791 | 323-0362-00 | 2000 |  | $57.6 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec |  | 1\% |
| R792 | 301-0102-00 | 100 | 1999 | $1 \mathrm{k} \Omega$ | 1/2W |  |  | 5\% |
| R792 | 322-0289-00 | 2000 |  | $10 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ | Prec |  | 1\% |
| R794 | 305-0103-00 | 100 | 1999 | $10 \mathrm{k} \Omega$ | 2 W |  |  | 5\% |
| R794 | 323-0327-00 | 2000 |  | $24.9 \mathrm{k} \Omega$ | 1/2W | Prec |  | 1\% |
| R795 | 303-0203-00 | 100 | 1999 | $20 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R795 | 307-0106-00 | 2000 |  | $4.7 \Omega$ | $1 / 4 W$ |  |  | 5\% |
| R796 ${ }^{5}$ | 311-0596-00 | 100 | 1999 | $10 \mathrm{k} \Omega$, Var |  |  |  |  |
| R796 | 301-0184-00 | 2000 |  | $180 \mathrm{k} \Omega$ | 1/2W |  |  | 5\% |
| R797 | 315-0302-00 | 100 | 1999 | $3 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R797 | 321-0318-00 | 2000 |  | $20 \mathrm{k} \Omega$ | $1 / 8 \mathrm{~W}$ | Prec |  | 1\% |
| R798 | 301-0105-00 | 100 | 1999 | $1 \mathrm{M} \Omega$ | 1/2W |  |  | 5\% |
| R798 | 308-0313-00 | 2000 |  | $20 \mathrm{k} \Omega$ | 3 W | WW |  | 1\% |
| R799 | 315-0114-00 | 100 | 1999 | $110 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |
| R799 | 316-0101-00 | 2000 |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R800 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |  |
| R802 | 303-0513-00 |  |  | $51 \mathrm{k} \Omega$ | 1 W |  |  | 5\% |
| R804 | 301-0303-00 |  |  | $30 \mathrm{k} \Omega$ | $1 / 2 W$ |  |  | 5\% |
| R805 | 301-0912-00 |  |  | $9.1 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |

${ }^{5}$ Furnished as a unit with R1394.

Resistors (cont)

| Ckt. No. | Tektronix Part No. | Seria Eff | No. Disc |  | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R807 | 302-0103-00 |  |  | $10 \mathrm{k} \Omega$ | 1/2W |  |  |
| R810 | 301-0393-00 |  |  | $39 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R811 | 302-0471-00 |  |  | $470 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R813 | 301-0752-00 |  |  | $7.5 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R814 | 302-0152-00 |  |  | $1.5 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R816 | 301-0203-00 |  |  | $20 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R817 | 301-0274-00 |  |  | $270 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R818 | 315-0203-00 |  |  | $20 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R819 | 315-0120-00 |  |  | $12 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R821 | 302-0221-00 |  |  | $220 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R822 | 316-0226-00 |  |  | $22 \mathrm{M} \Omega$ | 1/4W |  |  |
| R823 | 301-0183-00 |  |  | $18 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R824 | 315-0394-00 |  |  | $390 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R825 | 324-0339-00 |  |  | $33.2 \mathrm{k} \Omega$ | 1 W | Prec | 1\% |
| R827 | 308-0268-00 |  |  | $22 \mathrm{k} \Omega$ | 5 W | WW | 1\% |
| R829 | 316-0101-00 |  |  | $100 \Omega$ | 1/4W |  |  |
| R831 | 323-0368-00 |  |  | $66.5 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R832 | 323-0399-00 |  |  | $140 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R833 ${ }^{8}$ | 311-0596-00 | X2000 |  | 10 k , Var |  |  |  |
| R834 | 323-0275-00 |  |  | $7.15 \mathrm{k} \Omega$ | 1/2W | Prec | 1\% |
| R835 | 302-0562-00 |  |  | $5.6 \mathrm{k} \Omega$ | 1/2W |  |  |
| R836 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R837 | 301-0754-00 |  |  | $750 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R839 | 301-0226-00 |  |  | $22 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R840 | 315-0202-00 |  |  | $2 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R841 | 303-0823-00 |  |  | 82 k ת | 1 W |  | 5\% |
| R843 | 316-0272-00 |  |  | $2.7 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R845 | 305-0243-00 |  |  | $24 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R847 | 316-0153-00 |  |  | $15 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R848 | 316-0122-00 |  |  | $1.2 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R850 | 315-0152-00 | X2000 |  | $1.5 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R851 | 323-0362-00 | $\times 2000$ |  | 57.6 k | $1 / 2 W$ | Prec | 1\% |
| R852 | 322-0289-00 | X2000 |  | $10 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ | Prec | 1\% |
| R853 ${ }^{7}$ | 311-0596-00 | X2000 |  | $10 \mathrm{k} \Omega$, Var |  |  |  |
| R854 | 323-0327-00 | X2000 |  | $24.9 \mathrm{k} \Omega$ | 1/2W | Prec | 1\% |
| R855 | 307-0106-00 | X2000 |  | $4.7 \Omega$ | $1 / 4 W$ |  | 5\% |
| R856 | 301-0184-00 | X2000 |  | $180 \mathrm{k} \Omega$ | $1 / 2 W$ |  | 5\% |
| R857 | 321-0318-00 | $\times 2000$ |  | $20 \mathrm{k} \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R858 | 308-0313-00 | X2000 |  | $20 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R859 | 316-0101-00 | X2000 |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R860A |  |  |  | $7 \mathrm{M} \Omega$ | 1/2W |  | 1\% |
| R860B $\}$ | *312-0641-00 | 100 | 599 | $2.8 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 1\% |
| R860C |  |  |  | $1.4 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 1\% |

${ }^{6}$ Furnished as a unit with R1344.
${ }^{7}$ Furnished as a unit with R1394.

| Resistors (cont) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Serial/Model Eff | No. Disc |  |  | Desc | ription |  |
| $\left.\begin{array}{l}\text { R860A } \\ \text { R860B } \\ \text { R860C } \\ \text { R860G }\end{array}\right\}$ | *312-0641-01 | 600 |  | $\begin{aligned} & 7 M \Omega \\ & 2.8 M \Omega \\ & 1.4 M \Omega \\ & 47 \mathrm{k} \end{aligned}$ | (nominal | $\begin{gathered} 1 / 2 \mathrm{~W} \\ 1 / 2 \mathrm{~W} \\ 1 / 2 \mathrm{~W} \\ \text { value) } \end{gathered}$ | Selected | $\begin{aligned} & 1 \% \\ & 1 \% \\ & 1 \% \end{aligned}$ |
| $\left.\begin{array}{l}\text { R860D } \\ \text { R860E } \\ \text { R860F } \\ \text { R861 } \\ \text { R862 }^{8}\end{array}\right\}$ | $\begin{aligned} & * 312-0640-00 \\ & 311-0600-00 \\ & 311-0391-00 \end{aligned}$ |  |  | $\begin{aligned} & 700 \mathrm{k} \Omega \\ & 280 \mathrm{k} \Omega \\ & 140 \mathrm{k} \Omega \\ & 7.5 \mathrm{k} \Omega, \mathrm{Var} \\ & 150 \mathrm{k} \Omega, \text { Var } \end{aligned}$ |  | $\begin{aligned} & 1 / 2 W \\ & 1 / 2 W \\ & 1 / 2 W \end{aligned}$ |  | $\begin{aligned} & 1 \% \\ & 1 \% \\ & 1 \% \end{aligned}$ |
| R863 <br> R864 <br> R866 <br> R868 <br> R869 | $\begin{aligned} & 302-0105-00 \\ & 302-0104-00 \\ & 316-0101-00 \\ & 304-0473-00 \\ & 304-0473-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \mathrm{M} \Omega \\ & 100 \mathrm{k} \Omega \\ & 100 \Omega \\ & 47 \mathrm{k} \Omega \\ & 47 \mathrm{k} \Omega \end{aligned}$ |  | $\begin{aligned} & 1 / 2 W \\ & 1 / 2 W \\ & 1 / 4 W \\ & 1 W \\ & 1 W \end{aligned}$ |  |  |
| $\begin{aligned} & \text { R870 } \\ & \text { R873 } \\ & \text { R875 } \\ & \text { R876 } \\ & \text { R877 } \end{aligned}$ | $\begin{aligned} & 316-0101-00 \\ & 316-0101-00 \\ & 301-0155-00 \\ & 302-0102-00 \\ & 303-0183-00 \end{aligned}$ |  |  | $\begin{aligned} & 100 \Omega \\ & 100 \Omega \\ & 1.5 \mathrm{M} \Omega \\ & 1 \mathrm{k} \Omega \\ & 18 \mathrm{k} \Omega \end{aligned}$ |  | $\begin{aligned} & 1 / 4 W \\ & 1 / 4 W \\ & 1 / 2 W \\ & 1 / 2 W \\ & 1 W \end{aligned}$ |  | $5 \%$ $5 \%$ |
| R878 <br> R879 <br> R881 <br> R882 <br> R883 | $\begin{aligned} & 311-0011-00 \\ & 305-0363-00 \\ & 323-0356-00 \\ & 323-0356-00 \\ & 323-0352-00 \end{aligned}$ |  |  | $\begin{aligned} & 5 \mathrm{k} \Omega, \mathrm{Var} \\ & 36 \mathrm{k} \Omega \\ & 49.9 \mathrm{k} \Omega \\ & 49.9 \mathrm{k} \Omega \\ & 45.3 \mathrm{k} \Omega \end{aligned}$ |  | $\begin{aligned} & 2 W \\ & 1 / 2 W \\ & 1 / 2 W \\ & 1 / 2 W \end{aligned}$ | Prec <br> Prec <br> Prec | $\begin{aligned} & 5 \% \\ & 1 \% \\ & 1 \% \\ & 1 \% \end{aligned}$ |
| $\begin{aligned} & \text { R884 } \\ & \text { R885 } \\ & \text { R886 } \\ & \text { R887 } \\ & \text { R888 } \end{aligned}$ | $\begin{aligned} & 311-0510-00 \\ & 321-0192-00 \\ & 301-0272-00 \\ & 306-0683-00 \\ & 302-0104-00 \end{aligned}$ |  |  | $\begin{aligned} & 10 \mathrm{k} \Omega, \text { Var } \\ & 976 \Omega \\ & 2.7 \mathrm{k} \Omega \\ & 68 \mathrm{k} \Omega \\ & 100 \mathrm{k} \Omega \end{aligned}$ |  | $\begin{aligned} & 1 / 8 W \\ & 1 / 2 W \\ & 2 W \\ & 1 / 2 W \end{aligned}$ | Prec | $\begin{aligned} & 1 \% \\ & 5 \% \end{aligned}$ |
| $\begin{aligned} & \text { R889 } \\ & \text { R890 } \\ & \text { R892 } \\ & \text { R894 } \\ & \text { R896 } \end{aligned}$ | $\begin{aligned} & 316-0101-00 \\ & 304-0273-00 \\ & 302-0104-00 \\ & 302-0101-00 \\ & 302-0101-00 \end{aligned}$ |  |  | $\begin{aligned} & 100 \Omega \\ & 27 \mathrm{k} \Omega \\ & 100 \mathrm{k} \Omega \\ & 100 \Omega \\ & 100 \Omega \end{aligned}$ |  | $\begin{aligned} & 1 / 4 W \\ & 1 W \\ & 1 / 2 W \\ & 1 / 2 W \\ & 1 / 2 W \end{aligned}$ |  |  |
| $\begin{aligned} & \text { R897 } \\ & \text { R900 } \\ & \text { R901 } \\ & \text { R902 } \\ & \text { R903 } \end{aligned}$ | $\begin{aligned} & 316-0101-00 \\ & 316-0101-00 \\ & 301-0102-00 \\ & 315-0471-00 \\ & 308-0321-00 \end{aligned}$ |  |  | $\begin{aligned} & 100 \Omega \\ & 100 \Omega \\ & 1 \mathrm{k} \Omega \\ & 470 \Omega \\ & 24.4 \mathrm{k} \Omega \end{aligned}$ |  | $\begin{aligned} & 1 / 4 W \\ & 1 / 4 W \\ & 1 / 2 W \\ & 1 / 4 W \\ & 5 W \end{aligned}$ | WW | $\begin{aligned} & 5 \% \\ & 5 \% \\ & 1 \% \end{aligned}$ |
| $\begin{aligned} & \text { R904 } \\ & \text { R905 } \\ & \text { R906 } \\ & \text { R907 } \\ & \text { R908 } \end{aligned}$ | $\begin{aligned} & 301-0391-00 \\ & 316-0101-00 \\ & 301-0102-00 \\ & 315-0471-00 \\ & 305-0303-00 \end{aligned}$ |  |  | $\begin{aligned} & 390 \Omega \\ & 100 \Omega \\ & 1 \mathrm{k} \Omega \\ & 470 \Omega \\ & 30 \mathrm{k} \Omega \end{aligned}$ |  | $\begin{aligned} & 1 / 2 W \\ & 1 / 4 W \\ & 1 / 2 W \\ & 1 / 4 W \\ & 2 W \end{aligned}$ |  | $5 \%$ $5 \%$ $5 \%$ $5 \%$ |

${ }^{8}$ Furnished as a unit with SW862.

Resistors (cont)


Resistors (cont)

| Ckt. No. | Tektronix Part No. |  | No. Disc |  | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1054 | 306-0332-00 |  |  | $3.3 \mathrm{k} \Omega$ | 2 W |  |  |
| R1060 | 316-0472-00 |  |  | $4.7 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1061 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1062 | 321-0258-00 |  |  | $4.75 \mathrm{k} \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R1063 | 323-0370-00 |  |  | $69.8 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1065 | 316-0185-00 |  |  | 1.8 Ma | $1 / 4 \mathrm{~W}$ |  |  |
| R1068 | 316-0105-00 |  |  | $1 \mathrm{M} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1071 | 315-0474-00 |  |  | $470 \mathrm{k} \Omega$ | $1 / 4 W$ |  | 5\% |
| R1072 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1074 | 306-0332-00 |  |  | $3.3 \mathrm{k} \Omega$ | 2 W |  |  |
| R1100B | 323-0611-00 |  |  | $900 \mathrm{k} \Omega$ | 1/2W | Prec | 1\% |
| R1100D | 323-0610-00 |  |  | $111 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1102 | 323-0481-00 |  |  | $1 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1103 | 316-0102-00 |  |  | $1 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1105 | 315-0201-00 |  |  | $200 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1106 | 306-0333-00 |  |  | $33 \mathrm{k} \Omega$ | 2 W |  |  |
| R1107 | 306-0333-00 |  |  | $33 \mathrm{k} \Omega$ | 2 W |  |  |
| R1108 | 311-0599-00 |  |  | $10 \mathrm{k} \Omega$, Var |  |  |  |
| R1110 | 311-0026-00 |  |  | $100 \mathrm{k} \Omega$, Var |  |  |  |
| R1111 | 302-0224-00 |  |  | $220 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1112 | 316-0332-00 |  |  | $3.3 \mathrm{k} \Omega$ | 1/4W |  |  |
| R1113 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |
| R1115 | 305-0183-00 |  |  | $18 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1116 | 323-0356-00 |  |  | $49.9 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1117 | 301-0475-00 |  |  | 4.7 M $\Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1118 | 302-0154-00 |  |  | $150 \mathrm{k} \Omega$ | 1/2W |  |  |
| R1120 | 315-0390-00 |  |  | $39 \Omega$ | $1 / 4 W$ |  | 5\% |
| R1125 | 301-0201-00 |  |  | $200 \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1130 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1131 | 315-0394-00 |  |  | $390 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1132 | 304-0123-00 |  |  | $12 \mathrm{k} \Omega$ | 1 W |  |  |
| R1134 | 315-0390-00 |  |  | $39 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1136A, B | 311-0594-00 |  |  | $2 \times 50 \mathrm{k} \Omega$, Var |  |  |  |
| R1137 | 323-0369-00 |  |  | $68.1 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1139 | 323-0446-00 |  |  | $432 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1141 | 302-0123-00 |  |  | $12 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1142 | 303-0753-00 |  |  | $75 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1144 | 304-0822-00 | 100 | 519 | $8.2 \mathrm{k} \Omega$ | 1 W |  |  |
| R1144 | 308-0286-00 | 520 |  | $8.2 \mathrm{k} \Omega$ | 3 W | WW | 5\% |
| R1146 | 311-0172-00 | 100 | 1999 | $2.5 \mathrm{k} \Omega$, Var |  |  |  |
| R1146 | 311-0629-00 | 2000 |  | $3 \mathrm{k} \Omega$, Var |  |  |  |
| R1147 | 323-0284-00 | 100 | 1999 | $8.87 \mathrm{k} \Omega$, | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1147 | 323-0279-00 | 2000 |  | $7.87 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1149 | 305-0393-00 |  |  | $39 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1151 | 302-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |

Resistors (cont)


| Ckt. No. | Resistors (cont) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tektronix Part No. | $\begin{gathered} \mathrm{Se} \\ \mathrm{Eff} \\ \hline \end{gathered}$ | No. Disc |  | Description |  |  |
| R1216 | 323-0356-00 |  |  | $49.9 \mathrm{k} \Omega$ | 1/2W | Prec | 1\% |
| R1217 | 301-0475-00 |  |  | $4.7 \mathrm{M} \Omega$ | $1 / 2 W$ |  | 5\% |
| R1218 | 302-0154-00 |  |  | $150 \mathrm{k} \Omega$ | 1/2W |  |  |
| R1220 | 315-0390-00 |  |  | $39 \Omega$ | $1 / 4 W$ |  |  |
| R1225 | 301-0201-00 |  |  | $200 \Omega$ | 1/2W |  | 5\% |
| R1230 | 316-0101-00 |  |  | $100 \Omega$ | $1 / 4 W$ |  |  |
| R1231 | 315-0394-00 |  |  | $390 \mathrm{k} \Omega$ | $1 / 4 W$ |  | 5\% |
| R1232 | 304-0123-00 |  |  | $12 \mathrm{k} \Omega$ | 1 W |  |  |
| R1234 | 315-0390-00 |  |  | $39 \Omega$ | $1 / 4 W$ |  | 5\% |
| R1236A, B | 311-0594-00 |  |  | $2 \times 50 \mathrm{k} \Omega$, Var |  |  |  |
| R1237 | 323-0369-00 |  |  | $68.1 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1239 | 323-0446-00 |  |  | $432 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R1241 | 302-0123-00 |  |  | $12 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1242 | 303-0753-00 |  |  | $75 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1244 | 304-0822-00 | 100 | 519 | $8.2 \mathrm{k} \Omega$ | 1 W |  |  |
| R1244 | 308-0286-00 | 520 |  | $8.2 \mathrm{k} \Omega$ | 3 W | WW | 5\% |
| R1246 | 311-0172-00 | 100 | 1999 | $2.5 \mathrm{k} \Omega$, Var |  |  |  |
| R1246 | 311-0629-00 | 2000 |  | $3 \mathrm{k} \Omega$, Var |  |  |  |
| R1247 | 323-0284-00 | 100 | 1999 | $8.87 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1247 | 323-0279-00 | 2000 |  | $7.87 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1249 | 305-0393-00 |  |  | $39 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1251 | 302-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 2 W$ |  |  |
| R1253 | 301-0303-00 |  |  | $30 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1254 | 308-0211-00 |  |  | $12 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1255 | 323-0295-00 |  |  | $11.5 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R1257 | 323-0252-00 |  |  | $4.12 \mathrm{k} \Omega$ | $1 / 2 W$ | Prec | 1\% |
| R1258 | 302-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 2 W$ |  |  |
| R1260 | 302-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 2 W$ |  |  |
| R1262 | 308-0211-00 |  |  | $12 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1263 | 323-0281-00 |  |  | $8.25 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1265 | 301-0122-00 |  |  | $1.2 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R1266 | 323-0162-00 |  |  | $475 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1267 | 311-0598-00 |  |  | $500 \Omega$, Var |  |  |  |
| R1268 | 311-0026-00 |  |  | $100 \mathrm{k} \Omega$, Var |  |  |  |
| R1269 | 302-0473-00 |  |  | $47 \mathrm{k} \Omega$ | 1/2W |  |  |
| R1270 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 W$ |  |  |
| R1272 | *310-0600-00 |  |  | $18 \mathrm{k} \Omega$ | 8 W | ed $4.5 \mathrm{k} \Omega$ | 1\% |
| R1273 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 W$ |  |  |
| R1274 | *310-0601-00 |  |  | $30 \mathrm{k} \Omega$ | 8 W | Prec | 1\% |
| R1276 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 W$ |  |  |
| R1278 | 308-0266-00 |  |  | $5 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1279 | 303-0203-00 |  |  | $20 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1280 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1282 | *310-0611-00 |  |  | $18 \mathrm{k} \Omega$ | 6 W | ed $3.7 \mathrm{k} \Omega$ |  |
| R1283 | 316-0470-00 |  |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |

Resistors (cont)

| Ckt. No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$ No. |  | Descris |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1284 | *310-0601-00 |  | $30 \mathrm{k} \Omega$ | 8 W | Prec | 1\% |
| R1286 | 316-0470-00 |  | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1288 | 306-0224-00 |  | $220 \mathrm{k} \Omega$ | 2 W |  |  |
| R1290 | 302-0104-00 |  | $100 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1291 | 302-0563-00 |  | $56 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1292 | 302-0102-00 |  | $1 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1293 | 316-0470-00 |  | $47 \Omega$ | $1 / 4 W$ |  |  |
| R1295 | 302-0473-00 |  | $47 \mathrm{k} \Omega$ | 1/2W |  |  |
| R1297 | 304-0103-00 |  | $10 \mathrm{k} \Omega$ | 1 W |  |  |
| R1300 | 316-0102-00 |  | $1 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1301 | 306-0101-00 |  | $100 \Omega$ | 2 W |  |  |
| R1302 | 301-0333-00 |  | $33 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1303 | 308-0272-00 | X2000 | $20 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1305 | 306-0271-00 |  | $270 \Omega$ | 2 W |  |  |
| R1307 | 301-0393-00 |  | $39 \mathrm{k} \Omega$ | $1 / 2 W$ |  | 5\% |
| R1308 | 301-0153-00 |  | 15 k , | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1310 | 315-0304-00 |  | $300 \mathrm{k} \Omega$ | $1 / 4 W$ |  | 5\% |
| R1311 | 301-0105-00 |  | $1 \mathrm{M} \Omega$ | 1/2W |  | 5\% |
| R1312 | 304-0154-00 |  | $150 \mathrm{k} \Omega$ | 1 W |  |  |
| R1314 | 302-0684-00 |  | $680 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1315 | 302-0333-00 |  | 33 k ת | 1/2W |  |  |
| R1316 | 302-0333-00 |  | $33 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1317 | 305-0755-00 |  | $7.5 \mathrm{M} \Omega$ | 2 W |  | 5\% |
| R1318 | 305-0755-00 |  | 7.5M | 2 W |  | 5\% |
| R1319 | 311-0415-00 |  | $1 M \Omega$, Var |  |  |  |
| R1320 | 302-0335-00 |  | 3.3M | 1/2W |  |  |
| R1321 | 301-0164-00 |  | $160 \mathrm{k} \Omega$ | $1 / 2 W$ |  | 5\% |
| R1322 | 301-0205-00 |  | $2 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1323 | 317-0107-00 |  | $100 \mathrm{M} \Omega$ | $1 / 8 \mathrm{~W}$ |  | 5\% |
| R1324 | 302-0333-00 |  | $33 \mathrm{k} \Omega$ | 1/2W |  |  |
| R1325 | 316-0336-00 |  | $33 \mathrm{M} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1326 | 316-0336-00 |  | $33 \mathrm{M} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1327 | 316-0224-00 |  | $220 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1328 | 316-0105-00 |  | $1 \mathrm{M} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1329 | 316-0105-00 |  | $1 \mathrm{M} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1330 | 302-0226-00 |  | $22 \mathrm{M} \Omega$ | 1/2W |  |  |
| R1331 | 315-0104-00 |  | $100 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1332 | 311-0034-00 |  | $500 \mathrm{k} \Omega$, Var |  |  |  |
| R1333 | 303-0155-00 |  | $1.5 \mathrm{M} \Omega$ | 1 W |  | 5\% |
| R1334 | 303-0365-00 |  | $3.6 \mathrm{M} \Omega$ | 1 W |  | 5\% |
| R1335 | 303-0365-00 |  | 3.6M $\Omega$ | 1 W |  | 5\% |
| R1336 | 311-0121-00 |  | $5 \mathrm{M} \Omega$, Var |  |  |  |
| R1337 | 303-0245-00 |  | $2.4 \mathrm{M} \Omega$ | 1 W |  | 5\% |
| R1338 | 301-0474-00 |  | $470 \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1339 | 316-0681-00 |  | $680 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |


| Resistors (cont) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Serial/Model Eff | No. Disc | Description |  |  |  |
| R1342 | 311-0026-00 |  |  | $100 \mathrm{k} \Omega$, Var |  |  |  |
| R1344 | 311-0023-00 | 100 | 1999 | $50 \mathrm{k} \Omega$, Var |  |  |  |
| R1344 ${ }^{9}$ | 311-0596-00 | 2000 |  | $50 \mathrm{k} \Omega$, Var |  |  |  |
| R1346 | 301-0512-00 |  |  | $5.1 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1347 | 302-0471-00 |  |  | $470 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1349 | 302-0105-00 |  |  | $1 \mathrm{M} \Omega$ | 1/2 W |  |  |
| R1351 | 306-0101-00 |  |  | $100 \Omega$ | 2 W |  |  |
| R1352 | 301-0333-00 |  |  | $33 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1355 | 306-0271-00 |  |  | $270 \Omega$ | 2 W |  |  |
| R1357 | 301-0393-00 |  |  | $39 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1358 | 301-0153-00 |  |  | $15 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1360 | 315-0304-00 |  |  | $300 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1361 | 301-0105-00 |  |  | $1 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1362 | 304-0154-00 |  |  | $150 \mathrm{k} \Omega$ | 1 W |  |  |
| R1364 | 302-0684-00 |  |  | $680 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1365 | 302-0333-00 |  |  | $33 \mathrm{k} \Omega$ | $1 / 2 W$ |  |  |
| R1366 | 302-0333-00 |  |  | $33 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1367 | 305-0755-00 |  |  | $7.5 \mathrm{M} \Omega$ | 2 W |  | 5\% |
| R1368 | 305-0755-00 |  |  | $7.5 \mathrm{M} \Omega$ | 2 W |  | 5\% |
| R1369 | 311-0415-00 |  |  | $1 \mathrm{M} \Omega$, Var |  |  |  |
| R1370 | 302-0335-00 |  |  | $3.3 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1371 | 301-0164-00 |  |  | $160 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1372 | 301-0205-00 |  |  | $2 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1374 | 302-0333-00 |  |  | $33 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1376 | 316-0102-00 |  |  | $1 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1379 | 308-0272-00 | X2000 |  | $20 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1382 | 311-0034-00 |  |  | $500 \mathrm{k} \Omega$, Var |  |  |  |
| R1383 | 303-0155-00 |  |  | $1.5 \mathrm{M} \Omega$ | 1 W |  | 5\% |
| R1384 | 303-0365-00 |  |  | $3.6 \mathrm{M} \Omega$ | 1 W |  | 5\% |
| R1385 | 303-0365-00 |  |  | $3.6 \mathrm{M} \Omega$ | 1 W |  | 5\% |
| R1386 | 311-0121-00 |  |  | $5 \mathrm{M} \Omega$, Var |  |  |  |
| R1387 | 303-0245-00 |  |  | $2.4 \mathrm{M} \Omega$ | 1 W |  | 5\% |
| R1388 | 301-0474-00 |  |  | $470 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1389 | 316-0681-00 |  |  | $680 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1390A, ${ }^{10}$ | 311-0595-00 |  |  | $2 \times 500 \mathrm{k} \Omega$, Var |  |  |  |
| R1391 | 311-0026-00 |  |  | 100 k , Var |  |  |  |
| R1392 | 323-0356-00 |  |  | $49.9 \mathrm{k} \Omega$ | 1/2W | Prec | 1\% |
| R1393 | 321-0373-00 |  |  | $75 \mathrm{k} \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R1394 ${ }^{11}$ | 311-0596-00 | 100 | 1999 | $50 \mathrm{k} \Omega$, Var |  |  |  |
| R1394 ${ }^{12}$ | 311-0596-00 | 2000 |  | $50 \mathrm{k} \Omega$, Var |  |  |  |

${ }^{9}$ Furnished as a unit with R833.
${ }^{10}$ Furnished as a unit with R182.
${ }^{11}$ Furnished as a unit with R796.
${ }^{12}$ Furnished as a unit with R853.

Resistors (cont)

| Ckt. No. | Tektronix Part No. | Seria <br> Eff | No. Disc |  | Descr |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1396 | 301-0512-00 |  |  | $5.1 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R1397 | 302-0471-00 |  |  | $470 \Omega$ | $1 / 2 W$ |  |  |
| R1399 | 302-0105-00 |  |  | $1 \mathrm{M} \Omega$ | $1 / 2 W$ |  |  |
| R1412 | 305-0183-00 | 100 | 1999 | $18 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1412 | 308-0302-00 | 2000 |  | $20 \mathrm{k} \Omega$ | 5 W | WW | 1\% |
| R1413 | 316-0102-00 | X2000 |  | $1 \mathrm{k} \Omega$ | $1 / 4 W$ |  |  |
| R1414 | 305-0123-00 | 100 | 1999 | $12 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1414 | 308-0302-00 | 2000 |  | $20 \mathrm{k} \Omega$ | 5 W | WW | 1\% |
| R1416 | 308-0302-00 | 100 | 1999 | $20 \mathrm{k} \Omega$ | 5 W | WW | 1\% |
| R1416 | 301-0393-00 | 2000 |  | $39 \mathrm{k} \Omega$ | $1 / 2 W$ |  | 5\% |
| R1418 | 308-0302-00 | 100 | 1999 | $20 \mathrm{k} \Omega$ | 5 W | WW | 1\% |
| R1418 | 301-0224-00 | 2000 |  | $220 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R1420 | 308-0310-00 | 100 | 1999 | $12 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1420 | 315-0473-00 | 2000 |  | $47 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1421 | 315-0330-00 |  |  | $33 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1422 | 308-0402-00 | 100 | 829 | $30 \Omega$ | 5 W | WW | 5\% |
| R1422 | 308-0446-00 | 830 | 1999X | $15 \Omega$ | 5 W | WW | 5\% |
| R1424 | 306-0221-00 | 100 | 829 | $220 \Omega$ | 2 W |  |  |
| R1424 | 306-0181-00 | 830 | 1999 | $180 \Omega$ | 2 W |  |  |
| R1424 | 305-0243-00 | 2000 |  | $24 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1425 | 305-0391-00 | X2000 |  | $390 \Omega$ | 2 W |  | 5\% |
| R1427 | 308-0183-00 | 100 | 829 | $500 \Omega$ | 10 W | WW | 5\% |
| R1427 | 308-0352-00 | 830 |  | $425 \Omega$ | 25 W | WW | 1\% |
| R1429 | 307-0023-00 | 100 | 1999 | $4.7 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1429 | 308-0402-00 | 2000 |  | $30 \Omega$ | 5 W | WW | 5\% |
| R1430 | 306-0563-00 | 100 | 1999 | $56 \mathrm{k} \Omega$ | 2 W |  |  |
| R1430 | 303-0183-00 | 2000 |  | $18 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1431 | 301-0121-00 | X2000 |  | $120 \Omega$ | $1 / 2 W$ |  | 5\% |
| R1432 | 303-0393-00 | X2000 |  | $39 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1433 | 301-0363-00 | 100 | 1999 | $36 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1433 | 303-0273-00 | 2000 |  | $27 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1434 | 303-0473-00 | 100 | 1999X | $47 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1435 | 316-0102-00 |  |  | $1 \mathrm{k} \Omega$ | $1 / 4 W$ |  |  |
| R1436 | 308-0301-00 |  |  | $10 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R1437 | 308-0302-00 |  |  | $20 \mathrm{k} \Omega$ | 5 W | WW | 1\% |
| R1438 | 316-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1439 | 311-0218-00 |  |  | $50 \mathrm{k} \Omega$, Var |  |  |  |
| R1440 | 306-0223-00 | 100 | 1999 | $22 \mathrm{k} \Omega$ | 2 W |  |  |
| R1440 | 305-0223-00 | 2000 |  | $22 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1442 | 308-0266-00 | 100 | 1999 | $5 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1442 | 308-0402-00 | 2000 |  | $30 \Omega$ | 5 W | WW | 5\% |
| R1443 | 306-0221-00 | 100 | 1999 | $220 \Omega$ | 2 W |  |  |
| R1443 | 308-0402-00 | 2000 |  | $30 \Omega$ | 5 W | WW | 5\% |
| R1444 | 308-0401-00 | 100 | 1999X | $20 \Omega$ | 5 W | WW | 5\% |
| R1445 | 308-0404-00 | 100 | 1999 | $250 \Omega$ | 25 W | WW | 5\% |

Resistors (cont)

| Ckt. No. | Tektronix Part No. | Seria Eff | No. Disc | Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1445 | 308-0447-00 | 2000 |  | $260 \Omega$ | 25 W | WW | 1\% |
| R1446 | 308-0404-00 | 100 | 1999 | $250 \Omega$ | 25 W | WW | 5\% |
| R1446 | 308-0447-00 | 2000 |  | $260 \Omega$ | 25 W | WW | 1\% |
| R1447 | 308-0401-00 | 100 | 1999X | $20 \Omega$ | 5 W | WW | 5\% |
| R1448 | 316-0100-00 |  |  | $10 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1449 | 301-0101-00 | X2000 |  | $100 \Omega$ | 1/2W |  | 5\% |
| R1450 | 306-0333-00 | 100 | 1999 | $33 \mathrm{k} \Omega$ | 2 W |  |  |
| R1450 | 305-0273-00 | 2000 |  | $27 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1451 | 315-0121-00 | X2000 |  | $120 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1452 | 303-0393-00 | X2000 |  | $39 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1453 | 301-0303-00 | 100 | 1999 | $30 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R1453 | 303-0243-00 | 2000 |  | $24 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1454 | 303-0473-00 | 100 | 1999X | $47 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1455 | 308-0320-00 |  |  | $15.6 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R1456 | 315-0204-00 |  |  | $200 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1457 | 316-0102-00 | 100 | 1999 | $1 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1457 | 308-0359-00 | 2000 |  | $10.35 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R1458 | 308-0359-00 | 100 | 1999 | $10.35 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R1458 | 316-0102-00 | 2000 |  | $1 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1459 | 311-0218-00 |  |  | $50 \mathrm{k} \Omega$, Var |  |  |  |
| R1461 | 308-0266-00 | 100 | 1999X | $5 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1462 | 316-0100-00 |  |  | $10 \Omega$ | $1 / 4 W$ |  |  |
| R1463 | 306-0223-00 | 100 | 1999 | $22 \mathrm{k} \Omega$ | 2 W |  |  |
| R1463 | 305-0163-00 | 2000 |  | $16 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1464 | 308-0246-00 |  |  | $20 \Omega$ | 10 W | WW | 5\% |
| R1465 | 301-0221-00 | X2000 |  | $220 \Omega$ | 1/2W |  | 5\% |
| R1467 | 308-0240-00 | X2000 |  | $2 \Omega$ | 3 W | WW | 5\% |
| R1469 | 308-0246-00 |  |  | $20 \Omega$ | 10 W | WW | 5\% |
| R1472 | 306-0121-00 | 100 | 1999X | $120 \Omega$ | 2 W |  |  |
| R1474 | 308-0240-00 | X2000 |  | $2 \Omega$ | 3 W | WW | 5\% |
| R1476 | 308-0404-00 |  |  | $250 \Omega$ | 25 W | WW | 5\% |
| R1477 | 308-0404-00 |  |  | $250 \Omega$ | 25 W | WW | 5\% |
| R1478 | 308-0404-00 |  |  | $250 \Omega$ | 25 W | WW | 5\% |
| R1484 | 301-0243-00 |  |  | $24 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1485 | 316-0562-00 | 100 | 1999 | $5.6 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1485 | 315-0103-00 | 2000 |  | $10 \mathrm{k} \Omega$ | 1/4W |  | 5\% |
| R1488 | 301-0103-00 | 100 | 1999 | $10 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R1488 | 301-0153-00 | 2006 |  | $15 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |
| R1490 | 304-0103-00 | 100 | 1999 | $10 \mathrm{k} \Omega$ | 1 W |  |  |
| R1490 | 305-0822-00 | 2000 |  | $8.2 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1494 | 308-0301-00 |  |  | $10 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R1495 | 308-0403-00 | X2000 |  | $8.5 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R1496 | 316-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 4 W$ |  |  |
| R1498 | 311-0218-00 |  |  | $50 \mathrm{k} \Omega$, Var |  |  |  |
| R1500 | 304-0223-00 | 100 | 1999 | $22 \mathrm{k} \Omega$ | 1 W |  |  |

Resistors (cont)

| Ckt. No. | Tekfronix Part No. | $\begin{aligned} & \text { Seri } \\ & \text { Eff } \end{aligned}$ | No. Disc |  | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1500 | 305-0133-00 | 2000 |  | $13 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1501 | 301-0103-00 | 100 | 1999 | $10 \mathrm{k} \Omega$ | 1/2W |  | 5\% |
| R1501 | 303-0622-00 | 2000 |  | $6.2 \mathrm{k} \Omega$ | 1 W |  | 5\% |
| R1504 | 308-0266-00 | 100 | 1999X | $5 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1506 | 306-0333-00 | 100 | 1999 | $33 \mathrm{k} \Omega$ | 2 W |  |  |
| R1506 | 305-0223-00 | 2000 |  | $22 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1507 | 316-0100-00 |  |  | $10 \Omega$ | $1 / 4 W$ |  |  |
| R1513 | 308-0403-00 | 100 | 1999 | $8.5 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R1513 | 301-0101-00 | 2000 |  | $100 \Omega$ | $1 / 2 W$ |  | 5\% |
| R1514 | 308-0313-00 | X2000 |  | $20 \mathrm{k} \Omega$ | 3 W | WW | 1\% |
| R1517 | 308-0399-00 | 100 | 1999 | $10 \Omega$ | 5 W | WW | 5\% |
| R1517 | 308-0446-00 | 2000 |  | $15 \Omega$ | 5 W | WW | 5\% |
| R1519 | 308-0404-00 |  |  | $250 \Omega$ | 25 W | WW | 5\% |
| R1525 | 307-0103-00 |  |  | $2.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1527 | 316-0103-00 |  |  | $10 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1528 | 316-0222-00 |  |  | $2.2 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1529 | 307-0103-00 |  |  | $2.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1533 | 316-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1534 | 308-0269-00 |  |  | $22 \Omega$ | 3 W | WW | 5\% |
| R1535 | 307-0103-00 |  |  | $2.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1536 | 311-0377-00 |  |  | $25 \Omega$, Var |  |  |  |
| R1537 | 316-0103-00 |  |  | $10 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1538 | 316-0222-00 |  |  | $2.2 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1539 | 307-0103-00 |  |  | $2.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1550 | 302-0185-00 |  |  | $1.8 \mathrm{M} \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1552 | 323-0097-00 |  |  | $100 \Omega$ | 1/2W | Prec | 1\% |
| R1555 | 324-0097-00 |  |  | $100 \Omega$ | 1 W | Prec | 1\% |
| R1558 | 323-0097-00 |  |  | $100 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1562 | 323-0097-00 |  |  | $100 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1565 | 307-0103-00 |  |  | $2.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1582 | 323-0097-00 |  |  | $100 \Omega$ | 1/2W | Prec | 1\% |
| R1585 | 324-0097-00 |  |  | $100 \Omega$ | 1 W | Prec | 1\% |
| R1588 | 323-0097-00 |  |  | $100 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1592 | 323-0097-00 |  |  | $100 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1\% |
| R1595 | 307-0103-00 |  |  | $2.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |
| R1601 | 302-0221-00 |  |  | $220 \Omega$ | $1 / 2 W$ |  |  |
| R1602 | 305-0332-00 |  |  | $3.3 \mathrm{k} \Omega$ | 2 W |  | 5\% |
| R1604 | 302-0101-00 |  |  | $100 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1605 | 308-0310-00 |  |  | $12 \mathrm{k} \Omega$ | 5 W | WW | 1\% |
| R1607 | 316-0104-00 |  |  | $100 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1608 | 301-0914-00 |  |  | $910 \mathrm{k} \Omega$ | $1 / 2 W$ |  | 5\% |
| R1615 | 308-0400-00 |  |  | $18 \mathrm{k} \Omega$ | 5 W | WW | 5\% |
| R1616 | 302-0470-00 |  |  | $47 \Omega$ | $1 / 2 W$ |  |  |
| R1617 | 316-0102-00 |  |  | $1 \mathrm{k} \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1618 | 301-0914-00 |  |  | $910 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |


| Resistors (cont) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tekfronix Part No. | Serial/Model Eff | No. Disc | Description |  |  |  |
| R1620 | 302-0103-00 |  |  | $10 \mathrm{k} \Omega$ | 1/2W |  |  |
| R1622 | 302-0470-00 |  |  | $47 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  |
| R1624 | 316-0220-00 |  |  | $22 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  |
| R1626 | 304-0104-00 |  |  | $100 \mathrm{k} \Omega$ | 1 W |  |  |
| R1628 | 311-0365-00 |  |  | $1 \mathrm{k} \Omega$, Var |  |  |  |
| R1630 | 323-0636-00 |  |  | $50 \mathrm{k} \Omega$ | 1/2W | Prec | 1\% |
| R1632 | 323-0709-01 |  |  | $10.048 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/2\% |
| R1633 | 323-0708-01 |  |  | $6.628 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/2\% |
| R1 634 | 323-0707-01 |  |  | $1.782 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/2\% |
| R1635 | 323-0706-01 |  |  | $800 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/2\% |
| R1636 | 323-0705-01 |  |  | $452 \Omega$ | 1/2W | Prec | 1/2\% |
| R1637 | 323-0704-01 |  |  | $146 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/2\% |
| R1638 | 323-0703-01 |  |  | $72.4 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/2\% |
| R1639 | 323-0702-01 |  |  | $43.1 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/2\% |
| R1640 | 323-0701-01 |  |  | $28.6 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/2\% |
| R1645 | 323-0700-01 |  |  | $21.4 \Omega$ | 1/2W | Prec | 1/2\% |
| R1647 | 323-0638-00 |  |  | $50 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/4\% |
| R1650 | 323-0637-00 |  |  | $50 \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | 1/4\% |
| R1654 | *308-0090-00 |  |  | $0.25 \Omega$ | 1 W | WW |  |

## Switches

| Unwired or Wired |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SW105 | 260-0601-00 |  |  | Push-Button | Compensation |
| SW155 | 260-0763-00 |  |  | Push-Button | BEAM LOCATE |
| SW185 | Wired *262-0768-00 | 100 | 1999 | Rotary | UPPER BEAM DISPLAY |
| SW185 | 260-0752-00 | 100 | 1999 | Rotary | UPPER BEAM DISPLAY |
| SW185 | Wired *262-0768-01 | 2000 |  | Rotary | UPPER BEAM DISPLAY |
| SW185 | 260-0752-01 | 2000 |  | Rotary | UPPER BEAM DISPLAY |
| SW205 | 260-0601-00 |  |  | Push-Button | Compensation |
| SW500 |  |  |  | Lever | SOURCE |
| SW505 | Wired *262-0774-00 |  |  | Lever | MODE |
| SW510 | Wired (A Sweep) |  |  | Lever | COUPLING |
| SW515 | (A Sweep) |  |  | Lever | SOURCE |
| SW520) |  |  |  | Lever | SLOPE |
| SW500 | 260-0753-00 |  |  | Lever | SOURCE |
| SW505 | 260-0750-00 |  |  | Lever | MODE |
| SW510 | 260-0754-00 |  |  | Lever | COUPLING |
| SW515 | 260-0749-00 |  |  | Lever | SOURCE |
| SW518 ${ }^{13}$ |  |  |  | Push-Pull | Pull for $\times 10$ Range Increase |
| SW520 | 260-0472-00 |  |  | Lever | SLOPE |
| SW547 | 260-0552-00 |  |  | Reed |  |
| SW620 | 260-0574-01 |  |  | Push-Pull | RESET |


| Ckt. No. | Tektronix Part No. | Switches (cont) |  |  | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Serial/Model Eff | No. Disc |  |  |
| SW625 | 260-0640-00 |  |  | Lever | A MODE |
| SW660 | Wired *262-0766-00 |  |  | Rotary | A TIME/CM |
| SW660 | 260-0756-00 |  |  | Rotary | A TIME/CM |
| SW662 ${ }^{14}$ |  |  |  |  |  |
| SW700 |  |  |  | Lever | SOURCE |
| SW705 |  |  |  | Lever | MODE |
| SW710 | Wired *262-0775-00 <br> (B Sweep) |  |  | Lever | COUPLING |
| SW715 | (B Sweep) |  |  | Lever | SOURCE |
| SW720 |  |  |  | Lever | SLOPE |
| SW700 | 260-0753-00 |  |  | Lever | SOURCE |
| SW705 | 260-0750-00 |  |  | Lever | MODE |
| SW710 | 260-0754-00 |  |  | Lever | COUPLING |
| SW715 | 260-0749-00 |  |  | Lever | SOURCE |
| SW718 ${ }^{15}$ |  |  |  | Push-Pull | Pull for $\times 10$ Range Increase |
| SW720 | 260-0472-00 |  |  | Lever | SLOPE |
| SW747 | 260-0552-00 |  |  | Reed |  |
| SW775 | Wired *262-0769-00 | 100 | 1999 | Rotary | LOWER BEAM DISPLAY |
| SW775 | 260-0751-00 | 100 | 1999 | Rotary | LOWER BEAM DISPLAY |
| SW775 | Wired *262-0769-01 | 2000 |  | Rotary | LOWER BEAM DISPLAY |
| SW775 | 260-0751-01 | 2000 |  | Rotary | LOWER BEAM DISPLAY |
| SW820 | 260-0574-01 |  |  | Push-Button | RESET |
| SW825 | 260-0748-00 |  |  | Lever | B MODE |
| SW860 | Wired *262-0767-00 |  |  | Rotary | B TIME/CM |
| SW860 | 260-0756-00 |  |  | Rotary | B TIME/CM |
| SW862 ${ }^{16}$ |  |  |  |  |  |
| SW1120 | Wired *262-0796-00 | X520 |  | Lever | DISPLAY MAG (upper beam) |
| SW1120 | 260-0755-00 |  |  | Lever | DISPLAY MAG (upper beam) |
| SW1125 | 260-0552-00 |  |  | Reed |  |
| SW1220 | Wired *262-0796-01 | X520 |  | Lever | DISPLAY MAG (lower beam) |
| SW1220 | 260-0755-00 |  |  | Lever | DISPLAY MAG (lower beam) |
| SW1225 | 260-0552-00 |  |  | Reed |  |
| SW1345 | 260-0784-00 |  |  | Toggle | CRT Cath Selector (lower beam) |
| SW1395 | 260-0784-00 |  |  | Toggle | CRT Cath Selector (upper beam) |
| SW1402 | 260-0785-00 |  |  | Toggle | POWER |
| SW1403 ${ }^{17}$ |  |  |  |  |  |
| SW1404 ${ }^{17}$ |  |  |  |  |  |
| SW1630 | Wired *262-0731-00 |  |  | Rotary | AMPLITUDE CALIBRATOR |
| SW1630 | 260-0536-00 |  |  | Rotary | AMPLITUDE CALIBRATOR |
| ${ }^{14}$ Furnished as a unit with R662. |  |  |  |  |  |
| ${ }^{15}$ Furnished as a unit with R718. |  |  |  |  |  |
| ${ }^{16}$ Furnished as a unit with R862. |  |  |  |  |  |
| ${ }^{17}$ See Mech | nical Parts List. Line | ltage Selector Body |  |  |  |

## Thermal Cut-Out

| Ckt. No. | Tektronix <br> Part No. | Eff | Serial/Model |
| :--- | :---: | :---: | :---: |
| TK404 | $260-0618-00$ |  | $140^{\circ} \mathrm{F}$ |

## Transformers

T555
T755
T905
T1301
T1351
T1401

T1401
T1525
T1535
*120-0437-00
*120-0437-00
*120-0434-00
*120-0432-00
*120-0433-00
*120-0431-00
100
1999
Toroid, 2 windings
Toroid, 2 windings
Toroid, 5 turns, bifilar
H.V. Power (lower beam)
H.V. Power (upper beam)
L.V. Power
L.V. Power

Toroid, 6 turns, bifilar
Toroid, 6 turns, bifilar

## Electron Tubes

| V3 | *157-0118-00 | 12AT7 aged |
| :---: | :---: | :---: |
| V64 | 154-0491-00 | 8608 |
| V164 | 154-0491-00 | 8608 |
| V203 | *157-0118-00 | 12AT7 aged |
| V254 | 154-0491-00 | 8608 |
| V454 | 154-0491-00 | 8608 |
| V534 | 154-0187-00 | 6DJ8 |
| V574 | 154-0493-00 | $6 \mathrm{M11}$ |
| V583 | 154-0187-00 | 6DJ8 |
| V625 | 154-0187-00 | 6DJ8 |
| V661 | 154-0040-00 | 12AU6 |
| V673 | 154-0187-00 | 6DJ8 |
| V734 | 154-0187-00 | 6DJ8 |
| V774 | 154-0493-00 | $6 \mathrm{Ml1}$ |
| V783 | 154-0187-00 | 6DJ8 |
| V825 | 154-0187-00 | 6DJ8 |
| V861 | 154-0040-00 | 12AU6 |
| V873 | 154-0187-00 | 6DJ8 |
| V904 | 154-0187-00 | 6DJ8 |
| V1043 | 154-0187-00 | 6DJ8 |
| V1063 | 154-0187-00 | 6DJ8 |
| V1104 | 154-0187-00 | 6DJ8 |
| V1174 | 154-0187-00 | 6DJ8 |
| V1184 | 154-0187-00 | 6DJ8 |
| V1194 | 154-0146-00 | 6197 |
| V1204 | 154-0187-00 | 6DJ8 |
| V1274 | 154-0187-00 | 6DJ8 |
| V1284 | 154-0187-00 | 6DJ8 |

Electron Tubes (cont)

| Ckt. No. | Tektronix Part No. | Serial/Model No. Eff Disc | Description |
| :---: | :---: | :---: | :---: |
| V1294 | 154-0146-00 |  | 6197 |
| V1300 | 154-0494-00 |  | 6GF5 |
| V1322 | 154-0051-00 |  | 5642 |
| V1332 | 154-0051-00 |  | 5642 |
| V1342 | 154-0051-00 |  | 5642 |
| V1350 | 154-0494-00 |  | 6GF5 |
| V1359 | *154-0500-00 |  | T5560-31-1 CRT Standard Phosphor |
| V1482 | 154-0370-00 |  | ZZ1000 |
| V1605 | 154-0493-00 |  | $6 \mathrm{M11}$ |

## INDEX OF MECHANICAL PARTS LIST ILLUSTRATIONS

(Located behind diagrams)
FIG. 1 FRONT \& SWITCHES
FIG. 2 A SWEEP, VERTICAL AMPLIFIER \& HIGH VOLTAGE
FIG. 3 B SWEEP, VERTICAL AMPLIFIER \& HIGH VOLTAGE
FIG. 4 CAPACITOR MOUNTING CHASSIS \& TRANSFORMER
FIG. 5 POWER CHASSIS \& PLUG-IN HOUSING
FIG. 6 FAN MOTOR \& HEAT SINK CHASSIS
FIG. 7 CRT SHIELD \& REAR
FIG. 8 CABINET \& RAILS
FIG. 9 STANDARD ACCESSORIES

## FIGURE AND INDEX NUMBERS

Items in this section are referenced by figure and index numbers to the illustrations which appear on the pullout pages immediately following the Diagrams section of this instruction manual.

## INDENTATION SYSTEM

This mechanical parts list is indented to indicate item relationships. Following is an example of the indentation system used in the Description column.

> Assembly and/or Component Detail Part of Assembly and/or Component mounting hardware for Detail Part Parts of Detail Part mounting hardware for Parts of Detail Part mounting hardware for Assembly and/or Component

Mounting hardware always appears in the same indentation as the item it mounts, while the detail parts are indented to the right. Indented items are part of, and included with, the next higher indentation.

Mounting hardware must be purchased separafely, unless otherwise specified.

## PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix, Inc. Field Office or representative.

Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number, instrument type or number, serial or model number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix, Inc. Field Office or representative will contact you concerning any change in part number.

Change information, if any, is located at the rear of this manual.

## ABBREVIATIONS AND SYMBOLS

For an explanation of the abbreviations and symbols used in this section, please refer to the page immediately preceding the Electrical Parts List in this instruction manual.

## SECTION 8

## MECHANICAL PARTS LIST

FIG. 1 FRONT \& SWITCHES

| Fig. \& Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | $\begin{gathered} \mathrm{Q} \\ \mathrm{t} \\ \mathrm{y} \\ \hline \end{gathered}$ | 12345 Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1-1 | 333-0922-01 | $\begin{aligned} & 100 \\ & 2010 \end{aligned}$ | 2009 | 1 | PANEL, front |
|  | 333-0922-05 |  |  | 1 | PANEL, front |
|  | - |  |  | - | mounting hardware: (not included w/panel) |
| -2-3 | 213-0055-00 |  |  | 4 | SCREW, thread forming, $2-56 \times 3 / 16$ inch, PHS |
|  | 213-0113-00 |  |  | 2 | SCREW, thread forming, $2-32 \times 5 / 16$ inch, RHS |
| -4-5-6-7 | 354-0262-00 |  |  | 1 | RING, light reflector, plate <br> PLATE, light reflector <br> FILTER, light, smokey grey (see fig. 9) <br> FILTER, mesh <br> filter includes: <br> FRAME, rear mesh filter mounting hardware: (not included w/filter) NUT, knurled, $3 / 8-24 \times 9 / 16$ inch |
|  | 386-0212-00 |  |  | 1 |  |
|  | - - . - |  |  | - |  |
|  | 378-0572-00 |  |  | 1 |  |
|  | - -- |  |  | - |  |
| -8 | 426-0273-00 |  |  | 1 |  |
|  | - - - - |  |  | - |  |
| -9 | 210-0424-00 |  |  | 4 |  |
| -10 | 386-1008-00 |  |  | 1 | PLATE, sub-panel, front plate includes: RING, ornamental |
|  | ---- |  |  | - |  |
|  | 354-0282-00 |  |  | 1 |  |
| -11 | 355-0043-00 |  |  | 4 | STUD, graticule (replacement) each stud includes: <br> SCREW, $10-32 \times 3 / 8$ inch, PHS LOCKWASHER, internal, \#10 |
|  | - - -- |  |  | - |  |
|  | 212-0507-00 |  |  | 1 |  |
|  | 210-0010-00 |  |  | 1 |  |
| -12 | 131-0106-01 |  |  | 9 | CONNECTOR, coaxial, 1 contact, BNC |
| -13 | 131-0274-00 |  |  | 1 | CONNECTOR, insulated, 1 contact, BNC |
| -14 | 337-0850-00 |  |  | 1 | GUARD, shielding, gasket, B inside |
|  | ---- |  |  | 4 | mounting hardware: (not included w/guard) |
| -15 | 211-0559-00 |  |  | 4 | SCREW, $6-32 \times 3 / 8$ inch, $100^{\circ}$ csk, FHS |
| -16 | 352-0084-00 |  |  | 6 | HOLDER, neon |
| -17 | 378-0541-00 |  |  | 2 | LENS, neon, clear |
| -18 | 378-0541-01 |  |  | 4 | LENS, neon, green |
| -19 | 200-0609-00 |  |  | 6 | COVER, neon holder |
| -20 | 214-0335-00 |  |  | 1 | BOLT, current loop, $U$ shaped |
|  | ---. - |  |  | - | mounting hardware: (not included w/bolt) |
| -21 | 210-0593-00 |  |  | 2 | NUT, hex., 3-48 x 1/4 inch, current loop |
| -22 | 361-0059-00 |  |  | 1 | SPACER, current loop |
|  | 210-0849-00 |  |  | 2 | WASHER, fiber, $0.110 \mathrm{ID} \times 0.250$ inch OD |
|  | 210-0801-00 |  |  | 2 | WASHER, flat, $0.140 \mathrm{ID} \times 0.281$ inch OD |
|  | 210-0201-00 |  |  | 2 | LUG, solder, \#4 |
|  | 210-0442-00 |  |  | 2 | NUT, hex., 3-48 $\times 3 / 16$ inch |
| -23 | 136-0027-00 |  |  | 1 | SOCKET, light, w/green jewel |

FIG. 1 FRONT \& SWITCHES (cont)

| Fig. \& Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 1-24 | 260-0574-01 |  | 2 | SWITCH, push button-RESET |
|  | - - . . - |  | - | mounting hardware for each: (not included w/switch) |
|  | 354-0055-00 |  | 1 | RING, switch locking, $15 / 32$ ID $\times 23 / 32$ inch OD |
|  | 210-0902-00 |  | 1 | WASHER, flat, $0.470 \mathrm{ID} \times 21 / 32$ inch OD |
|  | 210-0473-00 |  | 1 | NUT, 12 sided, $15 / 32-32 \times 5 / 64$ inch |
| . 25 | 260-0785-00 |  | 1 | SWITCH, toggle-POWER |
|  | - - - . |  | - | mounting hardware: (not included w/switch) |
|  | 354-0055-00 |  | 1 | RING, switch locking, 15/32 $1 \mathrm{D} \times 23 / 32$ inch OD |
|  | 210-0902-00 |  | 1 | WASHER, flat, $0.470 \mathrm{ID} \times 21 / 32$ inch OD |
|  | 210-0473-00 |  | 1 | NUT, 12 sided, $15 / 32-32 \times 5 / 64$ inch |
| -26 | 366-0215-01 |  | 1 | KNOB, charcoal-SOURCE A |
| -27 | 366-0215-01 |  | 1 | KNOB, charcoal-SOURCE A |
| -28 | 366-0215-01 |  | 1 | KNOB, charcoal-COUPLING A |
| -29 | 366-0215-01 |  | 1 | KNOB, charcoal-SLOPE A |
| -30 | 366-0215-01 |  | 1 | KNOB, charcoal-MODE A |
| -31 | 262-0774-00 |  | 1 | SWITCH, wired-TRIGGER BANK A |
|  | - |  | - | switch includes: |
| -32 | 260-0749-00 |  | 1 | SWITCH, unwired-SOURCE A |
| -33 | 260-0753-00 |  | 1 | SWITCH, unwired-SOURCE A |
| -34 | 260-0754-00 |  | 1 | SWITCH, unwired-COUPLING |
| -35 | 260-0472-00 |  | 1 | SWITCH, unwired-SLOPE A |
| -36 | 260-0750-00 |  | 1 | SWITCH, unwired-MODE A |
|  | - - . - |  | - | mounting hardware for each: (not included $\mathrm{w} /$ switch) |
| -37 | 213-0141-00 |  | 10 | SCREW, thread forming, $4-40 \times 1 / 4$ inch, PHS |
| -38 | 407-0211-01 |  | 2 | BRACKET, switch mounting |
| -39 | 670-0433-00 |  | 1 | ASSEMBLY, circuit board |
|  | -- - |  | ; | assembly includes: |
|  | 388-0690-00 |  | 1 | BOARD, circuit |
|  | - - |  | - | board includes: |
| -40 | 131-0214-00 |  | 25 | CONNECTOR, square pin, male |
|  | - -- |  | - | mounting hardware: (not included $\mathrm{w} / \mathrm{switch}$ ) |
| -41 | 210-0586-00 |  | 4 | NUT, keps, $4-40 \times 1 / 4$ inch |
| -42 | 366-0215-01 |  | 1 | KNOB, charcoal-MODE B |
| -43 | 366-0215-01 |  | 1 | KNOB, charcoal--SLOPE B |
| -44 | 366-0215-01 |  | 1 | KNOB, charcoal-COUPLING B |
| -45 | 366-0215-01 |  | 1 | KNOB, charcoal-SOURCE B |
| -46 | 366-0215-01 |  | 1 | KNOB, charcoal-SOURCE B |
| -47 | 262-0775-00 |  | 1 | SWITCH, wired-TRIGGER BANK B |
|  | ---- |  | - | switch includes: |
| -48 | 260-0750-00 |  | 1 | SWITCH, unwired-MODE B |
| -49 | 260-0472-00 |  | 1 | SWITCH, unwired-SLOPE B |
| -50 | 260-0754-00 |  | 1 | SWITCH, unwired-COUPLING B |
| -51 | 260-0753-00 |  | 1 | SWITCH, unwired-SOURCE B |
| -52 | 260-0749-00 |  | 1 | SWITCH, unwired-SOURCE B |
|  | - - - - |  | - | mounting hardware for each: (not included w/switch) |
| -53 | 213-0141-00 |  | 10 | SCREW, thread forming, $4-40 \times 1 / 4$ inch, PHS |
| -54 | 407-0211-02 |  | 2 | BRACKET, switch mounting |

FIG. 1 FRONT \& SWITCHES (cont)

| Fig. \& Index No. | Tektronix Part No. |  | Serial/Model Eff | No. Disc | $\begin{aligned} & Q \\ & \mathrm{t} \\ & \mathrm{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-55 | 670-0434-00 |  |  |  | 1 | ASSEMBLY, circuit board |
|  | - . . - - |  |  |  | - | assembly includes: |
|  | 388-0689-00 |  |  |  | 1 | BOARD, circuit |
|  | - - - |  |  |  |  | board includes: |
| -56 | 131-0214-00 |  |  |  | 25 | CONNECTOR, square pin |
|  | - - . |  |  |  | - | mounting hardware: (not included w/switch) |
| -57 | 210-0586-00 |  |  |  | 4 | NUT, keps, $4-40 \times 1 / 4$ inch |
| -58 | 366-0215-01 |  |  |  | 1 | KNOB, charcoal-B MODE |
| -59 | 260-0748-00 |  |  |  | 1 | SWITCH, unwired-B MODE |
|  | ---- |  |  |  | 2 | mounting hardware: (not included w/switch) |
|  | 210-0586-00 |  |  |  | 2 | NUT, keps, $4-40 \times 1 / 4$ inch |
| -60 | 366-0215-01 |  |  |  | 1 | KNOB, charcoal-DISPLAY MAG B |
| -61 | 260-0755-00 | 100 | 519 |  | 1 | SWITCH, unwired-DISPLAY MAG B |
|  | 262-0796-01 | 520 |  |  | 1 | SWITCH, wired-DISPLAY MAG B |
|  | - - - - |  |  |  | - | switch includes: |
|  | 260-0755-00 | 520 |  |  | 1 | SWITCH, unwired |
|  | - - - |  |  |  | - | mounting hardware: (not included w/switch) |
| -62 | 220-0413-00 |  |  |  | 2 | NUT, hex., $4-40 \times 3 / 16 \times 0.562$ inch long |
| $\begin{aligned} & -63 \\ & -64 \end{aligned}$ | 366-0215-01 |  |  |  | 1 | KNOB, charcoal-A MODE |
|  | 260-0640-00 |  |  |  | 1 | SWITCH, unwired-A MODE |
|  |  |  |  |  | - | mounting hardware: (not included $\mathrm{w} /$ /switch) |
|  | 210-0586-00 |  |  |  | 2 | NUT, keps, $4-40 \times 1 / 4$ inch |
| $\begin{aligned} & -65 \\ & -66 \end{aligned}$ | 366-0215-01 |  |  |  | 1 | KNOB, charcoal-DISPLAY MAG A |
|  | 260-0755-00 | 100 | 519 |  | 1 | SWITCH, unwired-DISPLAY MAG A |
|  | 262-0796-00 | 520 |  |  | 1 | SWITCH, wired-DISPLAY MAG A |
|  | - - |  |  |  | - | switch includes: |
|  | 260-0755-00 | 520 |  |  | 1 | SWITCH, unwired |
|  | - - - - |  |  |  | - | mounting hardware: (not included w/switch) |
|  | 220-0413-00 |  |  |  | 2 | NUT, hex., $4-40 \times 3 / 16 \times 0.562$ inch long |
| -67 | 366-0220-00 |  |  |  | 1 | KNOB, charcoal-INTENSITY B |
|  | - - - - |  |  |  | - | knob includes: |
|  | 213-0020-00 |  |  |  | 1 | SCREW, set, $6.32 \times 1 / 8$ inch, HSS |
| -68 | - . . - |  |  |  | 1 | RESISTOR, variable |
|  | - |  |  |  | 1 | mounting hardware: (not included w/resistor) |
|  | 210-0013-00 |  |  |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 1 / 16$ inch OD |
|  | $210-0978-00$ |  |  |  | 1 | WASHER, flat, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| -69 | 200-0269-00 |  |  |  | 4 | COVER, variable resistor, plastic |
| -70 | 366-0220-00 |  |  |  | 1 | KNOB, charcoal-FOCUS |
|  | ---- |  |  |  | - | knob includes: |
|  | 213-0020-00 |  |  |  | 1 | SCREW, set, $6-32 \times 1 / 8$ inch, HSS |
| . 71 | - - - - |  |  |  | 1 | RESISTOR, variable |
|  | 210-0013-00 |  |  |  | $i$ | mounting hardware: (not included $\mathrm{w} / \mathrm{resistor)}$ |
|  | 210-0978-00 |  |  |  | 1 | WASHER, flat, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |

## Mechanical Parts List-Type 556

FIG. 1 FRONT \& SWITCHES (cont)

| Fig. \& Index No. | Tektronix Part No. |  | Serial/Model Eff | No. Disc | Q | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.72 | 366-0220-00 | 100 | 2009 |  | 1 | KNOB, charcoal-ASTIGMATISM |
|  | 366-0360-00 | 2010 |  |  | 1 | KNOB, charcoal-ASTIGMATISM |
|  |  |  |  |  |  | knob includes: |
|  | 213-0020-00 |  |  |  | 1 | SCREW, set, $6.32 \times 1 / 8$ inch, HSS |
| -73 | - |  |  |  | 1 | RESISTOR, variable |
|  | … |  |  |  | - | mounting hardware: (not included w/resistor) |
|  | 210-0012-00 |  |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0978-00 |  |  |  | 1 | WASHER, flat, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| -74 | 366-0117-00 |  |  |  | 1 | KNOB, charcoal-AMPLITUDE CALIBRATOR |
|  |  |  |  |  |  | knob includes: |
|  | 213-0020-00 |  |  |  | 1 | SCREW, set, $6-32 \times 1 / 8$ inch, HSS |
| -75 | 262-0731-00 |  |  |  | 1 | SWITCH, wired-AMPLITUDE CALIBRATOR |
|  |  |  |  |  | ; | switch includes: |
|  | 260-0536-00 |  |  |  | 1 | SWITCH, unwired-AMPLITUDE CALIBRATOR |
|  |  |  |  |  |  | mounting hardware: (not included w/switch) |
|  | 210-0013-00 |  |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 11 / 16$ inch OD |
|  | 210-0590-00 |  |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| $\begin{aligned} & -76 \\ & -77 \end{aligned}$ | 366-0361-00 |  |  |  | 1 | KNOB, charcoal-BEAM LOCATE |
|  | 260-0763-00 |  |  |  | 1 | SWITCH, unwired-BEAM LOCATE |
|  | - - - - |  |  |  |  | mounting hardware: (not included w/switch) |
|  | 210-0413-00 |  |  |  | 1 | NUT, hex., $3 / 8-32 \times 3 / 8$ inch |
| -78 | 220-0448-00 |  |  |  | 1 | NUT, hex., spacing, $3 / 8-32 \times 1 / 2 \times 23 / 4$ inches long |
|  | 210-0012-00 |  |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
| -79 | 358-0299-00 |  |  |  | 1 | BUSHING, $3 / 8-32 \times 0.397$ inch long |
| -80-81 | 331-0091-00 |  |  |  | 1 | DIAL, duo dial, w/o brake |
|  | 366-0220-00 |  |  |  | 1 | KNOB, charcoal-UPPER BEAM EXT HORIZ VAR 1-10 |
|  |  |  |  |  |  | knob includes: |
|  | 213-0020-00 |  |  |  | 1 | SCREW, set, $6-32 \times 1 / 8$ inch, HSS |
| -82 | - - - |  |  |  | 1 | RESISTOR, variable |
|  |  |  |  |  |  | mounting hardware: (not included w/resistor) |
|  | 210-0013-00 |  |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 11 / 16$ inch OD |
|  | 210-0978-00 |  |  |  | 1 | WASHER, flat, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| -83 | 366-0254-00 |  |  |  | 1 | KNOB, charcoal-TRACE ROTATION TRACE SEPARATION |
|  | $\cdots$ |  |  |  | - | knob includes: |
|  | 213-0020-00 |  |  |  | 1 | SCREW, set, $6-32 \times 1 / 8$ inch, HSS |
| -84 | - - - |  |  |  | 1 | RESISTOR, variable |
|  | $\cdots$ |  |  |  | i | mounting hardware: (not included w/resistor) |
|  | 210-0207-00 |  |  |  | 1 | LUG, solder, $3 / 8 \mathrm{ID} \times 5 / 8$ inch OD, SE |
|  | 210-0012-00 |  |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0978-00 |  |  |  | 1 | WASHER, flat, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| -85 | 366-0220-00 |  |  |  | 1 | KNOB, charcoal-SCALE ILLUM |
|  | $\cdots$ |  |  |  | $i$ | knob includes: SCREW, set, $6-32 \times 1 / 8$ inch, HSS |

FIG. 1 FRONT \& SWITCHES (cont)

| Fig. \& Index No. | Tektronix Part No. |  | Serial/Model Eff No. Disc | Q t y | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1-86 | - . - . |  |  | 1 | RESISTOR, variable |
|  | - - . . - |  |  | - | mounting hardware: ( not included $\mathrm{w} / \mathrm{resistor)}$ |
|  | 210-0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0978-00 |  |  | 1 | WASHER, flat, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| -87 | 366-0220-00 |  |  | 1 | KNOB, charcoal-LOWER BEAM EXT HORIZ VAR 1-10 |
|  | - - - |  |  | - | knob includes: |
|  | 213-0020-00 |  |  | 1 | SCREW, set, $6-32 \times 1 / 8$ inch, HSS |
| -88 | - - |  |  | 1 | RESISTOR, variable |
|  | - - |  |  | - | mounting hardware: (not included w/resistor) |
|  | 210-0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0978-00 |  |  | 1 | WASHER, flat, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| -89 | 366-0160-00 |  |  | 1 | KNOB, charcoal-LOWER BEAM DISPLAY |
|  | - - - - |  |  | - | knob includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| -90 | 366-0081-00 |  |  | 1 | KNOB, red-POSITION B |
|  | - . . - |  |  | - | knob includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| -91 | 262-0769-00 | 100 | 2009 | 1 | SWITCH, wired-LOWER BEAM DISPLAY |
|  | 262-0769-01 | 2010 |  | 1 | SWITCH, wired-LOWER BEAM DISPLAY |
|  | - - - - |  |  | - | switch includes: |
|  | 260-0751-00 | 100 | 2009 | 1 | SWITCH, unwired |
|  | 260-0751-01 | 2010 |  | 1 | SWITCH, unwired |
| -92 | - - |  |  | 1 |  |
|  | --. - |  |  | - | mounting hardware: (not included w/resistor) |
| -93 | 210-0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
| . 94 | 210-0413-00 |  |  | 2 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| -95 | 376-0014-00 |  |  | 1 | COUPLING, wire, steel |
| . 96 | 384-0391-00 |  |  | 1 | ROD, extension, shaft |
|  | - --- |  |  | - | mounting hardware: (not included w/switch) |
|  | 211-0008-00 |  |  | 2 | SCREW, $4-40 \times 1 / 4$ inch, PHS |
|  | $210-0013-00$ |  |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 11 / 16$ inch OD |
|  | 210-0590-00 |  |  | 1 | NUT, hex., $3 / 8.32 \times 7 / 16$ inch |
| -97 | 366-0144-00 |  |  | 1 | KNOB, charcoal-B TIME/CM |
|  | ---- |  |  | I | knob includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| -98 | 366-0038-00 |  |  | 1 | KNOB, red-VARIABLE B |
|  | ---- |  |  | - | knob includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6-32 \times 3 / 10$ inch, HSS |
| -99 | 262-0767-00 |  |  | 1 | SWITCH, wired-B TIME/CM |
|  | - - - - |  |  | 1 | switch includes: |
|  | 260-0756-00 |  |  | 1 | SWITCH, unwired-B TIME/CM |
| -100 | - - . . - |  |  | 1 | RESISTOR, variable mounting hardware: (not included $w /$ resistor) |
| -101 | 210-0413-00 |  |  | 2 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| -102 | 210-0255-00 |  |  | 1 | LUG, solder, $3 / 8$ ID $\times 0.500$ inch OD, SE |

FIG. 1 FRONT \& SWITCHES (cont)

| Fig. \& Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | Q $\dagger$ y | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 1-103 | - |  | 1 | RESISTOR, variable |
|  | - - - - |  | - | resistor includes: |
|  | 210-0438-00 |  | 2 | NUT, hex., $1.72 \times 5 / 32$ inch |
|  | - - - |  | - | mounting hardware: (not included w/resistor) |
| . 104 | 406-0635-00 |  | 1 | BRACKET, variable resistor mounting |
| -105 | 213-0088-00 |  | 2 | SCREW, thread forming, \#4 $\times 1 / 4$ inch, PHS |
| -106 | 407-0214-00 |  | 1 | BRACKET, switch mounting |
|  | - - . - |  | - | mounting hardware: (not included w/bracket) |
|  | 210-0006-00 |  | 2 | LOCKWASHER, internal \#6 |
|  | 210-0449-00 |  | 2 | NUT, hex., $5-40 \times 1 / 4$ inch |
| -107 | - - - |  | 1 | CAPACITOR |
|  | . . . - - |  | - | mounting hardware: (not included w/capacitor) |
| -108 | 210-0457-00 |  | 2 | NUT, keps, $6-32 \times 5 / 16$ inch |
|  | 210-0407-00 |  | 2 | NUT, hex., $6.32 \times 1 / 4$ inch |
| $\begin{aligned} & -109 \\ & -110 \end{aligned}$ | 348-0055-00 |  | 1 | GROMMET, plastic, $1 / 4$ inch diameter |
|  | 131-0183-00 |  | 2 | CONNECTOR, terminal feed thru |
|  | --- |  | - | mounting hardware for each: (not included w/connector) |
|  | 358-0136-00 |  | 1 | BUSHING, plastic, connector |
| -111 | - - - - |  | 1 | CAPACITOR |
|  | - -- |  | - | mounting hardware: (not included w/capacitor) |
|  | 210-0018-00 |  | 1 | LOCKWASHER, internal, 3/16 inch |
| -112 | 210-0524-00 |  | 1 | NUT, hex., $5 / 16-24 \times 1 / 2$ inch |
|  | 179-1073-00 |  | 1 | CABLE HARNESS, time/cm switch |
| -113-114 | 384-0389-00 |  | 1 | ROD, external shaft, $0.125 \times 8$ inches long |
|  | 376-0014-00 |  | 1 | COUPLING, wire steel |
|  | -- - - - |  | I | mounting hardware: (not included w/switch) |
|  | 210-0012-00 |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0590-00 |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
|  | 211-0507-00 |  | 2 | SCREW, $6.32 \times 5 / 16$ inch, PHS |
| -115 | 366-0173-00 |  | 1 | KNOB, charcoal-LEVEL B |
|  | --- - |  | - | knob includes: |
|  | 213-0004-00 |  | 1 | SCREW, 6-32 $\times 3 / 16$ inch, HSS |
| -116 | - - - - |  | 1 | RESISTOR, variable |
|  | --- - |  | - | mounting hardware: (not included w/resistor) |
|  | 210-0978-00 |  | 1 | WASHER, flat, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0590-00 |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| -117 | 366-0144-00 |  | 1 | KNOB, charcoal-A TIME/CM |
|  | ---- |  | ; | knob includes: |
|  | 213-0004-00 |  | 1 | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |

FIG. 1 FRONT \& SWITCHES (cont)

| Fig. \& Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { No. }}{\text { Disc }}$ | Q t y | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 1-118 | 366-0038-00 |  | 1 | KNOB, red—VARIABLE A |
|  | . . . . . - |  | - | knob includes: |
|  | 213-0004-00 |  | 1 | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| -119 | 262-0766-00 |  | 1 | SWITCH, wired-A TIME/CM |
|  | - - . |  | - | switch includes: |
|  | 260-0756-00 |  | 1 | SWITCH, unwired-A TIME/CM |
| -120 | . - - - |  | 1 | RESISTOR, variable |
|  | - . - - |  | - | mounting hardware: (not included $\mathrm{w} /$ resistor) |
|  | 210-0413-00 |  | 2 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| -121 | 210-0255-00 |  | 1 | LUG, solder, $3 / 8 \mathrm{ID} \times 0.500$ inch OD, SE |
| -122 | 407-0215-00 |  | 1 | BRACKET, switch mounting |
|  | - - - - |  | - | mounting hardware: (not included w/bracket) |
|  | 210-0006-00 |  | 2 | LOCKWASHER, internal, \#6 |
|  | 210-0449-00 |  | 2 | NUT, hex., $5-40 \times 1 / 4$ inch |
|  | 179-1073-00 |  | 1 | CABLE HARNESS, time/cm switch |
| -123 | - - - |  | 1 | CAPACITOR |
|  | ---- |  |  | mounting hardware: (not included w/capacitor) |
| -124 | 210-0457-00 |  | 2 | NUT, keps, $6-32 \times 5 / 16$ inch |
|  | 210-0407-00 |  | 2 | NUT, hex., $6.32 \times 1 / 4$ inch |
| $\begin{aligned} & -125 \\ & -126 \end{aligned}$ | 348-0055-00 |  | 1 | GROMMET, plastic, $1 / 4$ inch diameter |
|  | - . - |  | 1 | CAPACITOR |
|  | - . - - |  | - | mounting hardware: (not included w/capacitor) |
|  | 210-0018-00 |  | 1 | LOCKWASHER, internal, $5 / 16$ inch |
| -127 | 210-0524-00 |  | 1 | NUT, hex., $15 / 16 \times 1 / 2$ inch |
| $\begin{aligned} & -128 \\ & -129 \end{aligned}$ | 384-0389-00 |  | 1 | ROD, external shaft 0.125 dia $\times 8$ inches long |
|  | 376-0014-00 |  | 1 | COUPLING, wire, steel |
|  | $\ldots$ |  | - | mounting hardware: (not included w/switch) |
|  | 210-0012-00 |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0590-00 |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
|  | 211-0507-00 |  | 2 | SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -130 | 366-0360-00 |  | 1 | KNOB, charcoal-ASTIGMATISM A |
|  | .-. . - |  | - | knob includes: |
|  | 213-0020-00 |  | 1 | SCREW, set, $6.32 \times 1 / 8$ inch, HSS |
| $\begin{aligned} & -131 \\ & -132 \end{aligned}$ | 366-0283-00 |  | 1 | KNOB, charcoal-CONTRAST (A INTENS BY B) |
|  | - - - - |  | 1 | RESISTOR, variable |
|  | ---- |  | 1 | mounting hardware: (not included w/resistor) |
|  | 210-0013-00 |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 11 / 16$ inch OD |
|  | 210-0978-00 |  | 1 | WASHER, flat, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0590-00 |  | 1 | NUT, hex., $3 / 8.32 \times 7 / 16$ inch |
| -133 | 366-0220-00 |  | 1 | KNOB, charcoal-FOCUS A |
|  | $\cdots$ |  | 1 | knob includes: |
|  | 213-0020-00 |  | 1 | SCREW, set, $6-32 \times 1 / 8$ inch, HSS |

FIG. 1 FRONT \& SWITCHES (cont)

| Fig. \& Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }} \quad$No. <br> Dise | $\begin{gathered} \mathrm{Q} \\ \mathrm{t} \\ \mathrm{y} \\ \hline \end{gathered}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1-134 | - |  |  | 1 | RESISTOR, variable |
|  | . . . . - |  |  | - | mounting hardware: (not included w/resistor) |
|  | 210-0013-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times{ }^{11 / 16}$ inch OD |
|  | 210-0978-00 |  |  | 1 | WASHER, flat, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| -135 | 366-0220-00 |  |  | 1 | KNOB, charcoal-INTENSITY A |
|  | - . - |  |  | - | knob includes: |
|  | 213-0020-00 |  |  | 1 | SCREW, set, $6-32 \times 1 / 8$ inch, HSS |
| -136 | - . . . - |  |  | 1 | RESISTOR, variable |
|  | ---- - |  |  | - | mounting hardware: (not included w/resistor) |
|  | 210-0013-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times{ }^{1 / 16}$ inch OD |
|  | 210-0978-00 |  |  | 1 | WASHER, flat, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0413-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| -137 | 366-0160-00 |  |  | 1 | KNOB, charcoal-_UPPER BEAM DISPLAY |
|  | - - . - |  |  | - | knob includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| -138 | 366-0081-00 |  |  | 1 | KNOB, red-POSITION A |
|  | - - - - |  |  | - | knob includes: |
|  | 213-0004-00 |  |  | , | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| -139 | 262-0768-00 | 100 | 2009 | 1 | SWITCH, wired-UPPER BEAM DISPLAY |
|  | 260-0768-01 | 2010 |  | 1 | SWITCH, wired-UPPER BEAM DISPLAY |
|  |  |  |  |  | switch includes: |
|  | 260-0752-00 | 100 | 2009 | 1 | SWITCH, unwired-_UPPER BEAM DISPLAY |
|  | 260-0752-01 | 2010 |  | 1 | SWITCH, unwired |
| -140 | - . - |  |  | 1 | RESISTOR, variable |
|  | - . . . . - |  |  | - | mounting hardware: (not included w/resistor) |
|  | $210-0012-00$ |  |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 1 / 2$ inch OD |
| -141 | $210-0413-00$ |  |  | 2 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| $\begin{aligned} & -142 \\ & -143 \end{aligned}$ | 376-0014-00 |  |  | 1 | COUPLING, wire, steel |
|  | 384-0390-00 |  |  | 1 | ROD, external shaft, 0.125 dia $\times 4.074$ inches long |
|  | - - - |  |  | - | mounting hardware: (not included w/switch) |
|  | 211-0008-00 |  |  | 2 | SCREW, $4-40 \times 1 / 4$ inch, PHS |
|  | $210-0013-00$ |  |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| . 144 | 366-0173-00 |  |  | 1 | KNOB, charcoal-LEVEL A |
|  | - . - . - |  |  |  | knob includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| -145 | ... - - |  |  | 1 | RESISTOR, variable |
|  | - . . - . - |  |  | - | mounting hardware: (not included w/resistor) |
|  | 210-0978-00 |  |  | 1 | WASHER, flat, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0590-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 16$ inch |

FIG. 1 FRONT \& SWITCHES (cont)


FIG. 2 A SWEEP, VERTICAL AMPLIFIER \& HIGH VOLTAGE

| Fig. \& Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\substack{\text { Serial/Model } \\ \text { No. } \\ \text { Disc }}}$ | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2-1 | 441-0655-00 | $\begin{aligned} & 100 \\ & 2010 \end{aligned}$ | 2009 | 1 | CHASSIS, A Sweep |
|  | 441-0655-01 |  |  | 1 | CHASSIS, A SWEEP |
|  | - - - - |  |  | - | mounting hardware: (not included w/chassis) |
|  | 211-0559-00 |  |  | 4 | SCREW, $6-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
|  | 212-0040-00 |  |  | 1 | SCREW, $8-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
|  | 212-0004-00 |  |  | 2 | SCREW, $8.32 \times 5 / 16$ inch, PHS |
| $-2$ | 670-0431-00 |  |  | 1 | ASSEMBLY, circuit board assembly includes: SWITCH, reed SOCKET, transistor, 3 pin BOARD, circuit board includes: |
|  | - - - - |  |  | - |  |
|  | 260-0552-00 |  |  | 1 |  |
| -3 | 136-0220-00 |  |  | 2 |  |
|  | 388-0696-00 |  |  | 1 |  |
|  | - - - - |  |  |  |  |
| -4 | 214-0506-00 |  |  | 12 |  |
|  | - - - |  |  | - | mounting hardware: (not included w/assembly) |
| -5 | 211-0601-00 |  |  | 3 | SCREW, sems, 6 -32 $\times 5 / 16$ inch, PHB |
| -6 | 129-0088-00 |  |  | $3$ |  |
|  | $210-0006-00$ |  |  | $3$ | LOCKWASHER, internal, \#6 |
| -7 | - - - - |  |  | 1 | RESISTOR |
|  | - - - - - |  |  | - | mounting hardware: (not included w/resistor) |
| -8 | 211-0544-00 |  |  | 1 | SCREW, $6-32 \times 3 / 4$ inch, THS |
| -9 | 210-0478-00 |  |  | 1 | NUT, hex., $5 / 16 \times 21 / 32$ inch long |
|  | 211-0507-00 |  |  | 1 | SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -10 | 136-0181-00 | $\begin{aligned} & 100 \\ & 2010 \end{aligned}$ | 2009 | $19$ |  |
|  | $136-0181-00$ |  |  | 20 | SOCKET, transistor, 3 pin mounting hardware for each: (not included w/socket) |
| -11 | 354-0234-00 |  |  | 1 | RING, socket mounting |
| -12 | - - - - |  |  | 2 | COIL |
|  | ---. - |  |  | - | mounting hardware for each: (not included w/coil) |
| -13 | 407-0236-01 |  |  | 1 | BRACKET, plastic, coil mounting |
|  | $212-0004-00$ |  |  | 1 | SCREW, $8-32 \times 5 / 16$ inch, PHS |
| -14 | 200-0642-00 |  |  | 2 | CAP, $1 / 4$ inch |
| -15 | - - - |  |  | 1 | CAPACITOR |
|  | --- |  |  |  | mounting hardware: (not included w/capacitor) |
| -16 | 386-0255-00 |  |  | 1 | PLATE, flange, metal capacitor mounting |
| -17 | 211-0534-00 |  |  | 2 | SCREW, sems, $6-32 \times 5 / 16$ inch, PHS |
|  | 210-0457-00 |  |  | 2 | NUT, keps, $6-32 \times 5 / 16$ inch |

fig. 2 A SWEEP, VERTICAL AMPLIFIER \& HIGH VOLTAGE (cont)

| Fig. \& Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Disc | $\begin{aligned} & \mathrm{Q} \\ & \dagger \\ & \mathrm{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 2-18 | $\begin{aligned} & 337-0813-00 \\ & \cdots- \\ & 210-0586-00 \end{aligned}$ |  | $\begin{aligned} & 1 \\ & 2 \\ & 2 \end{aligned}$ | SHIELD mounting hardware: (not included w/shield) NUT, keps, $4-40 \times 1 / 4$ inch |
| . 19 | $\begin{gathered} \cdots \cdots \\ 210-0207-00 \\ 210-0012-00 \\ 210-0840-00 \\ 210-0413-00 \end{gathered}$ |  | $\begin{aligned} & 2 \\ & - \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | RESISTOR, variable mounting hardware for each: (not included w/resistor) LUG, solder, $3 / 8$ ID $\times 5 / 8$ inch $O D, S E$ LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD WASHER, flat, $0.390 \mathrm{ID} \times 9 / 16$ inch OD NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| -20 | $\begin{aligned} & 210-0840-00 \\ & 210-0413-00 \end{aligned}$ |  | $\begin{aligned} & 3 \\ & i \\ & 1 \\ & 1 \end{aligned}$ | RESISTOR, variable <br> mounting hardware for each: (not included w/resistor) <br> WASHER, flat, $0.390 \mathrm{ID} \times 9 / 1$ inch $O D$ <br> NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| -21 -22 | $\begin{aligned} & 136-0158-00 \\ & \hdashline- \\ & 213-0044-00 \end{aligned}$ |  | $\begin{aligned} & 2 \\ & 2 \\ & 2 \end{aligned}$ | SOCKET, tube, 12 pin, w/ground lugs mounting hardware for each: (not included w/socket) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -23 | $\begin{aligned} & 210-0201-00 \\ & \hdashline 213-0044-00 \end{aligned}$ |  | $\begin{array}{r} 11 \\ 1 \\ \hline \end{array}$ | LUG, solder, SE \#4 mounting hardware for each: (not included w/lug) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -24 | $\begin{aligned} & 210-0204-00 \\ & -0- \\ & 213-0044-00 \end{aligned}$ |  | $\begin{aligned} & 4 \\ & i \end{aligned}$ | LUG, solder, DE \#6 mounting hardware for each: (not included w/lug) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| $\begin{aligned} & -25 \\ & -26 \\ & -27 \end{aligned}$ | $\begin{aligned} & 384-0542-00 \\ & 211-0507-00 \end{aligned}$ |  | $\begin{aligned} & 2 \\ & i \\ & 1 \\ & 1 \end{aligned}$ | CAPACITOR <br> mounting hardware for each: (not included w/capacitor) ROD, plastic, $5 / 16 \times 1$ inch long SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -28 | $\begin{gathered} 136-0174-00 \\ \hdashline 213-0044-00 \end{gathered}$ |  | $\begin{aligned} & 2 \\ & 2 \\ & 2 \end{aligned}$ | SOCKET, tube, 9 pin, w/ground lugs mounting hardware for each: (not included w/socket) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -29 | $\begin{aligned} & 136-0015-00 \\ & \hdashline- \\ & 213-0044-00 \end{aligned}$ |  | $9$ | SOCKET, tube, 9 pin, w/ground lugs mounting hardware for each: (not included w/socket) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -30 -31 | $\begin{aligned} & 136-0008-00 \\ & \hdashline- \\ & 213-0044-00 \end{aligned}$ |  | 1 - 2 | SOCKET, tube, 7 pin, w/ground lugs mounting hardware: (not included w/socket) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |

FIG. 2 A SWEEP, VERTICAL AMPLIFIER \& HIGH VOLTAGE (cont)

| Fig. \& Index No. | Tektronix Part No. |  | Serial/Mode Eff | No. Disc | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \\ & \hline \end{aligned}$ | 12345 Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2-32 | $\begin{gathered} 337-0005-00 \\ --- \\ 213-0044-00 \end{gathered}$ |  |  |  | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | SHIELD, socket, STSI79 mounting hardware: (not included $w /$ shield) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| $\begin{aligned} & -33 \\ & -34 \\ & -35 \\ & -36 \\ & -37 \\ & -38 \end{aligned}$ | $\begin{aligned} & 337-0008-00 \\ & 348-0050-00 \\ & 348-0056-00 \\ & 348-0031-00 \\ & 348-0055-00 \\ & 385-0151-00 \\ & ---1 \\ & 211-0507-00 \end{aligned}$ |  |  |  | $\begin{aligned} & 1 \\ & 2 \\ & 1 \\ & 6 \\ & 2 \\ & 2 \\ & - \\ & 1 \end{aligned}$ | SHIELD, tube, $11 / 32$ ID $\times 2^{13 / 32}$ inches $h$, w/spring GROMMET, plastic, $3 / 4$ inch diameter GROMMET, plastic, $3 / 8$ inch diameter GROMMET, plastic, $5 / 32$ inch diameter GROMMET, plastic, $1 / 4$ inch diameter ROD, plastic, $5 / 16$ OD $\times 29 / 16$ inches long mounting hardware for each: (not included w/rod) SCREW, $6.32 \times 5 / 16$ inch, PHS |
| -39 | $\begin{aligned} & 385-0168-00 \\ & --- \\ & 210-0006-00 \\ & 211-0507-00 \end{aligned}$ |  |  |  | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | ROD, spacer, hex., $1 / 4$ OD $\times 1.168$ inches long mounting hardware: (not included w/rod) LOCKWASHER, internal, \#6 SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -40 | $\begin{aligned} & 385-0138-00 \\ & 385-0137-00 \\ & \hdashline-- \\ & 213-0041-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 117 \end{aligned}$ | 116 |  | $\begin{aligned} & 1 \\ & 1 \\ & - \\ & 1 \end{aligned}$ | ROD, plastic, $1 \% / 16$ inches long ROD, plastic, $21 / 4$ inches long mounting hardware: (not included w/rod) SCREW, thread cutting, $6-32 \times 3 / 8$ inch, PHS |
| -41 | $\begin{aligned} & 337-0790-00 \\ & --- \\ & 210-0457-00 \end{aligned}$ |  |  |  | $\begin{aligned} & 1 \\ & - \\ & 2 \end{aligned}$ | SHIELD, top half mounting hardware: (not included $w /$ shield) NUT, keps, $6-32 \times 5 / 16$ inch |
| -42 -43 | $\begin{aligned} & 337-0789-00 \\ & ---- \\ & 211-0007-00 \\ & 210-0457-00 \end{aligned}$ |  |  |  | $\begin{aligned} & 1 \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | SHIELD, bottom half mounting hardware: (not included $w /$ shield) SCREW, $4-40 \times 3 / 16$ inch, PHS NUT, keps, $6-32 \times 5 / 16$ inch |
| -44 | $\begin{aligned} & 210-0940-00 \\ & 210-0583-00 \end{aligned}$ |  |  |  | $\begin{aligned} & 2 \\ & \vdots \\ & 1 \\ & 1 \end{aligned}$ | RESISTOR, variable mounting hardware for each: (not included w/resistor) WASHER, flat, $1 / 4 \mathrm{ID} \times 3 / 8$ inch OD NUT, hex., $1 / 4-32 \times 5 / 16$ inch |
| -45 | $\begin{aligned} & 337-0792-00 \\ & 210-0457-00 \end{aligned}$ |  |  |  | $\begin{aligned} & 1 \\ & - \\ & 5 \end{aligned}$ | SHIELD, high voltage mounting hardware: (not included $w /$ shield) NUT, keps, $6-32 \times 5 / 16$ inch |
| -46 -47 | $\begin{aligned} & 200-0645-00 \\ & \hdashline-\cdots \\ & 211-0097-00 \end{aligned}$ |  |  |  | 1 4 | COVER, high voltage mounting hardware: (not included w/cover) SCREW, $4-40 \times 5 / 16$ inch, PHS |

## FIG. 2 A SWEEP, VERTICAL AMPLIFIER \& HIGH VOLTAGE (cont)

| Fig. \& Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 2-48 | 386-1099-00 |  | 1 | PLATE, CRT shield |
|  | - - - - |  | - | mounting hardware: (not included w/plate) |
| -49 | 211-0008-00 |  | 4 | SCREW, 4-40 $\times 1 / 4$ inch, PHS |
| -50 | 407-0242-00 |  | 4 | BRACKET, angle |
|  | 211-0507-00 |  | 4 | SCREW, 6-32 $\times 5 / 16$ inch, PHS |
| -51 | 343-0007-00 |  | 4 | CLAMP, cable, $5 / 8$ inch plastic |
| -52 | 441-0659-00 |  | 1 | CHASSIS, vertical amplifier "A" |
|  | - - - - |  | - | mounting hardware: (not included w/chassis) |
|  | 212-0004-00 |  | 2 | SCREW, $8-32 \times 5 / 16$ inch, PHS |
|  | 212-0040-00 |  | 2 | SCREW, $8.32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| $\begin{aligned} & -53 \\ & -54 \\ & -55 \end{aligned}$ | 348-0063-00 |  | 1 | GROMMET, plastic, $1 / 2$ inch diameter |
|  | 348-0056-00 |  | 3 | GROMMET, plastic, $3 / 8$ inch diameter |
|  | - . - - |  | 1 | RESISTOR, variable |
|  |  |  | - | mounting hardware: (not included w/resistor) |
|  | $210-0840-00$ |  | 1 | WASHER, flat, 0.390 ID $\times \% / 16$ inch OD |
|  | 210-0413-00 |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
|  | $210-0207-00$ |  | 1 | LUG, solder, $3 / 8 \mathrm{ID} \times 5 / 8$ inch OD, SE |
|  | $210-0012-00$ |  | 1 | LOCKWASHER, internal, $3 / 810 \times 1 / 2$ inch OD |
| -56 | 210-0201-00 |  | 8 | LUG, solder, SE \#4 |
|  |  |  | - | mounting hardware for each: (not included w/lug) |
|  |  |  |  | SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -57 | 210-0204-00 |  | 1 | LUG, solder, DE \#6 |
|  | $213-0044-00$ |  | 1 | mounting hardware: (not included w/lug) SCREW, thread forming, $5.32 \times 3 / 16$ inch, PHS |
|  |  |  |  |  |
| $\begin{aligned} & -58 \\ & -59 \end{aligned}$ |  |  | $f t$. | PLASTIC, extruded channel (specify $33 / 8$ inches long) |
|  | 136-0015-00 |  | 1 | SOCKET, tube, 9 pin, w/ground lugs |
|  | $213-0044-00$ |  | 2 | mounting hardware: (not included w/socket) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -60 | 136-0181-00 |  | 18 | SOCKET, transistor, 3 pin |
|  | - - - |  | - | mounting hardware for each: (not included w/socket) |
| -61 | 354-0234-00 |  | 1 | RING, socket mounting |
| -62 | 385-0168-00 |  | 1 | ROD, spacer, $1 / 4$ inch hex., $\times 1.168$ inches long |
|  | - -- |  | - | mounting hardware: (not included w/rod) |
|  | 210-0006-00 |  | 1 | LOCKWASHER, internal, \#6 |
| -63 | $\cdots$ |  | 3 | CAPACITOR |
|  | - - - - |  | $i$ | mounting hardware for each: (not included w/capacitor) |
| -64 | 214-0153-00 |  | 1 | FASTENER, plastic, snapin |

## fig. 2 A sWeep, vertical amplifier \& high voltage (cont)

| Fig. \& Index No. | Tekfronix Part No. |  | $\begin{aligned} & \text { Serial/Model } \\ & \text { Eff } \\ & \hline \end{aligned}$ | No. Disc | Q t y | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.65 |  |  |  |  | 1 | CAPACITOR |
|  |  |  |  |  | - | mounting hardware: (not included w/capacitor) |
| -66 | 432-0048-00 |  |  |  | 1 | BASE, plastic, capacitor mounting |
|  | 386-0255-00 |  |  |  | 1 | PLATE, metal, capacitor mounting |
|  | 211-0516-00 |  |  |  | 2 | SCREW, $6-32 \times 1 / 8$ inch, PHS |
|  | 210-0457-00 |  |  |  | 2 | NUT, keps, $6-32 \times 5 / 16$ inch |
| -67 | ---- |  |  |  | 1 | CAPACITOR |
|  |  |  |  |  | ; | mounting hardware: (not included w/capacitor) |
| $\begin{aligned} & -68 \\ & -69 \end{aligned}$ | 432-0047-00 |  |  |  | 1 | BASE, plastic, capacitor mounting |
|  | 386-0252-00 |  |  |  | 1 | PLATE, fiber, capacitor mounting |
|  | 211-0516-00 |  |  |  | 2 | SCREW, 6-32 $7 / 8$ inch, PHS |
|  | 210-0457-00 |  |  |  | 2 | NUT, keps, $6-32 \times 5 / 16$ inch |
| -70-71 | 200-0533-00 |  |  |  | 1 | COVER, capacitor, 1 ID $\times 0.750$ inch long |
|  | 344-0116-00 |  |  |  | 1 | CLIP, capacitor mounting |
| -72 | --.-. |  |  |  | 2 | COIL |
|  | -0-00 |  |  |  |  | mounting hardware for each: (not included w/coil) |
|  | 213-0044-00 |  |  |  | 1 | SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -73 | 119-0069-00 |  |  |  | 1 | ASSEMBLY, delay line |
|  |  |  |  |  |  | assembly includes: |
| $\begin{aligned} & -74 \\ & .75 \\ & -76 \end{aligned}$ | $131-0271-00$ $380-0049-00$ |  |  |  | ${ }_{1}^{2}$ | CONNECTOR, cable termination |
|  | 200-0482-00 | 100 | 2009 |  | 1 | COVER, delay line |
|  | 200-0482-06 | 2010 |  |  | 1 | COVER, delay line |
|  |  |  |  |  |  | mounting hardware: (not included w/cover) |
|  | 211-0514-00 |  |  |  | 3 | SCREW, 6-32 ${ }^{3} / 4$ inch, PHS |
|  | 210-0407-00 |  |  |  | 3 | NUT, hex., $6-32 \times 1 / 4$ inch |
|  | - - - - |  |  |  |  | mounting hardware: (not included w/assembly) |
| -77 | 211-0516-00 |  |  |  | 2 | SCREW, $6-32 \times 7 / 8$ inch, PHS |
| -78 | 385-0018-00 |  |  |  | 2 | ROD, plastic, $5 / 16 \times 1 / 4$ inches long |
| .79-80 | 211-0510.00 |  |  |  | 1 | SCREW, $6-32 \times 3 / 8$ inch, PHS |
|  | 392-0147-00 |  |  |  | 1 | ASSEMBLY, high voltage board |
| -81 | $\cdots$ |  |  |  | i | assembly includes: STRIP, ceramic, $7 / 16$ inch $h$, w/4 notches |
|  | $\cdots$ |  |  |  |  | strip includes: |
| -82 | 355-0046-00 |  |  |  | 1 | STUD, plastic |
|  |  |  |  |  | ; | mounting hardware: (not included w/strip) |
| -83 | 361-0007-00 |  |  |  | 1 | SPACER, plastic, 0.156 inch long |
| -84-85-86 | 346-0032-00 |  |  |  | 1 | STRAP, mousetail, rubber, 0.075 dia $\times 4$ inches long |
|  | 124-0164-00 |  |  |  | 2 | STRIP, ceramic, 0.437 inch h , w/4 notches |
|  | 124-0163-00 |  |  |  | 4 | STRIP, ceramic, 0.437 inch $h$, w/2 notches |
|  | 211-0507-00 |  |  |  | $i$ | mounting hardware: (not included w/assembly) SCREW, $6-32 \times 5 / 18$ inch, PHS |

fig. 2 A SWEEP, VERTICAL AMPLIFIER \& high voltage (cont)

| Fig. \& Index No. | Tektronix Part No. |  | Serial/Model No. <br> Eff <br> Disc | $\begin{aligned} & Q \\ & t \\ & y \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.87 |  |  |  | 1 | TRANSFORMER |
|  |  |  |  |  | mounting hardware: (not included w/transformer) |
| -88-89 | 211-0521-00 |  |  | 2 | SCREW, $6-32 \times 1 / \frac{\text { inches, RHS }}{}$ |
|  | 210-0869-00 |  |  | 2 | WASHER, plastic, $5 / 32$ ID $\times 3 / 8$ inch OD |
| .90.91 | 200-0475-00 |  |  | 1 | COVER, high voltage box |
|  | 337-0814-00 |  |  | 1 | SHIELD, high voltage |
|  |  |  |  |  | mounting hardware: (not included w/shield) |
| $\begin{aligned} & -92 \\ & -93 \end{aligned}$ | 211-0530-00 |  |  | 2 | SCREW, $6.32 \times 13 / 4$ inches, PHS |
|  | 210-0716-00 |  |  | 2 | WASHER, plastic insulating |
| $\begin{aligned} & -.94 \\ & -95 \\ & -96 \end{aligned}$ | 166-0357-00 |  |  | 1 | SLEEVE, plastic, anode lead |
|  | 166-0319-00 |  |  | 2 | SLEEVE, plastic, insulating |
|  | 380-0048-00 |  |  | 1 | HOUSING, high voltage |
|  | $\cdots$ |  |  | - | mounting hardware: (not included w/housing) |
|  | 211-0507-00 |  |  | 2 | SCREW, $6.32 \times 5 / 16$ inch, PHS |
|  | 211-0542-00 |  |  | 1 | SCREW, $6.32 \times 5 / 16$ inch, THS |
| $\begin{aligned} & -97 \\ & -98 \\ & -99 \end{aligned}$ | 179-1069-00 |  |  | , | CABLE HARNESS, high voltage \#1 |
|  | 179-1071-00 |  |  | 1 | CABLE HARNESS, high voltage \#2 |
|  | 179-1054-00 | 100 | 2009 | 1 | CABLE HARNESS, "A" Sweep \#2 |
|  | 179-1054-01 | 2010 |  | 1 | CABLE HARNESS, "A" SWEEP \#2 |
| $\begin{aligned} & -100 \\ & -101 \end{aligned}$ | 179-1067-00 |  |  | 1 | CABLE HARNESS, high voltage |
|  | 179-1053-00 | 100 | 2009 |  | CABLE HARNESS, "A" Sweep \#1 |
|  | 179-1053-01 | 2010 |  | , | CABLE HARNESS, "A" SWEEP \# 1 |
| -102 | $124-0145-00$ |  |  | 11 | STRIP, ceramic, $7 / 16$ inch $h$, w/20 notches each strip includes: |
|  | 355-0046-00 |  |  | 2 | STUD, plastic |
|  | $361-0009-00$ |  |  | 2 | mounting hardware for each: (not included w/strip) SPACER, plastic, 0.406 inch long |
| -103 | 124-0146-00 |  |  | 14 | STRIP, ceramic, $7 / 16$ inch $h$, w/16 notches |
|  | 355-0046-00 |  |  | 2 | each strip includes: <br> STUD, plastic |
|  | - . - |  |  | . | mounting hardware for each: (not included w/strip) |
|  | 361-0009-00 |  |  | 2 | SPACER, plastic, 0.406 inch long |
| -104 | 124-0162-00 |  |  | 1 | STRIP, ceramic, $7 / 16$ inch $h$, w/4 notches |
|  | $355-0046-00$ |  |  | 2 | strip includes: <br> STUD, plastic |
|  | - - |  |  |  | mounting hardware: (not included w/strip) |
|  | 361-0009-00 |  |  | 2 | SPACER, plastic, 0.406 inch long |
| -105 | 124-0149-00 |  |  | 2 | STRIP, ceramic, $7 / 16$ inch $h, w / 7$ notches |
|  | 355-0046-00 |  |  | 2 | STUD, plastic |
|  | - |  |  |  | mounting hardware for each: (not included w/strip) |
|  | 361-0009-00 |  |  | 2 | SPACER, plastic, 0.406 inch long |

## FIG. 2 A SWEEP, VERTICAL AMPLIFIER \& HIGH VOLTAGE (cont)

| Fig. \& Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | $\begin{gathered} Q \\ t \\ y \end{gathered}$ | 12345 Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2-106 | $\begin{aligned} & 124-0147-00 \\ & --- \\ & 355-0046-00 \\ & --- \\ & 361-0009-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | STRIP, ceramic, $7 / 16$ inch $h, w / 13$ notches strip includes: <br> STUD, plastic <br> mounting hardware: (not included w/strip) SPACER, plastic, 0.406 inch long |
| -107 | $\begin{aligned} & 124-0147-00 \\ & -0-0 \\ & 355-0046-00 \\ & \hdashline 361-0007-00 \end{aligned}$ |  |  | $\begin{aligned} & 2 \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | STRIP, ceramic, $7 / 16$ inch $h, w / 13$ notches each strip includes: <br> STUD, plastic <br> mounting hardware for each: (not included w/strip) SPACER, plastic, 0.188 inch long |
| -108 | $\begin{aligned} & 124-0148-00 \\ & 355-0046-00 \\ & -\cdots 61-0009-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | STRIP, ceramic, $7 / 16$ inch $h, w / 9$ notches strip includes: <br> STUD, plastic <br> mounting hardware: (not included w/strip) SPACER, plastic, 0.406 inch long |
| -109 | $\begin{aligned} & 124-0089-00 \\ & -0 \\ & 355-0046-00 \\ & 361-0009-00 \end{aligned}$ |  |  | $\begin{aligned} & 4 \\ & - \\ & 2 \\ & 2 \end{aligned}$ | STRIP, ceramic, $3 / 4$ inch $h$, w/7 notches each strip includes: <br> STUD, plastic <br> mounting hardware for each: (not included w/strip) SPACER, plastic, 0.406 inch long |
| $\begin{aligned} & -110 \\ & -111 \\ & -112 \end{aligned}$ | $\begin{aligned} & 179-1061-00 \\ & 179-1061-01 \\ & 179-1063-00 \\ & 124-0145-00 \\ & 335-0046-00 \\ & 361-0009-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 2010 \end{aligned}$ | 2009 | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 2 \\ & - \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | CABLE HARNESS, left Vertical Amplifier CABLE HARNESS, left Vertical Amplifier CABLE HARNESS, left coaxial STRIP, ceramic, $7 / 16$ inch $h, w / 20$ notches each strip includes: <br> STUD, plastic <br> mounting hardware for each: (not included w/strip) SPACER, plastic, 0.406 inch long |
| -113 | $\begin{gathered} 124-0147-00 \\ \hdashline 355-0046-00 \\ \hdashline 361-0009-00 \end{gathered}$ |  |  | $\begin{array}{r} 10 \\ \hline \\ 2 \\ 2 \end{array}$ | STRIP, ceramic, $7 / 16$ inch $h, w / 13$ notches each strip includes: <br> STUD, plastic <br> mounting hardware for each: (not included w/strip) <br> SPACER, plastic, 0.406 inch long |
| -114 | $\begin{gathered} 385-0138-00 \\ \hdashline-- \\ 213-0041-00 \end{gathered}$ | X117 |  | $\begin{aligned} & 1 \\ & i \end{aligned}$ | ROD, plastic, $19 / 16$ inches long mounting hardware: (not included w/rod) SCREW, thread cutting, $6-32 \times 3 / 8$ inch, THS |

FIG. 3 B SWEEP VERTICAL AMPLIFIER \& HIGH VOLTAGE

| Fig. \& Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3-1 | 441-0656-00 | $\begin{aligned} & 100 \\ & 2010 \end{aligned}$ | 2009 | 1 | CHASSIS, "B" sweep |
|  | 441-0656-01 |  |  | 1 | CHASSIS, "B" sweep |
|  | - - - . |  |  |  | mounting hardware: (not included w/chassis) |
|  | 211-0559-00 |  |  | 4 | SCREW, $6-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
|  | 212-0040-00 |  |  | 1 | SCREW, $8-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
|  | 212-0004-00 |  |  | 2 | SCREW, $8-32 \times 5 / 16$ inch, PHS |
| -2 | 670-0432-00 |  |  | 1 | ASSEMBLY, circuit board |
|  | - - - - |  |  | - | assembly includes: |
|  | 260-0552-00 |  |  | 1 | SWITCH, reed |
| -3 | 136-0220-00 |  |  | 2 | SOCKET, transistor, 3 pin |
|  | 388-0696-00 |  |  | 1 | BOARD, circuit |
|  | - -- - |  |  |  | board includes: |
| -4 | 214-0506-00 |  |  | 12 | PIN, connector, straight, male |
|  | - - - |  |  | - | mounting hardware: (not included w/assembly) |
| -5 | 211-0601-00 |  |  | 3 | SCREW, sems, $6-32 \times 5 / 16$ inch, PHB |
| -6 |  |  |  | $3$ | POST, hex., 0.250 dia $\times 0.700$ inch long |
|  | $210-0006-00$ |  |  | $3$ | LOCKWASHER, internal, \#6 |
| $-7$ | - - - - |  |  | 1 | RESISTOR |
|  | - - - |  |  | - | mounting hardware: (not included w/resistor) |
| -8 | 211-0544-00 |  |  | 1 | SCREW, $6-32 \times 3 / 4$ inch, THS |
| -9 | 210-0478-00 |  |  | 1 | NUT, hex., alum. $5 / 16 \times{ }^{21 / 32}$ inch long |
|  | 211-0507-00 |  |  | 1 | SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -10 | 136-0181-00 | $\begin{aligned} & 100 \\ & 2010 \end{aligned}$ | 2009 | 21 | SOCKET, transistor, 3 pin |
|  | 136-0181-00 |  |  | 20 | SOCKET, transistor, 3 pin |
|  | - - - - |  |  |  | mounting hardware for each: (not included w/socket) |
| -11 | 354-0234-00 |  |  | 1 | RING, socket mounting |
| -12 | - - - - |  |  | 2 | COIL |
|  | - - - |  |  | - | mounting hardware for each: (not included w/coil) |
| -13 | 407-0236-01 |  |  | 1 | BRACKET, plastic, coil mounting |
|  | 212-0004-00 |  |  | 1 | SCREW, $8.32 \times 5 / 1.6$ inch, PHS |
| $\begin{aligned} & -14 \\ & -15 \end{aligned}$ | 200-0642-00 |  |  | 2 | CAP, $1 / 4$ inch |
|  | - - |  |  | 1 | CAPACITOR |
|  | - - - |  |  | - | mounting hardware: (not included w/capacitor) |
| $\begin{aligned} & -16 \\ & -17 \end{aligned}$ | 386-0255-00 |  |  | 1 | PLATE, flange, metal, capacitor mounting |
|  | 211-0534-00 |  |  | 2 | SCREW, sems, $6-32 \times 5 / 16$ inch, PHS |
|  | 210-0457-00 |  |  | 2 | NUT, keps, $6-32 \times 5 / 16$ inch |
| -18 | 337-0813-00 |  |  | 1 | SHIELD |
|  | --- |  |  | - | mounting hardware: (not included $\mathrm{w} /$ shield) |
|  | 210-0586-00 |  |  | 2 | NUT, keps, $4-40 \times 1 / 4$ inch |

## Mechanical Parts List-Type 556

FIG. 3 B SWEEP VERTICAL AMPLIFIER \& HIGH VOLTAGE (coni)

| Fig. \& Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Dise | $\begin{aligned} & Q \\ & t \\ & y \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 3-19 | 343-0002-00 |  | 1 | CLAMP, cable, $3 / 16$ inch, plastic |
|  | - - - - |  | - | mounting hardware: (not included w/clamp) |
| -20 | 211-0507-00 |  | 1 | SCREW, 6-32 $\times 5 / 16$ inch, PHS |
| -21 | 210-0863-00 |  | 1 | WASHER, D type |
|  | 210-0457-00 |  | 1 | NUT, keps, $6-32 \times 5 / 16$ inch |
| -22 | - - - - |  | 2 | RESISTOR, variable |
|  | - - - - |  | - | mounting hardware for each: (not included w/resistor) |
|  | 210-0207-00 |  | 1 | LUG, solder, $3 / 8$ ID $\times 5 / 8$ inch OD, SE |
|  | 210-0012-00 |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0840-00 |  | 1 | WASHER, flat, $0.390 \mathrm{ID} \times 9 / 16$ inch OD |
|  | 210-0413-00 |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| -23 | - - - - |  | 3 | RESISTOR, variable |
|  | - |  | - | mounting hardware for each: (not included w/resistor) |
|  | 210-0840-00 |  | 1 | WASHER, flat, 0.390 ID $\times 9 / 16$ inch OD |
|  | 210-0413-00 |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
|  | 210-0255-00 |  | 1 | LUG, solder, $3 / 8$ ID $\times 0.500$ inch OD |
| -24 | 136-0158-00 |  | 2 | SOCKET, tube, 12 pin, w/ground lugs |
|  | - - - |  | - | mounting hardware for each: (not included w/socket) |
| -25 | 213-0044-00 |  | 2 | SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -26 | 210-0201-00 |  | 12 | LUG, solder, SE \#4 |
|  | $213-0044-00$ |  | $1$ | mounting hardware for each: (not included w/lug) SCREW, thread forming, $5.32 \times 3 / 16$ inch, PHS |
| -27 | 210-0204-00 |  | 4 | LUG, solder, DE \#6 |
|  | -- |  | - | mounting hardware for each: (not included w/lug) |
|  | 213-0044-00 |  | 1 | SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -28 | - - - - |  | 2 | CAPACITOR |
|  | ---- |  | 1 | mounting hardware for each: (not included w/capacitor) |
| -29 | $\begin{aligned} & 384-0542-00 \\ & 211-0507-00 \end{aligned}$ |  | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | ROD, plastic, $5 / 16$ dia $\times 1$ inch long SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -30 | 136-0174-00 |  | 2 | SOCKET, tube, 9 pin, w/ground lugs |
|  | --- |  | - | mounting hardware for each: (not included w/socket) |
|  | 213-0044-00 |  | 2 | SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -31 | 136-0015-00 |  | 9 | SOCKET, tube, 9 pin, w/ground lugs |
|  | - - - |  | - | mounting hardware for each: (not included w/socket) |
| -32 | 213-0044-00 |  | 2 | SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |

FIG. 3 B SWEEP VERTICAL AMPLIFIER \& HIGH VOLTAGE (cont)

| Fig. \& Index No. | Tektronix <br> Part No. |  | Serial/Model No. Eff Disc | $\begin{aligned} & \mathrm{Q} \\ & \mathbf{t} \\ & \mathrm{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3-33 | $\begin{aligned} & 136-0008-00 \\ & \hdashline \cdots \\ & 213-0044-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 2 \\ & 2 \end{aligned}$ | SOCKET, tube, 7 pin, w/ground lugs mounting hardware: (not included w/socket) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -34 | $\begin{aligned} & 337-0005-00 \\ & -- \\ & 213-0044-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 2 \\ & 2 \end{aligned}$ | SHIELD, socket, STSI79 mounting hardware: (not included $\mathrm{w} /$ shield) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| $\begin{aligned} & -35 \\ & -36 \\ & -37 \\ & -38 \\ & -39 \\ & -40 \end{aligned}$ | $\begin{aligned} & 337-0008-00 \\ & 348-0050-00 \\ & 348-0056-00 \\ & 348-0031-00 \\ & 348-0055-00 \\ & 385-0151-00 \\ & \hdashline--- \\ & 211-0507-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 2 \\ & 1 \\ & 6 \\ & 2 \\ & 2 \\ & - \\ & \hline \end{aligned}$ | SHIELD, $1 \frac{1 / 32}{}$ ID $\times 2^{13 / 32}$ inches $h$, $w /$ spring GROMMET, plastic, $3 / 4$ inch diameter GROMMET, plastic, $3 / 8$ inch diameter GROMMET, plastic, $5 / 32$ inch diameter GROMMET, plastic, $1 / 4$ inch diameter ROD, plastic, $5 / 16 \times 29 / 16$ inches long mounting hardware for each: (not included w/rod) SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -41 | $\begin{aligned} & 385-0168-00 \\ & \hdashline-- \\ & 210-0006-00 \\ & 211-0507-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & \vdots \\ & 1 \\ & 1 \end{aligned}$ | ROD, spacer, $1 / 4$ hex., $\times 1.168$ inches long mounting hardware: (not included w/rod) LOCKWASHER, internal, \#6 SCREW, $6-32 \times 5 / 1 s$ inch, PHS |
| -42 | $\begin{aligned} & 385-0138-00 \\ & 385-0137-00 \\ & \hdashline--- \\ & 213-0041-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 117 \end{aligned}$ | 116 | $\begin{aligned} & 1 \\ & 1 \\ & - \\ & \hline \end{aligned}$ | ROD, plastic, $19 / 16$ inches long ROD, plastic, $21 / 4$ inches long mounting hardware: (not included $w /$ rod) SCREW, thread cutting, $6-32 \times 3 / 8$ inch, PHS |
| -43 | $\begin{aligned} & 337-0812-00 \\ & --- \\ & 210-0457-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | SHIELD, top half mounting hardware: (not included w/shield) NUT, keps, $6-32 \times 5 / 16$ inch |
| -44 -45 | $\begin{aligned} & 337-0789-00 \\ & ---- \\ & 211-0007-00 \\ & 210-0457-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & - \\ & 2 \\ & 2 \end{aligned}$ | SHIELD, bottom half mounting hardware: (not included w/shield) SCREW, $4-40 \times 3 / 16$ inch, PHS NUT, keps, $6-32 \times 5 / 16$ inch |
| -46 | $\begin{aligned} & 210-0940-00 \\ & 210-0583-00 \end{aligned}$ |  |  | 3 1 1 | RESISTOR, variable WASHER, flat, $1 / 4$ ID $\times 3 / 8$ inch OD NUT, hex., $1 / 4-32 \times 5 / 16$ inch |
| -47 | $\begin{aligned} & 337-0791-00 \\ & 210-0457-00 \end{aligned}$ |  |  | 1 5 | SHIELD, high voltage mounting hardware: (not included w/shield) NUT, keps, $6-32 \times 5 / 16$ inch |
| -48 -49 | $\begin{gathered} 200-0644-00 \\ 211-0097-00 \end{gathered}$ |  |  | 1 4 | COVER, high voltage mounting hardware: (not included w/cover) SCREW, $4-40 \times 5 / 16$ inch, PHS |

## Mechanical Parts List-Type 556

FIG. 3 B SWEEP VERTICAL AMPLIFIER \& HIGH VOLTAGE (cont)

| Fig. \& Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Disc | $\begin{aligned} & Q \\ & \dagger \\ & y \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 3-50 | $\begin{aligned} & 441-0660-00 \\ & \cdots- \\ & 212-0004-00 \\ & 212-0040-00 \end{aligned}$ |  | $\begin{aligned} & 1 \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | CHASSIS, vertical amplifier " B " mounting hardware: (not included w/chassis) SCREW, $8-32 \times 5 / 16$ inch, PHS SCREW, $8-32 \times 3 / 8$ inch, FHS |
| $\begin{aligned} & -51 \\ & -52 \\ & -53 \end{aligned}$ | $348-0063-00$ $348-0056-00$ $-\cdots-\cdots$ $-\cdots-\cdots$ $210-0840-00$ $210-0413-00$ $210-0207-00$ |  | $\begin{aligned} & 1 \\ & 3 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | GROMMET, plastic, $1 / 2$ inch diameter GROMMET, plastic, $3 / 8$ inch diameter RESISTOR, variable mounting hardware: (not included w/resistor) WASHER, flat, $0.390 \mathrm{ID} \times \% / 16$ inch $O D$ NUT, hex., $3 / 8-32 \times 1 / 2$ inch LUG, solder, $3 / 8$ inch ID |
| -54 | $\begin{aligned} & 210-0201-00 \\ & \hdashline 213-0044-00 \end{aligned}$ |  | $\begin{aligned} & 5 \\ & i \end{aligned}$ | LUG, solder, SE \#4 mounting hardware for each: (not included w/lug) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -55 -56 | $\begin{gathered} 210-0204-00 \\ \hdashline- \\ 213-0044-00 \end{gathered}$ |  | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | LUG, solder, DE \#6 mounting hardware: (not included w/lug) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| $\begin{aligned} & -57 \\ & -58 \end{aligned}$ | $\begin{aligned} & 252-0564-00 \\ & 136-0015-00 \\ & ---0 \\ & 213-0044-00 \end{aligned}$ |  | $\begin{gathered} \mathrm{ft} . \\ 1 \\ \hline 2 \end{gathered}$ | PLASTIC, extruded channel (specify $3 / 8$ inches long) SOCKET, tube, 9 pin, w/ground lugs mounting hardware: (not included w/socket) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -59 | $\begin{aligned} & 136-0181-00 \\ & \hdashline-- \\ & 354-0234-00 \end{aligned}$ |  | $\begin{array}{r} 10 \\ 7 \end{array}$ | SOCKET, transistor, 3 pin mounting hardware for each: (not included w/socket) RING, socket mounting |
| -60 | $\begin{aligned} & 385-0168-00 \\ & \hdashline-0-0 \\ & 210-0006-00 \\ & 211-0507-00 \end{aligned}$ |  | $\begin{aligned} & 1 \\ & \vdots \\ & 1 \end{aligned}$ | ROD, spacer, $1 / 4$ hex., $\times 1.168$ inches long mounting hardware: (not included $\mathrm{w} / \mathrm{rod}$ ) LOCKWASHER, internal, \#6 SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -61 -62 | $214-0153-00$ |  | 1 1 | CAPACITOR <br> mounting hardware: (not included w/capacitor) FASTENER, snap in, plastic |
| -63 -64 -65 -66 | $\begin{aligned} & 432-0048-00 \\ & 386-0255-00 \\ & 211-0516-00 \\ & 210-0457-00 \end{aligned}$ |  | 1 - 1 2 2 | CAPACITOR <br> mounting hardware: (not included w/capacitor) BASE, plastic, capacitor mounting PLATE, metal, capacitor mounting SCREW, $6-32 \times 7 / 8$ inch, PHS NUT, keps, $6-32 \times 5 / 16$ inch |

Fig. 3 B SWEEP VERTICAL AMPLIFIER \& HIGH VOltage (cont)

| Fig. \& Index No. | Tektronix Part No. |  | Serial/Model Eff | No. Dise | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3-67 | - |  |  |  | 1 | CAPACITOR |
|  |  |  |  |  |  | mounting hardware: (not included w/capacitor) |
| -68 | 432-0047-00 |  |  |  | 1 | BASE, plastic, capacitor mounting |
|  | 386-0252-00 |  |  |  | 1 | PLATE, fiber, capacitor mounting |
|  | 211-0516.00 |  |  |  | 2 | SCREW, $6-32 \times 7 /$ inch, PHS |
|  | 210-0457-00 |  |  |  | 2 | NUT, keps, $6-32 \times 5 / 1 \mathrm{~s}$ inch |
| $\begin{aligned} & -70 \\ & -71 \end{aligned}$ | 200-0533-00 |  |  |  | 1 | COVER, capacitor, 1 ID $\times 0.750$ inches long |
|  | 344-0116-00 |  |  |  | 1 | CLIP, capacitor mounting |
|  |  |  |  |  | - | mounting hardware: (not included w/clip) |
|  | 213-0044-00 |  |  |  | 1 | SCREW, thread forming, $5-32 \times 3 / 16$ inch |
| . 72 | -...- |  |  |  | 2 | COIL |
|  | - - - - |  |  |  | - | mounting hardware for each: (not included w/coil) |
|  | 213-0044-00 |  |  |  | 1 | SCREW, thread forming, $5-32 \times 3 / 16$ inch |
| -73 | 119-0069-00 |  |  |  | 1 | ASSEMBLY, delay line |
|  | --- |  |  |  |  | assembly includes: |
| .74.75.76 | 131-0271-00 |  |  |  | 2 | CONNECTOR, cable termination |
|  | 380-0049-00 |  |  |  | 1 | HOUSING, delay line |
|  | $200-0482-00$ $200-0482-06$ | 100 | 2009 |  | 1 | COVER, delay line COVER, delay line |
| -76 | 200-0482-06 | 2010 |  |  | 1 | COVER, delay line mounting hardware: (not included w/cover) |
| . 77 | 211.0514 .00 |  |  |  | 3 | mounting hardware: (not included w/cover) SCREW, $6-32 \times 3 / 4$ inch, PHS |
|  | 210-0407-00 |  |  |  | 3 | NUT, hex., $6-32 \times 1 / 4$ inch |
|  |  |  |  |  |  | mounting hardware: (not included w/assembly) |
| $\begin{aligned} & -78 \\ & -79 \end{aligned}$ | 211.0516 .00 |  |  |  | 2 | SCREW, $6-32 \times 7 / 8$ inch, PHS |
|  | 385-0018-00 |  |  |  | 2 | ROD, plastic, $5 / 16 \times 1 / 4$ inches long |
|  | 211-0507-00 |  |  |  | 2 | SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -80.81 | 211-0510-00 |  |  |  | 1 | SCREW, $6-32 \times 3 / 8$ inch, PHS |
|  | 392-0147-00 |  |  |  | 1 | ASSEMBLY, High Voltage board |
| -82 | 124-0162-00 |  |  |  | $i$ | assembly includes: STRIP, ceramic, $7 / 16$ inch $h$, w/4 notches |
|  | $\cdots$ |  |  |  | ; | strip includes: |
| -83 | 355-0046-00 |  |  |  | 1 | STUD, plastic |
|  |  |  |  |  |  | mounting hardware: (not included w/strip alone) |
| -84 | 361-0007-00 |  |  |  | 1 | SPACER, plastic, 0.156 inch long |
|  | 346-0032-00 |  |  |  | 1 | STRAP, rubber, 0.075 dia $\times 4$ inches long |
| $\begin{aligned} & -85 \\ & -86 \end{aligned}$ | 124-0164-00 |  |  |  | 2 | STRIP, ceramic, 0.437 inch $h$, w/4 notches |
|  | 124-0163-00 |  |  |  | 5 | STRIP, ceramic, 0.437 inch $h$, w/2 notches |
|  | 211-0507-00 |  |  |  | ; | mounting hardware: (not included w/assembly) SCREW, $6.32 \times 5 / 16$ inch, PHS |

## Mechanical Parts List-Type 556

FIG. 3 B SWEEP VERTICAL AMPLIFIER \& HIGH VOLTAGE (cont)

| Fig. \& Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Nisc }}{\text { No. }}$ | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3-87 | - - - - |  |  | 1 | CAPACITOR |
|  | - . . . - |  |  | - | mounting hardware: (not included w/capacitor) |
| -88 | 211-0587-00 |  |  | 1 | SCREW, $6.32 \times 3 / 16$ inch, HHS |
| -89 | 210-0261-00 |  |  | 2 | LUG, solder, high voltage |
|  | 210-0966-00 |  |  | 2 | WASHER, rubber, $7 / 16 \mathrm{ID} \times 7 / 8$ inch OD |
| -90 | 211-0542-00 |  |  | , | SCREW, $6-32 \times 5 / 16$ inch, THS |
| -91 | - - - - |  |  | 1 | TRANSFORMER |
|  | . - . - - |  |  | - | mounting hardware: (not included w/transformer) |
| -92 | 211-0521-00 |  |  | 2 | SCREW, $6.32 \times 11 / 2$ inches, RHS |
| -93 | $210-0869-00$ |  |  | 2 | WASHER, plastic, $5 / 32$ ID $\times 3 / 8$ inch OD |
| -94 | 200-0475-00 |  |  | 1 | COVER, high voltage box |
| -95 | 337-0814-00 |  |  | 1 | SHIELD, high voltage |
|  | - - - |  |  | - | mounting hardware: (not included $\mathrm{w} /$ shield) |
| -96 | 211-0530-00 |  |  | 2 | SCREW, $6.32 \times 13 / 4$ inches, PHS |
| -97 | 214-0716-00 |  |  | 2 | WASHER, plastic, insulating |
| -98 | 166-0357-00 |  |  | 1 | SLEEVE, plastic, anode lead |
| -99 | 166-0319-00 |  |  | 2 | SLEEVE, plastic, w/o hole |
| -100 | 380-0048-00 |  |  | 1 | HOUSING, high voltage box |
|  | - - |  |  | - | mounting hardware: (not included w/housing) |
|  | 211-0507-00 |  |  | 2 | SCREW, $6-32 \times 5 / 16$ inch, PHS |
|  | 211-0542-00 |  |  | 1 | SCREW, $6-32 \times 5 / 16$ inch, THS |
|  | 210-0006-00 | X270 |  | 1 | LOCKWASHER, internal, \#6 |
| $\begin{aligned} & -101 \\ & -102 \\ & -103 \end{aligned}$ | 179-1070-00 |  |  |  |  |
|  | 179-1071-00 |  |  | 1 | CABLE HARNESS, high voltage \#2 |
|  | 214-0210-00 |  |  | 1 | ASSEMBLY, solder spool |
|  | - - . - |  |  | - | assembly includes: |
|  | 214-0209-00 |  |  | 1 | SPOOL, w/o solder |
|  | - .-. - |  |  | - | mounting hardware: (not included w/assembly) |
|  | 361-0007-00 |  |  | 1 | SPACER, plastic, 0.188 inch long |
| -104 | 179-1055-00 | $100$ | 2009 | 1 | CABLE HARNESS, "B" sweep CABLE HARNESS, "B" SWEEP |
|  | 179-1055-01 $179-1068-00$ | $2010$ |  | 1 | CABLE HARNESS, "B" SWEEP <br> CABIE HARNESS, "B" sweep high voltage |
| -106 | $179-1068-00$ $124-0145-00$ |  |  | 11 | CABLE HARNESS, "B" sweep high voltage STRIP, ceramic, $7 / 16$ inch $\mathrm{h}, \mathrm{w} / 20$ notches |
|  | ...... |  |  | - | each strip includes: |
|  | 355-0046-00 |  |  | 2 | STUD, plastic |
|  | - - |  |  | - | mounting hardware for each: (not included w/strip) |
|  | 361-0009-00 |  |  | 2 | SPACER, plastic, 0.406 inch long |
| -107 | 124-0146-00 |  |  | 14 | STRIP, ceramic, $7 / 16$ inch $\mathrm{h}, \mathrm{w} / 16$ notches |
|  | - - - |  |  | - | each strip includes: |
|  | 355-0046-00 |  |  | 2 | STUD, plastic |
|  | --- |  |  | 2 | mounting hardware for each: (not included w/strip) |
|  | 361-0009-00 |  |  | 2 | SPACER, plastic, 0.406 inch long |

FIG. 3 B SWEEP VERTICAL AMPLIFIER \& HIGH VOLTAGE (cont)

| Fig. \& Index No. | Tektronix Part No. | Serial/Model Eff No. Dise | $\begin{gathered} Q \\ \mathbf{t} \\ \mathbf{y} \\ \hline \end{gathered}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 3-108 | 124-0162-00 |  | 1 | STRIP, ceramic, $7 / 16$ inch $h$, w/4 notches |
|  | - - - |  | - | strip includes: |
|  | 355-0046-00 |  | 2 | STUD, plastic |
|  | . - - . |  | - | mounting hardware: (not included w/strip) |
|  | 361-0009-00 |  | 2 | SPACER, plastic, 0.406 inch long |
| -109 | 124-0149-00 |  | 2 | STRIP, ceramic, $7 / 16$ inch $h$, w/7 notches |
|  | - - - - |  | - | each strip includes: |
|  | 355-0046-00 |  | 2 | STUD, plastic |
|  | - - - |  | - | mounting hardware for each: (not included w/strip) |
|  | 361-0009-00 |  | 2 | SPACER, plastic, 0.406 inch long |
| -110 | 124-0147-00 |  | 1 | STRIP, ceramic, $7 / 1{ }^{\text {c }}$ inch $h, w / 13$ notches |
|  | - -- |  | - | strip includes: |
|  | 355-0046-00 |  | 2 | STUD, plastic |
|  | - - - - |  | - | mounting hardware: (not included w/strip) |
|  | 361-0009-00 |  | 2 | SPACER, plastic, 0.406 inch long |
| -111 | 124-0147-00 |  | 2 | STRIP, ceramic, $7 / 16$ inch $h, w / 13$ notches |
|  | - - - |  | - | each strip includes: |
|  | 355-0046-00 |  | 2 | STUD, plastic |
|  | - . - - |  | - | mounting hardware for each: (not included w/strip) |
|  | 361-0007-00 |  | 2 | SPACER, plastic, 0.188 inch long |
| -112 |  |  |  |  |
|  | ․ . . - |  | - | strip includes: |
|  | 355-0046-00 |  | 2 | STUD, plastic |
|  | - . - |  | - | mounting hardware: (not included w/strip) |
|  | 361-0009-00 |  | 2 | SPACER, plastic, 0.406 inch long |
| -113 | 124-0089-00 |  | 4 | STRIP, ceramic, $3 / 4$ inch $h$, w/7 notches |
|  | - - - - |  | - | each strip includes: |
|  | 355-0046-00 |  | 2 | STUD, plastic |
|  | - - - - |  | - | mounting hardware for each: (not included w/strip) |
|  | 361-0009-00 |  | 2 | SPACER, plastic, 0.406 inch long |
| $\begin{aligned} & -114 \\ & -115 \\ & -116 \\ & -117 \end{aligned}$ | 179-1062-00 |  | 1 | CABLE HARNESS, right vertical amplifier |
|  | 179-1064-00 |  | 1 | CABLE HARNESS, coaxial \#1 |
|  | 179-1065-00 |  | 1 | CABLE HARNESS, coaxial \#2 |
|  | 124-0145-00 |  | 2 | STRIP, ceramic, $7 / 1$ is inch $h$, w/20 notches |
|  | ---. |  | - | each strip includes: |
|  | 355-0046-00 |  | 2 | STUD, plastic |
|  | ---- |  |  | mounting hardware for each: (not included w/strip) |
|  | 361-0009-00 |  | 2 | SPACER, plastic, 0.406 inch long |

## Mechanical Parts List-Type 556

FIG. 3 B SWEEP VERTICAL AMPLIFIER \& HIGH VOLTAGE (cont)

| Fig. \& Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Dise | $\begin{gathered} Q \\ t \\ y \\ \hline \end{gathered}$ | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3-118 | $\begin{gathered} 124-0147-00 \\ \hdashline 355-0046-00 \\ \hdashline 361-0009-00 \end{gathered}$ |  |  | $\begin{aligned} & 6 \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | STRIP, ceramic, $7 / 16$ inch $h, w / 13$ notches each strip includes: <br> STUD, plastic <br> mounting hardware for each: (not included w/strip) SPACER, plastic, 0.406 inch long |
| -119 | $\begin{aligned} & 385-0138-00 \\ & \hdashline--- \\ & 213-0041-00 \end{aligned}$ | X117 |  | $\begin{aligned} & 1 \\ & \vdots \end{aligned}$ | ROD, plastic, $19 / 16$ inches long mounting hardware: (not included $w /$ rod) SCREW, thread cutting, $6-32 \times 3 / 8$ inch, THS |
| -120 | $\begin{aligned} & 670-0514-00 \\ & --- \\ & 388-0822-00 \\ & 136-0220-00 \end{aligned}$ |  |  | 1 1 1 | ASSEMBLY, circuit board, high voltage delay assembly includes: <br> BOARD, circuit <br> SOCKET, transistor, 3 pin |

FIG. 4 CAPACITOR MOUNTING CHASSIS \& TRANSFORMER

| Fig. \& Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 4-1 | $\begin{aligned} & 441-0654-00 \\ & ---- \\ & 212-0004-00 \end{aligned}$ |  | $\begin{array}{r} 1 \\ 12 \end{array}$ | CHASSIS, capacitor mounting mounting hardware: (not included w/chassis) SCREW, $8-32 \times 5 / 16$ inch, PHS |
| $\begin{aligned} & -2 \\ & -3 \end{aligned}$ | $\begin{aligned} & 343-0089-00 \\ & 352-0025-00 \\ & \hdashline--- \\ & 213-0146-00 \end{aligned}$ |  | $\begin{aligned} & 3 \\ & 2 \\ & 2 \\ & 2 \end{aligned}$ | CLAMP, plastic, snap-in <br> HOLDER, fuse, dual 3AG <br> mounting hardware for each: (not included w/holder) SCREW, thread forming, $6-32 \times 5 / 16$ inch, PHS |
| -4 -5 | $213-0044-00$ |  | 1 2 | THERMAL CUTOUT mounting hardware: (not included w/thermal cutout) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -6 -7 -8 -9 -10 | $\begin{aligned} & 348-0050-00 \\ & 348-0063-00 \\ & \cdots \cdots \\ & \hdashline \cdots \\ & 407-0270-00 \\ & 210-0006-00 \\ & 210-0407-00 \end{aligned}$ |  | 1 <br> 1 <br> 1 | GROMMET, plastic, $3 / 4$ inch diameter GROMMET, plastic, $1 / 2$ inch diameter CAPACITOR <br> mounting hardware: (not included w/capacitor) BRACKET, capacitor mounting LOCKWASHER, internal, \#6 NUT, hex., $6-32 \times 1 / 4$ inch |
| $\begin{aligned} & -11 \\ & -12 \\ & -13 \\ & -14 \end{aligned}$ | $\begin{aligned} & 432-0048-00 \\ & 386-0254-00 \\ & 211-0588-00 \\ & 210-0457-00 \end{aligned}$ |  | 2 - 1 1 2 2 | CAPACITOR <br> mounting hardware for each: (not included w/capacitor) BASE, plastic, capacitor mounting PLATE, fiber, capacitor mounting SCREW, $6-32 \times 3 / 4$ inch, HHS NUT, keps, $6-32 \times 5 / 16$ inch |
| $\begin{aligned} & -15 \\ & -16 \\ & -17 \end{aligned}$ | $\begin{gathered} -\cdots- \\ -\cdots--- \\ 432-0048-00 \\ 386-0255-00 \\ 211-0588-00 \\ 210-0457-00 \end{gathered}$ |  | 2 - 1 1 2 2 | CAPACITOR <br> mounting hardware for each: (not included w/capacitor) BASE, plastic, capacitor mounting PLATE, metal, capacitor mounting SCREW, $6-32 \times 3 / 4$ inch, HHS NUT, keps, $6-32 \times 5 / 16$ inch |
| -18 -19 | $\begin{aligned} & 386-0254-00 \\ & 211-0543-00 \\ & 210-0457-00 \end{aligned}$ |  | 1 - 1 2 2 | CAPACITOR <br> mounting hardware: (not included w/capacitor) PLATE, fiber, capacitor mounting SCREW, $6-32 \times 5 / 16$ inch, RHS NUT, keps, $6-32 \times 5 / 16$ inch |

## Mechanical Parts Lisi-Type 556

FIG. 4 CAPACITOR MOUNTING CHASSIS \& TRANSFORMER (cont)

| Fig. \& Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\substack{\text { Serial/Model } \\ \text { No. } \\ \text { Disc }}}$ | $\begin{aligned} & Q \\ & t \\ & y \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 4-20 | 200-0293-00 |  |  | 2 | COVER, plastic, capacitor, $29 / 16$ inches long |
| -21 | 200-0259-00 |  |  | 1 | COVER, plastic, capacitor, $39 / 16$ inches long |
| -22 | 670-0430-00 | 100 | 829 | 1 | ASSEMBLY, circuit board |
|  | 670-0430-02 | 830 | 2009 | 1 | ASSEMBLY, circuit board |
|  | 670-0430-01 | 2010 |  | 1 | ASSEMBLY, circuit board |
|  | - . - |  |  |  | assembly includes: |
|  | 388-0691-00 | 100 | 2009 | 1 | BOARD, circuit, power |
|  | - - |  |  | - | board includes: |
| -23 | 214-0506-00 |  |  | 129 | CONNECTOR, square pin |
|  | 337-0607-00 |  |  | 1 | SHIELD |
|  | 388-0691-01 | 2010 |  | 1 | BOARD, circuit |
|  | 214-0506-00 | 2010 |  | 129 | CONNECTOR, square pin |
|  | 337-0607-00 | 2010 |  | 1 | SHIELD |
|  | - - - - |  |  | - | mounting hardware: (not included w/assembly) |
| -24 | 211-0601-00 |  |  | 4 | SCREW, sems, $6-32 \times 5 / 16$ inch, PHB |
| -25 | 129-0088-00 |  |  | 4 | POST, hex., 0.250 dia $\times 0.700$ inch long |
| -26 | 210-0006-00 |  |  | 3 | LOCKWASHER, internal, \#6 |
|  | 210-0202-00 |  |  | 1 | LUG, solder, SE \#6, w/2 wire holes |
| -27 | 407-0210-00 |  |  | 1 | BRACKET, transformer mounting (right) |
|  | - |  |  | - | mounting hardware: (not included w/bracket) |
|  | 212-0004-00 |  |  | 5 | SCREW, $8-32 \times 5 / 16$ inch, PHS |
| -28 | 407-0209-00 |  |  | 1 | BRACKET, transformer mounting (left) |
|  | -- |  |  | 5 | mounting hardware: (not included w/bracket) |
|  | 212-0004-00 |  |  | 5 | SCREW, $8-32 \times 5 / 16$ inch, PHS |
| -29 | 210-0201-00 |  |  | 1 | LUG, solder, SE \# 4, w/2 wire holes |
|  | -- |  |  | 1 | mounting hardware: (not included w/lug) |
|  | 213-0044-00 |  |  | 1 | SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
| -30 | 129-0089-00 |  |  | 2 | POST, hex., 0.250 dia $\times 0.830$ inch long |
|  | ---- |  |  | 1 | mounting hardware for each: (not included w/post) |
|  | 210-0006-00 |  |  | 1 | LOCKWASHER, internal, \#6 |
| -31 | 337-0817-01 |  |  | 1 | SHIELD, transformer |
| -32 | 348-0056-00 |  |  | 1 | GROMMET, plastic, $3 / 8$ inch diameter |
|  | 348-0050-00 |  |  | 1 | GROMMET, plastic, $3 / 4$ inch diameter |
| -34 | 337-0816-01 |  |  | 1 | SHIELD, transformer |
| -35 | - . - . |  |  | 1 | TRANSFORMER |
|  | - - - - - |  |  | - | mounting hardware: (not included w/transformer) |
|  | 212-0509-00 |  |  | 4 | SCREW, $10-32 \times 5 / 8$ inch, PHS |
|  | 220-0410-00 |  |  | 4 | NUT, keps, $10-32 \times 5 / 16$ inch |
| -36 | 179-1057-00 | 100 | 2009 | 1 | CABLE HARNESS, capacitor chassis |
|  | 179-1057-01 | 2010 |  | 1 | CABLE HARNESS, capacitor chassis |
| -37 | 179-1058-00 | 100 | 2009 | 1 | CABLE HARNESS, transformer \#1 |
|  | 179-1058-01 | 2010 |  | 1 | CABLE HARNESS, transformer \#1 |
| -38 | 179-1059-00 |  |  | 1 | CABLE HARNESS, transformer \#2 |
| -39 | 348-0056-00 |  |  | 2 | GROMMET, plastic, $3 / 8$ inch diameter |

FIG. 5 POWER CHASSIS \& PLUG-IN HOUSING

| Fig. \& Index No. | Tektronix Part No. |  | Serial/Model Eff No. Disc | Q t Y | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 5-1 | 441-0657-00 | $\begin{aligned} & 100 \\ & 2010 \end{aligned}$ | 2009 | 1 | CHASSIS, power |
|  | 441-0657-01 |  |  | 1 | CHASSIS, power |
|  | - . - - - |  |  | - | chassis includes: |
| -2 | 214-0329-00 |  |  | 2 | FASTENER, screw, retractable |
|  | - - - - |  |  | - | mounting hardware: (not included w/chassis) |
| -3 | 214-0639-00 |  |  | 2 | HINGE, power chassis |
|  | 211-0507-00 |  |  | 4 | SCREW, $6-32 \times 5 / 16$ inch, PHS |
| -4 | - |  |  | 2 | RESISTOR, variable |
|  | ---. |  |  | - | mounting hardware for each: (not included w/resistor) |
| -5 | 210-0840-00 |  |  | 1 | WASHER, flat, $0.390 \mathrm{ID} \times 9 / 1 \mathrm{~s}$ inch OD |
| -6 | 210-0413-00 |  |  | 1 | NUT, hex., $3 / 8.32 \times 1 / 2$ inch |
| -7 | --- |  |  | 1 | RESISTOR, variable |
|  | $\cdots$ |  |  | - | mounting hardware: (not included w/resistor) |
|  | 210-0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0840-00 |  |  | 1 | WASHER, flat, 0.390 ID $\times 9 / 16$ inch OD |
|  | 210-0413-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| -8 | - - - - |  |  | 2 | RESISTOR, variable |
|  | ---- |  |  | - | mounting hardware for each: not included w/resistor) |
| -9 | 210-0207-00 |  |  | 1 | LUG, solder, $3 / 8 \mathrm{ID} \times 5 / 8$ inch OD, SE |
|  | 210-0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0840-00 |  |  | 1 | WASHER, flat, $0.390 \mathrm{ID} \times 9 / 18$ inch OD |
|  | 210-0413-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| -10 | - - - - |  |  | 1 | RESISTOR, variable |
|  | - - - - |  |  | - | mounting hardware: (not included w/resistor) |
| -11 | 210-0255-00 |  |  | 1 | LUG, solder, 3/8 ID $\times 0.500$ inch OD, SE |
| -12 | 210-0413-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| -13 | 348-0064-00 |  |  | 1 | GROMMET, plastic, 5/8 inch diameter |
| -14 | 348-0055-00 |  |  | 2 | GROMMET, plastic, $1 / 4$ inch diameter |
| -15 | 348-0031-00 |  |  | 7 | GROMMET, plastic, $5 / 32$ inch diameter |
| -16 | 136-0014-00 |  |  | 1 | SOCKET, tube, 9 pin |
|  | - - - - |  |  | - | mounting hardware: (not included w/socket) |
| -17 | 213-0044-00 |  |  | 2 | SCREW, thread forming, 5-32 $\times 3 / 16$ inch, PHS |
| -18 | 136-0236-00 |  |  | 1 | SOCKET, tube, 12 pin |
|  | ---- |  |  | - | mounting hardware: (not included w/socket) |
|  | 213-0044-00 |  |  | 2 | SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |

FIG. 5 POWER CHASSIS \& PLUG-IN HOUSING (cont)

\begin{tabular}{|c|c|c|c|c|c|}
\hline Fig. \& Index No. \& Tektronix Part No. \& \& $\underset{\text { Eff }}{\substack{\text { Serial/Model } \\ \text { No. } \\ \text { Disc }}}$ \& $$
\begin{aligned}
& \mathrm{Q} \\
& \mathrm{t} \\
& \mathrm{y} \\
& \hline
\end{aligned}
$$ \& $12345 \quad$ Description <br>
\hline 5-19 \& $$
\begin{aligned}
& 210-0201-00 \\
& \hdashline 213-0044-00
\end{aligned}
$$ \& \& \& $$
6
$$ \& LUG, solder, SE \#4 mounting hardware for each: (not included w/lug) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS <br>
\hline -20 \& $$
\begin{aligned}
& 210-0204-00 \\
& 213-0044-00
\end{aligned}
$$ \& \& \& $$
2
$$ \& LUG, solder, DE \#6 mounting hardware for each: (not included w/lug) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS <br>
\hline -21
-22 \& $$
\begin{gathered}
136-0181-00 \\
\hdashline 354-0234-00
\end{gathered}
$$ \& \& \& $$
\begin{array}{r}
12 \\
i
\end{array}
$$ \& SOCKET, transistor, 3 pin mounting hardware for each: (not included w/socket) RING, socket <br>
\hline -23 \& $$
\begin{aligned}
& 344-0124-00 \\
& 344-0124-00 \\
& 213-0055-00
\end{aligned}
$$ \& $$
\begin{aligned}
& 100 \\
& 2010
\end{aligned}
$$ \& 2009 \& $$
\begin{aligned}
& 2 \\
& 3 \\
& i
\end{aligned}
$$ \& CLAMP, capacitor mounting CLAMP, capacitor mounting mounting hardware for each: (not included w/clamp) SCREW, thread forming, $2-32 \times 3 / 16$ inch, PHS <br>
\hline -24 \& $$
\begin{aligned}
& 426-0121-00 \\
& 361-0007-00
\end{aligned}
$$ \& \& \& $$
\begin{aligned}
& 1 \\
& i
\end{aligned}
$$ \& HOLDER, toroid mounting hardware: (not included w/holder) SPACER, plastic, 0.188 inch long <br>
\hline -25
-26
-27 \& $$
\begin{aligned}
& 380-0092-00 \\
& \hdashline-\cdots \\
& 212-0004-00 \\
& 210-0458-00
\end{aligned}
$$ \& \& \& 3 \& HOUSING, left, outside mounting hardware: (not included w/housing) SCREW, $8-32 \times 5 / 16$ inch, PHS NUT, keps, $8-32 \times 11 / 32$ inch <br>
\hline -28 \& $$
\begin{aligned}
& 380-0091-00 \\
& \hdashline 211-0559-00 \\
& 21200040 \\
& 210-0458-00 \\
& \hline
\end{aligned}
$$ \& \& \& $$
\begin{aligned}
& 4 \\
& 1 \\
& 1
\end{aligned}
$$ \& HOUSING, left, inside mounting hardware: (not included w/housing) SCREW, $6-32 \times 3 / 8$ inch, FHS SCREW, $8-32 \times 5 / 16$ inch, PHS NUT, keps, $8.32 \times 1 / 32$ inch <br>
\hline -29
-30 \& $$
\begin{gathered}
386-1007-01 \\
\hdashline 211-0038-00
\end{gathered}
$$ \& \& \& 2 \& PLATE, electrical shield mounting hardware for each: (not included w/plate) SCREW, $4-40 \times 5 / 16$ inch, $100^{\circ}$ csk, FHS <br>
\hline -31

-32

-33 \& $$
\begin{aligned}
& 386-0249-00 \\
& \cdots 212-0011-00 \\
& 2120000 \\
& 210-0458-00
\end{aligned}
$$ \& \& \& 1

1
5
6 \& PLATE, bulkhead, left mounting hardware: (not included w/plate) SCREW, $8.32 \times 3 / 4$ inch, $100^{\circ}$ csk, FHS SCREW, $8.32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS NUT, keps, $8-32 \times 11 / 32$ inch <br>
\hline -34

-35 \& $$
\begin{gathered}
386-1004-00 \\
\hline 211-0541-00
\end{gathered}
$$ \& \& \& 2 \& PLATE, bulkhead cover mounting hardware for each: (not included w/plate) SCREW, $6-32 \times 1 / 4$ inch, $100^{\circ} \mathrm{csk}$, FHS <br>

\hline
\end{tabular}

FIG. 5 POWER CHASSIS \& PLUG-IN HOUSING (cont]

| Fig. \& Index No. | Tektronix Part No. |  |  | $\begin{aligned} & \mathrm{Q} \\ & \dagger \\ & \mathrm{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 5.36 | 131-0018-00 |  |  | 2 | CONNECTOR, 16 contact |
|  | - - - - |  |  | - | mounting hardware for each: (not included w/connector) |
| -37 | 211-0014-00 |  |  | 2 | SCREW, $4-40 \times 1 / 2$ inch, PHS |
| -38 | 166-0031-00 | 100 | 2099 | 2 | TUBE, spacer, $0.180 \mathrm{ID} \times 1 / 4 \mathrm{OD} \times 1 / 4$ inch long |
|  | 166-0030-00 | 2100 |  | 2 | TUBE, spacer, 0.180 ID $\times 1 / 4$ OD $\times 3 / 16$ inch long |
| -39 | 210-0586-00 |  |  | 2 | NUT, keps, $4-40 \times 1 / 4$ inch |
| -40 | 260-0601-00 |  |  | 2 | SWITCH, unwired-COMPENSATION |
|  | - - |  |  | - | mounting hardware for each: (not included w/switch) |
|  | 211-0504-00 |  |  | 2 | SCREW, $6-32 \times 1 / 4$ inch, PHS |
| -41 | 366-0271-00 |  |  | 2 | KNOB, plastic-COMPENSATION |
| -42 | 385-0138-00 |  |  | 2 |  |
|  |  |  |  | i | mounting hardware for each: (not included $w / \mathrm{rod}$ ) |
|  |  |  |  |  | SCREW, $6-32 \times 1 / 2$ inch, PHS |
| -43 | 343-0006-00 |  |  | 1 | CLAMP, cable, $1 / 2$ inch, plastic |
|  | - . - - |  |  | - | mounting hardware: (not included w/clamp) |
| -44 | 211-0559-00 |  |  | 1 | SCREW, $6-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| -45 | 210-0863-00 |  |  | 1 | WASHER, D type |
| -46 | 210-0457-00 |  |  | 1 | NUT, keps, $6.32 \times 5 / 16$ inch |
| -47 | 351-0058-00 |  |  | 8 | GUIDE, shoe, plastic, $827 / 32$ inches long |
| -48 | 380-0093-00 |  |  | 1 | HOUSING, right, outside |
|  | - - - |  |  | - | mounting hardware: (not included w/housing) |
| -49 | $212-0004-00$ |  |  | 3 | SCREW, $8-32 \times 5 / 16$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| -50 | 210-0458-00 |  |  | 3 | NUT, keps, $8-32 \times 1 / 32$ inch |
| - 51 | 380-0090-00 |  |  | 1 | HOUSING, right, inside |
|  | ----- |  |  | , | mounting hardware: (not included w/housing) |
|  | 211-0559-00 |  |  | 4 | SCREW, $6-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
|  | 212-0004-00 |  |  | 1 | SCREW, $8-32 \times 5 / 16$ inch, PHS |
|  | 210-0458-00 |  |  | 1 | NUT, keps, $8-32 \times 11 / 32$ inch |
| -52 | 386-0250-00 |  |  | 1 |  |
|  | --- - |  |  | 1 | mounting hardware: (not included w/plate) |
|  | 212-0011-00 |  |  | 1 | SCREW, $8-32 \times 3 / 4$ inch, $100^{\circ} \mathrm{csk}$, FHS |
|  | $212-0040-00$ $210-0458-00$ |  |  | 5 | SCREW, $8-32 \times 3 / 8$ inch, $100^{\circ}$ csk, FHS |
| -53 | 210-0458-00 |  |  | 6 | NUT, keps, $8-32 \times 11 / 32$ inch |
| -54 | 343-0002-00 |  |  | 1 | CLAMP, cable, $3 / 16$ inch, plastic |
|  | - --- |  |  | I | mounting hardware: (not included w/clamp) |
|  | 211-0559-00 |  |  | 1 | SCREW, $6-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
|  | 210-0863-00 |  |  | 1 | WASHER, D type |
|  | 210-0457-00 |  |  | 1 | NUT, keps, 6-32 $\times 5 / 16$ inch |

FIG. 5 POWER CHASSIS \& PLUG-IN HOUSING (cont)

| Fig. \& Index No. | Tektronix Part No. |  | Serial/Model Eff No. Disc | $\begin{aligned} & Q \\ & t \\ & y \\ & \hline \end{aligned}$ | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 5-55 | $\begin{aligned} & 386-0248-00 \\ & \cdots \\ & 211-0559-00 \\ & 210-0457-00 \end{aligned}$ |  |  | $\begin{aligned} & 1 \\ & 2 \\ & 2 \\ & 4 \end{aligned}$ | PLATE, bulkhead, top mounting hardware: (not included w/plate) SCREW, $6.32 \times 3 / 8$ inch NUT, keps, $6-32 \times 5 / 1$ inch |
| $\begin{aligned} & -56 \\ & -57 \\ & -58 \\ & -59 \end{aligned}$ | $\begin{aligned} & 343-0006-00 \\ & 212-0011-00 \\ & 210-0863-00 \\ & 210-0458-00 \end{aligned}$ |  |  | $\begin{aligned} & 2 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | CLAMP, cable, $1 / 2$ inch, plastic mounting hardware for each: (not included $\mathrm{w} /$ clamp) SCREW, $8-32 \times 3 / 4$ inch, $100^{\circ}$ csk, FHS WASHER, D type NUT, keps, $8-32 \times 11 / 32$ inch |
| $\begin{aligned} & -60 \\ & -61 \end{aligned}$ | $\begin{aligned} & 348-0050-00 \\ & 385-0034-00 \\ & \hdashline--- \\ & 213-0041-00 \end{aligned}$ |  |  | $\begin{aligned} & 2 \\ & 1 \\ & 1 \end{aligned}$ | GROMMET, plastic, $3 / 4$ inch diameter ROD, plastic, $5 / 16$ dia $\times 3 / 4$ inch long mounting hardware: (not included w/rod) SCREW, thread cutting, $6.32 \times 3 / 8$ inch, THS |
| -62 -63 | $\begin{aligned} & 179-1056-00 \\ & 179-1056-01 \\ & 124-0145-00 \\ & \cdots \\ & 355-0046-00 \\ & \cdots-\cdots \\ & 361-0008-00 \end{aligned}$ | $\begin{aligned} & 100 \\ & 2010 \end{aligned}$ | 2009 | $\begin{array}{r} 1 \\ 1 \\ 12 \\ \hline \\ 2 \\ \hline \end{array}$ | CABLE HARNESS, power <br> CABLE HARNESS, power <br> STRIP, ceramic, $7 / 15$ inch $h, w / 20$ notches each strip includes: <br> STUD, plastic <br> mounting hardware for each: (not included w/strip) SPACER, plastic, 0.281 inch long |
| -64 | $\begin{aligned} & 214-0147-00 \\ & --- \\ & 355-0046-00 \\ & \hdashline 361-0008-00 \end{aligned}$ |  |  | $\begin{aligned} & 4 \\ & - \\ & 2 \\ & 2 \end{aligned}$ | STRIP, ceramic, $7 / 16$ inch $h, w / 4$ notches each strip includes: <br> STUD, plastic <br> mounting hardware for each: (not included w/strip) SPACER, plastic, 0.281 inch long |

FIG. 6 FAN MOTOR \& HEAT SINK CHASSIS

| Fig. \& Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 6-1 | 147-0029-00 |  | 1 | MOTOR, fan, 115 Volt |
|  | - - - . - |  | - | mounting hardware: (not included w/motor) |
| -2 | 211-0529-00 |  | 4 | SCREW, $6-32 \times 1 \frac{1}{4}$ inches, PHS |
| -3 | 210-0949-00 |  | 2 | WASHER, flat, $9 / 64 \mathrm{ID} \times 1 / 2 \mathrm{OD}, 1 / 16$ inch thick |
| -4 | 210-0457-00 |  | 4 | NUT, keps, $6.32 \times 5 / 16$ inch |
| -5 | 386-1006-00 |  | 1 | PLATE, adapter, fan motor |
|  | - . - . - |  | - | mounting hardware: (not included w/plate) |
|  | 212-0010-00 |  | 4 | SCREW, $8-32 \times 5 / \mathrm{s}$ inch, PHS |
| -6 | 210-0458-00 |  | 3 | NUT, keps, $8.32 \times 11 / 32$ inch |
| -7 | 166-0098-00 |  | 1 | TUBE, spacing, $3 / 8 \mathrm{OD} \times 21 / 32$ inch long |
| -8 | 343-0002-00 |  |  |  |
|  | - - - |  | - | mounting hardware: (not included w/clamp) |
|  | 210-0863-00 |  | 1 | WASHER, D type |
|  | 212-0004-00 |  | 1 | SCREW, $8-32 \times 5 / 16$ inch, PHS |
| -9 | 426-0193-00 |  | 1 | MOUNT, fan motor |
|  | ---- |  | - | mounting hardware: (not included w/mount) |
| -10 | 212-0004-00 |  | 4 | SCREW, $8.32 \times 5 / 16$ inch, PHS |
| -11 | 380-0088-00 |  | 1 | HOUSING, fan \& heat sink |
|  | - - . . - |  | - | mounting hardware: (not included w/housing) |
| -12 | 212-0004-00 |  | 4 | SCREW, $8-32 \times 5 / 16$ inch, PHS |
| -13 | 210-0457-00 |  | 4 | NUT, keps, $6-32 \times 5 / 16$ inch |
| -14 | 369-0022-00 |  | 1 | FAN, blade |
| -15 | 348-0056-00 |  | 1 | GROMMET, plastic, $3 / 8$ inch diameter |
| -16 | 348-0063-00 |  | 1 | GROMMET, plastic, $1 / 2$ inch diameter |
| -17 | 214-0001-00 |  | 2 | HINGE, $11 / 2 \times 1$ inches |
|  | --- - |  | - | mounting hardware for each: (not included w/hinge) |
| -18 | 210-0457-00 |  | 2 | NUT, keps, $6-32 \times 5 / 16$ inch |
| -19 | 124-0088-00 |  | 1 | STRIP, ceramic, $3 / 4$ inch $h, w / 4$ notches |
|  | $\cdots$ |  | 2 | strip includes: |
| -20 | 355-0046-00 |  | 2 | STUD, plastic |
| -21 | - - - - |  | 2 | mounting hardware: (not included w/strip) SPACER, plastic, 0.406 inch long |
| -22 | 407-0208-00 |  | 1 | BRACKET, resistor mounting |
|  | $210-0458-00$ |  | 2 | mounting hardware: (not included w/bracket) NUT, keps, $8-32 \times 11 / 32$ inch |

FIG. 6 FAN MOTOR \& HEAT SINK CHASSIS (cont)


FIG. 6 FAN MOTOR \& HEAT SINK CHASSIS (cont)

| Fig. \& Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Disc | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6-39 | 378-0768-00 |  |  | 1 | SCREEN, filter |
|  | . . - . . - |  |  | - | mounting hardware: (not included w/screen) |
| -40 | 211-0097-00 |  |  | 4 | SCREW, 4-40 $\times 1 / 4$ inch, PHS |
| -41 | 210-0851-00 |  |  | 4 | WASHER, flat, 0.119 ID $\times 3 / 8$ inch OD |
| -42 | 384-0616-00 |  |  | 4 | ROD, spacer, hex., $1 / 4 \times 1.380$ inches long |
| -43 | 210-0004-00 |  |  | 4 | LOCKWASHER, internal, \#4 |
| -44 | 179-1060-00 | 100 | 2009 | 1 | CABLE HARNESS, heat sink |
|  | 179-1060-01 | 2010 |  | 1 | CABLE HARNESS, heat sink |
| -45 | 386-1309-00 | X2010 |  | 1 | BRACKET, screen support |
| -46 | - - - - |  |  | 3 | TRANSISTOR |
|  | - - - - |  |  | - | mounting hardware for each: (not included w/transistor) |
| -47 | 211-0514-00 | $\begin{aligned} & 100 \\ & 2010 \\ & \times 2010 \end{aligned}$ | 2009 | 2 | SCREW, $6-32 \times 3 / 4$ inch, PHS |
|  | 211-0514-00 |  |  | 1 | SCREW, $6.32 \times 3 / 4$ inch, PHS |
| -48 | 211-0516-00 |  |  | 1 | SCREW, $6.32 \times 7 / 8$ inch, PHS |
| -49 | 386-0978-00 |  |  | 1 | PLATE, mica, insulating |
|  | 214-0719-00 |  |  | 2 | INSULATOR, bushing |
|  | 210-0803-00 |  |  | 2 | WASHER, flat, $0.0150 \times 3 / 8$ inch OD |
|  | 210-0202-00 |  |  | 1 | LUG, solder, SE \#6 |
|  | 210-0457-00 |  |  | 2 | NUT, keps, $6.32 \times 5 / 16$ inch |
| -50 | 200-0692-00 |  |  | 1 | COVER, transistor |

FIG. 7 CRT SHIELD \& REAR

| Fig. \& Index No. | Tektronix Part No. |  | Serial/Model Eff | $\begin{aligned} & \mathrm{Q} \\ & \mathrm{t} \\ & \mathrm{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 7.1 | 337-0793-01 |  |  | 1 | SHIELD, cathode ray tube |
|  | - - - - |  |  | - | mounting hardware: (not included w/shield) |
|  | 211-0590-00 |  |  | 3 | SCREW, $6-32 \times 1 / 4$ inch, PHS |
|  | 407-0242-00 |  |  | 3 | BRACKET, angle, CRT shield mounting |
|  | 210-0457-00 |  |  | 3 | NUT, keps, $6-32 \times 5 / 16$ inch |
|  | 211-0101-00 |  |  | 3 | SCREW, $4-40 \times 1 / 4$ inch, FHS |
| -2 | 354-0204-00 |  |  | 1 | RING, plastic, CRT shockmount |
| -3 | 131-0435-00 |  |  | 1 | ASSEMBLY, anode connector |
|  | - - |  |  | - | assembly includes: |
| -4 | 200-0674-00 |  |  | 1 | COVER, anode connector |
| -5 | 175-0012-00 |  |  | ft . | CABLE, high voltage, insulated (specify 26 inch) |
| -6 | 131-0026-00 |  |  | 1 | CLIP, anode connector |
| -7 | - . - |  |  | 1 | LINE FILTER |
|  | - - - |  |  | - | mounting hardware: (not included w/line filter) |
| -8 | 211-0071-00 |  |  | 2 | SCREW, $4-40 \times 3 / 8$ inch, THS |
| -9 | 386-1009-00 | 100 | 2009 | 1 | PLATE, subpanel, rear |
|  | 386-1009-01 | 2010 |  | 1 | PLATE, subpanel, rear |
|  | - . - - |  |  | - | plate includes: |
|  | 354-0282-00 |  |  | 1 | RING, ornamental |
| -10 | 260-0784-00 |  |  | 1 | SWITCH, toggle-UPPER BEAM CHOPPED BLANKING |
|  | - - - |  |  | - | mounting hardware: (not included w/switch) |
|  | 354-0055-00 |  |  | 1 | RING, switch locking, $15 / 32$ ID $\times{ }^{23 / 32}$ inch OD |
|  | 210-0902-00 |  |  | 1 | WASHER, flat, 0.470 ID $\times 21 / 32$ inch OD |
|  | 210-0473-00 |  |  | 1 | NUT, 12 sided, $15 / 32-32 \times 5 / 64$ inch |
| -11 | 260-0784-00 |  |  | 1 |  |
|  | - . . - - |  |  | - | mounting hardware: (not included w/switch) |
|  | 354-0055-00 |  |  | 1 | RING, switch locking, $15 / 32 \mathrm{ID} \times 23 / 32$ inch OD |
| -12 | 210-0902-00 |  |  | 1 | WASHER, flat, $0.470 \mathrm{ID} \times 21 / 32$ inch OD |
| -13 | 210-0473-00 |  |  | 1 | NUT, 12 sided, $15 / 32-32 \times 5 / 64$ inch |
| -14 | $\begin{aligned} & 386-1010-00 \\ & 386-1010-01 \end{aligned}$ | $\begin{aligned} & 100 \\ & 2010 \end{aligned}$ | 2009 | 1 | PLATE, rear overlay PLATE, rear overlay |
|  | - - - - - |  |  | - | mounting hardware: (not included w/plate) |
|  | 213-0104-00 | 100 | 569 | 1 | SCREW, thread forming, $6-32 \times 3 / 8$ inch, THS |
|  | 213-0088-00 | 570 |  | 1 | SCREW, thread forming, $4-40 \times 1 / 4$ inch, PHS |
| . 15 | 179-1072-00 |  |  | 1 | CABLE HARNESS, CRT socket |
|  | - - - - - |  |  | - | cable harness includes: |
|  | 136-0240-00 |  |  | 1 | ASSEMBLY, CRT socket |
|  | - - - - |  |  | - | assembly includes: |
| -16 | 136-0202-01 |  |  | 1 | SOCKET, CRT |
|  | - - - - |  |  | - | socket includes: |
|  | 136-0202-00 |  |  | 1 | SOCKET, CRT |
|  | 214-0464-00 |  |  | 14 | PIN, CRT |
| -17 | 200-0616-00 |  |  | 1 | COVER, CRT socket |

FIG. 7 CRT SHIELD \& REAR (cont)


FIG. 7 CRT SHIELD \& REAR (cont)

| Fig. \& Index No. | Tektronix <br> Part No. |  | Serial/Mode Eff | No. Disc | Q | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7-35 | 378-0034-01 |  |  |  | 1 | FILTER, air, foam |
| -36 | 386-1012-00 |  |  |  | 1 | PLATE, baffle, filter housing |
|  | - . . . |  |  |  | - | mounting hardware: (not included w/plate) |
|  | 211-0542-00 |  |  |  | 2 | SCREW, $6-32 \times 5 / 16$ inch, THS |
| -37 | 380-0089-00 | 100 | 599 |  | 1 | HOUSING, filter |
|  | 380-0089-01 | 600 |  |  | 1 | HOUSING, filter |
|  | - - - - |  |  |  | - | mounting hardware: (not included w/housing) |
| -38 | 212-0012-00 |  |  |  | 4 | SCREW, $8-32 \times 1 \frac{1}{4}$ inches, FHS |
| -39 | 210-0458-00 |  |  |  | 4 | NUT, keps, $8-32 \times 1 / 32$ inch |
| -40 | 210-0402-00 |  |  |  | 4 | NUT, cap, hex., $8-32 \times 5 / 16$ inch |
| -41 | 175-0588-00 |  |  |  | 1 | WIRE, CRT lead, orange stripe |
|  | 175-0592-00 |  |  |  | 1 | WIRE, CRT lead, green stripe |
|  | 175-0595-00 |  |  |  | 1 | WIRE, CRT lead, red stripe |
|  | 175-0641-00 |  |  |  | 1 | WIRE, CRT lead, brown stripe |
|  | 175-0642-00 |  |  |  | 1 | WIRE, CRT lead, blue stripe each wire includes: |
| -42 | 131-0049-00 |  |  |  | 1 | CONNECTOR, cable end, female |

## FIG. 8 CABINET \& RAILS







MRH
666
666
B
HORIZONTAL BLOCK DIAGRAM



MRU
867
LEFT VERTICAL AMPLIFIER © S/N 2000-UP











$\square$





REFERENCE DIAGRAM:
(4) A SWEEP GENERATOR


A SWEEP TIMING SWITCH〈








REFERENCE DIAGRAM:
(1) B SWEEP GENERATOR

MRH
167
167
B SWEEP TIMING SWITCH



## SEE PARTS LIST FOR SEMICONDUCTOR TYPES

REFERENCE DIAGRAMS:
(4) A SWEEP GENERATOR
(7) B SWEEP GENERATOR







REFERENCE DIACRAMS
(4) A SWEEP GENERATOR
(7) B SWEEP GENERATOR
(18) HORIZONTAL DISPLAY \& MODE SWITCHING

MRH




SEE PARTS LIST FOR SEMICONDUCTOR TYPE

REFERENCE DIAGRAM: (7) B SWEEP GENERATOF


SEE PARTS LIST FOR
SEMICONDUCTOR TYPES
REFERENCE DIAGRAM:
$\widehat{\gamma}$ B SWEEP GENERATOR
$M R H$
867
A
LOWER BEAM HORIZONTAL AMPLIFIER (12) S/N 2000-UP


SEE PARTS LIST FOR SEE PARTS LIST FOR
SEMICONDUCTOR TYPES REFERENCE DIAGRAM: (7) B SWEEP GENERATOR


SEE PARTS LIST FOR SEMICONDUCTOR TYPES
REFERENCE DIAGRAM:
(7) B SWEEP GENERATOR

MRH
666
666




T1351
(Upper Beam)
TRANSFORMER DETAILS











REFERENCE DIACRAMS:
(1) LEFT VERTICAL AMPLIFIER 2) RIGHT VERTICAL AMPLIFIEF (3) A sweep trigger
4) A SWEEP GENERATOR 6. B SWEEP TRIGGER
7) B SWEEP GENERATOR (10) alternate trace locic $\& \mathrm{E}$ (14) POWER SUPPLY (15) HEATER WIRING






FIG. 1 FRONT \& SWIT



FIG. 2 "A" SWEEP, VERTICAL AMPI



FIG. 3 "B" SWEEP, VERTICAL AMPLIFIER



TYPE 556 OSCILLOSCOPE

FIG. 4 CAPACITOR CHASSIS \&



FIG. 5 PLUG-IN HOUSINGS \&



FIG. 6 FAN MOTOR \& HEAT SIN



FIG. 7 CRT SHIELD \&


FIG. 7 CRT SHIELD \& REAR


FIG. 8 CABINET \& RAIL



FIG. 9 STANDARD ACCESSORIES


Fig. \&

| Index No. | Tekłronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Disc | $\begin{aligned} & \mathrm{t} \\ & \mathrm{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 9-1 | 200-0382-00 |  | 1 | COVER, graticule |
| -2 | 378-0567-00 |  | 1 | FILTER, light, smokey grey |
| -3 | 010-0129-00 |  | 4 | PROBE, P6008, 10 MEG, 10X BNC |
| -4 | 016-0088-00 |  | 8 | COVER, BNC, non-shorting w/strap |
| -5 | 103-0013-00 |  | 1 | ADAPTER, power cord, 3 wire to 2 wire |
| -6 | 161-0030-00 |  | 1 | CORD, jower, 3 conductor, 9 feet long |
| -7 | 387-0918-00 |  |  | PLATE, CRT face protector |
|  | 070-0757-00 |  | 2 | MANUAL, instruction (not shown) |

## MANUAL CHANGE INFORMATION


#### Abstract

At Tektronix, we continually strive to keep up with latest electronic developments by adding circuit and component improvements to our instruments as soon as they are developed and tested,

Sometimes, due to printing and shipping requirements, we can't get these changes immediately into printed manuals. Hence, your manual may contain new change information on following pages. If it does not, your manual is correct as printed.


TYPE 556

## PARTS LIST CORRECTION

CHANGE TO:

| R559 | $321-0245-00$ | 3.48 kS | $1 / 8 \mathrm{~W}$ | Prec | $1 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R561 | $315-0560-00$ | $56 \Omega$ | $1 / 4 \mathrm{~W}$ |  | $5 \%$ |
| R563 | $323-0326-00$ | $24.3 \mathrm{k} \Omega$ | $1 / 2 \mathrm{~W}$ | Prec | $1 \%$ |
| R759 | $321-0245-00$ | $3.48 \mathrm{k} \delta$ | $1,9 \mathrm{~W}$ | Prec | $1 \%$ |
| R761 | $315-0560-00$ | $56 \Omega$ | $1 / 4 \mathrm{~W}$ |  | $5 \%$ |
| R763 | $323-0326-00$ | $24.3 \mathrm{k} \delta$ | $1 / 2 \mathrm{~W}$ | Prec | $1 \%$ |

TYPE 556
TYPE R556

PARTS LIST CORRECTION

CHANGE TO:

| R1319 | $311-0415-01$ |
| :--- | :--- |
| R1336 | $311-0121-01$ |
| R1369 | $311-0415-01$ |
| R1386 | $311-0121-01$ |

TYPE 556/R556

PARTS LIST CORRECTION

CHANGE TO:
FLl400 119-0135-03

ADD:
C1400 285-0672-00 .1 $\mu \mathrm{F} \quad 600 \mathrm{~V}$

SCHEMATIC CORRECTION


PARTIAL
POWER SUPPLY 14

## PARTS LIST AND SCHEMATIC CORRECTION

ADD:

| C661 | $281-0524-00$ | 150 pF | Cer | 500 V |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| C861 | $281-0524-00$ | 150 pF | Cer | 500 V |  |
| R665 | $315-0271-00$ | $270 \Omega$ | $1 / 4 \mathrm{~W}$ | $5 \%$ |  |
| R674 | $315-0272-00$ | 2.7 k | $1 / 4 \mathrm{~W}$ | $5 \%$ |  |
| R865 | $315-0271-00$ | $270 \Omega$ | $1 / 4 \mathrm{~W}$ | $5 \%$ |  |
| R874 | $315-0272-00$ | 2.7 k | $1 / 4 \mathrm{~W}$ | $5 \%$ |  |



PARTIAL
A SWEEP CENERATOR


PARTIAL
B SWEEP ENERATOR



PARTS LIST CORRECTION

ADD:

| C1034 | $283-0000-00$ | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |
| :--- | :--- | :--- | :--- | :--- |
| C1035 | $283-0000-00$ | $0.001 \mu \mathrm{~F}$ | Cer | 500 V |
|  |  |  |  |  |
| R1101 | $315-0101-00$ | $100 \Omega$ | $1 / 4 \mathrm{~W}$ | $5 \%$ |
| R1201 | $315-0101-00$ | $100 \Omega$ | $1 / 4 \mathrm{~W}$ | $5 \%$ |

SCHEMATIC CORRECTION


ADD: ClO34 and ClO35 as shown above:

UPPER BEAM HORIZONTAL AMPLIFIER 17
ADD: RllOl as shown below:


LOWER BEAM HORIZONTAL AMPLIFIER

$A D D: ~ R I 201$ as shown below:


## K4XL's BAMA

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[^0]:    When the Upper Beam DISPLAY switch is set to any position except RIGHT PLUG-IN A, the B gate from the B Sweep Gating Emitter Follower Q763 is applied via the DISPLAY switch to the grid circuit of V1063A. Only the positive-going portion of the gate as it terminates is used to produce an alternate-trace sync pulse for switching the channels during the $B$ sweep retrace time.

[^1]:    Fig. 6-13. Melhod of adjusting Amplifude Callbralor.

[^2]:    ${ }^{4}$ Furnished as a unit with SW 718.

