## INSTRUCTION

MANUAL

## TYPE <br> 3A5

AUTOMATIC/PROGRAMMABLE
AMPLIFIER

## WARRANTY

All Tektronix instruments are warranted against defective materials and workmanship for one year. Tektronix transformers, manufactured in our own plant, are warranted for the life of the instrument.

Any questions with respect to the warranty mentioned above should be taken up with your Tektronix Field Engineer.

Tektronix repair and replacement-part service is geared directly to the field, therefore all requests for repairs and replacement parts should be directed to the Tektronix Field Office or Representative in your area. This procedure will assure you the fastest possible service. Please include the instrument Type and Serial number with all requests for parts or service.

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Fig. 1-1. Type 3A5 Automatic/Programmable Amplifier.

## SECTION 1

## CHARACTERISTICS

## Introduction

The Tektronix Type 3A5 Automatic/Programmable Amplifier is a wideband oscilloscope vertical amplifier plugin unit. Its most distinctive feature is the ability to seek and automatically select an appropriate deflection fat tor for a usable display of an input signal. The Type $: \mathrm{A} 5$ is designed to operate in Tektronix Types $561 \mathrm{~A}, 564,565$ and 567 oscilloscopes (including rack-mount instruments of the same type number), or in the 4 -channel Tektronix Tipe 129 Plug-In Unit Power Supply. It is most often used in the Type 564 or 561A Oscilloscope, with a Type 3B5 A itomatic/Programmable Time Base in the horizontal compartment.

Front-panel operated modes include SEEK: automatic deflection factor seeking; MAN: manually selected deflection factor using the MANUAL VOLTS/DIV switch; ind EXT: external programming of the deflection factor und
input coupling by external circuit closures. The SEEK mode can also be selected by pressing the SEEK button located on the P6030 $10 \times$ Probe, or by command through the PROGRAM CONNECTOR.

A front-panel illuminated readout indicates the deflection factor (correctly scaled with or without the Tektronix P6030 $10 \times$ Probe); the input coupling $A C$ or DC; and uncalibrated deflection factor when the VARIABLE control is not at its detent CAL position. Display amplitude is read from the oscilloscope crt by the operator.

## ELECTRICAL CHARACTERISTICS

The following characteristics apply over an ambient temperature range of $0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$, except as otherwise stated. These characteristics apply only after an instrument warm-up time of at least 20 minutes.

TABLE 1-1

| General Characteristics | Performance Requirements | Supplemental Information |
| :---: | :---: | :---: |
| Deflection Factors | $1 \mathrm{mV} /$ DIV to $50 \mathrm{~V} /$ DIV in 15 calibrated steps selectable by MANUAL VOLTS/DIV switch. $10 \mathrm{mV} / \mathrm{DIV}$ to $50 \mathrm{~V} / \mathrm{DIV}$ in 12 calibrated steps selectable by automatic or external circuits. | Steps are in 1, 2, 5 sequence. <br> Steps are in 1, 2, 5 sequence. <br> Both ranges are automatically scaled $10 \times$ to maximum of $0.5 \mathrm{kV} /$ DIV when P 6030 $10 \times$ Probe is installed on INPUT connector. Other probes will not scale deflection factor. |
| Deflection Accuracy | $\pm 3 \%$ of indicated detlection when VARIABLE control is at CAL detent position. |  |
| Variable Deflection Factor | VARIABLE control redu ces display size to between $55.5 \%$ and $715 \%$ of calibrated size as it is rotated from CAL to full ccw position. As control rotates from CAL position clockwise, display size incr:ases. Full display size altenuation ratio as co itrol is rotated throughout its range is $\geq 2.5$ : | Readout V/DIV turns off and red UNCAL turns on when VARIABLE control is at other than CAL. |
| Input Resistance and Capacitance To Ground | $1 \mathrm{M} \Omega \pm 0.75 \%$ paralleled by $24 \mathrm{pF} \pm 1 \mathrm{pF}$. <br> Type 3A5 ONLY With P6030 Probe (Calculated) | Capacitance measured at 140 kHz . |
| Frequency Response <br> (Amplitude Response not more than $-30 \%$ from 50 kHz calibrated deflection.) $10 \mathrm{mV} / \mathrm{DIV}$ to $50 \mathrm{~V} /$ DIV | DC to $\geq 15 \mathrm{MHz}$ DC to $\geq 14 \mathrm{MHz}$ <br> $\leq 5 \mathrm{~Hz}$ to $\geq 15 \mathrm{MHz}$ $\leq 5 \mathrm{~Hz}$ to $\geq 14 \mathrm{MHz}$ <br> $\leq 5 \mathrm{~Hz}$ to $\geq 15 \mathrm{MHz}$ $\leq 5 \mathrm{~Hz}$ to $\geq 14 \mathrm{MHz}$ | Response measured at $10 \mathrm{mV} / \mathrm{DIV}$. <br> DC coupled. <br> AC coupled. <br> AC-TRACE STABILIZED. |
| $1 \mathrm{mV} / \mathrm{DIV}$ to $5 \mathrm{mV} /$ DIV | DC to $\geq 5 \mathrm{MHz}$ DC to $\geq 5 \mathrm{MHz}$ <br> $\leq 5 \mathrm{~Hz}$ to $\geq 5 \mathrm{MHz}$ $\leq 5 \mathrm{~Hz}$ to $\geq 5 \mathrm{MHz}$ <br> $\leq 30 \mathrm{~Hz}$ to $\geq 5 \mathrm{MHz}$ $\leq 30 \mathrm{~Hz}$ to $\geq 5 \mathrm{MHz}$ | Response measured at $1 \mathrm{mV} / \mathrm{DIV}$. <br> DC coupled. <br> AC coupled. <br> AC-TRACE STABILIZED. <br> AC-TRACE STABILIZED operation is recommended. |

TABIE 1-1 (Cont'd)

| General Characteristics | Performance Kequirements | Supplemental Information |
| :---: | :---: | :---: |
| Risetime (Calculated) $10 \mathrm{mV} / \mathrm{DIV}$ to $50 \mathrm{~V} / \mathrm{DIV}$ <br> $1 \mathrm{mV} /$ DIV to $5 \mathrm{mV} /$ DIV | 23.2 ns 25 ns <br> 70 ns 70 ns | $10 \% \text { to } 90 \%$ <br> Related to sine-wave frequency response at $10 \mathrm{mV} /$ DIV. |
| Transient Response | $\leq 3 \%$ overshoot, rourding, ringing or tilt. | Measured at $10 \mathrm{mV} / \mathrm{DIV}$ with centered 4 div fast step display. |
| Attenuator Compensation | $\leq 3 \%$ peak-to-peak ove rshoot, rounding, ringing or tilt. | Measured af $20 \mathrm{mV} / \mathrm{DIV}$ to $50 \mathrm{~V} / \mathrm{DIV}$ using 1 kHz 10 ns risetime square wave, 4 div display through 24 pF time-constant standardizer. |
| Position Effect On Transient Response | $\leq \pm 5 \%$ overshoot, rolinding, ringing or tilt. | While displaying a 400 kHz 6 div step pulse. |
| Compression or Expansion | $\pm 5 \%$ compression or $\in x$ pansion of 2 division display from crt top tc bottom. | Measured with test oscilloscope at crt pins. |
| Position Control Range | $\geq \pm 6$ div | AC coupled symmetrical 12 div display top and bottom can be positioned past crt centerline. |
| Maximum Input Voltage | 600 volts combined dc plus peak ac. | 500 volts with P6030. |
| Trace Drift With Line Voltage Change | $\pm 0.5$ major div from 105 to 125 volts rms. | At $10 \mathrm{mV} /$ DiV and after one minute at each voltage. |

## Automatic Mode Characteristics

| CRT Displayed Size | 1. When the DISPLAY SIZE control is adjusted for the oscilloscop: in which the Type 3A5 is operating: <br> The CRT display size will be reduced so that top and bottom are $\leq 3.5$ div above and below the graticule certerline when the SEEK button is pressed. <br> 2. The crt display size will not be reduced once the deflection fa:tor of $50 \mathrm{~V} /$ DIV has been reached. | A dc coupled display peak-to-peak amplitude is dependent upon the signal zero de level, polarity, <br> amplitude, <br> crt electrical center and the POSITION control. <br> An ac coupled display peak-to-peak amplitude is dependent upon the signal waveshape, crt electrical center and the POSITION control. <br> A typical sine-wave display peak-to-peak amplitude (when the display zero do level is at the graticule centerline) will be between 2 and 6 DIV. |
| :---: | :---: | :---: |
| Automatic Seeking Time | $\leq 200 \mathrm{~ms}$. | With $100 \mathrm{~V}, 1 \mathrm{kHz}$ signal. |
| Automatic Cycling Time | 2 to 4 seconds. | When SEEK command is continuous. Slightly faster in first 5 seconds. |
| Automatic Seeking Circuit Will Respond to Signals: | DC and 30 Hz sinewaves to 20 MHz . 30 Hz sinewaves to 20 WHz . | DC coupled. <br> AC coupled. Waveform does not have to be sinusoidal above 60 Hz . Some signals below 60 Hz will allow proper operation depending upon waveform. |

## OPERATING CHARACTERISTICS

## General

All front panel controls of the Type 3A5 lexcept the POSITION and VARIABLE controls) operate transistor (ircuits and internal magnetic reed switches that perform the indicated functions. All functions, including positionig (but not the VARIABLE control), can be performed either
manually or programmed externally. The following paragraphs describe which functions operate for each mode.

## Manual Mode (No external program connected)

The Type 3A5 operates as a normal oscilloscope vertical amplifier in the manual mode whenever the MAN pushbutton is illuminated. The manual mode operates when the MAN button is pressed, or whenever the MANUAL VOLTS/

DIV switch setting is changed. An external mode cummand through the PROGRAM connector takes priority civer all other modes.

The operating functions available in manual mode, und the corresponding readout panel indications are listed in Table 1-2.

TABLE 1-2
Manual mode functions and readout

| Functions | Control Used | Readout |
| :---: | :---: | :---: |
| Input Coupling | Three position lever switch |  |
| DC |  | DC |
| AC |  | AC |
| AC-TRACE |  |  |
| STABILIZED |  | $A C$ |
| Deflection Factor Selection | MANUAL VOLTS/ DIV | $1 \frac{\mathrm{~m} \mathrm{~V}}{\text { DIV }} k$ |
|  |  | $50 \frac{V}{\text { DIV }}$ |
| Variable Deflection Factor Selection | VARIABLE control | $\qquad$ <br> V extinguis'les and red UNCAL turns on |
| Deflection Factor $10 \times$ probe scaling | P6030 Probe mechanically depresses unlabeled $10 \times$ scaling switch | WITH PROBE frō $10 \frac{\mathrm{~m} V}{\text { DIV }}$ <br> to |
|  |  | $.5 \frac{\mathrm{k} V}{\text { DIV }}$ |
| Display Positioning | POSITION control | None |

## Automatic Seeking Mode (No external program connected)

Automatic deflection factor selection is obtained by pressing the front panel SEEK pushbutton. Internal circuitry disables the MANUAL VOLTS/DIV switch; the MAN pushbutton lamp goes out; the automatic circuits cycle through the reed switch-operated attenuators to a point determired by the display amplitude; and the SEEK pushbutton is ifluminated. Automatic deflection factor seeking is also uperated by the P6030 Probe SEEK button whenever the probe is connected to the front panel INPUT and REMOTE SEEK connectors.

The Type 3A5 will recycle to seek a new deflection fuctor each 2 to 4 seconds when either SEEK button is hilld closed longer than 5 seconds. The recycle time is slightly faster during the first 5 seconds.

## External Mode

Deflection factor selection can be switched to exterial programming through the Type 3A5 front panel exterral PROGRAM connector. Also, the mode will change to $\cdot x$ ternal when the EXT pushbutton is held depressed. The
mode remains external only by permanent command through the PROGRAM connector. The Type 3A5 deflection factor must be programmed instead of automatically selected when operating in the external mode. Deflection factor selection is by external circuit closures through the external PROGRAM connector. An external mode command through the PROGRAM connector has priority over all other modes. Functions that can be externally operated are listed in Table 1-3.

TABLE 1-3
External Operations Through PROGRAM connector

1. SEEK Mode.
2. EXTernal Mode.
3. Deflection factor, including readout.
4. Input coupling, including readout.
5. WITH PROBE $10 \times$ scaling, including readout.
6. Vertical position (adds to POSITION control).

External operation disconnects the front panel input coupling selector switch and the probe $10 \times$ scaling switch. The oscilloscope $-12.2,-100$, and +125 -volt power supplies are always available through the external PROGRAM connector. See the Operating Instructions for available current.

The external PROGRAM lead voltage and current ratings required of external programming equipment are given at the back of the Operating Instructions section of this manual.

## ENVIRONMENTAL CHARACTERISTICS

## Storage

Temperature- $-40^{\circ} \mathrm{C}$ to $+65^{\circ} \mathrm{C}$.
Altitude-to 50,000 feet.

## Operating

Operating temperature $-0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$.
Operating altitude-to 10,000 feet.

## MECHANICAL CHARACTERISTICS

Dimensions-161/2 inches $\times 4 \frac{1}{4}$ inches $\times 6 \frac{1}{4}$ inches. Weight-5 pounds, net.
Construction-aluminum alloy chassis.
Finish-anodized and silk screened front panel.

## ACCESSORIES

## Standard Accessories

|  | Tektronix <br> Part No. |
| :--- | :--- |
| 1—P6030 $10 \times$ Probe with its acces- <br> sories. | $010-0195-00$ |
| 1—37 pin Connector, male, to mate with |  |$\quad 131-0422-00$

Part No.
010-0195-00

131-0422-00
200-0660-02
070-0500-00

## SECTION 2

# OPERATING INSTRUCTIONS 

## Introduction

The Type 3A5 Automatic/Programmable Amplifier plugin unit is an internally or externally controlled vertical amplifier for Tektronix oscilloscopes Types 561A, 564, 565 and 567 (including rack-mount instruments of same t:pe number). It will also operate in the Type 129 Plug-In IJnit Power Supply. Vertical deflection factor and other functions can be controlled from the Type 3A5 front-panel controls, or through the 37-pin front-panel external PROGRAM connector. The Type 263 Programmer can be connected directly to the Type 3A5 to remotely operate all its functions except the VARIABLE VOLTS/DIV control.
Automatic selection of deflection factor allows the operator to obtain meaningful displays more easily and quickly than is normally possible with hand operated MANLIAL VOLTS/DIV control. The instrument deflection factor is always indicated on an illuminated readout panel. A $111 \times$ scaling factor is included when the Tektronix P6030 111X Probe is connected to the INPUT connector. The mode of operation is always shown by one of three illuminated pushbuttons.

Connection to the external PROGRAM connector is $b$ : $a$ mating male 37 -pin connector supplied with the instrument, or by the Tektronix Type 263 programmer. Detailed external programming information is supplied at the back of this section. Should the user build his own external progrumming equipment, the oscilloscope $-100,-12.2$ and +125 volt regulated power supplies can provide some curient through the PROGRAM connector J-20. Table 2-1 lists the maximum allowable external currents that can be taken through J-20.

TABLE 2-1
J-20 Maximum Power Supply Currents

| Supply | Pin | Current |
| :---: | :---: | :---: |
| $+125-\mathrm{V}$ | 18 | 20 mA |
| $-100-\mathrm{V}$ | 19 | 10 mA |
| $-12.2-\mathrm{V}$ | 1 | 50 mA |

## VERTICAL AMPLIFIER OPERATION

## Manual vs Automatic Selection of Deflection Factor

An oscilloscope's vertical deflection factor is normally selected by manual adjustment of the Volts/Div contiol. This provides a useful display for a particular input $\cdot$ ignal, but any sizable change in signal amplitude is likely to require re-adjustment of the Volts/Div control.

With the Type 3A5 this problem is eliminated by prissing the front-panel SEEK pushbutton and letting the pl.ggin automatically select the correct deflection factor. If using the P6030 $10 \times$ Probe, pressing the probe SEEK button will also cause the Type 3 A5 to automatically select the
correct deflection factor. The deflection factor is automatically scaled to include the P6030 Probe $10 \times$ attenuation. (Other probes or cables with normal size BNC connectors will not cause the Type 3A5 to scale the deflection factor $10 \times 1$.

## Function of Front Panel Controls and Connectors (without external program connected)

REMOTE SEEK A phone jack for connection of an externally operated SEEK switch. Normally used by the P6030 $10 \times$ Probe SEEK circuit. When the probe SEEK button is pressed, both the Type 3A5 and the Type 3B5 seek circuits operate.

When pressed, causes the deflection factor to be controlled by the front-panel MANUAL VOLTS/DIV switch.
When held depressed, switches the control of all front panel operations (except POSITION and VARIABLE volts/div) to the external PROGRAM connector. EXT button is illuminated when external program commands the mode of operation.
When turned, changes the mode of operation from SEEK to manual, and sets the deflection factor to the value indicated between the two black lines marked on the knob skirt. Operates the Type 3A5 deflection factor from $1 \mathrm{mV} /$ DIV through $50 \mathrm{~V} / \mathrm{DIV}$. The MANUAL VOLTS/DIV switch offers a maximum of $10 \times$ gain over the minimum automatically selected deflection factors, with a decreased bandwidth of dc to $\geq 5 \mathrm{MHz}$.

Permits uncalibrated plus and minus changes of each fixed calibrated deflection factor. Has at least 2.5:1 range that provides continuous overlap of calibrated deflection factors.

| POSITION | Permits the display position to be adjusted. Has at least a 12 -division range. (Has about 120-division range when MANUAL VOLTS/DIV switch is at $1,2,0$ ol 5 $\mathrm{mV} /$ DIV.) |
| :---: | :---: |
| OVERSCAN LAMP | (Not labeled) Neon lamp that is illumirated if any part of the display is beyend the display size limits, when deflection factor is between $10 \mathrm{mV} / \mathrm{DIV}$ and 50 V/DIV. The lamp is located just above the POSITION control. When deflection factor is manually operated to 1,2 and $5 \mathrm{mV} /$ DIV, the overscan lamp is $1 / 10$ as sensitive and turns on only when disp'ay is about 45 divisions off screen. |
| INPUT COUPLING SWITCH | Three-position lever switch that sets he input coupling circuit when the mode of operation is either MAN or SEEK. <br> DC: Input connector is directly couped to the input attenuator circuits. <br> AC: Input connector is ac coupled through a $0.04 \mu \mathrm{~F}$ capacitor. <br> AC-TRACE STABILIZED: Input is ac esupled through $0.04 \mu \mathrm{~F}$ capacitor and tetal vertical amplifier is feedback stabilized. Trace drift normal for de operation is canceled and display remains at fised level for long periods. |
| INPUT CONNECTOR | BNC connector for installing input sigial cable or P6030 $10 \times$ Probe. |
| PROBE $10 \times$ SCALING SWITCH | (Not labeled) Small gray pushbutton 10 cated between the input connector and the word INPUT. Special P6030 $16 \times$ Probe BNC connector presses switch in when probe is installed. This chansles readout panel deflection factor indi ation to agree with the probe $10 \times$ atte, uation. |
| DISPLAY SIZE | Screwdriver adjust potentiometer that (i)ntrols sensitivity of the automatic deflection factor-seeking circuit. |
| CAL | Screwdriver adjust potentiometer that cinntrols the vertical amplifier gain so Type 3A5 deflection factor can be set to agiee with the crt deflection factors when changing crt or oscilloscope. |
| VAR BAL | Screwdriver adjust potentiometer for varying the vertical amplifier balance so the display zero do level will remain stationary when turning the VARIABLE contiol. |
| EXTERNAL PROGRAM CONNECTOR | 37 -pin female connector that permits :xternal programming of (1) Deflection Factor; (2) Readout panel; (3) Input Coupling; (4) With Probe, $10 \times$ scaling of deflect on factor readout; (5) Changing mode of operation from internal to external; and (6) changing mode of operation fr.mm external to internal SEEK. The oscilloscepe $-12.2,-100$, and +125 -volt regulated power supplies are also available through |

the PROGRAM connector. Two leads permit override of the front-panel POSITION control.

## Installing the Type 3A5 Into the Oscilloscope <br> CAUTION

## Turn off oscilloscope power while inserting or removing plug-in units.

The Type $3 A 5$ is designed to provide dc to $\geq 15 \mathrm{MHz}$ information to the oscilloscope crt vertical deflection plates. It may be used in either the vertical or the horizontal plugin compartments of the Type 561A or Type 564. It can be used in the vertical compartment of the Type 565. The Type 3A5 may also be used in the four-channel Type 129 Plug-In Unit Power Supply.

Before inserting the plug-in unit, turn the front-panel knurled aluminum locking knob counterclockwise so the locking dog will clear the lower front panel. Press the unit firmly in place for proper interconnection plug mating, then turn the knurled locking knob a few turns clockwise until it is hand tight.

To remove the plug-in unit, turn the knurled aluminum knob a few turns counterclockwise until the locking dog is obviously clear, then pull the unit straight out of the oscilloscope.

## First Time Operation

The following procedure covers a complete first time operation of the Type 3A5 in a Type 561A Oscilloscope. Operation in a Type 564 and Type 565 is essentially the same except for display storage operation of the Type 564.

## INSTALLATION

1. Insert the Type $3 A 5$ into the vertical plug-in compartment of the oscilloscope. Set the oscilloscope INTENSITY control fully counterclockwise. Set the Type 3A5 controls as in 2 below, then turn on the oscilloscope power and allow two or three minutes warm up.
2. Set the Type 3A5 front-panel controls as follows:

| POSITION | Midrange |
| :--- | :--- |
| Input Coupling | DC |
| MANUAL VOLTS/DIV | 10 mV |
| VARIABLE | CAL |
| Mode | MAN |

3. Set the time-base controls for an automatically triggered $5 \mathrm{~ms} /$ div sweep. Set the oscilloscope CALIBRATOR control to 50 mVOLTS .
4. Connect a coax with BNC connectors between the CAL OUT connector and the Type 3A5 INPUT connector. Turn the oscilloscope INTENSITY control for a display of normal brilliance. Set the Type 3A5 POSITION control so the display is centered.

## SET CAL CONTROL

5. If the Type $3 A 5$ was not calibrated in the oscilloscupe in which it is now operating, it is necessary to adjust the CAL control. Vertical deflection accuracies of $\pm 3 \%$ are attained only when the reference signal accuracy is $\pm 0 .: 3 \%$ or better, and the Type 3A5 has been turned on at least 20 minutes. However, familiarization of the Type $3 A 5$ is possible using the oscilloscope CALIBRATOR. With the display as already obtained, adjust the CAL control for exactly five divisions between peaks of the calibrator : ignal. Do not include the trace width in the adjustment, but use the top or bottom of the trace when comparing the display amplitude to the graticule markings.

## Set DISPLAY SIZE Control

6. If the Type 3A5 was not calibrated in the oscillosecpe in which is it now operating, it is necessary to adjust the DISPLAY SIZE control.

## NOTE

Operate the Type 3A5 for at least 20 minutes before adjusting the DISPLAY SIZE control.

Remove the signal and obtain a free run trace. Position the trace above the graticule centerline until the overscan lamp (the small neon lamp located just above he POSITION control) turns on. Note the trace position. Pusition the trace below the graticule centerline until the overscan lamp turns on. Note the trace position.

The trace should have moved further from graticule $c: n-$ ter in one direction than in the other before causing he overscan lamp to light. Position the trace in the direction of the farthest move, and set it exactly 3.5 divisions from graticule center. Using a small screwdriver, adjust the DISPLAY SIZE control so that the overscan lamp blinks periudically. To find the correct DISPLAY SIZE setting, adjust he control so that the overscan lamp lights steadily, then buck it off so the lamp blinks.

Position the trace to the opposite half of the graticale, and note the vertical position at which the overscan la np starts blinking. This position must be no closer than 2.1 divisions from graticule center. This DISPLAY SIZE linit represents maximum allowable error in vertical amplitier balance and crt electrical center. Normally, if the CISPLAY SIZE control is adjusted with the trace 3.5 divisions from center in one half of the graticule, the overscan la np will blink only when the display is 3 or more divisions fr 1 m center in the other half. Fig. 2-1 illustrates the worst-cuse limits of DISPLAY SIZE, in a system which has its elecrical center 0.7 division from graticule center. Since this is the maximum allowable deviation in all oscilloscopes with which the Type 3A5 may be operated, Fig. 2-1 applies to all uses of the Type 3A5.

## SEEK MODE OPERATION

7. Reconnect the coax from the oscilloscope CALIBRATI)R to the Type 3 A5 INPUT connector. Press the MAN mcde button and obtain a centered, stable 5 -division display.

Change the CALIBRATOR control to . 1 VOLT then priss the SEEK button. Increasing the input signal voltage vill deflect the top of the display off the crt screen, then as


Fig. 2-1. Example of minimum display size when system electrical center is +0.7 division from graticule centerline.
the SEEK button is pressed, the display will again be five divisions peak to peak, and the readout will indicate a $20-\mathrm{mV}$ /DIV deflection factor.

Position the display top to more than +3.5 divisions from the graticule centerline and press the SEEK button. The display will drop to two divisions peak to peak with an indicated deflection factor of $50 \mathrm{mV} / \mathrm{DIV}$.

Position the display bottom to more than -3.5 divisions from the graticule centerline and press the SEEK button. The display will change to a straight line with an indicated deflection factor of $50 \mathrm{~V} / \mathrm{DIV}$. This is true only when the Input Coupling is at DC and the signal displayed is positive going.

Change the Input Coupling switch to AC and position the trace to the graticule centerline. Press the SEEK button and the display will be either almost six or slightly greater than two divisions peak to peak, with an indicated deflection factor of either $20 \mathrm{mV} /$ DIV or $50 \mathrm{mV} / \mathrm{DIV}$. The display and deflection factor obtained are determined by the DISPLAY SIZE limits as previously adjusted and checked.

## REMOTE SEEK OPERATION

8. Remove the coax cable from the Type 3A5 INPUT connector and install the P6030 $10 \times$ Probe. Insert the Probe small phono plug into the REMOTE SEEK jack located just under the INPUT connector.

Remove the coax from the CALIBRATOR output connector and change the CALIBRATOR control to 1 VOLTS.

Touch the P6030 Probe tip to the CAL OUT centerpin and press the probe SEEK button. The display will be the same as at the end of step 7 with the same readout, except that the readout panel WITH PROBE light will be on.

## MAN MODE OPERATION

9. With the signal and display as at the end of Step 8, change the MANUAL VOLTS/DIV switch to .1 VOLTS. The mode will change from SEEK to MAN and the display will be slightly greater than one division peak to peak. The readout will not agree with the setting of the MANUAL VOLTS/DIV switch, but will indicate the true deflection factor of 1 V/DIV including the $10 \times$ attenuation of the P6030 probe.

Remove the probe tip from the CALIBRATOR output connector.

## TRACE STABILIZED OPERATION

10. Set the input coupling to $A C$ and position the trace to the graticule centerline. Touch the probe tip to the C CAL OUT centerpin. Press the SEEK button and position the display so the most negative part is -2 divisions from the graticule centerline. Change the input coupling to $A C-$ TRACE STABILIZED. The display will momentarily disappear, and will then return within $\pm 1$ division of its previous $A C$ coupled position. Rapidly move the POSITION control to center the display and note the stabilizing circuit affect upon positioning. The display moves with a rather rubkery appearance when the POSITION control is moved rapidly. This shows the presence of the low-pass filter in the stabilizing circuit. The filter permits only dc and very low frequency feedback around the vertical amplifier to cancel any internal drift signals. Therefore, the display will always remain on the crt, regardless of how long the equipment remains in a set up state before use.

## 1-, 2-, AND 5-MILLIVOLT SWITCH POSITIONS

11. Remove the P6030 Probe. Set the oscilloscope CALIBRATOR control to 20 mVOLTS , the input coupling to $A C$-TRACE STABILIZED and the MANUAL VOLTS/DIV switch to 10 mV . Connect a coax with BNC connectors between the CAL OUT and the Type 3A5 INPUT connectors und center the display with the POSITION control.
12. Set the MANUAL VOLTS/DIV switch to 5 mV . The display rise and fall will double in amplitude, but the RC decay during the flat portion of the calibrator signal will fall farther than at $10 \mathrm{mV} / \mathrm{DIV}$. See Fig. 2-2.

The increased rate of fall is because the trace stabilizing circuit feedback voltage is now 10 times greater than at $10 \mathrm{mV} / \mathrm{DIV}$ with increased low frequency signal attenuation.

DC or $A C$ input coupling at 1,2 , or $5 \mathrm{mV} / \mathrm{DIV}$ will sonetimes permit the display to drift a little. Thus, make measurements at 1,2 , or 5 mV /DIV with the input $A C-T R A C E$ STABILIZED.

## FRONT-PANEL ADJUSTMENTS

Three front-panel screwdriver adjust controls offer the operator the ability to ensure a proper display at all tines. Simple procedures listed below show the value of the three controls: (1) DISPLAY SIZE, (2) CAL and (3) VAR BAL. Proper operation requires that the VAR BAL control always be properly adjusted before adjusting either the [MSPLAY SIZE or the CAL control.

VAR BAL. Turning the front panel VARIABLE control may alter the display zero do level if the VAR BAL is misadjusted. To adjust the VAR BAL control, use the following procedure.

1. Remove any signal from the Type 3A5 INPUT connector. Set the input coupling to DC and the MANUAL VOLTS/DIV switch to 10 mV . Set the VARIABLE conirol to its detent CAL position. Set the POSITION control midrange with the red mark near the word POSITION. Free run the time base.

a. AC display, 10 mV /DIV.

b. AC-TRACE STABILIZED display, $5 \mathrm{mV} / \mathrm{DIV}$.

Fig. 2-2. Normal display difference in ac coupled 60 -cycle calibrator signal.
2. If the trace is off screen, turn the VAR BAL control until it comes on screen. Turn the VARIABLE control fully clockwise and bring the trace near screen center with the VAR BAL control.
3. Turn the VARIABLE control counterclockwise and note which direction the trace moves. Return the VARIABLE control fully clockwise. Adjust the VAR BAL control so the trace moves in the same direction it moved due to counterclockwise rotation of the VARIABLE control. Move the trace about 1.5 times as far with the VAR BAL control as it was moved by full rotation of the VARIABLE control. If necessary, use the POSITION control to bring the trace back on the screen.
4. Turn the VARIABLE control counterclockwise and check which way the trace moves and how far. Repeat adjustment of the VAR BAL control following the VARIABLE control until the trace does not move when the VARIABLE control is turned.

CAL. The front panel CAL control allows the operator to adjust the Type 3A5 overall vertical amplifier gain to calibrate the vertical deflection factors.

Perform the First Time Operation CAL adjust procedure whenever there is doubt about the deflection factor calibration, and always when first placing the plug-in unit into an oscilloscope. The accuracy of the Type 3A5 deflection factors will be related directly to the accuracy of the signal used. In order for the Type 3A5 deflection factors to be within the specified $\pm 3 \%$ limits, the calibrating signal must be accurate to within $0.3 \%$. (The Tektronix Standard Amplitude Calibrator, Part No. 067-0502-00 meets the accuracy requirements.)

## SIGNAL CONNECTION PRECAUTIONS

To ensure valid measurements, certain precautions should be taken when connecting signals to the Type 3A5 INPUT connector. Table 2-2 lists several practical coupling methods, their advantages, limitations and other data. Not included in Table $2-2$ is the Type 3A5 input voltage limit of 600 volts de plus ac peak. The Type 3A5 input circuit is designed to withstand such signals for a few moments at deflection factor ratings as low as $10 \mathrm{mV} / \mathrm{DIV}$. The input voltage limit is set by input circuit insulation and the voltage rating of the input ac coupling capacitor. The P6030 $10 \times$ Probe has a maximum voltage limit of 500 volts dc plus ac peak.

TABLE 2-2
Signal Coupling Methods

| Method | Advantages | Limitations | Accessories Required | Source Loading | Precautions |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1. Open test leads. | Simplicity. | Limited frequency response. Subject to stray pickup that limits use of full sensitivity. | BNC to Banana Jack adapter \{103-0033-00) Two test leads. | $1 \mathrm{M} \Omega$ and 24 pF at input, plus test leads. | Stray pickup. |
| 2. Untermined coax cable. | Full sensitivity. | Limited frequency response. High capacitance of able. | Coax cable with BNC connectors. | $1 \mathrm{M} \Omega$ and 24 pF plus cable capacitance. | High capacitive loading. |
| 3. Terminated coax cable. Termination at 3 A 5 input. | Full sensitivity, total bandwidth. Flat-response , resistive loading. Long cable with uniform response. | Presents R $\mathrm{R}_{0}$ (typically $50 \Omega$ ) loading at end of coax. May need blockin! capacitor to prevent dc loading or damage to termin ation. | Coax cable with BNC connectors. $\mathrm{R}_{\mathrm{o}}$ termination at input. (BNC $50 \Omega$ Termination 011 -0049-00) | $\mathrm{R}_{0}$ plus 24 pF at 3A5 end of coax can cause reflections. | Reflection from 24 pF at input. Dc and ac loading on test point. Power limit of termination. |
| 4. Same as 3 , with coax attenuator at termination. | Less reflection from 24 pF at termination. | Sensitivity is reduced (increased deflection factor). | BNC coaxial attenuators. | $\mathrm{R}_{\text {o }}$ only. | Dc and ac loading on test point. Power limit of attenuator. |
| 5. Tap into terminated coax system. (BNC Tee: UG$274 / \mathrm{U}$ at 3 A 5 input.) | Permits signal to go to normal load. Dc or ac coupling without coaxial attenuators. | 24 pF load ar tap point. | BNC Tee and BNC connectors on signal cables. | $1 \mathrm{M} \Omega$ and 24 pF at tap point. | Reflections from 24 pF input. |
| 6. $1 \times$ Probe. | Full sensitivity. Less capacitance than equal length $93 \Omega$ coax. Convenient small tip. | Limited frequency response. Vcltage derating above 0.5 kHz . | P6011 $1 \times$ passive probe. | $1 \mathrm{M} \Omega$ and $52 \mathrm{pF}(24$ pF of $3 \mathrm{~A} 5+28 \mathrm{pF}$ of probe). | High capacitance loading. |
| 7. $10 \times, 10 \mathrm{M} \Omega$ probe. $100 \times, 10$ $M \Omega$ probe. $1000 \times$ $100 \mathrm{M} \Omega$ probe. | Reduced resistive and capacitive loading; full bandwidth. $1000 \times$ : High voltage measurements. P6030 Remote SEEK. P6015 has $\pm 9 \%$ adjustable attenuation. | $10 \times$ Defl. factor. <br> $100 \times$ Defl. factor. <br> $1000 \times$ Defl. fictor. <br> P6013: 12 kV . <br> P6015: 40 kV . <br> Each probe has certain CW voltage limits. | ```P6030: 10X P6007: 100X P6013 and P6015: 1000\times``` | $\begin{aligned} & \mathrm{P} 6030: 12 \mathrm{pF}, 10 \\ & \mathrm{M} \Omega \\ & \mathrm{P} 6007: \approx 2.1 \mathrm{pF} \\ & 10 \mathrm{M} \Omega \\ & \mathrm{P} 6013: 3 \mathrm{pF}, 100 \\ & \mathrm{M} \Omega \\ & \mathrm{P} 6015: \approx 2.7 \mathrm{pF} \\ & 100 \mathrm{M} \Omega \end{aligned}$ | Check probe frequency compensation. Use square wave frequency less than 5 kHz , preferably 1 kHz . |

TABLE 2-2 Cont'd

| 8. Current Transformer, or clip-on AC current probe. | Current transformer can be permanent part of test circuit. Less than 2.2 pF to test circuit chassis. Measure signal currents in transistor circuits: CT-1 - 100 A pk, CT-2-100 A pk, P6016-15 A pk to pk. is a quick connect probe. | RMS current rating: CT-1 -0.5 A CT-2 - 2.5 A Sensitivity: CT-1 - $5 \mathrm{mv} / \mathrm{inA}$ CT-2 - $1 \mathrm{mv} / \mathrm{nA}$ P6016-Slight reduction of 3A5 bandpass. 1 n $A /$ div to $1 \mathrm{~A} / \mathrm{di} \%$. | CT-1: Coax adapter and BNC termination. CT-2: Nothing extra (perhaps additional coax cable for either transformer). P6016 - 131 amplifier. | CT-1: Insertion; $1 \Omega$ paralleled by about $5 \mu \mathrm{H}$. Up to 1.5 pF . CT-2: insertion; $0.04 \Omega$ paralleled by about 5 $\mu \mathrm{H}$. Up to 2.2 pF . P6016: Insertion; $\approx 0.04 \Omega$ paralleled $\approx 1 \mathrm{pF}$. | Transformer is not a quick-connect device. CT-l: lowfrequency limit about 75 kHz . CT-2: low-frequency limits about 1.2 kHz and is $1 / 5$ th as sensitive as the CT-1. P6016; low frequency limit about 50 Hz . |
| :---: | :---: | :---: | :---: | :---: | :---: |

## INPUT COUPLING

To display both the ac and de components of an appled signal, set the input coupling switch to DC ; to display only the ac component of a signal, set the input coupling to $A C$; to ensure trace stability for long periods of time, set the input coupling to AC-TRACE STABILIZED. In either ac position of the input coupling switch, the dc component of the signal is blocked by a capacitor in the input ircuit. The AC coupled low-frequency response $(-3 \mathrm{db}=$ $70 \%$ of calibrated amplitude) is about 5 Hz when the :ignal source resistance is low. When using a $10 \times 10 \mathrm{M} \Omega$ probe, the low-frequency response is about 0.5 Hz . "he 1,2 , and $5 \mathrm{mV} / \mathrm{DIV}$ AC-TRACE STABILIZED low-frequency response is about 30 Hz whether a probe is used or rot Therefore, some low-frequency distortion of 60 Hz sigrals can be expected at 1,2 and $5 \mathrm{mV} /$ div when operat ng AC--TRACE STABILIZED.

## DEFLECTION FACTOR

The amount of display vertical deflection produced by a signal is determined by the signal amplitude, the ir dicated deflection factor, the attenuation factor of any prabe other than the P6030, and the setting of the VARIAILLE control. Calibrated deflection factors indicated on the readout panel apply only when the VARIABLE control is at its detent CAL position with or without a P6030 1 ( $X$ Probe. When the VARIABLE control is at any other pusifion, the readout V/DIV lamp goes out and the red UNCAL lamp turns on. The VARIABLE control increases the $T_{>}$pe 3A5 deflection factor to above $70 \mathrm{~V} / \mathrm{div}$.

## VOLTAGE MEASUREMENTS

To measure the voltage between two points on a display (such as peak-to-peak ac volts), measure the vertical distance in graticule divisions between the two points c.nd multiply by the readout panel indicated deflection factor. (If the probe is other than the P6030, multiply the indica'ed deflection factor by the probe attenuation.) Be certain the VARIABLE control is at its detent CAL position.

For example, assume the use of a $100 \times$ probe, an irdicated deflection factor of $20 \mathrm{mV} /$ DIV, and a vertical (lisplay of 4 divisions. In this case, 4 divisions $\times 0.02$ volis/ div $=0.08$ volts. This voltage times the probe $10 C \times$ attenuation shows a true peak-to-peak voltage of 8 vo'ts.

To measure the de level at a given point on a wa'eform when using the P6030 $10 \times$ Probe, proceed as follo'vs:

1. Set the input coupling to DC and install the P6030 to the INPUT connector, and the small plug into the REMOTE SEEK jack. Attach the probe ground clip to the chassis of the equipment being checked. Touch the probe tip to the signal source and press the probe SEEK button. Adjust the time base triggering for a valid display.
2. Press the probe PUSH TO GROUND button at the compensating block mounted to the Type 3A5 INPUT connector. Check the zero dc level of the trace (auto or free run time base). If the zero level trace is near the graticule center, position it in a direction away from the ac component polarity and release the grounding button. Again press the probe SEEK button to assure that the automatic circuits offer the largest display within normal limits.
3. Measure the number of divisions between the zero signal trace level and the desired point of the display. Multiply this by the indicated deflection factor to obtain the dc volts of the signal.

## VOLTAGE COMPARISON MEASUREMENTS

In some applications, a set of vertical deflection factors other than the calibrated values need to be used. This is convenient for measuring signals that are multiples of fractional voltages with other than the calibrated deflection factor values.

To establish a set of deflection factors based upon some specific voltage, use the following procedure:

1. Apply the new reference voltage signal to the Type 3A5 INPUT connector and set the MANUAL VOLTS/DIV to obtain several divisions of display. Adjust the VARIABLE control until the display is an exact number of graticule divisions peak to peak. Do not move the VARIABLE control through the rest of this procedure.
2. Divide the true voltage amplitude of the reference signal (in volts) by the product of the number of divisions set in step 1 times the setting of the MANUAL VOLTS/DIV switch. The result is the deflection conversion factor.

$$
\begin{aligned}
& \text { Conversion Factor }= \\
& \quad \begin{array}{l}
\text { Amplitude of reference signal (in volts) } \\
\hline \text { Div deflection } \times \text { MANUAL VOLTS/DIV setting }
\end{array}
\end{aligned}
$$

3. To calculate the true deflection factor at any position of the MANUAL VOLTS/DIV switch, multiply the switch setting by the deflection conversion factor

Deflection Factor $=$ MANUAL VOLTS/DIV setting $\times$ Conversion Factor.

The new set of deflection factor values applies only as long as the VARIABLE control is not moved.

## SPECIAL MEASUREMENTS

Several oscilloscope waveform and time measurements require special uses of the horizontal time-base. Phase measurements made on a Y-T basis use the precision of the time base coupled with the display positioning of the vertical unit. For phase measurements, see the time-base instruction manual, such as the Type 3B5 or Type 3B4.
$X-Y$ operation with the horizontal signal (X-axis) other than a time base can be useful to measure the freuency


Fig. 2-3. External PROGRAM connector leads labeled in relation to their program function. Blank pins have no internal lecids connected.
difference of harmonically-related signals. Use of two Type 3A5 plug-in units for X-Y measurements must be limited to operation in an ambient temperature not over $30^{\circ} \mathrm{C}$, and at a line voltage to the oscilloscope not higher than 117 volts rms (or 234 volts rms if the power supply is wired for the higher line voltage). The limits are necessary due to plug-in unit and oscilloscope heating.

## Exłernal Programming

Production pre-testing of subassemblies in either pulse or sine wave systems can be simplified for the operator by use of external programming to the Type $3 A 5$ and the oscilloscope time-base unit. The following section describes what is required for complete programming of the Type 3A5. All functions are included in the Tektronix Type 263 Programmer, including all facilities to program the Type 3B5 Automatic/Programmable Timebase and auxiliary equipment.

## EXTERNAL CONNECTIONS

All leads that pass through the front-panel external PROGRAM connector J-20 are shown in Fig. 2-3. Each lead is labeled according to its external program function. The connector pins are shown from the front, which is the same view as normally used for making external connections to the rear of the supplied mating connector.

Terminology of programming used in Fig. 2-3 should aid in making external connections. As an example, to program a deflection factor of $50 \mathrm{mV} /$ DIV, it is necessary to ground pins 37 (no probe), 12 ( $10 \mathrm{mV} / \mathrm{DIV}$ ) and $13(\times 5)$. All program ground connections are made through pin 20, the Carry Out GND. The word "carry" indicates that more than one external program can be wired up and connected, and with proper diode isolation (explained below) each program can be switched into operation by one connection to the Carry Out GND lead.

Program logic is of the two state $1 / 0$ type. Each program logic lead is at -12.2 volts for 1 logic, and each lead is at 0 volts for 0 logic. Power supply leads and POSITION control override leads are classified as linear circuits.

External switches must handle current in the 0 logic state. Table 2-2 lists the currents for each pin of J-20.

TABLE 2-2
J-20 Current Ratings

| J-20 Pins | Current in mA |
| :---: | :---: |
| 4 and 37 | 17 |
| 8-9-10-12-13-15-16 | 5 |
| $23-24-26-36$ | 10 |

## MULTIPLE PROGRAM DIODE ISOLATION

If more than one external program is to be used with the Type 3A5, diodes must be used to isolate the inactive programs from the program in use. Fig. 2-4 shows three possible external programs, with the required isolation diodes and switching for simple program selection. The germanium diodes must be able to handle the currents listed


Fig. 2-4. Three external programs with isolation diodes and selection switches.
in Table 2-2. Diodes are available from your Tektronix Field Office. Order germanium diades by part number $152-0075-00$. Order silicon diodes by part number 152 -0185-00. The circled resistors, R, can be either $270 \Omega 2$-uatt composition resistors (Tektronix Part No. 306-0271-00), or indicator lamps, G.E. \#2107D (Tektronix Part Number 150-0046-00).

Fig. 2-4 has heavy lines to indicate program current flow, and to aid in understanding how the diodes disconnect the position override resistors of the inactive program. The :ircled resistors ensure that the position override resistors are disconnected by drawing their current to -12.2 vilts and placing the variable position control ends more negative than the nominal - 6 volts at pins J-20/5 and J-20/7. The PROG SELECT switches disconnect the carry gnd from succeeding programs. If PROG 1 is on, throwing the PR()G SELECT switches of PROG 2 or PROG 3 on will not farallel programs. PROG 1 select switch must be off for PR()G 2 or PROG 3 to operate.
J-20/21 is grounded by any PROG SELECT switch in its ON position. This EXT COMMAND circuit ground prevents returning the Type $3 A 5$ operating mode to internal operation by accidentally pressing the MAN or SEEK buttons

Table 2-3 shows which pins of J-20 to ground, to obtrin proper VOLTS/DIV and readout with and without a $10 \times$ probe. Note that three pins must always be grounded for proper operation. Use of a probe with other than $10 \times$
attenuation is the same as NO PROBE for programming purposes. Refer to Fig. 2-3 and Fig. 2-4 for other J-20 leads and programming functions.

TABLE 2-3
J-20 Pins to Be Grounded To Obtain Deflection Factors Listed.

| VOLTS/DIV | NO PROBE <br> pin 37 | 10 and PROBE <br> pin 36 and |
| :---: | :---: | :---: |
| 10 mV | 1216 |  |

# LOGIC AND CIRCUIT DESCRIPTION 

## Introduction

The Type 3A5 Automatic/Programmable Amplifier circuits provide several ways to obtain a useful crt display ea ily. The plug-in includes the normal vertical amplifier circuits needed to deflect the crt beam, plus circuits and cont ols that allow automatic or external control of the deflection factor, input coupling and mode of operation. This secion of the manual describes first the system (through block diagrams), then the circuits of the Type 3A5.

## LOGIC AND BLOCK DIAGRAM

The system interconnections of the Type 3A5 are shewn fully in the complete block diagram at the back of this manual. The logic description begins with simplified block diagrams that show the general vertical and automatic fortions of the instrument. Circuit interconnections for se een operating modes follow the simplified block diagrams. The seven mode block diagrams are drawn with the blocks in the same order as the complete block diagram.
A simplified block diagram of the most basic blocks of the Type 3A5 is shown in Fig. 3-1. The Type 3A5 inout attenuators are operated by either the MANUAL VOLTS/ DIV control or the automatic circuits. Display size information from the vertical amplifier controls the response of the automatic circuits once they have been put into operation. The two connections between the automatic block and the MANUAL VOLTS/DIV switch block (of Fig. 3-1) are poiver control lines. The automatic control circuits supply - 12.2 volts to the MANUAL VOLTS/DIV switch only during manual mode operation. The MANUAL VOLTS/DIV switch vill change the mode of operation from SEEK to manual any time the switch is turned (provided an external programıner is not connected and operating). The +6.8 volts to the al tomatic block is interrupted as the MANUAL VOLTS/DIV switch travels between detent positions, changing the mode to manual.

Fig. 3-2 block diagram shows more basic interconnecti ns between the automatic circuits and the vertical system. "he connections added to those of Fig. 3-1 are: (1) "W TH PROBE" switch for $10 \times$ scaling of the readout when of erating with P6030 10× Probe; (2) two sets of reed-switcl ed attenuators; (3) the AC-TRACE STABILIZED feedback pith around the vertical amplifier, and (4) the Input Coupl ng switch is shown as feeding information to the readsut circuits.

The diodes in the lines to the two sets of reed switcled attenuators switch out the Automatic circuits when operation is manual; similarly for automatic operation, the MANUAL VOLTS/DIV switch is diode-switched out of operation.

Automatic circuits is the name thus far given to both he mode control circuits and the circuits that set the deflect on factor automatically. Before studying any of the control or automatic deflection factor selection circuits, refer to Fig. 3-3 which shows the complete vertical amplifier block diagre $m$. All the front panel controls that affect the vertical systam are shown.

Fig. 3-3 shows that several functions of the vertical amplifier can be controlled in more than one manner. The functions and their source of control are:

| Function | Controlled By: |
| :---: | :---: |
| Input Coupling | Front-panel three position switch; or external program. |
| Deflection Factor | MANUAL VOLTS/DIV switch; or SEEK auto selection circuits; or external program. |
| With Probe $10 \times$ scaling of readout | By P6030 $10 \times$ Probe connector; or by external program. |
| VARIABLE | Front-Panel only. |
| UNCAL to readout | Front-Panel only. |
| POSITION | Front-Panel; or external program override of front-panel control. |
| CAL | Front-Panel only. |
| DISPLAY SIZE | From front-panel only. Display size information controls SEEK auto circuit selection of deflection factor. |

1, 2, or $5 \mathrm{mV} /$ Front-Panel MANUAL VOLTS/DIV switch DIV Deflection only, changes Output Amplifier gain 10X. Factors

The seven major operating modes are block diagrammed in Fig. 3-4 through Fig. 3-10. Each figure has all the circuit blocks laid out in the same order as used on the complete block diagram at the back of this manual. Interconnections and readout are shown for only those leads that are active for each mode. (The INT-EXT switch indicates that the input coupling, and "with probe" switching can be front-panel or externally controlled.)

Fig. 3-4 and Fig. 3-5 show two manual operating modes. The major difference between the two diagrams is the $10 \times$ probe, the Input Coupling, and the Output Stage $10 \times$ gain. Note that the MANUAL VOLTS/DIV switch receives a $10 \times$ readout scaling command when the P6030 $10 \times$ Probe is used.

Fig. 3-6 shows a simple automatic SEEK mode block diagram with an uncalibrated $10 \mathrm{~V} /$ DIV deflection factor, and no probe. Note that the Mode Control provides -12.2 volts to the two Ring Counters and the $1 \times 110 \times$ Readout Scaler. The +6.8 -volt lead from the MANUAL VOLTS/DIV switch to the Mode Control circuits is the control lead that will change the mode from SEEK to Manual any time the MANUAL VOLTS/DIV switch position is changed (providing there is no external program in operation). The SEEK mode is obtained by pressing the front-panel SEEK pushbutton, or by momentary grounding of the correct external PROGRAM lead (dashed line). A SEEK command pulse goes to the Advance Gate. (Pressing the P6030 SEEK button causes a REMOTE SEEK command pulse to go to both the Advance Gate and the horizontal unit.) The leading edge of the


Fig. 3-1. Type IA5 simplified block diagram.

SEEK command signal is used as a Ring Counter reset pulse to set them both to $\div 1$. If the vertical signal out of the Driver Amp exceeds the voltage set by the DISPLAY $\subseteq I Z E$ control, the Display Comparator Multi will send a posi:ive pulse or a series of pulses to the Advance Gate. If the Advance Gate has received a SEEK Command, negative Advance pulses are sent to the $\div 3$ Ring Counter. Each pulse advances the $\div 3$ Ring Counter to the next state in its cy le, $\div 1$ to $\div 2$ to $\div 5$, each state corresponding to an input attenuator value. After the $\div 3$ Ring Counter reaches - 5 , its next step is back to $\div 1$, and $a \div 3$ Advance Pulse is sent to the $\div 4$ Ring Counter. Pulses to the $\div 4$ Ring Courter advance it one step at a time from $\div 1$ to $\div 10$ to $\div 100$ and to $\div 1000$. If the Display Comparator Multi sends zut enough pulses for the $\div 3$ Ring Counter to reach $\div 5$ at the same time the $\div 4$ Ring Counter reaches $\div 1000$, a $50 \mathrm{~V} /$ DIV Advance Inhibit locks out any more Advance Puses from leaving the Advance Gate (see Fig. 3-9). If the signal out of the Driver Amp still exceeds the voltage set by the DISPLAY SIZE control, the Display Comparator Multi continues to send out pulses, but they are used only to light the Overscan Lamp. The $10 \mathrm{~V} / \mathrm{DIV}$ Deflection Factor of lig. 3-6 required 9 Advance Pulses (after the reset of both ring counters) in order for the Ring Counters to activate the $\div 1000$ and $\div 1$ attenuator reed switches.

Fig. 3-7 is a 20 V/DIV SEEK mode WITH PROBE bluck diagram. The major difference from Fig. $3-6$ is the $10 \times$ Command to the $1 \times 110 \times$ Readout Scaler, and the $\div 1100$ and $\div 2$ attenuators that are activated by the Ring Counters.

Fig. 3-8 connections differ from Fig. 3-7 only in the Input Coupling, and the fact that the VARIABLE control is in its calibrated position. The Deflection Factor is different and shows that the $1 \times 110 \times$ Readout Scaler can turn on more than one readout lamp.

Fig. 3-9 shows signals of the ring counter $\div 1000$ and $\div 5$ stages coupled to the Advance Gate at 50 V/DIV. When both Ring Counters reach their maximum count, an inhibit signal to the Advance Gate stops any more Advance Pulses from reaching the $\div 3$ Ring Counter. If there were no 50 V/DIV inhibit signal, the attenuators next step would be back to $10 \mathrm{mV} /$ DIV $(\div 1$ and $\div 1)$ and the system would not stop cycling until the end of the SEEK command pulse.

Fig. 3-10 is an External Mode block diagram at .5 V/DIV, WITH PROBE, and uncalibrated. Note that the Mode Control sends -12.2 volts to the Ring Counters and the $1 \times 10 \times$ Readout Scaler. Ring Counter input leads are grounded through the External PROGRAM connector, labeled EXT PROGRAM. The Input Coupling is externally controlled, and the $1 \times / 10 \times$ Readout Scaler is externally controlled. The POSITION control can receive override current through the PROGRAM connector if desired.

## CIRCUIT DESCRIPTION

## Attenuators

The attenuators, detailed on diagram number 1 , Section 9 are selected by magnetic coil reed switches. Each attenuator


Fig. 3-2. Basic interconnections between vertical system and automatic system.
is a time constant compensated divider that is corre ttly compensated when its load is $1 M \Omega$ and 24 pF . Fig. -11 shows the basic components of an attenuator, assuming no stray capacitance. The output voltage is equal to the input voltage multiplied by the ratio of the resistor values at dr or low frequencies, and by the ratio of the capacitive reacta ice of the two capacitors at high frequencies. Another way of expressing the same thing is to say the time constant of $R_{1}$ $\times C_{1}$ equals the time constant of $R_{2} \times C_{2}$, and the voltrige attenuation is the same for all frequencies.

Fig. 3-12 shows that the $\div 2$ attenuator output resistor and capacitor (equal to $\mathrm{R}_{2}$ and $\mathrm{C}_{2}$ of Fig. 3-11) consist of $\mathrm{R}_{5} 5 \mathrm{DD}$ in parallel with R70, and C70 in parallel with stray lead capacitance and the vertical amplifier input capacitarice. R55D and R70 in parallel equals $500 \mathrm{k} \Omega$, which, in turn is equal to R55A. This gives the attenvator a ratio of 2 tc 1 . Capacitors C55A and C55B serve only to bring the $\div 2$ attenuator input capacitance up to 24 pF . Without C5.5A and C55B, the system input would be less than 24 pF with the $\div 2$ attenuator in use.

The number of components between the INPUT connector and the vertical amplifier input changes considerably, de-
pending upon what deflection factor is required. The attenuator components sequence (without component numbers) is shown in Fig. 3-13. Fig. 3-13 indicates that the input resistance and capacitance (at the INPUT connector) remains the same regardless of deflection factor, and the input capacitance of each attenuator input section is adjustable. An attenuator probe such as the P6030 $10 \times$ Probe can be used with the Type 3A5 without having to change its compensation as different input attenuators are switched into service.

All attenuator switching is done by magnetic reed switches which are operated remotely by the various circuits. Circuits that can operate the reed switches are shown on the block diagram. They include: (1) the MANUAL VOLTS/DIV switch, (2) the $\div 3$ and $\div 4$ Ring Counters, and (3) the external PROGRAM. External control lead voltage and current requirements are given in the Operating Instructions under External Programming.
The input circuit to the attenuators includes the reed-relay operated AC coupling capacitor, C1. Resistor R1 is placed in series with the reed switch and Cl to limit the discharge current through the reed switch in the event Cl is charged to a high voltage.


Fig. 3-3. Block diagram of the complete virtical amplifier system with simplified automatic circuits.

## Vertical Amplifier

The input grid of the vertical amplifier (at V113) recei'es a standard signal of 10 mV peak to peak for each major division of vertical deflection. This is true for deflect on factors of $10 \mathrm{mV} /$ DIV, through $50 \mathrm{~V} / \mathrm{DIV}$. For deflect on factors of 1,2 , or $5 \mathrm{mV} /$ DIV, the standard input signal to V113 grid is 1 mV peak to peak for each major division of vertical deflection. The total amplifier is symmetrically talanced, with some sections push-pull and some sections pa aphase. The push-pull stages have no common coupling between balanced halves, while the paraphase stages do hove common coupling.

Referring to Fig. 3-3 (or the complete block diagram) he Input Amplifier has a single-ended input to push-pull output voltage gain of approximately 9.5 when the VARIABLE control is at CAL. The gain of 9.5 is from the grid of V113 to the two Delay Line input terminals. The gain of the Dri,er Amplifier is adjustable by the front-panel CAL control. The nominal push-pull voltage gain of the Driver Amplifier (when the crt vertical deflection factor is 20 volts/div) is approximately 5.5. The gain of 5.5 is measured from the two Delay

Line output terminals to the two emitters of Q183/Q383. The Output Amplifier push-pull voltage gain is approximately 41 as measured from the emitters of Q183/Q383 to the plates of $\mathrm{V} 524 / \mathrm{V} 334$. The total gain from V113 grid to the push-pull output at the crt is approximately 2000.

Input Amplifier. The Input Amplifier consists of five balanced stages. The input is a pair of vacuum tube cathode followers. V113 grid receives the standard signal from the input attenuators. V313 receives either a fixed level dc voltage from the VAR BAL control, or a dc feedback signal from the Output Amplifier at V524 plate. The input tubes have large cathode resistors to the -100 -volt supply to stabilize their operation and make their gain nearly unity. R115 and C115 decouple the power supply lead from the input stage cathodes. Since R115 is 47 ohms and C115 is $0.01 \mu \mathrm{~F}$, the two cathodes have no common signal coupling, and the tubes operate independently.

The cathode output impedance of V 113 is not low enough to properly drive the base circuit of Q134, so the second stage is a transistor emitter follower. Q123/Q323 each have relatively large emitter resistors to the decoupled +4.2 -volt


Fig. 3-4.


Fig. 3-5.


Fig. 3-6.


Fig. 3-7.


Fig. 3-8.


Fig. 3-9.


Fig. 3-10.


Fig. 3-11. Basic input attenuator.
supply. L122 and C122 decouple the power supply lead from the emitters and provide the low impedance that i;olates the emitters. Thus Q123 emitter signal is not coup'ed to Q323 emitter.

Thus far in the Input Amplifier, signal voltage is appl ed only to V113 and Q123. There is no signal associated with V313 and Q323. V313 grid is normally fed from the VAR BAL control. The VAR BAL control sets the dc level to V: 13 grid, which is the minus input to the vertical amplifier. The VAR BAL control adjusts the do level of Q334 emitter (through V313 and Q323) to exactly the same voltage tha' is at Q134 emitter. Thus, changing the VARIABLE resistance will not shift the display do level. The other use of V313/Q:23
is discussed under AC-TRACE STABILIZED feedback operation later in this section.

Two diodes located between V313 cathode circuit and Q323 emitter, D315 and D316, protect Q123 and Q134 bases. from large overdrive signals. If V113 cathode voltage rises to about +0.75 volt (about 25 times larger than a normal signal) D316 conducts and places the emitter circuit of Q323 in parallel with V113 cathode. (The output signal of the Input Amplifier reaches its limits before either D316 or D315 conducts.) If V113 cathode voltage falls to about -0.45 volt, D315 conducts and parallels the cathode circuit of V313 across V113 cathode circuit. D315 applies a turn-on signal to Q323 base through R315 (D316 applies a turn-on signal to Q323 emitter) and Q323 then couples some of the overdrive signal to Q334 to limit the unbalanced signal in Q134/Q334 stage.

Q134/Q334 form the first voltage amplifier of the vertical system. The input signal is essentially the same peak-to-peak value through V113/Q123, but is given considerable current gain by the cathode of V113 and the emitter of Q123. Q134/ Q334 is a paraphase amplifier with adjustable emitter coupling to allow gain adjustment. The front-panel VARIABLE control is in the signal path between emitters.

As a positive going signal arrives at Q134 base, PNP transistor Q134 conducts less current. Decreased current causes Q134 emitter to go positive and the collector to go negative. As Q134 emitter goes positive, the VARIABLE circuit couples part of the signal to Q334 emitter in a direction to increase its conduction. As Q334 conduction increases, its collector voltage goes positive. Thus the output of Q134/Q334 is push-pull with only single-ended input. Since the VARIABLE circuit attenuates some of the signal from


Fig. 3-12. Reed switches and attenuator components at either $\mathbf{2 m V / D I V}$ or $\mathbf{2 0} \mathbf{m V} / \mathrm{DIV}$.


Fig. 3-13. Attenuator sections, single or in cascade, identified for each of the 15 calibrated deflection factors.

Q134 emitter to Q334 emitter, Q334 collector signal amplitude is not quite as great as that of Q134 collector. The difference is not great, because the VARIABLE circuit also provides degeneration to Q134. If the resistance value of the VARIABLE circuit is decreased, the collector signal amplit de of both Q134 and Q334 increases. The two $20 \mathrm{k} \Omega$ resis'ors between Q134/Q334 emitters and the decoupled +125 Volt supply keep the stage current essentially constant. The signal gain is stabilized against transistor $\beta$ difference by the preceeding stage low driving impedance. Bypassed $r \in$ sistors R124 and R324 in Q134/Q334 collector circuits provide the proper dc and low frequency collector load impedar ce. R134/R324 allow optimum power dissipation in Q134/Q 334 collectors.

C124 and C324 restore the high frequency response that would be lost if pure resistance were placed between the collector (as a signal source) and the next stage base ( $a$; a signal load). RT40 is a power supply voltage dropping resistor that sets Q143/Q343 base voltage to the correct va've.

Q143/Q343 are isolated emitter followers that prov.de current gain to the signal between Q134/Q334 collector :ircuits and the bases of amplifier Q154/Q354. These emi'ter followers are necessary to maintain the overall amplifier high frequency response.
Q154/Q354 is the paraphase output stage of the In, put Amplifier. R354 provides de signal coupling between Q1:14/ Q354 emitters. Several capacitors and series resistanie/ capacitance networks parallel R354 to provide high trequency compensation to the vertical system. Emitter ret נrn resistors R350/R352 assure constant stage current. The collector circuit of Q154/Q354 drives both the Driver Amplitier and the Signal/Trigger Takeoff Amplifier. These amplifiers
are driven through power compensating resistors R160/R360. The power compensating resistors keep Q154/Q354 collector junction power dissipation within required limits regardless of signal level.

Delay Line. The delay line is a balanced $186 \Omega$ transmission line. Each end is terminated in $186 \Omega$. The input end termination is the $186 \Omega$ series value of R194/R394 (at the Signal/Trigger Takeoff Amplifier input) and the low emitter resistance of Q194/Q394. The power compensating resistors, R160/R360 are not in parallel with R194/R394 due to the very high collector resistance of Q154/Q354.

The Delay Line output is terminated by the $186 \Omega$ series resistance of R166/R366 and the virtual ground input resistance of the Driver Amplifier.

Signal/Trigger Takeoff Amplifier. The Signal/Trigger Takeoff Amplifier input is the common-base stage Q194/ Q394. The stage effectively isolates the base circuits of paraphase amplifier Q204/Q404 from the delay line input termination, and prevents interaction between the Driver Amplifier and the Signal/Trigger Takeoff Amplifier input.

Q204/Q404 is a non-linear paraphase amplifier that has more gain for low level signals than it does for higher level signals. The stage is designed to have increased low level gain required by the change in standard signal level at V113 input grid. When the deflection factor is 1,2 , or $5 \mathrm{mV} /$ DIV, the Signal/Trigger Takeoff Amplifier receives $1 / 10$ as much signal per crt division as at $10 \mathrm{mV} / \mathrm{DIV}$ and up. The stage gain is offset upward at low levels by diodes D204/D404 and C404. Without any signal, D204/D404 are conducting and they place C404 in parallel with the normal emitter signal coupling resistor R202. As a positive 0.5 -volt signal is
applied to the base of Q204, and a negative 0.5 -volt signal the base of Q404, D204 remains in conduction; howeter, D404 is reverse biased and stops conducting. This is because the charge on C404 takes the cathode of D404 positive while Q404 emitter is going negative. However, if the push-pull signals to the bases of Q204/Q404 are not greater thalı a total of 0.4 volt, neither diode will cease conducting, and C404 will remain diode-connected across R202, making the stage gain higher than for larger signals.

The collector signal of Q404 is de coupled to emitter tollower Q213. The emitter voltage of Q213 is slightly negalive with respect to ground. To bring the output voltage near ground with only small attenuation, R216 and R218 appl: a small positive offset to the output signal. C216 couples high frequencies around R216. R214 is a parasitic suppression resistor.

Driver Amplifier. The Driver Amplifier is a paraphise feedback amplifier (usually called an Operational Amplifer) that drives the Output Amplifier and provides Display Size Information to the automatic circuits. The input bases of Q174/Q374 are a virtual signal ground due to negative feedback applied from the output back to the input. The feedback current is nearly equal in magnitude, and is opposite in polarity to the input current. The result is that essentially no signal voltage appears at the input bases, implying a virtual signal ground. Since the input bases are a very low impedance, more than one signal current can be injected or withdrawn to alter the amplifier output voltage. This is dune without affecting the amplifier's ability to amplify normal signals. Thus, the POSITION control injects or withdrciws current at the Driver Amplifier input to position the crt display.

The input signal current to the Driver Amplifier is appled through the Delay Line and the Delay Line terminating resistors to the base circuit junctions of Q174 and Q374. Assume that a positive voltage signal appears at the Delay Line pin I and a negative voltage signal appears at pin H . Q174 base current increases its collector current. Q374 decreases its collector current. Q174/Q374 emitters are fied directly together to a single return resistor, so the paraphase voltcige gain of these two transistors is very high. Q174/Q374 collector signals receive current gain from emitter followers Q183/Q383 and are then metered back to the input base circuit junctions through R179/R183 to Q174, and through R379/R383 to Q374. When the output voltage signal is great enough for the signal current through the feedback resistors to almost equal the input signal current, Q174/Q374 no longer see the signal and they stop changing current. Fart of the feedback current is shunted away from Q174/Q:174 by the CAL control. The stage gain is adjusted by changing the feedback current by the CAL control which does not change the feedback resistance.

The emitter follower dc return circuit is through R178/R378. These resistors also shunt some of the signal current from the input bases.

Display Size information is diode coupled from the Driver Amplifier output through D188 or D388 to the Display Cr,mparator Multi. Only negative-going signals cause D188 or D388 to conduct; thus, the push-pull Driver Amplifier output signal is converted to single-ended negative-going information. The voltage at which D188 or D388 conduct is set by the Display Size control and the Display Comparator Multi.

Output Amplifier. The Output Amplifier is a combination transistor-vacuum tube amplifier with high voltage gain. The push-pull input signals arrive through T501 to the emitters of common base stages Q504/Q514. T501 assures that the two signals arrive with identical time relationship, even if a minor phase difference exists out of the Driver Amplifier. T501 also inserts a small loss in the signal path, providing parasitic suppression.

Common base amplifiers Q504/Q514 each carry about 17 mA current which passes through the Driver Amplifier output transistors Q183/Q383. Voltage levels are included on the diagram in Section 9. Q504 and Q514 are both feedback amplifiers with feedback applied from the output tube cathodes to the individual transistor bases.

Assume that a negative voltage signal arrives at Q504 and a positive voltage signal arrives at Q514. Q504 reduces its current and Q514 increases its current. As Q504 collector voltage goes negative, the conduction of V524 is reduced. The output voltage to the crt goes positive, and V524 cathode goes negative. V524 cathode is directly coupled to Q504 base, so the negative cathode signal becomes inverse feedback and increases Q504 current again. Q504 current is not increased as much by V524 cathode signal as it was reduced by the Driver Amplifier signal, because the cathode of V524 changes less voltage than the grid changed. Therefore, Q504 receives a turn off signal equal to the difference between its emitter and base voltage changes. D524 (and D534) assure that Q504 (and Q514) have sufficient emitter to collector voltage for proper operation.

V524/V534 are paraphase-connected with about $50 \Omega$ (R518) between cathodes. Thus the Output Stage receives push-pull signals and acts on them in a push-pull balanced fashion. The stage cathode current passes through R521 and R522 to the -12-Volt supply.

When operating at 1,2 , or $5 \mathrm{mV} /$ DIV, the input coupling switch (SW610) causes L515 to close SW515 and parallel less than $3 \Omega$ across R518. Several frequency compensating networks are also placed across R518 to keep the bandwidth as great as possible at the increased gain. SW5I5 changes the Output Amplifier gain 10X. T524 and T534 are parasitic suppression loss networks.

The plates of V524/V534 include double peaking coils L526 and L536. The plate load resistors are R526 and R536. R528 reduces the +300 -Volt supply voltage to limit the plate dissipation in the output tubes. This lowers the output voltage below that which provides proper crt deflection plate voltage (it is low enough to cause defocusing). Therefore, Zener diodes D546 and D556 offset the output voltage (and signal) positively to the required level of about +187 volts at center screen. R546 and R556 provide current to the Zener diodes to assure that they remain at a fixed 62 volts drop. C546 and C556 bypass any Zener diode noise and assure that high frequencies are not attenuated.

## AC—TRACE STABILIZED Operation

AC-TRACE STABILIZED operation of the overall vertical amplifier places a dc and low-frequency feedback circuit from the plus output plate circuit of V 524 to the minus input grid of V313. The feedback is large in magnitude, causing the whole vertical amplifier to be an operational amplifier with a de gain much less than unity. Fig. 3-14 is a simplified


Fig. 3-14. AC-TRACE STABILIZED operational amplifier circuit.
diagram showing the feedback and POSITION control cismponents. Fig. $3-15$ shows the circuit connections in greater detail. Feedback resistor R520 is bypassed by C530 to assure that only low frequency signals leave the physical area of the Output Amplifier. The feedback information is cablect to the Control Board for connection with other components. The signal and feedback values included in Fig. 3-14 are for operation at $10 \mathrm{mV} /$ DIV to 50 VOLTS/DIV. Operation at to $5 \mathrm{mV} /$ DIV provides ten times as much feedback due to the Output Amplifier operating at $10 \times$ gain.

Feedback current through R530 is equaled by curient through R311 and R309 so that their common junction is a virtual signal ground. R308 and C308 in parallel with C306 establish a long time constant to the feedback to assure it is dc and low frequencies only. The feedback network chariges the current feedback to about $109 \mathrm{mV} / \mathrm{DIV}$, almost 11 times the standard input signal fed to the amplifier plus input. This amount of feedback would be sufficient to make the overall vertical amplifier do gain zero, except that the inside l.oop gain is approximately 2000 . Thus the actual dc gain urider stabilized feedback conditions is about 0.025 instead of zero. This very low de gain assures that the crt trace will renain stable for long periods of time regardless of drift signals within the amplifier loop.

With a total vertical amplifier de closed loop gair of 0.025 , normal positioning currents injected at the Diver Amplifier input will not allow control of the crt trace k.osition. Therefore, R309, in addition to opposing R530 feedk.ack signal, also provides offset current to the feedback current so the trace can be positioned. Position affect of the cortrol is approximately one half its normal affect when operation is not feedback-stabilized.

## AUTOMATIC CIRCUITS

Some of the automatic circuits have been diagrammed on more than one page of the diagrams in Section 9. The duplication includes interconnections, and is done to help the reader gain understanding of the instrument in the least amount of time.

## Mode Control Circuits

The Mode Control Circuits are physically divided between the Automatic Card and the Control board. Drawings Number 4 and 5 in Section 9 show all the control circuits. Number 4 is the MODE CONTROL AND READOUT CONNECTIONS with part of the Control Board and Automatic Card circuits combined in one drawing with the Readout Board bulbs. Number 5 is the complete AUTOMATIC CARD.

The mode of operation is controlled by grounding the proper lead associated with Q624/Q654/Q664 diagrammed on Drawing Number 4. A simplified mode control circuit is shown in Fig. 3-16 joining the physically separated mode control transistors to the proper control relays. The two control relays, L622 and L612 operate as follows:

1. MANUAL operation, both L612 and L622 energized by Q624.
2. SEEK operation, L612 energized by Q664.
3. EXT operation, neither relay energized.

Fig. 3-16 shows that L612/SW612 (the INT-EXT SELECT relay) supplies a ground return circuit for both the Input Coupling switch SW610, and the With Probe switch SW70.


Fig. 3-15. Position control and AC-TRACE STABILIZED connections.


Fig. 3-16. Simplified mode control circuits.

Thus $L 612$ is energized for both SEEK and MAN mode operation. L622/SW622 (the MANUAL POWER or AUTO/EXT POWER relay) supplies - 12.2 volts to the MANUAL VOLIS/ DIV switch SW80 during MAN mode operation only. It provides -12.2 volts to the Automatic Card for both SEEK and EXT mode operation. Details of each operation mode foll. Jw .

SEEK mode operation begins by grounding pin Jl؛-22 or pin JT5-21 by either the SEEK button or through the REMOTE SEEK jack or through the external PROGRAM connector J20-34. Momentarily grounding either of these three points will turn Q664 on. See Fig. 3-17. (The scime grounding action will operate the SEEK MULTI explained below.) Q664 conducts current through the SEEK bulb and the Internal-External control relay L612, allowing the Irput Coupling switch SW610 and the $1 \times 110 \times$ With Probe c)mmand switch SW70 to operate normally. Q664 also drims current through the biasing network of Q624 so that Q524 is held cutoff. Q664 is held in saturated conduction by base current through R666/D666/D664; base current is apprisximately 4.5 mA .

The voltage at the un-operated SEEK button (Fig. 3-17) of -6.0 volts is due to current through the resistance divider R660/R661/R662. As shown, D662 is reverse-biased. Grounding the anode of D661 would let R661/R662 apply turr-on base current to Q664 through D662. Likewise, grouncling the anode of D660 will also apply turn-on base curren to Q664.

EXT Mode operation requires a continuous ground connection at the base circuit of Q654 through the exteınal PROGRAM connector J20 at pin 21. See Fig. 3-18. Grounding the collecior circuit of Q654 (by pressing the EXT pushbutton) allows external mode operation only as long as the button is held depressed. When J20-21 is grounded, Qí54 conducts to saturation drawing current through R630 and the EXT readout bulb. Q654 a'so draws current through R666 and R626 to assure that Q664 and Q624 are held cui off. With only Q654 conducting, neither control re'ay, L612 nor L622, has any current flow and operation of the Type 3A5 must be controlled through the External PROGR $4 M$ connector.

MAN Mode operation begins by first releasing any external program and then grounding the collector cir =uit of Q624. See Fig. 3-19. Grounding the collector circui: of Q624 is done by pressing the MAN pushbutton. At hat time curreni through D624 and D668 assures that Q664 tırns off. With both Q654 and Q664 cut off, Q624 biasing network automatically applies turn-on current to Q624 holcing it saturated. Q624 conducts current through the MAN kulb and through both control relays L612 and L622. Q624 cilso conducts current through R666, biasing Q664 to cutoff. Dól 4 assures that the collector circuit of Q664 is not pulled dc.wn by Q624. During internal SEEK operation, MAN MCDE operation is assured when changing the MANUAL VOLIS/ DIV switch position because its 3 R section momentarily interrupts the +6.8 -volt power to Q664 biasing netw.rrk. The result is that Q664 stops conducting and with both Q664/Q654 collector circuits at +6.8 volts (through B620/ B621), Q624 is turned on for manual mode operation.

Q664 SEEK Mode bias network is shown in detail in Fig. 3-20. Note that D662 does not conduct when the modi: is SEEK and the SEEK button is not pressed. The bias network for Q624 is similar to that shown in Fig. 3-20. D664/D. 66
provide the necessary voltage drop from the junction of R665/D663 so Q624 conduction assures that Q664 base is reverse biased (Fig. 3-20C).

## SEEK Multi

The SEEK multi (See Fig. 3-21) is a monostable multivibraior that drives the Advance Gate and supplies a reset pulse to the Ring Counters. The SEEK multi transistors, Q674 and $Q 684$, do not conduct current in the quiescent state. Quiescent conditions are conirolled by six resistors in a multiple divider between ground and minus voltages. Resistors R674/R673/R675/R678 establish -7.5 volts at their junction with germanium diodes D675/D678. D678 conducts 0.42 mA through $\mathrm{R} \in 79$ to the -100 -volt supply. D675 conducts 0.933 mA through R676 to the -100 -volt supply. The cathode of D678 sets the emitter of Q676 to -7.7 volts, and the cathode of D675 sets the base of Q674 to -7.7 volts. Q674 does not conduct any collector current with the zero bas conditions. Since Q674 does not conduct, R682 in its collector circuit has no voltage drop across it and thus Q684 base emitter junction has zero bias. Q684 does not conduct with the zero bias conditions. All diodes shown in Fig. 3-21 are listed in Table 3-1 with their conduction conditions marked.

## TABLE 3-1

SEEK Multi Diode Conduction
( X means conduction)

| Diode | Quiescent | SEEK button pressed | Multi conducting | REMOTE SEEK pressed |
| :---: | :---: | :---: | :---: | :---: |
| D660 | OFF | OFF | OFF | $X$ |
| D661 | OFF | $X$ | OFF | OFF |
| D669 | $X$ | OFF | OFF | OFF |
| D672 | OFF | X | OFF | X |
| D673 | OFF | $X$ | OFF | X |
| D674 | OFF | OFF | OFF* | OFF |
| D675 | X | OFF | OFF | OFF |
| D678 | X | OFF | OFF | OFF |
| D684 | OFF | X | X | $X$ |
| D689 | OFF | X | OFF | OFF |

*D674 protects C674 if Q674 emitter goes positive.
When either the SEEK button or the REMOTE SEEK button is momentarily pressed, the following action takes place:

1. Q674 base receives turn on current through R671/D672. Q674 collector conducts current and applies several mA of turn on current to Q684 base. Q684 collector rises positive and Q674 base receives regenerative turn on current through R672/R686/C672. Both transistors saturate.
2. Q674 conduction causes its emitter voltage to rise positively and decrease the charge on C674. See Fig. 3-22 and 3-23. As the emitter rises positive, so does the base. C672 signal current to Q674 base increases C672 charge slightly. R672/R686/C672 continue to apply turn on current to Q674 base until Q674 collector voltage rises to about -6.7 volts. (Q674 is still saturated.) At this point the positive side of


Fig. 3-17. Typical SEEK Mode control circuit conditions.

Logic and Circuit Description-Type 3A5


Fig. 3-18. Typical EXT Mode control circuit conditions.


Fig. 3-19. Typical MAN Mode control circuit conditions.


Fig. 3-20. Mode control bias network conditions.


Fig. 3-21. SEEK multivibrator quiescent voltage and current conditions.


Fig. 3-22. Q674 base and emitter signals when SEEK button is momentarily pressed. (Initial - 8-volt level differs from Fig. : $\mathbf{i - 2 1}$ -7.7 volts due to $10 \times$ probe loading.)


Fig. 3-23. Q674 collector and base signals.

C672 has reached about -1.5 volts and the turn on current to Q674 base through R672/R686 falls below the level where Q674 can remain in saturation.
3. As Q674 comes out of saturation, its collector voltcige rises positively until R682/R684 reduce the turn on current to Q684 and it starts to reduce its collector current. As Q684 reduces its current, R689 pulls its collector negative. As the collector goes negative, R686/C672 apply a regenerative turn off signal to Q674 base and both transistors stop conducting.
4. R689 pulls R686/C672 back to their original level and the base of Q675 returns almost to its original level. However, C674 gains its charge back through the large value of R679. This means an interval of about two seconds is requied before Q674 emitter returns to its original level, which prevents immediate recycling by the SEEK button. It is the pusitive signal from Q684 that is the SEEK COMMAND signal to the rest of the automatic circuits.


Fig. 3-24. Q674 emitter and base signals over a nine second period. SEEK button was held pressed.

When either the SEEK button or the REMOTE SEEK bution is held depressed, the SEEK multi will automatically recy-le as shown in Fig. 3-24. Note that the current through R6;1/ D672 causes the base-emitter voltages of Q674 to graducilly rise about 2 volts from the single cycle or quiescent values.

## Advance Control

The Advance Control circuits are so named because they combine information from several sources to control he number of advance pulses sent to the Ring Counters. When advance pulses are sent to the ring counters from he Advance Control circuits, the reed switched attenuators change the deflection factor.

Sources of information to the Advance Control Circuits

1. SEEK Command pulse from Q684. (See Fig. 3-25 ond Diagram 5 in Section 9.)
2. Display Size de level from the DISPLAY SIZE Contiol.
3. Display Size information from the vertical Driver Amplifier.
4. $50 \mathrm{~V} / \mathrm{DIV}$ inhibit signal from the Ring Counter $\div 5$ and $\div 1000$ stages.

Quiescent conditions in the circuit are:

1. Q714 and Q724, Display Comparator Multi transistors, are both cut off.
2. The Display Size dc reference level to the Display Comparator Multi is about -2.6 volts at the anode of D706.
3. Q743 emitter follower Advance Gate prevents any signal from turning on Q754 Gated Advance Pulse Amplifier. Q743 is controlled through D740/D743 negative OR gate by either the SEEK Multi or the 50 V/DIV inhibit from the Ring Counters.
4. Q743 Overscan Amplifier is saturated.
5. The Display Size voltage information from the vertical Driver Amplifier depends upon the display. If the crt beam exceeds plus or minus 3.5 divisions from electrical center, the base of Q714 (Display Comparator Multi input) will be taken sufficiently negative to cause Q714 to draw current. The Display Comparator Multi will free run and turn on the Overscan Lamp, but will not pass signals to the Ring Counters until a SEEK Command pulse arrives at Q743. An operation description of each circuit follows:

Display Comparator Multi. The quiescent de voltage at Q714 emitter is set by current through R714, D705 and D706 and the DISPLAY SIZE control. (See Fig. 3-25.) D706 sets C714 most positive potential, but disconnects the low impedance DISPLAY SIZE control if C714 and the emitter of Q714 try to go more negative than the quiescent level. Both D705 and D706 provide temperature compensation to Q714.

As Q714 starts to conduct current (point \#1 of waveforms of Fig. 3-25) its collector voltage begins to rise positive. Q724 base comes out of cutoff after Q714 collector rises about 2 volts. As Q724 starts to conduct, its collector goes negative and couples a negative regenerative turn on signal to Q714 base. Q714 and Q724 both saturate quickly. Q714 remains saturated during the time attenuator reed bounce occurs, and so is insensitive to bounce voltages. Current through R712 and R710 quickly take some of C714 charge and transfer it to C723. As C723 charges, Q714 base becomes reverse biased, and the regenerative action starts in reverse, turning Q714 and Q724 off rapidly. During the time Q714 was conducting, C714 let Q714 emitter fall about - 1.5 volts below its quiescent level (point \#2 of waveforms of Fig. 3-25). As Q724 collector rises positive to cutoff, C723 drive to Q714 base is limited by D710.

The waveforms of Fig. 3-25 were taken while the Display Comparator Multi was free running. The free run action was caused by positioning the trace 4 divisions from the graticule center. Note that Q714 emitter voltage following point \#2 rises slowly and the multi is off longer than it is on. The slow rise is due to C 714 charging through R 714 . As soon as Q714 emitter rises to a level where the base-emitter voltage will again cause it to conduct, the Display Comparator Multi flips and both transistors again saturate.

The Display Comparator Multi thus sends positive pulses to Q754, the Gated Advance Pulse Amplifier.

Overscan Amplifier. The base of Q734, the Overscan Amplifier, is directly coupled to Q724 collector. When Q724 is cut off, R726 applies about 0.125 mA turn-on current to


Fig. 3-25. Advance control circuits.

Q734 base. Q734 is thus quiescently saturated. Whene er the Display Comparator Multi develops Advance Pulses, Q734 is turned off during the time Q724 is conducting. The collector circuit of Q734 rises positive toward +125 volts. At about +75 volts B 736 the Overscan Lamp fires and m mediately returns the voltage level to about +55 volts, he normal holding potential for the neon bulb. C732 couples part of the output voltage back to Q734 base to limit he rate of collector voltage rise, and thus limit high frequelıcy signals from being coupled to the input attenuators. Qi34 saturates each time Q724 turns off. Thus the Overscan La:np is pulsed on and off whenever it is illuminated.

Advance Gate. The Advance Gate (see Fig. 3-26) cinnsists of Q743, Q754 and associated diodes. It is the Advance Gate that permits Advance Pulses to pass to the Ring Counters whenever the SEEK button is pressed.

Assume the deflection factor is $50 \mathrm{~V} /$ DIV; that a signal of 10 volts peak to peak is applied to the INPUT connector; and that the input coupling is AC. The display will be $1 / 5$ division peak to peak and cannot be read with any accurocy. Press the SEEK button and the display will change tc 5 divisions peak to peak. The sequence of events that takes place to set the deflection factor to $2 \mathrm{~V} / \mathrm{DIV}$ is:

1. The SEEK multi output step raised the emitter of Q.' 43 from -11 volts to -0.9 volt. The leading edge of the SEEK Command was used as a reset pulse to the Ring Counters, and they changed the deflection factor to $10 \mathrm{~m} \cdot \mathrm{~V} /$ DIV. The signal to the vertical amplifier input is now :'00 times the value it will be.
2. The Display Comparator Multi changes state immediately. The Overscan Lamp lights. The base of Q754 recei res enough turn-on current through R570 to cause it to saturate and send a -12.2 volt Advance Pulse to the $\div 3$ Ring Counter. The $\div 3$ Ring Counter does not respond to the first advance pulse because the ac coupled Reset Pulse enegy lasts long enough to override the Advance pulse.
3. The Display Comparator Multi and Q754 put out another advance pulse. This time the $\div 3$ Ring Counter advances to its $\div 2$ state and actuates the 20 mV /DIV deflection factor. The signal to the vertical amplifier is now 100 times what it will be.
4. The Display Comparator Multi continues to cycle until the $\div 3$ and $\div 4$ Ring Counters set the deflection factor to 2 V/DIV. At that time the signal to the vertical amplifier is such that the Display Comparator Multi stops sending pulses to Q754 and the Ring Counters. The SEEK Commeind remains up for several more milliseconds, and then drops to inhibit Q743/Q754.

50 V/DIV Inhibit. The conditions are slightly different if the display zero dc level is above or below the Display Comparator Multi trip level. If the Display Comparator multi receives a constant turn-on signal it continues to send positive pulses to Q754 and the deflection factor will cycle to 50 VOLTS/DIV whenever the SEEK or REMOTE SEEK buttons are pressed. To prevent advancing the Ring Counters fast 50 VOLTS/DIV back to $10 \mathrm{mV} / \mathrm{DIV}$, two Ring Counter output signals are diode-connected back to the Advance Gate through D745 and D746. The signals are the $\div 3$ Ring Counter $\div 5$ state output and the $\div 4$ Ring Counter $\div 1100$ state output.

The 50 V/DIV Inhibit diode switching operates in the following manner (see Fig. 3-26). When the attenuator $\div 1000$ and $\div 5$ coils, $L 30$ and L60, are not energized, D745 and D746 anodes rest at zero volts. A small current $1 / 2$ mA per diode) flows through them and the coils to the -100 volt supply through R745. If one of the two attenuators is energized, the current through R745 switches to pass 1 mA through one diode and the other diode is reverse-biased. If both attenuators are energized, the anodes of both diodes drop to -12.2 volts and R745 current passes through D743 taking the base of Q743 sufficiently negative to inhibit Q745 from sending any more advance pulses to the $\div 3$ Ring Counter. Thus D740 and D743 form a negative AND gate such that either diode can couple a turn-off signal to Q743 and inhibit advance pulses.
Another diode, D684 in the collector lead of SEEK Multi transistor Q684 (see Fig. 3-26) assures proper deflection factor selection when there is no signal and the trace is at a position that will not trip the Display Comparator Multi. D684 sets the SEEK COMMAND pulse plus voltage to -0.9 volt. This sets the anode of D740 (by current through R743) and the base of Q743 to - 0.3 volt, sufficiently negative that D743 is not turned on. If D743 were to turn on and change the $1 / 2 \mathrm{~mA}$ current in either D745 or D746, L30 or L60 magnetic flux change would couple enough energy to the attenvator reed switch to be seen by the vertical amplifier and cause the no-signal deflection factor to be $20 \mathrm{mV} /$ DIV instead of $10 \mathrm{~V} / \mathrm{DIV}$.

## Ring Counters

The $\div 3$ Ring Counter receives Advance Pulses, changes state, directly energizes attenuator reed coils, and sends a $\div 3$ Advance Pulse to the $\div 4$ Ring Counter. The $\div 4$ Ring Counter directly energizes attenuator reed coils and drives the $1 \times 110 \times$ Readout Scaler. Both ring counters will reset to an initial condition whenever a positive reset pulse arrives through C801 to the base circuits of both Q814 and Q854. See Fig. 3-27 and drawing number 5 during the following discussion.

Each ring counter can be described as a set of saturating transistors that are biased and interconnected in a manner that allows only one to conduct at a time. Coupling circuits allow an incoming negative advance pulse to turn off the conducting transistor. The next transistor is turned on by the collector signal from the turned off transistor. All signals are ac coupled.

A cycle of operation begins with the arrival of a reset pulse, and proceeds as follows:

1. The leading edge of the SEEK command signal is ac coupled through C801 to the base circuits of Q814 and Q854. Both transistors turn on to saturation.
2. An advance Pulse arrives at the $\div 3$ Ring Counter and tries to turn Q814 off, but the reset pulse lasts long enough to leave Q814 on.
3. Diode D826 turns Q824 off and D836 turns Q834 off in the $\div 3$ Ring Counter. In the $\div 4$ Ring Counter, D866 turns Q864 off, D876 turns Q874 off and D886 turns Q884 off.
4. Q814 collector current includes current through D814/ L45, R814, D815/R841, D826/R826, D836/R836 and R819 through germanium diode D819 and R812/R816. D819 is


Fig. 3-26. Advance Gate interconnections and signals.
conducting so that the next negative Advance Pulse will turn Q814 off.
5. The base voltage of Q814 is about - 11.5 volts; the collector voltage is -12 volts. Base current is through R8। $2 /$ R816. Current through R816 reverse biases D812 and D 816 . Current through R816 reverse biases D812 and D816. Current through D802/R802 (at reset input) reverse biases D804.
6. The base voltage of the other $\div 3$ Ring Counter transistors is about -13.3 volts due to Q814 current through D826 and D836. The same conditions exist in the $\div 4$ Ring

Counter. The anode of D826 is at about - 11.7 volts; thus, current through R821 and R822 sets Q824 base negative from its emitter and keeps it cut off. With Q824 collector at 0 volts, D829 is reverse biased 13.3 volts so that the -12.2 volt Advance Pulse does not affect Q824 base.
7. After the reset pulse decays, and as the second Advance Pulse arrives, C819 couples the signal to Q814 base and turns it off. As Q814 collector stops conducting current, R814 and L45 pull the collector voltage to ground. D45 clamps L45 inductive backswing. C822 couples the positive going signal to Q824 base and Q824 turns on to saturation. Q824
collector goes to -12 volts and D816 keeps Q814 off and D832 keeps Q834 off.
8. The 3rd Advance Pulse turns Q824 off, and Q824 turns Q834 on.
9. The 4th Advance Pulse turns Q834 off and Q834 turns Q814 on. The signal coupling from Q834 collector to Q814 base is through C812 diagrammed with Q814 biasing nistwork.
10. As Q814 turns on, D815 couples the $\div 3$ negative Advance signal to Q854 base and turns it off. Q854 then tuins Q864 on in the same manner as earlier described when Q814 turned Q824 on.

During manual mode, the MAN/AUTO select switch SW622 turns off the - 12.2 -volt power to the Ring Counter and the Readout Scaler circuits.

Each Ring Counter transistor can be turned on by exterrial command through the external PROGRAM connector. A positive pulse or a ground connection to the correct pin of J20 will turn on the desired transistor, and thus the desired attenuator. See the Operating Instructions for programming details. The external ground connection applies turn on current to the base of the selected Ring Counter transistors through resistors R810, R820, R830, R850, R860, R870 and R880. External connections must be removed before the Type 3A5 can be operated for the SEEK mode.

## Readout Scaler

The Readout Scaler is a set of four saturating emiter follower transistors with diode input control. The emit'er followers act as switches to turn on the Readout Board decimal, zero, K and m bulbs. Bulb current is limited by R935 or R939. Whether or not the emitter follower(s) condict is determined by both the $\div 4$ Ring Counter and the unlabeled front-panel "with probe" switch SW70.

There are eight possible control conditions shown in Figues $3-28$ through 3-35. The figures show the current paths for each possible condition, both bulb current and lockout current. An example of lockout current is shown in Fig. 3.30 where none of the $\div 4$ Ring Counter current turns on a Readout Scaler emitter follower. All of Q864 is "locked olit" and bypasses all scaler emitter followers. When reading Figures 3-27 through 3-34, note that the $\div 4$ Ring Counter transistors are numbered out of numerical sequence.

Fig. 3-27 is the only figure with voltage included. All other figures will have similar voltages for the portion carrying bulb current, and similar voltages for the portion carrying lockout current.

## Power Supplies

Power for the Type 3A5 operation comes from the oscilloscope. Power supply interconnections, and two low voltage supplies within the Type 3A5 are diagrammed on drawing \#6 of Section 9.
The oscilloscope power supplies are capable of operating
with various current loads, depending upon the plug-in units in use. To keep each supply in regulation, some plug-in units place shunt resistors across the oscilloscope regulator circuits. Diagram \#6 indicates which leads of the Type 3A5 are used for supplying regulated current to the Type 3A5 circuits, and which leads are the shunt return circuits for the oscilloscope. P11 pins $10,15,16$ and 23 are the regulated supply leads to the Type 3 A5 circuits. Pins 6, 20 and 22 are the shunt return leads to the oscilloscope power supplies.

Power supply leads that serve more than one part of the Type 3A5 have signal isolation networks to decouple the various circuits. For instance the +125 volt supply enters the Type 3A5 at P11 pin 15, goes directly to the Vertical board and the Output Amplifier. The supply is then cabled to the Control board where R110 and C110 decouple the control and automatic and external circuits from the vertical circuit. R636 is the power supply shunt resistor. The output side of R110/C110, is labeled +125 V (DCPD), indicating the lead is decoupled from the preceding circuits.

Three additional voltages are provided by circuits within the Type 3A5. +75 volts for the Vertical Amplifier Input stage; +6.8 volts for readout lamps, relay coils and some control circuits; and +4.2 volts regulated for the Vertical Amplifier and control circuits.
+75 Volt Regulator. Q108, physically located on the Control board, and diagrammed on drawing \#2, is an emitter follower. Q108 collector supply is the +125 -volt supply. The base voltage is set at approximately +75 volts by the resistive divider, R106 and R107. Q108 emitter resistance to ground is the plate circuit of V113 and V313. Thus, Q108 emitter provides +75 volts (at a sufficiently low impedance) to the input stage plate circuits.
$\mathbf{+ 6 . 8}$-Volt Supply. The +6.8 -volt supply is a simple four-diode bridge rectifier and an electrolytic capacitor. D422 A, B, C, and D rectify the oscilloscope 6.3 -volt ac voltage, and C422 is the filter capacitor. The supply output voltage is directly related to the power line voltage. It is not regulated, because its major use is for readout lamps and relay coils.
$\mathbf{+ 4 . 2 - V o l t ~ R e g u l a t o r . ~ A ~ s t a b l e ~}+4.2$ volts is provided by Q423 and Q424 to several of the transistor circuits of the Type 3A5. The regulator source is the unregulated +6.8 volt supply. The circuit consists of an emitter follower (Q423) with an inverse feedback amplifier (Q424). Q423 emitter output voltage is divided by R426 and R427 to provide the feedback signal to Q424 base. The low-voltage end of the divider is the oscilloscope regulated -12.2 -volt supply. The -12.2 volts is the reference voltage that sets the +4.2 volts output value.

Assume the circuit to be operating. The load current reduces, causing the output voltage to rise positive. Q424 base receives part of the positive change, Q424 collector current increases changing the voltage drop across R422 and taking Q423 base negative. The negative signal at Q423 base takes the output voltage back to its original value. Thus the supply output voltage remains essentially constant with only a few millivolts of 120 Hz ripple.


Fig. 3-27. $\div 3$ and $\div 4$ Ring Counter collector voltages related to VOLTS/DIV readout. Coupling sequence and components are identified.


Fig. 3-28. Readout Scaler current رraths for $10,20,50 \mathrm{mV} / \mathrm{DIV}$, no P6030 Probe.


Fig. 3-29. Readout Scaler current paths for .1, .2, .5 V/DIV, with P6030 Probe.


Fig. 3-30. Readout Scaler current paths for .1, .2, . 5 V/DIV, no P6030 Probe.


Fig. 3-31. Readout Scaler current paths for 1, 2, 5 V/DIV, with P6030 Probe.


Fig. 3-32. Readout Scaler current paths for 1, 2, 5 V/DIV, no P6030 Probe.


Fig. 3-33. Readout Scaler current puths for 10, 20, 50 V/DIV, with P6030 Probe.


Fig. 3-34. Readout Scaler current paths for 10, 20, 50 V/DIV, no P6030 Probe.


Fig. 3-35. Readout Scaler current puths for .1, 2, .5 kV/DIV, with P6030 Probe.

## SECTION 4

## MAINTENANCE

## Introduction

This section contains maintenance instructions for the Tektronix Type 3A5, and includes preventive maintenance, troubleshooting hints, and corrective maintenance.

## PREVENTIVE MAINTENANCE

Preventive maintenance consists of cleaning, visual ins eection, lubrication and, if needed, recalibration. Prevertive maintenance is generally more economical than corrective maintenance, since preventive maintenance can usually be done during idle periods at a time convenient to the i,ser. The preventive maintenance schedule established for the instrument should be based on the amount of use and the environment in which the instrument is used.

Cleaning. The Type 3A5 should be cleaned as oftel as operating conditions require. The oscilloscope side panels provide some protection against dust accumulating in the interior of the instrument, but a small amount of dust is brought in by circulating air. Operation without the ide panels in place is not recommended for internal temperaiure control reasons.

Dirt on the circuit components prevents efficient heat dissipation and may cause component overheating. Clean the instrument by loosening the accumulated dust with a dry, ioft paint brush. Remove the loosened dust by vacuum anc//or dry, low-pressure compressed air (high-velocity air can dismage some components). Hardened dirt and grease may be removed with a cotton-tipped swab or a soft cloth dimpened with water and a mild detergent solution (such as Kelite or Spray White). Abrasive cleaners should not be u:ed.

## CAUTION

Do not permit water to get inside controls or shaf, bushings. Store the instrument in a dust-tigh, covering when not in use.

Lubrication. The life of potentiometers and rotary swite ies is lengthened if they are properly lubricated. Use a clean ng type lubricant (such as Cramoline) on shaft bushings, pl sgin connector contacts, and switch contacts. Lubricate he switch detents with a heavier grease (Beacon grease IVo. 325 or equivalent). The necessary materials and instructi ins for proper lubrication of Tektronix instruments are contair ed in a component lubrication kit which may be ordered $\mathrm{fr}, \mathrm{m}$ Tektronix. Order Tektronix Part No. 003-0342-00.

Visual Inspection. After cleaning, the instrument sho sld be carefully inspected for such defects as poor connecticns, damaged parts, and improperly seated tubes or transisters. The remedy for most visible defects is obvious; however if heat-damaged parts are discovered, determine the cause of overheating before the damaged parts are replaced. Otherwise, the damage may be repeated.

Tube and Transistor Checks. Periodic preventive maintenance checks consisting only of removing the tubes and transistors from the instrument and testing them in a tester
are not recommended. The circuits within the instrument provide the only satisfactory means of checking tube and transistor performance. Defective tubes or transistors will usually be detected during recalibration of the instrument. Details of in-circuit tube and transistor checks are given in the troubleshooting procedures later in this section.

Recalibration. To ensure accurate measurements, the instrument calibration should be checked after each 500 hours of operation or every six months if the instrument is used intermittently. The calibration procedure is helpful in isolating major troubles in the instrument. Moreover, minor troubles not apparent during regular operation are frequently revealed and corrected during recalibration. Complete calibration instructions are contained in Section 6.

## CORRECTIVE MAINTENANCE

Troubleshooting. If the instrument is not operating, attempt to isolate the trouble by a quick operational and visual check. Make sure that any apparent trouble is actually due to a malfunction within the Type 3A5 and not due to improper control settings or a fault in associated equipment.

Operate the controls to see what effect, if any, they have on the trouble symptoms. The normal or abnormal operation of each control helps in establishing the nature of the trouble. The normal function of each control is listed in Section 2 of this manual.

If t'ie trouble cannot be located by means of front-panel checks, remove the oscilloscope side panel and check voltages and waveforms against those presented in the circuit descriptions and schematics, starting with the power-supply connections.

## Trouble Symptoms

Three specific vertical amplifier troubles can be located by their symptoms as viewed on the crt trace.

1. If Q143 and Q343 (see Fig. 4-1) are operating with very low $\beta$ (between 5 and 10 ), the crt will exhibit compression of a signal at either or both the crt top and bottom. The POSITION control has limited effect upon the display position. The de voltages for a centered display are altered for the whole vertical amplifier beginning at Q134 and Q334 collectors.
2. If Q404 in the Signal/Trigger Takeoff Amplifier is shorted, an internal trigger signal of low amplitude is still sent to the time-base. Triggering becomes difficult with one division peak-to-peak signals. The dc voltage of the vertical amplifier are unbalanced for the whole amplifier beginning at Q134 and Q334 collectors.
3. The Output Stage tubes are of frame-grid construction. If a grid wire pops loose and shorts to the screen and suppressor grids, the POSITION control can position a free-run trace from the crt center to either the top only or the bottom only. The two preceding transistors (on the same side of the


Fig. 4-1. Vertical Amplifier board transistor (and rube) locations with signal flow and phase noted.
amplifier as the bad tube) will probably be either shortect or open. For instance, if V524 fails this way, check and change Q183 and Q504.

Automatic circuit troubles usually fall in the complete failure category and can be located with normal voltage und signal tracing techniques.

## Transistor Checks

Transistors should not be replaced unless they are acturilly defective. Transistor defects usually take the form of the transistor opening, shorting, or developing excessive leaka،ge. To check a transistor for these and other defects, use a trimsistor curve display instrument such as a Tektronix Type 575. However, if a good transistor checker is not readily availatle, a defective transistor can be found by signal-tracing, by making in-circuit voltage checks, by measuring the transistor forward-to-back resistance using proper ohmmeter resistarice ranges, or by using the substitution method. The location of all transistors is shown in the parts location figures later in this section.

To check transistors using a voltmeter, measure the emitter-to-base and emitter-to-collector voltages and determine if the voltages are consistent with the normal resistances and currents in the circuit (see Fig. 4-2).

To check a transistor using an ohmmeter, know your ohinmeter ranges, the currents they deliver, and the internal bitttery voltage(s). If your ohmmeter does not have sufficient resistance in series with its internal voltage source, excessive current will flow through the transistor under test. Exce:ssive current and/or high internal source voltage may permanently damage the transistor.


Fig. 4-2. In-circuit voltage checks NPN or PNP transistors.

## NOTE

As a general rule, use the $\mathrm{R} \times 1 \mathrm{k}$ range where the current is usually liminted to less than 2 mA and the internal voltage is usually $11 / 2$ volts. You can quickly check the current and voltage by inserting a multimeter between the ohmmeter leads and measuring the current and voltage for the range you intend to use.
When you know which ohmmeter ranges will not harm the transistor, then use those ranges to measure the resistance
with the ohmmeter connected both ways as given in Table 4-1.

TABLE 4-1
Transistor Resistance Checks

| Ohmmeter Connections ${ }^{1}$ | Resistance Reading That Can Be Expected Using the $R \times 1 \mathrm{k}$ Range |
| :---: | :---: |
| Emitter-Collector | High readings both ways (about 60 k to around 500 k ). |
| Emitter-Base | High reading one way (about 200 k or more). Low reading the other way (abcut $400 \Omega$ to 2.5 k ). |
| Base-Collector | High reading one way (about 500 k or more). Low reading the other way (abcut $400 \Omega$ to 2.5 k ). |

${ }^{1}$ Test prods from the ohmmeter are first connected one way to the transistor leads and then the test prods are reversed (connected the other way). Thus, the effects of the polarity reversal of the voltage applied from the ohmmeter to the transistor can be observed.

If there is doubt about whether the transistor is good, : ubstitute a new transistor; but first, be certain the circuit voltages applied to the transistor are correct before making the substitution.

When checking transistors by substitution, be sure that the voltages on the transistor are normal before making the substitution. If a transistor is substituted without first checking out the circuit, the new transistor may immediately be damaged by some defect in the circuit.

## CAUTION

Be careful when making measurements on live circuits. The small size and high density of components used in this instrument result in close spacing An inadvertent movement of the test probes, or the use of oversized probes may short between circuits

## Parts Identification

Identification of Switch Wafers. Wafers of the MANLIAL VOLTS/DIV switch shown on the circuit diagrams are numbered from the first wafer located behind the detent section of the switch to the last wafer. The letters F and R indicate whether the front or the rear of the wafer is used to perferm the particular switching function. For example, the designation 2 R printed by a switch section on a schematic identilies the switch section as being on the rear side of the secend wafer when counting back from the front panel.

Wiring Color Code. The wiring in the Type 3A5 is cclor coded to facilitate circuit tracing. In the case of power-supply leads, the color code indicates the voltage carried, with the widest stripe denoting the first signficant figure. Table 4-2 lists the color combinations and the voltages indicated by the colors.

All leads that clip to the permanently mounted etch-wied circuit boards are color coded. The color code of each lead, and the pin lettering is shown in parts location figures later on in this section.

Resistor Coding. The Type 3A5 uses a number of very stable metal film resistors identified by their gray ba:kground color and color coding.

TABLE 4-2
Power Supply Color Coding

|  | Supply | Color Code |
| :--- | :--- | :--- |
| +300 | Orange/Black/Purple on White |  |
|  | +125 | Brown/Red Black on White |
| -12.2 | Brown/Red/Black on Tan |  |
| -100 | Brown/Black/Brown on Tan |  |

If the resistor has three significant figures with a multiplier, the resistor will be EIA color coded. If it has four significant figures with a multiplier, the value will be printed on the resistor. For example, a 333 k resistor will be color coded, but a 333.5 k resistor will have its value printed on the resistor body.

The color-coding sequence is shown in Fig. 4-3.

|  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |

## Fig. 4-3. Standard EIA color code for metal film resistors.

Parts Replacement. All parts used in the Type 3A5 can be purchased directly through your Tektronix Field Office or Representative. However, replacements for standard electronic items can generally be obtained locally in less time than is required to obtain them from Tektronix. Replacements for the special parts used in the assembly of the Type 3A5 should be ordered from Tektronix since these parts are either manufactured or selected by Tektronix to satisfy a particular requirement. Before purchasing or ordering, consult the Electrical Parts List in Section 7 to determine the value, tolerance, and ratings required.

## NOTE

When selecting the replacement parts, it is important to remember that the physical size and shape of a component may affect its performance at high frequencies. Parts orientation and lead dress should duplicate those of the original part since many of the components are mounted in a particular way to reduce or control stray capacitance and inductance. After repair, portions of the instrument may require recalibration.

Rotary Switches. Individual wafers or mechanical parts of rotary switches are normally not replaced. If a switct is defective, replace the entire assembly. The availability of replacement switches, either wired or unwired, is detailec in the Electrical Parts List Section 7.

Replacing Components on Etch-Wired Circuits. I/se ordinary electronic grade $60 / 40$ solder and a 35- to 40 -watt pencil soldering iron with a $1 / 8$ inch wide chisel tip. The tip of the iron should be clean and properly tinned for best $h$ :at transfer in a short time to a soldered connection. A hig'er wattage soldering iron, if used and applied for too lonc, a time may ruin the bond between the etched wiring and bise material by charring the glass epoxy laminate. The step-'systep technique is as follows:

1. To remove a component, cut the leads near the body. This frees the leads for individual unsoldering.
2. Grip the lead with needle-nose pliers. Apply the tinted tip of the soldering iron to the lead between the pliers end the solder joint; then pull gently.
3. When the solder first begins to melt, the lead will cone out, leaving a clean hole. If the hole is not clean, use the soldering iron and a toothpick or a piece of enamel wire to open the terminal hole. Do not attempt to drill the sol ter out since the through-hole plating might be destroyed.
4. Clean the leads on the new component and bend them to the correct shape. Carefully insert the leads into the hcles from which the defective component was removed.
5. Hold the leads of diodes with tweezers or pliers to form a heat sink. Apply the iron for a short time at elich connection on the side of the board opposite the component to properly seat the component.
6. Apply the iron and a little solder to the connections to finish the solder joint.
7. Clean all flux from the joint, thus avoiding fut se corrosion.

## Replacing Components on Ceramic Terminal Strips.

Special silver-bearing solder is used to establish a bond to the ceramic terminal strips used in Tektronix instrume its. This bond may be broken by repeated use of ordinary inlead solder or by excessive heating. Solder containing ab.sut $3 \%$ silver is recommended. Silver-bearing solder is usucilly available locally or may be purchased in one-pound rolls through your Tektronix Field Office or Representative. Orider by Tektronix Part No. 251-0514-00.

Because of the shape of the ceramic strip terminals $i$ is recommended that a soldering iron with a wedge-shaped tip be used. A wedge-shaped tip allows the heat to be con-
centrated on the solder in the terminals. It is important to use as little heat as possible while producing a full-flow joint. The step-by-step technique is as follows:

1. Use long-nose pliers for a heat sink. Attach pliers between the component and the point where heat is applied.
2. Use a 50 - to 75 -watt soldering iron with a clean tip, properly tinned with solder containing about $3 \%$ silver.
3. Apply heat directly to the solder in the terminal without touching the ceramic. Do not twist the iron in the notch as this may chip or break the ceramic strip.
4. Apply only enough heat to make the solder flow freely.
5. Do not attempt to fill the notch with solder; instead apply only enough solder to cover the wires adequately and form a small fillet. Overfilling the notches may result in cracked terminal strips. If the lead extends beyond the solder joint, clip off the excess close to the joint.
6. Clean all solder flux from the joint.

## 7. Remove all wire clippings from the chassis.

Ceramic Strip Replacement. Unsolder all connections, then use a $3 / 8$ inch long plastic or hardwood dowel and a small ( 2 to 4 oz ) mallet to knock the stud pins out of the chassis. Place one end of the dowel on the end of the stud pin protruding through the chassis. Rap the opposite end of the dowel smartly with the mallet. When both studs of the strip to be removed have been loosened in this fashion, the strip is removed as a unit. The spacers will probably come out with the studs. If not, they can be pulled out separately. An alternative method of removing the terminal strip is to use diagonal cutters to cut off the sides of the studs. The ceramic strip is removed and the studs pulled from the chassis with a pair of pliers. Replacement ceramic strips are supplied with studs and spacers, so the old studs need not be salvaged. The ceramic strip and its parts are shown in Fig. 4-4.


Fig. 4-4. The ceramic strip and its parts.
The only ceramic strips in the Type 3A5 are located under the output amplifier at the rear panel.

## Glass Reed Switch Replacement

The glass reed switches used in the Type 3A5 are of high quality and should not need replacement unless broken.

## WARNING

Wear safety glasses when replacing the reed switches.

Tools required are a small soldering iron, long nose pliers and diagonal cutters.

Removal. Observe the lead and glass physical position of the old switch and compare it with the new switch before removing the old. If the switch leads go through the etchwired laminate, cut both switch leads about $3 / 8$ inch from the laminate (leaving two leads as solder posts) and pull the switch out of the coil with long-nose pliers.

If the switch has two leads on one end, place the pliers on the lead to be unsoldered before applying heat to the junction of lead and pin. Hold the lead just far enough away from the pin to let the molten solder cool, then unsolder the next lead. Use the pliers to pull the old switch out of the coil by the single lead end.

If removing switches from the attenuator board, note the associated component physical positions before unsoldering so all parts can be repositioned the same way after replacement.

Installing the new switch. Start the new two-lead switch into the coil from either end. Start the three-lead switch into the coil so the single lead enters first. Start an attenuator switch into the coil with the small lead first, passing the lead through the variable capacitor lead. Pull the switch into exactly the same physical position as the old switch.

## CAUTION

Do not apply side pressure to any lead in a manner that will allow the stress to reach the glass. If necessary to bend a lead, use two long-nose pliers.
Clip the leads to the needed length. Solder them in place using good quality $60 / 40$ solder. Check that all parts are dressed correctly and check the circuit operation.

## PARTS LOCATION

Text and illustrations for the remainder of this section are devoted to showing locations of major eircuits. Circuit numbers for all parts mounted on etch-wired circuit boards, and color codes for all pin connections are also shown.

## Subassembly Removal

Attenuator removal (see Fig. 4-5) requires a small soldering iron, a pair of long-nose pliers, a number 10 ( $5 / 16$ inch) socket wrench, a $5 / 16$ inch end wrench, a number 6 ( $3 / 18$ inch) socket wrench and a small screwdriver. Remove the attenuator assembly as follows:

1. Remove the Automatic card from the Type 3A5.
2. Remove the attenuator shield by removing the two 4-40 bolts located on the instrument left side. Then lift the shield free.
3. Unsolder the output lead and disconnect the ground pin from pin W of the vertical board. See Fig. 4-5A.
4. Use the long-nose pliers to lift all nine leads from the pins on the attenuator underside. Use the $5 / 16$ inch end
wrench and socket wrench to remove the two nuts shown in Fig. 4-5B.
5. Lay the instrument on its right side with the attenuator up. Use the $3 / 16$ inch socket wrench to remove the two nuts shown in Fig. 4-5C. Remove the plastic knob from the front of the input coupling switch by pulling it off.

B. Right side mounting nuts (two) and connections to be removed.

C. Left side panel mounting nuts (two) removed and attenuator partially removed.

Fig. 4-5. Mechanical details for removing aftenuator from the Type 3 A5.
6. Lift the attenuator rear upward and slide the assembly away from the front panel for removal. If the attenuator needs to be taken more than a few inches from its normal location, lift the input coupling switch wires from the control board.

To replace the attenuator switch:

1. Slide the assembly into the front-panel opening at a slight angle. It may be necessary to watch the probe $10 \times$ scaling switch button through the panel hole to align it correctly.
2. Install the two right side nuts, but do not tighten. Install the two front-panel nuts and lockwashers, and tighten. Tighten the right side nuts.
3. Install all removed wires from the attenuator right side, the control board and vertical board pins. The wire color code and pin letters are shown in Fig. 4-9 and Fig. 4-10 at the back of this section. Solder the attenuator output lead in place. Do not apply excess heat or the reed switch may be damaged. Replace the attenuator shield.

Vertical Board removal requires a small soldering iron, a small screwdriver and long-nose pliers. Remove the Vertical board as follows:

1. Remove the attenuator shield and unsolder the attenvator output lead as shown in Fig. 4.5A.
2. Lift all wires from the connecting pins with the longnose pliers. Pull on the pins, not the wires. Unsolder six leads: H, I, N, O, and the two leads of C422 shown in Fig. 4.6. Place the removed delay line leads so they can be soldered again in correct order.)


Fig. 4-6. Unsolder two leads of C422 when removing Vertical board.
3. Remove the six mounting bolts they have captive nuts permanently mounted in the chassis) and lift the board out.
To replace the Vertical board:

1. Gently lower it into place so the positive terminal of C422 comes through its opening. Secure it in place with the six mounting bolts and their split washers.
2. Solder C422 leads and the delay line leads. If the delay line lead orientation is unknown, an ohmmeter ( $10 \times$ scale) will help. The pins H and N connect through the ferrite transformers to the rear delay line terminals. Pins I and O connect through the ferrite transformers to the front delay line terminals.
3. Solder the attenuator output lead in place and install the attenuator shield.
4. Replace all leads to the Vertical board pins following the color coding and pin lettering of Fig. 4.11.

Two tubes and two transistors are mounted on the Vertical board under clamped-down heat sinks. Q123-Q323 heat sink is removed by lifting the black clamp straight away from the board.
To remove V113 and V313 use a sharp pointed tool such as a scribe to unlock the phosphor-bronze clip at the rear side of the heat sink. Pry the clip away from the bottom of the heat sink so it can come out of the mounting hole. Repeat for the front side of the heat sink and remove the clip. Lift the heat sink straight away from the board with a steady pressure. The heat sink will slip slowly off the tubes due to silicone grease lubricant. To remove the tubes DO NOT use long nose pliers, but use either the fingers or a specially shaped tool that will not cave in the tube sides.

Replace the tubes and heat sink in the reverse order. If new tubes are installed, coat them lightly with silicone grease such as Dow Corning DC.4.

## WARNING

Do not let the silicone grease touch the face or eyes. Serious damage may result from silicone grease in the eyes. Wash your hands after working with V113-V313 heat sink.

Control Board removal requires only a screwdriver and long nose pliers. Disconnect all leads, remove four mounting screws and lift the board out. To replace the Control board place it so that Q624 is at the instrument top. Color coding of the wires and pin lettering is shown in Fig. 4. 12.

Readout Panel removal (see Fig. 4-13) requires only a Phillips number 1 screwdriver and long-nose pliers. Remove the leads, unscrew the two through-panel mounting bolts and lift the board out. Readout lamps can be replaced using a small soldering iron and normal soldering procedures. Use a heat sink on the diode leads when soldering in new diodes.

Mode Switches Panel removal (see Fig. 4-13) requires a small soldering iron, long-nose pliers, and a $1 / 4$ inch box end wrench. Remove the two mounting nuts with the $1 / 4$ inch wrench, withdraw the board, then unsolder the leads. The leads can be soldered most easily if the board is removed through the instrument left side. Installation is the reverse of removal, and lead color code and pin lettering is shown in Fig. 4-13.

Position Control removal requires a pair of long nose pliers, a No. 6 ( $3 / 16$ inch) end wrench and a small soldering iron. Remove the two special $1 / 2$ inch long mounting nuts that are located next to each other at the top of the control. Withdraw the control, make a record of lead color coding
and placement, then unsolder the leads. Remove the knob with a 0.035 inch Allen wrench.

Re-install the POSITION control with the knob on the shaft, but not screwed tight. Correct knob position is with the red mark positioned out of sight behind the panel and over the top terminal (to which -12.2 volts is connerted) when the control is at its counterclockwise end of rotation (instrument lying on its right side). Tighten the knob with a 0.035 inch Allen wrench.

Delay Line removal requires a small soldering iron, a screwdriver and long nose pliers. Unsolder the four delay line leads at the through-chassis terminals. Remove the mounting bolts at the delay line ends. Remove the delay line cover bolt and lift the delay line out.

If the delay line leads develop a short circuit, it will probably be at one end. It may not be necessary to remove the delay line to make the repair. Each end of the delay line can have up to ten turns removed without affecting performance. Thus, if the line is shorted, remove a few turns (equal number for each lead) from the shorted end and resolder the leads to the through-chassis terminals. An ohmmeter (10X scale) will tell you which end is shorted. When soldering the delay line leads, use the pliers as heat sink to prevent the soldering heat from going back into the line and causing a short circuit. The lead orientation must be checked with an ohmmeter before soldering. One side of the line goes to the front terminals and the other side of the line goes to the rear terminals of the two pairs of through-chassis terminals.


1. Reed switched attenuators.
2. Vertical amplifier before delay line.
3. Trigger amplifier.
4. Output stage driver amplifier.
$5 .+6.8 \mathrm{~V}$ and +4.2 V power supplies
5. Output amplifier.
6. Control circuits,
7. Readout panel.

Fig. 4-7. Left side major circuit locations.


Fig. 4-8. Right side major circuit locations.


Fig. 4-9. Attenuator left side parts locations and wire color code.


Fig. 4-10. Aftenuator right side parts locations and wire color code.

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Fig. 4-11. Vertical amplifier board parts locations, and wire color code.


Fig. 4-12. Control circuit board parts locations, and wire color code.


Fig. 4-13. (A) Mode switch lamps. (B) Mode switch panel wire color code. (C) Readout panel diode locations and wire color code. (D) Readout panel lamps.


Fig. 4-14. Output amplifier parts locations.


Fig. 4-15. One half automatic card parts locations.


Fig. 4-16. One half automatic card parts locations.

## SECTION 5

PERFORMANCE CHECK

## Introduction

This performance check procedure is to be performed entirely from the Type 3A5 front panel, without removing the oscilloscope side or bottom panel. The procedure may be used for incoming inspection, quality control after recalibration, and instrument familiarization.

Failure to meet the characteristics and limits given in this procedure indicates that the instrument requires inte nal checks and/or adjustments. See the Calibration section of this instruction manual.

## Recommended Equipment

The following equipment is necessary for a complete performance check of the Type 3A5. If other than the recimmended equipment is used, it must meet or exceed the specifications of the recommended equipment.

Special calibration equipment is used in the performance check procedure for obtaining the maximum accuracy and convenience. Some of these items are manufactured specially by Tektronix. Items available from Tektronix are identified by type or nine digit part number. Order by part number from your local Tektronix Field Office or Representative.

1. A Type 561A Oscilloscope, or other oscilloscope in which the Type 3A5 will normally operate. A time-base unit for the oscilloscope, such as a Type 3B5 Automatic/Programmable Time-Base. The Type 3B5 is required to perform ,se check of the Type 3A5.
2. A sine wave signal generator with constant amplit,ide control at 50 kHz and from approximately 2 MHz through 25 MHz . Amplitude continuously variable from 5 mV to 10 V peak to peak. Example, Tektronix Type 191 Constant Amplitude Signal Generator.
3. Fast rise pulse generator with amplitude adjustable from 5 mV to 120 V peak-to-peak at a repetition rate of approximately 1 kHz . Risetime of $\leq 2.3 \mathrm{nsec}$ into $50 \Omega$ at 400 kHz and 40 mV peak to peak. Tektronix Type 106 Square-Wave Generator is recommended.
4. A low frequency sine wave oscillator with an output frequency of 10 Hz at an amplitude of 10 mV peak to peak. Example, Heathkit Model IG-72 Audio Generator.
5. An accurate-amplitude signal generator of appreximately 1 kHz square-wave repetition rate. Voltage from 0.2 mV to 100 V with accuracy of $\pm 0.25 \%$. Tektronix 067 -0502-00 Standard Amplitude Calibrator.
6. A 24 pF Input Time Constant Standardizer with B $N C$ connectors, Tektronix Part No. 011-0067-00.
7. $\mathrm{A} \pm 1 \% 50 \Omega$ termination with BNC connectors, such as Tektronix Part No. 011-0049-00.
8. Two $50 \Omega 10: 1$ attenuators with BNC connectors, such as Tektronix Part No. 011-0059-00.
9. Two (one required, two can be used) GR Type 874 connector to BNC adapters. General Radio 874-QBJA, Tektronix Part No. 017-0063-00.
10. A $50 \Omega$ coax cable about 3 or 4 feet long with BNC connectors. Such as 42 inch cable, Tektronix Part No. 012 -0057-00.
11. A BNC to clip lead adapter (if the 10 Hz sine wave generator is the suggested Heath unit), Tektronix Part No. 013-0076-00.
12. Variable line voltage autotransformer, such as the General Radio VARIAC, Type WIOMT3W, metered 600 watt rating.
13. Small screwdriver for adjusting front-panel screwdriver controls.
14. A de resistance bridge of $\pm 0.075 \%$ or better accuracy at $1 \mathrm{M} \Omega$.
15. A power line 3 -wire to 2 -wire adapter.

## PROCEDURE

In the following procedure, control settings are listed in complete form just once. Changes required for each step are stated at the time the control is to be changed. Thus, perform the procedure in the order stated without any alterations. Signal connections are listed as required.

## Preliminary Checks

1. Check all front-panel controls for proper indexing. Check the variable controls for smooth operation. Check that the POSITION control red mark rests approximately half way between the end of rotation limits. Correct any defects found.
2. Check Input Resistance. This check is required in order to make accurate measurement of input grid current and to assure correct input time constant when compared to a Tektronix input time constant standardizer.

Requirement-Input de resistance to ground must be $1 \mathrm{M} \Omega$ $\pm 0.75 \%$.
a. Lay the Type 3A5 on its right side on the work bench (with the Vertical Amplifier board up). Locate the lead coming out the rear of the attenuator shield (white with black tracer). This lead is connected directly to the $1 M \Omega$ input resistor.
b. Use a dc resistance bridge. Connect its common lead to the Type 3A5 front-panel ground connector and its active lead to the white with black tracer lead located in (a) above. Measure the resistance.

## Connections and Control Settings

Place the Type 3A5 into the test oscilloscope. Connect the oscilloscope power cord to the variable line voltage autotransformer. Set the Type 3A5 controls before turning

## Performance Check-Type 3A5

on the power, then turn on the power and adjust the line voltage to 117 volts rms ( 234 volts rms if the oscillosccipe is wired for the higher voltage).

Set the Type 3A5 controls:

| POSITION | Midrange |
| :--- | :--- |
| Input Coupling | AC-TRACE STABILIZED |
| MANUAL VOLTS/DIV | 10 mV |
| VARIABLE | CAL |
| Mode | MAN |

Set the Time-Base controls:

| Position | Midrange |
| :--- | :--- |
| Manual Time/Div | 1 msec |
| Variable | Cal |
| Trigger Mode | Auto |
| Coupling | + Int, AC |
| Trigger Level | Midrange |
| Magnifier | $\times 1$ or Off |
| Delay | 0.00 |
| Mode | Man |

Set the oscilloscope controls:

| Intensity | Normal brilliance trace |
| :--- | :--- |
| Focus | As required |
| Calibrator | Off |
| Power | On |

## Operation Checks

## 1. Trace Alignment check

Position the trace to the graticule centerline and adjust the oscilloscope Alignment control so that the trace is parallel with the graticule markings.

## 2. Check INPUT grid current

Requirement-2 nanoamperes or less grid current atter 20 minutes operation.

Set the Input Coupling switch to DC and position the trace to graticule centerline. Short the INPUT connector center conductor to ground and note trace shift. The shift should not be greater than 0.2 division, or 2 nanoamperes. Remcive the INPUT short circuit.

## 3. Check Microphonics

Requirement-No ringing microphonics. No microphonics greater than 0.2 minor division at $10 \mathrm{mV} /$ division.
a. Lightly tap the oscilloscope top front panel area. The trace should show no microphonics of a prolonged ringing nature, and no short-term microphonics of greater amplitude than 2 minor divisions.

## 4. Check trace drift with change in line voltage

Requirement-Trace does not drift over $\pm 0.5$ ma,or division between the line voltages of 105 volts and 125 volts rms after 1 minute at each voltage.
a. Set the line voltage autotransformer to deliver 105 volts rms to the oscilloscope. Wait one minute. Position the trace to the graticule centerline. Change the autotransformer to deliver 125 volts rms to the oscilloscope. After one minute the trace must not have drifted more than $\pm 0.5$ major division. Return the autotransformer output to 117 volts.

## 5. Check Readout Panel Lamps

Requirement-All lamps light in accordance with the following procedure.
a. Set the Input Coupling to AC-TRACE STABLIZED and position the trace to the graticule centerline. The AC lamp must be lighted. Set the Input Coupling to $A C$ and then $D C$. The $A C$ and then the DC lamps should light. Return the Input Coupling switch to AC-TRACE STABILIZED. Center the trace.
b. Set the MANUAL VOLTS/DIV switch to 1 mV . The VARIABLE control to CAL. The readout should be AC; 1 $\mathrm{mV} / \mathrm{DIV}$ and the MAN button is lighted. Operate the MANUAL VOLTS/DIV switch through each step up to 50 V/DIV and observe that the readout agrees with the switch position at each step.
c. Press the gray unlabeled $10 \times$ probe switch located just above the INPUT connector. Note that the display changes to: WITH PROBE and $.5 \mathrm{KV} / \mathrm{DIV}$.
d. While holding the $10 \times$ probe switch depressed, operate the MANUAL VOLTS/DIV switch from 50 V/DIV to $1 \mathrm{mV} /$ DIV and note that the readout is $10 \times$ each switch position. Release the $10 \times$ probe switch.
e. Turn the VARIABLE control first left, then right from its detent CAL position and note that the V/DIV lamp goes out and the red UNCAL lamp turns on. Return the VARIABLE control to CAL. Return the MANUAL VOLTS/DIV switch to 10 mV .
f. Press the SEEK button and note that the display reads $A C$ and $10 \mathrm{mV} / \mathrm{DIV}$, and that the SEEK button is lighted. Turn the MANUAL VOLTS/DIV switch to 20 mV and note that the SEEK button light goes out and the MAN button is lighted. Press and hold the EXT button and note that only the V/DIV lamp comes on. Other lamps may light, but this is normal without an external program connected. Release the EXT button. Set the MANUAL VOLTS/DIV switch to 10 mV .
g. Position the trace to plus four divisions, and then to minus four divisions and note that the unlabeled neon overscan lamp above the POSITION control is lighted in both cases. Set the Input Coupling switch to DC and center the trace.

## 6. Check Variable Balance

Requirement-Trace does not shift vertically when VARIABLE control is turned. (Drifts slightly with ambient temperature and is considered an operator adjustment prior to any accurate de or VARIABLE measurements.)
a. Turn VARIABLE control counterclockwise and note any shift of the trace. Return VARIABLE to CAL and shift trace in same direction $1 \frac{1}{3}$ times its (VARIABLE) travel by the VAR BAL control. Repeat until trace does not shift verti-
cally throughout full rotation of VARIABLE control. Return VARIABLE to CAL.

## 7. Check Vertical Amplifier $10 \mathrm{mV} / \mathrm{DIV}$ through 50 V/DIV Deflection Accuracy

Requirement--Vertical deflection must be within $3 \%$ of VOLTS/DIV indicated deflection factor between $10 \mathrm{mV} / \mathrm{DIV}$ and $50 \mathrm{~V} / \mathrm{DIV}$.
a. Connect the Standard Amplitude Calibrator right ide (signal) OUTPUT connector to the Type 3A5 INPUT connector using a $50 \Omega$ coax.
Set the Type 3A5 VARIABLE control to CAL and the MANUAL VOLTS/DIV switch to 10 mV . Set the Calibrutor Amplitude control to 50 mvolts, the Mode control for square wave output, and the Mixed switch up.

## NOTE

Determine that the Standard Amplitude Calibrator has been operating at least 15 minutes before: proceeding.
b. If the Type 3A5 was not calibrated in the oscilloscope in which it is now operating, adjust the CAL control to exactly 5 divisions peak-to-peak display.
c. Use Table 5-1 and Figures 5-1, 5-2 and 5-3 to determine the deflection accuracy at each setting of the MAN(JAL VOLTS/DIV switch between $10 \mathrm{mV} / \mathrm{DIV}$ and $50 \mathrm{~V} /$ DIV. If any one switch setting causes an out-of-tolerance display, record the amount of error, continue to $50 \mathrm{~V} / \mathrm{DIV}$, then return to $10 \mathrm{mV} / \mathrm{DIV}$ and adjust the CAL control. Adjust the CAL control to reduce the one error, but not far enough to give any other switch setting an opposite out-of tolerance error. Correct adjustment of the CAL control is complete when all ranges are within $3 \%$, and $10 \mathrm{mV} / \mathrm{DIV}$ is not necessarily at $\pm 0 \%$. If one switch position causes a flus error greater than $+3 \%$ and another causes a minus eiror greater than $-3 \%$, record the error of all switch setting'. in order to determine which attenvator is in error.

TABLE 5-1
Vertical Deflection Accuracy Check

| MANUAL <br> VOLTS/DIV <br> Switch <br> Setting | Standard <br> Amplitude <br> Calibrator <br> AMPLITUDE <br> Control | Vertical <br> Deflection <br> In <br> Divisions | \% Error <br> See Fig. <br> Fig. 5 thru |
| :---: | :---: | :---: | :---: |
| 1 mV | 5 mV | 5 | $\pm 5 \%$ |
| 2 mV | 10 mV | 5 | $\pm 5 \%$ |
| 5 mV | 20 mV | 4 | $\pm 5 \%$ |
| 10 mV | 50 mV | 5 | $\pm 3 \%$ |
| 20 mV | 0.1 V | 5 | $\pm 3 \%$ |
| 50 mV | 0.2 V | 4 | $\pm 3 \%$ |
| .1 V | 0.5 V | 5 | $\pm 3 \%$ |
| 2 V | 1 V | 5 | $\pm 3 \%$ |
| .5 V | 2 V | 4 | $\pm 3 \%$ |
| 1 V | 5 V | 5 | $\pm 3 \%$ |
| 2 V | 10 V | 5 | $\pm 3 \%$ |
| 5 V | 20 V | 4 | $\pm 3 \%$ |
| 10 V | 50 V | 5 | $\pm 3 \%$ |
| 20 V | 100 V | 5 | $\pm 3 \%$ |
| 50 V | 100 V | 2 | $\pm 3 \%:$ |


a. DEFLECTION ACCURACY $\pm 0 \%$

b. DEFLECTION ACCURACY $+3 \%$ ( $+3 / 4$ MINOR DIV).

c. DEFLECTION ACCURACY $-3 \%$ ( $-3 / 4$ MINOR DIV).

Fig. 5-1. Deflection accuracy limits between $10 \mathrm{mV} / \mathrm{DIV}$ and $20 \mathrm{~V} / \mathrm{DIV}$ when VOLTS/DIV has the number 1 or 2 in it.

a. DEFLECTION ACCURACY $\pm 0 \%$.

b. DEFLECTION ACCURACY $+3 \%(+2 / 3$ MINOR DIV $)$.

c. DEFLECTION ACCURACY $-3 \%(-2 / 3$ MINOR DIV $)$

a. DEFLECTION ACCURACY $+0 \%$

b. DEFLECTION ACCURACY $+3 \%$ ( +0.3 MINOR DIV).

c. DEFLECTION ACCURACY $-3 \%$ ( -0.3 MINOR DIV).

Fig. 5-2. Deflection accuracy limits between $10 \mathrm{mV} / \mathrm{DIV}$ and $20 \mathrm{~V} /$ DIV when VOLTS/DIV has a number 5 in it.

Fig. 5-3. Deflection accuracy limits at $50 \mathrm{~V} / \mathrm{DIV}$.

## 8. Check Vertical Amplifier Manual 1, 2 and $5 \mathrm{mV} /$ DIV Deflection Accuracy

Requirement-Vertical Deflection must be within $5 \%$ of VOLTS/DIV indicated deflection factor between $1 \mathrm{mV} /$ DIV and $5 \mathrm{mV} /$ DIV.
a. With the Standard Amplitude Calibrator as connecied, set Type 3A5 MANUAL VOLTS/DIV switch to 10 mV . Set the Calibrator Amplitude control to 50 mvolts. Set the Type $3 A 5$ Input Coupling Switch to AC-TRACE STABILIZED and center the display vertically.
b. Set the Calibrator Amplitude control to 5 mvolts and the Type 3A5 MANUAL VOLTS/DIV switch to 1 mV . The display transition must be 5 divisions $\pm 5 \%$ as showr in Fig. 5-14. Use Table 5-1 and Figures 5-4 and 5-5 for 1, 2 and $5 \mathrm{mV} /$ DIV checks. If all three checks show the ciain to be either high or low, check the Outpui Amplifier cuthode circuit.

## 9. Check VARIABLE Range

Requirement- $\geq 2.5: 1$ overall and from CAL position to full counterclockwise, reduced to between $55 \%$ and $71 \%$ of display size at CAL detent.
a. Use a $50 \Omega$ coax cable and connect the Standard Amplitude Calibrator Output connector to the Type : :A5 INPUT, connector. Set the Calibrator Amplitude control to 50 mvolts. Set the Type 3A5 MANUAL VOLTS/DIV switch to 10 mV and the Input Coupling Switch to AC.
b. Turn the VARIABLE control fully counterclockwise. The display must be between 2.8 and 3.6 divisions peak to $p \in a k$. Record the amplitude.
c. Set the Calibrator Amplitude control to 20 mvelts. Turn the Type 3A5 VARIABLE control fully clockwise. The display amplitude must be equal to or greater in amplitude than the display of step $b$. Set the VARIABLE control to CAL.

## 10. Check POSITION Range

a. With the Standard Amplitude Calibrator connected as in step 9, set the Amplitude control to 50 mvolts. Ad ust the Type 3A5 VARIABLE control for a 6 division display. Change the Calibrator Amplitude control to . 1 volts.
b. Position the display as far up screen as possible. The display bottom must be above the graticule centerline.
c. Position the display as far down screen as possitle. The display top must be below the graticule centerline.

## NOTE

Steps 9 and 10 are checks of the transistors installed in the Driver Amplifier and the Output Amplifier. Less than the required performance could mean one or more of the transistors have inadequate $\beta$.

## 11. Check Input Capacitance and Attenuator Compensations

Requirements-Input capacitance must be $24 \mathrm{pF} \pm 1 \mathrm{pF}$. Square-wave display must not have greater than $3 \%$ peak to peak overshoot, rounding, ringing or tilt when driven by a flat-topped square wave, and when using the Input RC Standardizer mentioned in the Equipment Required list.

a. DEFLECTION ACCURACY $\pm 0 \%$.

b. DEFLECTION ACCURACY $-5 \%$ ( -1.25 MINOR DIV).

c. DEFLECTION ACCURACY $5 \%$ ( 1.25 MINOR DIV).

Fig. 5-4. Deflection accuracy limits at 1 and $2 \mathbf{m V} /$ DIV.

a. DEFLECTION ACCURACY $\pm 0 \%$.

b. DEFLECTION ACCURACY $+5 \%$ ( +1 MINOR DIV).

c. DEFLECTION ACCURACY $-5 \%$ ( -1 MINOR DIV) .

Fig. 5-5. Deflection accuracy limits at $\mathbf{5} \mathbf{~ m V / D I V}$.
a. Install the Input RC Standardizer on the Type 3A5 INPUT connector. Install the BNC $50 \Omega$ termination on the Input RC Standardizer. Connect a $50 \Omega$ BNC connector cable to the termination.
b. The signal generator recommended is the Tektronix Type 106. A Tektronix Type 105 will work equally well, and does not require a connector adapter.

Install one $10 \times 50 \Omega$ attenuator to the signal generator Output connector. (Use the GR to BNC adapter with the Type 106); attach it to the Hi Amplitude Output connector.)

Set the Type 106 controls:

| Repetition Rate Range | 1 kHz |
| :--- | :--- |
| Multiplier | Near 2 |
| Symmetry | Midrange |
| Amplitude | Fully Counterclockwise |
| Hi Amplitude |  |
| Fast Rise Switch | Hi Amplitude |
| Fast Rise Controls | Optional |

Set the Type 3A5 controls:

| Input Coupling | $D C$ |
| :--- | :--- |
| MANUAL VOLTS/DIV | 10 mV |
| VARIABLE | $C A L$ |

Connect the $50 \Omega$ cable to the $10 \times$ attenuator and check that the oscilloscope FOCUS control is properly adjusted for a sharply defined display.
c. Set the Time-Base TIME/DIV control to .1 msec and obtain a stable display. Adjust the square-wave generator Amplitude control for exactly 4 divisions peak to peak.
d. Check the input capacitance by observing any spike or rolloff of the square-wave leading edge for approximately 0.02 msec (or 1 minor horizontal division). 1 pF error of input capacitance will cause approximately 1 minor vertical division spike or rolloff, an error greater than the allowed $3 \%$ peak to peak aberration limits of $2 / 3$ minor division. If the Input RC Standardizer being used is different than the Standardizer used in calibration, up to $1 / 4$ minor division additional spike or rolloff is allowable due to Standardizer capacitance tolerance. Note the spike or rolloff, and take it into account during the rest of this step.
e. Use Table 5-2 and Fig. 5-6 to check the aberration of the input attenuators. Start at $10 \mathrm{mV} / \mathrm{DIV}$ and work to $50 \mathrm{~V} /$ DIV, adjusting the Calibrator Amplitude control, removing the attenuator, termination and standardizer when it is not possible to obtain four divisions at higher deflection factors.

## CAUTION

Maximum full-time peak-to-peak display with the $10 \times$ attenuator/50 $\Omega$ termination/Standardizer combination is 0.3 volts as displayed on the crt. This keeps the attenuator $50 \%$ signal duty cycle power dissipation within its $1 / 2$ watt rating. Remove the $10 \times$ attenuator beginning at $.1 \mathrm{~V} / \mathrm{DIV}$ deflection factor. Maximum full-time peak-topeak display with the $50 \Omega$ termination/Standardizer combination is 5 volts as displayed on the crt. Thus remove the attenuator beginning at 2 V/DIV deflection factor.

a. DISPLAY FOR CHECKING SHORT TIME CONSTANT SPIKE OR ROLLOFF.

b. DISPLAY FOR CHECKING LONGER TIME CONSTANT TILT OR ROUNDING.

Fig. 5-6. Changes in sweep rate for best displays while checking attenuator compensation. Signal generator repetition rate is the same in both cases.
f. Install the 3 -wire to 2 -wire power cord adapter at the Type 106 power connector to eliminate 60 Hz ground current signals that may be displayed at 1,2 and $5 \mathrm{mV} / \mathrm{DIV}$. Install two $10 \times$ attenuators to the Type 106 Output and the $50 \Omega$ termination to the Input RC Standardizer. Set the Type 106 Amplitude control fully counterclockwise.

Set the Type 3A5 controls:
MANUAL VOLTS/DIV 10 mV
Input Coupling DC
POSITION Vertically centered display

Change the MANUAL VOLTS/DIV switch to 1 mV and position the display to the crt center. Increase the sigrial amplitude for four divisions display. The display should be


APPROX. 2 kHz SIGNAL . $2 \mathrm{mS} / \mathrm{DIV}$.

Fig. 5-7. Normal square-wave display at 1,2 , or $5 \mathrm{mV} / \mathrm{DIV}$ when attenuators are correctly compensated af 10,20 and $50 \mathrm{mV} / \mathrm{DIV}$.

TABLE 5-2
Step 11 Operating Conditions

| MANUAL VOLTS/DIV Switch Setting | Use <br> 10× <br> Atten. | $\begin{aligned} & \text { Use } \\ & 50 \Omega \\ & \text { Term. } \end{aligned}$ | Use RC Stand. | Display Divisions Peak to Peak |
| :---: | :---: | :---: | :---: | :---: |
| 10 mV | X | X | X | 4 |
| 20 mV | X | X | X | 4 |
| 50 mV | X | X | X | 4 |
| . 7 V |  | X | X | 4 |
| . 2 V |  | X | X | 4 |
| . 5 V |  | X | X | 4 |
| 1 V |  | X | X | 4 |
| 2 V |  |  | X | 4 |
| 5 V |  |  | X | 4 |
| 10 V |  |  | X | 4 |
| 20 V |  |  |  | 4 |
| 50 V |  |  |  | $\approx 2.2$ |

similar to Fig. 5-7. The $5 \%$ square-wave leading edge rolloff is due to limited high frequency response, and not to the attenuator.

## 12. Check AC-TRACE STABILIZED Operation

Requirement-Position control will have approximately one-half normal control at $10 \mathrm{mV} /$ DIV to $50 \mathrm{~V} /$ DIV when the Input Coupling is at AC-TRACE STABILIZED. Trace will not drift at 1,2 and $5 \mathrm{MV} / \mathrm{DIV}$.
a. Set the MANUAL VOLTS/DIV switch to 10 mV . Set the VARIABLE control to CAL. Set the Input Coupling switch to $A C$.
b. Position the trace to the top graticule line. Change the Input Coupling Switch to AC-TRACE STABILIZED. The


Fig. 5-8. Correct high frequency transient response. $\approx 400 \mathrm{kHz}$ at $0.5 \mathrm{~ms} / \mathrm{div}$ and $10 \mathrm{mV} / \mathrm{div}$.
trace must return at least 1 major division toward the graticule centerline.
c. With the Input Coupling at AC-TRACE STABILI:'ED and the trace position as at the end of step $b$, change the MANUAL VOLTS/DIV switch to 5 mV . The trace should not change position from its $10 \mathrm{mV} / \mathrm{DIV}$ position.

## 13. Check High Frequency Transient Response

Requirement-Display has no more than $\pm 3 \%$ overshisot, rounding, ringing or tilt of a 400 kHz square-wave siçnal with $10 \%$ to $90 \%$ risetime of $\leq 12 \mathrm{nsec}$. MANUAL VOLTS/ DIV switch at 10 mV .
a. Connect the Type 106 Fast Rise + Output connecto to the Type 3A5 INPUT connector. Use a BNC $50 \Omega$ termination directly on the INPUT connector, and a GR to BNC adapter on the Type 106 + Output connector. Use a $50 \Omega$ coax between the adapter and termination.
b. Set the Type 106 +Amplitude control fully counterclockwise and the Hi Amplitude/Fast Rise switch to last Rise. Obtain a 400 kHz repetition rate signal.

Set the oscilloscope time-base Time/Div switch to $.5 / \mathrm{sec}$ and obtain a stable triggered display that is like Fig. j-8. The display should be the same for all three positions of the Type 3A5 Input Coupling switch.
c. If using a Type 105 Square-Wave Generator, put wo $10 \times$ attenuators on the Output connector and then fred the $50 \Omega$ cable and Type $3 A 550 \Omega$ termination. The display must be the same as Fig. $5-8$ with limits as above.

## 14. Check Display Positioning Effect Upon Transient Response

Requirement-Four division fast-rise signal display will not have more than $\pm 5 \%$ overshoot, rounding, ringing or tilt when top of AC coupled display is positioned to bottom of graticule or when bottom of display is positioned to tor of graticule.

a. 4 DIVISION DISPLAY POSITIONED DOWN.

b. 4 DIVISION DISPLAY POSITIONED UP.

Fig. 5-9. Position effect upon transient response, step 14.
a. With the display as in step 13, position the display top to the graticule bottom. See Fig. 5-9. The aberrations must not exceed $\pm 5 \%$ : $\pm 1$ minor division maximum ( 2 minor divisions peak to peak).
b. Move the Type 106 output cable to the -Output connector. Obtain a centered Ac-coupled four division display. Position the display bottom to the graticule top. See Fig. 5-9. The aberrations must not exceed $\pm 5 \%$ : $\pm 1$ minor divisions ( 2 minor divisions peak to peak).

## NOTE

Step 14b cannot be performed if using a Type 105 Square-Wave Generator.

## 15. Check Vertical Amplifier 10\% to $90 \%$ Risetime

Requirement-10\% to $90 \%$ risetime must be $\leq 23 \mathrm{nsec}$ when clean fastrise signal of $\leq 2.3$ nsec risetime drives Type


Fig. 5-10. Difference in risetime measurement using Type 105 (A) and Type 106 FAST RISE (B).

3A5 INPUT at $10 \mathrm{mV} / \mathrm{DIV}$. The risetime requirement is rounded off to $\leq 23$ nsec here because of the difficulty of visually resolving 0.2 nsec .
a. Connect the GR to BNC adapter to the Type 106 +Output connector. ( $50 \Omega$ termination at Type 3 A5 INPIJT connector.) Obtain a four division 400 kHz display.
b. Increase the sweep rate to at least $0.05 \mu \mathrm{sec} / \mathrm{div} 50$ nsec/div) and obtain stable triggering on the rising slope of the signal. The display should be similar to Fig. 5-10. Measure the risetime between the $10 \%$ and $90 \%$ points as shown in Fig. 5-10.

If you are using the recommended Type 106 fast rise signal, read the vertical amplifier risetime directly from the display (as in Fig. 10B).

If you are using a Type 105 Square-Wave Generator (w,th two $10 \times 50 \Omega$ attenuators at the Type 105 Output connect.r)
the true amplifier risetime will be essentially 2 nsec faster than that displayed (as in Fig. 5-10A).

## 16. Check Vertical Amplifier Bandwidth

Requirement-Sine wave high frequency amplitude response at $10 \mathrm{mV} /$ DIV remains no less than $70 \%$ of the dc or low frequency sine wave response to at least 15 MHz .
a. Set the Type 191 Constant Amplitude Signal Generator controls:

| Amplitude Range | $5-50 \mathrm{mV}$ |
| :--- | :--- |
| Amplitude | 35 |
| Variable | 4 div display |
| Frequency Range | 50 kHz |
| Frequency Control | Fully Clockwise |

Set the Type 3A5 controls:

| Input Coupling | AC |
| :--- | :--- |
| MANUAL VOLTS/DIV | 10 mV |
| POSITION | Midrange |

Set the time-base controls:

| Manual Time/Div | 10 msec |
| :--- | :--- |
| Triggering | $+\operatorname{lnt} \mathrm{AC}$ |

b. Connect a $50 \Omega$ cable from the Type 191 Output connector (use the GR to BNC adapter) to the Type 3A5 INPUT connector. Use a $50 \Omega$ termination at the Type 3 A5 INPUT connector. Obtain a four-division peak-to-peak display as shown in Fig. $5-11 \mathrm{~A}$. Fig. $5-11 \mathrm{~A}$ shows how the bottom "side" of the trace is positioned to the top side of the -2 division graticule line, and then the Type 191 Variable control adjusted to place the same side of the trace to the top side of the +2 division graticule line. This gives an accurately centered four division peak to peak display that does not include the trace thickness.
c. Change the Type 191 Frequency Range control to the $8-18 \mathrm{MHz}$ range. Set the oscilloscope time base for a triggered sweep at $.05 \mu \mathrm{sec} / \mathrm{div}$. Check the display peak-topeak amplitude and turn the Type 191 frequency adjust control slowly higher in frequency until the display amplitude is 2.8 divisions as in Fig. 5-11B. Position the plus peak of a sine wave to the graticule vertical centerline so the minor divisions can best be used. Record the frequency.

## 17. Check Automatic Seeking Circuit High Frequency Performance

Requirement-Seek circuit will respond at 20 MHz .
a. With the connections and display as at the end of step 16, set the Type 191 Frequency Range control to the $18-42 \mathrm{MHz}$ range and the frequency control to $20(\mathrm{MHz})$. Position the display to be equally balanced at the graticule centerline.
b. Change the Type 191 Amplitude Range switch to 50 500 mV and then press the Type 3A5 SEEK button. The display must first extend to near the graticule limits, then as the SEEK button is pressed the display must return to less than 6 divisions peak to peak.
c. Change the Type 191 Amplitude Range switch to 5-50 mV and then press the Type 3A5 SEEK button. The display


Fig. 5-11. Bandwidth measurement displays, step 16.
must first become small (or extinguish due to loss of internal trigger) and then as the SEEK button is pressed, return to its original amplitude and a deflection factor of $10 \mathrm{mV} /$ DIV

## 18. Check Trigger Circuit Output

Requirement-A display can be triggered with a signal of 2 mV peak to peak at $10 \mathrm{mV} /$ DIV deflection factor.
a. With the equipment as connected for steps 16 and 17 , install one $50 \Omega 10 \times$ attenuator in series with the signal coax between the Type 191 and the Type 3A5.

## NOTE

If you do not have a Type 191, use the special Standard Amplitude Calibrator without attenuators or termination in this step.
b. Set the Type 191 controls:

| Amplitude Range | $5-50 \mathrm{mV}$ |
| :--- | :--- |
| Amplitude | 20 |
| Variable | Cal |
| Frequency Control | Fully clockwise |
| Frequency Range | 50 kHz |

Set the Type 3A5 MANUAL VOLTS/DIV control to 10 mV , the VARIABLE control to CAL.

Set the oscilloscope time-base controls:

| Mode | Manual |
| :--- | :--- |
| Manual Time/Div | $10 \mu \mathrm{sec}$ |
| Dly'd Swp Mag | Off |
| Triggering | + Int AC (Not Auto) |

c. Adjust the time base Triggering Level control for a stable display.

## NOTE

It is assumed here that the time base trigger circuit is calibrated and operating within its specifications. If it is impossible to obtain a stable display, check the controls before assuming that the Type 3A5 trigger circuits are faulty.

## 19. Check REMOTE SEEK Operation

Requirement-The Type 3A5 and the Type 3B5 will both change mode of operation to SEEK when the Type 3A5 REMOTE SEEK button is pressed.
a. Remove the $50 \Omega$ termination and signal cable from the Type 3A5 INPUT connector. Install the Type P6030 10X Probe to the INPUT connector and the small phono plug into the REMOTE SEEK jack. Compensate the probe.
b. Set the Type 191 controls:

| Amplitude Range | $50-500 \mathrm{mV}$ |
| :--- | :--- |
| Amplitude | 10 |
| Variable | Cal |
| Frequency Range | 50 kHz |
| Frequency Control | Fully clockwise |

Set the Type 3B5 controls:

| Manual Time/Div | $20 \mu \mathrm{sec}$ |
| :--- | :--- |
| Variable | Cal |
| Mode | Man |
| Mag | Off or $\times 1$ |
| Triggering | + Int AC |

c. Connect the P6030 $10 \times$ Probe ground clip to the Type 191 Output connector edge and touch the probe tip to the connector center conductor. With the Type 3A5 MANUAL VOLTS/DIV switch at 10 mV , the display should be about 2.5 divisions peak to peak and 10 complete cycles.
d. Set the Type 191 Amplitude Range switch to .55 V and press the probe SEEK button. The display will first extend past the top and bottom of the screen and ther as the probe SEEK button is pressed, both the vertical amplifier and the time base will respond. The display will be atout five divisions peak to peak depending upon the POSITION control affect on the display, and as many cycles as the time base is calibrated to display.

## 20. Check SEEK Cycle Time

Requirement-Type 3A5 seeks for proper deflection fa:tor once every two to four seconds (after holding SEEK buiton pressed the preceding five seconds).
a. With the connections and signal as in step 19D, hold the P6030 Probe SEEK button pressed. After the first five seconds, count the number of seconds between times the system seeks for a new deflection factor. (A wrist watch second hand is adequate as a time reference.)

## 21. Check SEEK Selected DISPLAY SIZE Limits

Requirement-All SEEK selected displays will either bring display limits within 3.5 divisions of the graticule centerline,
or will seek to $50 \mathrm{~V} /$ DIV and leave all or part of the display outside the limits.
a. With the connections and signal as in Step 20, carefully balance the display to be equally above and below the graticule centerline.
b. Hold the SEEK button depressed and slowly increase the display amplitude with either the signal generator Variable control or the Type 3A5 VARIABLE control until the display size is automatically reduced. Note the display top and bottom points at the time the display size is reduced by slightly reducing the signal with the same Variable control, and then increasing it again and watching the point at which the display size is reduced. Neither the top nor the bottom of the display will extend past 3.5 divisions from the graticule centerline.
c. Holding the SEEK button depressed, slowly position the display up (or down) and note that the display size will continue to be reduced as the display zero level reaches the previously measured limits. The deflection factor will rest at $50 \mathrm{~V} / \mathrm{DIV}$ as soon as the display zero level has been taken at least $3 / 4$ minor division past either the plus or minus dynamic signal limit.

## SECTION 6 <br> CALIBRATION

## General

Recalibrate the Type 3A5 after each 500 hours of operation, or every six months if used intermittently. It nay also be necessary to recalibrate certain sections of the instrument when tubes, transistors, or other components are replaced. Before recalibrating the instrument, clean it as outlined in Section 4.

## NOTE

The performance standards described in this section of the manual are provided strictly as guides to calibration of the Type 3A5 and should not be construed as advertised performance specifications. However, if the Type 3A5 performs within the guide tolerances given in the calibration procedure, it will also perform as listed in the Characteristics section of this manual.

This section of the instruction manual presents a step-bystep calibration procedure. The title of each step identities the step as adjustment or verification. All adjustments must be completed in the order given and none should be omitted. Proper overall operation of the Type 3A5 is ensured when all steps in the procedure are completed.

Do not set any screwdriver controls to midrange as a preliminary to recalibration. Presetting controls to midrarige will only require more time to completely recalibrate the instrument.

## Equipment Required

Equipment required for the complete calibration of the Type 3A5 is shown in Fig. 6-1 and Fig. 6-2 and listed beliw. Alternate equipment may be substituted for that listed, if the performance specifications of the substituted equipment meet the particular requirements of the test. All test equipment must be calibrated and in good working order.

1. Test oscilloscope with a deflection factor of $5 \mathrm{mV} /[\mathrm{IV}$ minimum, and bandwidth of at least 25 MHz at $0.02 \mathrm{~V} / \mathrm{DIV}$, such as Tektronix Type 543B Oscilloscope with either Ty pe IAl or Type L Plug-In Unit.
2. Type 561 A Oscilloscope in which to operate the Type $3 A 5$; with Type 3B5, 3B4 or other time-base unit that will normally be used with the Type 3A5.
3. Sine-wave signal generator with constant amplitude continuously variable from 5 mV to 10 V peak to peak. Tektronix Type 191 Constant Amplitude Signal Generator is recommended.
4. Fast-rise pulse generator with amplitude adjustable fr.sm 5 mV to 120 V peak to peak at a repetition rate of apprcximately 1 kHz . Risetime of 2.3 ns or less into $50 \Omega$ at 400 kHz , and 40 mV peak to peak. For example, Tektronix Type 106 Square-Wave Generator.
5. Variable line voltage autotransformer, such as General Radio VARIAC Type W10MT3W, metered, 600 watt rating.
6. Low frequency sine wave oscillator with output frequency of 10 Hz at an amplitude of 10 mV peak to peak. Example, Heathkit Model IG-72 Audio Generator.
7. Accurate-amplitude signal generator of approximately 1 kHz square-wave repetition rate; voltage from 0.2 mV to 100 V with accuracy of $\pm 0.25 \%$. Tektronix Standard Amplitude Calibrator 067-0502-00 recommended.
8. 24 pF Input Time Constant Standardizer with BNC connectors, Tektronix Part No. 011-0067-00.
9. $50 \Omega$ in-line termination ( $\pm 1 \%$ accuracy) with BNC connectors, Tektronix Part No. 011-0049-00.
10. Two $50 \Omega$ 10:1 attenuators with BNC connectors, Tektronix Part No. 011-0059-00.
11. Two (one required, two can be used) GR Type 874 connector to BNC adapters. General Radio 874-QBJA, Tektronix Part No. 017-0063-00.
12. $50 \Omega$ coaxial cable 3 or 4 feet long with BNC connectors. For example, 42 inch Tektronix cable, Part No. 012-0057-00.
13. Two $10 \times$ attenuator probes, such as Tektronix P6006 $10 \times$ Probe with BNC connector, Part No. 010-0127-00.
14. $1 \times$ probe with BNC connector, such as Tektronix P6028, Part No. 010-0074-00.
15. Flexible plug-in extension cable, Tektronix Part No. 012-0066-00.
16. BNC to clip lead adapter (for use with Heath IG-72 Audio Generator), Tektronix Part No. 013-0076-00.
17. Bench multimeter with ohmmeter, such as Simpson 262, 20,000 ohms/volt.
18. Non-metallic capacitor adjusting tool, such as $1 / 4$ inch diameter plastic rod, sharpened to a screwdriver point at one end (not shown).
19. Plastic handle capacitor adjusting tool with small metal bit, such as Walsco No. 2519. Tektronix Part No. 003-0003-00.
20. Plastic coil adjusting tool with handle. Tektronix Part No. 003-0307-00.
21. Small screwdriver for adjusting front-panel screwdriver controls. (not shown.)
22. A dc resistance bridge of $\pm 0.075 \%$ or better accuracy at $1 \mathrm{M} \Omega$. (Not shown.)
23. A power line 3 -wire to 2 -wire adapter. (Not shown.)


Fig. 6-1. Equipment required for calibration of the Type 3 A5.


Fig. 6-2. Calibration tools.

## CALIBRATION RECORD AND INDEX

This Calibration Record is provided as a convenient check list and record of calibration conditions. The step numbers and title are identical to the complete procedure that follows this check list. This abbreviated procedure may be photocopied without special permission from Tektronix for convenience of use or record keeping in the Calibration Laboratory.

## Type 3A5, Serial No.

## Calibration Date

$\square$ 1. Preliminary Control Check. Page 6-4.2. Measure Input Resistance. $1 \mathrm{M} \Omega \pm 0.75 \%$. Page 6-4.3. Oscilloscope Trace Alignment. Page 6.5.
4. Check Power Supplies. Page 6-7.

| Supply | Tolerance | Value | Max <br> Ripple | Value |
| :--- | :---: | :---: | :---: | :---: |
| +6.8 V | 6 to 7 V <br> at 117 VAC | - | no spec |  |
| +4.2 V | 4.0 to 4.3 V | - | 20 mV | - |
| +75 V | 70 to 85 V | - | 10 mV | - |5. Check Readout Lamps (Operating Modes). Page 6-7.

## VERTICAL AMPLIFIER

6. Preliminary Adjust Variable Balance. Page 6-8.7. Check Microphonics. Page 6-8.No Ringing microphonics. $\leq 0.2$ DIV max short ferm microphonics.8. Check Amplifier Balance. Page 6.8.9. Final Adjust Variable Balance. Page 6-9.10. Check Trace Drift. Page 6.9.
$\leq 0.4$ DIV max after 1 minute at 105 and then 125 VAC.11. Check DC Shift. Page 6-9.
$\leq 0.1$ div after 5 div de signal applied.12. Check AC-TRACE STABILIZED Operation. Page 6-9.13. Preliminary Adjust Amplifier Gain. Page 6-10.14. Check Input Grid Current. Page 6-1015. Check Amplifier Compression/Expansion. Page 6-13. $\leq 5 \%$ gain change at CRT pins.16. Check Amplifier Dynamic Range. Page 6-13. $\geq 185 \mathrm{~V}$ Peak to Peak for 10 div centered display. Value $\qquad$17. Check POSITION Range. Page 6-13.

Both top and bottom of 8 -division display can be positioned past graticule center.18. Check VARIABLE Range. Page 6-13.
$\geq 2.5: 1$.
19. Check Amplifier DC Voltage to CRT. Page 6-13. +165 V to +190 V at crt center. Value $\qquad$
20. Check Deflection Accuracies at $10 \mathrm{mV} / \mathrm{DIV}$ through $50 \mathrm{~V} / \mathrm{DIV}$. Page 6-13.21. Check Deflection Accuracies at 1,2 and $5 \mathrm{mV} /$ DIV. Page 6-15.22. Adjust Input Capacitance and Attenuator Compinsations. Page 6-18.23. Adjust Amplifier High Frequency Compensation: Page 6-20.24. Check Amplifier 10\% to $90 \%$ Risetime. Page 6-! 0 .25. Check Display Position Affect Upon Transient kesponse. Page 6-21.26. Check Vertical Amplifier Bandpass. Page 6-23.

Dc to $\geq 15 \mathrm{MHz}$. Amplifier 15 MHz response at $10 \mathrm{mV} / \mathrm{DIV}$ not less than 0.7 dc gain. Frequen $y$ : _-_ MHz27. Check Signal/Trigger Amplifier Dc Output Voltasue. Page 6-26. $\leq \pm 1.5 \mathrm{~V}$.28. Check Signal/Trigger Amplifier Gain. Page 6-:'6. At $10 \mathrm{mV} / \mathrm{DIV}: 2 \mathrm{mV}$ square-wave sig; $\geq 0 . \approx \mathrm{V}$ peak to peak out. Value_
50 mV square-wave sig; $\geq 5 \mathrm{~V}$ peak to peak out. Value
29. Check Signal/Trigger Amplifier High and Low Fequency Response. Page 6-26.
At 10 mV /DIV: Set display 1 div 50 kHz . Output must not be less than 0.7 of 50 kHz amplitude at 8 MHz . Amplitude: \%

Set display 1 div 10 Hz . Output must be $\geq 0.1 \mathrm{~V}$ peak to peak. Value

## AUTOMATIC CIRCUITS

30. Adjust DISPLAY SIZE Control, R703. Page 6-26. Trace trip levels: +_ DIV, ____ DIV.
31. Check SEEK Operation at 20 MHz and 30 Hz . Page 6-28.
32. Check REMOTE SEEK Operation. Page 6-28.

SEEK pulse sent to time-base when remote seek button pressed.
33. Check SEEK Multi Pulse and Cycle Time. Page 6-30. SEEK Pulse on time: $\geq 200 \mathrm{msec}$. Time Cycle time after first 5 sec , between 2 and 4 seconds. Time.

System must seek to $50 \mathrm{~V} / \mathrm{DIV}$ in less than 200 msec .

## CALIBRATION PROCEDURE

## Preliminary

The deflection factor calibration (Step 21), tive attenuator compensation (Step 22) and the input stage grid current measurement all require that the input resistance value be known. Perform the first two steps of this calibration procedure with the Type 3A5 out of the oscilloscope. All other checks and performance limits are valid only after the system has operated for at least twenty minutes at normal room temperature.

## 1. Preliminary Control Checks

a. Check all front panel controls for proper indexing. Check the variable controls for smooth operation. Check that the micro switch at the rear of the VARIABLE shaft functions at the CAL detent position. Correct any defects found before proceeding.

## 2. Measure Input Resistance

a. Use a dc resistance bridge to measure the Type 3A5 input resistance.
b. Lay the instrument on its right side, with the Vertical Amplifier board up. Connect the bridge between the chassis (front panel ground terminal) and the white wire with black tracer out the rear of the attenuator shield. Measure and record the resistance value.

## 3. Adjust Oscilloscope Trace Alignment (O)

a. Install the Type 3A5 in the Type 561 A vertical compartment and the appropriate time-base in the horizontal compartment. Connect the oscilloscope power cord to the variable autotransformer output. Set the autotransformer for 117 volts output and turn on the oscilloscope power switch.
b. Set the instrument controls as shown under Fig. 6-3 and obtain a trace on the Type 561A crt.
c. Physically orient the Type 561A in the position in which it will remain during this calibration procedure. Adjust the oscilloscope Alignment controls so that the no-signal trace is parallel to the horizontally scribed graticule lines.


Fig. 6-3. Test setup for checking power supplies.

## Control Settings

Type 3A5

| POSITION | Midrange |  |
| :--- | :---: | :---: |
| MANUAL VOLTS/DIV | 10 mV |  |
| VARIABLE | CAL |  |
| Input Coupling | AC |  |
| Mode | MAN |  |
|  | Time |  |
|  | Base |  |
| Position | Midrange |  |
| Trigger Mode | Auto |  |
| Triggering Level | As required |  |
| Time/Div | 2 msec |  |
| Variable | Cal |  |
| Slope | + |  |
| Coupling | AC |  |
| Source | Int |  |

Type 561A

## Power

Calibrator
Focus
Intensity

On
Off
As required
Counterclockwise

Test Oscilloscope

| Trigger Slope | + Line |
| :--- | :--- |
| Triggering Mode | AC |
| Stability | Preset |
| Triggering Level | Midrange |
| Horizontal Display | Normal |
| Sweep Switch | Normal Sweep |
| Horizontal Position | Midrange |
| Intensity, Focus, | As Required |
| Astigmatism, Scale Illum | As Required |
| Amplitude Calibrator | Off |

## Type 1 Al

Mode
Norm/Invert
Variable Volts/Cm
Volts/Cm
Input Selector (both)

Ch 1
Norm
Calib
.005 Ch 1
AC

## Connections

Connect the P6028 $1 \times$ Probe to the Type 1 A1 Channel 1 input connector. Connect the probe ground clip to the Type $3 A 5$ rear panel. Connect the voltmeter negative lead to the ground post on the Type 3 A5 front panel.


Fig. 6-4. Power Supply test points.

## WARNING

Avoid the leads and connections at the bottom end of the large tan-colored $1.05 \mathrm{k} \Omega$ resistor. The two lower terminals rest at about +170 volts.

## 4. Check Power Supplies

a. Change the Time Base Trigger Mode switch to Norm so the trace disappears. Make the power supply check without a sweep running.
b. Measure the voltage at each of the test points shown in Fig. 6-4. The meter must be correct to within $\pm 1 \%$, or have a scale that is corrected to $\pm 1 \%$ at the voltages listed. Tolerances are listed in Table 6-1.

TABLE 6-1
Power Supply Tolerances and Ripple

| Supply | Tolerance | Maximum Ripple <br> Peak to Peak |
| :---: | :---: | :---: |
| +6.8 V | 6 to 7 V <br> at 117 VAC | No spec. |
| +4.2 V | 4.0 to 4.3 V <br> $\pm 1 \%$ at limits | 20 mV |
| +75 V | 70 to 85 V <br> $\pm 1 \%$ at limits | 10 mV |

c. Measure the ripple voltage on the 4.2 - and 75 -volt supplies with the test oscilloscope and 1 X probe. Use the test points shown in Fig. $6-4,20 \mathrm{mV}$ equals four divisions, and 10 mV equals two divisions on the test oscilloscope cr .

## 5. Check Readout Lamps (Operating Modes)

a. The test setup remains the same as for Step 4.
b. Set the Time-base Trigger Mode switch to Auto. Obtain a trace. Control settings used in step 4 should cause the following readout lamps to now be lighted: $A C, 1,0, m$ and V/DIV in the readout panel, and the MAN Mode button.
c. Set the Input Coupling to AC-TRACE STABILIZED and position the trace to the graticule centerline. The AC lamp must be lighted. Set Input Coupling to $A C$ and then to $D C$. The $A C$, and then the DC lamps should light. Return the Input Coupling switch to AC-TRACE STABILIZED. Center the trace.
d. Set the MANUAL VOLTS/DIV switch to 1 mV . The readout should now be $A C_{;} 1 \mathrm{mV} /$ DIV, and the MAN button should be lighted. Operate the MANUAL VOLTS/DIV switch through each step up to $50 \mathrm{~V} /$ DIV and note that the readout agrees with the switch position at each step.
e. Press the gray unlabeled $10 \times$ probe switch (SW70) located just above the INPUT connector. Note that the readout changes to WITH PROBE and $.5 \mathrm{KV} / \mathrm{DIV}$.


Fig. 6-5. Trunsistor locations, step 8.
f. While holding the $10 \times$ probe switch depressed, uperate the MANUAL VOLTS/DIV switch through the prisitions from $50 \mathrm{~V} /$ DIV to $1 \mathrm{mV} / \mathrm{DIV}$. Notice that the readrot is 10 times greater than the switch reading at each position. Release the $10 \times$ probe switch.
g. Turn the VARIABLE control left, then right from its detent CAL position. Note that the V/DIV lamp goes sut and the red UNCAL lamp turns on. Return the VARIABLE control to CAL. Return the MANUAL VOLTS/DIV switch to 10 mV .
h. Press the SEEK button. The display should read AC and $10 \mathrm{mV} / \mathrm{DIV}$, and the SEEK button should light. Turn the MANUAL VOLTS/DIV switch to 20 mV . The SEEK li.ght should go out, and the MAN button should light. Press and hold the EXT button, and note that only the V/[IIV lamp comes on. Other lamps may light, or may light only dimly. This does not indicate a problem. Release the EXT button. Set the MANUAL VOLTS/DIV switch to 10 mV , and the Input Coupling switch to $A C$.

## 6. Preliminary Adjust Variable Balance VAR BAL, R300

a. Test setup remains as in Step 5.
b. Turn the VARIABLE control counterclockwise. Note ciny shift of the trace. Return the VARIABLE control to CAL, and by use of the VAR BAL control, shift the trace in the
same direction about one and one-third times as far as it moved when the VARIABLE control was rotated. Repeat this procedure until there is no vertical shift of the trace throughout the full rotation of the VARIABLE control. Return the VARIABLE control to CAL.

## 7. Check for Microphonics

a. Test setup remains as in Step 6.
b. Tap the top of the oscilloscope front panel with the fingers of one hand. The trace should show no prolonged ringing-type microphonics, and no short-term microphonics of greater amplitude than 2 minor divisions.

## 8. Check for Balance

a. Test setup remains the same as in step 7.
b. Set the Input Coupling switch to DC.
c. Note the trace position. Remove both Q134 and Q334 and re-insert the transistors in reverse positions. See Fig. 6-5F or transistor locations. Trace shift as a result of changing the transistors must not be greater than 2 divisions. If the trace shift is more than 2 divisions, replace the transistors one at a time until you have a pair that will cause a trace shift of 2 divisions or less when their positions are reversed. Readjust the VAR BAL control as directed in Step 6.
d. Repeat the procedure of Step c with Q154 and Q354. Again, trace shift must not be more than 2 major graticule divsions when the transistor positions are reversed.

## 9. Final Adjust Variable Balance VAR BAL, R300

a. Repeat the procedure described in Step 6 until no vertical trace shift occurs when the VARIABLE control is turned throughout its range.

## 10. Check Trace Drift

a. Test setup remains the same as for Step 8.
b. Set the line voltage autotransformer to deliver 105 volts rms to the oscilloscope. Allow one minute for the trace position to stabilize. Position the trace to the graticule centerline. Change the autotransformer selting to deliver 125 volts rms to the oscilloscope. After one minute, the trace must not have drifted more than 0.5 major graticule division. Return the autotransformer output to 117 volts.

## 11. Check DC Shift

a. Test setup remains as in Step 10.
b. Set the Type 3 A5 MANUAL VOLTS/DIV control to 5 VOLTS. Set the bench multimeter to an ohms range with internal 1.5 volt battery.
c. Connect one ohmmeter lead to the Type 3A5 front panel ground terminal. Touch the other lead to the INPUT connector center conductor and note the direction of trace shift. Remove the lead from the input. Position the trace three divisions in the direction opposite to trace shift, and set the MANUAL VOLTS/DIV switch to .2 VOLTS. Touch the ohmmeter lead to the INPUT center conductor again, and adjust the VARIABLE control for a trace change of 5 divisions from zero input volts. Remove the meter lead from the input and wait one minute.
d. Touch the meter lead to the INPUT center conductor and carefully watch the trace. There should be no more than $\pm 5 \%$ slow trace shift after the meter lead is connected. $(5 \%=1.25$ minor division). Remove the meter leads.

## NOTE

This step checks the thermal compensations in the amplifier, and can reveal a weak cathode in an output tube.


Fig. 6-6. Shorting ert vertical deflection pins, step 12.

## 12. Check AC-TRACE STABILIZED Operation

a. Test setup remains as in Step 11.
b. Set the Type 3A5 VARIABLE control to CAL and the MANUAL VOLTS/DIV switch to 10 mV .
c. Position the trace to the graticule centerline. Use a non-magnetic tool or wire (with insulation for the hands) and short the ert vertical deflection pins together. See Fig. 6-6. Note the trace position on the crt. This is the crt electrical center.

## CAUTION

No not short either pin to ground, or the Output Amplifier may be damaged.
d. Remove the shorting tool and position the trace to the crt electrical center. Change the Input Coupling switch to AC-TRACE STABILIZED. The trace will disappear, but will return quickly. It must return to within one major division of the crt electrical center. Set the Input Coupling to $A C$.
e. Position the trace to the top graticule line. Change the Input Coupling Switch to AC-TRACE STABILIZED. The trace must return at least one major division toward the graticule centerline.
f. With the Input Coupling at AC-TRACE STABILIZED and the trace position as at the end of Step $e$, change the MANUAL VOLTS/DIV switch to 5 mV . The trace should not shift from its $10 \mathrm{mV} /$ DIV position.


Fig. 6-7. Test setup for adjusting Vertical Amplifier gain.

## Control Settings

## TYPE 3A5

| MANUAL VOLTS/DIV | 10 mV |
| :--- | :---: |
| VARIABLE | CAL |
| Input Coupling | DC |
| Mode | MAN |
|  | Time Base |
| Time/Div | $\mathbf{1} \mathrm{msec}$ |
| Variable | Cal |
| Trigger Mode | Auto |
| Triggering Level | Midrange |
| Slope | + |
| Coupling | AC |
| Source | Int |

## Standard Amplitude Calibrator

Amplitude
Mode
Mixed
$\times 100$ Amplifier

50 mvolts
Square-wave
Up
Optional

## Connections

Install a BNC $50 \Omega$ coaxial cable from the calibrator right side Output connector to the Type 3A5 INPUT connector.

## NOTE

The Standard Amplitude Calibrator must be turned on for at least fifteen minutes before using it in the following step.

## 13. Preliminary Adjust Amplifier Gain, CAL Control, R186

a. Set up the equipment and controls as shown in Fig. 6.7.
b. Obtain a square-wave display and adjust the frontpanel CAL control for exactly five divisions deflection. Do not include the trace thickness in the adjustment.

## 14. Check Input Grid Current

a. Leave equipment controls as set, but remove the coax from the Type 3A5 INPUT connector. The Standard Amplitude Calibrator will be used again in step 15.
b. Position the trace to the graticule centerline. Short the INPUT connector center conductor to ground and note any trace shift. The trace must not shift more than 0.2 division, indicating a grid current of $\pm 2$ nanoampere maximum.
c. If the grid current is greater, change V113. Normally grid current decreases with use of V 113 , so if the grid curlent is greater than 2 nanoamperes, it can mean the tube will soon fail in other ways also.
d. If V 113 is replaced, the Type 3A5 must operate for at least 20 minutes before making the grid current test again. Then, if the new tube grid current is marginally greater than allowed, proceed with the rest of this procedure, and check
grid current again after several hours use. Normally, tubes used for V113 will noticeably decrease grid current in the first ten hours of operation in a circuit that allows normal plate current flow.

After V113 selection provides a tube with grid current within limits, recheck for microphonics as in Step 7; readjust the VAR BAL control as in Step 9 and check trace drift as in Step 10.


Fig. 6-8. Test setup for checking compression/expansion.

## Control Settings

Type 3A5

| MANUAL VOLTS/DIV | 10 mV |
| :--- | :--- |
| VARIABLE | CAL |
| Mode | MAN |
| Input Coupling | AC |

## Time Base

| Time/Div | 1 msec |
| :--- | :--- |
| Variable | Cal |
| Trigger Mode | Auto |
| Triggering Level | Midrange |
| Slope | + |
| Coupling | AC |
| Source | Int |

Standard Amplitude Calibrator

| Amplitude | $\mathbf{2 0}$ mvolts |
| :--- | :--- |
| Mode | Square-wave |
| Mixed | Up |
| $\times 100$ Amplifier | Optional |

Test Oscilloscope
Trigger Slope
$+\ln t$

Triggering Mode
Stability
Triggering Level
Time / Cm
Variable
Horizontal Display
Sweep Switch
Horizontal Position
Type 1A1

| Volts/Cm (both) | 1 |
| :--- | :--- |
| Variable Volts/Cm | See Step 15 |
| Channel 1 Norm/Invert | Norm |
| Channel 2 Norm/Invert | Invert |
| Mode | Add |
| Input Selector (both) | AC |

## Connections

Connect a 50 ohm (BNC connector) coaxial cable from the Calibrator right side Output connector to the Type 3A5 INPUT connector. Connect two $10 \times$ probes to the Type 1A1 input connectors. Compensate both probes, and check that the display gain (. $05 \mathrm{~V} / \mathrm{Cm}$ Gain) control of both channels is properly adjusted. Connect the two probe ground clips to the Type 3A5 chassis, and the probe tips to the crt vertical deflection plate pins. See Fig. 6-8.

## CAUTION

Do not let either probe tip touch the crt shield Be careful not to apply unnecessary pressure with the probes to the crt neck pins.

## 15. Check Amplifier Compression/Expansion

a. Set up test equipment and connections as shown in Fig. 6-8.
b. Obtain a stable, centered two-division display on the Type 561 A cr , and a stable 5 -division display on the rest oscilloscope. (Use Channel 1 Variable Volts/Cm control to set the test oscilloscope display to 5 divisions.)
c. Position the Type 561A display so that the waveform top rests on the top graticule line. After the ac-coupled test oscilloscope display settles down, record its peak topeak amplitude, compared to its previously-set 5 -division amplitude.
d. Position the Type 561A display so that the waveform bottoms rests at the bottom graticule line. After the accoupled test oscilloscope display has settled down, record its peak-to-peak amplitude as compared to the original 5divisions.

The measurements described above should be molde between the end of a positive half-cycle and the beginning of a negative half-cycle, near the test oscilloscope crt center. Compression or expansion of the Type 3A5 vertical amplifier gain as seen on the test oscilloscope must not be greciter than 5\% ( 1.25 minor divisions).

Any compression or expansion greater than $\pm 5 \%$ an probably be traced to transistor unbalance in step 8, or to unbalance Output Stage tubes or transistors.

## 16. Check Amplifier Dynamic Range

a. Test equipment setup remains as in step 15. Charige the controls as follows:

## Standard Amplitude Calibrator

Amplitude
. 1 volts
Type 3A5
No change
Type 1A1
Volts/cm (both)
5
Variable Volts/cm (both) Calib

Type 543B

## No change

b. Center the Type 561A two-division display. Charige the Standard Amplitude Calibrator AMPLITUDE control to . 1 volts. The display will now be approximately 10 divisisus peak to peak, and the top and bottom should both be out of sight above and below the crt edges.
c. The test oscilloscope deflection factor is 50 volts $/ \mathrm{cm}$. The display should be $\geq 185$ volts peak to peak. Remove the $10 \times$ probes from the Type 561A crt neck pins.

## 17. Check Amplifier POSITION Range

a. Test setup remains as in Step 16. However, the test oscilloscope is not used. Change the Standard Amplitude Calibrator Amplitude control to 50 mvolts . Adjust the Type 3 A5 VARIABLE control to obtain a six division peak-to-peak display.
b. Change the Calibrator Amplitude control to .1 volts. The Type 3A5 POSITION control must now be able to position the display bottom above the graticule centerline, and the display top below the graticule centerline.

If the POSITION control cannot position the display sufficiently, check the Driver and Output Stage transistors and tubes.

## 18. Check VARIABLE Range

a. Test setup remains the same as in Step 17.

## Control Settings

| Standard Amplitude Calibrator |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Amplitude | $\mathbf{5 0}$ mvolts |  |  |  |
| Type |  |  |  | 3A5 |
| MANUAL VOLTS/DIV | 10 mV |  |  |  |
| VARIABLE | CAL |  |  |  |
| Input Coupling | DC |  |  |  |

b. Check that the Type 561A crt display is five divisions peak to peak.
c. Turn the VARIABLE control fully counterclockwise. The display must be between 2.8 and 3.6 divisions peak to peak in vertical height. Record the display size.
d. Set the Calibrator Amplitude control to 20 mvolts. Turn the VARIABLE control fully clockwise. Display amplitude must be equal to or greater than the amplitude shown in Step c. Return the VARIABLE control to CAL.

## 19. Check Amplifier DC Voltage to CRT

a. Disconnect the $50 \Omega$ coaxial cable from the Type 3 A5 INPUT connector. Do not turn off the Standard Amplitude Calibrator, since it will be used again in the next step.
b. Position the trace to the crt electrical center which was located in Step 12.
c. Use the $20,000 \Omega / \mathrm{V}$ bench multimeter, set to at least a 400 volt range ( $\geq 8 \mathrm{M} \Omega$ meter resistance) to measure the dc voltage at either crt vertical deflection plate pin. The voltage must be between +165 and +190 volts $\pm 3 \%$.

## 20. Check deflection accuracy at $10 \mathrm{mV} / \mathrm{DIV}$ through 50 V/DIV.

a. Reconnect the Standard Amplitude Calibrator coaxial cable to the Type 3A5 INPUT connector. Set the Calibrator Amplitude control to 50 mvolts .

b. DEFLECTION ACCURAEY $+3 \%$ ( $+3 / 4$ MINOR DIV)

c. DEFLECTION ACCURACY $-3 \%(-3 / 4$ MINOR DIV).

a. DEFLECTION ACCURACY $\pm 0 \%$.

b. DEFLECTION ACCURACY $+3 \%$ ( $+2 / 3$ MINOR DIV).

c. DEFLECTION ACCURACY $-3 \%(-2 / 3$ MINOR DIV $)$

Fig. 6-9. Deflection accuracy limits between $10 \mathrm{mV} / \mathrm{DIV}$ and 50 V/DIV when VOLTS/DIV has the number 1 or 2 in it.

Fig. 6-10. Deflection accuracy limits between $10 \mathrm{mV} / \mathrm{DIV}$ and 50 V/DIV when VOLTS/DIV has a number 5 in it.
b. Use Table 6-2 and Figures 6-9, 6-10 and 6-11 to determine the deflection accuracy at each setting of the MANUAL VOLTS/DIV switch between $10 \mathrm{mV} / \mathrm{DIV}$ and $50 \mathrm{~V} /$ DIV. If any one switch setting causes an out-of-tolerance display, record the amount of error, continue to 50/DIV, then return to $10 \mathrm{mV} / \mathrm{DIV}$ and adjust the CAL control. Adjust the CAL control to reduce the one error, but not far enough to !!ive any other switch setting an opposite out-of-tolerance error. The CAL control is correctly adjusted when all ranges are within $3 \%$, and $10 \mathrm{mV} /$ DIV is not necessarily at zero per cent error. If one switch position causes a plus error greater than $+3 \%$ and another causes a minus error greater than $-3 \%$, record the error of all switch settings in ordel to determine which attenuator requires repair.

TABLE 6-2
Vertical Deflection Accuracy Check

| MANUAL <br> VOLTS/DIV <br> Switch <br> Setting | Standard <br> Amplitude <br> Calibrator <br> AMPLITUDE <br> Control | Vertical <br> Deflection <br> In | \%ivisions Erroı, <br> See Fig <br> 6-9 thru <br> Fig. 6-13 |
| :---: | :---: | :---: | :---: |
| 1 mV | 5 mV | 5 | $\pm 5 \%$ |
| 2 mV | 10 mV | 5 | $\pm 5 \%$ |

## 21. Check deflection accuracy at 1, 2 and 5 mv/DIV

a. With the Standard Amplitude Calibrator connected, set Type 3A5 MANUAL VOLTS/DIV switch to 10 mV . Set the Calibrator Amplitude control to 50 mvolts. Set the $\mathrm{T}_{>}$pe 3A5 Input Coupling switch to AC-TRACE STABILIZED and center the display vertically.
b. Set the Calibrator Amplitude control to 5 mvolts, and the Type 3A5 MANUAL VOLTS/DIV switch to 1 mV . The display must be 5 divisions peak to peak $\pm 5 \%$ as shown in Fig. 6-12. Use Table 6-2 and Figs. $6-12$ and $6-13$ for 1,2 and $5 \mathrm{mV} /$ DIV checks. If all three checks show the gain to be either high or low, check the Output Amplifier cathode circuit.

b. DEFLECTION ACCURACY $+3 \%$ (+0.3 MINOR DIV).

c. DEFLECTION ACCURACY $-3 \%$ ( -0.3 MINOR OIV).

Fig. 6-11. Deflection accuracy limits at 50 V/DIV.

Calibration-Type 3A5


Fig. 6-12. Deflection accuracy limits at 1 and $2 \mathrm{mV} /$ DIV.

a. DEFLECTION ACCURACY $\pm 0 \%$.

b. DEFLECTION ACCURACY $+5 \%$ ( +1 MINOR DIV).

c. DEFLECTION ACCURACY $-5 \%$ ( -1 MINOR DIV)

Fig. 6-13. Deflection accuracy limits at $5 \mathrm{mV} /$ DIV.


Fig. 6-14. Test setup for adjusting input capacitance and attenuator compensations, 5tep 22.

## Control settings

Type 106
Repetition Rate Range
Multiplier
Symmetry
Amplitude
Hi Amplitude Fast
Rise Switch
Fast Rise controls

| Triggering Level | Midrange |
| :--- | :--- |
| Slope | + |
| Coupling | AC |
| Source | Int |

## Connections

Install the Input RC Standardizer on the Type 3A5 INPUT connector. Install the BNC $50 \Omega$ termination on the Input RC Standardizer. Connect a $50 \Omega$ BNC cable to the termination. The signal generator recommended is the Tektronix Type 106. A Tektronix Type 105 will work equally well, and does not require a GR to BNC connector adapter.

Install one $10 \times 50 \Omega$ attenuator on the signal generator high amplitude Output connector. Use the GR to BNC adapter with the Type 106.

Connect the $50 \Omega$ cable to the $10 \times$ attenuator and check that the oscilloscope focus control is properly adjusted for a sharply defined display.

## 22. Adjust Input Capacitance and Attenuator Compensations

a. Make the connections and set the controls as stated under Fig. 6-14. Set the square-wave generator Amplitude control for a display of four divisions peak to peak.
b. Check the input capacitance by observing any spike or rolloff of the square-wave leading edge for approximately 0.02 msec . A difference of 1 pF in input capacitance as compared with the Standardizer capacitance will cause approximately 1 minor vertical division of spike or rolloff -an error greater than the allowed $3 \%$ peak-to-peak aberration limits of $2 / 3$ minor division.
c. Use item 19 of Equipment Required, and adjust C70 (attenuator adjustment locations shown in Fig. 6-15) so there is no spike, rounding or rolloff of the display. Use a time base sweep rate of $1 \mathrm{msec} / \mathrm{div}$ to obtain a display with the proper resolution. Set the sweep rate back to $0.1 \mathrm{msec} / \mathrm{div}$.
d. Use Table 6.3 and Fig. 6-16 while adjusting the input attenuator compensating capacitors. Start at $10 \mathrm{mV} /$ DIV and work to $50 \mathrm{~V} /$ DIV, adjusting the Calibrator Amplitude control and removing the attenuator, termination and standardizer when higher deflection factors make it no longer possible to obtain four divisions of display.
e. Install a 3 -wire to 2 -wire power cord adapter at the Type 106 power connector, to eliminate 60 Hz ground current signals that may be displayed at 1,2 and $5 \mathrm{mV} /$ DIV.


Fig. 6-15. Lecation of attenvator and input capacitance adjustments.

Install two $10 \times$ attenuators to the square-wave generator Output and the $50 \Omega$ termination to the Input RC Standardizer. Set the square-wave generator Amplitude control fully counterclockwise.

TABLE 6-3
Step 22d Operating Conditions

| MANUAL <br> VOLTS/ <br> DIV <br> Switch <br> Setting | Use <br> $10 \times$ <br> Atten | Use <br> $50 \Omega$ <br> Term | Use <br> RC <br> Stand | Display <br> Divisions <br> Pk-to-pk | Adjust for <br> square <br> corner. Fig. <br> 6-16A/B | Adjust for <br> optimum <br> level. Fig. <br> 6-16C/D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 mV | X | X | X | 4 | none | C70 |
| 20 mV | X | X | X | 4 | C55D | C55A |
| 50 mV | X | X | X | 4 | C65D | C65A |
| .1 V |  | X | X | 4 | C15D | C15A |
| .2 V |  | X | X | 4 | check | check |
| .5 V |  | X | X | 4 | check | check |
| 1 V |  | X | X | 4 | C25D | C25A |
| 2 V |  |  | X | 4 | check | check |
| 5 V |  |  | X | 4 | check | check |
| 10 V |  |  | X | 4 | C35D | C35A |
| 20 V |  |  |  | 4 | check | check |
| 50 V |  |  |  | $\approx 2.2$ | check | check |


a. C25A Capacitance too large.

b. C25A Capacitance too smail. $0.1 \mathrm{msec} / \mathrm{div}$.

c. C25D Capacitance too small.

d. C25D Capacitance too large.
$1.0 \mathrm{msec} / \mathrm{div}$.

Fig. 6-16. Examples of sweep rate and display when adjusting attenuator capacitors. Signal $\approx \mathbf{2 k H z}$. Type 3 A5 VOLTS/DIV $=1 \mathrm{VOLT} / \mathrm{DIV}$.

## CAUTION

Maximum full-time peak-to-peak display with the $10 \times$ attenuator / $50 \Omega$ termination / Standardizer combination if 0.3 volt as displayed on the crt. It will be necessary to remove the attenuator beginning at $2 \mathrm{~V} /$ DIV deflection factor.

Set the Type 3A5 controls:

$$
\begin{array}{ll}
\text { MANUAL VOLTS/DIV } & 10 \mathrm{mV} \\
\text { VARIABLE } & C A L
\end{array}
$$

## Input Coupling <br> POSITION

## DC

for vertically centered display
f. Change the MANUAL VOLTS/DIV switch to 1 mV and position the display to the crt center. Increase the signal amplitude to display 4 divisions. The display should be similar to Fig. 6-17. The 5\% square-wave leading edge rolloff is due to limited high frequency response, and not to the attenuator.


APPROX. 2 kHz SIGNAL . $2 \mathrm{mS} / \mathrm{DIV}$.

Fig. 6-17. Normal square-wave display at 1,2 , or $5 \mathrm{mV} / \mathrm{DIV}$ when attenuators are correctly compensated at 10,20 , and $50 \mathrm{mV} / \omega \mathrm{IV}$.

## 23. Adjust Amplifier High Frequency Compensations

a. Test equipment remains the same as in Step 22, vith new connections and control settings as listed below:

## Control Settings

Type 3A5

| MANUAL VOLTS/DIV | 10 mV |
| :--- | :--- |
| VARIABLE | CAL |
| Input Coupling | DC |
| Mode | Man |

Type 106

| Repetition Rate Range <br> Multiplier | 100 kHz <br> Symmetry |
| :--- | :--- |
| Near 4 <br> Adjust for 50\% |  |
| Amplitude | duty factor |
| Hi Amplitude | Fully counterclockwise |
| Fast Rise Switch |  |
| + Amplitude | Fast Rise |
| -Amplitude | Fully counterclockwise |

## Time Base

## Time/Div

Variable
Trigger Mode
Triggering Level
$5 u \mathrm{sec}$
Cal
Auto
Midrange for triggered display

$\stackrel{+}{A C}$
Int

## Connections

Install the BNC $50 \Omega$ termination directly to the Type 3A5 INPUT connector. Install the GR to BNC adapter to the Type 106 Fast Rise +Output connector. Join the adapter and $50 \Omega$ termination with a $50 \Omega$ coaxial cable.

If a Type 105 is being used in place of the Type 106, install two $10 \times 50 \Omega$ attenuators on the OUTPUT connector, and connect the $50 \Omega$ cable to the second attenuator output.
b. Adjust the Type 106 +Amplitude control for a display of four divisions peak to peak. Proper transient response is shown in Fig. 6-19. Fig. 6-18 shows the portions of the display affected by the four high-frequency transient response controls; R153, C152, L526 and L536.
c. Before making any adjustments, carefully note the display, then switch the Input Coupling to $A C$ and then to AC-TRACE STABILIZED. The transient response should not be altered. Leave the switch at AC-TRACE STABILIZED.
d. If it is necessary to make any high frequency adjustments, start with C152. C152 will probably be finally adjusted near maximum capacitance, which produces the fastest rise, possibly with a very slight overshoot spike.
e. Next, adjust R153 to remove any severe spike or hump (Fig. 6-18A and B).
f. For final control of the display leading corner, adjust either L526, L536 or both as needed. For correct adjustment, it is important that both ferrite slugs be adjusted to about the same depth within the coils. Final adjustment of transient response controls is complete when the spike, rolloff, rounding or tilt is no greater than $\pm 3 \%$ (or $\pm 0.3$ minor division maximum) and the $10 \%$ to $90 \%$ risetime is $\leq 23 \mathrm{nsec}$ as checked in Step 24.

## 24. Check Amplifier 10\% to $\mathbf{9 0 \%}$ Risetime

a. Test setup remains as in Step 23.
b. Set Time Base controls

| Time/Div | $.05 \mu$ sec |
| :--- | :--- |
| Position | Display positioned <br> as in Fig. 6-20 |
| Other controls | No change |

c. Carefully measure the $10 \%$ to $90 \%$ rise of the leading edge of the display. The $10 \%$ point is two minor divisions up from the display bottom, and the $90 \%$ point is two minor divisions down from the display top. If a Type 106 is being used and the risetime is measured to be $\leq 23$ nsec, proceed to Step 25. ( $\leq 23 \mathrm{nsec}$ is stated as the limit for calibration, even though in Section 1 risetime is noted as $\leq 23.2$ nsec.


Fig. 6-18. Transient response displays that show which control is misadjusted. Signal: Type 106 Fast Rise at 400 kHz; Type 3A5: 10 mV/ DIV; Time Base: $0.5 \mu \mathrm{SEC} / \mathrm{DIV}$.

This change is because of the difficulty in visually resolving a display time duration of 0.2 nsec ). If a Type 105 is being used or the measurement and risetime is found to be $\leq 25$ nsec, proceed to Step 25. If risetime is too long for either condilion just stated, return to Step 23 and adjust L526/L536 for slightly more peaking, and re-adjust C152 to reduce the display peak back to its proper limits. Measure the risetime again. Several repetitions of Step 23 may be necessary before both aberrations and risetime are within proper linits.

## 25. Check Display Position Affect on Transient Response

a. Test equipment setup remains as in Step 24.
b. Set the Time Base Time/Div control to $.5 \mu \mathrm{sec}$ and the Type 3A5 Input Coupling to AC. All other controls remain at the same settings as in Step 24.


Fig. 6-19. Correct high frequency transient response. $\approx 400 \mathrm{kHz}$, at $0.5 \mu \mathrm{~S} / \mathrm{div}$ and $10 \mathrm{mV} / \mathrm{div}$.


Fig. 6-20. Difference in risetime measurement using Type 105 (A) and Type 106 FAST RISE (B).
c. Position the top of the display to the bottom graticule line as in Fig. 6-21A. Aberrations must not exceed $\pm 5 \%$ or $\pm 1$ minor division ( 2 minor divisions peak to peak).

## NOTE

Step 25 d and e cannot be performed if a Type 105 Square-Wave Generator is being used.
d. Position the display back to graticule center. Move the cable from the Type 106 OUtput connector to the -Output connector, and adjust the -Amplitude control for a display of 4 major divisions peak to peak.
e. Position the bottom of the display to the top line of the graticule as in Fig. 6-21B. Aberrations must not exceed $\pm 5 \%$.

a. 4 DIVISION DISP LAY POSITIONED DOWN.

b. 4 DIVISION DISPLAY POSITIONED UP.

Fig. 6-21. Position effect upon transient response, step 25.


Fig. 6-22. Test setup for checking the Vertical Amplifier bandwidth, $10 \mathrm{mV} /$ DIV .

## Control Settings

Type 3A5

| MANUAL VOLTS/DIV | 10 mV |
| :--- | :--- |
| VARIABLE | CAL |
| Input Coupling | AC |
| POSITION | Centered display |

Time Base
Time / Div
10 /sec
Variable
Trigger Mode
Triggering Level
Slope
Coupling
Source
Cal
Auto
Midrange for triggered display
$+$
Int
Type 191
Amplitude Range
Amplitude
Variable
Frequency Range
Frequency Control

Amplitude Range
$5-50 \mathrm{mV}$
Amplitude
Frequency Range
Frequency Control

## Connections

Install a $50 \Omega$ termination on the Type 3 A5 INPUT con. nector. Connect a GR to BNC adapter on the Type 191 Output connector. Join the adapter and termination with a $50 \Omega$ coaxial cable.

## 26. Check Vertical Amplifier Bandwidth

a. Make the connections shown in Fig. 6.22.
b. Obtain a 4 -division peak-1o-peak display as shown in Fig. 6.23A. Fig. 6-23 illustrates alignment of the top and bottom of a centered 4 -division peak-to-peak display, with the same side of the trace referenced to a graticule line at both top and bottom. This makes the amplitude measure. ment more precise, eliminating error due to trace width.
c. Change the Type 191 Frequency Range control to the $8-18$ range. Set the oscilloscope Time Base for a triggered sweep at $.05 \mu \mathrm{sec} / \mathrm{div}$. Check the peak-to-peak amplitude of the display. Then turn the Type 191 Frequency Adjust control slowly higher in frequency until the display amplitude is 2.8 divisions, as in Fig. 6-23B. Position the plus peak of
a sine wave to the graticule vertical center line for best viewing of the minor divisions of display. Record the trequency. The Type 191 Frequency Adjust dial must be at or above 15 MHz .
d. Insert a $10 \times$ attenuator between the $G R$ to BINC adapter and the $50 \Omega$ coax. Set the Type 191 for 50 kHz signal again. Set the Type 3 A5 Input Coupling to AC-TRACE STABILIZED and then the MANUAL VOLTS/DIV switch to 1 mV . Obtain a stable triggered four division display a' a sweep rate of $10 \mu \mathrm{SEC}$. Set the Type 191 VARIABLE control and the Type 3A5 POSITION control for a display like that of Fig. 6-23A.
e. Change the Type 191 Frequency Range control to $\therefore 66$ 8 and the time-base for a sweep rate of $.1 \mu \mathrm{sec}$. Turn the Frequency Adjust Control to 5 MHz and check the display amplitude to be 2.8 or more divisions peak to peak. If the display is greater than 2.8 divisions, turn the Freque icy Adjust control up in frequency, and record the frequency at which the display is 2.8 divisions peak to peak.

a. $50 \mathrm{kHz} .10 \mu$ SIV. 4 DIVISIONS.

b. $-15 \mathrm{MHz} .05 \mu \mathrm{~S}$ DIV. 2.8 DIVISIONS

Fig. 6-23. Bandpass measurement displays, step 26b and c.


Fig. 6-24. Test setup for checking Signal/Trigger Amplifier.

## Control Settings

Type 3A5


Type 1AI

| Volts/Cm (Ch 1) | .05 |
| :--- | :--- |
| Mode | Ch 1 |
| Variable Volts/Cm | Calib |
| Position | Trace at graticule center- |
|  | line |
| Norm/Invert | Norm |
| Input Selector | DC |

Type 543B

| Trigger Slope | + Int |
| :--- | :--- |
| Triggering Mode | Auto |
| Stability | Preset |
| Triggering Level | Midrange |
| Time $/ \mathrm{Cm}$ | 5 msec |
| Variable | Calibrated |
| Horizontal Display | Normal |
| Sweep Switch | Normal Sweep |
| Horizontal Pasition | Midrange |

Standard Amplitude Calibrator

| Amplitude | 2 mvolts |
| :--- | :--- |
| Mode | Square Wave |
| Mixed | Up |

Type 191

| Amplitude Range | 5.50 mV |
| :--- | :--- |
| Amplitude | 10 |
| Variable | 1 division display |
| Frequency Range | 50 kHz |
| Frequency Control | 8 of $3.6-8$ Range |
| IG-72 Audio Generator |  |


| Multiplier | $\times 1$ |
| :--- | :--- |
| Cycles (Left) | 10 |
| Cycles (Center) | 0 |
| Int/Ext $600 \Omega$ Load Sw | Int |
| Output Switch | $-40 / .01$ |
| Output Variable | For one division display |

## Connections

The test setup of Fig. 6-24 applies to the following three steps in the procedure. Install a $10 \times$ Probe on the Type 1A1 Channel 1 Input connector. Connect the probe groind clip to the Type $3 A 5$ vertical board, pin K, and the tip to the vertical board, pin J.

## 27. Check Signal/Trigger Amplifier DC Output Voltage

a. Set up the equipment and make the connections shown in Fig. 6-24.
b. With the Type 561A trace at the crt electrical center, the test oscilloscope trace do level must be within not more than 3 divisions above or below graticule centerline. The test oscilloscope is set for 0.5 volt per division-so 3 divisi nns equal 1.5 volts. Thus, the Type 3A5 trigger amplifier output dc level must be $\leq \pm 1.5$ volts as measured with the lest oscilloscope.

## 28. Check Signal/Trigger Amplifier Gain

a. Set the Type 3 A5 Input Coupling to AC-TRACE SIABILIZED. Set the Standard Amplitude Calibrator contiols as stated under Fig. 6-24. Connect a $50 \Omega$ coax from the Calibrator Output (right side) to the Type 3A5 INPUT connector. The Type 561A display should be 0.2 division prak to peak.
b. Change the test oscilloscope Type 1A1 Input Selector to $A C$ and the Volts $/ \mathrm{Cm}$ switch to $.01(0.1$ volt $/ \mathrm{cm}$ with $11 \times$ probe). Adjust the Type 543B triggering controls for a stable display. The Type 543B display amplitude must be $\geq 0.3$ rolt peak to peak.
c. Change the Type 1 Al Volts/Cm switch to .2. Charge the Calibrator Amplitude control to 50 mvolts. The est oscilloscope display must be $\geq 5$ volts peak to peak.
d. Change the Type 1 Al Volts/Cm switch to .005 . Change the Calibrator Amplitude control to .2 mvolts. Change the Type 3A5 MANUAL VOLTS/DIV switch to 1 mV . The est oscilloscope display must be at least 0.03 volts peak to peak, equal to at least 0.3 major divisions peak to peak.
e. Set the Type 1 Al Volts $/ \mathrm{Cm}$ switch to .01 . Set the $\mathrm{C} 1 \mathrm{li}-$ brator Amplitude control to 5 mV . The test oscilloscope display must be 0.5 volts or greater peak to peak, equal to 5 major divisions or greater peak to peak.
Leave the test oscilloscope probe as connected. Disc $n$ nnect the Standard Amplitude Calibrator.

## 29. Check Signal/Trigger Amplifier High and Low Frequency Response

a. Set the Type 3 A5 MANUAL VOLTS/DIV switch to 10 mV , and the Input Coupling to DC. Center the trace.

Set the test oscilloscope Time/Cm switch to $10 \mu \mathrm{SEC}$; he Type 1 Al Volts/ Cm switch to .02 .

Connect a $50 \Omega$ termination to the Type 3A5 INPUT connector. Install a $50 \Omega$ coax between the Type 191 Output connector and the termination. Set the Type 191 controls as stated under Fig. 6-24. The Type 561 A crt display should be set to 1 division peak to peak by adjusting the Type 191 Variable control.
b. Adjust the Type 1A1 Variable Volts/Cm control counterclockwise to obtain a test oscilloscope display exactly four divisions peak to peak.
c. Set the Type 191 Frequency Range switch to the 3-8 MHz range. Set the Frequency Adjust control for 8 MHz output. The test oscilloscope display must be $\geq 2.8$ divisions peak to peak.
d. Leave the test oscilloscope probe as connected. Disconnect the Type 191. Remove the $50 \Omega$ termination from the Type 3A5 INPUT connector.
e. Set the low frequency audio oscillator for 10 cycles output for a 10 mV peak-to-peak signal. Connect a $50 \Omega$ coax from the signal generator output to the Type 3A5 INPUT connector. If using the Heath IG-72, use item number 16 of Equipment Required between the generator output terminals and the coax. The clip lead to BNC adapter center conductor is the red lead. Adjust the signal generator output for 1 division peak to peak on the Type 561A crt display.
f. Set the Type 1 Al Volts/Cm to .01 and the Variable Volts/Cm to Calib. Set the Type 543B Time/Cm switch to 50 msec . The test oscilloscope display must be $\geq 1$ division ( 0.1 volt) peak to peak.

Disconnect the test oscilloscope probe and the low frequency signal generator.

## AUTOMATIC CIRCUITS

## 30. Adjust DISPLAY SIZE Control, R702

a. Test equipment remains the same as in Fig. 6-24. Remove the test oscilloscope $10 \times$ probe from the Type 3A5 circuits. It will be used again in Step 33. Remove any input signal.

## Control Settings

Type 3A5

| MANUAL VOLTS/DIV | 10 mV |  |  |
| :--- | :---: | :---: | :---: |
| VARIABLE | CAL |  |  |
| Input Coupling | DC |  |  |
| Mode | MAN |  |  |
|  | Time |  | Base |
|  |  |  |  |
| Time/div | .5 msec |  |  |
| Variable | Cal |  |  |
| Trigger Mode | Auto |  |  |
| Triggering Level | Midrange |  |  |
| Slope | + |  |  |
| Coupling | AC |  |  |
| Source | INT |  |  |

## Standard Amplitude Calibrator

## Amplitude

Mode
Mixed

## 50 mvolts

Square Wave
Up

## Connections

a. Beginning at Step 30d, use a $50 \Omega$ coax cable and connect the Calibrator right-side OUTPUT connector to the Type 3A5 INPUT connector.

## NOTE

This step is written for a DISPLAY SIZE adjustment to match the Characteristics stated in Section 1 of this manual. Other limits may be used at the option of the user.
b. With no input signal, obtain a free run trace. Position the trace above the graticule centerline until the overstan lamp (the small neon lamp located just above the POSITI()N control) turns on. Note the trace position. Move the truce below the graticule centerline until the overscan lamp turns on. Note the trace position.

The trace should have moved farther from graticule certer in one direction than in the other before causing the overscan lamp to light. Position the trace in the direction it moved farthest and set it exactly 3.5 divisions from graticule center. Record the trace position. Using a small scre.wdriver, adjust the DISPLAY SIZE control so that the oversian lamp blinks periodically. To find the correct DISPLAY SIZE setting, adjust the control so that the overscan lamp lights steadily, then back it off so the lamp blinks.
c. Position the trace to the opposite half of the graticule, and note the vertical position at which the overscan lamp starts blinking. This position must be no closer than 2.1 divisions from graticule center. Record the trace position. This DISPLAY SIZE limit represents maximum allowable error in vertical amplifier balance and crt electrical center. Normally, if the DISPLAY SIZE control is adjusted with the truce 3.5 divisions from center in one half of the graticule, the overscan lamp will blink only when the display is 3 or m re divisions from center in the other half.

Fig. 6-25 illustrates the worst-case limits of DISPLAY SIZE in a Type 561A system which has its electrical center 0.7 division from graticule center. Since this is the maximum allowable deviation in all oscilloscopes with which the T; pe 3A5 may be operated, Fig. 6-25 applies to all uses of the Type 3A5.
d. Make the connection stated in Step 30a.
e. Use Table 6-4 and determine that the automatic seeking circuit will operate the Type 3A5 deflection factor correctly through each attenuator range, starting at $10 \mathrm{mV} /$ [IV. Start by setting the Standard Amplitude Calibrator Amıli-


Fig. 6-25. Worst-case DISPLAY SIZE limits.
tude control at 50 mvolts. Hold the SEEK button depressed and advance the Amplitude control one step at a time according to Table 6-4.

If all deflection factors presented on the readout board are incorrect or erratic, a problem probably exists in the Display Comparator Multi and Gating circuits. If only one deflection factor readout is in error, or each deflection factor with a common number in its value is in error, the problem is probably in the Ring Counter circuits.

## TABLE 6-4

## Verification Of Automatic Deflection

Factor Selection

| Readout <br> Panel <br> Deflection <br> Factor | Standard <br> Amplitude <br> Calibrator <br> AMPLITUDE <br> Control | Vertical <br> Deflection <br> In Divisions | $\%$ Error |
| :---: | :---: | :---: | :---: |
| 10 mV | 50 mV | 5 | $\pm 3 \%$ |
| 20 mV | 0.1 V | 5 | $\pm 3 \%$ |
| 50 mV | 0.2 V | 4 | $\pm 3 \%$ |
| .1 V | 0.5 V | 5 | $\pm 3 \%$ |
| .2 V | 1 V | 5 | $\pm 3 \%$ |
| $\frac{2 \mathrm{~V}}{}$ | 2 V | 4 | $\pm 3 \%$ |
| 1 V | 5 V | 5 | $\pm 3 \%$ |
| 2 V | 10 V | 5 | $\pm 3 \%$ |
| 5 V | 20 V | 4 | $\pm 3 \%$ |
| 10 V | 50 V | 5 | $\pm 3 \%$ |
| 20 V | 100 V | 5 | $\pm 3 \%$ |
| 50 V | 100 V | $2^{1}$ | $\pm 3 \%: \pm 0.3$ |

${ }^{1}$ Obtained by positioning display top upward until deflection factor is changed to $50 \mathrm{~V} / \mathrm{DIV}$.

## 31. Check SEEK Operation At 20 MHz and 60 Hz

a. Disconnect the Standard Amplitude Calibrator.

## Control Settings

Type 3A5


| Amplitude Range | $5-50 \mathrm{mV}$ |
| :--- | :--- |
| Amplitude | 50 |
| Variable | Five division display |
| Frequency Range | 50 kHz |
| Frequency Control | $\mathbf{2 0}$ of $\mathbf{1 8 - 4 2}$ Range |

## Connections

a. Install a $50 \Omega$ termination on the Type 3 A5 INPUT connector. Use a $50 \Omega$ coax cable from the Type 191 Output connector to the termination.
b. Obtain a triggered display of five divisions peak to peak.
c. Change the Time Base Time/div control to $.05 \mu \mathrm{sec}$, and the Type 191 Frequency Range control to the $18-42 \mathrm{MHz}$ range. Obtain a stable display.
d. Position the display + peaks slightly above the trip level recorded in Step 30 b, and press the SEEK button. The mode must change to SEEK, and the deflection factor to $50 \mathrm{mV} /$ DIV. Position the display to center screen and press the SEEK button. The deflection factor must change to $10 \mathrm{mV} /$ DIV.
e. Position the display negative peaks slightly below the trip level recorded in Step 30 c, and press the SEEK button. The deflection factor must change to $50 \mathrm{mV} /$ DIV. Position the display to center screen and press the SEEK button, the deflection factor must change to $10 \mathrm{mV} /$ DIV.
f. Disconnect the Type 191 and remove the $50 \Omega$ iermination.

## Control Settings

## Type 3A5

No Change
Time Base
Time/div $\quad 10 \mathrm{msec}$
No other change.

## IG-72 Audio Generator

| Multiplier | $\times 1$ |
| :--- | :--- |
| Cycles (Left) | 60 |
| Cycles (Center) | 0 |


| Int/Ext $600 \Omega$ Load Sw | $\operatorname{Int}$ |
| :--- | :--- |
| Output Switch | $-30 / .03$ |
| Output Variable | For five division display |

## Connections

Connect a $50 \Omega$ coax from the Audio Generator output to the Type 3A5 INPUT connector. Use the BNC to clip lead adapter at the Audio Generator output terminals.
g. Obtain a triggered display of the 60 Hz signal at five divisions peak to peak. Position the display positive peaks slightly above the trip level recorded in Step 30 b, and press the SEEK button. The deflection factor must change from $10 \mathrm{mV} / \mathrm{DIV}$ to $50 \mathrm{mV} / \mathrm{DIV}$. Position the display to center screen and press the SEEK button. The deflection factor must change to $10 \mathrm{mV} /$ DIV.
h. Position the display negative peaks slightly below the trip level recorded in Step 30 c , and press the SEEK button. The deflection factor must change to $50 \mathrm{mV} / \mathrm{DIV}$. Center the display and press the SEEK button. The deflection factor must change to $10 \mathrm{mV} /$ DIV.

## 32. Check REMOTE SEEK Operation

## NOTE

This step is to be performed only when the companion time-base unit is a Type 3B5 Automatic/ Programmable Time Base.
a. Disconnect the signal cable from both the Audio Generator and the Type 3A5. Connect a P6030 $10 \times$ Probe to the Type 3A5 INPUT connector and the probe small phono plug into the REMOTE SEEK jack. Check the probe compensation. Set the MANUAL VOLTS/DIV switch to 10 mV .

## Control Settings

## IG-72 Audio Generator

| Multiplier | X100 |
| :--- | :---: |
| Output Switch | $-10 / .3$ |
| No other change. Frequency is now 6 |  |
|  | Type |
|  | 3B5 |
|  |  |
| MANUAL TIME/DIV | .5 mSEC |
| VARIABLE | CAL |
| Mode | MAN |
| DLY'D SWP MAG | OFF |
| SLOPE | + |
| TRIGGER | AC/INT |

b. Connect the probe ground clip to the Audio Generator ground terminal and the probe tip to the signal output terminal. Adjust the Type 3B5 LEVEL control for a stable display.
c. Change the Audio Generator OUTPUT switch to $0 / 1$ and press the P6030 Probe SEEK button. The display will first extend past the graticule top and bottom, and then as the P6030 Probe SEEK button is pressed, will reduce in amplitude and show as many cycles as the Type 3B5 is calibrated to display.

The Type 3B5 will not respond when the Type $3 A 5$ frontpanel SEEK button is pressed.


Fig. 6-26. Test equipment setup for checking SEEK multi and Advance pulse times, Step 33

Control Settings
Type 3A5

| MANUAL VOLTS/DIV | $50 \mathrm{~V} / \mathrm{DIV}$ |
| :--- | :--- |
| VARIABLE | CAL |
| Input Coupling | DC |
| POSITION | Display zero at <br> $\quad$division |

Time Base
Time / Div
Variable
Trigger Mode
Triggering Level
Slope
Coupling
Source
Type 561A
Calibrator

5 msec
Cal
Auto
Midrange
$+$
Line

100 volts

Type IAI
Volts/Cm (Ch 1)
Mode
Variable Volts/Cm
Position
Norm/Invert
Input Selector

Type 543B
Trigger Slope
Triggering Mode
Stability
Triggering Level
Time/Cm
Variable
Horizontal Display
Sweep Switch
Horizontal Position

| Trigger Slope | + Int |
| :--- | :--- |
| Triggering Mode | Auto |
| Stability | Preset |
| Triggering Level | Midrange |
| Time/Cm | 1 sec |
| Variable | Calibrated |
| Horizontal Display | Normal |
| Sweep Switch | Normal Sweep |
| Horizontal Position | Midrange |

1
Ch 1
Calib
Centered display
Norm
AC

## Connections

Install a $10 \times$ Probe on the test oscilloscope Channel 1 Input connector. Attach the probe ground clip to the $T_{>}$pe 3A5 near the Automatic Card, and the probe tip to Test Point TP684 on the Automatic Card.

Connect the Type 561A Calibrator Cal Out connector to the Type 3A5 INPUT connector with a $50 \Omega$ coax.

## 33. Check SEEK Multi Pulse and Advance Pulse Times

a. Make the connections and control settings recs,mmended under Fig. 6-26. The display should be 2 divisions peak to peak.
b. Press and hold down the Type 3A5 SEEK button, and obtain a test oscilloscope display similar to Fig. 6-27A. The Type 3A5 deflection factor readout must be $50 \mathrm{~V} / \mathrm{DIV}$. The time between test oscilloscope display positive pulses must be between 2 and 4 seconds after the SEEK button has be:en held down for 5 seconds.
c. Change the test oscilloscope sweep rate to $50 \mathrm{~ms}: \mathrm{c} /$ div and the triggering for + Int, AC Mode (not Auto). Press and hold the Type 3 A5 SEEK button. The display will now be similar to Fig. 6-27B, and the time the signal is positive must be equal to or greater than 200 msec (more thar, 4 horizontal divisions).
d. Change the test oscilloscope sweep rate to $20 \mathrm{msec} / \mathrm{div}$ and for - $\mathrm{Int} A C$ triggering. Move the probe tip to 7 lest Point TP754 and press the SEEK button. The series of neryative Advance Pulses must be completed in less than 200 msec , or in less than 10 divisions, as in Fig. 6-27C.

## EXTERNAL PROGRAMMING

No test procedure is given here, since external operation requires special programming equipment. Each user has different external programming needs, so use your own programmer and check that the system performs as required. If you use the Tektronix Type 263 Programmer, use the checkout procedure in the Type 263 Instruction Manual.

a. I sec/div.

b. $50 \mathrm{msec} / \mathrm{div}$.

c. $20 \mathrm{msec} / \mathrm{div}$.

Fig. 6-27. Step 33 waveforms.

## PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix, Inc. Field Office or representative.

Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number, instrument type or number, serial or model number, and modification number if applicable.

If a part you have ordered has keen replaced with a new or improved part, your local Tektronix, Inc. Field Office or rep esentative will contact you concerning any change in part number.

## SPECIAL NOTES AND SYMBOLS

$\times 000$ Part first added $a$ this serial number
$00 \times$ Part removed afte this serial number
*000-0000-00 Asterisk preceding Tektronix Part Number indicates manufactured by or for Tektronix, Inc., or reworked or checked components.
Use 000-0000-00 Part number indicated is direct replacement.
(1) Screwdriver adjust nent.

Control, adjustmert or connector.
${ }^{\prime}$

## ABBREVIATIONS AND SYMBOLS

| A or amp | amperes | $\lambda$ | lambda-wavelength |
| :---: | :---: | :---: | :---: |
| AC or ac | alternating current | $<$ | less than |
| AF | audio frequency | LF | low frequency |
| $\alpha$ | alpha-common-base current amplification fa tor | $\lg$ | length or long |
| AM | amplitude modulation | LV | low voltage |
| $\approx$ | approximately equal to | M | mega or $10^{6}$ |
| $\beta$ | beta-common-emitter current amplification fator | m | milli or $10^{-3}$ |
| BHB | binding head brass | $M \Omega$ or meg | megohm |
| BHS | binding head steel | $\mu$ | micro or $10^{-6}$ |
| BNC | baby series ' N ' connector | mc | megacycle |
| $\times$ | by or times | met. mm | metal <br> millimeter |
| C | carbon | ms | millisecond |
| C | capacitance | - | minus |
| cap. | capacitor | mtg hdw | mounting hardware |
| cer | ceramic |  | no or |
| cm | centimeter |  | nano or 10 |
| comp | composition | no. or \# | number |
| conn | connector | ns | nanosecond |
| $\sim$ | cycle | OD | outside diameter |
| $\mathrm{c} / \mathrm{s}$ or cps | cycles per second | OHB | oval head brass |
| CRT | cathode-ray tube | OHS | oval head steel |
| csk | countersunk | $\Omega$ | omega-ohms |
| dB | decibe | $\omega$ | omega-angular frequency |
| dBm | decibel referred to one milliwatt |  | pico or $10^{-12}$ |
| $D C$ or dc | direct current | / | per |
| ${ }_{0}{ }_{0}$ | double end degrees | \% | percent |
| ${ }^{\circ} \mathrm{C}$ | degrees | PHB | pan head brass |
| ${ }^{\circ} \mathrm{F}$ | degrees Fahrenheit | $\phi$ | phi-phase angle |
| ${ }^{\circ} \mathrm{K}$ | degrees Kelvin | $\pi$ | pi-3.1416 |
| dia | diameter | $+$ | pan head steel plus |
| $\div$ | divide by | $\pm$ | plus or minus |
| div | division | PIV | peak inverse voltage |
| EHF | extremely high frequency | plstc | plastic |
| EMC | electrolytic, metal cased | PMC | paper, metal cased |
| EMT | electrolytic, metal tubutar | poly | polystyrene |
|  | epsilon-2.71828 or \% of error | prec | precision |
| $\geq$ | equal to or greater than |  | paper, tubular |
| $\leq$ | equal to or less than | PTM | paper or plastic, tubular, molded |
| ext | external | pwr | power |
| $F$ or f | farad | RC | resistance capacitance |
| F \& I | focus and intensity | RF | radio frequency |
| FHB | flat head brass | RFI | radio frequency interference |
| FHS | flat head steel | RHB | round head brass |
| Fil HB | fillister head brass | $\stackrel{\rho}{ }$ | rho-resistivity |
| Fil HS | fillister head steel | RHS | round head steel |
| FM | frequency modulation | $\mathrm{r} / \mathrm{min}$ or rpm | revolutions per minute |
| ft | feet or foot | RMS | root meon square |
| G | giga or $10^{9}$ | $s$ or sec. | second |
| g | acceleration due to gravity | SE | single end |
| Ge | germanium | Si | silicon |
| GMV | guaranteed minimum value | SN or S/N | serial number |
| GR | General Radio |  |  |
| $>$ | greater than | T | tera or $10^{12}$ |
|  |  | TC | temperature compensated |
| H or h | henry | TD | tunnel diode |
| $h$ | height or high | THB | truss head brass |
| hex. | hexagonal | $\theta$ | theta-angular phase displacement |
| HF | high frequency | thk | thick |
| HHB | hex head brass | THS | truss head steel |
| HHS | hex head steel | $\dagger$ tub. | tubular |
| HSB | hex socket brass |  |  |
| HSS | hex socket steel | UHF | ultra high frequency |
| HV | high voltage |  |  |
| Hz | hertz (cycles per second) | VAC | volt volts, alternating current |
| ID | inside diameter | var | variable |
| IF | intermediate frequency | VDC | volts, direct current |
| in. | inch or inches | VHF | very high frequency |
| incd | incandescent | VSWR | voltage standing wave ratio |
| $\infty$ | infinity |  |  |
| int | internal | W | watt or width |
| $r$ | integral | $w$ | wide or width |
|  |  | w/ | with |
| k | kilohms or kilo (103) | w/o | without |
| k $\Omega$ | kilohm | WW | wire-wound |
| kc | kilocycle |  |  |
|  |  | xmfr | transformer |

## SECTION 7

## ELECTRICAL PARTS LIST

Values are fixed unless marked Variable.
Tektronix

| Ckt. No. | Tektronix Part No. | Description |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bulbs |  |  |  |  |  |
| B104 | 150-0035-00 | Neon, AID |  |  |  |
| B420 | 150-0049-00 | Incandescent, ; $\ddagger 6835$ | 5 V | 60 mA |  |
| B422 | 150-0054-00 | Incandescent, ; $\ddagger 683$ | w/red coating tinned leads |  |  |
| B601 | 150-0049-00 |  | 5 V | 60 mA |  |
| B602 | 150-0049-00 | Incandescent, it 6835 | 5 V | 60 mA |  |
| B603 | 150-0049-00 | Incandescent, 沛 6835 | 5 V | 60 mA |  |
| B605 | 150-0049-00 | Incandescent, ; $\ddagger 6835$ | 5 V | 60 mA |  |
| B606 | 150-0048-00 | Incandescent, $\ddagger$ 683 | 5 V | 60 mA |  |
| B607 | 150-0049-00 | Incandescent, it 6835 | 5 V | 60 mA |  |
| B620 | 150-0049-00 | Incandescent, 汭6835 | 5 V | 60 mA |  |
| B621 | 150-0049-00 | Incandescent, it 6835 | 5 V | 60 mA |  |
| B624 | 150-0049-00 | Incandescent, 7t 6835 | 5 V | 60 mA |  |
| B626 | 150-0048-00 | Incandescent, 7 \% 683 | 5 V | 60 mA |  |
| B627 | 150-0049-00 | Incandescent, 7\% 6835 | 5 V | 60 mA |  |
| B628 | 150-0048-00 | Incandescent, 7568 | 5 V | 60 mA |  |
| B629 | 150-0048-00 | Incandescent, 7\%683 | 5 V | 60 mA |  |
| B736 | 150-0055-00 | Neon, 5 AB-B |  |  |  |

Capacitors
Tolerance $\pm 20 \%$ unless otherwise indicated.

| Cl | *285-0708-00 | $0.04 \mu \mathrm{~F}$ | PTM |  | 600 V | +5\%-15\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C7 | 281-0536-00 | 1000 pF | Cer |  | 500 V | 10\% |
| Cl 2 | 281-0536-00 | 1000 pF | Cer |  | 500 V | 10\% |
| C15A | 281-0102-00 | 1.7-11 pF | Air | Var |  |  |
| C15B | 281-0544-00 | 5.6 pF | Cer |  | 500 V | 10\% |
| C15D |  | 0.2-1.5 pF | Tub. | Var |  |  |
| C15H | 281-0104-00 | 0.5 pF | Mica |  |  |  |
| Cl5E | 281-0538-00 | 1 pF | Cer |  | 500 V |  |
| C22 | 281-0536-00 | 1000 pF | Cer |  | 500 V | 10\% |
| C25A | 281-0102-00 | 1.7-11 pF | Air | Var |  |  |
| C25B | 281-0544-00 | 5.6 pF | Cer |  | 500 V | 10\% |
| C25D | 281-0113-00 | $0.2-1.5 \mathrm{pF}$ | Tub. | Var |  |  |
| C25F | 281.0113-00 | $100 \mathrm{pF}$ | Mica |  |  |  |
| C32 | 281-0536-00 | 1000 pF | Cer |  | 500 V | 10\% |
| C35A | 281-0102-00 | 1.7-11 pF | Air | Var |  |  |
| C35B | 281-0572-00 | 6.8 pF | Cer |  | 500 V | 10\% |
| C35D | 281-0108-00 | 0.2-1.5 pF | Tub. | Var |  |  |
| C35F | 281-0108-00 | 1000 pF | Mica |  |  |  |
| C47 | 281-0536-00 | 1000 pF | Cer |  | 500 V | 10\% |
| C52 | 281-0536-00 | 1000 pF | Cer |  | 500 V | 10\% |

## Electrical Parts List-Type 3A5

Capacitors (Cont'd)
Tektronix
Ckt. No.

| C55A | 281-0064-00 | 0.2-1.5 pF | Tuls. | Var |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C55B | 281-0526-00 | 1.5 pF | Cor |  | 500 V | $\pm 0.5 \mathrm{pF}$ |
| C55D | 281-0102-00 | 1.7-11 pF | Air | Var |  |  |
| C55E | 281-0572-00 | 6.8 pF | Cier |  | 500 V | 10\% |
| C62 | 281-0536-00 | 1000 pF | Cis |  | 500 V | 10\% |
| C65A | 281-0102-00 | 1.7-11 pF | Air | Var |  |  |
| C65D | 281-0101-00 | 1.5-9.1 pF | Air | Var |  |  |
| C70 | 281-0064-00 | 0.2-1.5 pF | Tuis. | Var |  |  |
| Cl 01 | 281-0613-00 | 10 pF | Cim |  | 200 V | 10\% |
| Cl02 | 281-0591-00 | 5600 pF | Cor |  | 200 V |  |
| C106 | 283-0092-00 | $0.03 \mu \mathrm{~F}$ | Cier |  | 200 V | +80\% - $20 \%$ |
| C110 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cier |  | 250 V |  |
| C115 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cier |  | 250 V |  |
| C122 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cier |  | 25 V | +80\%-20\% |
| C124 | 283-0067-00 | $0.001 \mu \mathrm{~F}$ | Cir |  | 200 V | 10\% |
| C128 | 281-0546-00 | 330 pF | Ci.r |  | 500 V | 10\% |
| C134 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cir |  | 250 V |  |
| C145 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Ci.r |  | 25 V | +80\%-20\% |
| C151 | 281-0513-00 | 27 pF | Cer |  | 500 V |  |
| C152 | 281-0092-00 | 9.35 pF | Cer | Var |  |  |
| C153 | 281-0524-00 | 150 pF | C. r |  | 500 V |  |
| C154 | 281-0550-00 | 120 pF | Cir |  | 500 V | 10\% |
| C155 | 281-0518-00 | 47 pF | Cer |  | 500 V |  |
| C157 | 281-0525-00 | 470 pF | C. $\cdot \mathrm{r}$ |  | 500 V |  |
| C164 | 281-0552-00 | 25 pF | C.r |  | 500 V |  |
| C166 | 281-0549-00 | 68 pF | Ci.r |  | 500 V | 10\% |
| C176 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | + $80 \%-20 \%$ |
| C198 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | C.rer |  | 25 V | + $80 \%-20 \%$ |
| C206 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | + $80 \%-20 \%$ |
| C210 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | $C_{\text {er }}$ |  | 25 V | +80\%-20\% |
| C213 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  |  | +80\% - $20 \%$ |
| C216 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cer |  | 250 V |  |
| C306 | 283-0059-00 | $1 \mu \mathrm{~F}$ | Ce.t |  | 25 V | +80\% - $20 \%$ |
| C308 | 283-0089-00 | 82 pF | Cer |  | 1000 V | 5\% |
| C324 | 283-0067-00 | $0.001 \mu \mathrm{~F}$ | Cer |  | 200 V | 10\% |
| C328 | 281-0546-00 | 330 pF | Cer |  | 500 V | 10\% |
| C352 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | +80\% - $20 \%$ |
| C366 | 281-0549-00 | 68 pF | Cer |  | 500 V | 10\% |
| C404 | 290-0138-00 | $330 \mu \mathrm{~F}$ | EMT |  | 6 V |  |
| C422 | 290-0029-00 | $2000 \mu \mathbf{F}$ | EMi: |  | 20 V |  |
| C426 | 290-0121-00 | $2 \mu \mathrm{~F}$ | EMT |  | 25 V |  |
| C430 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | +80\% - $20 \%$ |
| C432 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | +80\% - $20 \%$ |
| C438 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | +80\% - $20 \%$ |
| C508 | 283-0029-00 | $0.005 \mu \mathrm{~F}$ | Cer |  | 500 V | 5\% |

$281-0064-00$
$281-0526-00$
$281-0102-00$
$281-0572-00$
$281-0536-00$

| C55A | 281-0064-00 | 0.2-1.5 pF | Tuls. | Var |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C55B | 281-0526-00 | 1.5 pF | Cor |  | 500 V | $\pm 0.5 \mathrm{pF}$ |
| C55D | 281-0102-00 | 1.7-11 pF | Air | Var |  |  |
| C55E | 281-0572-00 | 6.8 pF | Cier |  | 500 V | 10\% |
| C62 | 281-0536-00 | 1000 pF | Cis |  | 500 V | 10\% |
| C65A | 281-0102-00 | 1.7-11 pF | Air | Var |  |  |
| C65D | 281-0101-00 | 1.5-9.1 pF | Air | Var |  |  |
| C70 | 281-0064-00 | 0.2-1.5 pF | Tuis. | Var |  |  |
| Cl 01 | 281-0613-00 | 10 pF | Cim |  | 200 V | 10\% |
| Cl02 | 281-0591-00 | 5600 pF | Cor |  | 200 V |  |
| C106 | 283-0092-00 | $0.03 \mu \mathrm{~F}$ | Cier |  | 200 V | +80\% - $20 \%$ |
| C110 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cier |  | 250 V |  |
| C115 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cier |  | 250 V |  |
| C122 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cier |  | 25 V | +80\%-20\% |
| C124 | 283-0067-00 | $0.001 \mu \mathrm{~F}$ | Cir |  | 200 V | 10\% |
| C128 | 281-0546-00 | 330 pF | Ci.r |  | 500 V | 10\% |
| C134 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cir |  | 250 V |  |
| C145 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Ci.r |  | 25 V | +80\%-20\% |
| C151 | 281-0513-00 | 27 pF | Cer |  | 500 V |  |
| C152 | 281-0092-00 | 9.35 pF | Cer | Var |  |  |
| C153 | 281-0524-00 | 150 pF | C. r |  | 500 V |  |
| C154 | 281-0550-00 | 120 pF | Cir |  | 500 V | 10\% |
| C155 | 281-0518-00 | 47 pF | Cer |  | 500 V |  |
| C157 | 281-0525-00 | 470 pF | C. $\cdot \mathrm{r}$ |  | 500 V |  |
| C164 | 281-0552-00 | 25 pF | C.r |  | 500 V |  |
| C166 | 281-0549-00 | 68 pF | Ci.r |  | 500 V | 10\% |
| C176 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | + $80 \%-20 \%$ |
| C198 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | C.rer |  | 25 V | + $80 \%-20 \%$ |
| C206 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | + $80 \%-20 \%$ |
| C210 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | $C_{\text {er }}$ |  | 25 V | +80\%-20\% |
| C213 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  |  | +80\% - $20 \%$ |
| C216 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cer |  | 250 V |  |
| C306 | 283-0059-00 | $1 \mu \mathrm{~F}$ | Ce.t |  | 25 V | +80\% - $20 \%$ |
| C308 | 283-0089-00 | 82 pF | Cer |  | 1000 V | 5\% |
| C324 | 283-0067-00 | $0.001 \mu \mathrm{~F}$ | Cer |  | 200 V | 10\% |
| C328 | 281-0546-00 | 330 pF | Cer |  | 500 V | 10\% |
| C352 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | +80\% - $20 \%$ |
| C366 | 281-0549-00 | 68 pF | Cer |  | 500 V | 10\% |
| C404 | 290-0138-00 | $330 \mu \mathrm{~F}$ | EMT |  | 6 V |  |
| C422 | 290-0029-00 | $2000 \mu \mathbf{F}$ | EMi: |  | 20 V |  |
| C426 | 290-0121-00 | $2 \mu \mathrm{~F}$ | EMT |  | 25 V |  |
| C430 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | +80\% - $20 \%$ |
| C432 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | +80\% - $20 \%$ |
| C438 | 283-0081-00 | $0.1 \mu \mathrm{~F}$ | Cer |  | 25 V | +80\% - $20 \%$ |
| C508 | 283-0029-00 | $0.005 \mu \mathrm{~F}$ | Cer |  | 500 V | 5\% |

Description
S/N Range

## Capacitors (Cont'd)

| Ckt. No. | Tektronix <br> Part No. |  | Description |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C510 | 283-0051-00 | $0.0033 \mu \mathrm{~F}$ | Cer | 100 V | 5\% |  |
| C511 | 283-0027-00 | $0.02 \mu \mathrm{~F}$ | Cer | 30 V |  |  |
| C512 | 283-0029-00 | $0.005 \mu \mathrm{~F}$ | Cer | 500 V | 5\% |  |
| C520 | 281-0516-00 | 39 pF | Cer | 500 V | 10\% |  |
| C530 | 281-0523-00 | 100 pF | Cer | 350 V |  |  |
| C540 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cer | 250 V |  |  |
| C544 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cer | 250 V |  |  |
| C546 | 281-0591-00 | 5600 pF | Cer | 200 V |  |  |
| C550 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cer | 250 V |  |  |
| C556 | 281-0591-00 | 5600 pF | Cer | 200 V |  |  |
| C564 | 281-0597-00 | 2500 pF | Cer | 500 V |  |  |
| C638 | 290-0248-01 | $150 \mu \mathrm{~F}$ | EMT | 15 V |  |  |
| C640 | 283-0079-00 | $0.01 \mu \mathrm{~F}$ | Cer | 250 V |  |  |

## Diodes

D1
D5
D10
D20
D30

D45
D50
D60
D80
D82

D84
D90
D92
D96
D188

D204
D300
D315
D316
D388

D404
D422A,B,C,D
D515
D524
D534
D546
D556
D601
D602
D603
*152-0235-00
Zener, matched pair, $0.4 \mathrm{~W}, 60 \mathrm{~V}, 10 \%$
$\begin{array}{ll}\text { *152-0107-00 } & \text { Silicon } \\ \text { *152-0107-00 } & \text { Silicon }\end{array}$
Silicon
Silicon
Replaceable by 1 N647
Replaceable by 1 N647
Replaceable by 1 N647


## Transistors

| Ckt. No. | Tektronix Part No. | Description | S/N Range |
| :---: | :---: | :---: | :---: |
| Q108 | 151-0179-00 | 2N3877A |  |
| Q123 | 151-0162-00 | 2N3324 |  |
| Q134 | *151-0142-00 | Selected from 2N3546 |  |
| Q143 | *151-0120-00 | Selected from 2N2475 |  |
| Q154 | 151-0107-00 | 2N967 |  |
| Q174 | 151-0175-00 | 2N3662 |  |
| Q183 | *151-0120-00 | Selected from 2N2475 |  |
| Q194 | 151-0164-00 | 2N3702 |  |
| Q204 | *151-0155-00 | Replaceable b) 2N2925 |  |
| Q213 | *151-0120-00 | Selected from 2N2475 |  |
| Q323 | 151-0162-00 | 2N3324 |  |
| Q334 | *151-0142-00 | Selected from 2 N 3546 |  |
| Q343 | *151-0120-00 | Selected from 2N2475 |  |
| Q354 | 151-0107-00 | 2N967 |  |
| Q374 | 151-0175-00 | 2N3662 |  |
| Q383 | *151-0120-00 | Selected from ${ }^{\text {N } 2475}$ |  |
| Q394 | 151-0164-00 | 2N3702 |  |
| Q404 | *151-0127-00 | Selected from 2 N2369 |  |
| Q423 | *151-0103-00 | Replaceable b) 2N2219 |  |
| Q424 | *151-0155-00 | Replaceable by 2 N 2925 |  |
| Q504 | *151-0142-00 | Selected from 2 N3546 |  |
| Q514 | *151-0142-00 | Selected from 2 N 3546 |  |
| Q624 | *151-0183-00 | Selected from : N 2192 |  |

## Resistors

Resistors are fixed, composition, $\pm 10 \%$ unless otherwise indicated.

| R1 | 316-0122-00 | 1.2 k | $1 / 4 \mathrm{~W}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R7 | 317-0200-00 | $20 \Omega$ | 1/10 W |  | 5\% |
| R12 | 317-0200-00 | $20 \Omega$ | 1/10 W |  | 5\% |
| R15A | 322-0658-00 | 900 k | $1 / 4 \mathrm{~W}$ | Prec | 1/2\% |
| R15D | 321-0712-00 | 111 k | $1 / 8 \mathrm{~W}$ | Prec | 1/2\% |
| R22 | 317-0200-00 | $20 \Omega$ | 1/10 W |  | 5\% |
| R25A | 322-0659-00 | 990 k | $1 / 4 \mathrm{~W}$ | Prec | 1/2\% |
| R25D | 321-0711-00 | 10.1 k | $1 / 8 \mathrm{~W}$ | Prec | 1/2\% |
| R32 | 317-0200-00 | $20 \Omega$ | 1/10 W |  | 5\% |
| R35A | 322-0629-00 | 999 k | $1 / 4 \mathrm{~W}$ | Prec | 1\% |
| R35D | 321-0193-00 | 1 k | 1/8W | Prec | 1\% |
| R47 | 317-0200-00 | $20 \Omega$ | 1/10 W |  | 5\% |
| R52 | 317-0200-00 | $20 \Omega$ | 1/10 W |  | 5\% |
| R55A | 322-0610-00 | 500 k | $1 / 4 \mathrm{~W}$ | Prec | 1\% |
| R55D | 322-0481-00 | 1 meg | $1 / 4 \mathrm{~W}$ | Prec | 1\% |
| R62 | 317-0200-00 | $20 \Omega$ | 1/10 W |  | 5\% |
| R65A | 322-0620-00 | 800 k | $1 / 4 \mathrm{~W}$ | Prec | 1\% |
| R65D | 321-0618-00 | 250 k | $1 / 8 \mathrm{~W}$ | Prec | 1\% |
| R70 | 322-0481-00 | 1 meg | $1 / 4 \mathrm{~W}$ | Prec | 1\% |
| R90 | 301-0101-00 | $100 \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |


| Resistors (Cont'd) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt. No. | Tektronix <br> Part No. |  | Description |  |  |  | S/N Range |
| R92 | 301-0101-00 | $100 \Omega$ | $1 / 2 W$ |  |  | 5\% |  |
| R94 | 301-0101-00 | $100 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |  |
| R96 | 301-0101-00 | $100 \Omega$ | $1 / 2 \mathrm{~W}$ |  |  | 5\% |  |
| R101 | 315-0391-00 | $390 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R102 | 315-0104-00 | 100 k | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R104 | 315-0101-00 | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R106 | 315-0223-00 | 22 k | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R107 | 315-0393-00 | 39 k | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R108 | 301-0332-00 | 3.3 k | $1 / 2 \mathrm{~W}$ |  |  | 5\% |  |
| R110 | 315-0470-00 | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R113 | 303-0273-00 | 27 k | $1 W^{\prime}$ |  |  | 5\% |  |
| R115 | 315-0470-00 | $47 \Omega$ | $1 / 4 W$ |  |  | 5\% |  |
| R120 | 307-0106-00 | $4.7 \Omega$ | $1 / 4 W$ |  |  | 5\% |  |
| R123 | 315-0471-00 | $470 \Omega$ | $1 / 4 W$ |  |  | 5\% |  |
| R124 | 315-0301-00 | $300 \Omega$ | $1 / 4 W^{\prime}$ |  |  | 5\% |  |
| R125 | 321-0137-00 | $261 \Omega$ | $1 / 8{ }^{\prime}$ |  | Prec | 1\% |  |
| R128 | 321-0014-00 | $13.7 \Omega$ | $1 / 8{ }^{1}$ |  | Prec | 1\% |  |
| R130 | *311-0544-00 | $100 \Omega$ |  | Var |  |  |  |
| R132 | 308-0313-00 | 20 k | $3 W^{\prime}$ |  | WW | 1\% |  |
| R134 | 315-0102-00 | 1 k | $1 / 4 W$ |  |  | 5\% |  |
| R140 | 322-0187-00 | $866 \Omega$ | $1 / 4 W^{\prime}$ |  | Prec | 1\% |  |
| R143 | 315-0182-00 | 1.8 k | $1 / 4 W^{\prime}$ |  |  | 5\% |  |
| R145 | 307-0106-00 | $4.7 \Omega$ | $1 / 4 W^{\prime}$ |  |  | 5\% |  |
| R150 | 322-0145-00 | $316 \Omega$ | $1 / 4 W$ |  | Prec | 1\% |  |
| R153 | 311-0480-00 | $500 \Omega$ |  | Var |  |  |  |
| R154 | 315-0102-00 |  |  |  |  | 5\% |  |
| R155 | 315-0272-00 | 2.7 k | $1 / 4 W$ |  |  | 5\% |  |
| R157 | 315-0822-00 | 8.2 k | $1 / 4 W$ |  |  | 5\% |  |
| R160 | 315-0820-00 | $82 \Omega$ | $1 / 4 W^{\prime}$ |  |  | 5\% |  |
| R164 | 315-0102-00 | 1 k | $1 / 4 W^{\prime}$ |  |  | 5\% |  |
| R166 | 321-0093-00 | $90.9 \Omega$ | $1 / 8 W$ |  | Prec | 1\% |  |
| R167 | 315-0102-00 | 1 k | $1 / 4 W$ |  |  | 5\% |  |
| R170 | 315-0152-00 | 1.5 k | $1 / 4 W$ |  |  | 5\% |  |
| R172 | 311.0576-00 | $2 \times 1$ k |  | Var |  |  |  |
| R174 | 321-0146-00 | $324 \Omega$ | $1 / 8 W^{\prime}$ |  | Prec | 1\% |  |
| R176 | 323-0122-00 | $182 \Omega$ | 1/2W |  | Prec | 1\% |  |
| R178 | 322-0134-00 | $243 \Omega$ | $1 / 4 W$ |  | Prec | 1\% |  |
| R179 | 321-0115-00 | $154 \Omega$ | $1 / 8 W$ |  | Prec | 1\% |  |
| R183 | 321-0115-00 | $154 \Omega$ | $1 / 8 W$ |  | Prec | 1\% |  |
| R184 | 315-0270-00 | $27 \Omega$ | $1 / 4 W$ |  |  | 5\% |  |
| R186 | 311-0095-00 | $500 \Omega$ |  | Var |  |  |  |
| R188 | 315-0101-00 | $100 \Omega$ | $1 / 4 W$ |  |  | 5\% |  |
| R194 | 321-0093-00 | $90.9 \Omega$ | $1 / 8 W$ |  | Prec | 1\% |  |
| R196 | 315-0221-00 | $220 \Omega$ | $1 / 4 \mathrm{~W}$ |  |  | 5\% |  |
| R198 | 315-0821-00 | $820 \Omega$ | $1 / 4 W$ |  |  | 5\% |  |

7-6

Resistors (Cont'd)

| Ckt. No. | Tektronix <br> Part No. |  | Description |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R200 | 315-0181-00 | $180 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R202 | 315-0181-00 | $180 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R204 | 315-0202-00 | 2 k | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R206 | 307-0106-00 | $4.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R210 | 307-0106-00 | $4.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R213 | 315-0471-00 | $470 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R214 | 315-0470-00 | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R216 | 315-0302-00 | 3 k | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R218 | 322-0394-00 | 124 k | $1 / 4 \mathrm{~W}$ | Prec | 1\% |  |
| R300A, B | 311-0321-00 | $2 \times 500 \mathrm{k}$ | Var |  |  |  |
| R302 | 315-0335-00 | 3.3 meg | 1/4 W |  | 5\% |  |
| R303 | 315-0182-00 | 1.8 k | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R304 | 315-0274-00 | 270 k | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R306 | 315-0101-00 | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R308 | 316-0106-00 | 10 meg | $1 / 4 \mathrm{~W}$ |  |  |  |
| R309 | 321-0430-00 | 294 k | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R311 | 309-0377-00 | 3 meg | $1 / 2 \mathrm{~W}$ | Prec | 1\% |  |
| R313 | 303-0273-00 | 27 k | 1 W |  | 5\% |  |
| R315 | 315-0101-00 | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R320 | 307-0106-00 | $4.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R323 | 315-0471-00 | $470 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R324 | 315-0301-00 | $300 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R325 | 321-0137-00 | $261 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R328 | 321-0014-00 | 13.7 ת | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R332 | 308-0313-00 | 20 k | 3 W | WW | 1\% |  |
| R343 | 315-0182-00 |  |  |  | 5\% |  |
| R350 | 322-0145-00 | $316 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R352 | 307-0106-00 | 4.7 \% | $1 / 4$ W |  | 5\% |  |
| R354 | 321-0074-00 | $57.6 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R360 | 315-0820-00 | $82 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R366 | 321-0093-00 | $90.9 \Omega$ |  | Prec |  |  |
| R367 | 315-0102-00 | 1 k | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R370 | 315-0152-00 | 1.5 k | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R374 | 321-0146-00 | $324 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R378 | 322-0134-00 | $243 \Omega$ | $1 / 4 \mathrm{~W}$ | Prec | 1\% |  |
| R379 | 321-0115-00 | $154 \Omega$ | 1/8W | Prec | 1\% |  |
| R383 | 321-0115-00 | $154 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R384 | 315-0270-00 | $27 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R388 | 315-0101-00 | $100 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R394 | 321-0093-00 | $90.9 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R396 | 315-0221-00 | $220 \Omega$ | 1/4 W |  | 5\% |  |
| R400 | 315-0181-00 | $180 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R404 | 315-0202-00 | 2 k | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R408 | 315-0751-00 | $750 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R422 | 301-0473-00 | 47 k | $1 / 2 \mathrm{~W}$ |  | 5\% |  |

Resistors (Cont'd)

| Ckt. No. | Tekfronix Part No. |  | Des:cription |  |  | S/N Range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R424 | 315-0270-00 | $27 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R426 | 321-0227-00 | 2.26 k | 1/8W | Prec | 1\% |  |
| R427 | 322-0280-00 | 8.06 k | $1 / 4 \mathrm{~W}$ | Prec | 1\% |  |
| R430 | 315-0510-00 | $51 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R432 | 307-0106-00 | $4.7 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R438 | 307-0106-00 | $4.7 \Omega$ | 1/4 W |  | 5\% |  |
| R503 | 321-0099-00 | $105 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R504 | 321-0125-00 | $196 \Omega$ | 1/8W | Prec | 1\% |  |
| R506 | 321-0004-00 | $10.7 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R507 | 321-0004-00 | $10.7 \Omega$ | $1 / 8 \mathrm{~W}$ | Prec | 1\% |  |
| R508 | 315-0101-00 | $100 \Omega$ | 1/4 W |  | 5\% |  |
| R510 | 315-0300-00 | $30 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R511 | 315-0121-00 | $120 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R512 | 321-0001-00 | $10 \Omega$ | 1/8W | Prec | 1\% |  |
| R514 | 321-0125-00 | $196 \Omega$ | 1/8W | Prec | 1\% |  |
| R518 | 323-0626-00 | $50 \Omega$ | 1/2W | Prec | 1\% |  |
| R520 | 315-0681-00 | $680 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R521 | 308-0387-00 | $178 \Omega$ | 3 W | WW | 1\% |  |
| R522 | 308-0387-00 | $178 \Omega$ | 3 W | WW | 1\% |  |
| R526 | *310-0629-00 | 1.05 k | 11 W | Prec | 1\% |  |
| R528 | 308-0282-00 | 1.35 k |  |  | 5\% |  |
| R530 | 309-0275-00 | 2.15 meg | 1/2W | Prec |  |  |
| R536 | *310-0629-00 | 1.05 k | 11 W | Prec | 1\% |  |
| R540 | 315-0104-00 | 100 k | 1/4 W |  | 5\% |  |
| R542 | 302-0333-00 | 33 k | 1/2W |  |  |  |
| R544 | 315-0101-00 | $100 \Omega$ | 1/4W |  | 5\% |  |
| R546 | 301-0823-00 | 82 k | 1/2W |  | 5\% |  |
| R550 | 315-0104-00 | 100 k | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R552 | 302-0333-00 | 33 k | 1/2W |  |  |  |
| R556 | 301-0823-00 | 82 k | $1 / 2 \mathrm{~W}$ |  | 5\% |  |
| R605 | 301-0101-00 | $100 \Omega$ | 1/2W |  | 5\% |  |
| R624 | 315-0470-00 | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R626 | 315-0271-00 | $270 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R628 | 315-0104-00 | 100 k | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R630 | 315-0470-00 | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R632 | 315-0470-00 | $47 \Omega$ | 1/4 W |  | 5\% |  |
| R636 | 306-0102-00 | 1 k | 2 W |  |  |  |
| R637 | 305-0562-00 | 5.6 k | 2 W |  | 5\% |  |
| R640 | 315-0470-00 | $47 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R701 | 315-0750-00 | $75 \Omega$ | $1 / 4 \mathrm{~W}$ |  | 5\% |  |
| R702 | 311-0169-00 | $100 \Omega$ |  |  |  |  |
| R704 | 301-0361-00 | $360 \Omega$ | $1 / 2 \mathrm{~W}$ |  | 5\% |  |



## Transformers

| T160 | $* 120-0286-00$ | Toroid, 2 turns bifilar |
| :--- | ---: | :--- |
| T164 | $* 120-0286-00$ | Toroid, 2 turns bifilar |
| T501 | $276-0512-00$ | Core, Powder Iron |
| T524 | $276-0512-00$ | Core, Powder Iron |
| T534 | $276-0512-00$ | Core, Powder Iron |

## Electron Tubes

| V113 | $154-0306-00$ | 7586 |
| :--- | :--- | :--- |
| V313 | $154-0306-00$ | 7586 |
| V524 | $154-0361-00$ | 8233 |
| V534 | $154-0361-00$ | 8233 |

$\dagger$ Furnished with the Push-Button Board.

## AUTOMATIC CARD

Tektronix

| Ckt. No. | Part No. | Description | Model No. |
| :--- | :---: | :---: | :---: |
|  | $* 670-0092-00$ | Complete Card |  |

## Capacitors

Tolerance $\pm 20 \%$ unless otherwise indicated.

| C672 | 290-0158-00 | $50 \mu \mathrm{~F}$ | EMT | 25 V | +75\%-15\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C674 | *290-0299-00 | $330 \mu \mathrm{~F}$ | EMT | 10 V |  |
| C714 | 290-0219-00 | $5 \mu \mathrm{~F}$ | EMT | 25 V |  |
| C723 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C732 | 281-0536-00 | 1000 pF | Cer | 500 V | $\pm 100 \mathrm{pF}$ |
| C801 | 283-0059-00 | $1 \mu \mathrm{~F}$ | Ce.r | 25 V | +80\% - $20 \%$ |
| C812 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | $C_{e r}$ | 25 V |  |
| C819 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C822 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C829 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C832 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | $C_{6} \mathrm{r}$ | 25 V |  |
| C839 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | $\mathrm{Cer}_{\mathrm{r}}$ | 25 V |  |
| C852 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | $C_{\text {er }}$ | 25 V |  |
| C859 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C862 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | $C_{e} \mathrm{r}$ | 25 V |  |
| C869 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | $\mathrm{C} \in \mathrm{r}$ | 25 V |  |
| C872 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C879 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | Cer | 25 V |  |
| C882 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | $C_{e r}$ | 25 V |  |
| C889 | 283-0026-00 | $0.2 \mu \mathrm{~F}$ | $\mathrm{C} \in \mathrm{r}$ | 25 V |  |

## Diodes

Tek Spec
Tek Spec
Tek Spec
Tek Spec
Replaceable by 1N3605
Replaceable by 1N3605

Tek Spec
Tek Spec
Tek Spec
Tek Spec
Tek Spec

| *152-0075-00 | Germanium |
| :--- | :--- |
| *152-0075-00 | Germanium |
| *152-0075-00 | Germanium |
| *152-0075-00 | Germanium |
| *152-0185-00 | Silicon |
| *152-0185-00 | Silicon |

Tek Spec
Tek Spec
Tek Spec
Tek Spec
Tek Spec

# AUTOMATIC CARD (Cont'd) 

Diodes (Cont'd)

| Ckt. No. | Tektronix Part No. |  | Description | Model No. |
| :---: | :---: | :---: | :---: | :---: |
| D684 | *152-0185-00 | Silicon | Replaceable by 1N3605 |  |
| D689 | *152-0075-00 | Germanium | Tek Spec |  |
| D706 | *152-0075-00 | Germanium | Tek Spec |  |
| D710 | *152-0075-00 | Germanium | Tek Spec |  |
| D740 | *152-0075-00 | Germanium | Tek Spec |  |
| D743 | *152-0185-00 | Silicon | Replaceable by 1N3605 |  |
| D745 | *152-0075-00 | Germanium | Tek Spec |  |
| D746 | *152-0075-00 | Germanium | Tek Spec |  |
| D750 | *152-0075-00 | Germanium | Tek Spec |  |
| D802 | *152-0075-00 | Germanium | Tek Spec |  |
| D804 | *152-0075-00 | Germanium | Tek Spec |  |
| D812 | *152-0075-00 | Germanium | Tek Spec |  |
| D814 | *152-0107-00 | Silicon | Replaceable by 1N647 |  |
| D815 | *152-0075-00 | Germanium | Tek Spec |  |
| D816 | *152-0075-00 | Germanium | Tek Spec |  |
| D819 | *152-0075-00 | Germanium | Tek Spec |  |
| D822 | *152-0075-00 | Germanium | Tek Spec |  |
| D824 | *152-0107-00 | Silicon | Replaceable by 1N647 |  |
| D826 | *152-0075-00 | Germanium | Tek Spec |  |
| D829 | *152-0075-00 | Germanium | Tek Spec |  |
| D832 | *152-0075-00 | Germanium | Tek Spec |  |
| D834 | *152-0107-00 | Silicon | Replaceable by 1N647 |  |
| D836 | *152-0075-00 | Germanium | Tek Spec |  |
| D839 | *152-0075-00 | Germanium | Tek Spec |  |
| D844 | *152-0075-00 | Germanium | Tek Spec |  |
| D852 | *152.0075-00 | Germanium | Tek Spec |  |
| D853 | *152-0075-00 | Germanium | Tek Spec |  |
| D854 | *152-0075-00 | Germanium | Tek Spec |  |
| D856 | *152-0075-00 | Germanium | Tek Spec |  |
| D859 | *152-0075-00 | Germanium | Tek Spec |  |
| D862 | *152-0075-00 | Germanium | Tek Spec |  |
| D863 | *152-0075-00 | Germanium | Tek Spec |  |
| D864 | *152-0075-00 | Germanium | Tek Spec |  |
| D866 | *152-0075-00 | Germanium | Tek Spec |  |
| D869 | *152-0075-00 | Germanium | Tek Spec |  |
| D872 | *152-0075-00 | Germanium | Tek Spec |  |
| D873 | *152-0075-00 | Germanium | Tek Spec |  |
| D874 | *152-0075-00 | Germanium | Tek Spec |  |
| D876 | *152-0075-00 | Germanium | Tek Spec |  |
| D879 | *152-0075-00 | Germanium | Tek Spec |  |
| D882 | *152-0075-00 | Germanium | Tek Spec |  |
| D883 | *152-0075-00 | Germanium | Tek Spec |  |
| D884 | *152-0075-00 | Germanium | Tek Spec |  |
| D886 | *152-0075-00 | Germanium | Tek Spec |  |
| D889 | *152-0075-00 | Germanium | Tek Spec |  |


| AUTOMATIC CARD (Cont'd) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Diodes (Cont'd) |  |  |  |  |
| Ckt. No. | Tektronix <br> Part No. |  | Description | Model No. |
| D901 | *152-0075-00 | Germanium | Tek Spec |  |
| D902 | *152-0075-00 | Germanium | Tek Spec |  |
| D905 | *152-0075-00 | Germanium | Tek Spec |  |
| D906 | *152-0075-00 | Germanium | Tek Spec |  |
| D907 | *152-0075-00 | Germanium | Tek Spec |  |
| D911 | *152-0075-00 | Germanium | Tek Spec |  |
| D912 | *152-0075-00 | Germanium | Tek Spec |  |
| D915 | *152-0075-00 | Germanium | Tek Spec |  |
| D916 | *152-0075-00 | Germanium | Tek Spec |  |
| D917 | *152-0075-00 | Germanium | Tek Spec |  |
| D920 | *152-0075-00 | Germanium | Tek Spec |  |
| D930 | *152-0075-00 | Germanium | Tek Spec |  |
| D935 | *152-0107-00 | Silicon | Replaceable by 1N647 |  |
| Transistors |  |  |  |  |
| Q654 | *151-0183-00 |  | Selected from 2N2192 |  |
| Q664 | *151-0183-00 |  | Selected from 2N2192 |  |
| Q674 | *151-0155-00 |  | Replaceable by 2N2925 |  |
| Q684 | 151-0164-00 |  | 2N3702 |  |
| Q714 | 151-0164-00 |  | 2N3702 |  |
| Q724 | *151-0155-00 |  | Replaceable by 2 N 2925 |  |
| Q734 | 151-0179-00 |  | 2N3877A |  |
| Q743 | *151-0155-00 |  | Replaceable by 2N2925 |  |
| Q754 | *151-0155-00 |  | Replaceable by 2N2925 |  |
| Q814 | *151-0183-00 |  | Selected from 2N2192 |  |
| Q824 | *151-0183-00 |  | Selected from 2N2192 |  |
| Q834 | *151-0183-00 |  | Selected from 2N2192 |  |
| Q854 | *151-0183-00 |  | Selected from 2N2192 |  |
| Q864 | *151-0183-00 |  | Selected from 2N2192 |  |
| Q874 | *151-0183-00 |  | Selected from 2N2192 |  |
| Q884 | *151-0183-00 |  | Selected from 2N2192 |  |
| Q903 | 151-0164-00 |  | 2N3702 |  |
| Q913 | 151-0164-00 |  | 2N3702 |  |
| Q923 | 151-0164-00 |  | 2N3702 |  |
| Q933 | 151-0164-00 |  | 2N3702 |  |

## Resistors

Resistors are fixed, composition, $\pm 10 \%$ unless otherwise indicated.

| R650 | $315-0102-00$ | 1 k | $1 / 4 \mathrm{~W}$ | $5 \%$ |
| :--- | :--- | :--- | :--- | :--- |
| R651 | $315-0102-00$ | 1 k | $1 / 4 \mathrm{~W}$ | $5 \%$ |
| R652 | $315-0681-00$ | $680 \Omega$ | $1 / 4 \mathrm{~W}$ | $5 \%$ |
| R654 | $315-0104-00$ | 100 k | $1 / 4 \mathrm{~W}$ | $5 \%$ |

## AUTOMATIC CARD (Cont'd)

Resistors (Cont'd)

| Ckt. No. | Tekfronix Part No. |  | Description |  |
| :---: | :---: | :---: | :---: | :---: |
| R660 | 315-0102-00 | 1 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R661 | 315-0102-00 | 1 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R662 | 315-0681-00 | $680 \Omega$ | $1 / 4 \mathrm{~W}$ | 5\% |
| R664 | 315-0104-00 | 100 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R666 | 315-0102-00 | 1 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R669 | 315-0222-00 | 2.2 k | 1/4W | 5\% |
| R670 | 315-0562-00 | 5.6 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R671 | 315-0273-00 | 27 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R672 | 315-0223-00 | 22 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R673 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R674 | 315-0391-00 | $390 \Omega$ | 1/4 W | 5\% |
| R675 | 315-0391-00 | $390 \Omega$ | $1 / 4 \mathrm{~W}$ | 5\% |
| R676 | 315-0105-00 | 1 meg | $1 / 4 \mathrm{~W}$ | 5\% |
| R678 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R679 | 315-0224-00 | 220 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R682 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R684 | 315-0102-00 | 1 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R686 | 315-0223-00 | 22 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R689 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R710 | 315-0103-00 | 10 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R712 | 315-0222-00 | 2.2 k | 1/4 W | 5\% |
| R714 | 315-0104-00 | 100 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R720 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R721 | 315-0472-00 | 4.7 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R724 | 315-0471-00 | $470 \Omega$ | $1 / 4 \mathrm{~W}$ | 5\% |
| R726 | 315-0105-00 | 1 meg | 1/4 W | 5\% |
| R728 | 315-0563-00 | 56 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R732 | 315-0104-00 | 100 k | 1/4W | 5\% |
| R734 | 315-0333-00 | 33 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R743 | 315-0224-00 | 220 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R745 | 315-0104-00 | 100 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R748 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R749 | 315-0333-00 | 33 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R750 | 315-0562-00 | 5.6 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R752 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R754 | 315-0222-00 | 2.2 k | 1/4W | 5\% |
| R802 | 315-0104-00 | 100 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R804 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R810 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R811 | 315-0104-00 | 100 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R812 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R814 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R816 | 315-0222-00 | 2.2 k | $1 / 4 W$ | 5\% |
| R819 | 315-0103-00 | 10 k | $1 / 4 \mathrm{~W}$ | 5\% |
| R820 | 315-0222-00 | 2.2 k | $1 / 4 \mathrm{~W}$ | 5\% |



## AUTOMATIC CARD (Cont'd)

Resistors (Cont'd)

| Description |  | Model No. |
| :---: | :---: | :---: |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| 1/4 W | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| 1/4 W | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| 1/4W | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| 1/4 W | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~V}$ | 5\% |  |
| 1/4 W | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| 1/4 W | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| 1/4 W | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 4 \mathrm{~W}$ | 5\% |  |
| $1 / 2 \mathrm{~W}$ | 5\% |  |
| $1 / 2 \mathrm{~W}$ | 5\% |  |

## AUTOMATIC CARD (Cont'd) Test Points

Ckt. No.

TP684
TP754

Tektronix
Part No.
*214-0579-00 Pin, Test Point
*214-0579-00 Pin, Test Point

Description
Model No.

## SECTION 8 MECHANICAL PARTS LIST

A list of abbreviations and special :ymbols in use throughout this manual will be found immediately preceding the Electrical Parts List, Section 7. Abbreviations and symbols used in this manual are based on or taken directly from IEEE Standard 260 "Standard Symbols for Units", MIL-STD-12B and other standards of the electronics industry. Parts ordering information is also located immediately preceding Section 7.


FRONT

| $\begin{array}{\|l\|l\|} \hline \text { REF. } \\ \text { NO. } \\ \hline \end{array}$ | PART NO. | SERIAL/MODEL NO. |  | Q <br> $\mathbf{T}$ <br> $\mathbf{Y}$ | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EFF. | DISC. |  |  |
| 1 | 333-0914-00 |  |  |  | PANEL, front |
| 2 | 386-0230-00 |  |  | , | PLATE, front subpanel |
| 3 | 366-0230-00 |  |  | 1 | KNOB, charcoal-MANUAL VOLTS/DIV |
|  | - - - - |  |  | - | knob, includes: |
|  | 213-0004-00 |  |  | , | SCREW, set $6-32 \times 3 / 16$ inch, HSS |
| 4 | 366-0081-00 |  |  | 1 | KNOB, red-VARIABLE |
|  | - - - - |  |  | - | knob, includes: |
|  | 213-0004-00 |  |  | , | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| 5 | 262-0741-00 |  |  | 1 | SWITCH, wired-MANUAL VOLTS/DIV |
|  | - - - - |  |  | - | switch includes: |
|  | 260-0690-00 |  |  | 1 | SWITCH, unwired-MANUAL VOLTS/DIV |
| 6 | 179-1016-00 |  |  | 1 | CABLE HARNESS, switch |
|  | $\cdots$ |  |  | - | mounting hardware: (not included w/switch) |
|  | 210-0413-00 |  |  | 1 | NUT, hex., $3 / 8-32 \times 1 / 2$ inch |
| 7 | 336-0215-01 |  |  | 1 | KNOB, lever-AC-TRACE STABILIZED-AC-DC |
|  | 366-0341-00 |  |  | 1 | KNOB, charcoal-POSITION |
|  | - - - - |  |  | - | knob includes: |
|  | 213-0076-00 |  |  | 2 | SCREW, set, $2-56 \times 1 / 8$ inch, HSS |
| 9 | - . . . - |  |  | 1 | POT |
|  | - - - - |  |  | - | mounting hardware: (not included w/pot) |
|  | 210-0583-00 |  |  | 1 | NUT, hex., $1 / 4-32 \times 5 / 16$ inch |
|  | 210-0940-00 |  |  | 1 | WASHER, flat, $1 / 4 \mathrm{ID} \times 3 / 8$ inch OD |
|  | 210-0223-00 |  |  | , | LUG, solder, $1 / 4$ inch |
| 10 | 129-0053-00 |  |  | 1 | ASSEMBLY, binding post |
|  | - --- |  |  | - | assembly includes: |
|  | 355-0507-00 |  |  | 1 | STEM, binding post |
|  | 200-0103-00 |  |  | 1 | CAP, binding post |
|  | - - - - |  |  | - | mounting hardware: (not included w/assembly) |
|  | 210-0455-00 |  |  | 1 | NUT, hex., $1 / 4-28 \times 3 / 8$ inch |
|  | 210-0046-00 |  |  | 1 | LOCKWASHER, int, . 261 ID $\times .400$ inch OD |
| 11 | $366-0109-00$ $\cdots-\cdots$ $213-0004-00$ |  |  | 1 | KNOB, aluminum, securing, knob includes: SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| 12 | 214-0052-00 |  |  | 1 | FASTENER, pawl right, w/stop |
|  | - - - - |  |  | - | mounting hardware: (not included w/fastener) |
|  | 210-0004-00 |  |  | 2 | LOCKWASHER, internal, \#4 |
|  | 210-0406-00 |  |  | 2 | NUT, hex., $4-40 \times 3 / 16$ inch |
| 1314 | 131-0407-00 |  |  | 1 | JACK, telephone, w/hardware-REMOTE SEEK |
|  | 131-0408-00 |  |  | 1 | CONNECTOR, 37 pin , female |
|  | - -- - |  |  | - | mounting hardware: (not included w/connector) |
|  | 210-0004-00 |  |  | 2 | LOCKWASHER, internal, \#4 |
|  | 210-0406-00 |  |  | 2 | NUT, hex., $4-40 \times 3 / 16$ inch |
|  | 358-0054-00 |  |  | 3 | BUSHING, banana jack, $1 / 4-32 \times 13 / 32$ inch |
| 1516 | . . . . - |  |  | 1 | POT |
|  | … |  |  | - | mounting hardware: ( not included w/pot) |
|  | 210-0471-00 |  |  | 1 | NUT, hex., $1 / 4-32 \times 5 / 16 \times 19 / 32$ inch long |
|  | 210-0046-00 |  |  | 1 | LOCKWASHER, int, . 261 ID $\times .400$ inch OD |

FRONT (Cont'd)


FRONT (Cont'd)



CHASSIS


CHASSIS (Cont'd)



REAR (Cont'd)










## MANUAL CHANGE INFORMATION

At Tektronix, we continually strive to keep up with latest electronic developments by adding circuit and component improvements to our instruments as soon as they are developed and tested.

Sometimes, due to printing and shipping requirements, we can't get these changes immediately into printed manuals. Hence, your manual may contain new change information on following pages. If it does not, your manual is correct as printed.

TYPE 3 A 5
PARTS LIST CORRECTION

CHANCF TO:

| Q143 | $151-0175-00$ |
| :--- | :--- |
| Q183 | $151-0108-00$ |
| Q343 | $151-0175-00$ |
| Q383 | $151-0108-00$ |
| Q903 | $151-0188-00$ |
| Q913 | $1.51-0188-00$ |
| Q923 | $1.51-0188-00$ |
| Q933 | $151-0184-00$ |

Replaceable by $2 N 3662$
Silicon Replaceable by 2 N 2501
Replaceable by $2 N 3562$
Silicon Replaceable by $2 N 2501$
Replaceable by 2N3906
Replaceable by $2 N 3906$
Replaceable by $2 N 3906$
Replaceable by $2 N 3906$

PARTS LIST CORRECTION

Add:

| C2 | $283-0059-00$ | $1 \mu \mathrm{~F}$ | Cer. | $+80 \%$ | $-20 \%$ | 25 V |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| C528 | $283-0078-00$ | .001 | Cer. | $\pm 20 \%$ | 500 V |  |

SCHEMATIC CORRECTION


PART ATTEN. \& SWITCHING

PARIS LIST CORRECTION
ADD:
R421 308-0244-00 . $3 \Omega$ 2W $10 \%$
CHANGE TO:
Q724
R720
151-0108-00
Silicon
315-0103-00 10 k
Replaceable by $2 N 2501$ $1 / 4 \mathrm{~W} \quad 5 \%$

SCHEMATIC CORRECTION


PARTIAL PWR. DISTRIBUTION DIAG.

