## K4XL's BAMA

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## TEKTRONIX



INSTRUCTION MANUAL

Tektronix, Inc.
P.O. Box 500

Beaverton, Oregon 97077




## SECTION 1

## CHARACTERISTICS

## Introduction

The Type 547 Oscilloscope is a versatile laboraiory instrument designed for use with all Tektronix lettered or 1-Series plug-in units. The instrument features two identical time-base generators that can be used singly or electionically alternated for viewing a single signal or multiple signals at two sweep rates.

The two time-base generators can also used in 'delaying" and "delayed" sweep operation for highly accurate time measurements.

## Vertical Deflection System

Refer to Table 1-1 for the characteristics.

## Sweep Generation

Trigger features and sweep rates of both Type 547 timebase circuits are identical.

Sweep Rates (at $1 \times$ mag. nification)

Sweep
Magnification
Any sweep rate can be increased by expanding the center portion of the display horizontally in fixed steps of $2 \mathrm{X}, 5 \mathrm{X}$, and 10X. Sweep-rate accuracy is within $\pm 5 \%$ in the magnified positions.

Trigger Source Selection
$0.1 \mu \mathrm{sec} / \mathrm{cm}$ to $5 \mathrm{sec} / \mathrm{cm}$ in 24 calibrated steps. Displayed Sweep-rate accuracy is $\pm 2 \%$ for both sweeps. An uncalibrated variable sweep-rate control permits either sweep to be slowed to at least 0.4 of the indicated rate.

Trigger Coupling Dc, ac, and ac low-frequency rejection. Selection

Trigger Signal Requirements

Internal (ac): Minimum deflection is 2 mm , rising to 1 cm at about 50 mc .

TABLE 1-1
Plug-In Characteristics for the Type 547 Oscilloscope


[^0]Internal (dc): Minimum deflection is 5 mm at dc rising to 2.5 cm at 50 MHz .
Internal (ac low-frequency rejection): Minimum deflection is 2 mm with signals at about 2 kc , rising to 1 cm at about 50 mc .

External: Frequency ranges are the saine as internal. Minimum amplitude is 200 mvolts peak-to-peak (ac), 200 mve.lts change in dc level (dc) and, 200 mvelts peak-to-peak (ac low-frequency reje,t). A MAXIMUM INPUT OF $\pm 30$ VOITS must not be exceeded in the EXTERN4L trigger position. Minimum trigger le el range is greater than $\pm 2$ volts with the TRIGGER LEVEL control pushed in and $\pm 20$ volts with the control pulled out
Sweep Delay The time-base A sweep can be delayed by the main time base $(B)$ sweep. Delay is continuously variable over the range of $0.1 \mu \mathrm{sec}$ to 50 sec with the DELAY THE ME and DELAY-TIME MULTIPLIER contre Is. Delay time is accurate to $\pm 1 \%$ of indicated delay $\pm 2$ minor divisions of the DELAY-TIME MULTIPLIER at sweep rales from $50 \mu \mathrm{sec}$ to 50 sec . At delay times shorter than $50 \mu \mathrm{sec}$, indicated deliay accuracy is the same as above pius approximately 75.100 nsec . The 75.1100 nsec represents the fixed inherent deliay of the internal trigger circuitry of the Type 547. Incremental delay accuracy is
 MULTIPLIER dial at sweep rates from $1 \mu \mathrm{sec}$ to 50 sec . Incremental accuracy at the three fastest sweep rates $10.1,0.2$, and $0.5 \mu \mathrm{sec}$ ) is $\pm 10$ minor divisions. Stat :d accuracies apply only when the VARIABLE controls are set to CALIB. Delay fitter is no greater than 1 part in 20,000 .

## Horizontal Deflection System

The following characteristics apply when the HORIZONT-AL DISPLAY switch is set to the EXT positions.

| Deflection <br> Factor | Continuously variable from approximately <br> Frequency <br> Response |
| :--- | :--- |
| Input <br> Characteristics | Dc to $400 \mathrm{kc}(3-\mathrm{db}$ down $)$. |
|  | 5 pf. |

## Amplitude Calibrator

Output Voltages 0.2 mvolts to 100 volts peak-to-peak in 18 steps. In addition, a 100 -volt de oitput is available.
Frequency Approximately l-ke square wave.
Output Current 5 ma square wave available at the frot $t$. panel current loop.

Output Impedance

Amplitude Accuracy

$50 \Omega$ in .2 to 200 mVOLTS positions. Progressively higher output impedances in the .5 to 50 VOLT positions up to about 4 k in the 50 VOLT position. Output impedance of the 100 VOLT position (ac and dc) is about $420 \Omega$.

Peak-to-peak amplitude accuracy is $\pm 3 \%$ of indicated value when working into an impedance of 1 megohm. The .2 to 200 mVolts position will be within $\pm 3 \%$ of one-half of the indicated voltage when working into an impedance of 50 ohms. The 5 ma current accuracy is $\pm 3 \%$.

## Front-Panel Output Signals

+GATE B Approximately 20 -volt peak-to-peak square-wave pulse hoving the same duration as the B sweep. Minimum dc load resistance is 5 k .
DLY'D TRIG Approximately a 10 -volt peak-to-peak pulse occurring at the end of the delay period.
SWEEP A Approximately a 90 -volt, peak-to-peak sawtooth voltage having the same duration as the A sweep. Minimum load impedance is 10 k .
+GATE A Approximately 20 -volt peak-to-peak square-wave pulse having the same duration as the $A$ sweep. Minimum dc load resistance is 5 k .
VERT SIG OUT Vertical signal output connector. Output amplitude is approximately 0.3 volt per centimeter of deflection on the crt. Risetime is 20 nsec or faster. Output is ac coupled.
External Single- Requires a positive-going step or pulse Sweep Reset of at least +20 volts with a risetime of 0.5 Input-Signal $\mu \mathrm{sec}$ or faster.

Requirements

## Cathode-Ray Tube

Type
Unblanking
Accelerating 10 kv .
Potential
Usable Viewing $6 . \mathrm{cm}$ high by $10-\mathrm{cm}$ wide. Area
Focus Vertical: 2 horizontal lines/mm distinguishable over the center 4 cm . 1.5 horizontal lines $/ \mathrm{mm}$ distinguishable in the top and bottom 1 cm .
Horizontal: 2 time markers $/ \mathrm{mm}$ distinguishable over the middle $8 \mathrm{~cm} . \quad 1.5$ time markers $/ \mathrm{mm}$ distinguishable in the first and tenth cm .
Graticule Internal, adjustable edge lighting. $6 \times 10 \mathrm{~cm}$ with vertical and horizontal 1 . cm divisions with $2-\mathrm{mm}$ markings on the centerlines. Provision made for riselıme measurement.
$\pm 10 \%$ of nominal
erating Instructions)Line Frequency $\quad 50-60$ and 400 cps .*Power Con- 510 watts typical.sumption
Mechanical
Construction Front panel is anodized. Chassis is alu-minum alloy.
Dimensions See Dimension Drawing.

|  | Characteristics-Type 547/RM547 |
| :---: | :---: |
| Line Frequency | $50-60$ and 400 cps .* |
| Power Consumption | 510 watts typical. |
| Mechanical |  |
| Construction | Front panel is anodized. Chassis is aluminum alloy. |
| Dimensions | See Dimension Drawing. |


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## SECTION 2

## OPERATING INSTRUCTIONS

## FUNCTION OF CONTROLS AND CONNECTORS <br> NOTE

The Time Base A and Main Time Base (B) controls serve identical functions with the exception of the BRIGHTNESS control.

TRIGGERING LEVEL<br>GGERING MODE

SLOPE Determines whether the time base is tig-
Selects the amplitude point on the triggering signal where sweep-triggering occurs. When the knob is pulled out, greater tig. gering range is offered for triggering on higher amplitude signals. The trigseering circuit is most sensitive to small signals with the TRIGGERING LEVEL conirol pushed in and set to 0 .
AUTO STABILITY position permits norinal triggering on signals with repetition rotes higher than about 20 cps . With no tiigger signal, or with a lower repetition rite, the time-base circuit free runs and provides a handy reference trace.
TRIG (triggered) position permits norınal triggering on all triggering signals. No trace occurs when the triggering signal is removed.
gered on the negative- $(-)$ or positive$(+)$ going slope of the signal.

COUPLING AC position blocks the de component of the triggering signal and allows triggering to take place only on the changing portion of the signal. With frequencies below about 30 cps , use the DC position.
AC LF REJ position attenuates trigger ,ignal frequencies below about 1.5 kc , allowing the trigger circuits to respend only to higher frequencies.
DC position permits triggering on both high- and low- (to dc) frequency signals.
SOURCE INT NORM position uses a portion of the signal applied to the vertical deflection plates of the crt as a trigger signal.
INT PLUG IN position applies to multitrace plug-in units that provide a singlechannel trigger signal through pin 5 of the interconnecting plug (e.g. Tektronix Type 1A1 plug-in unit).
LINE position uses a line-frequency signal as a trigger.
EXT position is for external triggering on a signal applied to the TRIGGER INPUT connector.

TIME/CM
VARIABLE
Selects the sweep rate of Time Base A.
Provides an uncalibrated adjustment of sweep rate. The sweep rate can be

BRIGHTNESS

HORIZONTAL DISPLAY
slowed by a factor of at least $2.5 \times$. An UNCALIBRATED lamp lights when the VARIABLE control is not in the CALIBRATED position.
Allows adjustment of the contrast or brightness ratio of the B trace compared to the A trace.
The A position allows only Time Base A to display on the crt.
The ALT position, at the top permits alternate operation so that both time bases are displayed independently. The B position allows only the Main Time Base (B) to display on the crt.
B INTENS BY ' $A$ ' is one of the delayedsweep functions. In this position, a portion of the Main Time Base ( $B$ ) is intensified during the time that Time Base A the delayed sweep) is in operation.
The ALT position on the right-hand side permits alternate operation and display of both times bases while using the delayedsweep feature. This allows the operator to view both the delaying sweep (Main Time Base) and the delayed sweep (Time Base A).

A DLY'D is one of the delayed sweep functions. In this position Time Base $\mathbf{A}$ is displayed at the end of each delay period as determined by the B TIME/CM or DELAY TIME and DELAY-TIME MULTIPLIER controls.
EXT XI and XIO positions permit an external signal to be applied to the horizontal deflection circuit. Sensitivity is continuously variable (with the VAR 10-1 control).
READY Lamps These light when the corresponding timebase circuit is ready for triggering.
SWEEP Expands the sweep from the center of MAGNIFIER the graticule at any setting of the TIME/ CM switch by the amount indicated.
SINGLE SWEEP Permits single-sweep operation in all modes of horizontal display except EXT.
DELAY-TIME Works in conjunction with the TIME/CM MULTIPLIER or DELAY TIME control of the Main Time $1-10$

HORIZONTAL
POSITION VERNIER

AMPLITUDE CALIBRATOR or DELAY TIME control of the Main Time
Base (B). Varies sweep delay from 0.15 to 10.15 times the rate indicated by the Main Time Base (B) TIME/CM or DELAY TIME switch.
Positions the display along the horizontal axis of the crt.

Determines the peak-to-peak voltage available at the CAL OUT connector.

| 5mA Current | Provides a calibrated source of square- <br> wave current. The arrow shows direcion <br> of conventional current flow (i.e. posilive |
| :--- | :--- |
| to negative). |  |

Chopped Blank- Provides blanking of between-channel ing Switch (rear panel)
External Single Sweep Reset (rear panel)

EXTERNAL DELAY INPUT (rear panel) switching transients when using multichannel plug-in units in the chopped mode.

Allows remote control of resetting in single-sweep operation. See Section 1 for reset step or pulse requirements.
A four-pin connector is provided for an external delay generator (rather than the normal internal delay produced by the B sweep). Pin A of the connector permits disabling of the normal internal delayed trigger and is the feed-in point for the external delay trigger (see Fig. 2-1). Pin B is normally dc open and ac ground (through a $0.01 \mu \mathrm{f}$ capacitor), except in the B INTENS BY ' $A$ ' and ALT (between B INTENS BY ' $A$ ' and A DLY'D) positions of the HORIZONTAL DISPLAY switch, then it is dc ground. Pin C supplies a B-gate pulse. Pulse characteristics are: +2 volts minimum with a risetime of 50 nsec or faster into a load of 1.1 k paralleled by 100 pf . Duration of the pulse is the same as the length of the B sweep. Pin D is ground at all times.


Fig. 2-7. Method of coupling an external delayed trigger into the Type 547.

## NORMAL (NONDELAYED) SWEEP

The Type 547 Oscilloscope features two independent timebase circuits: Time Base A and the Main Time Base (B). The time bases can be used singly or alternately. When used alternately, an input signal can be displayed at two different sweep rates in two independent presentations.

## Sweep Triggering

Proper sweep triggering is essential for a stable presentation of an input signal. For a stable display, the sweep must be triggered at the same time relative to the displayed signal. Thus, the sweep must be triggered by the input
signal or by some external signal that has a fixed time relationship with the displayed signal. The external trigger signal must be the same frequency or a submultiple of the input signal.

In alternate-sweep operation, both sweeps must be triggered to obtain a display. The ready lights may be used to determine the proper triggering sequence.

## Selecting the Trigger Source

The SOURCE switch selects one of a variety of passible triggering signals. For most applications, the sweep can be triggered internally from the displayed signal. This oci urs with the SOURCE switch set at NORM.
The PLUG-IN position is for plug-in units that will sufply a single-channel triggering signal through pin 5 of the interconnecting plug, such as the Tektronix Type IAI D.alTrace Plug-In Unit. This position is useful when operaling the plug-in unit in dual-trace chopped-mode operation since the triggering signal is the same as the applied signal and is free from any between-channel switching transients.
The LINE position of the SOURCE switch connects a linefrequency signal to the triggering input. Line triggerin,, is useful whenever the input signal is frequency-related to the line frequency.
To trigger the time base from an external signal, set the SOURCE switch to EXT and connect the trigger signal to the TRIGGER INPUT connector. External triggerinç, is often used when signal tracing in amplifiers, phase:shift networks, and wave shaping circuits. The signal from a single point in the circuit can be used as the external trigger signal. With this arrangement, it is possible to observe the shaping and/or amplification of a signal at various points throigh the circuit without resetting the triggering controls for each new display.

## Selecting Trigger Coupling

Three means of trigger coupling are available with the COUPLING switch. The different coupling positions peimit you to accept or reject certain frequency components of the triggering signal.
With the COUPLING switch set at DC, the time base :an be triggered with all frequency components of the trigge ing signal within the trigger amplifier bandpass, including de levels.

With the COUPLING switch set of AC, the de component of the triggering signal is blocked. Also, low-frequency signals below about 30 cps are attenuated.
With the COUPLING switch set at AC LF REJ, de and liswfrequency signals (below about 1.5 kc ) are rejected or atienvated. Thus, the trigger circuit will respond best to the higher-frequency components of the triggering signal.
In general, use AC coupling. However, it will be ne essary to use DC coupling for very low-frequency signals. When line-frequency hum is mixed with the triggering sig.ial, it is best to use AC LF REJ coupling so that triggering trikes place only on the signal of interest (if the signal of interest contains frequency components above about 1.5 kc ].

The AC LF REJ position is also useful when triggering internally from multitrace plug-in units operated in the alternate dual-trace mode (unless the plug-in unit is a Type IAI and the SOURCE switch is set to PLUG IN). AC LF REJ coupling has a faster recovery time when subjected to the alternate de levels from the multitrace plug-in unit.

## Selecting Trigger Slope

The trigger SLOPE switch determines whether the triggering circuit responds on the rising (t setting) or the falling (- setting) portion of the triggering signal. When several cycles of a signal appear in the display, the selting of the SLOPE switch will probably be unimportant. However, if you wish to look at only a certain portion of a cycle, the SLOPE switch will help start the display on the desired slope of the input signal. Fig. $2-2$ illustrates the effect of both the SLOPE and TRIGGERING LEVEL controls.

## Selecting Trigger Mode

The automatic stability mode is generally more convenient. With the MODE switch set to AUTO STABILITY, proper triggering takes place after setting the TRIGGERING LEVEL control. When the triggering signal is removed, the timebase circuit automatically free runs and presents a reference display. In alternate sweep operation, both MODE switches should be set to AUTO STABILITY. If this is done, a display will be maintained if one of the triggering signals is removed.
The TRIG position of the MODE switch should be used if the trigger signal has a very low repetition rate (below about 20 cps ).

## Setting Triggering Level

The TRIGGERING LEVEL control determines the amplitude point on the signal where triggering occurs.

The trigger circuit is most sensitive to ac triggering signals with the TRIGGERING LEVEL control set near zero and pushed in. Moving the TRIGGERING IEVEL control in the + direction causes the trigger circuit to respond at some higher positive amplitude on the triggering signal. Moving the TRIGGERING LEVEL control in the - direction causes the trigger circuit to respond at some higher negative amplitude on the triggering signal. Fig. 2-2 illustrates the effect of the TRIGGERING LEVEL control and the SLOPE switch.
The range of the TRIGGERING LEVEL control is extended 10 times when pulled out.

## Selecting Time/Cm (Sweep Rate)

The TIME/CM and SWEEP MAGNIFIER switches control sweep rate, The SWEEP MAGNIFIER switch expands both time bases.
The TIME/CM and SWEEP MAGNIFIER switches allow you to view an applied signal at a wide variety of calibrated sweep rates. When you make time measurements from the crt, be sure the VARIABLE control is set to CALIBRATED.


Fig. 2-2. Effects of the TRIGGERING LEVEL and SLOPE controls.

When the SWEEP MAGNIFIER switch is set to XI , the TIME/CM switch indicates the true sweep rate. However, with the SWEEP MAGNIFIER switch set to X2, the setting of the TIME/CM switch must be divided by 2 to determine the true sweep rate. For example, assume that the TIME/CM switch is set at 1 mSEC and the SWEEP MAGNIFIER is set to X5. In this case, the true sweep rate would be 1 ( msec ) divided by 5 (SWEEP MAGNIFIER setting); resulting in a displayed sweep rate of 0.2 msec per division. Fig, 2-3 illustrates how to make time measurements from the graticule.


Fig. 2-3. Illustration of time measurement from the graticule.

## Alternate-Sweep Operation

Alternate-sweep operation occurs with the HORIZONTAL DISPLAY switch set to one of the ALT positions. The allar-nate-sweep features of the Type 547 allow signal to be displayed at two independent sweep rates. The alternotesweep features can be used in either delayed or nondelayed modes of operation.

To obtain a display in the alternate-sweep mode, buth time-base circuits must be triggered. To insure that buth time-base circuits are always triggered, the MODE switch of both Time Bases can be set to AUTO STABILITY. If this is done, the oscilloscope presents an alternate-sweep display even if there is no triggering signal or if the TRIGGERING LEVEL control is set improperly.

With a Tektronix Type 1AI Dual-Trace Plug-In Unit operating in the alternate dual-trace mode, Channel 1 will lock in with the Time Base A sweep, and Channel 2 will lock in with the Main Time Base (B) sweep. The result is two displays that are independent in sweep rate and vertical defliction factor. If a multitrace plug-in unit is operated in the chopped mode, each channel will be displayed on buth time bases.

The TRACE SEPARATION control allows vertical positioning of the Time Base A display in either ALT mode. The vertical position control of the plug-in unit positions $b_{c}$,th
displays. The BRIGHTNESS control varies the intensity of the Main Time Base ( $B$ ) trace. This adjusts brightness or contrast ratio of the B trace compared to A trace. In the delayed mode, this allows the operator to adjust the intensified zone on the delaying sweep for best viewing contrast. In the normal alternate mode the operator may adjust the brightness level so that the intensity of each sweep is equal while the sweep rates may be significantly different. Also, the BRIGHTNESS control provides a convenient means of identifying the Main Time Base (B) trace when both traces are displayed on the crt.

## Single-Sweep Operation

In applications where the displayed signal is not repetitive or varies in amplitude, shape, or time, a conventional repetitive display may produce a jumbled presentation. To avoid this, use the single-sweep feature of the Type 547. To use single sweep, first make sure the trigger circuit will trigger on the event you wish to display, Do this in the conventional manner with the single sweep switch set at NORMAL. Then, depress the single sweep switch to the RESET position and releose the switch so it returns to the SINGLE SWEEP position. When this is completed, the next trigger pulse will actuate the sweep and the instrument will display the event on a single trace. The READY lamps, near the HORIZONTAL DISPLAY switch, first light when the sweep is ready to accept a trigger and then go out after triggering has taken place. To ready the circuit for another single display, depress the single sweep switch to RESET and release. In single-sweep operation, make sure the MODE switch is set to TRIG.

In normal alternate mode, the single sweep switch controls the B sweep. Thus, the A sweep con run up only once after the B sweep has occurred due to the alternating function. Therefore, for each single-sweep reset, each time base produces a single alternate sweep upon being triggered.

In the delayed alternate mode, the single-sweep switch again controls only the B sweep. However, B sweep must run up for each display. Therefore, resetting is required for each display.

## NONTRIGGERED DELAYED SWEEP

The following procedures describe various measurements, the accuracy of those measurements, and other operations that can be performed using delayed sweep.
Insert a vertical plug-in unit and set the controls and switches on the instruments as listed in Table 2-1.
Set the HORIZONTAL POSITION control so the trace begins precisely at the left-hand edge of the graticule. Notice the position of the intensified segment in the trace.

Now set the B TIME/CM or DELAY TIME switch to .2 SEC and A TIME/CM to 20 mSEC . The intensified segment should be at the same position as with the previous sweep rates.
Connect the SWEEP A output to the vertical plug-in unit input. Notice that the A sweep sawtooth and the intensified segment in the trace start and end at the same time. This display shows that time base A produces one sweep during the intensified segment of each B sweep. The A TRIGGERING LEVEL control has no effect.

The B sweep rate is $0.2 \mathrm{sec} / \mathrm{cm}$. The intensified segment begins 5 cm after the beginning of the trace. Hence, the A sweep starts 1 sec after the $B$ sweep $(0.2 \mathrm{sec} / \mathrm{cm} \times 5(\mathrm{~m})$.
The number of centimeters between the beginning of the trace and the beginning of the intensified segment is established by the setting of the DELAY-TIME MULTIPLIER contiol. Therefore, with any dial setting, the time difference betw:en the beginning of the $A$ and $B$ sweeps is the product of the B TIME/CM or DELAY TIME switch and the DELAY-T/ME MULTIPLIER dial setting (see Fig. 2-4).


B TIME/CM or DELAY TIME Switch Sotting $X$ DELAY-TIME
MULTIPLIER Dial Setting $=$ Amount of delay between the start of the 8 (delaying) and the start of the A (delayed) sweep.

Fig. 2-4. Determining delay time.

## TABLE 2-1

| B MODE | AUTO STABILITY |
| :--- | :--- |
| B SOURCE | NORM |
| B COUPLING | AC |
| B SLOPE | + |
| B TRIGGERING LEVEL | 0 |
| B TIME/CM or DELAY |  |
| TIME | 1 mSEC |
| A MODE | AUTO STABILITY |
| A SOURCE | EXT |
| A TIME/CM | . 1 mSEC |
| VARIABLE (A and B) <br> HORIZONTAL DIS- <br> PLAY | CALIBRATED |
| SWEEP MAGNIFIER <br> DELAY-TIME <br> MULTIPLIER | OFF (X1) |
| AMPLITUDE CALIBRA. | 5.00 |
| TOR |  |

## HORIZONTAL POSITION

INTENSITY

Centered
So both intensity levels in the trace are easily seen.

Set the applicable controls and switches of the vertical plug-in unit as follows:

| VOLTS/DIV | 5 |
| :--- | :--- |
| VARIABLE | CALIBRATED |
| AC-DC-GND | DC |
| POSITION | Trace centered. |

The following procedures describe five common applications of the delayed-sweep feature. These applications are more accurate than time measurements taken directly from the crt display.

## Demonstration 1

This procedure describes how to measure pulse duration with the pulse triggering the Main Time Base (B).
Set the controls and switches as listed in Table 2-1 except as follows:

$$
\begin{array}{ll}
\begin{array}{l}
\text { B TIME/CM or DELAY } \\
\text { TIME }
\end{array} & .1 \mathrm{mSEC} \\
\text { A TIME/CM } & 1 \mu \mathrm{SEC}
\end{array}
$$

Apply the AMPLITUDE CALIBRATOR signal to the input of the vertical plug-in unit. If necessary, adjust B TRIGGERING LEVEL to obtain a stable display. The display should consist of nearly 1 cycle of the square-wave signal.
Set the DELAY-TIME MULTIPLIER dial to intensify the falling portion of the square wave. Set the HORIZONTAL DISPLAY switch to A DLY'D. The display should now be a horizontally expanded version of the signal observed in the intensified segment of the previous display. Set the HORIZONTAL DISPLAY switch to ALT (between the B INTENS BY ' $A$ ' and A DLY'D positions). Now, both the "delaying" and the "delayed" sweeps can be observed simultaneously. Adjust the BRIGHTNESS control of the Main Time Base (B) to equalize the intensity. Set the TRACE SEPARATION control so that the 0 and $100 \%$ amplitude points of both displays are exactly superimposed.
Set the DELAY-TIME MULTIPLIER dial so the falling $50 \%$ point on the delayed trace exactly crosses the $50 \%$ amplitude level on the rising portion of the intensified display (this point may be hard to see but will be very near the start of both traces). Multiply the DELAY-TIME MULTIPLIER dial reading (e.g. 5.03) by the B TIME/CM or DELAY TIME switch setting. The product is the time duration of the squarewave positive-going half-cycle.
Accuracy: Determined by the combination of all the follow. ing factors:

1. The basic accuracy of time measurements made by using the sweep delay is as stated in Section 1.
2. The Delay Pickoff and Time Base A generator circuits typically require a net total of about 75 to 100 nsec to respond to the signal event which triggers Delayed Sweep
(A). This small inherent delay need not be considered unless it is a significant percentage (delay times shoiter than $50 \mu \mathrm{sec}$ ) of the measured time or when measuring time differences using the same sweep rate. When nei essary, add the net circuit delay time to the measured tine: that is, when measuring the time from the start of th: B sweep.

Summary: The method described in Demonstration 1 provides a time measurement accuracy within $1 \%$ of reading $\pm 2$ minor divisions of the DELAY-TIME MULTIPLIER dial.

By comparing the delay reading to an accurate external timing standard (such as a Tektronix Type 180A Time-Mark Generator) and applying a correction factor, an accuracy of $\pm 2$ minor divisions of the DELAY-TIME MULTIPLIER dial an be achieved.

## Demonstration 2

This procedure describes how to measure time between two pulses, neither of which triggers Time Base A.

Set the controls and switches as listed in Table 2-1 excupt as follows:

| B TIME/CM or DELAY | .2 mSEC |
| :--- | :--- |
| TIME |  |
| A TIME/CM | $2 \mu \mathrm{SEC}$ |

Apply the AMPLITUDE CALIBRATOR signal to the vertical input. If necessary, adjust the B TRIGGERING LEVEL contiol to obtain a stable display. The display should consist of about 2 cycles of the square wave. Set the DELAY-TIME MULTIPLIER dial so the square-wave rise located near the center of the display is intensified.

Set the HORIZONTAL DISPLAY switch to ALT (between the B INTENS BY ' $A$ ' and A DLY'D positions). The display shoild now include a horizontally expanded version of the intensified segment.

Set the DELAY-TIME MULTIPLIER dial so the rising $50 \%$ amplitude level of the square wave intersects the vertin al centerline of the graticule. Note the exact setting of the DELAY-TIME MULTIPLIER dial (e.g. 5.48), Turn the DELAYTIME MULTIPLIER dial clockwise until the falling $50 \%$ amplitude level of the square wave intersects the same vertia al graticule centerline used with the previous dial setting. Again note the exact setting of the DELAY-TIME MULTIPLIER dial.

Subtract the first dial setting from the second setting. The product of the difference times the B TIME/CM or DELAY TIME switch setting equals the time duration of the square-wave positive-going half-cycle (between the $50 \%$ amplitude points). This measurement should indicate a time of about 0.5 msec .

Accuracy: Determined by the combination of the following factors:

1. The basic accuracy of the sweep delay as described in Demonstration 1.
2. The error added by the sweep-delay system linearity is $\pm 4$ minor dial divisions. Hence, $\%$ of measurement error decreases as the numerical dial difference increases.

## NOTE

When the separation between dial settings is 100 minor dial divisions or less, the time measurement can often be made more accurate by direct reading from a maginfied crt display. See Demonstration 3: Magnification.
3. The accuracy of time measurements made in Demonstration 2 is independent of the inherent circuit delays, provided the B TRIGGERING LEVEL control setting is the same for each of the two dial readings.

Summary: The method described in Demonstration 2, provides time measurement accuracy as stated in Section 1. Accuracy will be greatest when the numerical difference between the two DELAY-TIME MULTIPLIED readings is greatest.

## Demonstration 3

Complex signals contain a number of individual events of different amplitudes. Since the trigger circuits of the Type 547 respond to signal amplitude, a stable display will normally be obtained only when the sweep is triggered by the event having the greatest amplitude. The A delayed mode permits the start of the A sweep to be delayed for a selected time after the signal event having the greatest amplitude. Any event within the series of events may then be displayed in magnified form as follows:

Set the controls and switches on the instrument as listed in Table 2-1. Apply the AMPLITUDE CALIBRATOR signal to the vertical input. If necessary, odjust the B TRIGGERING LEVEL control to obtain a stable display. The display should consist of several cycles of the square-wave signal. Set the DELAY-TIME MULTIPLIER dial to intensify one of the positivegoing pulses.

Set the HORIZONTAL DISPLAY switch to ALT (between the B INTENS BY ' $A$ ' and A DLY'D positions). The display should now include the same signal information as the intensified trace segment, but horizontally expanded (magnified) ten times.

Increase the A sweep rate to $1 \mu \mathrm{sec} / \mathrm{div}$. The BRIGHTNESS and INTENSITY controls may require readjustment to view both displays. Set the DELAY-TIME MULTIPLIER dial to position a square-wave rise on the crt. The display now gives $\times 1000$ magnification of the intensified segment.

Slowly turn the DELAY-TIME MULTIPLIER dial. Note that any portion of the square wave can be brought into view in magnified form.

The DELAY-TIME MULTIPLIER dial reading corresponds to the number of centimeters between the beginning of the time base $B$ trace and the beginning of the time base $A$ (intensified) trace (e.g. $7.00=7$ major graticule divisions).

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The A delayed display will probably exhibit some horizontal jitter. The time jitter contributed by the delay system is less than $5 \times 10^{-5}$ times the B TIME/CM or DELAY TIME switch selting. Since the sweep rate of the delayed sweep, is now $1 \mu \mathrm{sec} / \mathrm{cm}$, the jitter due to the delay system is less than one-half centimeter.
Accuracy: Depends solely on the B sweep-rate accuracy as listed in Section 1.

## Demonstration 4

Ordinarily, the displayed signal is also used to trigger the oscilloscope sweep. In some situations, it may be desirable to reverse this situation. The sweep-related output pulses, available from the front-panel of the Type 547, an be used as a triggering signal for an external device. The output signal of the external devise can then product a stable display while the oscilloscope sweep free runs.
To demonstrate one method of performing this operation, proceed as follows:
Set the controls and switches as listed in Table 2-1 exciept as follows:
$\left.\begin{array}{ll}\text { B SOURCE } & \text { EXT } \\ \text { DELAY-TIME } & 1.00 \\ \text { MULTIPLIER }\end{array}\right]$

Connect a lead from the DLY'D TRIG connector to the vertical input. The display should consist of a positivegoing spike.
The oscilloscope display is the pulse that is available at the Type 547 at the end of each delay period. In a practical application, the pulse would not be applied to the vertical input but instead to some external device to be tested. The pulse would then serve as the trigger pulse or input signal for the external device, and the output of the device would provide a stable display on the oscilloscope, as through the oscilloscope were triggered in the normal manner.

## Demonstration 5

The +GATE A connector output signal of the Type 5.47 can be used as a variable repetition rate, variable duty-fisctor pulse generator. To use the Type 547 in this manner, proceed as follows:
Set the controls and switches as listed in Table 2-1 exci.pt as follows:

| HORIZONTAL DISPLAY | B INTENS BY 'A' |
| :--- | :--- |
| DELAY-TIME <br> MULTIPLIER | About 0.20 |
| B TRIGGERING MODE | AUTO |

Monitor the signal available at the +GATE connector on another oscilloscope and establish the desired pulse repetition rate by setting the B TIME/CM or DELAY TIME switch and VARIABLE B control. Establish the desired duty factor by setting the A TIME/CM switch.

The maximum pulse repetition frequency that can be obtained in this manner is 60.90 kc . Maximum duty factor is about 0.9 , decreasing to about 0.15 with faster sweep rates.

## TRIGGERED DELAYED SWEEP

Complex signals contain a number of individual events at different amplitudes. Since the trigger circuits in the Type 547 respond to signal amplitude, a stable display will normally be obtained only when the sweep is triggered by the event having the greatest amplitude.

The following instructions demonstrate that Time Base A can be triggered by any event with a series of events, regardless of relative amplifude.

Set the controls and switches on the instrument as listed in Table 2-1.

Connect the AMPLITUDE CALIBRATOR signal to the vertical input. You should obtain a square-wave display.
Turn the DELAY-TIME MULTIPLIER dial about 2 turns in either direction. Notice that the brightened segment in the display moves smoothly across the crt.

Set the DELAY-TIME MULTIPLIER dial so the brightened segment begins about in the middle of a pulse top. Now, set the A MODE switch to TRIG and the A SOURCE switch to NORM. Notice that the brightened segment in the display has shifted to the next pulse on the right. (If the brightened segment is not present, or is unstable, readjust the A TRIGGERING LEVEL control.) Turn the DELAY-TIME MULTIPLIER dial several full turns. The brightened segment in the dispiay should jump from one pulse to the next. Set the HORIZONTAL DISPLAY swith to A DLY'D and notice that the disploy now begins on the rising portion of the pulse. With the present display, turning the DELAY-TIME MULTIPLIER dial should not change the display since all of the AMPLITUDE CALIBRATOR pulses are the same shape. However, if the input signal consisted of a repeating series of several dissimilar pulses, turning the dial would provide a triggered display of each pulse in the series (provided the A TRIGGERING LEVEL control is set for triggering on the smallest pulse).

The display is produced in the following manner:
Time Base A produces one sweep during each B sweep. The Time Base A sweep will begin some time after the start of B sweep. This time is the total of the B TIME/CM or DELAY TIME switch setting multiplied by the DELAY-TIME MULIPLIER dial setting, plus the time between the end of this delay interval and the next event in the signal which can trigger Time Base B.

With the A TRIGGERING MODE switch in the TRIG position, the Time Base A sweep will occur only if A is armed and triggered before the B sweep ends. If Time Base A is not triggered, the scope waits.

## Polarized Light Filfer

The polarized light filter provided with the Type 547 minimizes undesirable reflections when viewing the display under high ambient light conditions. The filter may be left on when taking waveform photographs unless a high writing rate is required.

If the light filter is removed, the CRT protector plate should be installed to prevent scratches to the CRT tace plate.

## EXTERNAL HORIZONTAL DEFLECTION

For special applications, horizontal deflection can be produced with an externally derived signal. Thus, the o cilloscope system can be used to plot one function against another (e.g. Lissajous figures). However, the system is not intended for precise phase-angle measurements.

To use an external signal for horizontal deflection, ionnect the signal to the HORIZ INPUT connector. Set the HORIZONTAL DISPLAY switch to EXT. The signal is dc coupled to the deflection amplifier. The MAG switch, is inoperative when the HORIZONTAL DISPLAY switch is set to either external horizontal position.

## COOLING

A fan maintains safe operating temperature in the Type 547 by circulating filtered air over the power supply rictifiers, regulators, and other circuit components. Wher in operation, the instrument must be placed so that the air intake at the back and the vents in the side panels are clear of any obstruction that might impede the flow of air. Allow at least 3 inches clearance at the rear of the instrument and 2 inches at each side. The side panels should be in place (except during maintenance adjustments) for proper air circulation inside the instrument.

The Type 547 should never be operated without the fan running, since temperatures within the instrument will rise to a dangerous level in a few minutes. In this event, the thermal cutout switch disconnects the power and keep;s it disconnected until the temperature drops to a safe level

## POWER REQUIREMENTS

General. The Type 547/RM547 will regulate with input line voltages which are within $10 \%$ of designed center coltage range. Two possible methods of connecting the oscilloscope for use with the appropriate power supplies exist, and
the method to be used is determined by the serial number of the instrument as follows:

## SN 7980 and Above

The Type 547 can be operaled from either a 115 -volt or a 230 -volt nominal line-voltage source. The Line Voltage Selector assembly on the rear panel converts the instrument from one operating range to the other. In addition, this assembly changes taps on the primary winding of the power transformer to allow selection of one three regulating ranges. The assembly also includes the two line fuses. When the instrument is converted from 115 -volt to 230 -volt nominal operation, or vice versa, the assembly instails the proper fuse to provide instrument protection.

To convert from one nominal line voltage to the other and/or change regulating ranges, use the following procedure. (See Fig. 2-5)


Fig. 2-5. Voltage Selector assembly. Oscilloscope serial number 7980 and above.

1. Disconnect the instrument from the power source.
2. Loosen the two captive screws that hold the cover in the voltage selector switch base; then remove the cover by pulling it straight away from the base.
3. To change nominal line voltage selection, pull out the Voltage Selector plug, (see Fig. 2-5) rotate it $180^{\circ}$ and plug it back in.

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4. To change regulating ranges, pull out the Range 'jelector plug (see Fig. 2-5), slide it left or right to the desied position and plug it back in. Select a range which centers about the average line voltage to which the instrument is to be connected (see Table 2-2).
5. Re-install the cover and tighten the two captive screvs, making sure that the indicating tabs are protruding through the correct holes in the cover for the desired line voltage and regulating range.
6. Re-connect the instrument to the power source.

## CAUTION

Operation of this instrument with the Voltage Selector or Range Selector switch in the wrong position for the applied line voltage may damage the instrument or cause improper operation.

TABLE 2-2
Regulating Ranges SN 7980 and Above

| Range Selector Switch Position | Voltage Selector |  |
| :---: | :---: | :---: |
|  | 115-Volts Nominal | 230-Volts Nominal |
| LO (switch bar in left holes) | 90 to 110 volts | 180 to 220 volt |
| M (switch bar in middle holes) | 104 to 126 volts | 208 to 252 volt |
| HI (switch bar in right holes) | 112 to 136 volts | 224 to 272 volt: |

## SN 7979 and Below

Unless otherwise indicated, the Type 547 is shipped with the power transformer and fan wired for 115 -volt AC inpit. Fig. 2.6 and a connection diagram on the side of the transformer show alternate connections for other input voltages to the power transformer. When the transformer is chang d from 108.122 volts to $216-244$ volts connection, the fan wiring must also be changed. Fig. 2-7 shows the fan connections for each voltage range.

## Transformer and Fan Connections SN 7979 and Below

|  |  |  |
| :---: | :---: | :---: |
|  |  |  |

Fig. 2-6. Transformer connections for 108 to 244 volt, 50 to 60 cps. SN 7979 and below.


Fig. 2-7. Fan connections for 108 to 244 volt, 50 to $\mathbf{6 0}$ cps. SN 7979 and below.

## SECTION 3

## CIRCUIT DESCRIPTION

## Introduction

This section contains the theory of operation of the varisus circuits in the Type 547. A simplified block diagram analysis is given first to explain the operation of each cir: uit in general terms, then the operation of each circuit is covered in detail.

## BLOCK DIAGRAM ANALYSIS

In the following analysis, it is assumed that the o.cilloscope is equipped with a dual-channel vertical plurf-in preamplifier, and that the horizontal display switch is set in the ALT position between the A DLY'D BY B and the B INTENS BY ' A ' positions. Fig. 3-1 is a simplified block diagram showing the Type 547 operating in this mode. Detailed block diagrams showing circuit configuration for his and other modes of operation are contained in Section 6. The functions of the various blocks in Fig. 3-1 are explained in the following paragraphs.

Low-Voltage Power Supply. The low-valtage power sipply produces all operating voltages for the oscilloscope v. ith the exception of parts of the crt circuit. The low-voltage supply provides regulated $-150,+100,+225$, and +350 velts. it also provides heater voliages and an unregulated +325 volt output.

Vertical Plug-In Preamplifier. Any Tektronix letter-Se ies or 1 -Series vertical plug-in preamplifier can be used with the Type 547. For a circuit description of the plug-in unit refer to the plug-in unit instruction manual.

Vertical Input Amplifier. The vertical input amplifier is a balanced, hybrid amplifier that amplifies the output of the plug-in vertical preamplifier and applies the amplified vertical signal to the trigger-pickoff circuit and the vertical output amplifier,

Delay Line. The push-pull output of the vertical input amplifier is applied through the balanced delay line to the veitical output amplifier. The delay line is a specially braided 186 -ohm line which delays the application of the vertical signal to the vertical output amplifier for 170 nsec . This provicies time for unblanking crt and starting the horizontal sweep before the vertical signal reaches the deflection plates. The delay allows the leading edge of a single fast-rising pulse to be displayed. The delay line requires no adjistment because of the precision construction.

Vertical Output Amplifier. The vertical output amplifiet is a push-pull three-stage, transistor amplifier that takes the output of the delay line and amplifies it to a level sufficii nt 10 drive the vertical deflection plates of the cr .

Trigger-Pickoff Circuit, The trigger-pickoff circuit applies a sample of the input waveform to the trigger circuits of both time bases. The trigger is picked off at the output of the vertical input amplifier.

Main Time Base (B) Generator. The main time base (B) generator provides accurate ramp voltages for the horizontal deflection system, unblanking for the crt, sync pulse for the sweep switching circuit, and $a+B$ gate to a front-panel connector. The main time base ( $B$ ) generator may be triggered by signals derived from either internal or external sources.

Delay-Pickoff Circuit. The delay-pickoff circuit compares the ramp-voltage output of the main time base (B) generator with a variable reference voltage, and assuming indentical characteristics in the two halves of the comparator, generates a trigger pulse when the two voltages are equal. The trigger output of the delay-pickotf circuit may be used to arm or trigger Time Base $A$, and is also available at a front-panel connector.

Altarnate-Sweep Switching Circuit. When the HORIZON. TAL DISPLAY switch is in either of the alternate modes, the alternate-sweep switching circuit performs the following functions:

1. Gates the ramp signals from the time-base generators into the horizontal amplifier and thereby decides which of the two time-base generators is to be displayed.
2. Provides the vertical plug-in preamplifier with dual-frace slaving pulses.
3. Applies trace-separation voltage to the vertical amplifier during the $A$ sweep.
4. Disables the $B$ sweep unblanking circuit during presentation of the delayed A sweep.

In the A ALT B position of the HORIZONTAL DISPLAY switch, the alternate-sweep switching circuit provides sweepgenerator lockout voltages to the horizontal display switch.

Horizontal Amplifier. The input to the horizontal amplifier is selected from the outputs of the main time base (B) generator, time base A generator, or the external horizontal input amplifier. The selected input is split in phase and amplified to provide push-pull drive to the horizontal deflection plates of the crt.

External Horizontal Amplifier. The external horizontal input amplifier provides the necessary gain to drive the horizontal amplifier from external signals. An input attenuator and a gain control provide horizontal deflection factors from 0.1 to about 10 volts $/ \mathrm{cm}$.

Crt Power Supply. The crt power supply provides the high voltages for operating the crt. The power supply is of the if type, using a 50 -kc Hartiey oscillator. Secondary windings on the oscillator transformer supply voltages to the high-voltage rectifiers.

Cathode Ray Tube ( $\mathrm{Cr} t)$. The cathode-ray tube used in the Type 547 is a flat-faced, internal graticule, 5 -inch tube


Fig. 3-1. Type $5: 17$ simplified block diagram.
with 6 cm of usable vertical scan area. The tube is designed for low input capacitance to the vertical deflection plates and minimum $x$-axis center-to-edge defocusing.

Calibrator. The calibrator in the Type 547 is a multivibrcitor and cathode follower that provides a square-wave output with a maximum amplitude of 100 volts at a naminal 1 kc . A step attenuator permits switching the output amplitide from the front panel. In the 0.2 -mvolt to 200 -mvolt rarge, the output impedance is $50 \Omega$.

Time Base A Generator. The time base A generator clo ely resembles the main time base $(B)$ generator. The description of functions and the circuit analysis given for the time bise (B) generator in most instances apply also to the time bise A generator.

## CIRCUIT ANALYSIS

The following circuit analysis of the Type 547 descrizes the operation of the various circuits in detail. While reading through the description of a particular circuit, rf fer to the circuit diagram being discussed (see Section 6).

## Low-Voltage Power Supply

The low-voltage power supply in the Type 547 (see Po ver Supply schematic) actually consists of four interrelated , sp. plies that operate together as as system. This system deti ers filtered and regulated voltages of $-150,+100,+225$, and +350 volts as well as an unregulated de voltage of +125 volts. A common power transformer, T601, supplies the in sul power to each of the supplies, as well as heater power to thermal time-delay relay K600 and the tubes in the o:cilloscope. Unless otherwise specified, the Type 547 is ship ed with T601 wired for 115 -volt ac input. A connection digi am on the side of the transformer shows alternate connections for other input voltaes for SN 7979 and below. For SN 7180 and above, a Voltage Selector assembly is provided tiee Operating Instructions section of this manual).

The 115 -volt ac input power is applied to T601 throigh POWER ON switch SW601. Overload protection is provic ed by fuse F601. Thermal cutout TK601 in the primary cit uit of T601 is a protective device that opens the transfor ter primary circuit if the temperature inside the oscillosex pe rises above a safe value. TK601 resets automatically wien temperatures return to normal; and to shorten the cool ng time, the fan conlinues to run while TK601 is open (exs :pt when T601 is connected for $210-250$-volt operation). Ther ial time-delay relay K600 provides a filament warmup time of approimately 30 seconds before the dc power supplies re aclivated. The heater of K600 is rated at 6 volts one is connected to 6.3 volts on the T601 secondary winding. I uring heater warmup time, contacts 4 and 9 of relay K600 remain open. At the end of heater warmup time, contact. 4 and 9 close and apply power to magnetic relay K601. C in. tacts K601-1 of relay K601 remove the heater power $f 1$ m K600, but before K600 can open, contacts K601-I lock he holding circuit to the coil of K601. K601 now remains et ergized until the power to the oscilloscope is switched afl or otherwise interrupted. When K601 is energized, conte cts K601-2, K601-3, K601-4, K601-5, and K601-6 are also clo ed and thus activate their respective dc supplies.

- 150-Volt Supply. The - 150 -volt supply in the Type 547 is the reference voltage source for the other supplies and must be very stable. The -150 -volt supply includes a highgain electronic voltage regulator designed to give good regulation under extreme operating conditions. This regulator circuit contains a series regulator, a glow-discharge tube reference source, an error detector, and an amplifier.

In operation, the input power to the -150 -volt supply is supplied by one secondary winding of T601. The ac output of the secondary winding is rectified by silicon-diode rectifier bridge D642 and filtered by capacitor C642A, In series with the positive side of the supply and ground are series regulator tubes V637 and V647, paralleled by shunting resistors R646 and R647. The output of the -150 -volt supply is taken from the negative side.

Error sensing in the valtage-regulator circuit is accomplished by comparator tube V624. Current flow through V624 is established by the setting of the tap on R616 in the voltage divider R615, R616, and R617. The voltage on the grid of V624A is held at approximately +85 volts by reference tube V609. Assuming that the output voltage of the - 150 -valt supply increases due to increased line voltage or some other cause, the voltoge increase appears on the cathodes of V624 and throngh the tap on R616, on the grid of V624B, Due to the voltage divider, only a part of the voltage increase appears between the grid and cathode of V6248, but the full change appears on the grid and cathode of V624A. The increase is in the negative direction, therefore, V624A increases its conduction to maintain the proper bias between grid and cathode, and this holds both cathodes more or less fixed while the grid of V 624 B is pulled negative by the increasing negative voltage across the voltage divider. The increasing negative voltage on the grid of V 6248 causes a decrease in current; thus the plate voltage goes positive.
The positive change in plate voltage is amplified and inverted to a negative change by amplifier fube V634. The amplified error signal from V634 is applied to the grids of series regulator lubes V637 and V647. The negative-going error signal on the grids of V637 and V647 decreases the current through the tubes, effectively increasing their resistance and the voltage drop across them. The voltage necessary to provide the increased drop across the series regulator tubes and shunt resistor can only be obtained by subtracting it from the negative side of the supply, so the undesired increase in negative voltage is absorbed in the series regulators and shunt resistors. If the output of the - 150 -volt suppy had decreased instead of increased, then the error voltage applied to the grids of the series regulators would have been positive-going. The positive-going error voltage on the grids of the series regulators would lower the resistance of the series regulator tubes, and the voltage drop across them would decrease, leaving more voltage for the negative side of the supply. Since the output voltage of the -150 -volt supply depends upon the relationship of the voltage on the top of R616 and the reference voltage from V609, accurate adjusiment of the output voltage is provided by making R676 variable.

Filter capacitor C642A does not remove all the ripple from the output of the bridge rectifier, and the series regulator circuit functions also to reduce this output ripple voltage. Any ripple between the -150 -volt output point and ground reaches the grid (pin 2) of V624A via capacitor C610. This
input ripple voltage is amplified by V624 acting as a coth-ode-coupled amplifier. The ripple output voltage at the plate (pin 6) of V6248 has the same polarity as the ripple voltage at the -150 -volt output. C628 couples this ripple output voltage to the grid of V634. The ripple voltage is further amplified by V634 and applied to the grids of the series regulator tubes with a polarity that opposes the original ripple voltage. Ripple in the positive side of the -150 -volt supply is coupled into a degenerative feedb ick loop through R637 to the screen of V634.

Some of the components in the -150 -volt supply are not necessary in normal operation but are included to insire proper operation of the circuit under adverse conditicns. C636 provides for proper operation of the circuit wien extremely low temperatures reduce the capacitance of the electrolytic filter capacitors. R640 and R641 protect aga.nst large surge currents, and C642B suppresses sudden kiad changes that fall outside the bandwidth of the reguloror circuit.
+100 -Volt Supply. The input to the +100 -volt supply is the output of secondary winding 19-20 of transformer TCO1 and silicon-diode bridge D672, In addition to its other loads, the +100 -volt supply is required to supply curr-nt to a series string of filaments at all times. When the Type 547 is first turned on, relay K601 contacts are open and all the regulated supplies are inoperative. During this timie, the series-string filaments are supplied by the unregulaiad side of the +100 -volt supply through relay contacts K 6014 . By the time thermal relay K600 activates K601, the seriusstring filaments have reached operating temperature. Whan $K 601$ is activated by $K 600$, relay contacts K $601-4$ shift the series-string filaments to the regulated output of the +110 . volt supply.
The reference voltage source is the regulated output of the -150 -volt supply. V664A is the error amplifier, V664B compensates for V664A grid-cathode contact bias changes caused by changing line voltage, and V677 is the seties regulator tube. The error-feedback circuit is through RG50 and R651, the junction of which is connected to the grid of V664A. The top end of R650 is connected to the regulated +100 -volt output, and the lower end of R651 is connected to the output of the regulated - 150 -volt supply to obtcin reference voltage. With normal line voltages and loads, the voltage at the junction of R650 and R651 is about -1.7 vo ts with reference to ground; this is the operating bias of V6644.
If the load current, output voltage, or the input valta ie changes (including changes due to ripple), the output of the regulated +100 -volt supply starts to change also, tut any change appears across R650 and R651 and is applied '0 the grid of V664A as a change in operating bias. Assuming that the output of the regulated +100 -volt supply tries 'o decrease, the reduced voltage at the top end of R650 pormits the voltage at the junction of R650 and R651 to 50 more negative than the normal -1.7 -volt level at that poirt. The increase in negative bias on the grid of V664A reduc:s the flow of plate current through V664A, the voitage drcp across plate load resistor R663 decreases, and the pla'e voltage of V664 and the grid bias of V677 go more po: :tive. As the grid of V667 goes more positive, the resistanne that V677 offers to the flow of current is decreased and tie output voltage rises, compensating for the drop in oulp it voltage which initiated regulating action. Of course, the
regulator circuit can never completely compensate for a change in output voltage, for there must be an error input for the circuit to operate, but any error in output is reduced by a factor equal to the loop gain of the regulator circuit.

The screen grid of V664A is used as a signal grid for injecting a sample of any ripple or transient voltage present in the unregulated side of the +100 -volt supply into the regulator circuit. The regulator circuit thereby becomes a dynamic filter for ripple reduction. The ripple signal is applied to the screen of V664A, amplified and inverted in phase by V664A, then applied to the grid of V677. By the time the amplified and inverted ripple gets to the grid of V677, it is of proper amplitude and phase to cancel out the ripple appearing at the plate of V677.

To keep the proper load on the +100 -volt supply when the vertical plug-in preamplifier is removed, a plug-in sensing switch is built inte the main frame of the Type 547 at the top rear of the plug-in compartment. When the plug-in unit is removed, the sensing switch connects a resistive load in place of the series.filament string. When it is desired to operate the plug.in unit outside the Type 547 by means of a test harness, the sensing switch must be manually operated. To manually operate the switch, pull the plastic plunger outward to the stop position,

Unregulated $\mathbf{+ 3 2 5}$-Volt Supply. The unregulated +325 volt supply voltage source differs somewhat from the voltage sources for the -150 . and +100 -volt supplies. A centertapped secondary (13-14-15) on T601 and silicon diodes D702 and D732 form a center-tapped bridge rectifier circuit with the negative side connected to the positive unregulated side of the voltage source for the +100 -volt supply. The unregulated $\$ 325$-volt output is taken from the transformer centertap (14) connection.

The unregulated output of the voltage source for the +100 -volt supply is approximately +180 volts. The unregulated output of the center-tapped bridge circuit is approximately +290 volis; this, added to the unregulated +180 volts provides the +470 volts. However, for the unregulated +325 volt output, the connection is made at the center tap $(+145$ volts) of the bridge (the midpoint of the +290 volts). Adding the +180 and +145 volts provides the desired output of +325 volts.
$\mathbf{+ 2 2 5 - V o l t ~ S u p p l y . ~ T h e ~ v o l l a g e ~ s o u r c e ~ f o r ~ t h e ~ r e g u l a t e d ~}$ +225 -volt supply is the unregulated +325 -volt supply described in the preceding paragraphs. The regulator circuit is similar to the regulator circuit found in the -150 -volt supply; the main difference being that instead of using a glow discharge tube as a reference voltage source, the reference voltage is from the -150 -volt supply. The error signal is picked off the junction of precision resistors R680 and R681. The upper end of R680 is connected to the +225 -volt output, and the lower end of R681 is connected to the regulated -150 -volt supply. The voltage at the junction between R680 and R681 is approximately -0.9 volt which is applied through R682 and R683 to the grid of V684B. The cathodes of V684 are longtailed to the -150 -volt supply through 82 k resistor R685. The grid of V684A is grounded. The error signal is fed from the grid of V6848 through the commoncathode circuit to the A side of the tube. Notice that this comparator is somewhat different from the comparator used in the -150 -volt supply; the output is taken from the $A$
side. The error signal is amplified by V684 and fed, unchanged and in phase, to the voltage divider in the grics of V694. V694 also amplifies and inverts the error signal ind applies it out of phase with any change in the +225 . olt output, to the grid of series regulator tube V707.

Here again, the screen of the error amplifier tube is acting as an injection grid for ripple reduction. A sample of the unregulated supply ripple is applied to the screen of Ve94. V694 amplifies the ripple, inverts it in phase, and applies it to the grid of series regulator tube V707. The result is inat the same ripple appears simultaneously on the grid and plate of V707, but $180^{\circ}$ out of phase; thus the ripple can els out.
$\mathbf{+ 3 5 0}$-Volt Supply. The input to the +350 -volt suppl: is the fuil voltage output of the center-tapped bridge lisee description of unregulated +325 -volt supply) added to the unregulated side of the +100 -volt supply. The operation of the regulator circuit is very similar to the operation of the +100 -volt regulator except for different component values and no grid-cathode contact-bias compensating diode.

## Crt Circuit

The cit circuit (see Crt schematic) includes the crt, the high-voltage power supply, and the controls necessary to focus and orient the display. The crt (Tektronix Tjpe T5470-31-2) is an aluminized, 5 -inch, flat-faced, glass at with a helical post-accelerator and electrostatic focus and deflection. The crt circuit provides connections for externcilly modulating the crt cathode. The high-voltage power supsly is composed of a dc-to-50-kc power converter, a voltogeregulator circuit, and three high-voltage outputs. Frentpanel controls in the ert circuit adjust the trace rotation (screwdriver adjustment), intensity, focus, and astigmatim. Internal controls adjust the geometry and high-valtage cutput level.

High-Voltage Power Supply. The high-voltage power supply is a dc-to-ac converter operating at approximately 50 kc with the transformer providing three high-voltage outpits. The use of a 50 -kc input to the high-valtage transforiver permits the size of the transformer and filter components to be kept small. A modified Hartley oscillator convi fts de from the +325 -volt unregulated supply to the $50-\mathrm{kc}$ injut required by high-voltage transformer T801, C808 and the primary of T801 form the oscillator resonant tank cire jit, No provisions are made for precise tuning of the ascillator tank since the exact frequency of oscillation is not important.

Voltage Regulation. Voltage regulation of the high-voltoge outputs is accomplished by regulating the amplitude of oscillations in the Hartley oscillator. The - 1850 -volt outiut is referenced to the +350 -volt regulated supply througt a voltage divider composed of R841, R842, R843, R845, R8 16 , R847, R853, and variable resistors R840 and R846. Through a tap on the voltage divider, the regulator circuit samf'es the -1850 -volt output of the supply, amplifies any erturs and uses the amplified error voltage to adjust the scrien voltage of Hartley oscillator V800. If the -1850 -volt outiut changes, the change is detected at the grid of V8148. The detected error is amplified by V814B and V814A. The et or signal at the plate of V 874 A is direct coupled to the scrcen of V800 by making the plate-load resistor of V814A serve as
the screen-dropping resistor for V800. Any change in the -1850 -volt output thus changes the screen voltage of V800 and the amplitude of the $50-\mathrm{kc}$ oscillations. R 840 provides a means of controlling the high-voltage output through controlling oscillation amplitude.

Cit Grid Supply. The approximately - 1950-volt output of the high-voltage power supply is the rectified output of one of the two high-voltage secondaries on T801. To provide dc-coupled unblanking signals to the crt grid, the crt grid supply is floating (the dc voltage levels on the components shift in accordance with the unblanking signals). The positive side of the crt grid supply is returned to the -150 volt supply through the unblanking cathode-follower load resistor of the selected sweep generator and through R831 and R832. The negative side of the ert grid supply is applied through the INTENSITY control to the ert grid.
At the fastest sweep rates, the stray capacitance of the floating crt grid circuit makes it difficult for the crt grid to rise fast enough to unblank the crt in the required time. An isolation network consisting of R827, R828, C828, C829, and C830 isolotes the capacitive loading. By this arrangement, the fost leading edge of the unblanking pulse is coupled through C830 and C828 to the grid of the crt. For shortduration unblanking pulses, such as those that occur at the fastest sweep rates, the de levels on the rectifier and secondary winding ore not appreciably affected. Longer unblanking pulses, such as those that occur at the slower sweep rates, charge the stray capacitance in the -1950 -volts output through R827. This pulls up the floating ct grid circuit and holds the cit grid at the unblanked potential for the duration of the unblanking pulse.
+8150 -and $\mathbf{- 1 8 5 0}$-Yolt Outputs. Both the +8150 -and the -1850 -volt outputs are derived from the same secondary winding on T801. The full secondary voltage of approximately 2900 volts is applied to a voltage tripler consisting of rectifiers V832, V842, and V852 and associated capacitors. A tap on the secondary provides the input for half-wave rectifier V862 in the -1850 -volt output. Both outputs are referenced to the regulated +350 -volt supply through a valtage divider network. The +8150 -valt output is connected 10 the eft post-deflection-accelerator anode and the -1850 volt output is connected to the crt cathode, providing a total accelerating voltage of 10,000 volts.

Crt Circuit Controls and Connectors. Optimum size and shape of the fluorescent spot on the ert is obtained by adjusting the front-panel FOCUS and ASTIGMATISM controls. FOCUS control R846 provides the correct voltage for the second anode (focus ringl in the crt. Proper voltage for the third anode is obtained by adjusting ASTIGMATISM control R864. In order to obtain optimum spot size and shape, both the FOCUS and ASTIGMATISM controls are adjusted to provide the proper electronic lens configuration in the region of the second and third anodes of the crt. Spot intensity is adjusted by means of front-panel INTENSITY control R826. Varying the INTENSITY control changes the voltage on the crt grid, which in lurn varies the density of the electron stream. Internal GEOMETRY control R861 adjusts the isolation shield voltage in the cr , and is adjusted to minimize "bowing" or "filting" of the display. Front-panel TRACE ROTATION control R778 permits minor adjusiments in trace orientation. By adjusting the TRACE ROTATION control,

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the trace can be made parallel with the horizontal lines on the graticule, eliminating the need to physically lurn the crt to correct for minor deviations of the trace from the horizontal.
An input binding post on the rear panel of the Type ; 447 provides an input for externally modulating the crt cathede. The input binding post is normally grounded by a link if it is desired to intensity modulate the display from an external source, the link is opened, and the modulating signal is coupled to the crt cathode through C858.
When the Type 547 is used with a multichannel vert cal plug-in preamplifier that provides dual-trace chopped blanking pulses, the blanking pulses are applied to rear-ponel CRT CATHODE SELECTOR switch SW858. With the vert sal plug-in preamplifier operating in the chopped mode (ind SW858 set to the CHOPPED BLANKING position, a posi'ive pulse of approximately 20 -volts amplitude is applied throigh C858 to the cathode of the crt. At normal intensity levels, this pulse is sufficient to cut off the crt during the time the amplifier channels in the vertical plug-in preamplifiers se being switched.

## Vertical Amplifier System

The vertical amplifier system in the Type 547 consists of an appropriate vertical plug-in preamplifier, a push-pull catho lefollower input stage, a push-pull transistorized delay-1 ne driver, a delay line, and a push-pull transistorized outsut amplifier. In addition, the trigger-pickoff circuit functions as a part of the vertical amplifier by providing reverse termi iation for the delay line.

Vertical Input Amplifier. The push-pull output of the vertical plug-in preamplifier, with a fixed de level of appr $1 x$ imately +67.5 volts, is applied to the input of the vert: :al amplifier through terminals 1 and 3 of the plug-in connectir.

Transient-response compensation switch SW1000, capecitor C1000, and resistor R1000 at the input of the verh:al amplifier compensate for the difference in transient respoise that exists between different models of vertical plug-in $\mathrm{F}^{\prime} \mathrm{e}$ amplifiers. SW 1000 is actuated by a mechanical sensng device when the plug-in unit is inserted into the oscillosco $1 e$, and requires no attention on the part of the operator.
R1001 and R1011, in series with the grids of the push-f ull cathode-follower stage, are parasitic suppressors. In Int cathode followers V1003A and V1003B are the two hal es of a 12AT7 twin triode. The cathodes of the cathode |31lowers are relurned to ground through vertical dc balar ce control R1004, which is adjusted to equalize the de voltoge (about +68.5 volts) on the bases of delay-line driver tran istors Q1014 and Q1024. The heaters of V1003 are operal ad as part of the series string which receives power from 've +100 -volt dc supply. The use of dc on the heater preve its changes in line voltage from affecting the gain of the verti al amplifier.
The balanced delay-line driver stage is a push-pull an plifier with an adjustable vertical gain control ( $R 1017$ ) ornnected in the emitter circuit of the two transistors. Gain is adjusted by controlling the amount of degeneration in ine emitter circuit. Zener diode D1018 sets the operating poits of the termination transistors on both ends of the delay lise.

The RC networks in the collectors of Q1014, Q1024, Q1144, Q1154, and in the emitter leads of Q1034 and Q1044 set the individual transistor operating points to achieve thermal balance. The 5 -turn center-tapped cuils at the input of the delay line and the collector-base capacitance of the delay-line driver transistors form a T-section matching network. C1029 provides a means of varying the impedance of the $T$ section.

Vertical Output Amplifier. The vertical output amplifier must properly terminate the delay line and provide broadband amplifitication of the vertical signals. Proper termination of the delay line is obtained by connecting forwardtermination transistors in a common-base configuration. The common-base configuration also operates well in broad-band amplifier applications. To help meet the broad-band requirement, the collector load circuit of the termination transisfors contains RC low-frequency compensation networks, and in addition, LR network in the collectors of transistors Q1034 and Q1044 compensate for losses due to skin effect within the delay line.

Following the forward-termination amplifier is a wideband amplifier stoge consisting of Q1074 and Q1084 and associated elements. High-frequency compensation in this stage is provided by shunt peaking coils 11072 in the collector circuits. The high-frequency response is varied by adjusting C1076, which provides variable high-frequency degeneration in the emitter cirevit of Q1074 and Q1084.
The output stage of the vertical amplifier is a transistorized equivalent of a push-pull cascode amplifier. This circuit configuration is used to match the low impedance of the transistorized vertical-amplifier system to the higher impedance required at the ert vertical deflection plates. High-frequency compensation is provided by re networks between the collector of the driving transistor and the emitter of the driven transistor on each side. C1105 and C1106 provide a means of varying the high-Irequency response of the output stage. The outputs from Q1114 and Q1134 are connected to the deflection plate of the crt via seriespeaking coils $\$ 1115$ and 61135 .

Trigger-Pickoff Circuit. The trigger-pickoff circuit provides reverse termination for the delay line as mentioned in the preceding paragraphs. The input stage of the trigger-pickoff circuit, which provides the delay-line reverse termination, is a common-base circuit. The output stage of the triggerpickoff circuit is a push-pull emitter-follower amplifier that not only provides trigger signals to the two time bases, but supplies the VERT SIG OUT jack with a vertical signal and drives position indicator amplifier V1184.

## Main Time Base (B)

The main time base ( $B$ ) consists of the $B$ sweep trigger and the B sweep generator circuits. The B sweep trigger circuit is a wide-band hybrid amplifier driving a tunnel diode. The B sweep trigger circuit includes controls for selecting the type, source, and level of the trigger to be used, and circuit elements for regenerating the selected trigger into a pulse suitable for triggering the 8 sweep generator. The B sweep generator circuit is basically a Millerrunup circuit. The B sweep generator provides ramp voltages for the horizontal deflection system, alternate-trace sync pulses, unblanking puises, and +B gate pulses.

## Trigger Generator

The input to the B sweep trigger circuit (see B Swe ep Trigger Generator schematic) is selected by SOURCE swich SWI from the trigger-pickoff circuit in the vertical amplifier, the trigger output of the vertical plug-in preamplifer, the power transformer for line triggering, or from the frentpanel TRIGGER INPUT connector. COUPLING switch SWV5 permits further selection of the type of triggering signal; either ac, ac with low frequencies rejected, or dc. Orice the type and source of triggering signal has been select d , the slope on which triggering is desired is selected by SLCPE switch SWIO. The level of the triggering signal required by the 8 sweep trigger circuit is selected by adjusting TRIGGERING LEVEL control R15. After this triggering signal las been selected by the foregoing controls and switches, it is applied to trigger input amplifier V24.

Circuit Description SN 6740-UP. V24A and V24B form a switching comparator. The voltage level at which the conparator switches is set by the B TRIGGERING LEVEL eintrol R15. V24 drives Q34 and Q44, which form a currint type switching comparator. Q34 and Q44 drive tunnel ji ode D45 which in turn drives sweep gating tunnel diode D85.

If no triggering signal is applied to V 24 the stage cunsisting of V24A and V24B is unbalanced. One section (which one depends upon the setting of the B SLOPE and B TR/FGERING LEVEL controls) is conducting more current than 'he other. The voltages at the plates of V24A and V248 shoild therefore be different. However, diodes D21 and D22 clainp the two plate voltages to within 0.3 volt of each othar, with the plate of the section which is conducting the mist current being the most negative.

The second stage, made up of Q34 and Q44, is also unbalanced. The transistor whose base is the most nesiative conducts most of the current supplied by R36. This


Fig. 3-2. Tunnel diode characteristics.
current is not sufficient to cause the conducting transistor to saturate. The conducting transistor merely acts as a constant current source.

Tunnel diode D45 is biased to its low voltage state by current through R32, R33, R45, and R42. If the comparator stages are unbalanced in such a manner as to cause Q34 to conduct, an additional current flows through D45. This additional current biases D45 to its high voltage state (see Fig. 3-2 for tunnel diode characteristic curve).
When the current through D45 reaches a total of 10 mA the voltoge across D45 will suddenly increase to approximately 0.5 volts. This sudden voltage change is coupled to the sweep gating tunnel diode D85 by C56, D59, and C57. C56 differentiates the triggering signal which provides a fast rising pulse for D85. L56 and the low impedance of conducting diode D57 decrease the fall time of the triggering polse. D59 ensures that D85 is only triggered when D45 turns on, and not when D45 turns off.

Circuit Operation SN 101-6739. In operation, V24A and V24B form a push pull amplifier which drives a push-pull input, single-ended output amplifier consisting of Q34 and Q44, Tunnel diode D45 is biased at its low-voltage state (see Fig. $3-2$ for trigger tunnel-diode curve) by current flow through the voltage divider consisting of R44, R45, R47, and R48. When the desired slope of the triggering signal selected arrives at the grids of V24, V248 and Q44 are biased into conduction. The conduction of Q44 increases the current flow through D45, and D45 switches to its high-voltage state. The sudden voltage change across D45 as it switches to its high-voltage state produces a uniform last-rising trigger pulse which is used to trigger the main time base ( $B$ ) sweep generator.

## Sweep Generator

For purposes of explanation, assume that the HORIZONTAL DISPLAY switch (see B Sweep-Generator schematic) is in the B posittion, the SINGLE SWEEP switch is in the NORMAL position, the TRIGGERING MODE switch is in the TRIG position and that no trigger is being applied. Under these conditions, V145A in the holdoff multivibrator is conducting and V1458 is cut off. The paths for the current in V145A are from the -150 -volt supply through R164 and D163 in paraliel with R163. When V145A is conducting and no trigger is being received from the trigger generator, D85 is in its low-voltage state since the de current supplied from the +100 -volt supply through R82 and R81 is less than the peak current of D85. Under these conditions, Q84 is cut off. For SN 12480 and above, the collector voltage of Q84 is positive, thereby forward biasing Q86, D86, Q89 and Q103. (For units with serial numbers below SN 12480, the collector voltage of Q84 is positive, thereby forward biosing D86, Q89 and Q103.) Miller tube V91 is conducting. The circuit is now ready to be triggered.

Assuming that a trigger pulse is now applied, the positive trigger from the B sweep trigger circuit is coupled through C56 to 156 and D57. C56 and L56 form a differentiating network that narrows the trigger pulse to approximately 4 nsec in width. The sharpened trigger pulse passes through D59 to tunnel diode D85 and causes D85 to switch to its high state, where it remains after the trigger pulse decays to zero. When D85 switches to its high state, Q84 is biased into saturation and the voltage change across Q84 applies

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forward bias to Q173 and reverse biases Q89, Q103, ind D86. When D86 is reverse biased, the voltage on the !rid of V91 goes negative and the Miller circuit starts to run up. As the voltage on the cathode of V93A goes positivc, it starts to charge timing capacitor C90 through D98. At high sweep rates, boot-strap capacitor C94 couples the ri:ing cathode voltage to the plate circuit of V91 and effectively increases the plate supply voltage for V91, compensating for losses introduced by stray capacitance. In addition, the positive-going cathode voltage of V93A forward biases DI29 and starts putting a positive voltage on the grid of V1451: in the holdoff multivibrator, At a point determined by sweeplength resistor R125, the rising positive voltage biases VI 158 into conduction, and the holdoff multivibrator changes st the, cutting off V145A. When VI45A cuts off, its cathode voltrige drops to -20 volts and reverse biases D85 and Q84. As current flow through Q84 ceases, the voltage incre, sse across it again forward biases D86. When D86 beco nes forward biased, it applies a positive going voltage to the surid of V91 which resets the Miller circuit and ends the swcep.

Disconnect diode D100 ensures that the sweep starts fiom the same voltage point each time. Q103 is included in the circuit to reduce the amount of current that D100 has to switch, and thereby improves the linearity at the start of the sweep.

When the sweep ends, V145B has control of the holcioff multivibrator, and remains in control until the charge on holdoff capacitor C130 discharges through R130, During the time that VI45B has control of the holdoff multivibra'or, funnel diode D85 cannot be triggered; but when the holcoff capacitor discharges to the point where V145A can again assume control, D85 is again biased to a point where it an accept another trigger.

Automatic Stability Circuit. Q65, Q75, and associa'ed circuit components form a monostable multivibrator mat controls the stability of the B sweep generator. When the trigger MODE switch is in the TRIG position, the swich grounds the collector of Q75 and disables the automutic stability feature of the Type 547. When the triggering MODE switch is in the AUTO STABILITY position, the sweep geneiator free runs if no trigger pulses are received from the trigger generator.
In normal operation, Q65 is conducting due to the posit ve voltage applied to its base. Q75 is normally cut off rve to its base being grounded through R69. When the trig, ler MODE switch is set to the AUTO position, C76 starts to charge through R76. When the voltage across C76 exce ids the breakdown of Zener diode D76, D76 breaks down and provides an additional current path for tunnel diode D. 35 . The additional current through D85 causes it to switch to its high state and start the sweep. When the sweep ends and the holdoff multivibrator switches, the voltage on the cathede of V145A drops to approximately -20 volts, reverse bias ng D85. When the holdoff period ends, the cathode voltage of V145A goes slightly positive, and the current through [.76 again switches D85. If no trigger is applied, the cycle epeats only if the trigger MODE switch is in the AUTO pe sition.

When a trigger pulse is received at T52, a negative ost put from the secondary is applied to the base of G65 and causes the monostable multivibrator to switch. W th

Q65 now cut off, its collector voltage goes more positive, and C67 charges through R69, applying a positive voltage to the base of Q75. The positive voltage on the base of Q75 biases it to saturation, and Q75 provides a low-resistance path that discharges C76 and reverse biases D79 and D76. With the collector of Q75 below the D76 breakdown voltage, the collector circuit does not provide switching current for tunnel diode D85, so the only way D85 can be switched is by the application of a trigger pulse. If no further trigger pulses are received, Q75 is kept in saturation until the charge current for C67 decays and removes the positive voltage from the base of Q75.

During the charge time of C67, Q65 is kept cut off by the forward voltage drop across D71. When the decaying charge current removes saturation bias from Q75, the voltage drop across D71 decreases and permits Q65 to conduct, and the multivibrator switches back to its normal state. If no further trigger pulses are received, C76 charges through R76 and R75 until D76 again breaks down and provides switching current for D85.

Unblanking Circuit. With the HORIZONTAL DISPLAY switch set in the B position, an unblanking pulse is generated and applied to the crt unblanking circuit during B sweep time. The unblanking pulse is initioted when tunnel diode D85 switches to its high state and biases Q84 into conduction. When Q84 conducts, its collector voltage drops and removes the cutoff bias from Q173, biasing Q173 into conduction. When Q173 conducts, it removes the negalive bias from the emitter of Q184 and the grid of V193A. The base of Q184 is negative by the amount of forward voltage drop across D182, while the emitter is positive by the amount of forward voltage drop across D183. The sum of the forward voltage drops across the two diodes is sulficient to bias Q184 into conduction. When Q184 conducts, it puls a positive-going voltage on the grid of cathode follower V195B, and the positive-going voltage is coupled to the crt-unblanking supply.

Single-Sweop Circuit, When single-sweep operation is desired, NORMAL-SINGLE SWEEP-RESET switch SW1 35 is set to the SINGLE SWEEP position. When SW135 is pushed to the RESET position it operates switch SW369 which discharges C369 (see A Sweep Generator schématic) through R369, R368, and R367, generating a positive pulse which is applied through C166 and D164 to the cathode of holdoff tube V145B. The positive pulse on the cathode of V145B causes the holdoff multivibrator 10 switch, and V145A biases sweep tunnel diode D85 to the ready point as previously explained. Since Q84 and V145B are both cut off, the positive voltage on the collector of Q84 and the voltoge on the plate of V145A combine through R87 and R142 produce turn-on bias for Q89. When Q89 conducts, it completes the circuit for the NE- 23 READY lamp (B89). With the application of a trigger pulse, QB4 conducts and the voltage on its collector drops, removing the bias on Q89 and thereby extinguishing the READY lamp. The runup of the Miller circuit causes the hold-off mulitvibrator to switch, and V1458 takes control. NORMAL-SINGLE SWEEP.RESET switch SWI35 applies a positive voltage through D132 to the grid of V145B, and this positive voltage prevents the holdoff multivibrator from resetting until NORMAL-SINGLE SWEEP-RESET switch SW369 has been moved to either the RESET or NORMAL position.

Main Time Base (B) Sweep Timing. The sweep rate the rate at which the spot moves across the face of the crt is determined by the rate at which the timing capacitor and timing resistor permit the Miller circuil to run up. By means of TIME/CM or DELAY TIME switch SW90 (see B Sweep Timing. Switch schematic), both the size of the capacitor being charged and the charging current can be selected to co er a wide range of sawtooth slopes (sweep rates). Note that SW90 is connected so that switching 8 capacitors and 6 resistors provides 24 different sweep rates, varying from $5 \mathrm{sec} / \mathrm{cm}$ to $0.1 \mu \mathrm{sec} / \mathrm{cm}$ without magnification. The TIME/CM or DELAY TIME switch also selects the proper holdoff copocitor and discharge resistor for the sweep rate in use.

Continuously variable uncalibrated sweep rates are p.o. vided by R90Z and SW90Z (VARIABLE control). When SW 90 Z is switched to the UNCAL position, it removes the sh irt from around R90Z and switches on UNCAL lamp B90W, By turning VARIABLE control R90Z, the charging time of the ti.ning capacitor selected by the TIME/CM or DELAY TIHE switch may be increased by a least 2.5 times the calibratiod rate, providing continuously variable sweep rates.

Delay-Pickoff Circuit. The delay-pickoff circuit (see Del 3y Pickoff schematic) generates a trigger pulse that is delay ad form the start of the B sweep by an amount determined by the settings of the Main Time Base (B) TIME/CM or DELAY TIME switch and the DELAY-TIME MULTIPLIER dial. A conparator in the delay-pickoff circuit continuously monitors the ramp output voltage of the main time base ( $B$ ) Miller runup circuit and compares the ramp voltage with a voltage leiel established by the setting of the DELAY-TIME MULTIPLIER dial. When the ramp voltage bioses V404A into conduction, the comparator switches a lunnel diode. The tunnel diode generates a trigger pulse that is delayed from the start of the B sweep by the time it takes the ramp voltage to rise to a value approximately equal to the voltage established by the DELAY-TIME MULTIPLIER dial setting. After being amplified, the delayed trigger is applied through the HORIZONTAL DISPLAY switch as a source of delayed trigger for the tive base A generator, and to the DLY'D TRIG output connect or on the front panel for use in external equipment. Delay :d trigger pulses are connected to the time base A sweup generator when the HORIZONTAL DISPLAY switch is in the B INTENS BY 'A', A DLY'D BY B positions, and the ALT position between the two.
In actual operation, the comparator is longtailed throu ih a constant-current tube that keeps the current through the comparator relatively constant despite the large voltarie swings applied to the grids. The grid voltage of constantcurrent tube V93B is fixed at approximately -56 volts liy the voltage divider consisting of R406 and R407. With the grid of V93B biased at approximately - 56 volts, R409 maintains the current through V938 (and thereby the comparat or tube) to approximately 5 ma .

Comparator tube V404 receives the ramp output of the main time base $(B)$ sweep generator on one grid and the voltage from the tap on delay-time heliopot R416 on the other, At the start of the ramp, V404B is conducting ard V404A is cut off. Assume that the ramp input to the collparator is increasing at the rate of $10 \mathrm{volts} / \mathrm{msec}$, and the DELAY-TIME MULTIPLIER dial is set at 2.0 ( 2.0 is equal 'o 20 volts of a 100 -volt rampl, then the voltage on each gr d of the comparator becomes 20 volts, 2 msec atter the ran p starts. At this point, V404A starts conducting. V404A drav/s
current through R404, L404, and tunnel diode D405. The current flow through D405 causes it to switch to its high state, generating a sharp trigger pulse. R404 and L404 narrow the hysteresis zone of D405. The low resistance of R404 would attenuate the trigger pulse if it were not for the high-frequency peaking effects of L404. The trigger voltage developed across D405 is amplified by Q424 and applied to Q433 through a differentiating network. The output of Q433 is applied to the DLY'D TRIG connector on the front panel and to the HORIZONTAL DISPLAY switch as previously mentioned.

Jack J 435 provides a means of coupling in an externallygenerated delayed trigger. Terminals B and C provide function information to the external trigger generator, and the externally-generated delayed trigger is applied to terminal A. It is also necessary to apply sufficient dc bias to terminal A to back bias D433.

## Time Base A

Time base A in the Type 547 is very similar to the main time base (B) and the circuit description for main time base (B) generally applied to time base $A$. The two trigger-generafor schematics, in particular, show few differences other than circuit symbols.

The major differences in the two time bases are Q344 and cathode follower V293B which appear on sweep generator A but not on B, and Q184 (the function of which is described in the discussion of main time base (B) which appears on sweep generator 8 but not on A. Q344 is part of the alter-nate-sweep lockout circuit which is explained later in this section. Cathode follower V293B is a conventional long. tailed cathode follower that provides a sample of the output of the A sweep generator to the A SWEEP front-panel output connector.

## Alternate Sweep Switching Circuit

The alternate sweep switching circuit gates the desired sweep voltage to the horizontal deflection plates of the crt , provides trace-positioning voltages, and when a dual-channel vertical plug-in preamplifier is used, slaves the alternate trace multivibrator in the plug-in unit.

When the HORIZONTAL DISPLAY switch is in either ALT position, the alternate sweep switching circuit prevents B sweep from being unblanked whenever A sweep is being displayed.
Sweep Switching Multivibrator. The sweep-switching multivibrator (see Alternate Sweep Switching schematic) consisting of Q465, Q475, and associated circuit components is a conventional bistable transistor multivibrator. In alternatesweep operation, the multivibrator is switched by the trailing edge of a sweep-gating pulse from either time base. As the sweep-gating pulse ends and starts to go positive, Q464 is biased into conduction and applies a negative-going sig. nol to the differentiating network consisting of C459 and R459. The sharpened pulse is applied through D469 and D479 to the bases of both transistors in the multivibrator, cutting off the conducting transistor and turning on the other.
Assuming that Q465 is the conducting transistor, the resistance between its emitter and collector is quite low, effectively grounding its collector. With the collector of Q465 at ground, the voltage division accoss R467 and R479
applies approximately -3 volts to the base of Q475, keaping it cut off. With Q475 cut off, the voltage division across R467 and R479 applies sufficient bias to the base of Q465 to keep it saturated.

Sweep Gates. D461, D462, D471, D472, and associaied circuit components form an exclusive "or" gate. With Q. 65 saturated and Q475 at cutoff as described in the preceding paragraph, current flow through Q465 and D461 reverse biases D462, preventing the B sweep ramp voltage from passing through D462. With Q475 cut off, its collector voltag. is held at approximately +27 volts by Zener diode D475. This +27 volts reverse biases D471. The A sweep circuit then torward biases D472. D472 forward biased, the A sweep gat: is open, and the A sweep ramp voltage passes through to the horizontal amplifier. When Q475 is the conducting transisior, it forward biases D471 and reverse biases D472, closing the gate for the A sweep. When Q475 conducts, Q465 cuts off and opens the B sweep gate.

Trace-Separation Amplifier. In the ALT positions of the HORIZONTAL DISPLAY switch, the collector of Q475 is sinnected through the switch to D482 and D492 in the tra: e separation amplifier. When Q475 is cut off, D482 and D492 are reverse biased, and the operating points of V494A and V494B are determined by the setting of TRACE SEPARATIGIN control R484. The outputs of V494A and V494B are applied to opposite sides of the push-pull vertical amplifier and pessition the A trace in accordance with the setting of the TRACE SEPARATION control. When Q475 is saturated (during B sweep), D482 and D492 are forward biased, effectivily grounding out the positioning voltage from the TRACE SEPARATION control. Since Q475 alternates between cutoff and saturation with the HORIZONTAL DISPLAY switch in the ALT positions as explained in the preceding paiagraphs, the bias on trace-separation amplifier V494 is shiflad in synchronism with the alternate sweeps, thus providing trace separation.

A Sweep Terminating Circuit. When the HORIZONTAL DISPLAY switch is in B INTENS BY ' A ' or the adjacent ALT position and the B sweep intensified by A sweep is being displayed, it is desirable that the A sweep be terminated not later than the end of the B sweep. When the HORIZONTAL DISPLAY switch is in either of the foregoing positions, the signal at the plate of VI45A lin the B sweep.generator holdoff multivibrator) is coupled through the HORIZONTAL DISPLAY switch and C449 to the base of Q414. At the instant that the B sweep ends the B sweep-holdoff multivibrator switches, the voltage at the plate of V145A goes positive, and a differentiated positive spike is applied to Q444. The positive spike is amplified and inverted by Q414, and the now negative spike is coupled through C441 and D347 to the grid of V345B in the A sweep-holdoff multivibrator. If the A sweep-holdoff multivibrator has not yet switched and stopped the A sweep, the negative spike from Q444 triggers the sweep-holdoff multivibrator and stops the sweep. If the A sweep has not yet started, the negatise pulse resets the A sweep-holdoff multivibrator.

When the HORIZONTAL DISPLAY switch is in the ALT position (between B INTENS BY ' A ' and A DLY'D) some means must be used to disable the B sweep terminating pulse during the time that the delayed A sweep is being displayed. At His time, Q465 in the alternate-sweep switching multivibrator is soturated, so the B sweep terminating pulse is couplid
through D449 to the collector of Q465, where it is effectively grounded.

Alternate Trace Blanking. When the Type 547 is operated in the B INTENS BY ' $A$ ' - ALT - A DLY'D mode, it is necessary to keep the B sweep unblanking circuit cut off during the part of the sweep-switching cycle in which only the delayed A sweep is displayed. Cutoff is accomplished by applying the positive A sweep-gating voltage from the collector of Q475 to the base of Q184. When the HORIZONTAL DISPLAY switch is in either ALT position, the A sweep-gate voltage taken from the collector of Q475 is applied through the switch to D481. When the A sweep-gate voltage is positive, D481 is forward biased, and applies the positive voltage through R181 to the base of Q184. The positive voltage applied to the base of Q184 during the time that the A sweep gate is open is sufficient to keep Q184 cut off despite the unblanking signal from Q173.

## Alternate-Sweep Lockout and Blanking Circuits

When aiternate $A$ and $B$ sweeps are to be displayed, the horizontal amplifier and the ert must be time-shared between the two displays. Alternate-sweep lockout and blanking circuits are employed to ensure that the sweeps are displayed in proper sequence. The operations of the circuits for each position of the HORIZONTAL DISPLAY switch are described in the following paragraphs.

A Position. In this position of the HORIZONTAL DISPLAY switch, only the A sweep is displayed. The main time base (B) generator is blanked out by grounding the collector of Q465 in the alternate-sweep switching circuit, In the A position of the HORIZONTAL DISPLAY switch (SW530), the collector of Q564 is grounded through terminals 1 and 5 of wafer BF, Grounding the collector of Q465 closes the B sweep gate composed of D461 and D462. With the B sweep gate closed, any output from the main time base (B) generator does not get through to the horizontal amplifier.

B Position. This position of the HORIZONTAL DISPLAY switch grounds the collector of Q475, closing the A sweep gate composed of D471 and D472. In this case, the output of the A sweep generator is prevented from reaching the horizontal amplifier.

A-ALT-B Position. When the HORIZONTAL DISPLAY switch is placed in the ALT position midway between A and B, the horizontal amplifier and crt must be time-shared between the two time-base sweep generators. Note that in this position of the HORIZONTAL DISPLAY switch, the collector of Q475 is connected through D133 and terminals 9 and 11 of wafer $4 R$ to the 8 sweep-holdoff multivibrator. Likewise, the collector of Q465 is connected through terminals 3 and 10 of wafer 4F to the holdoff circuit of A sweep-holdoff multivibrator. This means that at the instant of turn on, the nonconducting transistor of the altemate-sweep switching multivibrator permits a lockout voltage to be applied to the holdoff multivibrator to which it is connected. The switching inputs to the sweep-switching multivibrator are taken from the plate of V345B in the A sweep-holdoff multivibrator, and from the plate of V145A in the B sweep-holdoff multivibrator. If, at the instant of furn on, no triggering signals are being applied and both TRIGGERING MODE switches are in the TRIG position, there is no sweep. Under
these conditions, if Q465 in the alternate-sweep switching multivibrator is the conducting transistor, the main time base (B) sweep generator is locked out and cannot be triggered until A sweep generator has been triggered. If a trigger is now applied to the A sweep generator, it runs up, its holdoff multivibrator switches, and a switching signal is sent by the holdoff multivibrator to the alternate-sweep switcling multivibrator via Q464. B sweep can now be triggeresl, If Q475 is the conducting transistor at the moment of turn on, and the TRIGGERING MODE switches are in the TRIG position, then the A sweep generator cannot be triggered intil the main time base ( $B$ ) has been triggered.

B INTENS BY 'A' Position. In this position of the H( )RIZONTAL DISPLAY switch and with the TRIGGERING MCIDE switch in the TRIG position, the pulse from the delay-pickoff circuit switches the A sweep-holdoff multivibrator, but the sweep waits for a trigger before starting to run up. When the A sweep generator completes its runup and goes nto holdoff, this fact is signaled to the main time base ( B ) senerator by Q344. The conduction of V345A during the A sweep-holdoff time is sufficient to reverse bias D356, utting off Q344. Cutting off Q344 permits the voltoge at the iunction of R135 and R136 to go more positive, keeping the main time base ( B ) sweep generator locked in holdoff. As the holdoff capacitor in the A sweep generator dischar jes, the voltage on the grid of V345A falls, decreasing the current flow through V345A. When the holdoff capacitor in the A sweep generator is finally discharged, the current flow through V345A has decreased to where D356 is no longer reverse biased, and Q344 conducts, removing the loct out voltage from the main time base ( 8 ) generator holdoff niultivibrator. The main time base (B) generator resets and is triggerable.

B INTENS BY 'A' - ALT - A DLY'D Position. In this pissition of the HORIZONTAL DISPLAY switch, the alternitesweep switching multivibrator alternately gates A sweep delayed by B and B sweep intensified by A into the horizontal amplifier. Note that in this mode of operation the main time base (B) generator sends a sweep-terminating pulse to thi A sweep-generator holdoff circuil at the end of the intensified B sweep, and that A sweep-generator holdoff multivibrator keeps the main time base (B) sweep generator locked out (in holdoff) until the A sweep generator has completed its he.Idoff period and is triggerable. The foregoing actions can be determined by tracing the signals through wafers 7 R, $8 F$, $8 R, 4 F, 4 R, 2 R$, and IF of the HORIZONTAL DISPLAY swith.

B INTENS BY 'A' Position. In this mode of operation, the collector of Q475 in the alternate-sweep switching n.ultivibrator is grounded through the contacts of wafer $8 R$, and the A sweep gate is closed. Contacts 5 and 10 of wofer 4F apply a positive voltage to the grid of V345A in the A sweep-holdoff multivibrator. The positive voltage on the grid of V345A assures that the A sweep generator will say in holdoff until the delayed trigger pulse from the delay-pickoff circuit overrides the holdoff voltage and resets the heldoff multivibrator. If the TRIGGERING MODE switch is in the TRIG position, runup of the A sweep generator does rot commence until a trigger is received from the A sweep-tigger circuit. At the end of the B sweep, Q444 in the alternctesweep switching circuit sends a termination pulse to he grid of V3458 lin the A sweep-generator holdoff mult vibrator) that resets the holdoff multivibrator and termina'es the A sweep.

A dLY'D Position. In this position of the HORIZONTAL DISPLAY switch, the collector of Q465 in the alternate-sweep switching multivibrator is grounded, closing the B sweep gate. The A sweep-generator holdoff multivibrator is kept in holdoff by a positive voltage applied through wafer $4 F$ of the HORIZONTAL DISPLAY switch, and, as in the case where the B sweep is intensified by the A sweep, can be brought out of holdoff only by a reset pulse from the delay-pickoff circuit. When the HORIZONTAL DISPLAY switch is in the A DLY'D position, the action starts when the main time base (B) generator receives a trigger and starts its runup. After a period of time selected by the DELAY-TIME MULTIPLIER dial, the delay-pickoff circuit generates a pulse that takes the A sweep generator out of holdoff. If the TIME BASE A-TRIGGERING-MODE switch is in the AUTO STABILITY position, the $A$ sweep generator starts its runup.

## Alternate-Trace Sync Amplifier

The alternate-trace sync amplifier (see Interconnecting Jack Jll schematic) amplifies and shapes the alternate-trace sync pulses and applies them to the vertical plug-in preamplifier, provides a sample of the pulse to the crt for blanking purposes, and amplifies the chopped blanking pulses from the vertical plug-in preamplifer for application to the crt.

## Horizontal Amplifier

The de-coupled horizontal amplifier (see Horizontal Amplifier schematic) consists of a transistor input amplifier, an emitter follower, a transistor paraphase amplifier, a pushpull vacuum-tube output amplifier, a pair of output cathode followers, and a capacitance-driver tube. In addition, the Type 547 contains a cathode-coupled preamplifier that is used to amplify externally applied horizontal deflection signals. The input to the horizontal amplifier is received from either the alternate-sweep switching circuit or the external HORIZ INPUT connector, depending upon the setting of the HORIZONTAL DISPLAY switch.

Input Stages. The selected input signal is applied to the base of Q534 along with dc-positioning voltages from the horizontal positioning controls. The composite signal output of Q534 is opplied to emitter follower Q543, and from that transistor to the paraphase amplifier. Negative feedback from the emitter of Q543 to the base of Q534 keeps the input and output impedance of the two stages low. R544 in the feedbock loop provides a means of adjusting the amount of feedback, thereby providing amplifier gain adjustment.

Paraphase Amplifier. Q554, Q564, and associated circuit components form a paraphase amplifier that splits the signal from Q543 into push-pull output. The signal from Q554 to Q564 is coupled through the emitter circuit, and by changing the value of the coupling resistor, the gain of the paraphase amplifier is changed to provide sweep magnification. Four selectable values of coupling resistor are available providing XI, X2, X5, or X10 sweep magnification.
The feedback loop from the collector of Q554 stabilizes the gain and balance of the paraphase amplifier. D542 and D561 provide base-operating bias. The feedback loops from the output cathode followers (V574B and V584B) to the emitters of Q554 and Q564 assist in slabilizing the gain of the horizontal amplifier.

## Circuit Description-Type 547/RM547

Output Amplifier and Cathode Followers. The ramp-veltage outputs of the paraphase amplifier are applied to the grids of amplifiers V574A and V584A. The ramp voltages are amplified by the two triodes, which then apply the ramp voltages to the output cathode followers. To maintain the desired linearity at high sweep rates, part of the output from each amplifier is bypassed around the cathode followers through small variable capacitors C572 and C51:2. C576 and C586 together with stray capacitance across R5 ${ }^{\prime} 6$ and R586 form o capacitance bridge to provide correct highfrequency feedback.

Capacitance Driver. The cathode of V574B drives the leithand deflection plate and, during the sweep, the cathoile voltage should go linearly in a negative direction. At high sweep rates, when V574B tries to drive the deflection plate negative, the deflection-plate capacitance and the output capacitance of cathode follower V5748 tend to distort the ideal linear ramp voltage into an re discharge curve. To overcome this tendency toward nonlinearity, the positivegoing ramp voltage at the cathode of V584B is applind through C591 to the grid of capacitance driver tube V5k9. The positive-going valtage on the grid of V589 forces it inıo heavy conduction, and the current supplied through the tulie provides extra current to the cathode of V574B and helps 10 discharge the capacitance in the output of V574B. Since the crt is blanked during the return trace, there is no need f . r a similar current driver at the cathode of V584B.

External Horizontal Preamplifier. The preamplifier appliss external horizontal deflection voltages through the HOKIZONTAL DISPLAY switch to the grid of V5148. For largeamplitude signals, a X10 attenuator position is provided in the HORIZONTAL DISPLAY switch. V514B and V514A form a cathode-follower grounded-grid amplifier, with the gain controlled by adjusting the value of the coupling resistor between the two cathodes. In this case, R511 provides at leost a 10:1 range of adjustment. The output of V514A is applied through the HORIZONTAL DISPLAY switch to the base of Q534.

## Amplitude Calibrator

The amplitude calibrator in the Type 547 is a 1 -kc squarswave generator (see Amplitude Calibrator schematic) thist provides both voltage and a 5 -ma current output to the front-panel connectors. The voltage output is taken from the CAL OUT connector on the front panel, where eith:r a selectable-amplitude squarewave or a steady +100 -volt de
reference voltage is available. By turning the AMPLITUDE CALIBRATOR switch, the amplitude of the square-wave output may be varied from 0.2 mvolt to 100 volis peak-to-peak. The current output is applied to the link marked $5 \mathrm{~mA} \Omega$, with the arrow indicating conventional current flow. When the AMPLITUDE CALIBRATOR switch is in the 100 V DC position, the link has 5 ma dc flowing through it; when the switch is in the $5 \mathrm{~mA} \Omega$ position, the current through the link is in the form of a $1-\mathrm{kc}, 5 \mathrm{ma}$ square wave.

## CAUTION

The link is designed for use with a snap-on current probe and does not unplug.

Square-Wave Generator. The square-wave generator is an astable multivibrator direct-coupled to a cathode follower. V935A and V945 are the mulitivibrator tubes, with the screen of V945 serving as an anode and furnishing feedback to V935A. The plate of V945 operates as an electron-coupled amplifier. The time constants in the grid circuits of the tubes are different to compensate for the difference in their characteristics. When the amplitude calibrator is furned on, the multivibrator cathodes are returned directly to the dc-coupled -150 -volt supply. Since the plate load and grid resistors are grounded, this means that the supply potential of the multivibrotor is 150 valts. The plate of V945 operates from the +225 -volt supply, but is clamped slightly above 100 volts by D942 and D948. The voltage on the plate of V945 swings from about -30 volts to about +102 volts. The plate of V945 is coupled through Zener diode D948 to the grid of sathode follower V935B. CAL AMPL control R943 is adjusted so that when the signal to V 935 is positive, its cathode voltage rises to +100 volts. When the signal from the V945 plate goes negative, V9358 is cut off and the cathode voltage goes to ground potential.

Output Level Selection. The cathode load for V935B is essentially the string of precision resistors starting with R950 and ending with R958. The junctions of the precision resistors are connected to the CAL OUT connector through AMPLITUDE CALIBRATOR switch SW950. The values of the precision resistors are selected to give output amplitude steps in multiples of 1,2, or 5 . In the steps from 200 mvolts to 100 volts, the junctions of the precision resistors are switched through R962 to the CAL OUT connector, while in the steps from 0.2 to 100 mvolts, an additional divider with a ratio of 1000:1 is inserted between the precision resistors and the CAL OUT connector. In the 0.2 mvolt to 200 mvolt range, the output impedance is $50 \Omega$.

# SECTION 4 <br> MAINTENANCE 

## PREVENTIVE MAINTENANCE

## CAUTION

Turn off power before removing or replacing parts.

## General Information

The Type 547 is a stable instrument and will provide miny hours of trouble-free operation. However, to mainlain measurement accuracy, a visual inspection and a calibration check should be made after each 500 hours of operation or every six months if used intermittently. The calibration procedures include steps for checking the operation of arious circuits. Minor troubles not apparent during regilar operation will often be revealed during calibration. Mcior troubles in the instrument are often isolated or eliminated by recalibrating the instrument.

## Visual Inspection

The Type 547 should be inspected occasionally for sich defects as broken connections, broken or damaged ceranic strips, improperly seated tubes or transistors, and ha atdamaged parts.
The remedy for most visible defects is obvious; howe er, particular care must be taken if heat-damaged parts are detected. Overheating is usually only a symptom of troulde. For this reason, it is essential to determine the actual canse of overheating before the heat-damaged parts are replacad; otherwise, the damage may be repeated.

## Cleaning

The Type 547 must be cleaned as often as operating conditions require. Accumulations of dirt in the instrument , an cause overheating and component breakdown. Dirt on the components acts as an insulating blanket (preventing efficient heat dissipation) and provides conducting paths for electricity. Dirt in the air filter chokes the flow of cooling air and leads to excessive operating temperature.

Air Filter. The air filter should be visually checked evary few weeks and cleaned if dirty. More frequent inspecti.ns and cleaning are required under servere operating conditions. To clean the filter, wash it out as you would a platic sponge. Rinse the filter and let it dry. Coat the dry fiter with fresh "Filter-Kote" (Tektronix art Number 006-580) or "Handi-Koter". (These products are available from the lo:al representative of the Research Products Corporation, and from some air-conditioner suppliers.) Let the filter Iry thoroughly before reinstalling.

Exterior. Loose dust accumulating on the outside of he Type 547 can be removed with a cloth or small paint brish. The paint brush is particularly useful for dislodging dust on and around the front-panel controls. Stubborn dirt can be
removed with a soft cloth dampened in a mild solution of water and detergent. Abrasive cleaners should not be used.

Clean the face of the crt with a soft, lint-free cloth dampened with denatured alcohol.

Interior. Although the air entering the Type 547 is filtered, some dust will eventually penetrate into the interior of the instrument. This dust should be removed occasionally due to its conductivity under high humidity conditions. The best way to clean the interior of the equipment is to first carefully vacuum all accessible areas and then blow away the remaining dust with dry low-pressure compressed air. Avoid the use of high-velocity air which might damage some of the components. Remove stubborn dirt with a soft paint brush or a cloth dampened with a mild water and detergent solution.

Pay special attention to high-voltage circuits, including parts inside the high-voltage shield. Arcing in the high-voltage circuits due to dust or other causes may produce false sweep triggering resulting in an unstable crt display.

## Lubrication

The fan motor bearings should be lubricated every three or four months with a few drops of light machine oil (see Fig. 4.1). Failure to lubricate the bearings periodically can cause the fan to slow down or stop.

## CORRECTIVE MAINTENANCE

## General Information

Many components in the Type 547 are mounted in a parricular way to reduce stray inductance and capacitance. While removal or replacement procedures for most parts in the Type 547 are obvious, remember to duplicate lead length, lead dress, and location of the original component when installing replacement ports. Since components of the same type may exhibit slightly different characteristics, it is desirable to check the calibration of the Type 547 after completion of repairs.

## Component Numbering

The component number of each electrical part is shown on the circuit diagrams. The following chart lists the component numbers associated with each circuit:



Fig. 4-1. Fan moter lubrication points.

## Soldering Precautions

In the production of Tektronix instruments, a special silver-bearing solder is used to establish a bond to the ceramic terminal strips. This bond may be broken by repeated use of ordinary tin-lead solder, or by excessive heating of the terminal strip with a soldering iron. Occasional use of ordinary $60-40$ solder will not break the bond unless excessive heat is applied, but it is advisable to stock solder containing about $3 \%$ silver for the maintenance of Tektronix instruments. This solder may be purchased directly from Tektronix in one-pound rolls; order by Part Number 251-514.

Because of the shape of the ceramic-strip terminals, it is recommended that a soldering iron with a wedge-shaped tip be used. A wedge-shoped tip allows the heat to be concentrated on the solder in the terminals and reduces the amount of heat required. It is important to use as little heat as possible while producing a futl-flow joint.

The following procedure is recommended for removing or replacing components mounted on ceramic strips:

1. Use a 50 - to 75 -watt soldering iron.
2. Tin the tip with solder containing about $3 \%$ silver.
3. Use long-nose pliers for a heat sink. Attach pliers between the component and the point where heat is applied.
4. Apply heat directly to the solder in the terminal without touching the ceramic. Do not twist the iron in the notch as this may chip or break the ceramic strip.
5. Apply only enough heat to make the solder flow freely.
6. Do not attempt to fill the notch on the strip with solder; instead apply only enough solder to cover the wires adequately and form a small fillet on the wire. Overfilling the notches may result in cracked terminal strips. If the lead extends beyond the solder joint, clip the excess as close to the joint as possible. Remove all wire clippings from the chassis.

## Tubes and Transistors

Tubes or transistors should not be replaced unless they are actually defective. If tubes or transistors are removed and found to be acceptable, be sure to return them to their original sockets. Tube or transistor-tester checks on the tubes or transistors used in the Type 547 are not recommended. Testers may indicate a fube or transistor to be defective when it is operating satisfactorily in a circuit, or may fail to indicate tube or transistor defects which affect the performance of the circuits. It is recommended that fubes and transistors be checked by substitution. If the tube or transistor is good, return it to its socket. Unnecessary replacement of tubes or transistors is not only expensive but may also result in needless recalibration of the instrument.

When installing replacement transistors on heat sinks in the instrument, the bottom of the transistor where it contacts the heat sink should be coated with silicone grease. If a heat sink has been replaced along with the transistor, then that area of the heat sink which contacts the chassis of the instrument should also be coated with silicone grease.

## Wafer Switches

Individual wafers are normally not replaced in the switch assemblies. If one wafer is defective, the entire switch assembly should be replaced. Switches can be ordered from Tektronix either wired or unwired. Refer to the parts list in Section 6 for wired and unwired switch part numbers.

The wafer switches shown on the schematics are coded to indicate the position of the wafer on the switch. The wafers are numbered from front to rear fi.e., the number 1 wafer is always closest to the front panel). The letters F and $R$ indicate the front or rear of the wafer. For example, code designation of $3 R$ means the rear side of the third wafer from the front panel.

## Cathode-Ray Tube

To remove and replace the cathode-ray tube, perform the following procedure:

## WARNING

Be careful when handling a crt. Avoid striking it on any object that might cause it to crack and implode. Flying glass from an imploding crt can cause serious injury. Use safety glasses or a plastic face mask for protection.

1. Remove the crt bezel nuts, bezel, and plastic polarized light filter (see Fig. 4-2).
2. Remove plastic eyebrow and retaining spring from the top of the ct (see Fig. 4-2).


Fig. 4-2. Crt berel and eyebrow arrangement.
3. Remove Cr anode lead, disconnect all leads to the neck of the crt.

## NOTE

Do not disconnect the crt trace-rotation coil leads.
4. Using a Phillips screwdriver, loosen crt base clamp (see Fig. 4-3).
5. With your left hand, wiggle the ct socket (see Fig. 4-3) to ensure that the base of the ct is loose in the base clamp.
6. With a chisel-tipped plastic or wooden dowel, carefully work the ct socket loose from the ct base.
7. Grasp the face of the cit with the right hand. Push the ctt carefully towards the front of the Type 547 with the left hand. Be careful not to bend the neck pins. Remove the oft through the front of the oscilloscope.
8. Before reinstalling the crt , dust talcum powder on the ct base. This keeps the base of the crt from sticking to the neoprene bushing inside the base clamp.
9. Carefully insert the new tube into the shield and the tube base clamp. Keep the anode button in line with the anode connector hole so that the button is aligned with the hole when the crt is fully inserted.

## NOTE

Make sure that the crt base clamp is loose enough to permit the crt base to slide through the neoprene bushing inside the base clamp.


Fig. 4-3. Leosening the crt base clamp.
10. Connect the tube socket to the tube base. Check that the socket is fully seated.
11. Align the Cr so that the horizontal graticule lines are parallel with the top of the front panel. Push the crt inward until the crt face protrudes exactly $3 / 16^{\prime \prime}$ beyond the front panel.

## NOTE

If the crt face is not parallel with the front of the oscilloscope, use a $7 / 4^{\prime \prime}$ hexagonal wrench to loosen the fwo mounting screws that fasten the base clamp to its mounting bracket (see Fig. 4-3). The base clamp and crt base may now be moved radially to align the face of the crt parallel with the front of the oscilloscope.
12. Reconnect the anode and neck pin leads (observe color code).
13. Install eyebrow and eyebrow retainer spring. Align the crt so that the front surfaces of the light pipe and eyebrow are flush.
14. Tighten the base clamp.
15. Turn on the oscilloscope. Obtain a free-running sweep on the crt.

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16. Check the alignment of the trace with the graticule linss. If the trace is not parallel with the graticule lines, align the trace with the TRACE ROTATION control.
17. Replace plastic polarized light filter, crt bezel and be :el nuts.

## Graticule Lamps

Proper illumination of the crt graticule depends upon he proper positioning of the graticule lamps. When replac ng graticule lamps, slide the lamp and sockets in or out $u$ util the filament of the lamp is at the middle of the light-p pe thickness.

## Ceramic Terminal Strips

To remove a ceramic terminal strip, first unsolder all leeds and components connected to it. Use diagonal cutters to ;ut off one side of each stud holding the strip. This frees he strip, and the remainder of the stud can then be pulled fee of the chassis with a pair of pliers. The spacers may cone out with the studs; if not, they can be pulled out separately. If they are not damaged, the spacers may be used with he new strip assembly. Ceramic strips are supplied with stids attached, so it is not necessary to salvage the old studs.

After removing a damaged strip and stud assembly, plece the spacers into the holes in the chassis and insert the stids into the spacers. Be sure the studs are completely sea ed in the spacers. If necessary, use a soft- faced mallet to ' Jp the studs into the spacers. Top the studs in equal increme ats to prevent strains on the ceramic strip. Fig. 4.4 shows he assembled ceramic strip.


Fig. 4-4. Ceramic strip assembly.

## Troubleshooting Techniques

If the instrument is not operating, first check that he power cord is plugged in and that there is power of he socket. Then check that the pilot lamp and tube heal ars are lit. If necessary, check the line fuse.

Attempt to isolate the trouble by a quick operatio ial and visual check. Make sure that any apparent trouble is actually due to a malfunction within the instrument and or to improper control settings or to a faulty plug-in unit or probe. Instructions for the operation of the Type 547 end general information concerning plug-in operation are c.m-
tained in Section 2. Operating instructions for a specific plug-in unit or probe will be found in the manual for that unit.

Check the settings of all controls on the Type 547 and the vertical plug-in preamplifier unit. A control set to the wrong position may cause what appears to be a trouble symptom. Operate the controls to see what effect, if any, they have on the trouble symptom. The normal or abnormal operation of each particular control helps in establishing the nature of the trouble.
When vertical-system troubles are encountered, isolate the trouble to the Type 547 or to the vertical plug-in preamplifier unit. The best way to determine this is by substituting another vertical plug-in preamplifier unit. If the trouble appears to be in the plug-in unit, refer to the Maintenance section of the plug-in unit instruction manual.
If other plug-in units are not available, and the symptoms are not definite, check the power-supply resistances and voltages since a failure in one of the regulated power supplies frequently presents unusual symptoms. Table 5.2 in the Calibration Procedure lists normal resistances to ground for each power-supply lead. Typical voltoges in the power supplies are shown on the power-supply schematic. The voltages shown may vary slightly from instrument to instrument.
All wiring used in the Type 547 is color coded to facilitate circuit tracing. In addition, all regulated power-supply leads are coded with specific color combinations for easy identification. In general, three stripes are placed on the wires of the regulated supplies. The code used is the standard EIA number-color code. The first color (widest stripe) indicates the first number of the voltage on that lead. The second color indicates the second number of the lead voltage, and the third color is a multiplier. The method is similar to that used in color coding resistors. Thus, the +100 -volt leads are coded brown, black, brown. The valtage is positive if the body color of the wire is white and negative if the body color of the wire is tan,
Reference voltage for the regulated supplies is obtained from the -150 -volt supply. If it is not operating properly, the other low-voltage supplies will be affected. For this reason, the -150 -volt supply should be checked first when trouble is suspected in the low-voltage supplies. If the output of the -150 -volt supply is correct, then check the outputs of the other supplies.

Most troubles that might occur in Tektronix instruments result from the failure of vacuum tubes or semiconductors. Once the trouble has been isolated to a particular area or circuit, check the tubes and semiconductors in the trouble area. It is preferable to check them by substitution rather than with a tester, since testers frequently fail to indicate certain troubles which can affect oscilloscope performance. Remember that when tubes or somiconductors fail, associated circuit components can be damaged.

## Circuit Troubleshooting

The Type 547 consists of ten main circuits plus the Calibrator and Alternate-Trace Sync Amplifier circuits. The ten main circuits are the:

1. Low-Voltage Power Supply
2. Crt Circuit (including the High-Voltage Power Sur.ply)
3. Vertical Amplifier and Delay Line
4. Main Time Base (B) Sweep Trigger Circuit
5. Main Time Base (B) Sweep Generator
6. Time Base A Sweep Trigger Circuit
7. Time Base A Sweep Generator
8. Delay-Pickoff Circuit
9. Alternate-Sweep Switching Circuit
10. Horizontal Amplifier

The crt display can often be used to identify a defec ive circuit. For example, if there is no vertical deflection when the intensity and horizontal deflection appear normal, the trouble can be open signal connections, no signal source, the
plug-in unit or even loose crt connections. Other abnormal characteristics in the crt display similarly point to a defective circuit or group of circuits.
Once the nature and approximate location of the trouble has been determined, further isolate the trouble by performing the steps in the calibration procedure for the circuits in which trouble is suspected. The voltages and waveforms to be expected in each circuit are shown on the schematics. Refer to Section 3 for an explanation of the operation of the defective circuit,

## IMPORTANT

When it is desired to operate the plug-in unit from a plug-in extension, the plug-in sensing switch (SW673, located at the top rear of the plug-in compartment) must be manually operated. To manually operate the switch, pull the plastic plunger outward to the stop position.

NOTES


# SECTION 5 <br> CALIBRATION 

## Introduction

The Type 547 Oscilloscope is a stable instrument which will provide many hours of trouble-free operation. How ver, to ensure measurement accuracy, it is suggested that you recalibrate the instrument after each 500 hours of operation or every six months if used intermittently. It will also be necessary to recalibrate certain sections of the instrument when tubes, transistors, or other components are replaced.
The steps in the following procedure are arranged in the proper order for complete recalibration to avoid unnecessary repetition.
This procedure is a combination performance check and adjustment procedure. The first portion of the step title refers to the name of the check or adjustment and the last portion of the title is the name of the circuit diagram aflected by the step or on which the adjusiment is located, whichever is applicable.
Figs. 5-5, 5.8, 5.11, 5.14, and 5-17 are oscilloscope fiontpanel illustrations that show the contral settings, signal annections and signal input (if any) at those particular puints in the procedure. These illustrations serve two purpeses: (1) as an aid to quickly check your own setup, and (2) to enable you to start in the "middle" of the procedure when it is necessary to recalibrate a certain portion of the instrument. For example, Fig. 5-5 shows the front-panel setul, at the completion of step 12e, Using this same setup as illustrated, this can be the starting point for recalibrating the A Sweep Trigger circuit. Fig. 5-5 can also be used as an aid when determining the selup needed for starting the recalilrad. tion of the B Sweep Trigger circuit. Unless otherwise stoted, all resistances and voltages are measured with respec to chassis ground.

## Equipment Required

The following equipment or equivalent is necessary for complete calibration of the Type 547 Oscilloscope:

1. Low-Bandwidth Test Oscilloscope with a XI attenustor probe. Description: Bandwidth, dc to 300 kc or better; calibrated vertical deflection factor of $5 \mathrm{mv} / \mathrm{cm}$.
Purpose: To check low-voltage power supply ou'put ripple amplitude.
2. Test load unit, Tektronix Type TU7 (067-0521-00), (ontains a pulse generator capable of producing pulses with a risetime of 3 ns or faster. This multi-purpose 'est-

## NOTE

Whenever the TU.7 (067-0521-00) REPETITION RATE switch is reffered to, the following switcil positions should be considered equivalent for test purposes:

| TU-7 (067-0521-00) | $067-0521-01$ |
| :---: | :---: |
| - LOW | $\frac{4 \mathrm{kHz}}{80 \mathrm{kHz}}$ |
|  | MED |
| HIGH | 500 kHz |

load unit is the only plug-in needed to perform a complete calibration of the Type 547 Oscilloscope.
3. Time-Mark generator, Tektronix Type 180A. Markers required at 1 and $5 \mathrm{sec}, 500,100,10,5$, and $1 \mathrm{msec}, 500$, $100,50,10,5$, and $1 \mu \mathrm{sec}, 5,10$, and $50-\mathrm{mc}$ sine waves. $10-\mu \mathrm{sec}$ trigger pulse output required. All outputs must have a time accuracy of a least $0.1 \%$.
4. VOM (Volt-Ohm-Milliammeter) Dc sensitivity of at least 20,000 ohms per volt. Calibrated for an accuracy of at least $1 \%$ at $-150,+100,+225$, and +350 volts, at least $5 \%$ at -1850 volts.
5. Variable autotransformer (e.g. Powerstat or Variac). Required specifications: A raling of a least 600 volt-amperes with an output voltage range covering the operating range of the oscilloscope under test.
6. Rms-calibrated ac voltmeter. Required specifications: A range of 0.150 volts $10-300$ volts if the oscilloscope is wired for 234 -volt nominal line-voltage operation).
7. Two coaxial cables, 50 -ohm nominal impedance, $42^{\prime \prime}$ long with BNC plug-connectors on each end. Tektronix Part No. 012-057.
8. Power cord adapter for connecting the 3 -wire oscilloscope power cord to a 2 -wire receptacle. Tektronix Part No. 103-013.
9. Adapter, single binding post fitted with a BNC plug. Tektronix Part No. 103-033.
10. Coaxial connector adapter with BNC-jack and UHF-plug connector fittings. Tektronix Part No, 103-015.
11. Jumper clip lead, about $4^{\prime \prime}$ long. Equipped with miniature alligator clips on each end.
12. Two interconnecting leads, $18^{\prime \prime}$ long, with combination plug-and-jock banana-type connectors on each end. Type PC-18R. Tektronix Part No. 012-031.
13. BNC T connector. Fits one BNC jack and accepts two BNC plugs. Tektronix Part No. 103-032.
14. Miscellaneous Items

1-Screwdriver, $3 / 16^{\prime \prime}$ wide bit, shank about $3^{\prime \prime}$ long.
1-Screwdriver, $3 / 32^{\prime \prime}$ wide bit, shank about $2^{\prime \prime}$ long.
1-Jaco No. 125 insulated low-capacitance-type screwdriver with a $11 / 2^{\prime \prime}$ long shank and $1 / 8^{\prime \prime}$ wide metal tip. Total length is $5^{\prime \prime}$. Tektronix Part No. 003-000.
1-Low-capacitance alignment tool consisting of a handle (Tektronix Part No. 003-307), a gray nylon insert with a metal screwdriver tip (Tektronix Part No. 003-334), a $5 / 64^{\prime \prime}$ hexagonal wrench insert (Tektronix Part No. 003-310).
1-Hexagonal wrench, $1 / 16^{\prime \prime}$. For repositioning, if necessary, the TRIGGERING LEVEL control knobs.

PRELIMINARY PROCEDURE

1. Remove the oscilloscope from the cabinet.
2. Insert the Type TU-7 in the oscilloscope vertical plug-in compartment. Set the Type TU-7 Tets Function switch to the Low Load position.
3. Lay the oscilloscope on its left side for access to the bottom of the instrument.
4. Using the VOM, check the resistance from the regulated power-supply terminals to ground as shown in Fig. 5-1. The values of resistance should be approximately as indicated in Table 5-1, once the capacitors are charged by the VOM internal battery.


Fig. 5-1, Low-voltage power supply test point locotions.
TABLE 5-1

| Power Supply Lead | Resistance to Ground |
| :---: | :---: |
| -150 volts | 1 k to 2 k |
| +100 volts | 1 k to 2 k |
| +225 volts | 2 k to 3 k |
| +350 volts | 25 k to 35 k |

5. Check the fuse at the rear of the instrument for correct value.
6. Connect the instrument and ac voltmeter to the autotransformer output. Connect the autotransformer to the power line.
7. Turn the INTENSITY control on the instrument fully counterclockwise and turn on the power to all the equipment. Adjust the autotransformer output voltage to 115 volts for the design-center voltage for which the instru: ment is wired).
8. Set the oscilloscope front-panel controls to the positions listed in Table 5-2.

# TABLE 5-2 

Cr Controls
INTENSITY 0
FOCUS As is

| ASTIGMATISM | As is |
| :--- | :--- |
| SCALE ILLUM | 5 |
| TRACE SEPARATION | 0 |

Time Base A

| TRIGGERING LEVEL | Fully counterclockwise <br> and pushed in |
| :--- | :--- |
| TRIGGERING | TRIG |
| MODE | + |
| SLOPE | AC |
| COUPLING | NORM INT |
| SOURCE | CALIBRATED |
| VARIABLE (TIME/CM) | .5 mSEC |
| TIME/CM |  |
| Horizontal Display |  |
| HORIZONTAL DISPLAY | A |
| SWEEP MAGNIFIER | $\times 1$ OFF |
| Single Sweep Switch | NORMAL |

Main Time Base (B)

| TRIGGERING LEVEL | Fully counterclockwise <br> and pushed in |
| :--- | :--- |
| TRIGGERING |  |
| MODE | + |
| SLOPE | TRIG |
| COUPLING | NORM INT |
| SOURCE | CALIBRATED |
| VARIABLE (TIME/CM) | .5 mSEC |
| TIME/CM | Fully clockwise |

## Other Controls

| DELAY-TIME MULTI- | 1.00 |
| :--- | :--- |
| PLIER |  |
| HORIZONTAL POSI- | Midrange |
| TION | Midrange |
| VERNIER (HORI- |  |
| ONTAL POSITION) | OFF |
| AMPLITUDE CALI- <br> BRATOR |  |

9. Set the Type TU. 7 front-panel controls as follows:

| Vertical Position | Centered |
| :--- | :--- |
| Test Function | Low Load |
| Other Controls | As is |

10. Allow about five minutes for warmup. Check that the EXT CRT CATHODE-to-GND shorting strap is in place on the terminals, and the CRT CATHODE SELECTOR switch is set to the EXTERNAL CRT CATHODE position.
11. Recheck the autotransformer output for proper designcenter voltage as soon as the instrument has warmed up.

## CHECK AND ADJUSTMENT PROCEDURE

1. Check Voltage Accuracy-Power Supply
a. Establish the conditions described previously under
"Preliminary Procedure".
b. Check the voltage accuracy of each power supply output using the VOM according to the information given in Table 5-3. The location of the test points is shown in Fig. 5-1.

TABLE 5-3

| Power <br> Supply | Tolerance | Maximum Peak-to- <br> Peak Ripple |
| :---: | :---: | :---: |
| -150 v | -147 to -153 v | 10 mv |
| +100 v | +98 to +102 v | 15 mv |
| +225 v | +220.5 to +229.5 v | 10 mv |
| +350 v | +343 to +357 v | 25 mv |

c. If necessary, adjust - 150 VOLTS R616 (see Fig. 5-2) so all power supply voltages are within tolerance.

## NOTE

Do not adjust the -150 VOLTS control unless one or more of the supplies is actually out of tolerance. Remember that the calibration of the entire instrument is affected by changes in the power supply voltages and all the positive volt-
age power supplies depend upon the -150 -volt supply output accuracy.

## 2. Check Regulation and Output Ripple-Power Supply

## NOTE

When checking for proper regulation of the power supplies at the lower line-voltage limit, the ac line voltage should contain no more than $3 \%$ distortion.
a. Monitor the regulated output of the -150 -volt supply with the VOM. The test point location is shown in Fig. 5-1.
b. Connect the $\times 1$ probe form the test oscilloscope to the -150 -volt test point and check the output ripple amplitude. The maximum ripple voltage is given in Table 5-3.

NOTE
Ground loops can cause erroneous ripple measurement. (Ripple due to ground loops is the same frequency as the line; Low voltage power supply ripple is twice the line rate.) One way to avoid


Fig. 5-2. Calibration adjustment locations.
ripple due to ground loops is to temporarily disconnect the chassis ground wire in the power cord by using an ungrounded 3 - to 2 -wire line-plug adapter. Then use a ground lead from the signal probe body to make a ground connection to the oscilloscope chassis at the location shown in Fig. $5-1$. The probe will then provide the only ground connection between the two instruments. The term "test oscilloscope" is item 1 under "Equipment Required" while the term "oscilloscope" or "instrument" is the oscilloscope being calibrated.
c. Slowly increase the output of the variable autotransformer to 126.5 vac (or $10 \%$ above the design-center line voltage for which the instrument is wired). The de output voltage should remain essentially constant; typically within $2 \%$ of that obtained with designcenter line voltage. The ripple voltage should not exceed the maximum peak-to-peak amplitude given in Table 5-3.
d. Repeat steps 2 a through 2 c for each supply.
e. Reset the autotransformer for 115 volts output for the design-center voltage for which the instrument is wired).
f. Set the Type TU-7 Test Function switch to High Load.
g. Reduce the line voltage to 103.5 volts for $10 \%$ below design-center voltage). The de output voltage of each supply should remain essentially constant; typically within $2 \%$ of that obtained at design-center voltage. Ripple voltage should not exceed the maximum peak-to-peak amplitude given in Table 5-3.
h. Disconnect the voltohmmeter and XI probe.
i. Reset the autotransformer for 115 volts output (or the design-center voltage).
i. Set the Type TU. 7 Test Function switch to Low Load.
k. Place the instrument in its upright position.

1. If the 3- to 2 -wire adapter was used during this step, turn off oscilloscope power and remove the adapter. Plug the line cord directly into the autotransformer and furn on the oscilloscope power.
2. Adjust HIGH VOLTAGE R840-Crt Circuit
a. Set the range of the voltohmmeter to measure - 1850 volts and connect the voltohmmeter to the highvoltage test point (see Fig. 5-3).
b. Adjust the HIGH VOLTAGE R840 (see Fig. 5-2) for a -1850 voltmeter indication.
3. Check High Voltage Regulation-Crt Circuit
a. Monitor the voltage at the high voltage test point with the voltohmmeter.
b. Set the A TRIGGERING MODE switch to AUTO.
c. Turn the INTENSITY control clockwise until the trace is at normal intensity. Use the Type TU-7 Vertical Position control to vertically center the trace. Defocus the trace with the FOCUS and ASTIG. MATISM controls. Set the INTENSITY control at 7.
d. Use the HORIZONTAL POSITION control to position the trace to start at the left side of the graticule.
e. Slowly increase the output of the variable autotransformer to 126.5 vac (or $10 \%$ above the design-center line voltage for which the instrument is wired). The high-voltage dc output should remain essentially constant; typically within $2 \%$ of that oblained with design-center line voltage. The trace should not show any signs of blooming. (Blooming is when the display changes size as the supply voltage changes.)
f. Reset the autotransformer for 115 volts output (or design-center voltage).
g. Set the Type TU-7 Test Function switch to High Load.
h. Reduce the line voltage to 103.5 volts lor $10 \%$ below design-center voltage). The dc output voltage should remain constant; typically within $2 \%$ of that obtained with design-center line voltage. The trace should not show any signs of blooming.
i. Reset the autotransformer for 115 volts output (or the design-center voltage).
i. Set the Type TU-7 Test Function switch to Low Load.
k. Descrease the trace intensity to normal with the INTENSITY control.
I. Disconnect the VOM.


Fig. 5-3. High-voltage test point location.

## 5. Adjust CAL AMPL (Calibrator Amplitude) R943Calibrator

a. Connect the single binding post adapter to the oscilloscope CAL OUT connector.
b. Connect the VOM to the binding post adapter and to the oscilloscope chassis.
c. Sef the AMPLITUDE CALIBRATOR switch to 100 V DC.
d. Adjust CAL AMPL R943 (see Fig. 5-2) for a voltmeter reading of exactly 100 volts.
6. Check Duty Factor of Signal-Calibrator
a. Set the AMPLITUDE CALIBRATOR switch to 100 VOLTS (not 100 V DC).
b. Check for +45 to +55 volts measured between the CAL OUT connector and ground.

## NOTE

+50 volts indicates a nominal duty factor of 0.5 . If the voltage is not within +45 to +55 volts, try new tubes.
c. Disconnect the VOM and set the AMPLITUDE CALIBRATOR switch to OFF.
d. Remove the adapter from the CAL OUT connector.

## 7. Adjust TRACE ROTATION-Crt Circuit

a. Adjust the FOCUS and ASTIGMATISM controls for the narrowest trace.
b. Position the trace directly behind the center horizontal graticule line, using the Type TU. 7 Vertical Position control.
c. If the trace and graticule line do not coincide over the width of the graticule, adjust the TRACE ROTATION control for correct trace alignment.
8. Adjust GEOMETRY R861-Crt Cricuit
a. Apply 50 - $\mu \mathrm{sec}$ markers from the time-mark generator through a coaxial cable to the Type TU. 7 Ext Input connector.
b. Set the A TIME/CM switch to $50 \mu \mathrm{SEC}$.
c. Advance the INTENSITY control to make the display visible.
d. Set the TRIGGERING LEVEL control to obtain a stable display of vertical marker lines.
e. Adjust the TU- 7 Variable control so the markers over-scan the cr ; set the Vertical Position control to position the base line of the markers below the display area.
f. Use the HORIZONTAL POSITION control to position the markers so they align with the graticule markings.
g. Adjust GEOMETRY R861 (see Fig. 5-2) for the straightest possible vertical marker-lines running parallel to
the 0 and $10-\mathrm{cm}$ graticule lines at the left and right edges of the graticule. Note the amount of bowing.
h. Disconnect the signal from the TU-7 Ext Input connector.
i. Reduce the trace intensity to normal with the $\mathbb{I N}$. TENSITY control while positioning the trace onto the crt with the TU-7 Vertical Position control.
i. Position the trace to the bottom of the graticule with the TU. 7 Vertical Position control. Note the amount of bowing. Then position the trace to the top of the graticule and note the amount of bowing.
k. Repeat steps 8 a through 8 j so the trace exhibits minimum bowing in both planes.
I. After completing the previous steps, disconnect the signal from the TU-7 Ext Input connector. Check that the trace is positioned into the display area and the INTENSITY control is set to a suitable tracebrightness level.
9. Adjust VERT DC BAL (Vertical Amplifier Dc Balance) R1004-Vertical Amplifier
a. Using a small screwdriver, short the crt vertical deflection-plate pins together (see Fig. 5-4].


Fig. 5-4. Vertical Amplifier test points and adjustment locations for performing steps 9 and 10.

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Fig. 5-5. Front-panel control settings and signal connections at the completion of step 12 e .

## CAUTION

Do not short the crt deflection-plate pins to ground.
b. Note the position of the trace. This is the electrical center of the crt vertical deflection plates.
c. Remove the screwdriver from the crt pins.
d. Short the cases of Q1074 and Q1084 (see Fig. !-4) together (not to ground) and note the trace deviation from electrical center. Deviation should not be more than 0.5 cm maximum. Remove the shist.
e. Short the collector of Q1034 to the collector of Q1044 (see Fig. 5-4) and note the trace deviation from electrical center. Deviation should not be more than 0.5 cm maximum. Remove the short.
f. Short the cases of Q1014 and Q1024 (see Fig. :3-4) together (not to ground) and note the trace deviation from electrical center. Deviation should not be mare than 0.5 cm maximum. Remove the short.
9. Set the Type TU.7 Test Function switch to Commion Mode.
h. Adjust VERT DC BAL R1004 (see Fig. 5-4) to position the trace to the center of the graticule.

## 10. Adjust VERT GAIN (Vertical Amplifier Gain) R1017 Vertical Amplifier

a. Set the Type TU-7 Test Function switch to the Gain Set position.
b. Connect a coaxial cable between the Type TU-7 Ext Input connector and the oscilloscope CAL OUT cinnector.
c. Set the AMPLITUDE CALIBRATOR switch to 100 VOLTS.
d. Pull the A TRIGGERING LEVEL control outward for a $\times 10$ range increase and turn the control filly clockwise to free run the time base.
e. Adjust VERT GAIN R1017 (see Fig. 5-4) so the display vertical deflection is exactly 4 cm in amplitude.
11. Check Common-Mode Rejection-Vertical Amplifier
a. Set the AMPLITUDE CALIBRATOR switch to 1 VOLT.
b. Set the TU-7 Test Function Switch to Common Mode.
c. Set the A TIME/CM switch to .5 mSEC .
d. Note the amplitude of the calibrator waveform. The amplitude of the waveform should not be mure than 3 mm maximum.

12A. Adjust A TRIGGER LEVEL CENTERING R225 and
A TRIGGER SENS R245-A Sweep Trigger (SN
6740-up)
a. Set the AMPLITUDE CALIBRATOR to .1 volts.

## NOTE

A 100 mv peak-to-peak signal is used in this portion of the procedure as an adjustment aid only and is not intended to be interpreted as a triggeramplitude specification that contradicts the one given in the Characteristics section of this manual.
b. Insert a BNC T connector between the CAL OUT connector and the coax cable to the TU-7 Ext Input. Connect another coax cable from the T connector to the A TRIGGER INPUT connector. (The CAL OUT connector should now be connected to the Ext Input connector on the TU-7 and to the A TRIGGER IN. PUT connector on the oscilloscope.)
c. Set the front-panel controls as follows:

Type 547/RM547
Controls not mentioned may be left as is.

| INTENSITY | As required for a visible <br> trace |
| :--- | :--- |
| FOCUS | As required for a focused <br> trace |
| ASTIGMATISM | As required for a focused <br> trace |
| SCALE ILLUM | As required for a visible <br> graticule |
| HORIZONTAL POSI- <br> TION required to position <br> trace to the left edge <br> of the graticule |  |
| VERNIER (HORIZON. <br> TAL POSITION) | Midrange |
| HORIZONTAL DIS- | A |
| PLAY |  |
| SWEEP MAGNIFIER | XI (OFF) |
| SINGLE SWEEP | Normal |
| Switch |  |


|  | Time Base A |
| :--- | :--- |
| TRIGGERING LEVEL | 0 |
| TIME/CM | .5 mSEC |
| TRIGGERING |  |
| MODE | TRIG |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | EXT |

TU-7

| Variable | Fully Clockwise |
| :--- | :--- |
| Vertical Position | Centered |
| Test Function | Low Load |

## Test Oscilloscope

| Input Coupling | AC |
| :--- | :--- |
| Volts/Div | .02 |
| Time/Div | .5 mSEC |

Triggering

| Mode | AUTO |
| :--- | :--- |
| Slope | + |
| Coupling | AC |
| Source | Internal |

d. Locate the junction of R217, C218, R218, ISee Fig. 5-6a). Connect a short jumper clip lead between the junction and ground. This jumper disables the A TRIGGERING LEVEL control.
e. Locate the junction of R252 and L250 (See Fig. 5-6a). Connect a $10 \times$ probe from the test oscilloscope to this junction.
f. Preset the A TRIGGER LEVEL CENTERING R225 control to midrange and the A TRIG SENS R245 control fully clockwise.
g. Adjust the A TRIGGER LEVEL CENTERING R225 control for a stable square wave display of approximately 200 mv peak-to-peak. Note that there is a range in the odjustment of R225 through which the square wave display will remain stable. Set R225 approximately in the middle of this range.
h. Change the SLOPE switch to - and readjust R225 if necessary. Continue alternating the position of the SLOPE switch and odjusting R225 until the square wave on the test scope is stable in both positions of the SLOPE switch.
i. Turn the A TRIGGER SENS R245 control counterclockwise until the square wave on the test oscilloscope just begins to break up. (This will occur where the square wave suddenly reduces in amplitude.) Leave R245 set at this point.
i. Readjust the A TRIGGER LEVEL CENTERING R225 control for a stable square wave display ot both positions of the SLOPE switch. (Note that there is a range in the adjusiment of R225 over which a stable square wave can be obtained. Set R225 in the center of this range.)
k. Set the AMPLITUDE CALIBRATOR switch to 50 mVOLTS. The amplitude of the square wave display on the test oscilloscope should be reduced to less than 100 millivolts in either position of the SLOPE switch. If the amplitude of the square wave on the test oscilloscope remains at approximately 200 millivolts, repeat ithrough k .
I. Disconnect the $10 \times$ probe from the junction of R252 and 2250 .

## 12B. Adjust A TRIGGER LEVEL CENTERING R225 and A TRIGGER SENS R245-A Sweep Trigger (SN 1016739)

a. Set the AMPLITUDE CALIBRATOR switch to 50 m volts.
b. Insert the BNC T connector between the AMPLITUDE CALIBRATOR connector and the coaxial cable.


Fig. 5-6. A Trigger clip-lead connections, edjustment and test point locations.
c. Connect another coaxial cable from the $T$ connector to the A TRIGGER INPUT connector. (The CAL OUT connector should now be connected to the Ext Input connector on the Type TU. 7 and to the A TRIGGER INPUT connector on the oscilloscope.)
d. Set the TU-7 front-panel controls as follows:

Variable
Vertical Position
Test Function
e. Set the A MODE switch to TRIG and the A TRIGGI RING LEVEL control to 0 . Check that the A COUPLING switch is set at AC and the A SOURCE switch is set to EXT.
f. Locate the junction of R217, C218, and R218. C(innect the short jumper clip lead between the junction and ground. This jumper disables the A TRIGGERING LEVEL control.
g. Connect a $10 \times$ Probe from the test oscilloscope to the junction of R245-R248.
h. Set the test oscilloscope controls as follows:

| INPUT COUPLING | AC |
| :--- | :--- |
| VOLTS/DIV | .02 |
| TIME/DIV | .2 mSEC |
| TRIGGERING |  |
| MODE | AUTOMATIC |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | INTERNAL |

i. Set the TRIGGER SENS R245 to midrange.
i. Rotate TRIGGER LEVEL CENTERING R225 fully counterclockwise.
k. Rotate TRIGGER LEVEL CENTERING R225 clockwise until a stable display 2 to 3 major divisions high appears on the test oscilloscope.
I. If no stable display appears on the test oscillosco()e, rotate the TRIGGER SENS R245 slightly clockw ise, then repeat part $k$.
m . Change the Triggering SLOPE switch to -and ch.ck for a stable display on the test oscilloscope. If neressary readjust the TRIGGER LEVEL CENTERING R: 25 slightly so as to obtain a stable test oscilloscope in both positions of the A SLOPE switch.
$n$. If a stable test oscilloscope display can not be obtained for both A SLOPE switch positions, rol.tite the TRIGGER SENS R245 slightly clockwise and repeot part $m$.
o. After obtaining a stable test oscilloscope display for both A SLOPE switch positions, rotate the TRIGC ER SENS R245 slightly counterclockwise. Again ch ck for a stable test oscilloscope display in both pisitions of A SLOPE switch. TRIGGER LEVEL CENTERING R225 may have to be readjusted slightly.
p. Continue rotating the TRIGGER SENS R245 slightily counterclockwise and then checking the test osciloscope display until a stable test oscilloscope display can not be obtained for both positions of the Tig. gering SLOPE switch.
q. Rotate the TRIGGER SENS R245 just enough clockwise to permit a stable test oscilloscope display to
be oblained for both positions of the Triggering SLOPE switch. Slight readjustment of TRIGGER LEVEL CENTERING R225 will probably be necessary.

## 13. Adjust A INT TRIG DC LEVEL R209-A Sweep Trigger

a. Set the AMPLITUDE CALIBRATOR switch to .5 VOLTS.
b. Set the A SOURCE switch to NORM INT.
c. Adjust the TU. 7 Variable control so the displayed waveform is 5 mm peak-to-peak in amplitude.
d. Using the TU-7 Vertical Position control, center the display for equal amplitude above and below the graticule centerline.
e. Set the A COUPLING switch to DC.
f. Adjust A INT TRIG DC LEVEL R209 (see Fig. 5-6) to obtain a stable display. (With the A SLOPE switch set to + , the sweep trace should start on the posi-five-going rise of the calibrator waveform.)

## 14. Check Internal Triggering-A Sweep Trigger

a. Set the A COUPLING switch to AC.
b. Adjust the TU. 7 Variable control until the display is 2 mm peak-to-peak in amplitude.
c. Disconnect the jumper clip lead.
d. Adjust the A TRIGGERING LEVEL control to obtain a stable display.
e. Check for stable time-base triggering on the -slope when the A SLOPE switch is set to - and on the + slope when the SLOPE switch is set to + . If necessary, readjust the A TRIGGERING LEVEL control to obtain a stable display when checking each SLOPE switch position.

## 15. Check A tRiggering level Control Zero Set-A Sweep Trigger

a. Check that the A TRIGGERING LEVEL control is set to 0 and the A SLOPE switch is set to + .
b. Connect the VOM between the R217/C218/R218 junction and ground.
c. Carefully turn the A TRIGGERING LEVEL control to obtain a reading of $\pm 0.1 \mathrm{~V}$ on the VOM.
d. If the A TRIGGERING LEVEL knob is set properly on the control shaft, the white dot on the knob should be directly below the 0 on the front panel. If the white dot does not point exactly to 0 , disconnect the VOM, loosen the setscrew in the knob and reposition the knob.
e. After tightening the knob, set the knob to 0 , reconnect the VOM, and recheck the reading. The VOM reading should be within $\pm 0.1 \mathrm{~V}$ of zero when the A TRIGGERING LEVEL knob is set to 0 .

## NOTE

A dc-coupled test oscilloscope with a $\times 10$ probe can be used in place of the VOM to perform step 15.

As another method, the TRIGGERING LEVEL knot, can be checked for correct position by repeating step 14e. This method does not require the useof a test oscilloscope or VOM. When performing step 14e the TRIGGERING LEVEL knob should point to 0 when stable triggering is obtained.
f. Disconnect the VOM or $\times 10$ probe, whichever is used.

16A. Adjust B tRigger level CENTERING R25 and B TRIGGER SENS R45-B Sweep Trigger (SN 6740-up)
a. Set the AMPLITUDE CALIBRATOR to 11 volts.

## NOTE

A 100 mv peak-to-peak signal is used in this portion of the procedure as an adjustment aid only and is not intended to be interpreted as a trigger-amplitude specification that contradicts the one given in the Characteristics section of this manual.
b. Insert a BNC T connector between the CAL CUT connector and the coax cable to the TU-7 Ext Input. Connect another coax cable from the T connector to the B TRIGGER INPUT connector. fihe CAL OUT connector should now be connected to the Ext Input connector on the TU. 7 and to th. B TRIGGER INPUT connector on the oscilloscope.)
c. Set the front panel controls as follows:

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Controls not mentioned may be left as is

| HORIZONTAL DIS- <br> PLAY <br> BRIGHTNESS | B |
| :--- | :--- |
| As required for visible |  |
| trace |  |

Time Base B

| TRIGGERING LEVEL | 0 |
| :--- | :--- |
| TIME/CM | .5 mSEC |
| TRIGGERING |  |
| $\quad$ MODE | TRIG |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | EXT |

## TU-7

Variable
Vertical Position
Test Function

## Test Oscilloscope

| Input Coupling | AC |
| :--- | :--- |
| Volits/Div | .02 |
| Time/Div | .5 mSEC |
| Triggering |  |
| Mode | AUTO |
| Slope | + |
| Coupling | AC |
| Source | Internal |

d. Locate the junction of R17, C18, R18 (See Fig. 5-7a). Connect a short jumper clip lead between the junction and ground. This jumper disables the B TRIGGERING LEVEL control.
e. Locate the junction of R52 and L50 (See Fig. 5-7a). Connect a $10 \times$ probe from the test oscilloscope to this junction.
f. Preset the B TRIGGER LEVEL CENTERING R25 control to midrange and the B TRIG SENS R45 fully clockwise.
g. Adjust the B TRIGGER LEVEL CENTERING R25 control for a stable display of square waves on the test oscilloscope. (The square waves will have an amplitude of approximately 200 mv peak-to-peak.) Note that there is a range in the adjustment of R25 through which the square wave will remain stable. Set R25 approximately in the middle of this range.
h. Change the SLOPE switch to - and readjust R25 if necessary. Continue alternating the position of the SLOPE switch and adjusting R25 until the square wave display on the test oscilloscope is stable in both positions of the SLOPE switch.
i. Turn the B TRIGGER SENS R45 control counterclockwise until the square wave display on the test oscilloscope just begins to break up. (This will occur where the square wave suddenly reduces in amplitude.) Leave R45 set at this point.
i. Readjust the B TRIGGER LEVEL CENTERING R25 control for a stable square wave display at both positions of the SLOPE switch. (Note that there is a range in the adjustment of the R25 over which a stable square wave can be obtained. Set R25 in the center of this range.)
k. Set the AMPLITUDE CALIBRATOR to 50 mVOLTS . The amplitude of the square wave display on the test oscilloscope should be reduced to less than 100 millivalts in either position of the SLOPE switch. If the amplitude of the square wave display on the test oscilloscope remains at approximately 200 millivolts, repeat steps ithrough $k$.
I. Disconnect the $10 \times$ probe from the junction of R52 and L 50 .

16B. Adjust B TRIGGER LEVEL CENTERING R25 and B TRIGGER SENS R45-B Sweep Trigger (SN 1016739)
a. Set the AMPLITUDE CALIBRATOR switch to 50 mvolts.
b. Insert the BNC T connector between the AMPLITUDE CALIBRATOR connector and the coaxial cable.
c. Connect another coaxial cable from the $T$ connector to the B TRIGGER INPUT connector. (The CAL OUT connector should now be connected to the Ext Input connector on the Type TU. 7 and to the B TRIGGER INPUT connector on the oscilloscope.)
d. Set the TU- 7 front-panel controls as follows:

| VARIABLE | Fully clockwise |
| :--- | :--- |
| POSITION | Centered |
| TEST FUNCTION | Low Load |

e. Set the B MODE switch to TRIG and the B TRIGGERING LEVEL control to 0 . Check that the B COU. PLING switch is set at AC and the B SOURCE switch is set to EXT.
f. Locate the junction of R17, C18, and R18. Connect the short jumper clip lead between the junction and ground. This jumper disables into A TRIGGERING LEVEL control.
g. Connect a $10 \times$ Probe from the test oscilloscope the junction of R45-R48.
h. Set the test oscilloscope controls as follows:

| INPUT COUPLING | AC |
| :--- | :--- |
| VOLTS/DIV | .02 |
| TIME/DIV | .2 mSEC |

TRIGGERING MODE AUTOMATIC

SLOPE
COUPLING SOURCE
$+$
AC
INTERNAL
i. Set the TRIGGER SENS R45 to midrange.
i. Rotate TRIGGER LEVEL CENTERING R25 fully counterclockwise.
k. Rotate TRIGGER LEVEL CENTERING R25 clockwise until a stable display 2 to 3 major divisions high appears on the test oscilloscope.
I. If no stable display appears on the test oscilloscope, rotate the TRIGGER SENS R45 slightly clockwise, then repeat part $k$.
m . Change the Triggering SLOPE switch to - and check for a stable display on the test oscilloscope. If necessary readjust the TRIGGER LEVEL CENTERING R25 slightly so as to obtain a stable test oscilloscope in both positions of the A SLOPE switch.
n. If a stable test oscilloscope display can not be obtained for both B SLOPE switch positions, rotate the TRIGGER SENS R45 slightly clockwise and repeat part m.
o. After obtaining a stable test oscilloscope display for both B SLOPE switch positions, rotate the TRIGGER SENS R45 slightly counterclockwise. Again check for a stoble test oscilloscope display in both positions of B SLOPE switch. TRIGGER LEVEL CENTERING R25 may have to be readjusted slightly.


Fig. 5-7, B Trigger clip-lead connections, adjustment and test point locations.
p. Continue rotating the TRIGGER SENS R45 slightly counterclockwise and then checking the test oscilloscope display until a stable test oscilloscope display can not be obtained for both positions of the Triggering SLOPE switch.


Fig. 5-8. Front-panel control settings at the completion of step 20a.
q. Rotate the TRIGGER SENS R45 just enough clockwise to permit a stable test oscilloscope display to be obtained for both positions of the Triggering SLOPE switch. Slight readjustment of TRIGGER LEVEL CEIVTERING R25 will probably be necessary.
17. Adjust B INT TRIG DC LEVEL R9 - B Sweep Trigger
a. Set the AMPLITUDE CALIBRATOR switch to .5 VOLIS.
b. Set the B SOURCE switch to NORM INT.
c. Adjust the TU-7 Variable control so the displayed waveform is 5 mm peak-to-peak in amplitude.
d. Using the TU. 7 Vertical Position control, center the display for equal amplitude above and below the graticule centerline.
e. Set the B COUPLING switch to DC.
f. Adjust B INT TRIG DC LEVEL R9 (see Fig. 5.7) ro obtain a stable display. (With the B SLOPE swit:h set to + , the sweep trace should start on the posi-tive-going rise of the calibrator waveform.)
18. Check Internal Triggering - B Sweep Trigger
a. Set the B COUPLING switch to AC.
b. Adjust the TU-7 Variable control until the display is 2 mm peak-to-peak in amplitude.
c. Disconnect the jumper elip lead.
d. Adjust the B TRIGGERING LEVEL control to obtain a stable display.
e. Check for stable time-base triggering on the - slop'e when the B SLOPE switch is set to - and on the + slope when the SLOPE switch is set to + . If necessary, readjust the B TRIGGERING LEVEL control 10 obtain a stable display when making the check fir each SLOPE switch position.
19. Check B TRIGGERING LEVEL Control Zero Set -B Sweep Trigger
a. Check that the B TRIGGERING LEVEL control is sat to 0 and the SLOPE switch is set to + .
b. Connect the VOM between the $\mathrm{R} 17 / \mathrm{Cl} 8 / \mathrm{RI} 8$ junstion and ground.
c. Carefully adjust the B TRIGGERING LEVEL control 'o obtain a reading of exactly zero volts on the VONI.
d. If the B TRIGGERING LEVEL knob is set properly en the control shaft, the white dot on the knob shouid be directly below the 0 on the front panel. If the white dot does not point exactly to 0 , disconnect the VOM, loosen the setscrew in the knob, and repo:ition the knob.
e. After tightening the knob, set the knob to 0 , reco:nect the VOM, and repeat steps (c) and (d).

## NOTE

A dc-coupled test oscilloscope with a X10 probe can be used in place of the VOM to perform this step, if desired.

As another method, the TRIGGERING LEVEL knob can be checked for correct position by repeating step 18 e . This method does not require the use of a test oscilloscope or VOM. When performing step 18e, the TRIGGERING IEVEL knob should point to 0 when stable triggering is obtained.
f. Disconnect the VOM or X10 probe, whichever is used.
g. Disconnect the coaxial cables, $T$ connector, and set the AMPLITUDE CALIBRATOR switch to OFF.
20. Adjust SWP/MAG REGIS R569 - Horizontal Amplifier
a. Set the Main Time Base (B) front-panel controls to these settings:

| TRIGGERING LEVEL | About $25^{\circ}$ clockwise <br> from 0. |
| :--- | :--- |
| MODE | AUTO |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | NORM INT |
| TIME/CM | 1 mSEC |

All front-panel control settings up to this point in the procedure are shown in Fig. 5-8.
b. Apply $100-\mu \mathrm{sec}, 1-\mathrm{msec}$, and $5-\mathrm{msec}$ time markers from the time-mark generator through a coaxial cable to the TU. 7 Ext Input connector.
c. Set the TU. 7 Variable control so the display is about 4 cm in amplitude.
d. Center the display vertically using the TU-7 Vertical Position control.
e. Adjust, if necessary, the B TRIGGERING LEVEL control to obtain stable triggering on the 5 -msec time marks. Fig. $5-9 \mathrm{a}$ shows the time markers displayed with respect to the graticule markings. Use the HORIZONTAL POSITION control to position the center $5 . \mathrm{msec}$ time marker to the center of the graticule as shown in the illustration.
f. Set the SWEEP MAGNIFIER switch to X10. Position the $5-\mathrm{msec}$ time marker to graticule center (see Fig. 5.9 b ) and then set the SWEEP MAGNIFIER switch to XI OFF.
g. Adjust SWP/MAG REGIS R569 (see Fig. 5-2) to position the center 5 -msec time marker to graticule center. If necessary, repeat steps $20 f$ and 20 g until there is no movement of the $5-\mathrm{msec}$ time marker as the SWEEP MAGNIFIER switch is changed from X10 to XI OFF.
21. Adjust X10 CAL R544 - Horizontal Amplifier
a. Set the SWEEP MAGNIFIER switch to X10.
b. Adjust X10 CAL R544 (see Fig. 5-2) so there is 1 marker $/ \mathrm{cm}$ from the $1-\mathrm{cm}$ to $9-\mathrm{cm}$ graticule lines. For accurate adjustment, set X10 CAL R544 so the 2nd and 10 th markers at the $1-\mathrm{cm}$ and $9 . \mathrm{cm}$ graticule

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lines respectively coincide exactly with the $1-\mathrm{cm}$ and $9-\mathrm{cm}$ graticule lines.
*

## NOTE

The following hints should help you to obtain the best results when checking and adjusting the timebase sweep rates:

It is quite difficult to detect small sweep-rate errors on the order of $1 \%$ or $2 \%$ unless measuring over most of the graticule width. It is therefore recommended that the sweep rates be checked for correct linearity and timing using the center 8 cm and the middle $80 \%$ of the display as shown in Fig. 5-10. Measuring over a distance of 8 cm , the adjustment can be made more accurately. Later in the procedure when checking the nonadjustable sweep rates without using the DELAY-TIME MULTIPLIER control, a $1.6-\mathrm{mm}$ error would indicate a $2 \%$ sweep-rate error as shown in Fig. 5-11. The marker peak provides an excellent reference point particularly if the amplitude is such that the base line is below the crt viewing area and the tips of the markers are located in the center of the crt. When using the sine waves for markers at the higher sweep rates, set the TU-7 Variable and Vertical Position controls so the lower half of the display is positioned below the crt and the tips of each cycle are near the center of the crt. By increasing the amplitude of the display in this manner each marker or cycle tip appears much narrower.

The adjustable sweep rates should be set for maximum accuracy. When adjusting the timing capacitors, use a screwdriver having a metal tip and a nonmetallic shank to minimize capacitive disturbances to the circuit. This will also lessen the chance of accidentally grounding connections elevated above or below ground.

## 22. Adjust XI CAL R566 - Horizontal Amplifier

a. Set the SWEEP MAGNIFIER switch to XI OFF.
b. Adjust XI CAL R566 (see Fig. 5-2) so the 1-m.ec markers are spaced $1-\mathrm{cm}$ apart and the $1-\mathrm{m} \cdot \mathrm{ec}$ markers at the $1-\mathrm{cm}$ and $9-\mathrm{cm}$ points coincide with the graticule lines.
c. Due to some interaction between the X10 CAL and XI CAL adjustments, repeat steps 21 and 22 uutil the timing is correct.

## 23. Check MAG ON Neon - Horizontal Amplifier

a. Check that the MAG ON neon lights when the SWEEP MAGNIFIER switch is set to each one of these positions: $\mathrm{X} 2, \mathrm{X} 5$, and X 10 .
b. Set the SWEEP MAGNIFIER switch to XI OFF.
24. Adjust B SWEEP LENGTH R125 - B Sweep Generator
a. Check that the display is positioned to start at the left side of the graticule or $0-\mathrm{cm}$ line.

(a) SWEEP MAGNIFIER at XI OFF.

(b) SWEEP MAGNIFIER at $\times 10$.

Fig. 5-9. Time-marker displays.
b. Adjust B SWEEP LENGTH RI25 (see Fig. 5-2) for sweep length of 10.5 cm . When the adjustment is made correctly, there will be five $100-\mu \mathrm{sec}$ time marks after the $5-\mathrm{msec}$ time mark located at the $10-\mathrm{cm}$ graticule line.


Fig. 5-10. Determining sweep-rate accuracy.


Fig. 5-11. Front-panel control settings at the completion of step 26j.

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## 25. Check B VARIABLE (TIME/CM) and UNCALIBRATED Neon - B Sweep Timing Switch

a. Set the time-mark generator for $10-\mathrm{msec}$ and 5 -misec time-mark output.
b. Adjust the B TRIGGERING LEVEL control to trigger on the $10-\mathrm{msec}$ time markers.
c. Turn the B VARIABLE (TIME/CM) control a few degrees in the counterclockwise direction. The IIN. CALIBRATED neon should light as the switch on the control is activated.
d. Turn the B VARIABLE control to its fully counterclockwise position. At least 25 msec of time for a distance of 10 cm should be displayed to indicate a ratio of 2.5 to 1 . That is, the $5 \cdot \mathrm{msec}$ marlers should be spaced at intervals of 2 cm or less.
e. Set the B VARIABLE control to the CALIBRATED p.osition.

## 26. Adjust DELAY START R418 - Delay Pickoff

a. Apply 1-msec time markers only to the TU-7 Ext Input connector.
b. Set the TU-7 Variable control so the display is about 2 cm in amplitude.
c. Set the oscilloscope front-panel controls to the tollowing positions:
Time Base A
triggering level
FULLY CW
TRIGGERING
MODE
SLOPE COUPLING SOURCE
TIME/CM
HORIZONTAL DISPLAY
Main Time Base (B)
TRIGGERING

| MODE | TRIG |
| :--- | :--- |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | NORM INT |
| TIME/CM | 1 mSEC |

d. Adjust the B TRIGGERING LEVEL control for stable triggering on the $1-\mathrm{msec}$ time markers.
e. Turn the BRIGHTNESS control in the counterclockw ise direction and the INTENSITY control in the clockw ise direction to make the brightened portion of the clisplay easily distinguishable.
f. Set the HORIZONTAL DISPLAY switch to ALT (B INTENS BY 'A'-ALT-A DLY'D) position.
g. Turn the oscilloscope TRACE SEPARATION conirol clockwise to position the delayed presentation (A display) above the intensified presentation ( $B$, lisplay). Use the TU. 7 and oscilloscope positioning controls to center the display vertically and to start at the left side of the graticule.
h. Turn the DELAY-TIME MULTIPLIER control fully counterclockwise and check for a dial reading of 0.15 . If the dial reading is not 0.15 , loosen the setscrew in the knob. Reposition the knob so the dial reading is 0.15 and then retighten the set-screw.
i. Turn the DELAY-TIME MULTIPLIER control fully clockwise and check for a minimum dial reading of 10.15.
j. Turn the DELAY-TIME MULTIPLIER control to read 1.00 . Fig. $5-11$ shows the front-panel control settings up to this point in the procedure.
k. Adjust DELAY START R418 (see Fig. 5-2) so the 2nd 1 -msec time marker on the B display is brightened. For an accurate adjustment, observe the A time-base display and set DELAY START R418 so the rising portion, starting from the $90 \%$ level of the marker, is displayed (see Fig. 5-12). The A display is a 100X magnification of the brightened portion of the B display.


Fig. 5-12. Adjusting the DELAY START R418 control for proper A delayed-sweep sfarting lime.

## 27. Adjust DELAY STOP R415 Delay Pickoff

a. Set the DELAY-TIME MULTIPLIER control to 9.00 .
b. Adjust DELAY STOP R415 (see Fig. 5-2) so the A display starts from the $90 \%$ point on the rise of the 1 -msec marker. This magnified 1 -msec marker on the $\mathbf{A}$ display is the same marker as the brightened $1-\mathrm{msec}$ marker located on the B display at the $9-\mathrm{cm}$ graticule line. If the adjustment is made correctly, the A display obtained in this step should appear the same as the A display obtained when performing step 26k (shown in Fig. 5-12).
c. Due to interaction between the DELAY START and DELAY STOP adjustments, set the DELAY-TIME MULTIPLIER control to 1.00 and repeat steps $26 j$ through 27b until the A sweep starts at the same point on the 1st- and 9th-cm time markers, respectively.
28. Check Incremental Accuracy - Delay Pickoff

Set the DELAY-TIME MULTIPLIER control so th: A sweep starts at the $90 \%$ point on the rising portion of the 1 -msec markers for each setting as givent in Table 5-4.
29. Adjust C186 (Unblanking Compensation Capacitor) B Sweep Generator
a. Set the oscilloscope and TU. 7 front-panel conirols to these seltings:

TU-7 Test Function Gain Set
TABLE 5-4

| DELAY TIME MULTIPLIER |  |
| :---: | :---: |
| Control Selting | Tolerance |
| 1.00 | 0 (Adjusted) |
| 2.00 | $\pm 2.0$ minor div. |
| 3.00 | $\pm 2.0$ minor div. |
| 4.00 | $\pm 2.0$ minor div. |
| 5.00 | $\pm 2.0$ minor div. |
| 6.00 | $\pm 2.0$ minor div. |
| 7.00 | $\pm 2.0$ minor div. |
| 8.00 | $\pm 2.0$ minor div. |
| 9.00 | 0 (Adjusted) |
| A TRIGGERING LEVEL | Fully clockwise |
| A TIME/CM | $50 \mu \mathrm{SEC}$ |
| HORIZONTAL DISPLAY | AlT (A-AlT-B) |
| B TRIGGERING LEVEL | Fully clockwise |
| B MODE | AUTO |
| B TIME/CM | $50 \mu$ SEC |
| BRIGHTNESS | Fully clockwise |
| INTENSITY | Slightly below normal |

b. Adjust the TRACE SEPARATION control so the 'wo traces are spaced 2 mm apart. Use the TU. 7 Vertical Position control to center the traces on the cri.
c. Readjust the BRIGHTNESS control so the B trac: is the same brightness as the A trace along the distance from about 2 cm to 10 cm .
d. Adjust Cl 86 (see Fig. 5 -13) so the starting portion of the B trace is the same brightness as the staring portion of the A trace.

## NOTE

C186 has the greatest effect on the first 8 mm of the $B$ trace.
30. Adjust C90C ( $10-\mu$ sec B Sweep-Rate Timing to DELAY-TIME MULTIPLIER) - B Sweep Timing Switch
a. Set the time-mark generator for a $10 . \mu \mathrm{sec}$ tinemarker output.
b. Set the TU-7 and oscilloscope front-panel controls as follows:

| TU-7 Test Function | Low Load |
| :--- | :--- |
| A TIME/CM | $.1 \mu$ SEC |
| HORIZONTAL DISPLAY | ALT (B INTENS BY 'A'- |
|  | ALT-A DLY'D) |
| B TRIGGERING LEVEL | Pushed in |
| B MODE | TRIG |
| B TIME/CM | $10 \mu$ SEC |
| BRIGHTNESS | Near midrange |
| INTENSITY | Normal intensity |

c. Adjust the B TRIGGERING LEVEL control to obtain a stable display.
d. Set the TU. 7 Variable control so the B display is about 2 cm in amplitude.
e. Turn the TRACE SEPARATION control to position the the $A$ delayed-sweep display above the $B$ display.
f. Set the DELAY-TIME MULTIPLIER so the $50 \%$ point on the rising portion of the 2 nd $10-\mu \mathrm{sec}$ time marker is brightened. Use the A display to accurately determine the $50 \%$ point.
g. Note the DELAY-TIME MULTIPLIER dial reading in relation to 1.00 .
h. Set the DELAY-TIME MULTIPLIER control to read exactly 8.00 plus the dial reading obtained in the previous step.
i. Adjust C90C (see Fig. $5-2$ ) so the $\mathbf{5 0} \%$ point on the rising portion of the 10 th time marker is the $50 \%$ starting point on the A display.
i. Since there is interaction which affects the dial reading obtained in step 30 g , repeat steps 30 f through 30i until the DELAY-TIME MULTIPLIER dial indicates a difference of exactly 8.00 between the 2 nd and 10th time markers.
31. Adjust C90B (1- $\mu$ sec B Sweep-Rate Timing to DE-LAY-TIME MULTIPLIER) - B Sweep Timing Switch
a. Set the time-mark generator for a $1-\mu \mathrm{sec}$ time-marker output.
b. Set the A TIME/CM switch to $.1 \mu$ SEC and the B TIME/CM switch to $1 \mu \mathrm{SEC}$.
c. Adjust the TU. 7 Variable control so the displays are each 2 cm in amplitude.
d. Adjust the B TRIGGERING LEVEL control to trigger on the time markers.
e. Set the DELAY-TIME MULTIPLIER control so the 2nd time marker on the B display is brightened starting at the $50 \%$ point on the rising portion of the marker. Use the A display to determine the $50 \%$ point accurately.
f. Note the DELAY-TIME MULTIPLIER dial reading.


Fig. 5-13. Calibration adjustment lecetions.
g. Set the DELAY-TIME MULTIPLIER control to read exactly 8.00 plus the dial reading noted in the previous step.
h. Adjust C90B (see Fig. 5-2) so the $50 \%$ point on the rising portion of the 10 th time marker is the $50 \%$ starting point of the A display.
i. Due to interaction that affects the DELAY-TIME MULTIPLIER dial reading that was obtained for the 2nd time marker, repeat steps 31 e through 31 h until the DELAY-TIME MULTIPLIER dial indicates an exact 8.00 difference between the 2nd and 10th time markers.
32. Adjust C90A ( $0.5-\mu \mathrm{sec}$ B Sweep-Rate Timing to the DELAY-TIME MULTIPLIER) - B Sweep Timing Switch
a. Set the time-mark generator for a 5 -mc sine-wave output,
b. Set the B TIME/CM switch to $.5 \mu \mathrm{SEC}$.
c. Adjust the TU-7 Variable control to reduce the amplitude of the display to a suitable level.
d. Adjust the B TRIGGERING LEVEL control to oblain stable displays.
e. Turn the INTENSITY control clockwise to increase the brightness of the two waveforms.
f. Check that the first 2 cm of the starting portion of the B display is linear. If it is not, preset C99 (see Fig. 5-2) to obtain best linearity of the storting portion of the display.
g. Check that there is $21 / 2$ cycles $/ \mathrm{cm}$ for the remaining portion of the B display. If there is not, preadjust C90A (see Fig. 5-2) for proper timing.
h. For a more exact adjustment of C90A, position the B display with the HORIZONTAL POSITION control so the tip of the 6th sine wave aligns with the $2-\mathrm{cm}$ graticule line.
i. Sef the DELAY-TIME MULTIPLIER control so the brightened portion of the B display starts at the $50 \%$ point on the rising portion of the 6th sine wave. To set the DELAY-TIME MULTIPLIER control as accurately as possible, use the A display to determine the 50\% point.
i. Note the DELAY-TIME MULTIPLIER dial reading. It should read approximately 2.00 .
k. Set the DELAY-TIME MULTIPLIER control to 7.00 plus the reading noted in the previous step. The falling portion of the 23rd sine wave, starting at the $50 \%$ point, should be brightened as observed on the B display. Use the A display to see the $50 \%$ point clearly. If the $50 \%$ point is not obtained, adjust C90A for the correct point on the A display while
maintaining a timing of $21 / 2$ cycles $/ \mathrm{cm}$ on the $B$ display.
I. Repeat steps 32 h through 32 k until the DELAY-TI/AE MULTIPLIER dial indicates an exact difference of 7.00 between the $50 \%$ point on the rising portion of the 6 th sine wave and the $50 \%$ point on the falling portion of the 23 rd sine wave. The list half cycle of the 23 rd sine wave is the port on of the B display that aligns with the $9-\mathrm{cm}$ gratic ile line when correct timing of $21 / 2 \mathrm{cycles} / \mathrm{cm}$ is ib. tained.
33. Adjust C99 (B Sweep Output Compensation to Crt Display) - B Sweep Generator
a. Set the time-mark generator for 10 -me sine-weive output.
b. Set the HORIZONTAL DISPLAY switch to B.
c. Set the B TIME/CM switch to $.1 \mu \mathrm{SEC}$.
d. Use the TU-7 Vertical Position control to center he display vertically.
e. Using the oscilloscope HORIZONTAL POSITICN control, position the tip of the 2nd sine wave to align with the $1 . \mathrm{cm}$ graticule line.
f. Adjust C 99 for correct timing of $1 \mathrm{cycle} / \mathrm{cm}$.
g. Due to interaction between the adjustment of (99 and C90A, repeat the procedure for these adjustments outlined in steps 32 a through 33 f until the desired results are obtained.
34. Check $0.2-\mu \mathrm{sec} / \mathrm{cm}$ Sweep Rate-B Sweep Timing Switch
a. Set the HORIZONTAL DISPLAY switch to the ALT (B INTENS BY 'A'-ALT-A DLY'D) position.
b. Set the B TIME/CM switch to $.2 \mu \mathrm{SEC}$.
c. Center the display vertically. The A display shculd be located above the B display.
d. Horizontally position the displays so the 2nd !ine wave of the B display coincides with the 2 cm graticule line.
e. Set the DELAY-TIME MULTIPLIER control so the 51$) \%$ point starting on the rising portion of the 2nd :ine wave is brightened on the B display. Use the A display to determine the $50 \%$ point.
f. Note the DELAY-TIME MULTIPLIER dial reading.
g. Turn the DELAY-TIME MULTIPLIER control clockvise until the $50 \%$ point starting on the rising portion of the sine wave at the $9-\mathrm{cm}$ graticule line is brightel ed. Use the A display to determine the $50 \%$ point. Note the dial reading.
$h$. The difference between the dial reading noter in step 34 f and the one noted in step 34 g should be 7.00 within a tolerance of 1.17 minor divisions.
i. Set the B TIME/CM switch to $.5 \mu \mathrm{SEC}$. Recheck He B $0.5 \mu \mathrm{sec}$ sweep-rate timing using the DELAY-TME

MULTIPLIER control and a 5 -me sine-wave input from the time-mark generator. Timing accuracy: $\pm 1 \%$.
35. Check $2-\mu \mathrm{sec}$ through $5-\mathrm{sec} / \mathrm{cm}$ Sweep Rates B Sweep Timing Switch
a. Using Table 5-5 as a guide, check the Main Time Base (B) sweep rates from $2 \mu \mathrm{sec}$ through 50 msec . Use the DELAY-TIME MULTIPLIER control to determine sweep-rate accuracy. First note the dial readings near the 1.00 setting of the DELAY-TIME MULTIPLIER dial for the sweep rate being checked. Do not move the B TRIGGERING LEVEL control after obtaining the reading. Then note the dial reading obtained near the 9.00 position for the same sweep rate. Next, determine the difference between the two dial readings. This difference should be 8.00 within a tolerance of $\pm 1 \%$. Check each sweep rate in Table 5-5 using this method.

TABLE 5-5

*Adjusted proviously.
b. Using Table 5.6 as a guide, check the sweep rates from $0.1 \mathrm{sec} / \mathrm{cm}$ through $5 \mathrm{sec} / \mathrm{cm}$. Use the same procedure as outlined in step 35a.
When checking each of these sweep rates, set the HORIZONTAL DISPLAY switch to B INTENS BY 'A' to check that the proper number of markers $/ \mathrm{cm}$ are obtained and to set the DELAY-TIME MULTIPLIER control so the marker at the $1 . \mathrm{cm}$ graticule line is brightened. Then, set the HORIZONTAL DISPLAY switch to A DLY'D and use the DELAY-TIME MULTIPLIER control to determine the exact point on the marker where the delayed sweep should start. Note the dial reading. Use this same method to obtain the dial reading from 9.00 . Determine the difference which should be 8.00 within a tolerance of $\pm 1 \%$.

TABLE 5-6

| B Time/Cm <br> Switch <br> Setting | A Time/Cm <br> Switch <br> Setting | Time-Mark <br> Generator <br> Output | Markers/C <br> on <br> on |
| :---: | :---: | :---: | :---: |
| .1 SEC | 10 mSEC | 100 msec | 1 |
| .2 SEC | 10 mSEC | 100 msec | 2 |
| .5 SEC | 10 mSEC | 500 msec | 1 |
| 1 SEC | .1 SEC | 1 sec | 1 |
| 2 SEC | .1 SEC | $\frac{1 \mathrm{sec}}{2}$ | 2 |
| 5 SEC | .1 SEC | 5 sec | 1 |

36. Adjust C572 and C582 (High-Speed Sweop Length Compensation) - Horizontal Amplifier.
a. Set the oscilloscope front-panel controls to these settings:

| HORIZONTAL DISPLAY | B |
| :--- | :--- |
| B SOURCE | EXT |
| B TIME/CM | $.1 \mu$ SEC |

b. Set the time-mark generator for a 50 -me sine-wove output.
c. Connect a coaxial cable from the trigger output of the time-mark generator to the B TRIGGER INPIJT connector.
d. Set the trigger rate of the time-mark generator tor a $10-\mu \mathrm{sec}$ trigger output.
e. Adjust the INTENSITY control so the display is easily visible and adjust the B TRIGGERING LEVEL control to obtain a stable display.
f. Adjust the HORIZONTAL POSITION control to pe.sition the display at start at the $0-\mathrm{cm}$ line of the graticule.
g. Check that C576 and C586 (see Fig. 5-13) slugadjusting screws are about six turns above the meial wiper contacts of the capacitors.
h. Set the SWEEP MAGNIFIER switch to X 10 .
i. Adjust C572 and C582 (see Fig. 5-13) for maximum center-sweep expansion. (Use a low-capacitance alignment tool when making the adjustments.) The se two capacitors should be adjusted to nearly the same physical setting.
37. Adjust C591 (High-Speed Sweep Linearity) - Horizontal Amplifier

Adjust C591 (see Fig. 5-13) for best center-sweap linearity of 1 cycle $/ 2 \mathrm{~cm}$.
38. Adjust C576 and C586 (High-Speed Timing Adjustments) - Horizontal Amplifier

Adjust C576 and C586 in equal increments for b.sst timing of $1 \mathrm{cycle} / 2 \mathrm{~cm}$ from the $2-\mathrm{cm}$ graticule line to the 8 cm graticule line.
39. Adjust C557H $(\times 10$ SWEEP MAGNIFIER Compenstation) - Horizontal Amplifier
a. Turn the HORIZONTAL POSITION control clo. $k$ wise so the start of the sweep (or display) can se
seen. Then, position the tip of the 4 th cycle from the start of the sweep to coincide with the $4-\mathrm{cm}$ graticule line.
b. Adjust C557H (see Fig. 5-2) for best timing of 1 cycle $/ 2 \mathrm{~cm}$ from the $4 . \mathrm{cm}$ to $10-\mathrm{cm}$ graticule lines.
c. Set the SWEEP MAGNIFIER switch to OFF.
d. Using the HORIZONTAL POSITION and VERNIER controls, position the display to the left so the 10 thcm portion of the sweep coincides with the $7-\mathrm{cm}$ graticule line.
e. Set the SWEEP MAGNIFIER switch to $\times 10$.
f. Note the timing error of the display from the $1 . \mathrm{cm}$ to the $9 . \mathrm{cm}$ graticule lines; it should be within $5 \%$.
40. Check Timing Accuracy - Horizontal Amplifier

Check the timing accuracy of the display between the 4 th cm and 80 th cm of the sweep. Magnifiedtiming in this region must be within $5 \%$ or less. If, in the 20 hh cm region some nonlinearity is observed, readjust C591 to make the sweep more linear.

## NOTE

If the adjustments in steps 36 through 40 are accurate, the magnified sweep timing can be adjusted to better than $\pm 5 \%$.
41. Adjust C557F $(\times 5$ SWEEP MAGNIFIER Compensafion) - Horizontal Amplifier
a. Set the SWEEP MAGNIFIER switch to $\times 5$.
b. Adjust C557F (see Fig, 5-2) for $1 \mathrm{cycle} / \mathrm{cm}$ after the first 2 cm from the start of the sweep.
42. Adjust C557D ( $\times 2$ SWEEP MAGNIFIER Compensation) - Horizontal Amplifier
a. Set the SWEEP MAGNIFIER switch to $\times 2$.
b. Adjust C557D (see Fig. 5-2) for $2 \frac{1}{2}$ cycles $/ \mathrm{cm}$ after the first cm from the start of the sweep.

## 43. Adjust A SWEEP DC LEVEL R470 - Alternate Sweep Switching

a. Set the time-mark generator for $100-\mu \mathrm{sec}$ timemarker output.
b. Set the front-panel controls of the oscilloscope to these settings (some of the controls need not be changed since they are already set properly):
A and B TRIGGERING

| TRIGGERING LEVEL | Pushed in |
| :--- | :--- |
| MODE | AUTO |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | NORM INT |
| A and B TIME/CM | 1 mSEC |
| HORIZONTAL DISPLAY | ALT (A-ALT-B) |
| SWEEP MAGNIFIER | $\times 1$ OFF |

c. Set the TU. 7 Variable control so the markers are 3 cm in amplitude.
d. Adjust the HORIZONTAL POSITION control so both sweeps start near the center of the crt.
e. Set the SWEEP MAGNIFIER switch to $\times 10$ (recenter start of sweep if necessary).
f. Adjust A and B TRIGERING LEVEL controls to :tart each sweep on a time marker.
g. Adjust TRACE SEPARATION control to superimpiose the two displays. Fig. $5-14$ shows the front-poinel setup thus far in the procedure.
h. Adjust A SWEEP DC LEVEL R470 (see Fig. 5-2) so the start of the $A$ sweep coincides with the start of the B sweep.

## 44. Adjust A SWEEP LENGTH R325 - A Sweep Generafor

a. Set the HORIZONTAL POSITION and VERNIER controls so the end of the B sweep is located near the center of the crt.
b. Set the A SWEEP LENGTH R235 (see Fig. 5-2) so the A sweep length equals the sweep length of th: B sweep.
45. Adjust A SWP CAL R290Y - A Sweep Timing Switch

Adjust A SWP CAL R290Y (see Fig. 5-2) so that ersch time marker on the A sweep display coincides $v$ ith the corresponding time marker on the B sweep tlisplay.
46. Check A VARIABLE (TIME/CM) and UNCALIBRATED Neon - A Sweep Timing Switch
a. Set the time-mark generator for a $10-\mathrm{msec}$ and $5-\mathrm{msec}$ time-marker output.
b. Set the HORIZONTAL DISPLAY switch to A and the SWEEP MAGNIFIER switch to $\times 1$ OFF,
c. Set the HORIZONTAL POSITION control to peisition the display to start at the $0-\mathrm{cm}$ graticule line.
d. Adjust the TU-7 Variable control so the $10-\mathrm{m}: \mathrm{ec}$ markers are about $3-\mathrm{cm}$ in amplifude.
e. Adjust the A TRIGGERING LEVEL control to trigser the sweep on the $10-\mathrm{msec}$ markers.
f. Turn the A VARIABLE (TIME/CM) control a fitw degrees in the counterclockwise direction. Check that the UNCALIBRATED neon lights as the switch on the control is activated.
g. Turn the A VARIABLE control to its fully countrclockwise position. At least 25 msec of time for a distance of 10 cm should be displayed to indicate a ratio of at least 2.5 to 1 .
h. Set the A VARIABLE control to the CALIBRATED pcsition.
47. Adjust C290C (10- $\mu$ sec A Sweep-Rate Timing) A Sweep Timing Switch
a. Set the time-mark generator for a $10-\mu \mathrm{sec}$ time marker output.
b. Set the oscilloscope front-panel controls to the following settings:
A and B TIME/CM
$10 \mu \mathrm{SEC}$
HORIZONTAL DISPLAY
ALT (A-ALT-B)
c. Set the TU-7 Variable control so the markers are about 3 cm in amplitude.
d. Adjust the A and B TRIGGERING LEVEL controls to trigger on the $10-\mu \mathrm{sec}$ time markers.
e. Check that the TRACE SEPARATION control is set to superimpose the displayed waveforms.
f. Adjust C290C (see Fig. 5-2) so that each time marker displayed by the A sweep coincides with the correspanding time marker on the B sweep.

## NOTE

For better accuracy, position the 2nd marker to graticule center using the HORIZONTAL POSITION control. Then set the SWEEP MAGNIFIER switch to $\times 10$, Adjust the A and B TRIGGERING LEVEL contrals carefully so the tips of the 2nd markers coincide. Set the SWEEP MAGNIFIER switch to $\times 1$ OFF and position the 10 th marker to graticule center, Set the SWEEP MAGNIFIER switch to $\times 10$. If the 10th A display marker does not coincide with the 10th B display marker, readiust C290C for proper matching of markers.
g. Set the SWEEP MAGNIFIER switch to $\times 1$ OFF.
h. Position the sweeps to start at the $0 . \mathrm{cm}$ graticule line,
48. Adjust C290日 (1- $\mu$ sec A Sweep-Rate Timing) A Sweep Timing Switch
a. Set the time-mark generator for a $1-\mu \mathrm{sec}$ timemarker output.
b. Set the $A$ and $B$ TIME/CM switches to $1 \mu S E C$.
c. Set the TU. 7 Variable control so the markers are about 3 cm in amplifude.
d. Adjust C290B (see Fig. 5-2) so that each time marker displayed by the A sweep exactly coincides with the corresponding time marker on the B sweep.

## NOTE

If exact matching of markers cannot be obtained by adjusting C 290 B , proceed to the next step since C299 affects the linearity of the A sweep for the first one half of the sweep. Repeat steps 48 and 49 until A sweep timing motches the B sweep timing as close as possible.
(To obtain best accuracy when adjusting C290B and C299, use the same basic procedure as described in the NOTE following step 47f).

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Fig. 5-14. Front-panel control settings at the completion of step $\mathbf{4 3} \mathrm{g}$.
49. Adjust C299 (A Sweep Output Compensation) A Sweep Generator
a. If the markers do not coincide accurately when adjusting C290B due to some nonlinearity in th: A sweep, adjust C299 (see Fig. 5-13) for best linearity for the first half of the A sweep.
b. Readjust C290B for correct matching of marker: at the end of the A sweep. Adjust C290B and C299 for best matching of the A display to the B display.
c. Check that the SWEEP MAGNIFIER switch is set to $\times 1$ OFF and the displays are positioned to start at the $0-\mathrm{cm}$ graticule line.
50. Adjust C290A ( $0.5-\mu$ sec $A$ Sweep-Rate Timing) A Sweep Timing Switch
a. Set the time-mark generator for a 5 -mc sine-wave output.
b. Set the A and B TIME/CM switches to $.5 \mu \mathrm{SEC}$
c. Use the TU-7 Variable control to reduce the an plitude of the displays to about $4-\mathrm{cm}$.
d. Adjust the A and B TRIGGERING LEVEL controls for two stable sine-wave displays whose first few cycles coincide.
e. Adjust C290A (see Fig. 5-2) so that each cycle sifter the first 5 cycles of the A display exactly coincides with the corresponding cycles of the B display. Use the $\times 10$ position of the SWEEP MAGNIFIER su itch to magnify the display to make the adjustment nore accurate.

## 51. Readjust C299 (0.1- $\mu$ sec A Sweep-Rate Timing) A Sweep Generator

a. Set the time-mark generator for a $10-\mathrm{mc}$ sine wave output.
b. Set the A and B TIME/CM switches to $.1 \mu^{\prime} \mathrm{iEC}$.
c. Adjust the A and B TRIGGERING LEVEL conirols for two stable sine-wave displays whose first few cycles coincide.
d. Readjust C299 to make the A display match the B display. Use the X10 position of the SWEEP MAGNIFIER switch for more exact adjustment.
e. Repeat steps 50a through 51d for the most accurate matching of the $A$ sweep to the $B$ sweep.
52. Check $0.1-\mu \mathrm{sec} / \mathrm{cm}$ Through $5-\mathrm{sec} / \mathrm{cm}$ Sweep Rates - A Sweep Timing Switch
a. Check that the A TMME/CM switch is set to, $1 \mu ; \mathrm{EC}$.
b. Starting with the $0.1-\mu \mathrm{sec} / \mathrm{cm}$ sweep rate, clieck each of the Time Base A sweep rates using Table 5.7 as a guide. Tolerance for the fixed (nonadjustable) sweep rates is $\pm \mathbf{2 \%}$.

## NOTE

If you prefer, leave the HORIZONTAL DISPLAY switch of A-ALT-B and compare the sweep-rate
timing of A with B on sweep rates from $0.1 \mu \mathrm{sec} /$ cm to $50 \mathrm{msec} / \mathrm{cm}$. Sweep rates slower than 50 $\mathrm{msec} / \mathrm{cm}$ can best be checked by setting the HORIZONTAL DISPLAY switch to A and checking the A sweep-rate timing with the graticule. At the slower sweep rates position the base of the marker display downward out of view and observe the tips of the mrakers.
c. After checking the sweep rates, disconnect the timemark generator and interconnecting cables from the oscilloscope/TU-7 combination.

TABLE 5-7

| A and B TIME/CM Switch Settings | Time-Mark Generator Output | Check For |
| :---: | :---: | :---: |
| . $1 \mu$ SEC* | 10 mc | $1 \mathrm{cycle} / \mathrm{cm}$ |
| , $2 \mu$ SEC | 5 mc | 1 cycle/cm |
| . $5 \mu$ SEC* | $1 \mu \mathrm{sec}$ | 1 marker/2 cm |
| $1 \mu \mathrm{SEC} *$ | $1 \mu \mathrm{sec}$ | 1 marker/cm |
| $2 \mu \mathrm{SEC}$ | $1 \mu \mathrm{sec}$ | 2 markers/cm |
| $5 \mu \mathrm{SEC}$ | $5 \mu \mathrm{sec}$ | 1 marker/cm |
| $10 \mu$ SEC* | $10 \mu \mathrm{sec}$ | 1 marker/cm |
| $20 \mu \mathrm{SEC}$ | $10 \mu \mathrm{sec}$ | 2 markers/cm |
| $50 \mu \mathrm{SEC}$ | $50 \mu \mathrm{sec}$ | 1 marker/cm |
| 1 mSEC | $100 \mu \mathrm{sec}$ | 1 marker/cm |
| . 2 mSEC | $100 \mu \mathrm{sec}$ | 2 markers/cm |
| .5 mSEC | $500 \mu \mathrm{sec}$ | 1 marker/cm |
| $1 \mathrm{mSEC} *$ | 1 msec | 1 marker/cm |
| 2 mSEC | 1 msec | 2 markers/cm |
| 5 mSEC | 5 msec | 1 marker/cm |
| 10 mSEC | 10 msec | 1 marker/cm |
| 20 mSEC | 10 msec | 2 markers/cm |
| 50 mSEC | 50 msec | 1 marker/cm |
| . $\mathrm{SEC}^{* *}$ | 100 msec | 1 marker/cm |
| . 2 SEC** | 100 msec | 2 markers/cm |
| . 5 SEC** | 500 msec | 1 marker/cm |
| 1 SEC** | 1 sec | 1 marker/cm |
| 2 SEC** | 1 sec | 2 markers/cm |
| $5 \mathrm{SEC**}$ | 1 sec | 1 marker/cm |

- Adjust previously for exact timing.
*'Set HORIZONTAL DISPLAY switch to A and the A TIME/CM swikh to this setting.


## 53. Adjust EXT HORIZ DC BAL R519 - (External) Horizontal Amplifier

a. Set the front-panel controls of the oscilloscope and TU-7 to the following settings:

## Oscilloscope

A TRIGGERING LEVEL Fully clockwise, pushed in
AUTO
$+$
AC

| A SOURCE | EXT |
| :--- | :--- |
| A TIME/CM | 1 mSEC |
| HORIZONTAL DISPLAY | EXT $\times 1$ |
| VAR 10-1 | Fully clockwise |
| B TRIGGERING LEVEL | Fully counterclockwise |

Type TU-7

Vertical Position
Test Function
Variable

## Centered

 Low Load 2.5b. Connect the single binding-post adapter to the TU 7 Ext Input connector.
c. Connect an interconnecting lead from the adapter at the TU. 7 Ext Input connector to the SWEEP A connestor on the oscilloscope.
d. Connect an interconnecting lead from the HORIZ INPUT connector to ground.
e. Using the HORIZONTAL POSITION control, po :itimon the vertical free-running sweep to the center of the graticule. Adjust the INTENSITY control, if necessary, to make the trace visible.
f. Adjust EXT HORIZ DC BAL R5I9 (see Fig. 5-2) for no horizontal shift of the vertical trace as the VAR 10-1 control is turned.
g. Disconnect the interconnecting lead from the HORIZ INPUT connector to ground.
54. Adjust C524 Output Compensation - (External) Horizontal Amplifier
a. Connect a BNC T connector to the oscilloscope CAL OUT connector.
b. Connect a coaxial cable from one end of the BNC T connector to the A TRIGGER INPUT connector.
c. Connect another coaxial cable from the other end of the BNC T connector through the coaxial connestor adapter to the HORIZ INPUT connector.
d. Set the AMPLITUDE CALIBRATOR switch to 5 VOLTS and adjust the A TRIGGERING LEVEL controt to obtain a stable display.
e. Check that the VAR 10-1 control is set fully clockwise.
f. Set the HORIZONTAL POSITION control so the display is centered on the crt.
g. Set the TU. 7 variable control so several cycles of the calibrator waveform are displayed (see Figs. 15a ard 15b).
h. Adjust C524 (see Fig. 5-13) for the least distort hd calibrator waveform (see Fig. 5-15a); that is, for minimum fast spike or rolloff.
55. Check Gain - (External) Horizontal Amplifier
a. Set the AMPLITUDE CALIBRATOR switch to 1 VOLTS and check that the VAR $10-1$ control is set fully clockwise.
b. Adjust the A TRIGGERING LEVEL control to obtain a stable display.
c. The calibrator waveform displayed on the crt should be greater than 1 cm in amplitude.


Fig. 5-15. Typical waveform displays with C524 both properly adjusted and misadjusted.
56. Check VAR 10-1 Control Range - (External) Horizontal Amplifier
a. Set the AMPLITUDE CALIBRATOR switch to .5 VOLTS.
b. Note the waveform amplitude in $\mathbf{c m}$.
c. Turn the VAR 10-1 control fully counterclockwise.
d. Check that the waveform amplitude is $1 / 10$, or less of that noted in step 56b.
e. Turn the VAR 10-1 control fully clockwise.

## 57. Adjust C503C ( $\times 10$ Attenuator Compensation) -(External) Horizontal Amplifier

a. Set the HORIZONTAL DISPLAY switch to EXT $\times 10$.
b. Set the AMPLITUDE CALIBRATOR switch to 5 VOLTs.
c. Adjust C503C (see Fig. 5-2) for optimum squarewave response. (Fig. 5-16 shows one form of distertion if C503C is misadjusted.) The display should exhibit no more than $5 \%$ hook on the positive-going or negative-going portion of the calibrator wavisform. When C503C is properly adjusted, the calibrixtor waveform should be similar to the display show. $n$ in Fig. 5-15a.


Fig. 5-16. Distortion oblained when C503C is misadiusted.
58. Check $\times 10$ Attenuation - (External) Horizontal Amplifier
a. Set the HORIZONTAL DISPLAY switch to EXT $\times 1$ and check that the VAR 10-1 control is set fully clockwise.
b. Set the AMPLITUDE CALIBRATOR switch to 5 VOLTS.
c. Note the waveform amplitude in cm .
d. Set the HORIZONTAL DISPLAY switch to EXT $\times 10$.
e. Set the AMPLITUDE CALIBRATOR switch to 5 VOLis and check the amplitude of the display. The signal amplitude should be within $\pm 3 \%$ of that ampliturle noted in step 58c.
f. Set the HORIZONTAL DISPLAY switch to B.
g. Disconnect the adapters, interconnecting lead and coaxial cables.
59. Check and/or Adjust High-Frequency Compenstition - Vertical Amplifier

## NOTE

For optimum adiustment of frequency response a modified Test Plug-in (Load Pulser), 067-0521.01 is recommended. The adjustment may also be accomplished with the Test Plug-in (Load Pulser), 067-0521-00. Both methods are described below.

## Method 1 (Using Test Plug-in 067-0521-01)

1. Same procedure as Step 59 a through g , except set the B TIME/CM switch to $.1 \mu \mathrm{Sec}$ and set the 067-0521-01 Repetition Rate switch to 4 kHz .
2. Adjust R1091 for the best square corner on the top of the display.
3. Set the 067-0521-01 Repetition Rate switch to 15 kHz and the B TIME/CM switch to $20 \mu \mathrm{Sec}$.
4. Adjust R1077 for the best square corner on the top of the display.
5. Set the 067.0521-01 Repetition Rate switch to 80 kHz and the B TIME/CM switch to $.1 \mu \mathrm{Sec}$.
6. Continue with Step $59 \mathrm{~h}, \mathrm{i}, \mathrm{i}$ and k .

## Method 2 (Using Test Plug-in 067-0521-00)

1. Same procedure as Step 59 a through $g$, except set the 067-0521-00 Repetition Rate switch to low.
2. Adjust R1091 for the best square corner on the top of the display.
3. Set the 067-0521-00 Repetition Rate switch to Med and the B TIME/CM switch to $10 \mu \mathrm{Sec}$.
4. Adjust R1077 for the best square corner on the top of the display.
5. Set the B TIME/CM switch to $.1 \mu \mathrm{Sec}$.
6. Continue with Step $59 \mathrm{~h}, \mathrm{i}, \mathrm{i}$ and k .
a. Set the front-panel controls of the oscilloscope to the following positions:

| B TRIGGERING LEVEL | Near 0 |
| :--- | :--- |
| B SOURCE | NORM INT |
| B TIME/CM | $.1 \mu$ SEC |
| SWEEP MAGNIFIER | $\times 1$ |
| BRIGHTNESS | Fully clockwise |
| AMPLITUDE CALIBRA- <br> TOR | OFF |

b. Set the TU-7 front-panel controls as follows:

| Vertical Position | Centered |
| :--- | :--- |
| Test Function | + Pulse |

c. Using the oscilloscope HORIZONTAL POSITION control, position the display to start near the graticule center,
d. Set the TU. 7 Amplitude and Vertical Position controls so the display is vertically centered on the crt and the amplitude of the step-waveform is exactly 4 cm . (See Fig. 5.17 for complete front-panel setup at this point in the procedure.)
e. Using the TU-7 Vertical Position control, position the waveform downward about 2 mm for better visibility (away from the graticule lines).
f. Adjust the INTENSITY control to increase the brightness of the display to normal viewing level.


Fig. 5-17. Front-panel control settings at the completion of step 59 d .


Fig. 5-18. Check of compensation adjustments for optimum Vertical Amplifier transient response.


Fig. 5-19. (a) Vertical Amplifier high-frequency adjustments and Transient Response Compensation switch lecations. (b) 11157 location.


Fig. 5-20. Measuring the risetime of a normal waveform when SW 1000 is actuoted; sweep rate is 10 nsec $/ \mathrm{cm}$.
g. Adjust the FOCUS and ASTIGMATISM controls to produce a well-defined leading top corner on the step waveform.
h. Examine the waveform for clean transient response. Typical waveform should appear similar to Fig. 5-18a.

TABLE 5-8
Vertical Amplifier High-Frequency Adjustments

| Adjustment | For Location See Fig. | Approximate Area Affected* |
| :---: | :---: | :---: |
| L1157 | 5-198 | 0.100 nsec , adjust for minımum wrinkle. |
| ${ }^{1} \mathrm{ClO27}$ | Located on terminals of VERT GAIN POT R1010 5-4 | $10 \%$ to $100 \%$ on the rising portion of the step function. |
| ${ }^{2} \mathrm{C} 1029$ | 5-19a | Termination bump at 340 ns. |
| C1076 | 5.19a | 0-15 nsec |
| C1105 | 5-19a | 1 nsec to 4 nsec |
| C1106 | 5.19a | 5 nsec to 35 nsec |
| C1126 | 5.19a | 20 nsec to 80 nsec |
| R1076 | 5-19a | 0 to 10 nsec |
| R1106 | 5.19a | 2 nsec to 20 nsec |

*Distonce measured to the right starting from $\mathbf{9 0 \%}$ point on the rising portion of the wavelorm. For example on Fig. 5.18 c .
${ }^{\prime}$ 'Aduast $\mathbf{C 1 0 2 7}$ for a sysiem risetime of $\mathbf{6 . 9 3}$ nsec or fastor; based on a 3 niec risetime pulse from the TU-7. (If C1027 is adjusted for a risetime considerably foster than 6.93 nsec and aberrations are difficult to smooth out with remaining adjustments, then make the system riselime slower, towards 6.93 nsec, by readjusting C 1027. Minimize the aberrations by readjusting all of the adjustments below C1027 in Toble 5-8.1 This odjustment applicable for SN 4750-up.
${ }^{2}$ If there is no tormination bump, adjust $\mathbf{C 1 0 2 9}$ for a low of C if possible, or for the fostest risetime.
i. Set the SWEEP MAGNIFIER switch to $\times 10$.
i. Measure the risetime of the rising portion of the waveform from the $10 \%$ point to the $90 \%$ point (see Fig. $5-18 b)$. The system risetime should not be any slower than 6.93 nsec based on a 3 -nsec risetime pulse from the TU-7. (Take into consideration sweep-timing error, if any, and/or geometry in the area where the measurement is made.)
k. If the aberrations appear excessive and/or the risetime is slower than 6.93 nsec , set the SWEEP MAGNIFIER switch to $\times 1$ and adjust the high-frequency adjustments using Table 5.8 as a guide. Since the adjustments interact, it is necessary to repeat the adjustment procedure several times to obtain a waveform with good transient response. When making the adjustments, keep the step waveform vertically centered on the crt.

## NOTE

To check the overall level and maintain a flat top when making the adjustments, use the different SWEEP MAGNIFIER switch positions.
60. Check Transient Response Compensation Switch SW1000 - Vertical Amplifier
a. Check that the B TIME/CM switch is set to $.1 \mu$ SEC and the SWEEP MAGNIFIER switch is set to $\times 10$.
b. Depress Transient Response Compensation Switch SW1000 \located at the bottom of the plug-in compartment rear panel). Check the risetime of the step waveform from the $10 \%$ to $90 \%$ points on the rising portion of the waveform (see Fig. 5-20). Overall risetime should not be any slower than 10 nsec .

# SECTION 6 <br> PARTS LIST and DIAGRAMS 

## PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix Field Office.
Changes to Tektronix instrument; are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engit eering department. It is therefore important, when ordering parts, to include the following information in your order: Part number including any suffix, instrument type, serial nu nber, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix Field Office will cont.uct you concerning any change in part number.

| ABBREVIATIONS AND SYMBOLS |  |  |  |
| :---: | :---: | :---: | :---: |
| a or amp | amperes | mm | millimeter |
| BHS | binding head steel | meg or M | megohms or mega ( $10^{6}$ ) |
| C | carbon | met. | metal |
| cer | ceramic | $\mu$ | micro, or $10^{6}$ |
| cm | centimeter | n | nano, or $10^{-9}$ |
| comp | composition | $\Omega$ | ohm |
| cps | cycles per second | OD | outside diameter |
| crt | cathode-ray tube | OHS | oval head steel |
| CSK | counter sunk | p | pico, or $10^{12}$ |
| dia | diameter | PHS | pan head steel |
| div | division | piv | peak inverse voltage |
| EMC | electrolytic, metal cased | pistc | plastic |
| EMT | electroylitic, metal tubular | PMC | paper, metal cased |
| ext | external | poly | polystyrene |
| $f$ | farad | Prec | precision |
| F \& I | focus and intensity | PT | paper tubular |
| FHS | flat head steel | PTM | paper or plastic, tubular, molded |
| Fil HS | fillister head steel | RHS | round head steel |
| $g \text { or } G$ | giga, or $10^{\circ}$ | rms | root mean square |
| Ge | germanium | sec | second |
| GMV | guaranteed minimum value | Si | silicon |
| h | henry | S/N | serial number |
| hex | hexagonal | $t$ or T | tera, or $10^{12}$ |
| HHS | hex head steel | TD | toroid |
| HSS | hex socket steel | THS | truss head steel |
| HV | high voltage | tub. | tubular |
| ID | inside diameter | v or V | volt |
| incd | incandescent | Var | variable |
| int | internal | w | watt |
| $\mathrm{k}_{\mathrm{kc}}$ or K | kilohms or kilo (10) | w/ |  |
| kc | kilocycle milli, or $10^{-3}$ | w/o | without ${ }_{\text {wire-wound }}$ |
| mc | megacycle |  |  |

## SPECIAL NOTES AND SYMBOLS

X000 Part first added at this serial number.
000X Part removed after this seiial number.
*000-000 Asterisk preceding Tektronıx Part Number indicates manufactured by or for Tektronix, or reworked or checked components.

Use 000-000
(1)

Part number indicated is direct replacement.
Internal screwdriver adjus'ment.
Front-panel adjustment or connector.


## EXPLODED VIEW



EXPLODED VIEW (Cont'd)

| REF. | Part no. |  | ODEL NO. | i | description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NO. | PART NO. | EFF. | Disc. |  | Descripmon |
| 15 | 333-0754-00 |  |  | 1 | PANEL, front |
|  | 213-0088-00 |  |  | 3 | Mounting Hardware: (not included) SCREW, thread forming, $4-40 \times 1 / 4$ inch PHS |
| 16 | 366-0038-00 |  |  | 2 | KNOB, VARIABLE, small red |
|  | … |  |  | - | Each Includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6.32 \times 3 / 16$ inch HSS |
| 17 | 366-0144-00 |  |  | 1 | KNOB, "B" TIME/CM OR DELAY TIME, large charcoal |
|  | 213-0004-00 |  |  | 1 | Includes: SCREW, set, $6.32 \times 3 / 16$ inch HSS |
| 18 | 262-0596-00 | 100 | 5309 | 1 | SWITCH, "B"' TIME/CM OR DELAY TIME, wired |
|  | 262-0596-01 | 5310 |  | 1 | SWITCH, "B" TIME/CM OR DELAY TIME, wired |
|  | - |  |  | , | Includes: |
|  | 260-0531-00 |  |  | 1 | SWITCH, unwired |
| 19 | 384.0287-00 |  |  | 1 | ROD, extension |
|  | 376-0014-00 |  |  | 1 | COUPLING, pot |
|  | 361-0233-00 | X12690 |  | 1 | RESTRAINT, shaft coupling |
|  | 361-0234.00 | X12690 |  | 1 | RESTRAINT, shaft coupling |
| 20 | 406-0898-00 |  |  | 1 | BRACKET, time/cm switch "B" |
|  | 210.0449-00 |  |  | 2 | Mounting Hardware NUT, hex, $5-40 \times 1 / 4$ inch |
|  | 210-0006-00 |  |  | 2 | LOCKWASHER, internal, \#6 |
|  | 348-0003-00 |  |  | 1 | GROMMET, $5 / 16$ inch (not shown) |
|  | - |  |  | - | Mounting Hardware For Capacitor: (not shown) |
|  | $210-0407-00$ $210-0006-00$ |  |  | 3 3 | NUT, hex, $6.32 \times 1 / 4$ inch |
|  | 210-0006-00 |  |  | 3 2 | LOCKWASHER, internal, \#6 WASHER, $6 L \times 3 / 8$ inch |
| 21 | -.... |  |  | - | Mounting Hardware For Pol: |
|  | 210-0413-00 |  |  | 2 | NUT, hex, $3 / 8.32 \times 1 / 2$ inch |
|  | 210-0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 6 \times 1 / 2$ inch |
|  | 210-0255-00 |  |  | 1 | LUG, solder |
| 22 | 352-0061-00 |  |  | 1 | HOLDER, component |
|  | 211000900 |  |  | $\stackrel{7}{2}$ | Mounting Hardware: (not included) |
|  | 211-0008-00 |  |  | 2 | SCREW, $4-40 \times 1 / 4$ inch BHS |
|  | 210-0004-00 |  |  | 2 | LOCKWASHER, internal, \#4 |
|  | 210-0406-00 |  |  | 2 | NUT, hex, $4.40 \times 3 / 16$ inch |
|  | 210-0413-00 |  |  | 1 | Mounting Hardware: (not included) NUT, hex, $3 / 6 \cdot 32 \times 1 / 2$ inch |
|  | 210-0013-00 |  |  |  | LOCKWASHER, internal, $3 / 8 \times 11 / 16$ inch |
|  | 212-0004-00 |  |  | 2 | SCREW, 8 -32 $\times 5 / 16$ inch BHS |
|  | 212-0023-00 |  |  | 1 | SCREW, $8.32 \times 3 / 8$ inch BHS |
|  | 210-0804-00 |  |  | 3 | WASHER, $85 \times 3 / 8$ inch |
|  | 211-0507-00 |  |  | 2 | SCREW, $6-32 \times 5 / 16$ inch BHS |
|  | 210-0803-00 |  |  | 2 | WASHER, 6L. $\times 3 / \mathrm{m}$ inch |
| 23 | 260-0199-00 |  |  | 1 | SWITCH, POWER ON, toggle |
|  | $210-0473-00$ |  |  | i | Mounting Hardware: (not included) NUT, switch, $15 / 32-32 \times 5 / 64$ inch |
|  | 210-0902-00 |  |  | 1 | WASHER, $470 \mathrm{ID} \times 21 / 32$ inch OD |
|  | 354-0055-00 |  |  | 1 | RING, locking switch |
|  | 210-0414-00 |  |  | 1 | NUT, hex, $15 / 32-32 \times 9 / 16$ inch |
| 25 | 352-0067-00 |  |  | 3 | HOLDER, neon, single |
|  | $\begin{aligned} & 211-0109-00 \\ & 210-0406-00 \end{aligned}$ |  |  | 1 | Mounting Hardware For Each: (not included) SCREW, $4-40 \times 7 / \mathrm{e}$ inch FHS NUT, hex, $4.40 \times 3 / 16$ inch |

EXPLODED VIEW (Cont'd)


EXPLODED VIEW (Cont'd)

| $\begin{array}{\|l\|} \hline \text { REF. } \\ \text { NO. } \end{array}$ | PART NO. | SERIAL/MODEL NO. |  | O | description |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC. |  |  |
| 32 | 262-0601-00 | $\begin{aligned} & 100 \\ & 4270 \end{aligned}$ | 4269 | 1 | SWITCH, HORIZONTAL DISPLAY, rear, wired <br> Includes: <br> SWITCH, unwired <br> SWITCH, unwired <br> BRACKET, switch mounting <br> Mounting Hardware: (not included) <br> NUT, hex, $3 / 8-32 \times 1 / 2$ inch <br> WASHER, 390 ID $\times 9 / 16$ inch OD <br> LOCKWASHER, internal, $3 / 8 \times 1 / 2$ inch <br> BRACKET, trimmer <br> Mounting Hardware: (not included) <br> NUT, hex, $4-40 \times 3 / 16$ inch <br> LOCKWASHER, internal, \# 4 <br> Mounting Hardware For Each Capacitor: <br> SCREW, thread forming, $4-40 \times 1 / 4$ inch PHS phillips <br> Mounting Hardware: (not included) <br> SCREW, $6-32 \times 5 / 16$ inch BHS <br> NUT, keps, $6-32 \times 5 / 16$ inch <br> KNOB, TRIGGERING LEVEL, large chorcoal Each Includes: <br> SCREW, set, $6-32 \times 3 / 16$ inch H\$S <br> Mounting Hardware For Each Por: NUT, hex, $3 / 8-32 \times 1 / 2$ inch LOCKWASHER, internal, $3 / 8 \times 11 / 16$ inch LUG, solder, $3 / 8$ inch <br> KNOB, SCALE ILLUM, small charcoal Inciudes: SCREW, set, $6.32 \times 3 / 16$ inch HSS <br> Mounting Hardware For Each Pot: NUT, hex, $3 / 8-32 \times 7 / 16$ inch WASHER, $390 \mathrm{ID} \times 9 / 16$ inch OD LOCKWASHER, internal, $3 / 6 \times 11 / 16$ inch <br> KNOB, ASTIGMATISM, small charcoal Includes: <br> SCREW, set, $6.32 \times 3 / 16$ inch HSS <br> KNOB, FOCUS, small charcoal Includes: SCREW, set, $6.32 \times 3 / 16$ inch HSS <br> KNOB, INTENSITY, small charcoal Includes: SCREW, set, $6.32 \times 3 / 16$ inch HSS <br> KNOB, " $A$ " TIME/CM, large charcoal Includes: <br> SCREW, set, $6.32 \times 3 / 16$ inch HSS |
|  | --...- |  |  |  |  |
|  | 260-0535-00 |  |  | 1 |  |
|  | 260-0796-00 |  |  | 1 |  |
|  | 406-0902-00 |  |  | 1 |  |
|  | - ... |  |  |  |  |
|  | 210-0413-00 |  |  | 1 |  |
|  | 210-0840-00 |  |  | 1 |  |
|  | 210.0012-00 |  |  | 1 |  |
| 34 | 406-0897-00 |  |  | 1 |  |
|  | - - . - |  |  |  |  |
|  | 210-0406-00 |  |  | 2 |  |
|  | 210-0004-00 |  |  | 2 |  |
| 35 | - .-. |  |  | - |  |
|  | 213-0088-00 |  |  | 2 |  |
|  | 211-0507-00 |  |  | 2 |  |
|  | 210.0457-00 |  |  | 2 |  |
| 36 | 366-0117-00 |  |  | 2 |  |
|  | … |  |  |  |  |
|  | 213-0004-00 |  |  | 1 |  |
|  | - . . - |  |  | - |  |
|  | 210-0413-00 |  |  | 1 |  |
|  | 210-0013-00 |  |  | 1 |  |
|  | 210.0207-00 |  |  | 1 |  |
| 37 | 366-0220-00 |  |  | 1 |  |
|  | … |  |  | ; |  |
|  | 213-0004-00 |  |  | 1 |  |
| 38 | $\cdots$ |  |  | - |  |
|  | 210-0590-00 |  |  | 1 |  |
|  | 210-0840-00 |  |  | 1 |  |
|  | 210-0013-00 |  |  | 1 |  |
| 39 | 366-0254-00 |  |  | 1 |  |
|  | … |  |  | - |  |
|  | 213-0004-00 |  |  | 1 |  |
| 40 | 366-0220-00 |  |  | 1 |  |
|  |  |  |  | - |  |
|  | 213-0004-00 |  |  | 1 |  |
| 41 | 366-0220-00 |  |  | 1 |  |
|  | … |  |  | - |  |
|  | 213-0004-00 |  |  | 1 |  |
| 42 | 366-0144-00 |  |  | 1 |  |
|  | $213-0004-00$ |  |  |  |  |
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EXPLODED VIEW (Cont'd)


EXPLODED VIEW (Cont'd)


EXPLODED VIEW (Cont'd)


EXPLODED VIEW (Cont'd)


EXPLODED VIEW (Cont'd)


EXPLODED VIEW (Cont'd)


6-12

EXPLODED VIEW (Cont'd)


EXPLODED VIEW (Cont'd)

| $\begin{array}{\|l\|l\|} \hline \text { REF. } \\ \text { no. } \end{array}$ | PART NO. | SERIAL/MODEL NO. |  | [a <br> $\mathbf{T}$ <br> $\mathbf{r}$ | description |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC. |  |  |
| 135 | 166-0319-00 |  |  | 2 | SLEEVE, high voltage |
| 136 | 337-0566-00 |  |  | 1 | SHIELD, high voltage |
|  | … |  |  |  | Mounting Hardware: (not included) |
|  | 211-0504-00 |  |  | 4 | SCREW, $6.32 \times 1 / 4$ inch BHS |
|  | 211.0541 .00 |  |  | 1 | SCREW, $6.32 \times 1 / 4$ inch FHS phillips |
| 137 | 210-0261-00 |  |  | 2 | LUG, solder, high voltage |
|  | - -... |  |  |  | Mounting Hardware: (not included) |
| 138 | 200-0475-00 |  |  | 1 | SCREW, $6-32 \times 1 / 32$ inch HHS |
|  | … ${ }^{\text {a }}$ |  |  |  | Mounting Hardware: (not included) |
| 139 | 211.0521-00 |  |  | 2 | SCREW, $6.32 \times 11 / 2$ inches RHS |
|  | 210.0801-00 |  |  | 2 | WASHER, $55 \times 9 / 32$ inch |
| 140 | 166-0357-00 |  |  | 1 | SLEEVE, high voltage anode lead |
| 141 | 392-0147-00 |  |  | 1 | BOARD, high voltage, with ceramic strips |
|  | -..- |  |  |  | Mounting Hardware: (not included) |
|  | 211-0507-00 |  |  | 1 | SCREW, $6.32 \times 5 / 16$ inch BHS |
| 142 | 210-0966-00 |  |  | 2 | WASHER, insulating, rubber, $7 / 1610 \times 7 / 6$ inch $O D$ |
| 143 | 384.0542-00 |  |  | 2 | ROD, capacitor mounting |
|  | 211-0507-00 |  |  | 1 | Mounting Hardware For Each: (not included) SCREW, $6.32 \times 5 / 16$ inch BHS |
| 144 | 385-0170-00 |  |  | 1 | ROD, spacer, nylon |
|  | $\cdots$ |  |  | , | Mounting Hardware: \{not included\} |
|  | 213-0041-00 |  |  | 1 | SCREW, thread cutting, $6.32 \times 3 / 6$ inch THS phillips |
| 145 | 337-0570-00 |  |  | 1 | SHIELD, horizontal preamplifier |
|  | 211-0504-00 |  |  | 2 | Mounting Hardware; (not included) SCREW, $6.32 \times 1 / 4$ inch BHS |
| 146 | 129-0072.00 |  |  | 1 | POST, diode tie-off |
|  | … |  |  | - | Includes: |
|  | 131-0309-00 |  |  | 1 | CONNECTOR, terminal |
|  | $\cdots$ |  |  |  | Mounting Hardware: (not included) |
|  | 361-0007-00 |  |  | 1 | SPACER, nylon, 063 inch |
| 147 | 136-0013-00 |  |  | 2 | SOCKET, STM8 |
|  | $\cdots$ |  |  | , | Mounting Hardware For Each: (not included) |
|  | 210-0407-00 |  |  | 2 | NUT, hex, $6-32 \times 1 / 4$ inch |
|  | 210-0006-00 |  |  | 2 | LOCKWASHER, internal, \#6 |
| 148 | 214.0435-00 |  |  | 2 | HEAT SINK, fransistor |
| 149 | ㄱ․… |  |  | 1 | Mounting Hardware For Each Miniature Pot: |
|  | $210.0471-00$ $210-0046-00$ |  |  | 1 | NUT, hex, $1 / 4-32 \times 5 / 16$ inch $\times 19 / 32$ inch <br> LOCKWASHER, internal, .261 inch ID $\times .400$ OD |
|  | 358-0054-00 |  |  | 1 | BUSHING, banana jack |
| 150 | 337-0588-00 |  |  | 1 | SHIELD, sweep generator |
|  | 211.0504-00 |  |  | 2 | Mounting Hardware: (not included) SCREW, $6.32 \times 1 / 4$ inch BHS |
| 151 | 136-0008-00 |  |  | 7 | SOCKET, STM7G |
|  | … |  |  |  | Mounting Hardware For Each: (not included) |
|  | 213-0044-00 |  |  | 2 | SCREW, thread culting, $5.32 \times 3 / 16$ inch PHS phillips |
| 152 | … |  |  | - | Mounting Hardware For Each Pot: |
|  | 210-0444-00 |  |  | 1 | NUT, hex, $3 / 8-32 \times 1 / 2$ inch |
|  | 210-0840-00 |  |  | 1 | WASHER, 390 ID $\times 9 / 16$ inch OD |
|  | 210-0012-00 |  |  | 1 | LOCKWASHER, internal, $3 / 0 \times 1 / 2$ inch |
|  | 210-0207-00 |  |  | 1 | LUG, solder, $3 / 8$ inch |
| 153 | 348-0031-00 |  |  | 14 | GROMMET, poly snap-in |
|  | 385-0134-00 |  |  | 3 | ROD, deltin |
|  | 213-0104-00 |  |  | 1 | Mounting Hardware For Each: (not included) SCREW, thread forming, $6.32 \times 3 / 8$ inch THS |
| 155 | 432-0047-00 |  |  | 1 | BASE, small capacitor mounting |
|  | $\cdots$ |  |  | - | Mounting Hardware: (not included) |
|  | $211-0588-00$ |  |  | 2 | SCREW, $6.32 \times 3 / 4$ inch HHS |
|  | 210-0006-00 |  |  | 2 | LOCKWASHER, internal, \#6 |
|  | 210.0407.00 |  |  | 2 | NUT, hex, $6.32 \times 1 / 4$ inch |
|  | 386-0253-00 |  |  | 1 | PLATE, metal, small capacitor |

EXPLODED VIEW (Coni'd)

| REF. <br> NO. | Part no. | SERIAL/MODEL NO. |  | O <br> $\mathbf{T}$ <br> $\mathbf{r}$ | description |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | Disc. |  |  |
| 156 | 384-0613-00 |  |  | 1 | ROD, anchor |
|  | ..... |  |  |  | Includes: |
| 157 | 134-0033-00 |  |  | 2 | PLUG, banana, male, push in type |
|  | 214.0370.00 |  |  | 1 | PIN, locating |
|  | $\cdots$ |  |  | , | Mounting Hardware: (not included) |
|  | 212-0004.00 |  |  | 2 | SCREW, $8-32 \times 5 / 16$ inch BHS |
|  | 210.0804-00 |  |  | 2 | WASHER, $85 \times 3 / 8$ inch |
| 159 | 337-0008-00 |  |  | 1 | SHIELD, tube |
| 160 | 376-0007-00 |  |  | 1 | COUPLING |
|  | 213-0005-00 |  |  | 2 | Includes: <br> SCREW, set, $8.32 \times 1 / \mathrm{e}$ inch HSS |
| 161 | 262-0602-00 |  |  | 1 | SWITCH, single sweep |
|  | $\cdots$ |  |  | - | Includes: |
|  | 260.0496-00 |  |  | 1 | SWITCH, unwired |
| 162 | 260-0516-00 |  |  | 1 | SWITCH, reset, push |
|  | $211.0034-00$ |  |  | 2 | Mounting Hardware: (not included) SCREW, $2.56 \times 1 / 2$ inch RHS |
|  | 210-0850-00 |  |  | 2 | WASHER, \#2 flat |
|  | 210-0001-00 |  |  | 2 | LOCKWASHER, internal, \#2 |
|  | 210-0405-00 |  |  | 2 | NUT, hex, $2.56 \times 3 / 16$ inch |
|  | 210-0586-00 |  |  | 2 | Mounting Hardware: (not included) NUT, keps, $4-40 \times 1 / 4$ inch |
| 163 | 343-0005-00 |  |  | 1 | CLAMP, cable, $1 / 16$ inch |
|  | … . - |  |  | - | Mounting Hardware: (not included) |
|  | 210-0457-00 |  |  | 1 | NUT, keps, $6.32 \times 5 / 16$ inch |
|  | 210-0863-00 |  |  | 1 | WASHER, "D" type, \#10 |
| 164 | 385-0170-00 |  |  | 1 | ROD, spacer, nylon |
|  | 213-0068-00 |  |  | 1 | Mounting Hardware: (not included) SCREW, thread culting, $6-32 \times 5 / 16$ inch FHS |
| 165 | 387-0756-00 | 100 | 4389 | 1 | PLATE, cabinet, bottom |
|  | 386-1093.00 | 4390 | 12799 | 1 | PLATE, cabinet, bottom |
|  | 386-1093-03 | 12800 |  | 1 | PLATE, cabinet, bottom |
|  | 214.0361-00 |  |  | 4 | Includes: <br> LATCH, quarter turn, assembly |
|  | 214-0361-00 |  |  | 4 | LATCH, quarter turn, assembly Each Consisting Of : |
|  | 214.0400-00 |  |  | 1 | PIN, securing, index |
|  | 358-0218-00 |  |  | 1 | BUSHING, latch bearing |
|  | 387-0871-00 |  |  | 1 | PLATE, latch index |
|  | 387-0804-00 |  |  | 1 | PLATE, latch locking |
|  | 214-0359-00 | 100 | 6929 | 1 | SPRING, latch |
|  | 220-0486-00 | 6930 |  | 1 | NUT, push-on |
| 166 | 122-0108-00 | 100 | 6729 | 2 | ANGLE, rail, bottom |
|  | 122-0108-02 | 6730 |  | 2 | ANGLE, rail, bottom |
|  | ㄱ.. |  |  | - | Mounting Hardware For Each: (not included) |
|  | 212-0039-00 |  |  | 4 | SCREW, $8-32 \times 3 / 6$ inch THS |
|  | 210.0458-00 |  |  | 4 | NUT, keps, $8-32 \times 11 / 32$ inch |
|  | 348-0052-00 | X2020 |  | 4 | FOOT, rubber (not shown) <br> Mounting Hardware: (not included) |
|  | 212-0071-00 | $\times 2020$ | 8149 | 2 | Mounting Hardware: (not included) SCREW, $8-32 \times 1$ inch, Fil HS |
|  | 212-0090-00 | 8150 |  | 2 | SCREW, $8.32 \times 0.875$ inch, Fil HS |
| 167 | 387-0759-00 |  |  | 1 | PLATE, vertical bulkhead |
|  | - . . - |  |  | - | Mounting Hardware: (not included) |
|  | 212.0040-00 |  |  | 4 | SCREW, $8.32 \times 3 / 8$ inch THS |
|  | 210-0458-00 |  |  | 4 | NUT, keps, $8-32 \times 11 / 32$ inch |
|  | 212-0001-00 |  |  | 3 | SCREW, $8-32 \times 1 / 4$ inch BHS |
|  | 212-0004-00 |  |  | 2 | SCREW, $8.32 \times 5 / 14$ inch BHS |
| 168 | 441-0478-00 |  |  | 1 | CHASSIS, power |
|  | 212-0040-00 |  |  | 5 | Mounting Hardware: (not included) SCREW, $8-32 \times 3 / 8$ inch THS |
|  | 210.0458-00 |  |  | 5 | NUT, keps, $8.32 \times 11 / 32$ inch |
|  | 212-0001-00 |  |  | 7 | SCREW, $8.32 \times 1 / 4$ inch BHS |

EXPLODED VIEW (Cont'd)

| REF. <br> No. | part no. | SERIAL/MODEL NO. |  | aT$\mathbf{r}$. | description |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC. |  |  |
| 169 | 210-0804-00 |  |  | 7 | WASHER, $85 \times 3 / 8$ inch |
|  | 337-0574-00 |  |  | 1 | SHIELD, upper calibrator switch |
|  | ㄱ․ |  |  |  | Mounting Hardware: (not included) |
|  | 211-0504-00 |  |  | 1 | SCREW, $6.32 \times 1 / 4$ inch BHS |
|  | 210-0803-00 |  |  | 1 | WASHER, $6 \mathrm{~L} \times 3 / 8$ inch |
|  | 210-0457-00 |  |  | 1 | NUT, keps, $6.32 \times 5 / 16$ inch |
| 170 | 136-0022-00 |  |  | 1 | SOCKET, STM9, shielded |
|  | ㄱ․ |  |  |  | Mounting Hardware: (not included) |
|  | 213-0044-00 |  |  | 2 | SCREW, thread cutting, $5.32 \times 3 / 16$ inch PHS |
| 171 | $\cdots$ |  |  |  | Mounting Hardware For Thermal Cutout: |
|  | 213-0044-00 |  |  | 2 | SCREW, thread cutting, $5.32 \times 3 / 16$ inch PHS BRACKEE, |
| 172 | 406-0023-00 |  |  | $\stackrel{\square}{2}$ | BRACKET, pot <br> Mounting Hardware For Each: (not included) |
|  | 211-0507-00 |  |  | 2 | SCREW, $6.32 \times 5 / 16$ inch BHS |
|  | 210.0006-00 |  |  | 2 | LOCKWASHER, internal, \#6 |
|  | 210-0407-00 |  |  | 2 | NUT, hex, $3 / 8-32 \times 1 / 2 \times 5 / 8$ inch long |
| 173 | … |  |  | - | Mounting Hardware For Pot: |
|  | 210.0444.00 |  |  | 1 | NUT, hex, $183-32 \times 1 / 2 \times 5 / 8$ inch |
|  | 210-0840-00 |  |  | 1 | WASHER, 390 ID $\times \frac{1}{16}$ inch OD |
|  | 210.0012.00 |  |  | 1 | LOCKWASHER, internal, $3 / 8 \times 1 / 2$ inch |
| 174 | 348.0003.00 |  |  | 5 | GROMMET, $5 / 18$ inch |
| 175 | 210.0259-00 |  |  | 1 | LUG, solder, \#2 |
|  | 213-0055-00 |  |  | $i$ | Mounting Hardware: (nol included) SCREW, thread culting, $2.32 \times 3 / 16$ inch PHS |
| 176 | 441-0474-00 | 100 | 12479 | 1 | CHASSIS, delayed sweep |
|  | 441-0474.01 | 12480 |  | 1 | CHASSIS, delayed sweep |
|  | … |  |  |  | Includes: |
| 177 | 213-0172-00 |  |  | 2 | THUMBSCREW, $6.32 \times 0.812$ inch |
|  | 354.0311.00 | 100 | 7529x | 2 | RING, rubber, 0.078 inch ID |
| 178 | 131.0269-00 |  |  | 2 | CONNECTOR, receptacle |
| 179 | 358.0214.00 |  |  | 2 | BUSHING, insulator |
|  | $212.0008-00$ |  |  | 3 | Mounting Hardware: (not included) SCREW, $8.32 \times 1 / 2$ inch BHS |
| 180 | 210-0255-00 |  |  | 1 | LUG, solder, pot |
|  | 381.0215-00 |  |  | 1 | BAR, stop |
|  | … |  |  | - | Mounting Hardware: (not included) |
|  | 212.0008.00 |  |  | 1 | SCREW, $8-32 \times 1 / 2$ inch BHS |
| 182 | 387-0762-00 | 100 | 12799 | 1 | PLATE, cabinet, right side |
|  | 387-0762-04 | 12800 |  | 1 | PLATE, cobinet, right side |
|  | - |  |  | 2 | Includes: |
|  | 214-0361-00 |  |  | 2 | LATCH, quarter turn, assembly |
|  | 214.0400-00 |  |  | 1 | Each Consisting Of: PIN, securing, index |
|  | 358-0218-00 |  |  | 1 | BUSHING, latch bearing |
|  | 387.0871-00 |  |  | 1 | PLATE, latch index |
|  | 387-0804.00 |  |  | 1 | PLATE, latch locking |
|  | 214-0359-00 | 100 | 6929 | 1 | SPRING, latch |
|  | 220.0486-00 | 6930 |  | 1 | NUT, push-on |
| 183 | 384.0614-00 |  |  | 1 | ROD, chassis hinge |
|  | … |  |  | - | MountingHardware: (not included) |
| 184 | 361.0052.00 | 100 | 174 | 1 | SPACER, hinge pin |
|  | 358-0237-00 | 175 |  | 1 | BUSHING, hinge rod |
|  | 212-0010-00 |  |  | 1 | SCREW, $8.32 \times 5 / \mathrm{mch}$ BHS |
| 185 | 358-0042-00 | 100 | 174 | 1 | BUSHING, nylon |
|  | 361-0052-00 | 175 |  | 1 | SPACER, hinge pin |
| 186 | 343-0003-00 |  |  | 1 | CLAMP, cable, $1 / 4$ inch |
|  | ㄱ․ |  |  | 1 | Mounting Hardware: (not included) |
|  | 212-0008-00 |  |  | 1 | SCREW, $8-32 \times 5 / 8$ inch BHS |
|  | 210.0863-00 |  |  | 1 | WASHER, "D" rype, \#10 |
| 187 | $\begin{aligned} & 406-0928-00 \\ & 406-0928-02 \end{aligned}$ | $\begin{aligned} & 100 \\ & 6730 \end{aligned}$ | 6729 | 1 | BRACKET, transformer BRACKET, transformer |

EXPLODED VIEW (Cont'd)

| REF. <br> No. | PARt no. | SERIAL/MODEL NO. |  | T | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC. | r. | description |
| 188 | . . - | 10067301006730 | 67296729 |  | Mounting Hardware: (not included) |
|  | 210.0564-00 |  |  | 2 | NUT, hex, $10.32 \times 3 / 8$ inch |
|  | 210.0010.00 |  |  | 2 | LOCKWASHER, internal, \# 10 |
|  | 381-0221-00 |  |  | 2 | BAR, transformer support |
|  | … .- |  |  | - | Mounting Hardware For Each: (not included) |
|  | 212-0033-00 |  |  | 2 | SCREW, $8.32 \times 3 / 4$ inch BHS |
|  | 210.0458-00 |  |  | 2 | NUT, keps, $8.32 \times 11 / 32$ inch |
|  | 212-0509.00 |  |  | 1 | SCREW, $10.32 \times 5 / 8$ inch BHS |
|  | 212-0559-00 |  |  | 1 | SCREW, $10-32 \times 5 / 8$ inch, $100^{\circ}$ csk, FHS |
|  | 212.0534.00 |  |  | 1 | SCREW, $10.32 \times 1$ inch BHS |
|  | 210-0010-00 |  |  | 2 | LOCKWASHER, internal, \#10 |
|  | 210-0010-00 |  |  | 1 | LOCKWASHER, internal, \#10 |
| $\begin{aligned} & 189 \\ & 190 \end{aligned}$ | 348-0012.00 |  |  | 1 | GROMMET, $5 / 8$ inch |
|  | … |  |  | - | Mounting Hardware For Transformer: |
| $\begin{aligned} & 191 \\ & 192 \end{aligned}$ | $212.0524-00$ |  |  | 4 | SCREW, $10.32 \times 31 / 4$ inches HHS |
|  | 210.0812.00 |  |  | 4 | WASHER, fiber, \#10 |
|  | 210.0010 .00 |  |  | 4 | LOCKWASHER, internal, \#10 |
|  | 210-0564.00 |  |  | 2 | NUT, hex, $10.32 \times 3 / 8$ inch |
|  | 384.0612.00 |  |  | 2 | ROD, transformer standoff |
|  | 202-0102-00 |  |  | 1 | CAN, relay cover |
| 193 | 210.0457-00 |  |  | 2 | Mounting Hardware: ( $n$ ( included) NUT, keps, $6.32 \times 3 / 16$ inch |
|  | 426-0193-00 |  |  | 1 | MOUNT, fan motor |
| 194 | 212-0039-00 |  |  | 4 | Mounting Hardware: (not included) SCREW, $8.32 \times 3 / 8$ inch THS |
|  | 147-0026-00 |  |  | 1 | MOTOR, fan |
| 195 | $\cdots$ |  |  | - | Mounting Hardware: (not included) |
|  | 214.0210 .00 |  |  | 1 | NUT, keps, $8-32 \times 1 / 32$ inch |
|  | ...... |  |  | , | Includes: |
| 196 | 214-0209-00 |  |  | 1 | SPOOL, solder |
|  | $\cdots$ |  |  | , | Mounting Hardware: (not included) |
|  | 361-0007-00 |  |  | 1 | SPACER, nylon, 063 inch |
|  | 369.0007-00 |  |  | 1 | FAN, 7 inch |
| 197 | 200-0260.00 |  |  | 1 | COVER, large capacitor |
| $\begin{aligned} & 198 \\ & 199 \end{aligned}$ | 200.0259.00 |  |  | 1 | COVER, large capacitor |
|  | 432-0048-00 |  |  | 2 | BASE, large capacitor mounting |
| 200 |  |  |  | 2 | Mounting Hardware For Each: (not included) SCREW $6.32 \times 3 /$ |
|  | 210.0006.00 |  |  | 2 | LOCKWASHER, internal, \#6 |
|  | 210.0407-00 |  |  | 2 | NUT, hex, $6.32 \times 1 / 4$ inch |
|  | 386-0254-00 |  |  | 2 | PLATE, fiber, large capacitor |
|  | 387-0758-00 | 100 | 7979 | 1 | PLATE, rear subpanel |
|  | 387-0758-02 | 7980 |  | 1 | PLATE, rear subpanel |
| 201 | $\cdots$ |  |  | - | Includes: |
|  | 354-0056-00 |  |  | 1 | RING, ornamental |
|  | 387-0766-00 | 100 | 7979 | 1 | PLATE, rear overlay |
|  | 387-0766-01 | 7980 |  | 1 | PLATE, rear overloy |
| 202 | … |  |  | - | Mounting Hardware: (not included) |
|  | 213-0104-00 $334-0904-00$ |  |  | 4 1 | SCREW, thread forming, $6.32 \times 3 / 8$ inch PHS |
|  | 334-0904-00 | 100 |  | 1 | TAG, voltage rating <br> Mounting Hardware: (not included) |
| 203 | 213-0088-00 | 100 | 7979X | 2 | SCREW, thread forming, $4-40 \times 1 / 4$ inch PHS |
|  | … |  |  | - | Mounting Hardware For 20 Watt Resistor |
| 204 | 212-0037-00 |  |  | 1 | SCREW, $8-32 \times 13 / 4$ inches Fil HS |
|  | 210.0808-00 |  |  | 1 | WASHER, resistor centering |
|  | 210-0462-00 |  |  | 1 | NUT, hex, resistor mounting |
|  | 212.0004-00 |  |  | 1 | SCREW, $8-32 \times 5 / 16$ inch BHS |
|  | 352-0002-00 | 100 | 7979X | 1 | HOLDER, fuse, assembly |
|  | $352-0010-00$ |  |  | 1 | Consisting Of: <br> HOLDER, fuse |

EXPLODED VIEW (Cont'd)


EXPLODED VIEW (Cont'd)

| ReF. <br> NO. | PART No. | SERIAL/MODEL NO. |  | a <br> $\mathbf{T}$ <br> $\mathbf{r}$ | description |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | Disc. |  |  |
| 209 | 122-0019-00 |  |  | 1 | ANGLE, frame, top right |
|  | $\cdots$ |  |  |  | Mounting Hardware: (not included) |
|  | 211-0559-00 |  |  | 4 | SCREW, $6.32 \times 3 / 8$ inch FHS |
|  | 210.0457-00 |  |  | 4 | NUT, keps, $6-32 \times 5 / 16$ inch |
| 210 | 380-0018-00 |  |  | 1 | HOUSING, air filter |
|  | … - - |  |  | - | Mounting Hardware: (not included) |
|  | 212-0031-00 |  |  | 2 | SCREW, $8.32 \times 11 / 4$ inches RHS |
|  | 210.0458.00 |  |  | 2 | NUT, keps, $8-32 \times 11 / 32$ inch |
|  | 210-0402-00 |  |  | 2 | NUT, cap, hex, 8 -32 $\times 5 / 16$ inch |
| 211 | 131-0206-00 |  |  | 1 | CONNECTOR, receptacle |
|  | ㄱ..- |  |  | ; | Mounting Hardware: (not included) |
|  | 210-0559.00 |  |  | 1 | NUT, hex, $7 / 16-28 \times 9 / 16$ inch |
|  | 210-0021-00 |  |  | 1 | LOCKWASHER, internal |
| 212 | 210.0260-00 |  |  | 1 | LUG, solder |
|  | 260.0209.00 |  |  | 1 | SWITCH, CRT CATHODE SELECTOR, toggle |
|  | 210-0473-00 |  |  | 1 | NUT, switch, $15 / 32 \cdot 32 \times 3 / 44$ inch |
|  | 210-0902-00 |  |  | 1 | WASHER, $4701 \mathrm{ID} \times 21 / 32$ inch OD |
|  | 210-0414.00 |  |  | 1 | NUT, hex, $15 / 32-32 \times 9 / 16$ inch |
| 214 | 387.0853-00 |  |  | 1 | PLATE, binding post mounting |
|  | 129.0064.00 |  |  | 1 | POST, binding |
|  | 210.0457.00 |  |  | $i$ | Mounting Hardware: (not included) NUT, keps, $6.32 \times 5 / 16$ inch |
| 215 | 346-0027-00 |  |  | 1 | STRAP, ground |
| 216 | 381-0217-00 |  |  | 1 | BAR, top support, with handle |
|  | … - |  |  | , | Includes: |
| 217 | 344-0098-00 |  |  | 4 | CLIP, handle |
|  | 212.0566 .00 | 100 | 4419 | 4 | SCREW, $10.32 \times 5 / 16$ inch RHS |
|  | 212.0507.00 | 4420 |  | 4 | SCREW, $10-32 \times 3 / 8$ inch PHS |
|  | 210.0010-00 | X4420 |  | 4 | LOCKWASHER, internal, \#10 |
| 218 | 367-0037-00 |  |  | 2 | HANDLE |
|  | $\cdots$ |  |  |  | Mounting Hardware: (nol included) |
| 219 | $\begin{aligned} & 381-0073-00 \\ & 212-0039-00 \end{aligned}$ |  |  | 2 | BAR, retaining <br> SCREW, $8.32 \times 3 / 8$ inch THS |
| 220 | … ${ }^{\text {a }}$ |  |  | - | Mounting Hardware For Relay: |
|  | 211-0503.00 |  |  | 2 | SCREW, $6.32 \times 3 / 16$ inch BHS |
| 221 | 441.0473-00 | 100 | 2339 | 1 | CHASSIS, vertical amplifier |
|  | 441.0473-01 | 2340 |  | 1 | CHASSIS, vertical amplifier |
|  | … |  |  | - | Mounting Hardware: (not included) |
|  | 212-0004.00 |  |  | 3 | SCREW, $8-32 \times 5 / 16$ inch BHS |
|  | 210.0804 .00 |  |  | 3 | WASHER, $85 \times 3 / 8$ inch |
|  | 212-0040.00 |  |  | 1 | SCREW, $8.32 \times 5 / 16$ inch PHS |
|  | 210.0458.00 |  |  | 1 | NUT, keps, $8.32 \times 11 / 32$ inch |
| 222 | 337-0589-00 |  |  | 1 | SHIELD, sweep amplifier |
|  | 211.0504-00 |  |  | 2 | Mounting Hardware: (not included) |
| 223 | 366-0220-00 |  |  | 1 | KNOB, TRACE SEPARATION, small charcoal |
|  | … ${ }^{\text {a }}$ |  |  | - | Includes: |
|  | 213.0004.00 |  |  | 1 | SCREW, set, $6.32 \times 3 / 16$ inch HSS |
| $\left\|\begin{array}{l} 224 \\ 225 \end{array}\right\|$ | 348-0063-00 |  |  | 1 | GROMMET, plastic, $1 / 2$ inch |
|  | . . . . . | X2340 |  | 1 | TRANSISTOR |
|  | … ${ }^{\text {a }}$ |  |  | - | Mounting hardware: (not included w/transistor) |
|  | 386-0143.00 |  |  | 1 | PLATE, mica insulator |
|  | 211-0510.00 |  |  | ? | SCREW, $6.32 \times 3 / 8$ inch, PHS |
|  | 210.0983.00 | 2340 | 4419 | 2 | WASHER, shoulder |
|  | 210.0935.00 | 4420 |  | 2 | WASHER, fiber, $0.140 \mathrm{ID} \times 0.375$ inch OD |
|  | 210.0802 .00 |  |  | 2 | WASHER, $65 \times 5 / 16$ inch |
|  | 210.0006 .00 | 2340 | 3269x | 1 | LOCKWASHER, internal, \#6 |
|  | 210.0202 .00 |  |  | 1 | LUG, solder, SE 6 |
|  | 210-0407-00 | 2340 | 3269 | 2 | NUT, hex, $6.32 \times 1 / 4$ inch |
|  | 210-0457-00 | 3270 |  | 2 | NUT, keps, $6.32 \times 5 / 16$ inch |



CABLE HARNESS AND CERAMIC STRIP DETAIL

| REF. <br> NO. | PART NO. | SERIAL/MODEL NO. |  | [¢ <br> $\mathbf{r}$ <br> $\mathbf{r}$ | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC. |  |  |
| 1 | 179.0771.00 | 100 | 7979 | 1 | CABLE HARNESS, inter-connecting |
|  | 179.0771.01 | 7980 |  | 1 | CABLE HARNESS, inter-connecting |
| 2 | 179.0761-00 | 100 | 7979 | 1 | CABLE HARNESS, power |
|  | 179.0761.01 | 7980 |  | 1 | CABLE HARNESS, power |
| 3 | 179.0765-00 | 100 | 7979 | 1 | CABLE HARNESS, 110 volt |
|  | 179.0765.01 | 7980 |  | 1 | CABLE HARNESS, 110 volt |
| 4 | 179.0764.00 | 100 | 7329 | 1 | CABLE HARNESS, 150 volt adjustment |
|  | 179.0764-01 | 7330 |  | 1 | CABLE HARNESS, 150 volt adjustment |
| 5 | 124.0089.00 |  |  | 5 | STRIP, ceramic, $3 / 4$ inch $\times 7$ notches |
|  | $\cdots$ |  |  |  | Each Includes: |
|  | 355-0046-00 |  |  | 2 | STUD, nylon |
|  | 361.0009-00 |  |  | 2 | Mounting Hardware For Each: (not included) |
| 6 | 124.0091.00 |  |  | 6 | SPACER, nylon, 313 inch |
|  | . . . . . |  |  | . | Each Includes: |
|  | 355-0046-00 |  |  | 2 | STUD, nylon |
|  | $\cdots$ |  |  |  | Mounting Hardware For Each: (not included) |
|  | 361.0009-00 |  |  | 2 | SPACER, nylon, .313 inch |
| 7 | 124.0090-00 |  |  | 8 | STRIP, ceramic, $3 / 4$ inch $\times 9$ notches |
|  | 3550046 |  |  | , | Each Includes: |
|  | 355-0046-00 |  |  | 2 | STUD, nylon |
|  | ㄱ․ . |  |  | - | Mounting Hardware For Each: (not included) |
|  | 361.0009-00 |  |  | 2 | SPACER, nylon, 313 inch |
| 8 | -.... |  |  | . | Each Includes: |
|  | 355-0046-00 |  |  | 2 | STUD, nylon |
|  | $\cdots$ |  |  |  | Mounting Hardware For Each: (not included) |
|  | 361-0009.00 |  |  | 2 | SPACER, nylon, 313 inch |
| 9 | 179.0762.00 |  |  | 1 | CABLE HARNESS, "A" sweep |
| 10 | 124-0094-00 |  |  | 1 | STRIP, ceramic, $7 / 16$ inch $\times 7$ notches |
|  | $\cdots$ |  |  | - | Includes: |
|  | 355-0046-00 |  |  | 2 | STUD, nylon |
|  | $\cdots 36$ |  |  | 2 | Mounting Hardware For Each: (not included) |
| 11 | 124-0095-00 |  |  | 2 | STRIP, ceramic, $1 / 16$ inch $\times 9$ notches |
|  | .-... |  |  | . | Each Includes: |
|  | 355.0046-00 |  |  | 2 | STUD, nylon |
|  | $\cdots$ |  |  | , | Mounting Hardware For Each: (not included) |
|  | $361-0009.00$ $124.0155-00$ |  |  | ${ }_{15}^{2}$ | SPACER, nylon, 313 inch |
| 12 | 124.0155-00 |  |  | 15 | STRIP, ceramic, $7 / 16$ inch $\times 16$ notches |
|  | 355-0082-00 |  |  | 2 | Each includes: STUD, nylon |
|  | $\cdots$ |  |  |  | Mounting Hardware For Each: (not included) |
|  | 361-0039-00 |  |  | 2 | SPACER, nylon, $11 / 32$ inch |
| 13 | 124-0157-00 |  |  | 8 | STRIP, ceramic, $7 / 16$ inch $\times 3$ notches |
|  | -355-. |  |  | - | Each Includes: |
|  | 355-0082-00 |  |  | 2 |  |
|  | $\cdots$ |  |  | 2 | Mounting Hardware For Each: (not included) |
| 14 | 124.0154-00 |  |  | 25 | STRIP, ceramic, ${ }^{\text {d }} / 16$ inch $\times 20$ notches |
|  | ...... |  |  | 5 | Each Includes: |
|  | 355-0082-00 |  |  | 2 | STUD, nylon |
|  | … |  |  | - | Mounting Hardware For Each: (not included) |
|  | 361-0039-00 |  |  | 2 | SPACER, nylon, $11 / 32$ inch |
| 151617 | 179.0769-00 |  |  | 1 | CABLE HARNESS, focus and intensity |
|  | 179.0767.00 |  |  | 1 | CABLE HARNESS, high voltage |
|  | 124.0120-00 |  |  | 1 | STRIP, ceramic, $7 / 16$ inch $\times 4$ notches |
|  | $355-0046 \cdot 00$ |  |  | 2 | Includes: <br> STUD, nylon |
|  | … |  |  | - | Mounting Hardware For Each: (not included) |
|  | 361-0008-00 |  |  | 2 | SPACER, nylon, 188 inch |

CABLE HARNESS AND CERAMIC STRIP DETAIL (Cont'd)



## NOTES

Values are fixed unless marked Variable.

| Ckt. No. | Tektronix Part No. |  | Description | S/N |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Bulbs |  |
| 889 | 150-030 | Neon, NE-2V |  | READY |
| B90W | 150-030 | Neon, NE-2V |  | UNCALIBRATED |
| B94 | 150-027 | Neon, NE-23 |  |  |
| 8289 | 150.030 | Neon, NE-2V |  | READY |
| B290W | 150.030 | Neon, NE-2V |  | UNCALIBRATED |
| B294 | 150.027 | Neon, NE-23 |  |  |
| B550 | 150-030 | Neon, NE-2V |  | MAG ON |
| 8579 | 150-037 | Neon, ST2-27S |  |  |
| B583 | 150-027 | Neon, NE-23 |  |  |
| B589 | 150-037 | Neon, ST2-27S |  |  |
| 8602 | 150.001 | Incandescent, \#47 | Pilot Light |  |
| B603 | 150.031 | Incandescent, \#44 | Graticule Light |  |
| B604 | 150-031 | Incandescent, \#44 | Graticule Light |  |
| B1184 | 150.030 | Neon, NE-2V |  |  |
| B1194 | 150.030 | Neon, NE-2V |  |  |
|  |  |  | Capacitors |  |



Capacitors (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Description |  |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C90E C90F C90G $\mathrm{C9OH}$ C90」 | *295-073 | $\begin{aligned} & 0.001 \mu f \\ & 0.01 \mu f \\ & 0.1 \mu f \\ & 1 \mu f \\ & 10 \mu f \end{aligned}$ |  | Timing Series |  |  | 100-5309 |
| C90E C90F C90G $\mathrm{C9OH}$ C90J | *295-0104-00 | $\begin{aligned} & 0.001 \mu f \\ & 0.01 \mu f \\ & 0.1 \mu f \\ & 1 \mu f \\ & 10 \mu f \end{aligned}$ |  | Timing Series |  |  | 5310-up |
| $\begin{aligned} & \mathrm{C9OK} \\ & \mathrm{C92} \\ & \mathrm{C94} \\ & \mathrm{C96} \\ & \mathrm{C98} \end{aligned}$ | $\begin{array}{r} 281.524 \\ 283.001 \\ 281-578 \\ 283.006 \\ \text { Use } 281.604 \end{array}$ | $\begin{aligned} & 150 \mathrm{pf} \\ & 0.005 \mu \mathrm{f} \\ & 18 \mathrm{pf} \\ & 0.02 \mu \mathrm{f} \\ & 2.2 \mathrm{pf} \end{aligned}$ | Cer <br> Cer <br> Cer <br> Cer <br> Cer |  | $\begin{aligned} & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 600 \mathrm{v} \\ & 500 \mathrm{v} \end{aligned}$ | $\begin{aligned} & 5 \% \\ & \pm 0.25 \mathrm{pf} \end{aligned}$ |  |
| $\begin{aligned} & \mathrm{C} 99 \\ & \mathrm{ClO1} \\ & \mathrm{ClO3} \\ & \mathrm{Cl} 28 \\ & \mathrm{Cl} 30 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 281.007 \\ & 281.523 \\ & 283-000 \\ & 281.550 \\ & 281.550 \end{aligned}$ | $\begin{aligned} & 3.12 \mathrm{pf} \\ & 100 \mathrm{pf} \\ & 0.001 \mu \mathrm{\mu f} \\ & 120 \mathrm{pf} \\ & 120 \mathrm{pf} \end{aligned}$ | Cer <br> Cer <br> Cer <br> Cer <br> Cer | Var | $\begin{aligned} & 350 v \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \end{aligned}$ | $\begin{aligned} & 10 \% \\ & 10 \% \end{aligned}$ |  |
| $\begin{aligned} & \mathrm{Cl30B} \\ & \mathrm{Cl} 30 \mathrm{C} \\ & \mathrm{Cl} 30 \mathrm{D} \\ & \mathrm{Cl} 30 \mathrm{E} \\ & \mathrm{Cl} 37 \end{aligned}$ | $\begin{aligned} & 285-543 \\ & 285-636 \\ & 285-633 \\ & 285-576 \\ & 281-523 \end{aligned}$ | $\begin{aligned} & 0.0022 \mu f \\ & 0.022 \mu \mathrm{f} \\ & 0.22 \mu \mathrm{f} \\ & 1 \mu \mathrm{f} \\ & 100 \mathrm{pf} \end{aligned}$ | $\begin{aligned} & \text { MT } \\ & \text { PTM } \\ & \text { PTM } \\ & \text { PTM } \\ & \text { Cer } \end{aligned}$ |  | $\begin{aligned} & 400 \mathrm{v} \\ & 200 \mathrm{v} \\ & 100 \mathrm{v} \\ & 100 \mathrm{v} \\ & 350 \mathrm{v} \end{aligned}$ | $\begin{aligned} & 10 \% \\ & 10 \% \end{aligned}$ |  |
| $\begin{aligned} & \mathrm{C} 144 \\ & \mathrm{C} 146 \\ & \mathrm{C} 166 \\ & \mathrm{C} 170 \\ & \mathrm{C} 175 \end{aligned}$ | $\begin{aligned} & 283-002 \\ & 281.512 \\ & 281.543 \\ & 281 .-605 \\ & 281.512 \end{aligned}$ | $\begin{aligned} & 0.01 \mu f \\ & 27 \mathrm{pf} \\ & 270 \mathrm{pf} \\ & 200 \mathrm{pf} \\ & 27 \mathrm{pf} \end{aligned}$ | Cer <br> Cer <br> Cer <br> Cer <br> Cer |  | $\begin{aligned} & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \end{aligned}$ | $\begin{aligned} & 10 \% \\ & 10 \% \\ & 10 \% \end{aligned}$ |  |
| C178 <br> C186 <br> C188 <br> C192 <br> C197 | $\begin{aligned} & 281-558 \\ & 281.012 \\ & 283-002 \\ & 283-006 \\ & 283-006 \end{aligned}$ | 18 pf $7-45 \mathrm{pf}$ $0.01 \mu$ $0.02 \mu \mathrm{f}$ $0.02 \mu \mathrm{f}$ | $\begin{aligned} & \text { Cer } \\ & \text { Cer } \\ & \text { Cer } \\ & \text { Cer } \\ & \text { Cer } \end{aligned}$ | Var | $\begin{aligned} & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 600 \mathrm{v} \\ & 600 \mathrm{v} \end{aligned}$ |  |  |
| C199 <br> C201 <br> C202 <br> C204 <br> C205 | $\begin{aligned} & 281-511 \\ & 2833-001 \\ & 281-523 \\ & 283-002 \\ & 283-000 \end{aligned}$ | 22 pf $0.005 \mu \mathrm{f}$ 100 pf $0.01 \mu \mathrm{f}$ $0.001 \mu \mathrm{f}$ | $\begin{aligned} & \text { Cer } \\ & \text { Cer } \\ & \text { Cer } \\ & \text { Cer } \\ & \text { Cer } \end{aligned}$ |  | $\begin{aligned} & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 350 \mathrm{v} \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \end{aligned}$ | 10\% |  |
| $\begin{aligned} & \mathrm{C} 206 \\ & \mathrm{C} 211 \\ & \mathrm{C} 212 \\ & \mathrm{C} 218 \\ & \mathrm{C} 241 \end{aligned}$ | $\begin{aligned} & 281-512 \\ & 283-001 \\ & 281-523 \\ & 283-000 \\ & 281-523 \end{aligned}$ | $\begin{aligned} & 27 \mathrm{pf} \\ & 0.005 \mu \mathrm{f} \\ & 100 \mathrm{pf} \\ & 0.001 \mu \mathrm{f} \\ & 100 \mathrm{pf} \end{aligned}$ | Cer <br> Cer <br> Cor <br> Cer <br> Cor |  | $\begin{aligned} & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 350 \mathrm{v} \\ & 500 \mathrm{v} \\ & 350 \mathrm{v} \end{aligned}$ | 10\% | 100-6739x |
| $\begin{aligned} & \mathrm{C} 243 \\ & \mathrm{C} 249 \\ & \mathrm{C} 253 \\ & \mathrm{C} 256 \\ & \mathrm{C} 256 \\ & \mathrm{C} 257 \end{aligned}$ | $\begin{aligned} & 281-525 \\ & 283-006 \\ & 283-000 \\ & 281-576 \\ & 281-0578-00 \\ & 281-0578-00 \end{aligned}$ | $\begin{aligned} & 470 \mathrm{pf} \\ & 0.02 \mu \mathrm{f} \\ & 0.001 \mu \mathrm{f} \\ & 11 \mathrm{pf} \\ & 18 \mathrm{pf} \\ & 18 \mathrm{pf} \end{aligned}$ | Cer Cer Cer Cer Cer Cer |  | $\begin{aligned} & 500 \mathrm{v} \\ & 600 \mathrm{v} \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \\ & 500 \mathrm{v} \end{aligned}$ | $\begin{aligned} & 5 \% \\ & 5 \% \\ & 5 \% \end{aligned}$ | $\begin{array}{r} 100-6739 \mathrm{X} \\ \\ 100-6739 \\ 6740 \cdot \mathrm{up} \\ \times 6740-\mathrm{up} \end{array}$ |

Capacitors (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Descrip |  |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C265 | 283-000 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C267 | 283.026 | $0.2 \mu{ }^{\prime \prime}$ | Cer |  | 25 v |  | 100.15049 |
| C267 | 285.0835-00 | $0.22 \mu \mathrm{f}$ | Plastic |  | 100 v | 2\% | 15050-up |
| C276 | 290-187 | 4.7 ¢ f | EMT |  | 35 v |  | 100.6739 |
| C276 | 290-0175-00 | $10 \mu \mathrm{f}$ | EMT |  | 35 v |  | 6740-up |
| C278 | 283-003 | $0.01 \mu \mathrm{f}$ | Cer |  | 150 v |  |  |
| C283 | 281.524 | 150 pf | Cer |  | 500 v |  |  |
| C290A | 281.007 | 3-12 pf | Cer | Var |  |  |  |
| C290B | 281.007 | 3.12 pf | Cer | Var |  |  |  |
| C290C | 281.010 | 4.5-25 pf | Cer | Var |  |  |  |
| C290D | 281-574 | 82 pf | Cer |  | 500 v | 10\% |  |
| C290E |  | $0.001 \mu \mathrm{f}$ |  |  |  |  |  |
| C290F |  | $0.01 \mu \mathrm{f}$ |  |  |  |  |  |
| C290G | *295-073 | $0.1 \mu \mathrm{f}$ |  | Timing Series |  |  | 100-5309 |
| C290H |  | $1 \mu \mathrm{f}$ |  |  |  |  |  |
| C290J |  | $10 \mu \mathrm{f}$ |  |  |  |  |  |
| C290E |  | $0.001 \mu f$ |  |  |  |  |  |
| C290F |  | $0.01 \mu \mathrm{f}$ |  |  |  |  |  |
| C290G | *295-0104-00 | $0.1 \mu \mathrm{f}$ |  | Timing Series |  |  | 5310-up |
| C 290 H |  | $1{ }^{1} \mathrm{f}$ |  |  |  |  |  |
| C290J |  | $10 \mu \mathrm{f}$ |  |  |  |  |  |
| C292 | 283-001 | $0.005 \mu$ | Cer |  | 500 v |  |  |
| C294 | 281.528 | 82 pf | Cer |  | 500 v | 10\% |  |
| C296 | 283-006 | $0.02 \mu \mathrm{f}$ | Cer |  | 600 v |  |  |
| C299 | Use 281-010 | 4.5-25 pf | Cer | Var |  |  |  |
| C301 | 281-519 | 47 pf | Cer |  | 500 v | 10\% |  |
| C303 | 283.000 | $0.001 \mu f$ | Cer |  | 500 v |  |  |
| C311 | 283.000 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C314 | 283-002 | $0.01 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C328 | 281.550 | 120 pf | Cer |  | 500 v | 10\% |  |
| C329 | 281.519 | 47 pf | Cer |  | 500 v | 10\% |  |
| C330A | 281-550 | 120 pf | Cer |  | 500 v | 10\% |  |
| C3308 | 285.543 | $0.0022 \mu \mathrm{f}$ | MT |  | 400 v |  |  |
| C330C | 285-636 | $0.022 \mu \mathrm{f}$ | PTM |  | 200 v |  |  |
| C330D | 285-633 | $0.22 \mu \mathrm{f}$ | PTM |  | 100 v | 10\% |  |
| C330E | 285-576 | $1 \mu \mathrm{f}$ | PTM |  | 100 v | 10\% |  |
| C337 | 281.523 | 100 pf | Cer |  | 350 v |  |  |
| C344 | 283-002 | $0.01 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C346 | $281-512$ | 27 pf | Cer |  | 500 v | 1.\% |  |
| C360 | 281.523 | 100 pf | Cer |  | 350 v |  |  |
| C365 | 281-543 | 270 pf | Cer |  | 500 v | 10\% |  |
| C369 |  | 330 pf |  |  |  | 10\% |  |
| C370 | 281.605 | 200 pf | Cer |  | 500 v |  |  |
| C375 | 281.544 | 5.6 pf | Cer |  | 500 v | 10\% |  |
| C380 | 281-536 | 1000 pf | Cer |  | 500 v | 10\% | X1880 up |
| C382 | 283-006 | $0.02 \mu \mathrm{f}$ | Cer |  | 600 v |  |  |
| C392 | 283-006 | $0.02 \mu \mathrm{f}$ | Cer |  | 600 v |  |  |
| C397 | 283.006 | $0.02 \mu \mathrm{f}$ | Cer |  | 600 v |  |  |
| C398 | 283-002 | $0.01 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C399 | 283-002 | 0.01 ¢f | Cer |  | 500 v |  |  |
| C406 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |

## Parts List-Type 547

Capacitors (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Descrip |  |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C412 | 285-572 | 0.1 ¢f | PTM |  | 200 v |  |  |
| $\mathrm{C}_{424}$ | 283-000 | $0.001 \mu \mathrm{f}$ | Cor |  | 500 v |  |  |
| C426 | 281-523 | 100 pf | Cer |  | 350 v |  |  |
| C428 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C436 | 283-002 | $0.01 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C438 | 283-002 | $0.01 \mu$ | Cer |  | 500 v |  |  |
| C439 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C441 | $281-528$ | 82 pf | Cer |  | 500 v | 10\% |  |
| C446 | 283-000 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C449 | 281-575 | 39 pf | Cer |  | 500 v | 1\% |  |
| C454 | 281.512 | 27 pf | Cer |  | 500 v | 10\% |  |
| C456 | 283.006 | $0.02 \mu \mathrm{f}$ | Cer |  | 600 v |  |  |
| C459 | 281.575 | 39 pf | Cer |  | 500 v | 1\% |  |
| C467 | 281.549 | 68 pf | Cer |  | 500 v | 10\% |  |
| C475 | 283-004 | $0.02 \mu \mathrm{f}$ | Cer |  | 150 v |  |  |
| C477 | 281-549 | 68 pf | Cer |  | 500 v | 10\% |  |
| C503A | 281-558 | 18 pf | Cer |  | 500 v |  |  |
| C503C | 281-012 | 7.45 pf | Cer | Var |  |  |  |
| C503D | 281.560 | 198 pf | Cer |  | 500 v |  |  |
| C516 | 283-001 | $0.005 \mu \mathrm{f}$ | Cor |  | 500 v |  |  |
| C524 | 281-010 | 4.5-25 pf | Cer | Var |  |  |  |
| C525 | 281-557 | 1.8 pf | Cor |  | 500 v |  |  |
| C538 | 281.549 | 68 pf | Cer |  | 500 v | 10\% |  |
| C541 | 283.002 | $0.01 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C544 | 281.549 | 68 pf | Cer |  | 500 v | 10\% |  |
| C550 | 283-000 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C557D | 281.009 | 3-12 pf | Cer | Var |  |  |  |
| C557F | 281.013 | 8.50 pf | Cor | Var |  |  |  |
| C557H | 281-013 | 8.50 pf | Cer | Var |  |  |  |
| C562 | 290-0214-00 | $10 \mu \mathrm{f}$ | EMT |  | 250 v |  | X5680-up |
| C572 | 281.022 | 8.50 pf | Cer | Var |  |  |  |
| C574 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C576 | 281.053 | 0.35-1. 37 pf | Poly | Var |  |  |  |
| C579 | 283-068 | $0.01 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C582 | 281.022 | 8.50 pf | Cer | Var |  |  |  |
| C584 | 283-001 | $0.005 \mu \mathrm{f}$ | Cor |  | 500 v |  |  |
| C586 | 281-053 | 0.35-1.37 pf | Poly | Var |  |  |  |
| C589 | 283-068 | $0.01 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C591 | 281.036 | 3-12 pf | Cer | Var |  |  |  |
| C592 | 283-002 | 0.01 mf | Cer |  | 500 v |  |  |
| C598 | 285-628 | $0.033 \mu \mathrm{f}$ | PTM |  | 300 v |  |  |
| C599 | 283-000 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C600 | 285-519 | $0.047 \mu \mathrm{f}$ | MT |  | 400 v |  |  |
| C610 | 285-510 | $0.01 \mu \mathrm{f}$ | MT |  | 400 v |  |  |
| C617 | 285-519 | $0.047{ }^{\mu}$ | MT |  | 400 v |  |  |
| C628 | 285-510 | $0.01 \mu^{f}$ | MT |  | 400 v |  |  |
| C636 | 281.519 | 47 pf | Cer |  | 500 v | 10\% |  |

Capacitors (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Descript |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C640 | 283-022 | $0.02 \mu \mathrm{f}$ | Cer | 1400 v |  |  |
| C642A,B | Use 290-197 | $250 \mu \mathrm{f} \times 40 \mu \mathrm{f}$ | EMC | $350 \mathrm{v} / 250 \mathrm{v}$ |  |  |
| C650 | 285-510 | $0.01 \mu \mathrm{l}$ | MT | 400 v |  |  |
| C665 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer | 500 v |  | X1081-up |
| C670 | 283-022 | 0.02 ¢f | Cer | 1400 v |  |  |
| C671 | Use 290-180 | $300 \mu \mathrm{f}$ | EMC | 250 v |  |  |
| C680 | 285.510 | $0.01 \mu \mathrm{f}$ | MT | 400 v |  |  |
| C688 | 285-510 | $0.01 \mu \mathrm{f}$ | MT | 400 v |  |  |
| C694 | 281-523 | 100 pf | Cer | 350 v |  | X260-up |
| C701 | Use 290-192 | $200 \mu \mathrm{f}$ | EMC | 400 v |  |  |
| C709A |  | $10 \mu \mathrm{f}$ |  | 450 v |  |  |
| C7098 | Use 290-195 | $10 \mu \mathrm{f}$ | EMC | 350 v |  |  |
| C709C |  | $20 \mu \mathrm{f}$ |  | 250 v |  |  |
| C710 | 285-511 | $0.01 \mu \mathrm{f}$ | PTM | 600 v |  |  |
| C730 | Use 290.179 | $125 \mu \mathrm{f}$ | EMC | 250 v |  |  |
| C754 | 283.002 | $0.01 \mu \mathrm{f}$ | Cer | 500 v |  |  |
| C756 | 283.002 | $0.01 \mu$ | Cer | 500 v |  |  |
| C760 | 281-549 | 68 pf | Cer | 500 v | 10\% |  |
| C765 | 281.505 | 12 pf | Cer | 500 v | 10\% |  |
| C767 | 283-003 | $0.01 \mu \mathrm{f}$ | Cer | 150 v |  |  |
| C768 | 281.634 | 2.2 pf | Cer | 500 v | $\pm 0.25 \mathrm{pf}$ |  |
| C769 | 283-006 | $0.02 \mu \dagger$ | Cer | 600 v |  |  |
| C770 | 283-002 | $0.01 \mu \mathrm{f}$ | Cer | 500 v |  |  |
|  | Uso 290-185 | $2 \times 40 \mu \mathrm{f}$ | EMC | 250 v |  |  |
| C772 | $283.002$ | $0.01 \mu f$ | Cer | 500 v |  |  |
| C773A |  | $40 \mu \mathrm{f}$ |  | 250 v |  |  |
| C773B | Use 290-196 | $20 \mu \mathrm{f}$ | EMC | 350 v |  |  |
| C773C |  | $20 \mu \mathrm{f}$ |  | 450 v |  |  |
| C774 | 283.002 | $0.01 \mu \mathrm{f}$ | Cer | 500 v |  |  |
| C775 | 283.002 | 0.01 mf | Cer | 500 v |  |  |
| C777 | 283-002 | $0.01 \mu \mathrm{f}$ | Cer | 500 v |  |  |
| C802 | Use 290-190 | $40 \mu \mathrm{f}$ | EMC | 400 v |  |  |
| C803 | 283.000 | $0.001 \mu \mathrm{f}$ | Cer | 500 v |  |  |
| C806 | 285.506 | $0.0047{ }^{\prime \prime}$ | Cer | 400 v |  |  |
| C808 | 285.502 | $0.001 \mu \mathrm{f}$ | MT | 1000 v |  |  |
| C820 | 283-082 | $0.01 \mu$ | Cer | 4000 v |  |  |
| C821 | 283.082 | 0.01 mt | Cer | 4000 v |  |  |
| C822 | 281.525 | 470 pf | Cer | 500 v |  |  |
| C823 | 283-101 | $0.0047 \mu \mathrm{f}$ | Cer | 6000 v |  |  |
| C828 | $281-536$ | $0.001 \mu \mathrm{f}$ | Cer | 500 v | 10\% |  |
| C829 | 283.082 | $0.01 \mu \mathrm{f}$ | Cer | 4000 v |  |  |
| C830 | 283-082 | $0.01 \mu \mathrm{f}$ | Cer | 4000 v |  |  |
| C832 | 283-002 | 0.01 mf | Cer | 500 v |  |  |
| C833 | 281.556 | 500 pf | Cer | 10000 v |  |  |
| C834 | $281-556$ | 500 pf | Cer | 10000 v |  |  |
| C835 | 281.511 | 22 pf | Cer | 500 v | 10\% |  |
| C836 | 283-096 | 500 pf | Cer | 20000 v |  |  |
| C841 | 283-006 | 0.02 'f | Cer | 600 v |  |  |
| C842 | 283-082 | $0.01 \mathrm{\mu l}$ | Cer | 4000 v |  |  |
| C852 | $283-082$ | $0.01 \mu$ | Cer | 4000 v |  |  |
| C854 | 283-082 | $0.01 \mu \mathrm{f}$ | Cer | 4000 v |  |  |

Capacitors (Cont'd)
Tektronix

| Ckt. No. | Part No. |  | Descrip |  |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C858 | 283-082 | 0.01 mf | Cer |  | 4000 v |  |  |
| C863 | 283-002 | 0.01 \%f | Cor |  | 500 v |  |  |
| C932 | 283.041 | $0.0033 \mu \mathrm{f}$ | Cer |  | 500 v | 5\% |  |
| C934 | 283.032 | 470 pf | Cor |  | 500 v | 5\% |  |
| C939 | 283-057 | $0.1 \mu \mathrm{f}$ | Cer |  | 200 v |  |  |
| C941 | 283-006 | $0.02 \mu \mathrm{f}$ | Cer |  | 600 v |  |  |
| C944 | 283-057 | $0.1 \mu \mathrm{f}$ | Cer |  | 200 v |  |  |
| C958 | 281-525 | 470 pf | Cer |  | 500 v |  |  |
| C965 | 281-523 | 100 pf | Cer |  | 350 v |  |  |
| Cl 000 | 281.601 | 7.5 pf | Cer |  | 500 v | $\pm 0.5 \mathrm{pf}$ |  |
| C1002 | 283.001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C1014 | 283-067 | $0.001 \mu \mathrm{f}$ | Cer |  | 200 v | 10\% |  |
| Cl 016 | 281-519 | 47 pf | Cer |  | 500 v | 10\% |  |
| C1019 | Use 281-0505-00 | 12 pf | Cer |  | 500 v | 10\% | X1272-up |
| C1024 | 283-067 | $0.001 \mu \mathrm{f}$ | Cer |  | 200 v | 10\% |  |
| C1026 | 281-519 | 47 pl | Cer |  | 500 v | 10\% |  |
| C1027 | 281-558 | 18 pf | Cer |  | 500 v |  | 100-4749 |
| C1027 | 281-0061-00 | 5.5.18 pf | Cer | Var |  |  | 4750-up |
| C1028 | 283-001 | $0.005 \mu \mathrm{f}$ | Cer |  | 500 v |  |  |
| C1029 | 281.006 | 1.5-7 pf | Cer | Var |  |  |  |
| C1031 | 281-572 | 6.8 pf | Cer |  | 500 v | $\pm 0.5 \mu \mathrm{f}$ |  |
| C1035 | 283-067 | $0.001 \mu \mathrm{f}$ | Cer |  | 200 v | 10\% | 100-4269 |
| C1035 | 283-0078-00 | $0.001 \mu \mathrm{f}$ | Cor |  | 500 v |  | 4270-up |
|  | $283-067$ | $0.001 \mu \mathrm{f}$ | Cer |  | 200 v | 10\% | 100.4269 |
| C1038 | 283-0078-00 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  | 4270-up |
| C1042 | 281.572 | 6.88 pf | Cer |  | 500 v | $\pm 0.5 \mu \mathrm{f}$ |  |
| C1048 | $283-067$ | $0.001{ }^{\mu}$ | Cer |  | 200 v | 10\% | 100-4269 |
| C1048 | 283-0078-00 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  | 4270-up |
| C1069 | 283-067 | $0.001 \mu \mathrm{f}$ | Cer |  | 200 v | 10\% | $100-4269$ |
| C1069 | 283-0078-00 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  | 4270-up |
| C1071 | 283-067 | $0.001 \mu \mathrm{f}$ | Cer |  | 200 v | 10\% | 100-4269 |
| C1071 | 283-0078-00 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  | 4270 -up |
| C1074 | 281-503 | 8 pf | Cer |  | 500 v | $\pm 0.5 \mathrm{pf}$ |  |
| C1076 Cl 1076 | $\begin{aligned} & 281-075 \\ & 281-0123-00 \end{aligned}$ | $5-25 \mathrm{pf}$ $5-25 \mathrm{pf}$ | Cer Cer | Var Vor |  |  | 100-10729 10730-up |
| C1077 | 281-549 | 68 pf | Cer |  | 500 v | 10\% | 100-10729 |
| C1077 | 281-0540-00 | 51 pf | Cer |  |  | 5\% | 10730-up |
| C1087 | $283-067$ | $0.001 \mu \mathrm{f}$ | Cer |  | 200 v | 10\% | 100-4269 |
| C1087 | 283-0078-00 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  | 4270.up |
| C1091 | 281-0605-00 | 200 pf | Cer |  | 500 v |  | X10730-up |
| C1103 | 281.511 | 22 pf | Cer |  | 500 v | 10\% |  |
| C1104 | 281-524 | 150 pf | Cer |  | 500 v |  |  |
| Cl105 | 281-075 | 5.25 pf | Cer | Var |  |  |  |
| C1106 | $281-075$ | 5.25 pf | Cer | Var |  |  |  |
| C1107 | 281-600 | 35 pf | Cer |  |  | 10\% |  |
| C1113 | 283.067 | $0.001 \mu \mathrm{f}$ | Cer |  | 200 v | 10\% | 100-4269 |
| C1113 | 283-0078-00 | $0.001 \mu \mathrm{f}$ | Cer |  | 500 v |  | 4270-up |
| Cl116 | 283-001 | $0.005 \mu \mathrm{f}$ | Cor |  | 500 v |  |  |
| C1124 | 281-524 | 150 pf | Cer |  | 500 v |  |  |
| C1126 | 281-075 | $5-25$ pf | Cer | Var |  |  |  |
| ${ }_{\mathrm{Cl} 1127}$ | $281-558$ |  | Cer |  | 500 v |  |  |
| C1132 | 283-067 | $0.001{ }^{\mu f}$ | Cer |  | 200 v | 10\% | 100-4269 |
| C1132 | 283-0078-00 | $0.001 \mu f$ | Cer |  | 500 v |  | 4270-up |
| C1142 | $283-067$ | $0.001 \mu f$ | Cer |  | 200 v | 10\% |  |
| C1152 | 283-067 | $0.001 \mu \mathrm{f}$ | Cer |  | 200 v | 10\% |  |

## Capacitors (Cont'd)



Parts List-Type 547



| Ckr. No. | Tektronix Part No. | Inductors Discription | S/N Range |
| :---: | :---: | :---: | :---: |
| LR21 | *108-230 | $3.25 \mu$ (on a $150 \Omega 1 / 2 w 5 \%$ resistor) |  |
| LR23 | *108-230 | $3.25 \mu \mathrm{~h}$ (on a $150 \Omega 1 / 2 \mathrm{w} 5 \%$ resistor) |  |
| 144 | 276-507 | Core, Ferramic Suppressor | 100-6739x |
| 150 | *108-0146-00 | $5 \mu \mathrm{~h}$ | X6740-up |
| 152 | *108-147 | $2.2 \mu \mathrm{~h}$ | 100-6739x |
| 156 | *108-215 | $1.1 \mu h$ |  |
| 185 | *108-0410-00 | $1 \mu \mathrm{~h}$ | X6740-up |
| LR221 | *108-230 | $3.25 \mu \mathrm{~h}$ (on a $150 \Omega 1 / 2 \mathrm{w} 5 \%$ resistor) |  |
| LR223 | *108-230 | $325 \mu$ (on a $150 \Omega 1 / 2 \mathrm{w} 5 \%$ resistor) |  |
| 1244 | 276-507 | Core, Ferramic Suppressor | 100-6739X |
| 1250 | *108-0146-00 | $5 \mu \mathrm{~h}$ | X6740-up |
| L252 | *108-147 | $2.2 \mu \mathrm{~h}$ | 100-6739x |
| L256 | *108-215 | $1.1 \mu \mathrm{~h}$ |  |
| L285 | *108-0410-00 | $1 \mu \mathrm{~h}$ | X6740-up |
| 1404 | *120-309 | Toroid, 6 T Single |  |
| 1553 | *119.030 | Delay Line Assembly |  |
| 1760 | 108-240 | $820 \mu \mathrm{~h}$ |  |
| 1778 | Use *108-323 | Beam Rotator |  |
| 11013 | *108-260 | $0.1 \mu$ h |  |
| 11018 | *120-266 | Toroid, 10T Single |  |
| 11023 | *108-260 | $0.1 \mu \mathrm{~h}$ |  |
| 11030 | *108-264 | $0.2 \mu \mathrm{~h}$ |  |
| 11040 | *108-264 | $0.2 \mu \mathrm{~h}$ |  |
| 11051 | *108-260 | $0.1 \mu \mathrm{~h}$ |  |
| LR1052 | *108-288 | $1.2 \mu \mathrm{~h}$ (on a $6.2 \Omega 1 / 2 \mathrm{w} 5 \%$ resistor) |  |
| 11061 | *108-260 | $0.1 \mu \mathrm{~h}$ |  |
| LR1062 | *108-288 | $1.2 \mu \mathrm{~h}$ (on a $6.2 \Omega \mathrm{y}$ / w 5\% resistor) |  |
| 11072 | *108-260 | $0.1 \mu \mathrm{~h}$ |  |
| 11082 | *108.260 | $0.1 \mu \mathrm{~h}$ |  |
| LR1115 | *131-335 | $0.5 \mu \mathrm{~h}$ (on a $330 \Omega 1 / 4 \mathrm{w}$ resistor) (brown) |  |
| (R1135 | *131-336 | $0.5 \mu$ (on a $330 \Omega 1 / 4 \mathrm{w}$ resistor) (blue) |  |
| 11144 | *108.095 | $1.4 \mu \mathrm{~h}$ |  |
| 11145 | 276-0507-00 | Core, Ferramic Suppressor | X14640-up |
| til54 | *108-095 | $1.4 \mu \mathrm{~h}$ |  |
| 11155 | 276-0507-00 | Core, Ferramic Suppressor | X14640-up |
| 11157 | *114.080 | $6.8 \mu \mathrm{~h}-14.6 \mu \mathrm{~h} \quad$ Var $\quad$ Core 276.0506.00 |  |
| 11160 | 276-528 | Core, Ferramic Suppressor |  |
| 11170 | 276-528 | Core, Ferramic Suppressor |  |
|  |  | Relays |  |
| $\begin{aligned} & \text { K600 } \\ & \text { K601 } \end{aligned}$ | $\begin{aligned} & 148-021 \\ & * 148-019 \end{aligned}$ | Tube Relay Tek Spec |  |
|  |  | Transistors |  |
| Q34 | 151-089 | 2N962 | 100-6059 |
| Q34 | 151-0188-00 | 2N3906 | 6060.6739 |
| Q34 | *151-0199-00 | Silicon Replaceable by MPS.3640 | 6740-up |
| Q44 | 151-089 | 2N962 | 100-6059 |
| Q44 | 151-0188-00 | 2N3906 | 6060.6739 |
| Q44 | *151.0199-00 | Silicon Replaceable by MPS-3640 | 6740-up |
| Q65 | *151-108 | Replaceable by 2N2501 |  |
| Q75 | *151-108 | Replaceable by 2N2501 |  |
| Q84 | *151-108 | Replaceable by 2N2501 | 100.12479 |
| Q84 | 151-0190-00 | 2N3904 | 12480-up |

Transistors (Cont'd)
Tektronix

| Ckt. No. | Part No. | Description | S/N Range |
| :---: | :---: | :---: | :---: |
| Q86 | 151-0277-00 | RCA 38520 | X12480-up |
| Q89 | -151-096 | Selected from 2N1893 |  |
| Q103 | 151.089 | 2N962 | 100-6059 |
| Q103 | 151-0188-00 | 2N3906 | 6060-up |
| Q173 | 151-063 | 2N2207 |  |
| Q184 | 151.063 | 2N2207 |  |
| Q234 | 151.089 | 2N962 | 100-6059 |
| Q234 | 151-0188-00 | 2N3906 | 6060.6739 |
| Q234 | *151-0199-00 | Silicon Replaceable by MPS-3640 | 6740 -up |
| Q244 | 151.089 | 2N962 | 100.6059 |
| Q244 | 151-0188.00 | 2N3906 | 6060.6739 |
| Q244 | 151.0199-00 | Silicon Replaceable by MPS-3640 | 6740-up |
| Q265 | *151-108 | Replaceable by 2 N 2501 |  |
| Q275 | *151-108 | Replaceable by 2N2501 |  |
| Q284 | *151-108 | Replaceable by 2N2501 | 100-12479 |
| Q284 | 151-0190-00 | 2N3904 | 12480-up |
| Q286 | 151-0277-00 | RCA 38520 | X12480-up |
| Q289 | *151-096 | Selected from 2N1893 |  |
| Q303 | 151-089 | 2N962 | 100-6059 |
| Q303 | 151-0188-00 | 2N3906 | 6060-up |
| Q344 | *151-096 | Selected from 2N1893 |  |
| Q373 | 151.063 | 2N2207 |  |
| Q424 | 151.063 | 2N2207 | 100.14709 |
| Q424 | *151-0322-00 | Replaceable by 2 N 4890 | 14710-up |
| Q433 | *151-103 | Replaceable by 2 N 2219 |  |
| Q444 | *151-103 | Replaceable by 2 N 2219 |  |
| Q454 | *151-103 | Replaceable by 2N2219 |  |
| Q464 | *151-108 | Replaceable by ${ }^{\text {2 }} \mathbf{N} 2501$ |  |
| Q465 | *151-108 | Replaceable by 2 N 2501 |  |
| Q475 | *151-108 | Replaceable by 2 N 2501 |  |
| Q534 | *151-121 | Selected from TA 1938 | 100-15299 |
| Q534 | *151-0124-00 | Selected from 2N13501 | 15300-up |
| Q543 | *151-096 | Selected from 2N11893 |  |
| Q554 | 151.063 | 2N2207 | 100-14709 |
| Q554 | *151-0322-00 | Replaceable by ${ }^{2} \mathrm{~N} 4890$ | 14710.up |
| Q564 | 151.063 | 2N2207 | 100-14709 |
| Q564 | *151-0322-00 | Replaceable by 2 N 4890 | 14710-up |
| $\begin{aligned} & \text { Q1014 } \\ & \text { Q1024 } \end{aligned}$ | *153-525 | Matched pair (Selected from 2N2475) |  |
| $\begin{aligned} & \text { Q1034 } \\ & \text { Q1044 } \end{aligned}$ | *153-527 | Matched pair (R-placeable by 2 N 2501 ) |  |
| Q1074 | *153-525 | Matched pair (Selected from 2N2475) |  |
| Q1104 $\dagger$ | *153-526 | Selected from 2 12369 |  |
| Q1109 | 151-0149-00 | 2N3441 | $\times 2340 \cdot \mathrm{up}$ |
| Q1114 ${ }^{\text {d }}$ | *153-524 | Selected from TA1938 | 100-5679 |
| Q1114+ | *153-0548-00 | Selected from 2113119 | 5680-up |
| Q1124 | *153-526 | Selected from 2N12369 |  |
| Q1134tt | *153-524 | Selecled from TA1938 | 100-5679 |
| Q1134t+ | *153-0548-00 | Selected from 2r 13119 | 5680-up |
| Q1144 O1154 | *153-527 | Matched pair (R.placeable by 2N2501) |  |
| Q1163 | *151-127 | Selected from 2N2369 |  |
| Q1173 | *151-127 | Selected from 2 12369 |  |

tQ1104 and Q1124 furnished as a matched pair.
HQ1114 and Q1134 furnished as a matched pair.

## Resistors

| Ckt. No. | Tektronix Part No. |  | Descrip |  |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Resistors are fixed, composition, $\pm 10 \%$ unless otherwise indicated. |  |  |  |  |  |  |  |
| R5 | 302.104 | 100 k | $1 /$ w |  |  |  |  |
| R6 | 321-385 | 100 k | $1 / 4 w$ |  | Prec | 1\% |  |
| R7 | 323-406 | 165 k | $1 / 1, w$ |  | Prec | 1\% |  |
| R8 | 316-101 | $100 \Omega$ | $1 / 4 w$ |  |  |  |  |
| R9 | 311.018 | 20 k |  | Var |  | B INT TRIG | DC Level |
| R 13 | 323-481 | 1 meg | $1 / w$ |  | Prec | $1 \%$ |  |
| R14 | 302-155 | 1.5 meg | $1 / 1, w$ |  |  |  |  |
| $\mathrm{Rl}^{\text {15 }} \dagger$ | $311-426$ | 300 k |  | Var |  | TRIGGERING | LEVEL |
| $R 16$ | 302-394 | 390 k | $1 / 2 w$ |  |  |  |  |
| R17 | 302-335 | 3.3 meg | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R18 | 302-104 | 100 k | 1/w |  |  |  |  |
| R19 | 316-105 | 1 meg | $1 / w$ |  |  |  |  |
| R20 | 316-101 | $100 \Omega$ | $1 / w$ |  |  |  |  |
| R21 | 316-221 | $220 \Omega$ | $1 / 4 w$ |  |  |  | 100.6739 |
| R21 | 315-0471-00 | $470 \Omega$ | $1 / 4 w$ |  |  | 5\% | 6740-up |
| R22 | 316-101 | $100 \Omega$ | 1/9w |  |  |  |  |
| R23 | 316.221 | $220 \Omega$ | $1 / \mathrm{w}$ |  |  |  | 100-6739 |
| R23 | 315.0471.00 | $470 \Omega$ | 1/w w |  |  | 5\% | 6740-up |
| R24 | 308.108 | 15 k | 5 w |  | WW | 5\% |  |
| R25 | 311-158 | $200 \Omega$ |  | Var |  | B TRIGGER LEVEL C | CENTERING |
| R27 | 308.267 | 7.5 k | $5 w$ |  | ww | 5\% |  |
| R28 | 302.102 | 1 k | 1/2w |  |  |  |  |
| R32 | 315-0471-00 | $470 \Omega$ | $1 / 4 w$ |  |  | 5\% | X6740-up |
| R33 | 308-0301-60 | 10 k | 3 w |  | WW | 1\% | X6740-up |
| R36 | 324-335 | 30.1 k | 1 w |  | Prec | 1\% | 100-6739 |
| R36 | 308-0320-00 | 15.6 k | 3 w |  | WW | 1\% | 6740 -up |
| R41 | $316-221$ | $220 \Omega$ | 1/4w |  |  |  | 100.6739x |
| R42 | 315-0471-00 | $470 \Omega$ | $1 / 4 w$ |  |  | 5\% | X6740-up |
| R43 | 316-100 | $10 \Omega$ | $1 / 4 w$ | . |  |  | 100.6739X |
| R44 | 322.001 | $10 \Omega$ | $1 / 4 w$ |  | Prec | 1\% | 100-6739X |
| $R 45$ |  | $50 \Omega$ | 1/2w | Var | WW | B TRIGGER SENS | 100.6739 |
| R45 | $311-0405-00$ | 10k |  | Va |  | B TRIGGER SENS | 6740-up |
| R46 | 308.0310.00 | 12 k | 5 w |  | WW | 1\% | X6740-up |
| R47 | 324-306 | 15k | 1 w |  | Prec | 1\% | 100.6739X |
| R48 | 324-306 | 15 k | 1 w |  | Prec | 1\% | 100.6739 ${ }^{\text {x }}$ |
| R49 | 302-101 | $100 \Omega$ | $1 / 2 w$ |  |  |  |  |
| R50 | 302-101 | $100 \Omega$ | $1 / 2 w$ |  |  |  |  |
| R51 | 302-101 | $100 \Omega$ | $1 / 2 w$ |  |  |  |  |
| 852 | 315-0560-00 | $56 \Omega$ | $1 / 4 w$ |  |  | 5\% | X6740-up |
| R53 | 323-370 | 69.8 k | $1 / 2 w$ |  |  | 1\% |  |
| R54 | 323-140 | $280 \Omega$ | $1 / 2 w$ |  | Prec | 1\% |  |
| R57 | 302-224 | 220 k | 1/2w |  |  |  | 100-6739 |
| 857 | 302.0104-00 | 100 k | $1 / 2 w$ |  |  |  | 6740-up |
| R63 | 316-470 | $47 \Omega$ | $1 / 4 w$ |  |  |  |  |
| R65 | 301.303 | 30 k | $1 / 2 w$ |  |  | 5\% |  |
| R67 | 301-912 | 9.1 k | $1 / 2 w$ |  |  | 5\% |  |
| tFurnished as a unit with SW15. |  |  |  |  |  |  |  |




Resistors (Cont'd)


| Ckt. No. | Tektronix Part No. |  | Resistors (Cont'd) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Description |  |  | S/N Range |
| R252 | 315-0560.00 | $56 \Omega$ | 1/4 w |  | 5\% | X6740-up |
| R253 | $323-370$ | 69.8 k | $1 / 2 w$ | Prec | 1\% | X6740.up |
| R254 | 323-140 | $280 \Omega$ | $1 / 2 \mathrm{w}$ | Prec | 1\% |  |
| R255 | 301-203 | 20 k | $1 / 2 \mathrm{w}$ |  | 5\% |  |
| R256 | $301-134$ | 130 k | $1 / 2 \mathrm{w}$ |  | 5\% | 100-6739 |
| R256 | 301-0304-00 | 300 k | 1/w |  | 5\% | 6740 -up |
| R258 | 302-473 | 47 k | 1/w |  |  |  |
| R263 | 316-470 | $47 \Omega$ | $1 / 4$ w |  |  |  |
| R265 | 301-303 | 30 k | 1/2w |  | 5\% |  |
| R267 | 301.912 | 9.1 k | 1/2: $w$ |  | 5\% |  |
| R269 | 316.103 | 10 k | 1/w |  |  |  |
| R271 | 303-513 | 51 k | \| w |  | 5\% |  |
| R275 | $301-513$ | 51 k | 1/w |  | 5\% | 100-6739 |
| R275 | 303-0243-00 | 24 k | is |  | 5\% | 6740-up |
| R276 | $302-471$ | 470 ת | Y/w |  |  | 100-6739 |
| R276 | 301-0221-00 | $220 \Omega$ | \% w |  | 5\% | 6740-up |
| R278 | $301-752$ | 7.5 k | $1 /$ w |  | 5\% | \% |
| R279 | 302-152 | 1.5 k | $\%$ w |  |  | 100.6739 |
| R279 | 302-0561-00 | $560 \Omega$ | \% w |  |  | 6740-up |
| $R 281$ | 316.101 | $100 \Omega$ | $1 / 4$ w |  |  | 100.6739 |
| R281 | 315.0181 .00 | $180 \Omega$ | 1/4w |  | 5\% | 6740-up |
| R282 | 323-333 | 28.7 k | $y / w$ | Prec | 1\% | 100-6739 |
| R282 | 323-0636-00 | 50 k | $1 / 2 \mathrm{w}$ | Prec | 1\% | 6740-up |
| R283 | 316-394 | 390 k | 1/4w |  |  |  |
| R284 | 305-153 | 15 k | 2 w |  | 5\% |  |
| R285 | $301-102$ | 1 k | 1/: w |  | 5\% |  |
| R286 | $303-513$ | 51 k | 1 w |  | 5\% |  |
| R287 | 301-273 | 27 k | \%/w |  | 5\% |  |
| R288 | $302-823$ | 82 k | 1/w |  |  |  |
| R289 | 302-105 | 1 meg | y/w |  |  |  |
| R290A |  | 140 k | 1/w |  | 1\% |  |
| R2908 R290C | *312.640 | 280k | $1 / \mathrm{w}$ $1 / \mathrm{w}$ |  | 1\% |  |
| R290C R290D |  | $700 k$ | Y/w |  | 1\% |  |
| R290E | *312.641 | 2.8 meg | $1 / \mathrm{w}$ $y / \mathrm{w}$ |  | 1\% | 100-5479 |
| R290F |  | 7 meg | y/w |  | 1\% | 100-5479 |
|  |  | 1.4 meg | $1 /$ w |  | 1\% |  |
| R290E | *312-0641-01 | 2.8 meg | $1 / \mathrm{w}$ |  | 1\% |  |
| R290F <br> R290G | *312-0641-01 | $7 \mathrm{meg}$ | $1 / w$ |  | 1\% | 5480-8299 |
| R290G R290D |  | 47 k <br> 1.4 meg | (nominal value) Selected 1/w |  |  |  |
| R290E |  | 2.8 meg | 1\%w |  | 1\% |  |
| R290F | *312-0541-02 | 7 meg | \% w |  | 1\% | $8300 \cdot 10259$ |
| R290G |  | 47 k | (nominal value) Selected |  |  |  |
| R290H |  | 39 k | (nominal value) Selected |  |  |  |
| R2900 |  | 1.4 meg | y/w |  | 1\% |  |
| R290E |  | 2.8 meg | 1/2 ${ }^{\text {w }}$ |  | 1\% |  |
| R290F | *312-0641-03 | 7 meg | 1/w |  | 1\% | 10260.15299 |
| R290G |  | 47 k | (nominal value) Selected |  |  |  |
| R290H |  | 39 k | (nominal value) Selected |  |  |  |
| R290D |  | 1.4 meg | $1 / 2 \mathrm{w}$ |  |  |  |
| R290E |  | 2.8 meg | 1/2w |  |  |  |
| R290F | *312-0641.04 | 7 meg |  |  |  |  |
| R290G | 312-0641.04 | 47 k | (noninal value) Selected |  |  | 15300-up |
| R290H |  | 39 k | (noninal value) Selected |  |  |  |
| R2901 |  | 10 k | (nominal value) Selected |  |  |  |
| R290W | 302-105 | 1 meg | \%/w |  |  |  |
| R290X | 302-104 | 100k | 1/w |  |  |  |
| R290Y | 311-388 | 7.5 k | Var | WW | A SW |  |
| R290Z $\dagger$ | 311-391 | 150 k | Var |  | VARI |  |

Resistors (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Description |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R292 | 316-101 | $100 \Omega$ | 1/4w |  |  |  |
| R293 | 304-473 | 47 k | 1 w |  |  |  |
| R294 | 304-473 | 47 k | 1 w |  |  |  |
| R295 | 316-101 | $100 \Omega$ | $1 / 4 w$ |  |  |  |
| R296 | 316-101 | $100 \Omega$ | $1 / 4$ w |  |  |  |
| R297 | 308-0400-00 | 18 k | 5 w | WW | 5\% | X12480-up |
| R298 | 315-0102-00 | 1 k | $1 / 4 w$ |  | 5\% | X12480-up |
| R299 | 323-356 | 49.9 k | 1/2w | Prec | 1\% |  |
| R300 | 315-0272-00 | 2.7 k | $1 / 4$ w |  | 5\% | X12480-up |
| R301 | 316-471 | $470 \Omega$ | $1 / 4 w$ |  |  |  |
| R302 | 316-153 | 15k | $1 / 4 w$ |  |  |  |
| R303 | 306-273 | 27 k | 2 w |  |  |  |
| R305 | 316.152 | 1.5 k | $1 / 4$ w |  |  |  |
| R310 | 301-272 | 2.7 k | $1 / 2 w$ |  | 5\% |  |
| R311 | 302-104 | 100 k | 1/2 w |  |  |  |
| R312 | 316.101 | $100 \Omega$ | $1 / 4 w$ |  |  |  |
| R314 | 316-101 | $100 \Omega$ | 1/4 w |  |  |  |
| R316 | 302-104 | 100 k | 1/2w |  |  |  |
| R321 | 306.683 | 68 k | 2 w |  |  |  |
| R324 | 303-163 | 16k | 1 w |  | 5\% |  |
| R325 | $311-011$ | 5 k | Var |  | A SWEEP | ENGTH |
| R326 | 305-393 | 39 k | 2 w |  | 5\% |  |
| R328 | 302-102 | 1 k | 1/2w |  |  |  |
| R329 | 302-562 | 5.6 k | 1/2w |  |  |  |
| R330A | 301.155 | 1.5 meg | $1 / 2 \mathrm{w}$ |  | 5\% |  |
| R330B | 301.565 | 5.6 meg | $1 / 2 w$ |  | 5\% |  |
| R330C | 301-156 | 15 meg | $1 / 2 w$ |  | 5\% |  |
| R330D | 301-226 | 22 meg | $1 / 2 \mathrm{w}$ |  | 5\% |  |
| R334 | 323-373 | 75 k | $1 / 2 \mathrm{w}$ | Prec | 1\% |  |
| k335 | 323-273 | 6.81 k | $1 / 2 \mathrm{w}$ | Prec | 1\% |  |
| R337 | 323-481 | 1 meg | $1 / 2 \mathrm{w}$ | Prec | 1\% |  |
| R338 | 309-439 | 5.9 meg | $1 / 2 w$ | Prec | 1\% |  |
| R339 | 316-101 | $100 \Omega$ | $1 / 4 w$ |  |  |  |
| R341 | 301-334 | 330 k | 1/2w |  | 5\% |  |
| R342 | 301-274 | 270 k | 1/2w |  | 5\% |  |
| R343 | 301-683 | 68 k | 1/2w |  | 5\% |  |
| R344 | 302-101 | $100 \Omega$ | 1/2w |  |  |  |
| R345 | 323-302 | 13.7 k | $1 / 2 w$ | Prec | 1\% |  |
| R346 | 323-385 | 100 k | $1 / 2 \mathrm{w}$ | Prec | 1\% |  |
| R347 | 323-402 | 150 k | $1 / 2 \mathrm{w}$ | Prec | 1\% |  |
| R348 | 316.101 | $100 \Omega$ | $1 / 4$ w |  |  |  |
| R349 | 302-122 | 1.2 k | 1/2w |  |  |  |
| R355 | 301-224 | 220 k | $1 / 2 \mathrm{w}$ |  | 5\% |  |
| R357 | 323-321 | 21.5 k | $1 / 2 w$ | Prec | 1\% |  |
| R358 | 323.426 | 267 k | $1 / 2 \mathrm{w}$ | Prec | 1\% |  |
| R359 | 301-334 | 330 k | $1 / 2 w$ |  | 5\% |  |
| R360 | 316-222 | 2.2 k | 1/4w |  |  |  |
| R361 | 323-243 | 2.32 k | 1/2w | Prec | 1\% |  |
| R362 | 308-268 | 22 k | 5 w | WW | 1\% |  |
| R363 | 324-343 | 36.5 k | 1 w | Prec | 1\% |  |
| R364 | 301-303 | 30 k | $1 / 2 w$ |  | 5\% |  |
| R365 | 301-274 | 270 k | 1/2w |  | 5\% |  |
| R366 | 316-102 | 1 k | 1/4w |  |  |  |
| R367 | 316-182 | 1.8 k | $1 / 4 \mathrm{w}$ |  |  |  |
| R368 | 316-336 | 33 meg | $1 / 4 \mathrm{w}$ |  |  |  |

## Parts List-Type 547

| Resistors (Cont'd) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Description |  |  | S/N Range |  |  |
| R369 | 316-182 | 1.8 k | $1 / 4$ w |  | 5\% |  |  |
| R370 | 301-472 | 4.7 k | $1 / 2 w$ |  |  |  |  |
| R371 | 302-472 | 4.7 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R372 | 302-274 | 270 k | $1 / 2 \mathrm{w}$ |  | Prec <br> Prec <br> Prec | $\begin{aligned} & 1 \% \\ & 1 \% \\ & 1 \% \end{aligned}$ |  |
| R373 | 316-470 | 47 ת | 1/4w |  |  |  |  |
| R374 | 323-353 | 46.4 k | 1/2w |  |  |  |  |
| R375 | 323-330 | 26.7 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R376 | 323-356 | 49.9 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R377 | 321.0193-00 | 1 k | \% w |  | Prec | 1\% | $\begin{aligned} & \text { X5680-up } \\ & \text { X1880-up } \end{aligned}$ |
| R380 | 302.0473-00 | 47 k | 1/2w |  |  |  |  |
| R381 | 316-470 | $47 \Omega$ | 1/4 w |  |  |  |  |
| R382 | 316-101 | 100 n | $1 / 4$ w |  |  |  |  |
| R383 | 302-104 | 100 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R384 | 316-820 | $82 \Omega$ | 1/6 w |  | Prec | 1\% |  |
| R390 | 323-373 | 75 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R391 | 316-470 | $47 \Omega$ | 1/4w |  |  |  |  |
| R392 | 316.101 | $100 \Omega$ | 1/4w |  |  |  |  |
| R393 | 302.472 | 4.7 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R394 | 316-101 | $100 \Omega$ | $1 / 4$ w |  | 5\% |  |  |
| R397 | 307-106 | $4.7 \Omega$ | 1/4w |  |  |  |  |  |  |
| R398 | 316.101 | $100 \Omega$ | $1 / 4$ w |  |  |  |  |  |  |
| R399 | 316-101 | $100 \Omega$ | $1 / 4$ w |  |  |  |  |  |  |
| R401 | 316.101 | $100 \Omega$ | 1/4w |  |  |  |  |  |  |
| R404 | 302-331 | $330 \Omega$ | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R406 | 301.563 | 56 k | $1 / 2 \mathrm{w}$ |  |  |  |  |  |  |
| R407 | 301.913 | 91 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R408 | 316.101 | $100 \Omega$ | 1/4w |  | 5\% |  |  |
| R409 | 303.183 | 18 k | 1 w |  |  |  |  |  |  |
| R412 | 316-101 | $100 \Omega$ | $1 / 4 w$ |  |  |  |  |
| R413 | $316-473$ | 47 k | 1/4w | Var Var | Prec WW | $\begin{gathered} 1 \% \\ \text { DELAY STOP } \\ \text { DELAY TIME MULTIPLIER } 1.10 \end{gathered}$ |  |
| R414 | 324-339 | 33.2 k | I w |  |  |  |  |  |
| R415 | 311-015 | 10k |  |  |  |  |  |  |
| R416 | 311-022 | 30 k |  |  |  |  |  |  |
| R417 | 302-331 | $330 \Omega$ | 1/2w | Var | WW WW | DELAY START 1\% |  |
| R418 | 311.141 | 2 k |  |  |  |  |  |  |
| R419 | 308-268 | 22 k | 5 w |  |  |  |  |  |
| R421 | 316-101 | $100 \Omega$ | 1/6 w |  |  |  |  |  |
| R424 | 302-564 | 560 k | 1/2w |  |  |  |  |  |
| R425 | 301.104 | 100 k | 1/2w |  | $\begin{aligned} & 5 \% \\ & 5 \% \end{aligned}$ |  |  |
| R426 | 301-223 | 22 k | 1/2w |  |  |  |  |  |  |  |
| R428 | 302-223 | 22 k | 1/2w |  |  |  |  |  |  |  |
| R429 | 302-682 | 6.8 k | $1 / 2 \mathrm{w}$ |  |  |  |  |  |  |  |
| R430 | 302-333 | 33 k | $1 / 2 \mathrm{w}$ |  |  |  |  |  |  |  |
| R431 | 302-151 | $150 \Omega$ | 1/2w |  |  |  |  |  |  |  |
| R432 | 316-470 | $47 \Omega$ | 1/4w |  |  |  |  |
| R433 | 302-102 | 1 k | 1/2w |  |  |  |  |
| R435 | 302-562 | 5.6 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R438 | 302-101 | $100 \Omega$ | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R439 | 302-102 | 1 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R441 | 302-105 | 1 meg | 1/2w |  |  |  |  |
| R443 | 302-823 | 82 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R444 | 302-104 | 100 k | 1/2w |  |  |  |  |
| R446 | 302-102 | 1 k | 1/2w |  |  |  |  |
| R448 | 302-103 | 10 k | 1/2w |  |  |  |  |

Resistors (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Description |  |  | 5/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R451 | 302.183 | 18 k | 1/2w |  |  |  |
| R452 | 304-223 | 22 k | 1 w |  |  |  |
| R453 | 302-103 | 10 k | $1 / 2 \mathrm{w}$ |  |  |  |
| R454 | 301-913 | 91 k | $1 / 2 w$ |  |  | 5\% |
| R455 | 304-393 | 39 k | 1 w |  |  |  |
| R456 | 316-100 | $10 \Omega$ | $1 / 4 \mathrm{w}$ |  |  |  |
| R457 | 302-472 | 4.7 k | $1 / 2 \mathrm{w}$ |  |  |  |
| R458 | 302-473 | 47 k | 1/2w |  |  |  |
| R459 | 302-332 | 3.3 k | $1 / 2 \mathrm{w}$ |  |  |  |
| R461 | 323-384 | 97.6 k | $1 / 2 \mathrm{w}$ |  | Prec | 1\% |
| R464 | 303.183 | 18 k | 1 w |  |  | 5\% |
| R467 | 316-273 | 27 k | $1 / 4 w$ |  |  |  |
| R469 | 302-155 | 1.5 meg | 1/2w |  |  |  |
| R470 | 311-153 | 10 k |  | Var |  | A SWEEP DC LEVEL |
| R471 | 323-382 | 93.1 k | 1/2w |  | Prec | 1\% |
| R474 | 303.183 | 18 k | 1 w |  |  | 5\% |
| R475 | 302-104 | 100 k | 1/2w |  |  |  |
| R477 | 316-273 | 27 k | $1 / 4 \mathrm{w}$ |  |  |  |
| R479 | 302-155 | 1.5 meg | $1 / 2 w$ |  |  |  |
| R481 | 301-154 | 150 k | $1 / 2 \mathrm{w}$ |  |  | 5\% 100-1159 |
| R481 | 304-273 | 27 k | 1 w |  |  | 1160-up |
| R483 | 301-434 | 430 k | 1/2w |  |  | 5\% |
| R484 | $311-028$ | $2 \times 100 \mathrm{k}$ |  | Var |  | TRACE SEPARATION |
| R485 | 315-203 | 20 k | 1/4w |  |  | 5\% |
| R486 | 316-470 | $47 \Omega$ | $1 / 4 w$ |  |  |  |
| R487 | 303-433 | 43 k | 1 w |  |  | 5\% |
| R488 | 303-433 | 43 k | 1 w |  |  | 5\% |
| R493 | 301-434 | 430 k | 1/2w |  |  |  |
| R495 | 315-203 | 20 k | $1 / 4 w$ |  |  | 5\% |
| R496 | 316-470 | $47 \Omega$ | 1/4w |  |  |  |
| R497 | 303-433 | 43 k | 1 w |  |  | 5\% |
| R498 | 303-433 | 43 k | 1 w |  |  | 5\% |
| R499 | 315-162 | 1.6k | 1/4 w |  |  | 5\% |
| R501 | 302-470 | $47 \Omega$ | 1/2w |  |  |  |
| R503C | 323.611 | 900 k | $1 / 2 w$ |  | Prec | 1\% |
| R503D | $323-610$ | 111 k | $1 / 2 w$ |  | Prec | 1\% |
| R507 | 323-481 | 1 meg | $1 / 2 \mathrm{w}$ |  | Prec | 1\% |
| R508 | 316-102 | 1 k | $1 / 4 \mathrm{w}$ |  |  |  |
| R509 | 306-333 | 33 k | 2 w |  |  |  |
| R510 | 301-201 | $200 \Omega$ | 1/2w |  |  | 5\% |
| R511 | Use 311-491 | 10 k |  | Var |  | VAR 10.1 |
| R512 | 306-333 | 33 k | 2 w |  |  |  |
| R514 | 316-101 | $100 \Omega$ | $1 / 4$ w |  |  |  |
| R516 | 302-332 | 3.3 k | $1 / 2 w$ |  |  |  |
| R 517 | $302-224$ | 220 k | 1/2w |  |  |  |
| R519 | $311-026$ | 100 k |  | Var |  | EXT HORIZ DC BAL |
| R522 | 305.183 | 18 k | 2 w |  |  |  |
| R524 | 323-356 | 49.9 k | 1/2w |  | Prec | 1\% |
| R525 | 301.565 | 5.6 meg | $1 / 2 w$ |  |  | 5\% |
| R526 | 302-101 | $100 \Omega$ | 1/2w |  |  |  |
| R530A R530B | 311-431 | 50 k 50 k |  | Var |  | HORIZ POSITION VERNIER |


| Resisfors (Cont'd) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. | Description |  |  |  | S/N Range |  |
| R531 | 323-369 | 68.1 k | $1 / 2 w$ |  | Prec | 1\% |  |
| R532 | 301-274 | 270 k | 1/2w |  |  | 5\% |  |
| R533 | 323.452 | 499k | $1 / 2 w$ |  | Prec | 1\% |  |
| R534 | 304.123 | 12k | 1 w |  |  |  |  |
| R535 | 316-390 | $39 \Omega$ | $1 / 4 w$ |  |  |  |  |
| R538 | 302-123 | 12k | 1/2w |  |  |  |  |
| R539 | 303.753 | 75 k | 1 w |  |  | 5\% |  |
| R540 | 304-822 | 8.2 k | 1 w |  |  |  |  |
| R541 | 316-101 | $100 \Omega$ | $1 / 6$ |  |  |  |  |
| R542 | 301.303 | 30 k | $1 / 2 w$ |  |  | 5\% |  |
| R543 | 306-393 | 39 k | 2 w |  |  |  |  |
| R544 | 311.172 | 2.5 k |  | Var |  | $\times 10 \mathrm{CAL}$ |  |
| R545 | 323-284 | 8.87 k | $1 / 2 w$ |  | Prec | 1\% | 100-5129 |
| R545 | 323-0281-00 | 8.25 k | $1 / 2 w$ |  | Prec | 1\% | 5130 up |
| R547 | 302-104 | 100 k | $1 / 2 w$ |  |  |  |  |
| R550 | 302.823 | 82 k | $1 / 2 w$ |  |  |  |  |
| R553 | 323-295 | 11.5 k | 1/2w |  | Prec | 1\% |  |
| R554 | 308-211 | 12k | 5 w |  | WW | 5\% |  |
| R556 | $323-252$ | 4.12 k | $1 / 2 w$ |  | Prec | 1\% |  |
| R557C | 323-662 | 4.28 k | $1 / 2 w$ |  | Prec | 1\% |  |
| R557E | 323-196 | 1.07 k | $1 / 2 w$ |  | Prec | 1\% |  |
| R557F | 301.182 | 1.8k | 1/2w |  |  | 5\% |  |
| R557G | $323-162$ | $475 \Omega$ | $1 / 2 \mathrm{w}$ |  | Prec | 1\% |  |
| R557H | 301.122 | 1.2 k | $1 / 2 w$ |  |  | 5\% |  |
| R558 | 302-104 | 100 k | $1 / 2 w$ |  |  |  |  |
| R561 | 302-104 | 100 k | $1 / 2 w$ |  |  |  |  |
| R562 | 302-0333-00 | 33 k | $1 / 2 w$ |  |  |  | X5680-up |
| R563 | 323.281 | 8.25 k | $1 / 2 w$ |  | Prec | 1\% |  |
| R564 | 308-211 | 12 k | 5 w |  | WW | 5\% |  |
| R566 | 311.066 | $500 \Omega$ | 2 w | Var |  | $\times 1$ CAL |  |
| R568 | 302-473 | 47 k | $1 / 2 w$ |  |  |  |  |
| R569 | 311 -026 | 100 k |  | Var |  | SWP/MAG | REGIS |
| R570 | 316.470 | $47 \Omega$ | 1/4w |  |  |  |  |
| R571 | 308-266 | 5 k | 5 w |  | WW | 5\% |  |
| $R 572$ | *310-600 | $18 \mathrm{k} / 4.5 \mathrm{k}$ | 7 w |  | WW |  |  |
| R573 | $316-470$ | $47 \Omega$ | $1 / 4 w$ |  |  |  |  |
| R574 | 316-470 | $47 \Omega$ | 1/4w |  |  |  |  |
| R576 | *310.601 | 30 k | 8 w |  | WW | 1\% |  |
| R577 | 302-154 | 150 k | $1 / 2 w$ |  |  |  |  |
| R578 | 316.103 | 10k | $1 / 4 w$ |  |  |  |  |
| R579 | 302-394 | 390 k | $1 / 2 w$ |  |  |  |  |
| R580 | 316-470 | $47 \Omega$ | $1 / 4 \mathrm{w}$ |  |  |  |  |
| R581 | 302-155 | 1.5 meg | 1/2w |  |  |  |  |
| R582 | *310-611 | $18 \mathrm{k} / 3.7 \mathrm{k} / 800 \Omega$ | 6 w |  | WW |  |  |
| R583 | 316-470 | $47 \Omega$ | 1/4w |  |  |  |  |
| R584 | 316-470 | $47 \Omega$ | $1 / 4 w$ |  |  |  |  |
| R585 | 306-224 | 220 k | 2 w |  |  |  |  |



Resistors (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Description |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R669 | 302-393 | 39 k | 1/2w |  |  |  |
| R670A | 306-100 | $10 \Omega$ | 2 w |  |  |  |
| R6708 | 306-100 | $10 \Omega$ | 2 w |  |  |  |
| R671 | 308-155 | $800 \Omega$ | 25 w | WW | 5\% |  |
| R673 | 308.147 | $750 \Omega$ | 25 w | WW | 5\% |  |
| R674 | 302-102 | 1 k | 1/2w |  |  |  |
| R675 | 303-470 | $47 \Omega$ | 1 w |  | 5\% |  |
| R676 | 303-470 | $47 \Omega$ | 1 w |  | 5\% |  |
| R677 | Use 308.065 | 2 k | 25 w | WW | 5\% |  |
| R680 | 324.443 | 402 k | 1 w | Prec | 1\% |  |
| R681 | 324-601 | 264 k | 1 w | Prec | 1\% |  |
| R682 | 302-124 | 120 k | 1/2w |  |  |  |
| R683 | 302.102 | 1 k | 1/2 w |  |  |  |
| R685 | 304-823 | 82 k | 1 w |  |  |  |
| R686 | 302-184 | 180 k | 1/2w |  |  |  |
| R688 | 302.155 | 1.5 meg | 1/2w |  |  |  |
| R689 | 302-225 | 2.2 meg | $1 / 2 \mathrm{w}$ |  |  |  |
| R693 | 302-155 | 1.5 meg | 1/2w |  |  |  |
| R694 | 302.473 | 47 k | 1/2w |  |  |  |
| R697 | 302-824 | 820 k | $1 / 2 \mathrm{w}$ |  |  |  |
| R698 | 302-274 | 270 k | 1/2w |  |  |  |
| R699 | 302-473 | 47 k | 1/2w |  |  |  |
| R700 | 306-100 | $10 \Omega$ | 2 w |  |  |  |
| R701 | 306-100 | $10 \Omega$ | 2 w |  |  |  |
| R703 | 303-470 | $47 \Omega$ | 1 w |  | 5\% |  |
| R704 | 302-102 | 1 k | 1/2w |  |  |  |
| R705 | $303-470$ | $47 \Omega$ | 1 w |  |  |  |
| R706 | Use 308-0282-00 | 1.35 k | 25 w | WW | 5\% |  |
| R707 | 308-102 | 1.25 k | 25 w | WW | 5\% |  |
| R710 | 324.467 | 715 k | 1 w | Prec | 1\% |  |
| R711 | 324.604 | 303 k | 1 w | Prec | 1\% |  |
| R712 | 302-154 | 150 k | 1/2w |  |  |  |
| R723 | 302-105 | 1 meg | $1 / 2 \mathrm{w}$ |  |  |  |
| R726 | 301-0204-00 | 200 k | 1/2w |  | 5\% | X7330-up |
| R727 | 302-105 | 1 meg | 1/2w |  |  |  |
| R728 | 302-684 | 680 k | 1/2w |  |  | 100-7329 |
| R728 | 301-0474-00 | 470 k | Y'2w |  | 5\% | 7330-up |
| R729 | 302-224 | 220 k | 1/2w |  |  | 100-7329 |
| R729 | 301-0224-00 | 220 k | 1/2w |  | 5\% | 7330-up |
| R730 | 302-100 | $10 \Omega$ | 1/2 w |  |  |  |
| R731 | 306-823 | 82 k | 2 w |  |  |  |
| R734 | 316-470 | $47 \Omega$ |  |  |  |  |
| R737 | 308-192 | 5k | 20 w | WW | 5\% |  |
| R741 | 302-104 | 100 k | 1/2w |  |  |  |
| R743 | 307-103 | 2.7 ת | $1 / 4 w$ |  | 5\% |  |
| R744 | 307-103 | 2.7 ת | $1 / 4$ w |  | 5\% |  |
| $\begin{aligned} & \text { R757 } \\ & \text { R758 } \end{aligned}$ | $\begin{aligned} & 302.154 \\ & 315.823 \end{aligned}$ | $\begin{aligned} & 150 k \\ & 82 k \end{aligned}$ | $1 / 2 \mathrm{w}$ $1 / 4$ w |  | 5\% |  |

Resistors (Cont'd)

tFurnished as a unit with R864.

| Resistors (Cont'd) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. |  | Descrip |  |  |  | /N Range |
| R858 | 302-105 | 1 meg | 1/2w |  |  |  |  |
| $R 859$ | 302-471 | $470 \Omega$ | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R861 | 311.026 | 100 k |  | Var |  | GEOMETRY |  |
| R862 | 301-823 | 82 k | 1/2w |  |  | 5\% | 100-1009 |
| R862 | 323-395 | 127 k | $1 / 2 w$ |  | Prec | 1\% | 1010-up |
| R863 | 301-473 | 47 k | $1 / 2 w$ |  |  | 5\% | 100-1009 |
| R863 | 323-356 | 49.9 k | 1/2w |  | Prec | 1\% | 1010-up |
| R864t $\dagger$ | 311-407 | 50 k |  | Var | WW | ASTIGMATISM |  |
| R931 | 302-154 | 150 k | 1/2w |  |  |  |  |
| R932 | 301-394 | 390 k | 1/2w |  |  | 5\% |  |
| $R 934$ | 301-475 | 4.7 meg | $1 / 2 w$ |  |  | 5\% |  |
| R935 | 302.103 | 10 k | 1/2w |  |  |  |  |
| ${ }^{R 936}$ | 302 -102 | 1 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| $R 938$ | 302-102 | 1 k | 1/2w |  |  |  |  |
| $R 939$ | 302-221 | $220 \Omega$ | 1/2w |  |  |  |  |
| R941 | 302-221 | $220 \Omega$ | 1/2w |  |  |  |  |
| R943 | $311-141$ | 2 k |  | Var | WW | CAL AMPL |  |
| R944 | 302-100 | $10 \Omega$ | 1/2w |  |  |  |  |
| R945 | 308.268 | 22 k | 5 w |  | WW | 1\% |  |
| R948 | 315.0682-00 | 6.8 k | 1/4w |  |  | 5\% | X3150-up |
| R949 | 302-274 | 270 k | $1 / 2 \mathrm{w}$ |  |  |  |  |
| R950 | 323-289 | 10 k | 1/2w |  | Prec | 1\% | 100-2889 |
| $R 950$ | 323-0709-01 | 10.048 k | $1 / 2 w$ |  | Prec | 1/2\% | 2890-up |
| R951 | 323-635 | 6.667 k | $1 / 2 w$ |  | Prec | 1\% | 100-2889 |
| R951 | 323.0708 .01 | 6.628 k | 1/2w |  | Prec | 1/2\% | 2890 -up |
| R952 | 323.634 | 1.789 k | 1/2 w |  | Prec | 1\% | 100-2889 |
| $R 952$ | 323-0707-01 | 1.728 k | $1 / 2 w$ |  | Prec | 1/2\% | 2890-up |
| $R 953$ | 323.633 | $801 \Omega$ | $1 / 2 w$ |  | Prec | 1\% | 100-2889 |
| $R 953$ | 323-0706-01 | $800 \Omega$ | 1/2w |  | Prec | 1/2\% | 2890-up |
|  | 323-632 | $452 \Omega$ |  |  | Prec |  |  |
| R954 | $323-0705-01$ | $452 \Omega$ | 1/2w |  | Prec | 1/2\% $\quad 2$ | 2890.14130 |
| R954 | 323-0632-01 | $452 \Omega$ | $1 / 2 \mathrm{w}$ |  | Prec | 1/2\% | 14131-up |
| $\mathrm{R955}$ | 323.631 | 146.1 ת | $1 / 2 \mathrm{w}$ | . | Prec | 1\% | 100-2889 |
| $R 955$ | 323-0704-01 | $146 \Omega$ | 1/2 w |  | Prec | 1/2\% | 2890 -up |
| $R 956$ | $323-630$ | 72.4 ת | 1/2w |  | Prec | 1\% | 100-2889 |
| $R 956$ | 323-0703-01 | 72.4 ת | 1/2w |  | Prec | 1/2\% $\quad 2$ | 2890-14130 |
| $R 956$ | 323-0630-01 | $72.4 \Omega$ | 1/2 w |  | Prec | 1/2\% | 14131-up |
| R957 | 323-629 | $43.1 \Omega$ | Yw |  | Prec | 1\% | 100-2889 |
| $R 957$ | 323.0702 .01 | $43.1 \Omega$ | 1/2w |  | Prec | 1/2\% $\quad 2$ | 2890.14130 |
| $R 957$ | 323-0629-01 | $43.1 \Omega$ | $1 / 2 \mathrm{w}$ |  | Prec | 1/2\% | 14131-up |
| $R 958$ | $323-628$ | $28.6 \Omega$ | $1 / 2 \mathrm{w}$ |  | Prec | 1\% | 100-2889 |
| ${ }^{R 958}$ | 323.0701 .01 | $28.6 \Omega$ | $1 / 2 w$ |  | Prec | $1 / 2 \% \quad 2$ | 2890-14130 |
| $\mathrm{R}^{2958}$ | 323-0628-01 | $28.6 \Omega$ | $1 / 2 \mathrm{w}$ |  | Prec | 1/2\% | 14131-up |
| $R 960$ | 323.636 | 50 k | 1/2w |  | Prec | 1\% |  |
| R962 | 323.627 | 21.4 ת | 1/2w |  | Prec | 1\% | 100.2889 |
| R962 | 323-0700-01 | 21.4 n | 1/2w |  | Prec | 1/2\% 2 | 2890-14130 |
| R962 | 323-0627-01 | $21.4 \Omega$ | $1 / 2 \mathrm{w}$ |  | Prec | 1/2\% | 14131-up |
| R964 | 323-638 | 50 k | 1/2w |  | Prec | 1/4\% | 100-10199 |
| R964 | 323-0638-06 | 50 k | 1/2w |  | Prec | 1/4\% | $10200 \cdot \mathrm{up}$ |
| $\mathrm{R965}$ | 323.637 | $50 \Omega$ | 1/2w |  | Prec | 1/4\% | 100-8849 |
| $R 965$ | 323-0637-06 | $50 \Omega$ | 1/2w |  | Prec | 1/4\% | 8850 -up |
| R969 | 308-242 | . $25 \Omega$ | 5 w |  | WW | 5\% |  |


| Resisfors (Cont'd) |  |  |  |  |  | S/N Range |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix Part No. |  | Description |  |  |  |  |  |
| R1000 | 316-820 | $82 \Omega$ | $1 / 4 \mathrm{w}$ |  |  |  |  |  |
| R1001 | 315-220 | $22 \Omega$ | 1/4w |  |  | 5\% |  |  |
| R1002 | 301.101 | $100 \Omega$ | $1 / 2 \mathrm{w}$ |  |  | 5\% |  |  |
| R1003 | 305-682 | 6.8 k | 2 w |  |  | 5\% |  |  |
| R1004 | $311-086$ | 2.5 k |  | Vor |  | VERT | DC BAL | 100-6729 |
| R1004 | 311-0629-00 | 3 k |  | Var |  | VERT | DC BAL | 6730-up |
| R1011 | 315-220 | $22 \Omega$ | 1/4w |  |  | 5\% |  |  |
| R1013 | 305-682 | 6.8 k | 2 w |  |  | 5\% |  |  |
| R1014 | 301-131 | $130 \Omega$ | 1/2w |  |  | 5\% |  |  |
| R1015 | 315-131 | $130 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |  |  |
| R1016 | 315-300 | $30 \Omega$ | 1/4w |  |  | 5\% |  |  |
| R1017 | 311.258 | $100 \Omega$ |  | Var |  | VERT | GAIN | 100-4749 |
| R1017 | 311-0097-00 | $200 \Omega$ |  | Var |  |  | GAIN | 4750-up |
| R1018 | 305-273 | 27 k | 2 w |  |  | 5\% |  |  |
| R1019 | 308-002 | 1.5 k | 5 w |  | WW | 5\% |  |  |
| R1020 | 316-331 | $330 \Omega$ | 1/4w |  |  |  |  | X940-up |
| R1024 | $301-131$ | $130 \Omega$ | 1/2w |  |  | 5\% |  |  |
| R1025 | 315-131 | $130 \Omega$ | $1 / 4$ w |  |  | 5\% |  |  |
| R1026 | 315-300 | 30 n | $1 / 4 w$ |  |  | 5\% |  |  |
| R1027 | 315-121 | $120 \Omega$ | 1/4w |  |  | 5\% |  | 100.1009 |
| R1027 | 315-471 | $470 \Omega$ | $1 / 4 w$ |  |  | 5\% |  | 1010-up |
| R1031 | 315.512 | 5.1 k | 1/4w |  |  | 5\% |  |  |
| R1032 | 322-092 | 88.7 ת | $1 / 4 \mathrm{w}$ |  | Prec | 1\% |  |  |
| R1034 | 315-100 | $10 \Omega$ | $1 / 4 w$ |  |  | 5\% |  |  |
| R1038 | 301-821 | $820 \Omega$ | 1/2w |  |  | 5\% |  |  |
| R1041 | 315-512 | 5.1 k | 1/4w |  |  | 5\% |  |  |
| R1042 | 322-092 | 88.7 ת | 1/4w |  | Prec | 1\% |  |  |
| R1048 | 301-821 | $820 \Omega$ | $1 / 2 w$ |  |  | 5\% |  |  |
| R1051 | 321.117 | $162 \Omega$ | 1/8 w |  | Prec | 1\% |  |  |
| R1061 | 321.117 | $162 \Omega$ | 1/6w |  | Prec | 1\% |  |  |
| R1069 | 315-361 | $360 \Omega$ | $1 / 4 w$ |  |  | 5\% |  |  |
| R1071 | 315-360 | $36 \Omega$ | $1 / 4 w$ |  |  | 5\% |  |  |
| R1072 | 323-105 | $121 \Omega$ | $1 / 2 w$ |  | Prec | 1\% |  |  |
| R1073 | 301.331 | $330 \Omega$ | $1 / 2 \mathrm{w}$ |  |  | 5\% |  |  |
| R1:74 | 321-073 | 56.2 ת | 1/0w |  | Prec | 1\% |  |  |
| R1076 | 311.442 | $250 \Omega$ |  | Var |  |  |  | 100-15279 |
| R1076 | 311.1223.00 | $250 \Omega$ |  | Var |  |  |  | 15280-up |
| R1077 | 315-163 | 16 k | 1/4w |  |  | 5\% |  | 100-10729 |
| R1077 | 311.0614-00 | 30 k |  | Var |  |  |  | 10730-up |
| R1082 | 323-105 | 1218 | 1/2w |  | Prec | 1\% |  |  |
| R1083 | 301.331 | $330 \Omega$ | $1 / 2 w$ |  |  | 5\% |  |  |
| R1084 | 321-073 | $56.2 \mathrm{\Omega}$ | 1/6w |  | Prec | 5\% |  |  |
| R1087 | 304-122 | 1.2 k | 1 w |  |  |  |  |  |
| R1088 | 305-681 | $680 \Omega$ | 2 w |  |  | 5\% |  |  |
| R1089 | 308-296 | 1.2 k | 5 w |  | WW | 5\% |  |  |
| R1091 | 311-0613-00 | 100 k |  | Var |  |  |  | X10730-up |
| R1104 | 301.270 | $27 \Omega$ | 1/2w |  |  | 5\% |  |  |
| R1105 | 323-102 | $113 \Omega$ | 1/2w |  | Prec | 1\% |  |  |
| R1106 | 311.442 | $250 \Omega$ |  | Var |  |  |  | 100-15279 |
| R1106 | 311-1223-00 | $250 \Omega$ |  | Var |  |  |  | 15280-up |
| R1108 | -310.603 | $600 \Omega / 300 \Omega$ | 3 w |  | WW | 2\% |  |  |
| R1109 | 305.0243-00 | 24 k | 2 w |  |  | 5\% |  | X2340-up |
| R1113 | 315-100 | $10 \Omega$ | $1 / 4 w$ |  |  | 5\% |  |  |
| R1114 | -310-602 | 1 k | $8 w$ |  | WW | 1\% |  |  |
| R1118 | 308-232 | $320 \Omega$ | 5 w |  | WW | 5\% |  |  |
| R1124 | 301-270 | $27 \Omega$ | $1 / 2 w$ |  |  | 5\% |  |  |



Switches (Cont'd)

| Ckt. No. | Tektronix Part No. |
| :---: | :---: |
| SW673 | 260.516 |
| SW858 | 260-209 |
| SW950 260 | 0-536 Use *262-0731-00 |
| SW1000 | 260-601 |
| TK601 | 260-336 |

## Description

S/N Range

| Push |  |
| :--- | :--- |
| Toggle | CRT CATHODE SELECTOR |
| Rotary | AMPLITUDE CALIBRATOR |
| Slide | COMPENSATION |
| Thermal |  |
| Cutout | $150^{\circ} \mathrm{F} \pm 5^{\circ} \mathrm{F}$ |

## Transformers

| T52 | Use | $* 120-0323-01$ | Toroid 2T-8T Bifilar |
| :--- | :---: | :--- | :---: |
| T52 | $* 120-0500-00$ | Toroid 2T-12T Bifilar | $100-6739$ |
| T252 | Use | $* 120-0323-01$ | Toroid 2T-8T Bifilar |
| T252 | $* 120-0500-00$ | Toroid 2T-12T Bifilar | $6740-\mathrm{up}$ |
| T601 | $* 120-307$ | L.V. Power | $100-6739$ |
|  |  |  | $6740-\mathrm{up}$ |
|  |  |  | $100-7979$ |
| T601 | $* 120-0521-00$ | L.V. Power |  |
| T801 | $* 120-308$ | H.V. Power | T980-up |
| T1030 | $* 120.341$ | Toroid 3T Bifilar |  |
| T1104 | $276-541$ | Core, Ferrite |  |

## Electron Tubes

| V24 | 154-187 | 6DJ8 | 100-6239 |
| :---: | :---: | :---: | :---: |
| V24 | *157-0122-00 | 6DJ8, Checked | 6240.7979 |
| V24 | *157-0125-00 | 6DJ8, Checked | 7980-up |
| V91 | 154.040 | 12AU6 | 100-4169 |
| V91 | 154-0040.05 | 8426 | 4170-up |
| V93 | 154.187 | 6DJ8 |  |
| V145 | 154-187 | 6DJ8 |  |
| V193 | 154-187 | 6DJ8 |  |
| V224 | 154-187 | 6DJ8 | 100.6239 |
| V224 | *157-0122-00 | 6DJ8, Checked | 6240-7979 |
| V224 | *157-0125-00 | 6DJ8, Checked | 7980 -up |
| V291 | 154-022 | 6AU6 |  |
| V293 | 154-187 | 6DJ8 |  |
| V345 | 154.187 | 6DJ8 |  |
| V393 | 154-187 | 6DJ8 |  |
| V404 | 154-187 | 6DJ8 |  |
| V494 | 154.187 | 6DJ8 |  |
| V514 | 154-187 | 6DJ8 |  |
| V574 | 154.187 | 6DJ8 |  |
| V584 | 154-187 | 6DJ8 |  |
| V589 | 154-146 | 6197 |  |
| V609 | 154-291 | OG3 |  |
| V624 | 154-043 | 12AX7 |  |
| V634 | 154-022 | 6AU6 |  |
| V637 | 154-202 | 6CW5 |  |
| V647 | 154.202 | 6CW5 |  |
| V664 | 154-414 | $6 \mathrm{BY8}$ |  |
| V677 | 154.056 | 6080 |  |

Electron Tubes (Cont'd)


## CRT Optional Phosphors

| $* 154-0568-01$ | P2 |
| :--- | :--- |
| $*$ | 154-0568-02 |
| *157-0568-03 | P11 |

$+\mathrm{S} / \mathrm{N} 100-2069$ add ${ }^{*} 050-0246$ kit.

## IMPORTANT:

All circuit voltages were obtained with a $\mathbf{2 0 , 0 0 0} \Omega /$ Volt VOM.
All readings are in volts. The voltages were measured with respect to ground unless otherwise indicated by the use of arrows to point out voltage drop.

Waveforms were obtained using a Type 530-Series Oscilloscope with a Type L Plug-In Unit and 10X attenuator probe. An equivalent oscilloscope having a vertical passband of dc to 10 mc or better and equal sensitivity can be used as a test oscilloscope.

Waveform de levels with respect to ground are indicated at the right side of waveform; measured when test oscilloscope AC-DC switch was set to DC.

Waveforms were photographed with test oscilloscope AC-DC switch set to $A C$; vertical deflection factor and Time/Cm switch set to those settings indicated adjacent to waveforms.

In most cases + Ext. AC triggering on the Type 547 1-kc AMPLITUDE CALIBRATOR signal was used. Exceptions: -Int., + Int. and + Line ( 60 cps ) triggering modes were also used; these modes, if used, are indicated above the waveforms.

## NOTE

Number of cycles displayed by waveform when calibrator signal was used as a trigger source depends mostly on the signal repetition rate. Though + Ext. triggering was used, a time difference of 1 msec can occur between waveforms because the test oscilloscope can trigger on a different cycle than the Type 547 and vice versa.

Voltage and waveform measurements are not absolute. They may vary between instruments due to normal manufacturing tolerances, and transistor and vacuum tube characteristics.

The plug-in unit used in the Type 547 Oscilloscope during the voltage and waveform measurements is a Type TU-7 Test Unit. Its front-panel control settings and other conditions are as follows:

| Input Signal | No |
| :---: | :---: |
| Position | Centered |
|  | (Exception: See Vertical |
| Test Function | Amplifier schematic diagram) |

Any letter-series or 1 -series plug-in unit or the TU-2 can be used in place of the Type TU-7 when troubleshooting the Type 547.


* DENOTES PRESRNCE IN UNITS BELOW SN 12480 , THE COMPONENT IS ABSENT.







TYPE 547 OSCILLOSCOPE






## POWER SUPPLY

VOLTAGE READINGS WERE OBTAINED under the following conditions:
LINE VOLTAGE 115 VAC (or Design Center)
INPUT SIGNAL None
'A' AND 'B' TRIGGER INPUT Signal None
'A' AND 'B' TRIGGERING LEVEL ..... ccw
'A' AND 'B' TRIGGERING MODE ..... TRIG
'A' AND 'B' TRIGGERING SOURCE ..... EXT
AMPLITUDE CALIBRATOR ..... OFF
POWER ..... ON
Also see IMPORTANT note on "A or B or External Mode" Block diagram.


Resessocs oenmims
(1) comse subar
(3) CRT circuit

人) - swer triacese
(8) \% swecp treacter


## CRT CIRCUIT

WAVEFORM AND DYNAMIC VOLTAGE READINGS were obtained under the following conditions:

INTENSITY . . . . . . . . . . . . . . . . . . . . . . . cew

POWER . . . . . . . . . . . . . . . . . . . . . . ON

* Voltage reading obtained with associated control set for normal operation. Voltage is dependent on position of the control.

Also see IMPORTANT note on "A or B or External Mode" Block diagram.




## VEKTICAI AMTFITIEK

 conditions:

Oscillóscupe:
POWER . ............ . (IV

Typé IIJ.
INPUT SIGVAL . . . . . . . . . . . . . Nore
VERTICAL POSITION .. ..... Centeiod
TESI FUNCTION . ......... COMMOH! Akル上
 unit Vertical Position control to obtain cero volts reading betwien pins 1 and 3 of the intercormecting plug.

## Also see IMPORIAI-f1 nute un Bloek Lhagram.





TYPE 547 OSCILLOSCOPE


## MAFERENCE DRAWIMG:

(3) verticnl amplifier
(5) ' $C$ ' SWBEP GENERATOR
(6) ' X ' SWAKP TRIGQER
(s) PLUG-IN Connector

SEA PARTS LIST FOR
SEMICONDUCTOR TYPES
Awls Ano stive mumate
WIM Eut ourtive.

"B' SWEER TRIGGER 《>
WAVEFORMS AND VOLTAGE READINGS were obtained under the fol- lowing conditions:
TIME BASE A -
TRIGGER INPUT Signal None TRIGGERING: MODE ........................... . . TRIG
SOURCE ..... EXT
MAIN TIME BASE (B)TRIGGERING:
MODE ..... TRIG
SLOPE ..... ${ }_{\text {AC }}^{+}$
SOURCE ..... EXT
HORIZONTAL DISPLAY ..... B
POWER ..... ON
WAVEFORM Conditions ..... -
'B' TRIGGER INPUT Signal 10 Volts P-P Calibrator
'B' TRIGGERING LEVEL $+45^{\circ}$; knob pushed in'B' TIME/CM1 mSEC
AMPLITUDE CALIBRATOR ..... 10 Volts
QUIESCENT VOLTAGE Conditions
'B' TRIGGER INPUT Signal ..... None
'B' TRIGGERING LEVEL with knob pushed in: Upper Voltage Readings ......... ccw Lower Voltage Readings . . . . . . . . cwAlso see IMPORTANT note on "A or B or External Mode" Block diagram.


TYPE 547 OSCILLOSCOPE
$+$




## 'B' SWEEP GENERATOR

## WAVEFORMS AND VOLTAGE READINGS were obtained under the fol-

 lowing conditions:```
TIME BASE A -
    TRIGGER INPUT Signal ............None
    TRIGGERING:
        MODE .......................... . TRIG
        SOURCE ....................... EXT
HORIZONTAL DISPLAY .............. B
    SINGLE SWEEP Switch . . . . . . . . . . . NORMAL
MAIN TIME BASE (B)
    TRIGGERING LEVEL ............... +45'; pushed in
    TRIGGERING:
        SLOPE ..........................
        COUPLING ....................... AC
        SOURCE ....................... EXT
    BRIGHTNESS ..................... cw
    TIME/CM ...................... . . }1\mathrm{ mSEC
    VARIABLE (TIME/CM) . ............. CALIBRATED
POWER ............................. ON
WAVEFORM CONDITIONS -
    'B' TRIGGER INPUT SIGNAL . . . . . . . . 10 Volts P.P Calibrator
    'B' TRIGGERING MODE . . . . . . . . . TRIG (AUTO for waveforms at
    collectors of Q65 and Q75).
    AMPLITUDE CALIBRATOR
10 Volts
```

```
QUIESCENT VOLTAGE CONDITIONS -
```

QUIESCENT VOLTAGE CONDITIONS -
'B' TRIGGER INPUT SIGNAL ......... None
'B' TRIGGER INPUT SIGNAL ......... None
'B' TRIGGERING MODE ............ TRIG

```
    'B' TRIGGERING MODE ............ TRIG
```

Also see IMPORTANT note on "A or B or External Mode" Block diagram.




## REFERENCE DRAWINGS:

(b) 'B' SWEEP GENERATOR


## DELAY PICKOFF

WAVEFORMS AND VOLTAGE READINGS were obtained under the following conditions:

```
TIME BASE A -
    'A' TRIGGER INPUT Signal . . . . . . . None
    'A' TRIGGERING LEVEL ........... cew
    TIME/CM ...................... . . . . mSEC/CM
    VARIABLE .......................... CALIBRATED
SINGLE SWEEP Switch . . . . . . . . . . . . . NORMAL
MAIN TIME BASE (B) -
    TRIGGERING LEVEL ............... +45'; push in
    TRIGGERING:
        MODE ......................... TRIG
        SLOPE ...........................
        COUPLING ................... AC
        SOURCE ........................ . . EXT
    TIME/CM ....................... . . . . mSEC/CM
    VARIABLE ..........................CALIBRATED
DELAY-TIME MULTIPLIER . . . . . . . . . . . 2.00
POWER .............................. ON
WAVEFORM CONDITIONS -
    'A' TRIGGERING MODE . . . . . . . . . . AUTO
    HORIZONTAL DISPLAY . . . . . . . . . . A DLY'D
    'B' TRIGGER INPUT Signal ........ 10 Volts P-P Calibrator
    AMPLITUDE CALIBRATOR .......... 10 Volts
QUIESCENT VOLTAGE CONDITIONS -
    'A' TRIGGERING MODE ........... . TRIG
    HORIZONTAL DISPLAY ............ B
    'B' TRIGGER INPUT Signal ......... None
```

Also see IMPORTANT note on "A or B or External Mode" Block diagram.


RAFSREMCE PRAMMAS
(6) 'B' SWEEP EENERATOR
() $\times$ ' swisp aenikrator
(13) HORIZONTAL DISPLAY SWITCH

80N

B

DELAY PICKOFF $\langle\widehat{7}$



REFEREMCE DRAWINGS


(3) vertical amplifier
(4) 'B' SWLEP TRIGGER
(9) 'A' SWEKP GEMERATOR

## 'A' SWEEP TRIGGER

## WAVEFORMS AND VOLTAGE READINGS were obtained under the following conditions:

TIME BASE A -TRIGGERING:
MODE ..... TRIG
SLOPE ..... $\stackrel{+}{A C}$
COUPLING ..... AC
SOURCE ..... EXT
MAIN TIME BASE (B) TRIGGER INPUT Signal ..... None
MODE ..... TRIG
SOURCE ..... EXT
HORIZONTAL DISPLAY ..... A
POWER ..... ON
WAVEFORM CONDITIONS
'A' TRIGGER INPUT Signal 10 Volts P-P Calibrator
A' TRIGGERING LEVEL $+45^{\circ}$; knob pushed in
A' TIME/CM ..... 1 mSEC
AMPLITUDE CALIBRATOR ..... 10 Volts
QUIESCENT VOLTAGE CONDITIONS
'A' TRIGGER INPUT Signal ..... None
' $A$ ' TRIGGERING LEVEL with knob pushed in: Upper Voltage Readings . . . . . . . . ccw Lower Voltage Readings . . . . . . . . cw


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WAVEFORMS AND VOLTAGE READINGS were obtained under the fol- lowing conditions:
time base A - TRIGGERING LEVEL $+45^{\circ}$; knob pushed in
TRIGGERING: SLOPE ..... $+$
COUPLING ..... AC
TIME/CM ..... 1 mSEC
VARIABLE ..... CALIBRATED
HORIZONTAL DISPLAY ..... A
SINGLE SWEEP Switch NORMAL
MAIN TIME BASE (B)TRIGGER INPUT SignalNone
TRIGGERING: ..... TRIG
SOURCE ..... EXT
POWER ..... ON
WAVEFORM CONDITIONS
'A' TRIGGER INPUT Signal10 Volts P-P Calibrator
'A' TRIGGERING MODEcollectors of Q265 and Q275).
AMPLITUDE CALIBRATOR ..... 10 Volts
QUIESCENT VOLTAGE CONDITIONS
'A' TRIGGER INPUT Signal ..... None
'A' TRIGGERING MODE ..... TRIGAlso see IMPORTANT note on "A or B or External Mode" Block diagram.




## ALTERNATE SWEEP SWITCHING

WAVEFORMS AND VOLTAGE READINGS were obtained under the following conditions:
TIME BASE A and MAIN TIME BASE (B) -
'A' TRIGGERING LEVEL . . . ......... ccw; pushed in
'B' TRIGGERING LEVEL ............ +45 ${ }^{\circ}$; pushed in
' $A$ ' and ' $B$ ' TRIGGERING SLOPE ..... +
' $A$ ' and ' $B$ ' TRIGGERING COUPLING . AC
'A' TIME/CM . . . . . . . . . . . . . . . . . . . . . 5 mSEC
'B' TIME/CM . . . . . . . . . . . . . . . . . . 1 mSEC
'A' and 'B' VARIABLE (TIME/CM) . . . . CALIBRATED
Single Sweep Switch . . . . . . . . . . . . . NORMAL
DELAY-TIME MULTIPLIER . . . . . . . . . . 2.00
HORIZONTAL POSITION . . . . . . . . . . Centered
VERNIER (HORIZONTAL POSITION) . . ccw
POWER . . . . . . . . . . . . . . . . . . . . . . ON
WAVEFORM CONDITIONS
TRACE ROTATION ................ Fully cw
'A' TRIGGERING MODE . . . . . . . . . . AUTO
'B' TRIGGERING MODE . . . . . . . . . . . TRIG
'A' and 'B' TRIGGERING SOURCE ... LINE (60 cps)
HORIZONTAL DISPLAY* ............ ALT B INTENS BY
'A'/ALT/A DLY'D
*Exception: See waveform at collector of Q454.
QUIESCENT VOLTAGE CONDITIONS -
'A' TRIGGER INPUT Signal . ........ None
TRACE ROTATION . . . . . . . . . . . . . . . 0
' $A$ ' and ' $B$ ' TRIGGERING MODE . . . . TRIG
'A' and 'B' TRIGGERING SOURCE ... EXT
HORIZONTAL DISPLAY ............ . B

Also see IMPORTANT note on "A or B or External Mode" Block diagram.


TYPE 547 OSCILLOSCOPE
c,

F-SWEEP SWITCHING MULTIVIBRATOR + A SWEEP GATE - +__-_ TRACE SEPARATION AMPLIFIER ——_-_



WTM BUT OUTUNE.

REFERENGE DRAWINGS
(3) VERTICAL AMPLIFIER
(5) 'B' SWEEP GENERATOR
6) 'A' SWEEP GENERATOR
12. HORIZONTAL DISPLAY SWITCH
(8) Horizontal amplifier
(1) PLUG-IN CONNECTOR


TERM SWEEP



WAVEFORM AND VOLTAGE READINGS were obtained under the following conditions:

```
MAIN TIME BASE (B) -
    TRIGGERING LEVEL ............. +45'; pushed in
    TRIGGERING:
        MODE ......................... . TRIG
        SLOPE .......................... +
        COUPLING ................... AC
        SOURCE
        EXT
    TIME/CM ...................... . . . mSEC/CM
    VARIABLE (TIME/CM) ............. CALIBRATED
    SWEEP MAGNIFIER ................ XI
    HORIZONTAL POSITION (VERNIER) . . ccw
```

POWER
ON

WAVEFORM CONDITIONS -
'B' TRIGGER INPUT Signal ........ 10 Volts P-P Calibrator
AMPLITUDE CALIBRATOR ........... 10 Volts
HORIZONTAL DISPLAY . . . . . . . . . . . B
SWEEP MAGNIFIER . . . . . . . . . . . . . . XI
HORIZONTAL POSITION .......... Centered

```
QUIESCENT VOLTAGE CONDITIONS -
    HORIZ INPUT Signal . . . . . . . . . . . . . None
    HORIZONTAL DISPLAY . . . . . . . . . . . Ext XI
    HORIZONTAL POSITION:
        Upper Voltage Readings . . . . . . . . ccw
        Lower Voltage Readings . ........ cw
```

Also see IMPORTANT note on "A or B or External Mode" Block diagram.




## SYNC AMP.

WAVEFORM AND VOLTAGE READINGS were obtained under the fol- lowing conditions:
HORIZONTAL DISPLAY ..... B
SINGLE SWEEP Switch ..... NORMAL
MAIN TIME BASE (B)
TRIGGER INPUT Signal None
TRIGGERING LEVEL ..... cw
TRIGGERING SOURCE ..... EXT
TIME/CM ..... $50 \mu \mathrm{SEC}$
VARIABLE ..... CALIBRATED
POWER ..... ON
WAVEFORM CONDITIONS
'B' TRIGGERING MODE ..... AUTO
QUIESCENT VOLTAGE CONDITIONS
'B' TRIGGERING MODE ..... TRIG

Also see IMPORTANT note on "A or B or External Mode" Block diagram.


REFERENCE DRAWINGS:



## CALIBRATOR

WAVEFORM AND DYNAMIC VOLTAGE READINGS were obtained under the following conditions:

## AMPLITUDE CALIBRATOR ............. 10 Volts

POWER ................................ ON

Also see IMPORTANT note on "A or B or External Mode" Block diagram.


## MANUAL CHANGE INFORMATION

At Tektronix, we continually strive to keep up with latest electronic developments by adding circuit and component improvements to our instruments as soon as they are developed and tested.

Sometimes, due to printing and shipping requirements, we can't get these changes immediately into printed manuals. Hence, your manual may contain new change information on following pages.

A single change may affect several sections. Since the change information sheets are carried in the manual until all changes are permanently entered, some duplication may occur. If no such change pages appear following this page, your manual is correct as printed.

## SERVICE NOTE

Because of the universal parts procurement problem, some electrical parts in your instrument may be different from those described in the Replaceable Electrical Parts List. The parts used will in no way alter or compromise the performance or reliability of this instrument. They are installed when necessary to ensure prompt delivery to the customer. Order replacement parts from the Replaceable Electrical Parts List.

## CALIBRATION TEST EQUIPMENT REPLACEMENT

## Calibration Test Equipment Chart

This chart compares TM 500 product performance to that of older Tektronix equipment. Only those characteristics where significant specification differences occur, are listed. In some cases the new instrument may not be a total functional replacement. Additional support instrumentation may be needed or a change in calibration procedure may be necessary.

| Comparison of Main Characteristics |  |  |
| :---: | :---: | :---: |
| DM 501 replaces 7D13 |  |  |
| PG 501 replaces 107 <br> 108 | PG 501 - Risetime less than 3.5 ns into $50 \Omega$. <br> PG 501-5 V output pulse; <br> 3.5 ns Risetime | 107 - Risetime less than 3.0 ns into $50 \Omega$. <br> 108-10 V output pulse 1 ns Risetime |
| $\begin{array}{r} \hline \text { PG } 502 \text { replaces } 107 \\ 108 \\ 111 \end{array}$ | PG 502-5 V output <br> PG 502 - Risetime less than $1 \mathrm{~ns} ; 10 \mathrm{~ns}$ Pretrigger pulse delay | 108-10 V output <br> 111 - Risetime $0.5 \mathrm{~ns} ; 30$ to 250 ns Pretrigger pulse delay |
| $\begin{array}{r} \hline \text { PG } 508 \text { replaces } 114 \\ 115 \\ 2101 \end{array}$ | Performance of replacement equipment is the same or better than equipment being replaced. |  |
| PG 506 replaces 106 | PG 506 - Positive-going trigger output signal at least 1 V ; High Amplitude output, 60 V . <br> PG 506 - Does not have chopped feature. | 106 - Positive and Negativegoing trigger output signal, 50 ns and 1 V ; High Amplitude output, 100 V . <br> 0502-01 - Comparator output can be alternately chopped to a reference voltage. |
| $\begin{array}{r} \hline \text { SG } 503 \text { replaces } 190, \\ \text { 190A, } 190 \mathrm{~B} \\ 191 \\ 067-0532-01 \end{array}$ | $\begin{aligned} & \text { SG } 503 \text { - Amplitude range } \\ & \text { 5 mV to } 5.5 \mathrm{~V} \text { p-p. } \\ & \text { SG } 503 \text { - Frequency range } \\ & 250 \mathrm{kHz} \text { to } 250 \mathrm{MHz} . \end{aligned}$ | 190B - Amplitude range 40 mV to 10 V p-p. <br> 0532-01 - Frequency range <br> 65 MHz to 500 MHz . |
| SG 504 replaces $067-0532-01$ | $\begin{aligned} & \text { SG } 504 \text { - Frequency range } \\ & 245 \mathrm{MHz} \text { to } 1050 \mathrm{MHz} . \end{aligned}$ | 0532-01 - Frequency range 65 MHz to 500 MHz . |
| 067-0650-00 |  |  |
| TG 501 replaces 180, 180A <br> 181 <br> 184 <br> 2901 | TG 501 - Trigger outputslaved to marker output from 5 sec through 100 ns . One time-mark can be generated at a time. <br> TG 501 - Trigger outputslaved to market output from 5 sec through 100 ns . One time-mark can be generated at a time. <br> TG 501 - Trigger outputslaved to marker output from 5 sec through 100 ns. One time-mark can be generated at a time. | 180A - Trigger pulses 1, 10, $100 \mathrm{~Hz} ; 1,10$, and 100 kHz . Multiple time-marks can be generated simultaneously. <br> 181 - Multiple time-marks <br> 184 - Separate trigger pulses of 1 and 0.1 sec; 10, 1, and 0.1 $\mathrm{ms} ; 10$ and $1 \mu \mathrm{~s}$. <br> 2901-Separate trigger pulses, from 5 sec to $0.1 \mu \mathrm{~s}$. Multiple time-marks can be generated simultaneously. |

NOTE: All TM 500 generator outputs are shori-prool. All TM 500 plug-In instrumente require TM 500-Series Power Module.


## SCHIMATIC CORRECTIONS

The serial numbers ( $6740 \& \mathrm{UJ}$ ) given on Diagrams 5 and 9 are not correct. The diagrams with the alove serial number are for instruments serial numbered 12840 and up.

These diagrams also apply to serial numbers between 6740 and 12839 except for the following:

1. Q86 and Q286 are not in these units, the circuitry at this point is like that shown for serial numbers 100 to 6739.
2. In the absence of Q86 and Q286, resistors R91, R97, R297, and R298 are not used.
3. R300 and D291 are not in anstruments below serial number 12839.

In cases of doubt, go by the serial number ranges given in the Electrical Parts List.


[^0]:    "Special feature plug-in units. See your Tektronix calalog for more information on any of these plug-in units.

    * Multiple-frace plug-in unils.
    **Not more than -3 dB af indicated frequencies,

