## PRELIMINARY INSTRUCTION MANUAL

## TYPE 5TIA TIMING UNIT



This is a preliminary instruction manual. It is not complete, and it may contain minor errors. We will send you the permanent instruction manual just as soon as it is ready. Be sure to complete and send in the attached card so that we can send the manual directly to the user of the instrument.

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Tektronix, Inc.
S.W. Millikan Way P. O. Box 500 - Beaverton, Oregon Phone MI 4-0161 Cables: Tektronix

Tektronix International A. G.

## SECITON 1

GENERAL DESCRIPTION
Introduction
The Type 5T1A Timing Unit is a sampling-type timing plug-in unit for use with the Tektronix Type 661 Oscilloscope, and 14 ' Series sampling plug-in units. The Type 5T1A can receive trigger signals either through a frontpanel connector (externally supplied) or through interconnecting wiring from vertical sampling units which have provisions for internal trigger takeoff. Trigger signals must bear a fixed time relationship to the signals to be displayed by the sampling unit.

The Type 5T1] has 16 calibrated equivalent-time sweep rates. Any sweep rate may be continuously increased to about $3 X$ faster than the calibrated rate. A 7 -position TTME EXPANDER switch allows any portion of the display to be expanded with a constant dot density. A front-panel control selects the number of samples per centimeter of horizontal deflection. A single-display circuit allows the operator to start a single horizontal sweep.

The triggering circuit will operate either on negativegoing or positive-going signals. Trigger threshold is adjustable over a $\pm 200-m i l l i v o l t ~ r a n g e ~ f o r ~ e i t h e r ~ p o s i t i v e-g o i n g ~ o r ~ n e g a t i v e-~$ going signals. Trigger source may be selected internally from the sampling unit, externally through a front-panel connector on the Type 5T1A, or internally from the Type 661 Amplitude/Time Calibrator. The trigger circuit may also be free-run at its maximum repetition rate. The repetition rate of the trigger circuit is determined by the setting of the SWEEP TTME/CM switch and the RECOVERY TIME control.

The RECOVERY TTME control provides a range of trigger recovery times, allowing the operator to adjust for jitter-free triggering.

A TIME POSITION control provides a variable time delay for time-positioning the signal display in the TIME EXPANDER switch $X_{1}$ position. In the expanded positions, the TIME POSITION control moves the time "window" anywhere within the original range displayed in the $X 1$ position of the TIME EXPANDER switch.

## Operating Characteristics

Sweep Time/Cm -- Sweep rates in 16 calibrated steps of equivalent time from $1 \mathrm{nsec} / \mathrm{cm}$ to $100 \mu \mathrm{sec} / \mathrm{cm}$ in a L, 2, 5, 10 sequence. An uncalibrated variable control provides a continuous range up to $3 X$ the calibrated rate between steps. A variable control extends the fastest rate to about $1 / 3 \mathrm{nsec} / \mathrm{cm}$. All calibrated rates better than 3\% accuracy.

Samples/Cm -- 5, 10, 20, 50, and 100, $\pm 3 \%$ accuracy; also 1000 and timed sweep, with an unmagnified display.

Sweep Mode -- Repetitive or single display.
Trigger Source -- External, internal, free run, and calibrator. Sensitive to positive-going or negativegoing slope.

Triggering Threshold -- Continuously variable over a $\pm 200-\mathrm{mv}$ range.

Trigger Sensitivity -- Internal or External: 5 mv external for a 1 nsec pulse. (Internal level is determined by output of sampling unit trigger-takeoff circuit.)

Recovery Time -- Variable from about 10 to about $13 \mu \mathrm{sec}$ on sweep rates faster than $0.2 \mu \mathrm{sec} / \mathrm{cm}$; longer on slower sweep rates.

Time Expansion -- Provides X1, X2, X5, X10, X20, X50, and X100 expansion of sweep rate selected with a constant number of samples/cm. Expansion may be selected to fall anywhere in basic time-base range, determined by SWEEP TIME/CM switch setting.

Time Position -- Provides continuously variable time display window. Time position range is controlled by the TTME EXPANDER and SWEEP TTME/CM switches. Table 1-1 lists the ranges as a function of control settings.

Time Jitter -- Less than 30 psec (picoseconds), or $10^{-4}$ $x$ (fast ramp duration), whichever is greater, in $100-\mu$ sec through $2-n s e c / \mathrm{cm}$ sweep rates. Less than 10 psec at $1 \mathrm{nsec} / \mathrm{cm}$ sweep rate. External trigger "kickout" is less than 5 mv .

TABIE 1-1
Time Range of TIME POSITION Control

| SWEEP TTME/CM switch Setting | TIME EXPANDER Switch Setting |  |  |
| :---: | :---: | :---: | :---: |
|  | XI | X2 | $\begin{aligned} & \times 5, x_{10}, \times 20, \\ & \times 50, x_{100} \end{aligned}$ |
| 100, 50, or $20 \mu \mathrm{SEC}$ | $100 \mu \mathrm{sec}$ | $500 \mu \mathrm{sec}$ | $1000 \mu \mathrm{sec}$ |
| 10, 5, or $2 \mu \mathrm{SEC}$ | $10 \mu \mathrm{sec}$ | $50 \mu \mathrm{sec}$ | $100 \mu \mathrm{sec}$ |
| 1, . 5 , or $2 \mu \mathrm{SEC}$ | $1 \mu \mathrm{sec}$ | $5 \mu \mathrm{sec}$ | $10 \mu \mathrm{sec}$ |
| . $1 \mu \mathrm{SEC}, 50 \mathrm{nSEC}$, or 20 nSEC | $0.1 \mu \mathrm{sec}$ | $0.5 \mu \mathrm{sec}$ | $1 . \mu \mathrm{sec}$ |
| 10, 5, or 2 nSEC | 100 nsec | 100 nsec | 200 nsec |
| 1 nsec | 10 nsec | 10 nsec | 20 nsec |

## SECTION 2

OPERATING INSTRUCTIONS
Introduction
The operating instructions are divided into three parts. First is a description of front-panel controls and connectors. Second is a discussion of methods of triggering the Type 5T1A. Third is a discussion of the controls.

Because the Type 5T1A is part of a system, we suggest that you also familiarize yourself with the information in the Type 661 Instruction Manual and for the '4' Series sampling unit used. Familiarize yourself with the operation of the system by displaying the Amplitude/Time Calibrator and Delayed Pulse signals available from the Type 661. We also suggest that you read the booklet "Sampling Notes", Tektronix publication number 061-557.

The Type 5T1A requires a trigger signal with a definite time relation to the signal to be displayed. These trigger signals may be obtained internally, when a sampling unit with internal trigger takeoff provisions is used. They may also be externally fed to the Type 5T1A through a front-panel connector. The Timing Unit may be triggered by either positiveor negative-going signals of 5-to 250-millivolts peak-to-peak amplitude.

FITVCTION OF FRONT-PANEL CONIROLS AND CONNECTORS
SWEEP TTME/CM ................. The SWEEP TIME/CM switch sets the equivalent time/horizontal cm of display when the VARIABLE control is in the CALIBRATED position.

system in a free-run mode at which time stable displays may be obtained from the Type 661 Delayed Pulse generator, or from a system that has been triggered by the delayed pulse.

TRIGGERING POIARITY Permits starting the display on a negative-polarity pulse (-), or on a positive-polarity pulse (+). A CAL position permits triggering on the Type 661 Amplitude/Time Calibrator signal, internally connected. The CAI position is useful when displaying small signals from the Amplitude/Time Calibrator.

EXIPERNAL TRIGGER INPUT A nominally $50 \Omega$, ac-coupled, external trigger input connector. Mates with General Radio Type 874 connectors. Allows direct connection of the Type 5T1A to the triggering signal when the signal is less than the required 40 mv for internal triggering. Signals from 5 to 250 mv will permit proper operation of the timing unit. For proper triggering on slow-rise signals, $10-\mathrm{mv} / \mu \mathrm{sec}$ minimum rate of change is required. See Fig. 2-1.



TRIGGERING THRESHOID .......... The Type 5TIA trigger system is sensitive to signals exceeding 5 mv. The THRESHOLD control determines the signal level needed to trigger the system. Setting the triggering POLARITY control in the + position and the THRESHOLD control fully clockwise will hold off the triggering system for normal amplitude positive trigger signals. Turning the THRESHOTD control counterclockwise permits proper triggering as the trigger-to-threshold voltage difference is brought to zero. Triggering occurs as the extreme positive portion of the triggering signal reaches the threshold voltage. Turning the THRESHOLD control further counterclockwise will finally produce a free-running sweep, at the condition when the trigger signal base-line level reaches the threshold voltage. The same conditions exist when the POLARITY switch is at - and the THRESHOLD control is turned in the + direction.


Installation
Before installing the Type 5T1A, be sure the Type 661 POWER and SCALE ILLUM. contrnt is in the POWER OFF position. If the Iype 5T1A is installed when the power is on, damage may result.

Pull out the lock bar located at the bottom of the Type 661 timing plug-in unit compartment. Insert the Type 5?1A in the plug-in compartment, and press it firmly in place so that the connectors mate. When placed properly, the Type 5T1A front panel will be tight against the Type 661 front panel, and the lock will move to about a. $45^{\circ}$ angle with the front-panels. Press the lock bar firmly against the front panel.

NOTE


#### Abstract

The Delayed Pulse generator of the Type 661 Oscilloscope must be readjusted for each Type 5TIA unit used. See the Calibration section of this manual for procedure.


## TRIGGERING CONSIDERATIONS

The Type 5T1A may be triggered from either internal trigger signals, when a sampling unit with trigger takeoff provisions is used, or from an external source. The Type 661 Amplitude/Time Calibrator may also be internally connected to trigger the Type 5T1A. The trigger pulse must be related in time, and have a repeitition rate equal to or less than that of the signal displayed. It must also meet amplitude and timing requirements, as discussed in the following paragraphs.

## Internal Source

When a sampling unit is used that has internal triggertakeoff circuitry and vertical-signal delay following the trigger takeoff, such as the Type 4,S1, the signal itself may be used to trigger the Type 5T1A. The signal sent from the sampling unit must be at least 5 mv , determined by the ratio of input signal to the division of signal by the sampling unit. The Type 4 Sl , for example, provides a trigger signal about $1 / 8$ the amplitude of the input signal, thus the input signal must be at least 40 millivolts for internal triggering. The internal trigger signal is ac or dc coupled into the Type 5TIA and is controlled by the sampling unit. Placing the Type 5T1A SOURCE swi.tch in the INT. position connects the
internal trigger from the sampling unit. The Type 4S1 provides vertical signal delay following the trigger-takeoff circuit which allows the signal that triggers the Type 5T1A to be displayed.

The Type 661 Delayed Pulse may be used to trigger a circuit under test. The Delayed Pulse generator is driven by the trigger circuit of the Type 5T1A, and delivers about a $-400-\mathrm{mv}$ pulse. The pulse appears about 40 nsec after the trigger circuit has operated, allowing the sampling unit to view the delayed pulse. To obtain the delayed pulse, place the triggering SOURCE switch in the FREF RUN position. Repetition rate of the pulse is determined by the repetition rate of the Type 5T1A trigger circuit, controlled by the triggerholdoff circuit. This rate may be varied by use of the RECOVERY TTME control.

When the Type 5T1A is used with a sampling unit having a delay line, such as the Type 4 Sl , the Delayed Pulse from the Type 661 must be viewed with the SWEEP TIME/CM switch in the 2 nSEC or slower sweep rate position. In the 1 nSEC sweep rate position, the signal delay of the sampling unit places normal input signals in the TITNE POSITION control range, which is 10 to 20 nsec at this sweep rate. To view the Delayed Pulse on a signal-delaying sampling unit at a l-nsec or faster sweep rate, place the SWEEP TIME/CM control in the 2 nSEC position and use the TIME EXPANDER switch to increase the sweep rate. This allows at least 100 nsec of TIME POSITION control range, and delays the sweep sufficiently to display the Delayed Pulse.

## External Source

When a sampling unit without signal delay (such as the Type 4 S2) is used, and external trigger signal must be supplied to the Iype 5TIA EXTERNAL TRIGGER INPUT connector. External triggering also may be used instead of internal triggering when a sampling unit such as the Type 4S1 is used. Placing the SOURCE switch in the EXT, position connects the EXXIERNAL TRIGGER INPUT connector through an ac-coupling circuit and through an isolation stage to the trigger circuit.

The Type 5T1A must be triggered at leas+ 35 nsec before the signal reaches the sampling gate of the sampling unit. The IIME POSIPION control allows an extra delay in operat:on, added to the 35 nsec requirement. Thus, the time window after triggering that is displayed may be moved a considerable distance in time, allowing flexibility in test setup. Remember that as little as 8 inches of $R G-8 A / U$ cable can insert an extra nsec of delay.

There are two methods of triggering the Type 5T1A before the signal arrives at the sampling-unit sampling gate. The first is to pretrigger the Iype 5T1A by using a pulse generator that triggers the system, and some time later triggers the circuit under test. The second is to insert some delay in the signal connections to the sampling unit so that the signal will arrive at the sampling gate after the Type 5T1A is triggered (occurs internally in Type 4S1). The following are some examples of each method:

## Pretriggering

This method may be used when the circuit under test can be triggered, producing the signal to be displayed some finite
time after it has been triggered. Iypical circuits of this sort are blocking oscillator and avalanche transistor circuits. A suitable pretrigger generator is a Tektronix Type 111 Pretrigger Pulse Generator. The Type $11 l$ supplies a trigger signal to the Type 5T1.A, and some time later, supplies a trigger signal for the circuit under test. The system should be adjusted so that the time between the pretrigger signal sent to the Type 5T1A and the trigger sent to the circuit under test is 35 to 50 nsec , minus the time delay in the circuit under test between triggering and signal output.

When using the pretriggering technique, remember that any time jitter between the pretrigger and the signal sampled will be displayed as time-jitter.

## Signal Delay

This method is suitable for circuits which cannot be triggered by some external means. A suitable delay line for most applications is the Tektronix Type 113 Delay Cable, which provides a 60-nsec delay with a risetime under 0.1 nsec .

When the input signal must be used to trigger the Type 5T1A, a suitable arrangement must be made to split the signal so that it may also drive the trigger circuit of the Type 5T1A.

A suitable transformer-type trigger takeoff is the Tektronix CT-1 Nanosecond Current Transformer. This unit does not require an input circuit of any specific impedance. Its output is $5 \mathrm{mv} / \mathrm{ma}$. Since the current in the input circuit follows ohm's law, the output of the CT-l may be quickly calculated from the following equation:
$E_{\text {out }}=\frac{5 E_{\text {sig }}}{Z}$
where: $E_{\text {out }}=5 T 1 \mathrm{~A}$ output in millivolts

$$
\begin{aligned}
E_{s i g} & =\text { signal amplitude (ac) in millivolts } \\
Z & =\text { characteristic impedance of the signal circuit }
\end{aligned}
$$

The CT-I output impedance is $50 \Omega$ - suitable for direct
connection to the Type 5TIA EXTERNAL TRIGGER INPUT connector. Remember that the input to the Type 5T1A must be in the 5 -to 250-mv range of the trigger circuit.

A Tektronix VP-1 Voltage Pickoff unit may also be used as a trigger signal source. The Type VP-1 works with either a Tektronix P6034 or P6035 Probe. When using the VP-1, the effect of the P 6034 or P 6035 on the system impedance must be considered, as well as the output voltage which will arrive at the EXIERNAL TRIGGER INPUT connector.

An impedance matched " T " with $16.7 \Omega$ in all 3 legs will divide an input signal into 2 equal, $1 / 2$ amplitude signals; one for a $50 \Omega$ vertical input to the sampling unit and one for the timing unit. Thus, a 10-mv signal will provide 5 mv for viewing and 5 mv for triggering.

The Type 110 allows transformer-type trigger takeoff from a $50 \Omega$ system. $98 \%$ of the signal passes through the signal system for viewing, while a trigger signal $20 \%$ of the signal voltage is provided by the unit for use in triggering the Type 5T1A. The Type 110 has a dynamic range versatility which will allow most signals from a $50 \Omega$ source to be used in triggering the Type 5T1A. When the Type 110 is used, be sure the trigger takeoff output fed to the Type 5T1LA is within the 5 -to 250-mv range of the trigger circuit. The pulse generator section of the Type 110 may be used to trigger a circuit under test. Typical test setups using the Type 110 are shown in the Type 110 Instruction Manual.

## Trigger Signal Repetition Rate

The Tektronix Type 280 Trigger Countdown unit can be used to reduce the repetition rate of trigger signals with frequencies (or repetition rates) up to $5 \mathrm{gc}\left(50 \times 10^{6}\right.$ to $5 \times 10^{9}$ trigger signals/second) for more stable triggering. The trigger signal is fed to the Type 280, and the output from the FAST RISE OUTPUT connector is connected to the Type 5TIA EXTERNAL TRIGGER INPUT connector. Adjusting Triggering POLARITY and THRESHOLD

The Type 5TIA POLARITY switch selects triggering on either positive-going (+) or negative-going (-) signals. The IHRESHOLD control can select the voltage point, (within a $\pm 20-\mathrm{mv}$ range) where the trigger circuit will actually operate. Once the signal voltage passes the threshold point set by the THRESHOID control, the trigger circuit can freerun until the signal voltage once again drops below the threshold point. The maximum repetition rate of the trigger circuit is controlled by a trigger holdoff circuit, and may be increased about $30 \%$ by the RECOVERY TIME control.

Set the POLARITY switch at + to trigger on positivegoing signals; at - to trigger on negative-going signals. The THRESHOLD control can set the triggering threshold anywhere over a $\pm 200-m v$ range. Adjustment should start with the THRESHOLD control in the same polarity region for which the POLARITY switch is set (+ for +, - for -). The THRESHOLD control should be adjusted toward the opposite polarity region. Set the THRESHOLD control so that stable minimum-jitter triggering occurs. If the THRESHOLD control is moved too far toward the opposite polarity region, multiple triggering
may occur, and multiple traces may be displayed on the crt. Turning the THRESHOLD control further will cause the trigger circuit to free-run, and the display will be meaningless. During these adjustments, the RECOVERY TIME control should be set to MIN., allowing the trigger circuit to operate at the highest possible repetition rate. Experimenting with the THRESHOLD control and a signal display from the Type 661 Amplitude/Time' Calibrator with the POLARITY switch set to CAL. will help you use the THRESHOLD control properly.

"False" Display

It is possible to nbtain a "false" display on the crt when using a low sampling density, and when the sweep rate selected is such that several cycles of signal will be displayed on the crt. To illustrate, connect a $100-\mathrm{mv}$, $10-\mu \mathrm{sec} / \mathrm{cyc} 1 \mathrm{e}$ signal from the Type 661 Amplitude/Time Calibrator to the Type 5TIIA. Set the Type 5TIA SWEEP TIME/CM control to $100 \mu \mathrm{SEC}$, the SAMPLES/CM control to 5, the triggering SOURCE switch to CAL., and the TIME EXPANDER switch to XI. You should obtain about a 2-cycle display on the crt, although, by calculation, you should obtain 10 cycles $/ \mathrm{cm}$. Now move the SAMPLES/CM switch to 1000 and observe the display in each position between 5 and 1000 samples $/ \mathrm{cm}$. You should see, with 1000-samples/cm density, the calculated 10 cycles $/ \mathrm{cm}$. The reason for the false display with the lower sampling densities is that there are not enough samples taken to trace the outline of each cycle. The samples seen in the false displays lie on the true curve, but àre insufficient to . display its outline. The effect is similar to the plotting of a graph with insufficient information points. Check for
false displays by moving the SAMPLES/CM control to another position. If the outline of the display is correct, the samples will remain the same in both positions. Inrreasing the sweep rate with a constant number of samples/cm decreases equivalent sweep time between samples, and allows a lower sampling density to provide a proper display.

Recovery Time
The recovery time of the trigger-recognition circuit is controlled by the holdoff circuit. The recovery time is dependent on the time required for fast-ramp operation, or the l00-kc maximum repetition rate, whichever is greater. If the duty factor of the trigger signal is long, in relation to the repetition rate of the Type 5T1A, multiple triggering may occur. The RECOVERY TIME control can often be used to improve triggering under these circumstances. This control should be set to MTN. for initial adjustments. If multiple triggering is obtained, the RECOVERY TIME control may be adjusted to provide proper triggering. The best setting for the control is determined by experiment. The RECOVERY TTME control can increase recovery time by about $30 \%$.

## OBTAINING A DISPI_AY

1. Set the iPRIGGERING SOURCE switch for the same polarity as the trigger signal.
2. Select a sweep time/cm long enough to permit viewing the signal. If unknown, start at $10 \mathrm{nsec} / \mathrm{cm}$.
3. Set the SAMPLES/CM switch to 5. This can be increased to a larger number if a more continuous trace is desired.
4. Turn the TIME POSITION control fully clockwise. It can later be set to bring the desired signals in view on the crt. Set the TIME EXPANDER switch to Xl .
5. Set the RECOVERY TIME control to MIN.
6. Set the THRESHOLD control to hold off the sweep (cw +, ecw -). Thurn the control toward zero for proper triggering.
7. If triggering difficulties occur, establish whether the trouble is due to: (a) too low or too high trigger amplitude, (b) too high a trigger-signal repetition rate, (c) too low a rate of rise (or fall) of trigger-signal voltage, or (d) interference due to recovery time. The cause can usually be found by operating the SWEEP TTME/CM switch, THRESHOID, and RECOVERY TIME controls. Inability to hold off the sweep with the THRESHOLD control indicates too large a trigger signal. Use an input attenuator to reduce amplitude. If advancing the THRESHOLD control causes the sweep to free-run before obtaining a stable display, either amplitude or rate-of-change is too low. If the problem is high repetition rate, and moving the RECOVERY TTME control does not stabilize a display, an external trigger-countdown unit such as Tektronix Type 280 may be needed. If the signal has a low rate of rise (for example, sinewaves below about 50 kc ), a faster-rising trigger signal is needed. (Dc triggering is available internally only. See sampling unit instruction manual.) Tf confused triggering results in the form of multiple
traces, try operating the RECOVERY TIME control.

ADJUSIING THE SYSTMM FOR BEST VIEWING
Once you have obtained a display and located the signal you wish to view on the crt, you may adjust for increased resolution by expanding the portion of the display you wish to study and by increasing sampling density.

1. To expand the portion you wish to display, increase the sweep rate with the SWEFP TIME/CM switch. This is the best method since time-jitter is held to a minimum. The TIME POSITION control may be used to position the signal onto the crt. Another method is to use the TTME EXPANDER switch and then to position the portion you wish to observe with the TIME POSITION control. The TIME EXPANDER switch allows you to position signals occurring over \& relatively large period of time compared with the length of the time window actually displayed.
2. To increase sampling density, increase the number of samples/cm with the SAMPTES/CM switch. Note that increased sampling density provides smoothing of the trace. When using smoothing, check for sufficient dot transient response by moving the SAMPTES/CM switch to the next higher density and checking for transient information that was not present on the display. Generally, the best setting for the SAMPLES/CM switch is for the highest density with reasonable display repetition rate.

Timed Operation
This includes using the timed sweep and single display
features. To use the timed sweep, set the SAMPTES/CM switch to TTMED. This should be done after the system is set up to display the desired signal. With the SAMPTES/CM switch in TIMED, the system is no longer dependent on trigger repetition rate for display sweep, but will display a signal linearly over 7 period of time. The rate at which the display moves across the crt may be adjusted by use of the front-panel screwdriver adjustment immediately under the SAMPTES/CM switch.

The timed sweep may be used when signals from the Type 661 vertical-signal output connectors are used to drive a clock-type recorder. The timed sweep allows the sweep rate (of the display) to be synchronized with the rate at which the recorder operates.

The Type 5T1A Timing Unit is used with '4' Series sampling units in the Type 661 Oscilloscope. The Timing Unit is triggered by signals with a fixed time relationship to repetitive identical signals displayed on the crt. The sampling technique allows resolution of repetitive identical signalvoltage changes occurring at fractional nanosecond (less than $10^{-9}$ second) rates with a broad bandpass for resolution of signals approaching de.

The function of the Type 5T1A is to control the time at which the sampling unit takes the sample, and to simultaneously provide the display oscilloscope with a horizontal deflection signal. The horizontal deflection signal represents the time that elapses after the Type 5T1A is triggered before the sample is taken. By taking a series of samples, each one occurring a little later after triggering than the last, the display constructs a representation of the repetitive signals that were sampled.

The Type 5T1A has three major functional sections shown in simplified block diagram, Fig. 3-1. First is the trigger recognition and regeneration circuit, which triggers the operation of the remainder of the unit, and in turn must be triggered by a signal time-related to that displayed. Second is the fast ramp and comparator circuit. The fast ramp is a voltage fall with a constant calibrated slope. This voltage is fed to the comparator and compared with another voltage which represents the amount of horizontal deflection. The comparator provides a pulse output trigger to the sampling unit when the voltages are equal. Thus, the horizontal-
deflection voltage level fed to the comparator represents a calibrated interval of time following the operation of the trigger circuit.


Fig. 3-1. Type 5TIA simplified block diagram.

Third is the staircase generator. When the Type 5T1A provides the horizontal deflection (Type 661 HORIZONTAL DISPLAY control in a SWEEP MAGNIFIER position), the staircase generator provides the horizontal deflection signal. The staircase steps one voltage increment after each sample is taken. When enough increments are stepped over, and a full display sweep is completed (about $101 / 2 \mathrm{~cm}$ ), the staircase resets and repeats the display. The size of each increment is controlled by the SAMPLES/CM switch determining the density (in equivalent time) of the samples.

The system may be triggered by an external 5 to 250 mv signal through a front-panel connector. Internal triggering from the signal applied to the sampling unit is also possible when the sampling unit used has a trigger takeoff circuit (such as the Type 4S1). Trigger circuit threshold may be set by a front-panel control.

The trigger recognition and regeneration circuit must receive trigger signals having a fixed time relation to the signal to be displayed. This circuit provides an output pulse to the time base (fast ramp) and the Type 661 Delayed Pulse generator for each trigger signal that operates the circuit. The holdoff circuit allows the trigger recognition circuit to operate only when the system is prepared for a new sample (never more often than about every 10 microseconds).

The trigger-recognition circuit triggers a fast-ramp voltage-rundown circuit. The fast-ramp circuit generates a voltage with a constant calibrated slope. Because the slope of the ramp is constant, some given time after triggering is equivalent to the time required for the fast-ramp voltage to travel from its starting point to a specific voltage. Thus, if the ramp slope is -5 volts/ $\mu \mathrm{sec}$, the equivalent voltage for $2 \mu \mathrm{sec}$ is -10 volts. In the Type 5T1A, the fast-ramp slope is controlled by the SWEEP TIME/CM switch. The total voltage change of the fast ramp, representing full-scale horizontal deflection on the crt, is selected by the SWEEP TIME/CM and TIME EXPANDER switches.

The Type 5T1A is provided with a staircase generator which advances a voltage increment after each run of the fast ramp. The staircase output voltage is normally fed to the Type 661 horizontal amplifier. When the Type 661 HORIZONTAL DISPLAY switch is in a SWEEP MAGNIFIER position, the staircase voltage is supplied to the comparator portion of the fast-ramp circuit. When the fast ramp has run from its starting voltage to the comparison voltage fed to the comparator, the comparator initiates a pulse, which is sent to
the sampling plug-in unit. The staircase voltage, which represents time after the trigger has occurred, is also fed to the horizontal display circuit of the Type 661. The horizontal deflection caused by the staircase voltage represents the time it takes the ramp voltage to run down to the same voltage as the staircase level. The voltage increments of each step of the staircase voltage determine the equivalent time-spacing between samples.

When the Type 661 HORIZONTAL DISPLAY switch is in the EXT. HORIZ. INPUT positions, the staircase voltage is not used. Instead, the deflection caused by the external horlzontal input voltage determines the time after triggering when samples are taken. The Type 5T1A must be triggered in the same manner as it was when the staircase was used to provide horizontal deflection. The position of the trace on the crt, determined by the horizontal input signal, determines the time after triggering when a sample will be taken. Thus, if the left graticule edge represents a specific time $T_{0}$, and the SWEEP TIME/CM switch is set at 10 nSEC, the vertical deflection at the fifth graticule mark will represent the signal at the input occurring 50 nsec after $\mathbb{T}_{0}$. Note that the input voltage to the external horizontal circuit of the Type 661 and Type 5TIA system always represent time when displayed on the crt.

Manual scan also provides a display of equivalent time. With the SWEEP TIME/CM switch at 10 nSEC , scanning the crt with the HORIZONTAL POSITION controls will cover an equivalent time from $T_{0}$ to $\left(T_{0}+100\right) \mathrm{nsec}$.

A time-expander circuit allows the system to view only a portion of the fast-ramp rundown time, displaying this time as a full 10 cm display. The expanded time portion of the turndown is determined by the TIME EXPANDER switch and TIME POSITION control. The TTME EXPANDER switch determines the length (difference in voltage between beginning and end) of the fast-ramp rundown portion used. The TIME POSITION control sets the de level of the portion used, effectively shifting the time scanned. Notice that magnifying the signal with the TIME EXPANDER switch allows a portion of the signal to be viewed with a constant number of samples/cm. The Type 661 SWEEP MAGNIFIER switch allows a portion of the signal to be viewed, with a decrease in the number of samples/ centimeter (constant time/dot) in the crt display. A combination of the two magnification methods may be used.

## Trigger Recognition Circuits

Two trigger-recognition circuits are used. One responds to positive-trigger information, and one responds to negativetrigger information. The trigger-recognition circuit used is selected by POLARITY switch SWIOB. When the POLARITY switch is in the CAL. position, the signal from the Type 661 Amplitude/Time Calibrator is fed to the negative-trigger recognition circuit. The trigger-recognition circuits are similar except that they use opposite input and supply voltage polarities. The external trigger information is inverted by T 2 before being fed to the trigger-recognition circuits. Isolation amplifier Q4 isolates the external trigger input from the trigger-recognition circuits.

The trigger source is selected by SOURCE switch SWIOA. Trigger signals may be internally supplied by the sampling unit if the sampling unit has a trigger takeoff circuit. They may also be supplied from an external source. External triggering is necessary when the sampling unit has no provisions for trigger takeoff or when low amplitude signals are being sampled. The SOURCE switch selects the trigger source, and feeds the signals to the POLARITY switch which directs the signals to one of the trigger-recognition circuits. When the SOURCE switch is in the FREE RUN position, a bias is applied to the trigger-recognition circuit selected by the POLARIIY switch, causing the trigger-recognition circuit to free-run. The THRESHOLD control sets the level (over a $\pm 200$ mv range) at which triggering occurs, and the + and - positions of the POLARITY switch set the direction in which the signal must move to cause triggering.

Assume TRIGGERING SWITCHES SWIOA and SW1OB are set to - INT as shown on the Trigger and Holdoff schematic. The THRESHOLD control is set far enough into the - region to hold off the trigger circuit. Assume also that the trigger circuits are ready to retrigger. D25 rests at its low state, near the switching point. D25 receives bias current from two sources. One is through R20, R21, R22, and L25. In addition, D35 is already in the high state, and current is supplied through R33. D25 is ready to trigger. If we move the THRESHOLD control to its + region, the small additional current supplied through the THRESHOID control switches D25 to its high state. This sends a positive pulse to T65 through C60 and R60. The other end of the drive winding of

T65 is connected to +19 volts through C61, R61, R47, R48, R49, and through R19 and the POLARITY switch. The connection through POLARITY switch SWIOB locks out positive triggerrecognition circuit D45 and D55.

The pulse from D25, through the drive winding of regenerator transformer $T 65$, causes enough additional current to flow in the circuit of D65 to switch D65 to its high state. After the pulse, D65 switches back to its low state. The regenerated output is taken from D65 through C65 and used to trigger the fast-ramp circuit. A negative gate signal is supplied by Q73 and D72 for use by the Type 661 Delayed Pulse generator. This gate circuit is driven by a separate winding on T65. D72 starts the delayed pulse and 073 ends it.

The positive pulse at D25 is also fed to the emitter of holdoff driver Q104, starting operation of the holdoff circuit. The holdoff assures that the sampling cycle does not repeat before the system is prepared to take another sample. The circuit will not retrigger until D35 is turned to the high state and Q84 and Q94 are turned off. Under the freerunning conditions described, D25 will retrigger immediately after D35 switches to its high state, which occurs after Q84 and 0.94 are turned off.

With normal trigger operation, D25 will not have sufficient bias to switch to its high state until a trigger signal is received. THRESHOLD control R16 determines the signal level needed to trigger D25 to its high state. Trigger signals are fed either from the external or the internal trigger inputs, depending on the setting of SOURCE switch SWIOA.

Operation of the positive trigger-recognition circuit is similar to that of the negative circuit. D45 is the recognition diode, and D55 is the recovery diode. The negative trigger-recognition circuit is locked out by -19 volts through POLARITY switch SWIOA, and R17. The holdoff circuit is driven when D45 switches to the high state and sends a signal to the base of 0104. D55 is switched to the low state by the collector of Q84. D45 and D55 are connected opposite in polarity to D25 and D35. Note that the negative trigger-recognition circuit actually operates on positivegoing signals, and the positive trigger-recognition circuit operates on negative-going signals. This is because trigger signals provided to the Type 5T1A are inverted before being fed to the trigger-recognition circuits.

Operation of the trigger-recognition circuits in FREE RUN is similar to the operation described previously. The input is driven by either +19 volts, in the - POLARITY, or -19 volts in the + POLARITY position.

## Holdoff

The holdoff circuit prevents the trigger-recognition circuit from operating after a trigger has been received and recognized until the remainder of the system is ready to take a new sample. The holdoff period is required to allow the fast ramp to run for a time equivalent to 10 cm of display; then reset, or to limit the system repetition rate to 100 kc , whichever time is longer. The holdoff period is variable; 1.3:1 from the MAX. to the MIN. position of the front-panel RECOVERY TIME control. This may be adjusted to
aid stable triggering if the triggering input frequency and the holdoff repetition rate are equal.

The holdoff circuit consists of two bistable multivibrators and a Miller integrator. Each bistable multivibrator drives a transistor which shunts supply current from one pair of the trigger-recognition circuit tunnel diodes. The output of the Miller integrator is also fed to a gate which switches both multivibrators. Recognition tunnel-diode multivibrator Q115-Q125 drives Q94. Recovery-diode multivibrator Q165-Q175 drives Q84. Miller integrator Q144 drives Q154 and gate D144. Tunnel diodes D25 and D45 are the recognition diodes, and D35 and D55 are the recovery diodes. Q104 drives the holdoff circuit.

When a trigger signal is received and recognized (assume the same conditions as for the trigger-recognition circuit discussion), D25 switches to the high state. This causes the emitter of Q104 to go positive, forward biasing the transistor. The collector voltage of Q104 rises, forward biasing Q115. The collector of Q115 drops, turning Q125 off. The same collector voltage drop at Q115 causes D92 to become forward biased, shunting the current source for D25 and causing D25 to return to its low state.

When Q125 turns off, its collector voltage rises, and current is supplied through R132 and RECOVERY TIME control R136, forward biasing Q144. This causes a voltage drop at the collector of 0144 which was clamped by Q154 at +19 volts. The collector drop of Q144 is fed back to its base through C145 and C146, preventing any large voltage swing at the base of Q144. Thus, the current through R132 and R136 that is charging C145 and C146 remains essentially constant. The
value of C145 determines the rate of voltage fall at the collector of Q144, and is selected by the SWEEP TIME/CM switch for the desired holdoff time. As soon as the collector voltage of Q144 begins to fall, Q154 becomes back-biased, and its collector voltage drops to ground.

When the collector of Q144 reaches ground, D144 is forward biased which lowers the base voltage of 2165 , turning it off and raising its collector voltage. C166 and R166 couple this collector voltage rise to Q175, turning it on. The collector of Q175 drops, forward biasing D82 and Q84. When Q84 is turned on, it shunts the current source for D35, returning D35 to the low state.

The collector voltage rise at Q165 is also coupled through D164, C164, and R164, to the base circuit of Q125, turning Q125 on. The collector voltage of Q125 drops, and this drop, coupled through C126 and R126, turns Q115 off. The collector voltage of Q115 rises, back biasing D92 and Q94, and restoring the current source to D25. Note, however, that D35 is in the low state, and that no current is available to D25 through R35. Thus, D25 remains in the low state, and cannot be triggered yet.

When Q125 is turned on, its collector voltage drops, and C145 and C146 discharge through R132 and R136. The voltage falls at the base of Q144 which decreases the collector current, causing the collector voltage to rise. This rise is fed back through C145 and C146, and the collector voltage of Q144 runs back up at a rate proportional to the total capacitance of C145 and C146. When the collector voltage of Q144 reaches +19 volts, Q154 becomes forward
biased. This clamps the collector voltage of Q144 at +19 volts. When Q154 becomes forward biased, its collector voltage rises, forward biasing Q165. The collector voltage of Q165 drops, and this drop, coupled through C166 and R166, turns Q175 off. The collector voltage clamps the base of Q144, through D146, from going below the collector voltage of Q165. D164 is back biased, preventing the drop at the collector of Q165 from operating multivibrator Q115-Q125.

The collector voltage rise of Q175 back biases D82, and turns Q84 off. This restores the operating current to D35, and D35 immediately switches to the high state. With D35 in the high state, D25 receives additional current through R33, and is ready to be retriggered to initiate a new sampling cycle.

## Fast Ramp

The fast-ramp circuit consists of a comparison-voltage amplifier, a ramp generator, and a pulse-forming comparator. The output of the ramp generator is a voltage fall with a con stant calibrated slope used as an internal time base. The comparison voltage is received either from the staircase generator or externally through the Type 661. In the manual scan mode, the comparison voltage is supplied by the Type 661. For this discussion, assume that the Type 661 HORIZONTAL DISPLAY control is in the $X 1$ position unless otherwise stated.

The comparison and fast-ramp voltages are fed to the pulse-forming comparator. When the two voltages are just equal, the comparator circuit generates a pulse used to
drive the sampler in the '4' Series sampling unit. A pulse from the comparator circuit also drives the staircase generator, causing it to advance one step. The fast-ramp circuit operates each time a trigger output signal is fed to it from the trigger circuit. As the staircase voltage advances, step by step, the fast-ramp voltage must become greater, and thus will run a little longer with each succeeding run-down before the comparator circuit generates a pulse. The fast-ramp voltage represents the real time on which the system reconstructs the signal.

Ramp Generator
Q261 is a constant-current supply. Before a trigger signal is received from the trigger circuit, D255 is in the high state and holds Q254 on. Current from Q261 passes through Q254 and holds C260 near ground voltage. D255 is held in the high state by current through R244. Current through R244 also provides base current for Q254, and Q254 conducts the current supplied by 0,261 .

Q261 receives a constant base voltage from the -19-volt supply through decoupling filter R260 and C260. Q261 emitter current, which comes from the -100 -volt supply, passes through R265 and R267 which drop about 81 volts. This determines the current through Q261. Current supplied by the transistor is determined by emitter current, and is little affected by any change in collector voltage.

The trigger cirait sends a positive pulse which causes Q244 to conduct more current. The collector voltage of 0244 rises to ground, and switches D255 to its low state, turning

Q254 off. After the trigger pulse passes, 0254 remains cut off, held by D255 which remains in the low state. 0261 collector current now flows through ramp-slope capacitor C260, whose value is selected by SWEEP TIME/CM switch SW260. Before the beginning of the fast-ramp rundown, comparator diode D270 is back biased, and all current from Q261 is fed to c260. The ramp voltage runs down until D270 becomes forward biased. Collector current from Q261 is now fed through D270 and Q276, and the collector voltage of Q276 drops. D275 switches to the high state.

Before D275 switches, the voltage on either side of D276 is about zero volts. When the current from Q261 passes through Q276, it causes a step at D275, quickly switching D275 to the high state. Because D276 was not conducting, it appears as an open circuit as D275 switches.

When D275 switches, D276 becomes back biased. Because it is a tunnel diode, D276 conducts current easily, coupling the step caused by the switching of D275 to D285. This causes D285 to switch. When D285 switches, a step is fed to T284, which is a doubling transformer. The output of T284 forward biases Q284, causing the collector voltage of Q284 to rise. This gate, which appears at the collector of Q284, is connected directly through interconnecting cables to the '4' Series sampling unit. The gate is also sent, through isolation resistance network R285, R286, and R287, to the stairstep generator, where it is used to advance the stairstep one step. When the current through T284 (fed from R288 and R289) rises, D285 is switched back to the low state.

The fast ramp is reset by the comparator pulse. When D275 changes to the high state, D256 conducts, and changes D255 to the high state. 0254 now conducts the current supplied by Q261 and discharges C260. RAMP RECOVERY control R254 sets the maximum current through 0254 to a safe value commensurate with speedy ramp recovery.

Because the fast ramp is triggered by the incoming signal (or in a fixed time relationship to it), the instant, in real time, when the comparator pulse is sent to the sampling unit is determined by the comparison voltage. This determines the time the fast ramp must take to run down before the comparator pulse is sent to the sampling unit.

The rate of fall of the fast-ramp voltage, except the $1 \mathrm{nsec} / \mathrm{cm}$ rate, is determined by C260. Five capacitors allow five rates of fall or ramp slope (in volts/ $\mu \mathrm{sec}$ ) over the range above $1 \mathrm{nsec} / \mathrm{cm}$. The $1 \mathrm{nsec} / \mathrm{cm}$ sweep rate is set by $C 263$ and circuit stray capacitance. With C260 disconnected, c263 remains in the collector circuit of 0261 at all sweep rates, but is a small fraction of the circuit capacitance in sweep rates slower than $1 \mathrm{nsec} / \mathrm{cm}$.

The effective portion of the fast-ramp voltage used is determined by the range of comparison voltage fed to the base of comparator transistor Q276. In the $.1 \mu$ SEC position of the SWEEP TIME/CM switch, the effective ramp length is 10 volts; in the 50 nSEC position, 5 volts; and in the 20 nSEC position, 2 volts. (These voltages are true with the TIME EXPANDER switch in X1.) In each of these three positions, the slope of the ramp voltage is the same.

The voltage fed to comparator transistor Q276 is determined by the current fed to the operational amplifier preceding it; Q223 and Q234. Because Q223 is an emitter follower, the amplifier is current driven. Because Q234 is collector loaded, the output is a voltage output. Feedback resistor R231 determines the characteristics of the amplifier. There are three sources of current for Q223; from DELAY ZERO control R220 fed through R223 (this is a calibration adjustment); from the TTME POSITION control circuit, and from the Type 661 HORIZONTAL DISPIAY switch. When the HORIZONTAL DISPLAY switch is in any of the SWEEP MAGNIFIER switch positions, the staircase voltage is fed to the comparator circuit through two attenuator networks. One network, R214 and R215, always looks like a constant impedance at the input to the attenua. tor, but divides the current fed to Q223. Table 3-1 lists the positions of the SWEEP TIME/CM switch and the current attenuation introduced in each position. The SWEEP TTME/CM switch controls the values of R214 and R215. Table 3-1 also lists the resulting comparison voltage output equal to 10 cm of horizontal deflection. This voltage is seen at the base of 2276 .

A second attenuator, R208 and R209, may be cascaded ahead of R214 and R215. R208 and R209 are controlled by the TIME EXPANDER switch, and are used to introduce further current division, above that introduced by R214 and R215. When R208 and R209 are switched into the circuit, the input continues to look like a constant impedance, and the current source for the comparator circuit is subjected only to a constant load impedance regardless of the settings of the

SWEEP TIME/CM and TIME EXPANDER switches.

The range of the TIME POSITION control depends on both the SWEEP TIME/CM and the TIME EXPANDER switch settings. This control is a variable current supply, and its range of operation (in time) depends on the voltage shift it can impose on the comparison voltage. Table 3-1 shows the voltages of the fast-ramp duration in SWEEP TIME/CM switch settings. Table $1-1$ shows the range of the TIME POSITION control in time according to SWEEP TIME/CM and TIME EXPANDER switch settings. The voltage ranges over which the TIME EXPANDER control can shift the comparison voltage limits are as follows: (a) A11 SWEEP TIME/CM switch settings slower than $10 \mathrm{nsec} / \mathrm{cm}$, and TTME EXPANDER switch at XI: 1 volt.
(b) $10 \mathrm{nsec} / \mathrm{cm}$ through $1 \mathrm{nsec} / \mathrm{cm}$ sweep rates and TIME EXPANDER switch at $X 1: 5$ volts.
(c) All SWEEP TIME/CM switch settings and TIME EXPANDER switch at $\times 2: 5$ volts.
(d) All SWEEP TTME/CM switch settings and TIME EXPANDER switch at $\times 5, \times 10, \times 20, \times 50$, or $\times 100: 10$ volts.

The voltage at the base of Q223 is controlled by INVERTER INPUT ZERO control R225. This control is set so that the base of $Q 223$ is at zero volts dc, allowing proper operation of the current sources feeding Q223.

Staircase Generator
With the Type 661 HORIZONTAL DISPLAY switch in the SWEEP MAGNIFIER positions, the staircase generator provides a staircase voltage for the comparison circuit of the fast ramp. The staircase generator is triggered by the fast-ramp

TABLE 3-1
SWEEP TIME/CM Switch

| SWEEP TTME/CM Switch Setting | Fast Ramp Slope | Attenuator Ratio | Duration of Fast Ramp Voltage $=10 \mathrm{~cm}$ Sweep |
| :---: | :---: | :---: | :---: |
| $\begin{array}{r} 100 \mu \mathrm{SEC} \\ 50 \mu \mathrm{SEC} \\ 20 \mu \mathrm{SEC} \\ \hline \end{array}$ | $\begin{aligned} & 0.01 \\ & \text { volt/ } \\ & \mu \mathrm{sec} \end{aligned}$ | $\begin{aligned} & x 1 \\ & \times 2 \\ & \times 5 \\ & \hline \end{aligned}$ | $\begin{array}{r} 10 \text { volts } \\ 5 \text { volts } \\ 2 \text { volts } \end{array}$ |
| $\begin{array}{r} 100 \mu \mathrm{SEC} \\ 5 \mu \mathrm{SEC} \\ 2 \mu \mathrm{SEC} \\ \hline \end{array}$ | 0.1 volt/ $\mu \mathrm{sec}$ | $\begin{aligned} & x 1 \\ & \times 2 \\ & \times 5 \\ & \hline \end{aligned}$ | $\begin{array}{r} 10 \text { volts } \\ 5 \text { volts } \\ 2 \text { volts } \end{array}$ |
| $\begin{array}{r} 1 \mu \mathrm{SEC} \\ .5 \mu \mathrm{SEC} \\ .2 \mu \mathrm{SEC} \\ \hline \end{array}$ | 1.0 volt/ $\mu \mathrm{sec}$ | $\begin{aligned} & x 1 \\ & x 2 \\ & \times 5 \\ & \hline \end{aligned}$ | $\begin{array}{r} 10 \text { volts } \\ 5 \text { volts } \\ 2 \text { volts } \end{array}$ |
| . $1 \mu \mathrm{SEC}$ <br> 50 nSEC <br> 20 nSEC | 10 volts/ $\mu \mathrm{sec}$ | $\begin{aligned} & x 1 \\ & x 2 \\ & x 5 \\ & \hline \end{aligned}$ | $\begin{array}{r} 10 \text { volts } \\ 5 \text { volts } \\ 2 \text { volts } \\ \hline \end{array}$ |
| $\begin{array}{r} 10 \mathrm{nSEC} \\ 5 \mathrm{nSEC} \\ 2 \mathrm{nSEC} \\ \hline \end{array}$ | 50 volts/ $\mu \mathrm{sec}$ | $\begin{aligned} & x 2 \\ & x 4 \\ & \times 10 \\ & \hline \end{aligned}$ | $\begin{gathered} 5 \text { volts } \\ 2.5 \text { volts } \\ 1 \text { volt } \end{gathered}$ |
| 1 nSEC | 500 volts/ $\mu \mathrm{sec}$ | X2 | 5 volts |

comparator pulse, and steps one step for each comparison pulse fed to it. The voltage increment of each step is determined by the SAMPLES/CM switch. When the staircase has stepped over a voltage equivalent to the sweep length, a reset circuit returns the staircase voltage and a new trace begins. In the TIMED position of the SAMPIES/CM switch, the staircase generator is allowed to run up linearly in a smooth runup. A single-sweep lockout circuit may be selected by SWEEP MODE switch SW325. A single sweep is obtained by preventing the staircase from starting until the SWEEP MODE switch is set to START. The staircase will then step through
one display cycle, return, and be locked out until the SWEEP MODE switch is set to START again.

The staircase circuit includes gate circuit Q335-Q345, single display lockout D325-Q324, blocking oscillator Q300, and step integrator V361-V373.

Assume that the gating circuit is allowing a staircase voltage run, and that the SWEEP MODE switch is in NORMAL with Q335 and Q345 conducting. Note that Q335 is a PNP transistor, and that Q345 is NPN. The circuit operates with both transistors turned on or turned off simultaneously. The collector circuit of each transistor is connected to the base of the other, and the circuit has two stable states. Its operation will be discussed later. With both Q335 and Q345 conducting, disconnect diodes D352 and D353 are back biased, allowing staircase capacitor $C 360$ to be charged by the staircase step integrator as pulses arrive from the blocking oscillator.

A pulse from the fast-ramp comparator passes through $C 30$ into the blocking oscillator circuit. The pulse sends current through the collector winding of T300. The trigger current induces a current in the base winding of T 300 which turns on blocking oscillator transistor Q300. Normal blocking oscillator saturation follows. D306 completes the basewinding circuit of T 300 . The negative emittex-output signal of Q300 is fed through C358 (SAMPLES/CM switch SW358) to the step integrator. The amplitude of the pulse fed to 0358 is controlled by R3O4, the internal SAMPLES/CM control.

Saturation occurs, and the blocking oscillator starts its backswing. D300 becomes forward biased and current
pesses through D300 instead of the collector winding of $T 300$. The negative pulse passed through $C 358$ back biases D361, and forward biases D360. The pulse energy is fed directly to C360 and the grid of V361. V361 and associated circuit is a Miller integrator. The pulse energy starts to charge C360, and lowers the grid voltage of V361 which allows plate voltage to rise. This rise is coupled to the grid of cathode follower V373B. The cathode of V373B is coupled to C360 via C378 and D378. The rise of V373B cathode voltage raises the voltage to 6360 . The result is that the voltage of the V361 grid side of 6360 remains nearly constant. The amount of charge given $C 360$ is proportional to the capacitance of C358, which is controlled by SAMPLES/CM switch SW358. In the TIMED position of the SAMPLES/CM switch, current through R355 and R356 causes C360 to charge in a linear ramp. C360 is paralleled by C361 in the SAMPLES/CM switch 1000 and TIMED positions, decreasing the staircase (or ramp) voltage slope for a given amount of charge fed through C358.

A positive feedback loop keeps the plate current of V361 constant over the output range to improve linearity and response time. The cathode voltage of $V 373 B$ is fed through Zener diode D377 and C377 to the grid of V373A. As C360 charges, the grid voltage of V373A rises. The cathode of V373A follows the grid and keeps the current through R371 and V361 essentially constant.

The staircase voltage at the cathode of V373B is fed through a resistance divider to pin 22 of P 4 and to the Type 661 HORIZONTAL DISPLAY switch. The voltage at pin 24 of P 4 runs from about 0 to 50 volts. Dc level of the output is
set by DC LEVEL control R381. This voltage is fed back to the comparator of the Type 5 TlA as a comparison voltage when the Type 661 HORIZONTAL DISPLAY switch is in any of the SWEEP MAGNIFIER positions.

Staircase Gating Circuit
The unattenuated output signal is fed from C360 to the gating circuit. This signal passes through R346, D345, R345, and R344 to the base circuit of Q335. As the staircase voltage rises, the base of $Q 335$ is moved toward cutoff. SWP LENGIH control R345 determines the amount of signal sent to Q335. When the base current approaches about 0.1 ma , the transistor turns off, and its collector voltage falls from 0 to -18 volts. This fall is coupled through R332 and C332 to the base of 0345 where the voltage drops from -18 to -20 volts. $Q 345$ turns off, and its collector voltage raises from -18 to 0 volts. The grid of $V 361$ is at about -0.9 volts, and D353 becomes forward biased. This raises the grid voltage of V361, since a current path is established through D353 to the +19 -volt supply. The step integrator circuit now runs down and discharges C360 until D352 becomes forward biased, and state of clamped equilibrium exists. When the Miller step-integrator circuit has discharged C360, D345 becomes back biased, and a current path no longer exists between the integrator circuit and the base of Q335. This prevents the staircase voltage from turning $Q 335$ and $Q 345$ back on.

The pulses from the blocking-oscillator circuit are fed through Q324 to switch the gate back on to start the next staircase output. C303 transmits each negative pulse through

R324 to D325 and the emitter of Q324. Each pulse switches D325 to the high state and forward biases Q324, which causes the emitter of 2324 to fall fram 6.3 volts to zero. At the end of each blocking oscillator pulse, D325 switches back to the low state, and Q324 turns off. The negative pulse at the collector of Q324 is transmitted through C322 and R336 to the base of Q335. The first pulse received after D345 becomes back biased and C345 has discharged allows Q335 to conduct, raising its collector to ground, and allowing $Q 345$ to conduct. C345 is paralleled by C346 in the SAMPLES/CM switch TIMED and 1000 positions which lengthens the holdoff time before Q335 can be turned back on. The collector of Q345 drops back to about -18 volts, back biasing D352 and D353, and the step integrator is free to mun up again until the feedback path from the integrator to the base of Q335 stops the run-up.

Blanking mixer $Q 314$ is driven by the gate circuit, and by the blocking oscillator to provide blanking signals to the Type 661. When the gate is in the off state (neither Q335 or Q345 conducting), Q314 is turned on through R331. When the gate is in the on state, (staircase run-up permitted) the collector voltage of Q335 turns off Q314 and permits each pulse from the blocking oscillator to turn on Q314 for the duration of the pulse. The collector circuit of Q314 is completed in the Type 661. Whenever Q314 is forward biased, collector current flows, and crt blanking occurs. Thus, the crt beam is off whenever deflection is occurring.

A single sweep is obtained by moving SWEEP MODE switch SW325 to the SINGIE SWEEP position. R325 is connected, by

SW325, to the -19-volt supply, and holds D325 in the high state. With D325 held in the high state, Q324 remains in conduction, and the negative pulse necessary to switch the gate transistors back into conduction is blocked. This locks the staircase at zero output. When the SWEEP MODE switch is moved to the START position, the junction of R310 and C310, which was at -19 volts, is grounded. $C 310$ sends a positive pulse through R312 and R315 to D325, causing it to switch back to the low state momentarily, turning Q324 off. D325 switches back to the high state with the next pulse from blocking oscillator Q335, and allows the staircase generator to generate one display. At the end of the single sweep, Q335 is turned back off in the normal manner, and the SWEEP MODE switch must be set to START to obtain the next staircase output.

SECTION 4
CALIBRATION
General
The Type 5T1A is a stable instrument, and should operate properly with a minimum of care. The instrument should be recalibrated at least once every 6 months or 500 hours of operation, whichever comes first. For best results, the steps in this calibration procedure should be followed in the order they appear.

Tunnel diodes used in the Type 5T1A should not be handled unless necessary. Do not connect probes directly to tunneldiode bodies. When tunnel diodes are marked with a color code, it will appear on the anode side. The cathode side has a small external disc. Locations of internal controls and tunnel diodes are shown in Figure 4-1.

Preset internal controls to midrange only if the type 5 T1A has undergone repairs, or is known to be seriously out of calibration.

## Equipment Required

1. Tektronix Type 661 Oscilloscope.
2. Tektronix '4' Series sampling unit.
3. Volt-ohm-milliammeter, dc resistance 5000 ohms/volt, or better.
4. Time-mark generator, Tektronix Type 180A, or equivalent.
5. Test oscilloscope, dc to 15 -mc bandpass, sensitivity capable of displaying 400-mv signal, Tektronix Type 531A with Type K Plug-In Unit or equivalent.


Fig. 4-1. Type 5T1A internal adjustment locations.
6. $30-\mathrm{cm}$ air line, General Radio part number 874 L 30 , or equivalent.
7. Pulse generator, Tektronix Iype 111, or equivalent.

## Procedure

1. Check Resistance to Ground at Power Plug

With common lead of test meter grounded, the follow-
ing resistances are typical: (This check necessary only after repair.)

| Pin | Power Supply <br> Voltage | Ohms |
| ---: | :---: | :---: |
|  | 300 | 40 k |
| 17 | 100 | 80 k |
| 5 | -100 | 10 k |
| 3 | -19 | $150 \Omega$ |
| 18 | 10 | $10 \Omega$ |

2. Preset Front-Panel Controls

Install plug-in units in Type 661 Oscilloscope.
Turn on power and set front-panel controls as
follows:
5T1A

| SWEEP TIME/CM | 10 nSEC |
| :--- | :--- |
| VARIABLE | CALIBRATED |
| SWEEP MODE | NORMAL |
| TIME POSITION | Clockwise |
| SOURCE | EXT. |
| POLARITY | NEG. |
| RECOVERY TTME | MIN. |

661

HORIZONTAL DISPLAY
AMPLITUDE/TTME CALIBRATOR
HORIZONTAL POSITION

F MANUAL SCAN
OFF
Centered

Sampling Unit

| Dc Offset | Zero Volts |
| :--- | :--- |
| Mv/Cm | 200 |
| Vertical Position | Centered |
|  | Test Oscilloscope |

3. 0 Threshold

Connect the de voltmeter between the center terminal of the THRESHOLD control (potentiometer nearest the front panel) and ground. Adjust THRESHOLD control for zero volts on the meter. The dot on the control knob should be aligned with the 0 on the front panel; if not, loosen and reposition the knob.
4. - Threshold

Connect the test oscilloscope probe to the junction of L25 and the anode of D25. Set -TRIG. RECOVERY T.D. BIAS R35 fully clockwise, and adjust -TRIG. RECOG. T.D. BIAS R25 for a stable display.
5. + Threshold

Connect the test oscilloscope probe to the junction of 145 and the anode of D45. Set +TRIG. RECOVERY T.D. BIAS R55 fully clockwise, and adjust +TRIG. RECOG. T.D. BIAS 845 for a stable display.
6. Output Tunnel-Diode Bias

Connect the test oscilloscope probe to the junction of C65 and the anode of D65. Adjust OUIPUT T.D. BIAS R65 for a stable display. The display should be about a $+0.4-$ volt, $0.3-\mu \mathrm{sec}$ pulse, and should disappear when the THRESHOLD control is turned fully clockwise.

## 7. Ramp Recovery

Connect the test oscilloscope probe to the junction of Q244 collector and D255 cathode. Adjust R254 for a stable +0.4-volt, $50-$ nsec pulse. You may have to adjust COMPARATOR LEVEL R275 for a stable display. All values are approximate.
8. Comparator Level

Connect the test oscilloscope probe to the collector of Q284. Adjust COMPARATOR LEVEL R275 for a stable +5.5 -to +6 -volt pulse, about 750 nsec wide at the top. This is the fast-ramp pulse to the sampling unit. A similar pulse (3v) should appear at the opposite end of R285 (560 $\Omega$ resistor). Set Type 661 HORIZONTAL DISPLAY switch to $\chi 1$; a sweep should appear on the crt. Remove test probe.

This is a preliminary adjustment. If the sweep is not on the crt, check the staircase generator circuit for proper operation.
9. Threshold Sensitivity

With a trace on the crt, aisiust -TRIG. RECOG. T.D. BIAS R25 so that the sweep free-runs as near the 0 position as possible when the THRESHOLD control is turned clockwise. Adjust -TRIG. RECOVERY T.D. BIAS R35 so that the sweep stops within $5^{\circ}$ to the right LEFT T of the 0 position.

With a trace on the crt, adjust +TRIG. RECOG. T.D. BIAS R45 so that the sweep free-runs as near the 0 position as possible when the THRESHOLD control is
turned counterclockwise. Adjust +TRIG. RECOVERY
T.D. BIAS R55 so that the sweep stops within $5^{\circ}$ to RT3t?
the loft of the 0 position.
10. Lockout Time

Apply a $0.1-\mu \mathrm{sec} / \mathrm{cyc} 1 \mathrm{e}, 100-\mathrm{mv}$ signal from the Type 661 Amplitude/Time Calibrator to the Type 5T1A EXTIERNAL TRIGGER INPUT connector. Adjust the THRESHOLD control to trigger the Type 5T1A. Touch the test oscilloscope probe to the junction of C65 and the anode of $D 65$, and adjust $C 146 B$ for 9.5 to 10 $\mu \mathrm{sec}$ between pulses.
11. Delayed-Pulse Generator Bias

Connect the test oscilloscope probe to the emitter of Q73. Adjust DELAYED PULSE GEN. BIAS R990 (located on the right side of the Type 661) until a -0.4-to -0.5-volt pulse appears on the crt. Repetition rate should be the same as that of output tunnel diode D65. This adjustment may require resetting OUIPUT T.D. BIAS R65 to maintain the stability of D65. Connect a cable from the Type 661 DELAYED PULSE $50 \Omega$ connector to the vertical input connector. The pulse at $Q 73$ should be stable when connecting and disconnecting cable.
12. Sweep Length

Adjust SWP LENGTH R345 for a $10.5-\mathrm{cm}$ sweep length. Connect the test oscilloscope probe to the center terminal of the VARIABLE SWEEP TTME/CM control (potentiometer at rear of SWEEP TIME/CM switch wafer). A $52.5 \pm 1$ volt, peak ac, staircase voltage
should appear on the crt.
13. Sweep Rate

Set the SWEEP TTME/CM switch to $1 \mu$ SEC, and apply 1$\mu s e c$ markers from the time-mark generator. Adjust SWEEP CAL R267 for 1 mark/cm between lat and 9th major graticule divisions. Timing should be within $2 \%$ on all ranges from $20 \mathrm{nsec} / \mathrm{cm}$ to $100 \mu \mathrm{sec} / \mathrm{cm}$. Check to see that the VARIABLE SWEEP TIME/CM control provides a $3: 1$ sweep-timing range.
14. Check Tlme Expander

With the SWEEP TIME/CM switch set to $1 \mu \mathrm{sec}$, check all ranges of the TIME EXPANDER switch with the TIME POSITION control at midrange. Locate the proper midrange point by setting the TIME POSITION control fully counterclockwise, and then turning clockwise to midrange. Also, recheck with $1-\mu s e c ~ t i m e ~ m a r k s ~$
in the $\mathrm{X1}$ position. Accuracy must be $\pm 1.5 \%$ between lst and 9th major graticule divisions.
15. Sweep Delay and Registration

Preset controls as follows:
5T1A

| DC LEVEL (R381) | Counterclockwise |
| :--- | :--- |
| DELAY ZERO (R220) | Clockwise |
| SAMPLES/CM | 100 |
| TRIGGERING | INT + |
| SWEEP TIME/CM | $2 \mu S E C$ |
| TIME EXPANDER | XI |
| TIME POSIIION | Clockwise |

661
AMPLITUDE/TIME CALIBRATOR
$1000 \mathrm{mv}, 1 \mu \mathrm{sec} / \mathrm{cyc} \mathrm{le}$
SWEFP MAGNIFIER

Connect output of Type 661 Amplitude/Time Calibrator to the sampling unit. Display a sinewave by adjusting THRESHOID, RECOVERY TIME, COMPARATOR LEVEL R275, and Type 661 POSITION controls.

Adjust R275 and R254 for best corner transition-tosine curve. Dots should be continuous. Connect the test oscilloscope probe to the base of Q223, with test oscilloscope set for $50 \mathrm{mv} / \mathrm{cm}$, de coupled. Adjust the test oscilloscope for a 0 -volt de reference level. Adjust R225, for 0 volt dc (same as reference level). Turn SWEEP TIME/CM switch to the 2, 1, and . $5 \mu \mathrm{SEC}$ positions. Adjust DELAY ZERO R220 so that the sinewave starts at the same place on the crt at each position of the SWEEP TTME/CM switch. Set the SWEEP TTME/CM switch to $1 \mu$ SEC. Adjust DC LEVEL R381 to remove the straight line of dots preceding the start of the sinewave. Disregard any dots that may appear at other de levels.

Apply a 2-nsec pulse from the pulse generator to the sampling unit. Pretrigger the Type 5T1A from the pulse-generator pretrigger output through the EXTERNAL TRIGGER INPUT connector. Set the SWEEP TIME/CM switch to 1 nSEC, and locate the pulse-generator output on the second major vertical graticule division where it crosses the horizontal centerline. Insert the $30-\mathrm{cm}$ air line in the signal connection to the sampling unit, and adjust $C 263$ so that the pulse now lies on the third major vertical graticule
division where it crosses the horizontal centerline. Remove the air line and reposition the pulse (with the Type 661 positioning controls) so that it again crosses the second major vertical graticule division. Recheck the adjustment by reinserting the air line. Repeat this procedure until inserting the $30-\mathrm{cm}$ air line causes a 1-cm signal delay.

Apply a 50-mc signal from the timemark generator to the sampling unit. Set the SWEEP TIME/CM switch to 10 nSEC and adjust C260F for 1 cycle $/ 2 \mathrm{~cm}$. Apply a 20-to 30 -nsec pulse from the pulse generator to the sampling unit. The pulse should remain on the crt through all the SWEEP TTME/CM switch positions from 2 nSEC to $2 \mu \mathrm{SEC}$. Use the TTME EXPANDER switch to increase resolution, and make it easier to locate the pulse on the slower sweep rates. Make the final adjustment of DELAY ZERO R22O to position the pulse at the same starting point as when the TIME POSITION control is set fully clockwise.

## 16. Sweep Timing

Apply a 50-mc sinewave from the time-mark generator to the sampling unit. Set the SWEEP TIME/CM switch to 10 nSEC and adjust C260F for 1 cycle $/ 2 \mathrm{~cm}$.
17. Time Position

Apply a $10-m e$ sinewave from the time-mark generator to the sampling unit. Set the SWEEP TIME/CM switch to 10 nSEC . Set the TIME POSITION control fully clockwise, and the TIME EXPANDER witch to Xl. Turn
the TTIME POSITION control fully counterclockwise.
Check delay range according to the following table:

| SWEEP TIME/CM | Input | TIME EXPANDER <br> Switch Setting | Frequency | Switch Setting |
| :--- | :---: | :---: | :---: | :---: |


| 10 nSEC | 10 mc | $\chi 1$ | greater than 100 nsec |
| ---: | ---: | ---: | :--- |
| 10 nSEC | 10 mc | $\chi 2$ | greater than 100 nsec |
| 10 nSEC | 10 mc | $\chi 5$ | greater than 200 nsec |
| 100 nSEC | 10 mc | x 1 | greater than 100 nsec |
| 100 nSEC | 10 mc | $\chi 2$ | greater than 500 nsec |
| 100 nSEC | 1 mc | $\chi 5$ | greater than 1000 nsec |

18. Samples/Cm

Set the SOURCE switch to FREE RUN, SAMPLES/CM switch to 5, SWEEP TTME/CM switch to $1 \mu \mathrm{SEC}$, and Type 661 HORIZONTAL DISPLAY switch to XI. Adjust SAMPLES/CM R304 for 5 dots/cm; l dot exactly at each minor division between the 1 st and 9 th major graticule divisions. Linearity must be $\pm 0.5 \mathrm{~mm}$.

Apply a $350-\mathrm{mv}$ pulse from the pulse generator to the sampling unit. Adjust the SOURCE switch and THRESHOLD control to trigger the Type 5T1A. Adjust the pulse-generator repetition rate for 100 kc with the RECOVERY TIME control at MIN. Change the pulsegenerator repetition rate to 50 cps . The samples (dots)/cm should not change more than $\pm 1 \%$. Return SOURCE switch to FREE RUN. Make the following preliminary adjustments for the samples (dots)/cm:

Type 661
HORIZONTAL DISPLAY
Switch Setting

| $\times 10$ | 10 | $C 358 D$ | 1 |
| ---: | ---: | ---: | ---: |
| $\times 20$ | 20 | $C 358 F$ | 1 |
| $\times 50$ | 50 | $C 358 \mathrm{H}$ | 1 |
| $\times 100$ | 100 | $C 358 \mathrm{~K}$ | 1 |

Set the SAMPIES/CM switch to 5, Type 661 HORIZONIAL DISPLAY switch to $X 1$, end SWEEP TITME/CM switch to 20 nSEC. Apply a 5-mc sinewave from the time-mark generator to the sampling unit. Adjust the THRESHOLD control to trigger the Type 5T1A for a good sinewave display. Then set the SWEEP TIME/CM switch to $1 \mu S E C$. A single row of dots should appear on the crt. Now set the time-mark generator for $1-\mu \mathrm{sec}$ markers. With the TIME POSITION control near its fully counterclockwise position, adjust SAMPIES/CM R304 and SWEEP CAL. R267 for a single level row of dots on the rise of $1-\mu s e c$ markers (use TIME POSITION control). A dot should occur at exactly the 2nd and loth major graticule divisions in a nearly level line across the crt. Set the timemmark generator for $50-\mathrm{mc}$ sinewaves, and use the following table for the final samples/cm adjustments. Adjust for straightest possible line, or better than table.

| SAMPLES/CM <br> Switch Setting | Adjust Rows of Dots | Maximum Number of <br> Cycles or Crossovers |  |
| :---: | :---: | :---: | :---: |
| 10 | C358D | 1 | 2.5 cycles |
| 20 | C358F | 2 | 5 crossovers |
| 50 | C358H | 1 | 2.5 cycles |
| 100 | $C 358 \mathrm{~K}$ | 2 | 5 crossovers |

19. Times Mode

Set the SAMPIES/CM switch to TTMED. Set R357 (front panel) fully clockwise. Set the SOURCE switch to FREE RUN. Set the time-mark generator for 1-sec marks. Fewer than ten marks should occur between
each two major graticule divisions (sweep rate
faster than $5 \mathrm{sec} / \mathrm{cm}$ ). Set R357 fully counterclock-
wise; sweep should stop.
20. Single Display

Turn the SWEEP MODE switch from SINGIE DISPIAY to
START; only one sweep should occur.

## SECTION 5

## PARTS LIST AND SCHEMATICS

ELECTRICAL PARTS
Values are fixed unless marked Variable.

| Ckt. No. | Tektronix <br> Part Number |  |
| :--- | :--- | ---: |
| B319 | BULBS |  |
|  | 150-002 | Neon, NE-2 |
|  |  | CAPACITORS |

Tolerance $\pm 20 \%$ unless otherwise indicated. Tolerance of all electrolytic capacitors are as follows (with exceptions):

$$
\begin{aligned}
3 V-50 V & =-10 \%,+250 \% \\
5 I V-350 V & =-10 \%,+100 \% \\
35 I V-450 V & =-10 \%,+50 \%
\end{aligned}
$$

| C1 | $283-002$ | $.01 \mu f$ | Disc Type | 500 v |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| C2 | $283-002$ | $.01 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C3 | $283-002$ | $.01 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C4 | $283-003$ | $.01 \mu \mathrm{f}$ | Disc Type | 150 v |  |
| C5 | $281-557$ | 1.8 pf | Cer. | 500 v |  |
|  |  |  |  | 500 v | $10 \%$ |
| C7 | $281-544$ | 5.6 pf | Cer. | 500 v | $\pm .25 \mathrm{pf}$ |
| C8 | $281-534$ | 3.3 pf | Cer. | 150 v |  |
| C9 | $283-003$ | $.01 \mu \mathrm{f}$ | Disc Type | 50 v |  |
| C10 | $283-010$ | $.05 \mu \mathrm{f}$ | Disc Type | 25 v |  |

CAPACITORS (Cont'd.)

| C21 | 281-580 | 470 pf | Cer. | 500 v | 10\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C30 | 283-026 | . $2 \mu \mathrm{f}$ | Disc Type | 25 v |  |
| C40 | 283-026 | . $2 \mu \mathrm{f}$ | Disc Type | 25 v |  |
| C50 | 283-026 | . $2 \mu \mathrm{f}$ | Disc Type | 25 |  |
| C60 | 281-504 | 10 pf | Cer. | 500 | 10\% |
| C61 | 281-504 | 10 pf | Cer. | 500 | 10\% |
| C65 | 281-549 | 68 pf | Cer. | 500 | 10\% |
| C75 | 283-000 | . $001 \mu \mathrm{f}$ | Disc Type | 500 |  |
| Cllo | 283-010 | . $05 \mu \mathrm{f}$ | Disc Type | 50 |  |
| Cl20 | 283-010 | . $05 \mu \mathrm{f}$ | Disc Type | 50 |  |
| Cl26 | 281-519 | 47 pf | Cer. | 500 | 10\% |
| C140 | 283-002 | . $01 \mu \mathrm{P}$ | Disc Type | 500 |  |
| C145A | 283-012 | .1 Hf | Disc Type | 100 |  |
| C145B | 283-010 | . $05 \mu \mathrm{f}$ | Disc Type | 50 |  |
| C145D | 283-003 | . $01 \mu \mathrm{f}$ | Disc Type | 150 |  |
| C145E | 283-001 | . $005 \mu \mathrm{f}$ | Disc Type | 500 |  |
| C145G | 283-000 | . $001 \mu \mathrm{f}$ | Disc Type | 500 |  |
| C145H | 283-032 | 470 pf | Disc Type | 500 | 5\% |
| C146A | 281-512 | 27 pf | Cer. | 500 | 10\% |
| C146B | 281-022 | 8-50 pf | Cer. |  |  |
| C155 | 283-000 | . $001 \mu \mathrm{P}$ | Disc Type | 500 |  |
| Cl60 | 283-010 | . $05 \mu \mathrm{f}$ | Disc Type | 50 |  |
| C164 | 281-511 | 22 pf | Cer. | 500 | 10\% |


| CAPACITORS (Cont'd.) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Cl66 | 281-523 | 100 pf | Cer. | 350 v |  |
| C200 | 283-026 | . $02 \mu \mathrm{f}$ | Disc Type | 25 v |  |
| C201 | 283-026 | . $02 \mu \mathrm{f}$ | Disc Type | 25 v |  |
| C202 | 283-002 | . $01 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C225 | 283-000 | . $001 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C231 | 281-518 | 47 pf | Cer. | 500 v |  |
| C232 | 283-002 | . $01 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C241 | 283-000 | . $001 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C242 | 281-543 | 270 pf | Cer. | 500 v | 10\% |
| C254 | 281-550 | 120 pf | Cer. | 500 v | 10\% |
| C261 | 283-026 | $.2 \mu \mathrm{f}$ | Disc Type | 25 v |  |
| C260A |  | $1 \mu \mathrm{f}$ |  |  |  |
| C260B ) | *295-065 | $.1 \mu f$ | Timing Series | Match | within 1\% |
| $\begin{aligned} & \text { C260C } \\ & \text { C260D } \end{aligned}$ |  | $.01 \mu \mathrm{f}$ <br> $.001 \mu \mathrm{f}$ |  |  |  |
| C260E | 283-591 | 150 pf | Mica | 500 v | 5\% |
| C260F | 281-022 | 8-50 pf | Cer. Var. |  |  |
| C263 | 281-061 | 5.5-18 pf | Cer. Var. |  |  |
| C270 | 281-518 | 47 pf | Cer. | 500 v |  |
| C274 | 283-028 | . $0022 \mu \mathrm{f}$ | Disc Type | 50 v |  |
| C288 | 283-000 | . $001 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C300 | 283-067 | . $001 \mu \mathrm{f}$ | Disc Type | 200 | 10\% |
| C301 | 290-107 | $25 \mu \mathrm{f}$ | Littl-Lytics | 25 |  |
| C302 | 283-003 | . $01 \mu \mathrm{f}$ | Disc Type | 150 |  |
| C303 | 281-551 | 390 pf | Cer. | 500 | 10\% |

Page 5-4
Type 5T1A

| CAPACITORS (Cont'd.) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C305 | 283-000 | . $001 \mu \mathrm{f}$ | Disc Type |  | 500 v |  |
| 6309 | 281-504 | 10 pf | Cer. |  | 500 v | 10\% |
| C310 | 283-003 | . $01 \mu \mathrm{f}$ | Disc Type |  | 150 v |  |
| C322 | 281-551 | 390 pf | Cer. |  | 500 v | 10\% |
| C332 | 281-523 | 100 pf | Cer. |  | 350 v |  |
| C335 | 283-003 | . $01 \mu \mathrm{f}$ | Disc Type |  | 150 v |  |
| C341 | 283-024 | $.1 \mu \mathrm{f}$ | Disc Type |  | 30 v |  |
| C342 | 283-000 | . $001 \mu \mathrm{f}$ | Disc Type |  | 500 v |  |
| C345 | 283-004 | . $02 \mu \mathrm{f}$ | Disc Type |  | 150 v |  |
| C346 | 285-623 | . $47 \mu \mathrm{f}$ | PIM |  | 100 v |  |
| C358A | 283-581 | 510 pf | Mica |  | 300 v | 5\% |
| C358C | 283-580 | 220 pf | Mica |  | 500 v | 5\% |
| C358D | 281-012 | 7-45 pf | Cer. | Var. |  |  |
| C358E | 283-579 | 100 pf | Mica |  | 500 v | 5\% |
| C358F | 281-012 | $7-45 \mathrm{pf}$ | Cer. | Var. |  |  |
| C358G | 283-578 | 27 pf | Mica |  | 500 v | 5\% |
| C358H | 281-012 | $7-45 \mathrm{pf}$ | Cer. | Var. |  |  |
| C358J | 281-542 | 18 pf | Cer. |  | 500 v | 10\% |
| C358K | 281-007 | 3-12 pf | Cer. | Var. |  |  |
| C360 | *291-019 | . $01 \mu \mathrm{f}$ | Polystyren |  | 500 | 5\% |

CAPACITORS (Cont'd.)

| C361 | 285-576 | $1 \mu \mathrm{f}$ | PIM | 100 v | 10\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C362 | 283-012 | $.1 \mu \mathrm{f}$ | Disc Type | 100 v |  |
| C365 | 283-003 | . $01 \mu \mathrm{f}$ | Disc Type | 150 v |  |
| C370 | 283-000 | . $001 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C373 | 283-000 | . $001 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C374 | 283-001 | . $005 \mu \mathrm{f}$ | Disc Type | 500 v |  |
| C377 | 285-572 | . $1 \mu \mathrm{f}$ | PTM | 200 v |  |
| C378 | 285-572 | . $1 \mu \mathrm{f}$ | PITM | 200 v |  |
| C390 | 290-015 | $100 \mu \mathrm{f}$ | EMPI | 25 v |  |
| C391 | 283-026 | $.2 \mu \mathrm{f}$ | Dise Type | 25 v |  |
| C396 | 290-026 | $5 \mu \mathrm{f}$ | EMT | 25 |  |
| C397 | 290-015 | $100 \mu \mathrm{f}$ | EMT | 25 |  |
| C398 | 283-026 | . $2 \mu \mathrm{f}$ | Disc Type | 25 |  |
|  |  | DIODES |  |  |  |
| D7 | 152-008 | Germanium | T12G |  |  |
| D25 | 152-043 | Tunnel | 1 N 312920 MA |  |  |
| D35 | 152-043 | Tunnel | 1N3129 20 MA |  |  |
| D45 | 152-043 | Tunnel | 1N3129 20 MA |  |  |
| D55 | 152-043 | Tunnel | 1 N 312920 MA |  |  |
| D65 | 152-043 | Tunnel | 1N3129 20 MA |  |  |
| D72 | 152-026 | Germanium | Q6-100 |  |  |
| D82 | 152-008 | Germanium | T12G |  |  |
| D92 | 152-008 | Germanium | T12G |  |  |
| D122 | 152-061 | Silicon | 6061 |  |  |


|  |  | DIODES (Cont'd.) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| D132 | 152-008 | Germanium | Tl2G |  |
| D144 | 152-008 | Germanium | Tl2G |  |
| D146 | 152-045 | Silicon | 6045 |  |
| D147 | 152-008 | Germanium | Tl2G |  |
| D164 | 152-008 | Germanium | T12G |  |
| D234 | 152-076 | Zener | OAZ10 |  |
| D255 | 152-074 | Tunnel | 1N3128 | 5 MA |
| D256 | 152-071 | Silicon | ED2007 |  |
| D270 | 152-071 | Silicon | ED2007 |  |
| D271 | 152-008 | Germanium | T12G |  |
| D272 | 152-058 | Stabistor | SG22 |  |
| D275 | 152-073 | Tunnel | 10 MA |  |
| D276 | 152-077 | Back | BD1 1 | MA |
| D285 | 152-043 | Tunnel | 1N3129 | 20 MA |
| D300 | 152-025 | Germanium | IN634 |  |
| D306 | 152-025 | Germanium | 1N634 |  |
| D324 | 152-071 | Silicon | ED2007 |  |
| D325 | 152-074 | Tunnel | 1 N3128 | 5 MA |
| D336 | 152-025 | Germanium | IN634 |  |
| D337 | 152-025 | Germanium | 1N634 |  |
| D345 | 152-045 | Silicon | 6045 |  |
| D352 | 152-045 | Silicon | 6045 |  |
| D353 | 152-045 | Silicon | 6045 |  |
| D360 | 152-045 | Silicon | 6045 |  |
| D361 | 152-045 | Silicon | 6045 |  |


| D362 |  | DIODES (Cont'd.) |  |
| :---: | :---: | :---: | :---: |
|  | 152-045 | Silicon | 6045 |
| D377 | 152-069 | Zener | 1M75210 |
| D378 | 152-069 | Zener | 1M75210 |
| D420 | 152-066 | Stilicon | 1N3194 |
| D421 | 152-066 | Sillicon | 1N3194 |
| D422 | 152-066 | Silicon | 1N3194 |
|  |  | INDUCTORS |  |
| L25 | *108-182 | $.3 \mu \mathrm{~h}$ |  |
| L35 | *108-182 | . $3 \mu \mathrm{~h}$ |  |
| L45 | *108-182 | . $3 \mu \mathrm{~h}$ |  |
| L55 | *108-182 | . $3 \mu \mathrm{~h}$ |  |
| L300 | *108-200 | $40 \mu \mathrm{~h}$ |  |
| L390 | *120-261 | Toroid 5 |  |
| L398 | *120-261 | Toroid 5 |  |

RESISTORS
Resistors are fixed, composition, $\pm 10 \%$ unless otherwise indicated.

| R3 | $316-121$ | $120 \Omega$ | $1 / 4 \mathrm{w}$ |
| :--- | :---: | :---: | :---: |
| R4 | $317-201$ | $200 \Omega$ | $1 / 10 \mathrm{w}$ |
| R5 | $316-222$ | 2.2 k | $1 / 4 \mathrm{w}$ |
| R6 | $317-510$ | $51 \Omega$ | $1 / 10 \mathrm{w}$ |
| R7 | $317-510$ | $51 \Omega$ | $1 / 10 \mathrm{w}$ |
| R8 | $316-152$ | 1.5 k | $1 / 4 \mathrm{w}$ |
| R9 | $317-510$ | $51 \Omega$ | $1 / 10 \mathrm{w}$ |

> RESISTORS (Cont'd.)

| R10 | $302-101$ | $100 \Omega$ | $1 / 2 \mathrm{w}$ |
| ---: | ---: | ---: | ---: |
| R11 | $302-101$ | $100 \Omega$ | $1 / 2 \mathrm{w}$ |
| R12 | $302-470$ | $47 \Omega$ | $1 / 2 \mathrm{w}$ |
| R14 | $316-472$ | 4.7 k | $1 / 4 \mathrm{w}$ |
| R15 | $302-223$ | 22 k | $1 / 2 \mathrm{w}$ |


| R164 | $311-299$ | 100 k |  |
| :--- | ---: | ---: | :--- |
| R17 | $316-472$ | 4.7 k | $1 / 4 \mathrm{w}$ |
| R18 | $302-470$ | $47 \Omega$ | $1 / 2 \mathrm{w}$ |
| R19 | $316-472$ | 4.7 k | $1 / 4 \mathrm{w}$ |
| R20 | $307-023$ | $4.7 \Omega$ | $1 / 2 \mathrm{w}$ |

Var.
THRESHOLD

Var. TRIG. RECOG. T.D. BIAS

5\%

5\%

5\%

5\%

R33
R34
+Concentric with R136. Furnished as a unit.

Type 5T1A
RESISTORS (Cont'd.)

R35
R40
R4I
R42
R44

R45
R47
R48
R49
R50

R51
R52
R53
R54
R55

R60
R61
R65
R66
R67

R73
R74
R75
R83

311-171
307-023
305-621
301-471
316-561

311-171
315-750
315-750
316-103
307-023

305-471
301-361
316-560
316-681
311-171

316-101
316-101
311-004
306-391
307-053

315-510
316-122
316-122
316-472

5 k
$4.7 \Omega \quad 1 / 2 \mathrm{w}$
620 2 w
$470 \Omega 1 / 2 \mathrm{w}$
$560 \Omega \quad 1 / 4 \mathrm{w}$

5 k
75 1/4 w
75 - $1 / 4 \mathrm{w}$
$10 \mathrm{k} \quad 1 / 4 \mathrm{w}$
$4.7 \Omega \quad 1 / 2 \mathrm{w}$
$470 \Omega \quad 2 \mathrm{w}$ $360 \Omega \quad 1 / 2 \mathrm{w}$ $56 \Omega \quad 1 / 4 \mathrm{w}$ $680 \Omega \quad 1 / 4 \mathrm{w}$ 5 k

100 1/4 w $100 \Omega \quad 1 / 4 \mathrm{w}$ $200 \Omega$

390 2 พ
$3.3 \Omega \quad 1 / 2 \mathrm{w}$

51 a $1 / 4 \mathrm{w}$
$1.2 \mathrm{k} \quad 1 / 4 \mathrm{w}$
$1.2 \mathrm{k} \quad 1 / 4 \mathrm{w}$
$4.7 \mathrm{k} \quad 1 / 4 \mathrm{w}$

Var.
TRIG RECOVERY T.D. BIAS

## 5\%

5\%

TRIG. RECOG. T.D.BIAS 5\%

5\%
$5 \%$
5\%

TRIG. RECOVERY T.D. BIAS

OUTPUT T.D. BIAS

| RESISTORS (Cont'd.) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R93 | 316-472 | 4.7 k | 1/4 w |  |  |  |
| R101 | 316-181 | $180 \Omega$ | 1/4 w |  |  |  |
| R103 | 316-181 | $180 \Omega$ | $1 / 4$ w |  |  |  |
| R110 | 316-220 | 229 | 1/4 w |  |  |  |
| R115 | 301-752 | 7.5 k | 1/2 w |  |  | 5\% |
| R116 | 316-393 | 39 k | 1/4 w |  |  |  |
| R117 | 316-683 | 68 k | 1/4 w |  |  |  |
| R120 | 316-220 | $22 \Omega$ | 1/4 w |  |  |  |
| R122 | 302-222 | 2.2 k | 1/2 w |  |  |  |
| R125 | 309-317 | 7.45 k | 1/2 w |  | Prec. | 1\% |
| R126 | 316-473 | 47 k | 1/4 w |  |  |  |
| R127 | 316-154 | 150 k | 1/4 w |  |  |  |
| R132 | 309-317 | 7.45 k | 1/2 w |  | Prec. | 1\% |
| R133 | 309-154 | 30 k | 1/2 w |  | Prec. | 1\% |
| R136 + | 311-299 | 5 k |  | Var. |  | RECOVERY TIME |
| R140 | 316-100 | 10 』 | 1/4 w |  |  |  |
| R144 | 306-154 | 150 k | 2 w |  |  |  |
| R145 | 316-560 | $56 \Omega$ | $1 / 4$ w |  |  |  |
| R147 | 302-222 | 2.2 k | 1/2 w |  |  |  |
| R154 | 315-472 | 4.7 k | $1 / 4 \mathrm{w}$ |  |  | 5\% |
| R155 | 316-271 | $270 \Omega$ | $1 / 4 \mathrm{w}$ |  |  |  |
| R157 | 316-223 | 22 k | 1/4 w |  |  |  |
| R160 | 316-220 | $22 \Omega$ | 1/4 w |  |  |  |
| R164 | 316-473 | 47 k | 1/4 w |  |  |  |
| R165 | 316-472 | 4.7 k | $1 / 4 \mathrm{w}$ |  |  |  |
| tConce | with R16 | shed as a | it. |  |  |  |


| RESISTORS (Cont'd.) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R166 | 316-393 | 39 k | 1/4 w |  |  |  |
| R167 | 316-683 | 68 k | 1/4 w |  |  |  |
| R175 | 315-472 | 4.7 k | 1/4 w |  |  | 5\% |
| R176 | 316-393 | 39 k | 1/4 w |  |  |  |
| R177 | 316-104 | 100 k | 1/4 w |  |  |  |
| R200 | 316-100 | 10 』 | 1/4 w |  |  |  |
| R201 | 316-100 | $10 \Omega$ | $1 / 4 \mathrm{w}$ |  |  |  |
| R202 | 316-100 | $10 \Omega$ | 1/4 w |  |  |  |
| R208B | 318-012 | 25 k | 1/8 w |  | Prec. | 1\% |
| R208C | 318-001 | 100 k | 1/8 w |  | Prec. | 1\% |
| R208D | 318-016 | 225 k | $1 / 8 \mathrm{w}$ |  | Prec. | 1\% |
| R208E | 321-450 | 475 k | 1/8 w |  | Prec. | 1\% |
| R208F | 318-121 | 1.225 meg | 1/8 w |  | Prec. | 1\% |
| R208G | 319-073 | 2.475 meg | 1/4 w |  | Prec. | 1\% |
| R209B | 321-356 | 49.9 k | $1 / 8 \mathrm{w}$ |  | Prec. | 1\% |
| R209C | 321-337 | 31.6 k | $1 / 8$ w |  | Prec. | 1\% |
| R209D | 321-331 | 27.4 k | $1 / 8 \mathrm{w}$ |  | Prec. | 1\% |
| R209E | 321-329 | 26.1 k | $1 / 8 \mathrm{w}$ |  | Prec. | 1\% |
| R209F | 321-328 | 25.5 k | $1 / 8 \mathrm{w}$ |  | Prec. | 2\% |
| R209G | 321-328 | 25.5 k | $1 / 8 \mathrm{w}$ |  | Prec. | 1\% |
| R2114 | *311-295 | 10 k |  | Var. | WW | VARTABLE |
| R212 | 309-159 | 5 k | $1 / 2 \mathrm{w}$ |  | Prec. | 1\% |
| R213A | 318-074 | 11.8 k | 1/8 w |  | Prec. | 1\% |
| R213B | 318-010 | 5.03 k | $1 / 8 \mathrm{w}$ |  | Prec. | 1\% |

+Concentric with SW211. Furnished as a unit.

RESISTORS (Cont'd.)

| R214A | 309-193 | 25 k | 1/2 w |  | Prec. | 1\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R214B | 309-389 | 50 k | 1/2 w |  | Prec. | 1\% |
| R214C | 309-376 | 125 k | 1/2 w |  | Prec. | 1\% |
| R214D | 309-389 | 50 k | 1/2 w |  | Prec. | 1\% |
| R2148 | 309-260 | 100 k | 1/2 w |  | Prec. | 1\% |
| R214F | 309-162 | 250 k | 1/2 w |  | Prec. | 1\% |
| R214G | 309-389 | 50 k | 1/2 w |  | Prec. | 1\% |
| R215B | 309-389 | 50.k | 1/2 w |  | Prec. | 1\% |
| R215C | 309-037 | 31.1 k | 1/2 w |  | Prec. | 1\% |
| R215D | 309-389 | 50 k | 1/2 w |  | Prec. | 1\% |
| R215E | 309-375 | 33.3 k | 1/2 w |  | Prec. | 1\% |
| R215F | 309-339 | 27.4 k | 1/2 w |  | Prec. | 1\% |
| R215G | 309-389 | 50 k | 1/2 w |  | Prec. | 1\% |
| R216 | 309-168 | 78 k | 1/2 w |  | Prec. | 1\% |
| R217A, B | 311-394 | $2 \times 10 \mathrm{k}$ |  | Var. |  | TIME POSITION |
| R218 | 318-074 | 11.8 k | 1/8 w |  | Prec. | 1\% |
| R219A | 309-181 | 2.5 k | 1/2 w |  | Prec. | 1\% |
| R219B | 302-223 | 22 k | $1 / 2 \mathrm{w}$ |  |  |  |
| R220 | 311-125 | 50 k | . 2 w | Var. |  | DELAY ZFRRO |
| R223 | 309-049 | 150 k | 1/2 w |  | Prec. | 1\% |
| R225 | 311-303 | $200 \Omega$ |  | Var. |  | INVERTER INPUT ZERO |
| R227 | 309-200 | 11.76 k | 1/2 w |  | Prec. | 1\% |
| R229 | 301-393 | 39 k | 1/2 w |  |  | 5\% |
| R231 | 309-159 | 5 k | 1/2 w |  | Prec. | 1\% |
| R232 | 316-100 | $10 \Omega$ | $1 / 4 \mathrm{w}$ |  |  |  |

RESISTORS (Cont'd.)

| R233 | 304-334 | 330 k | 1 w |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R234 | 303-153 | 15 k | 1 w |  |  | 5\% |
| R237 | 316-101 | $100 \%$ | 1/4 w |  |  |  |
| R240 | 316-562 | 5.6 k | 1/4 w |  |  |  |
| R241 | 316-122 | 1.2 k | 1/4 w |  |  |  |
| R242 | 315-510 | $51 \Omega$ | 1/4 w |  |  | 5\% |
| R243 | 316-124 | 120 k | 1/4 w |  |  |  |
| R244 | 315-133 | 13 k | 1/4 w |  |  | 5\% |
| R254 | 311-393 | 1 k |  | Var. |  | RAMP RECOV. |
| R261 | 316-100 | 102 | 1/4 w |  |  |  |
| R260A | 301-510 | 51. | 1/2 w |  |  | 5\% |
| R260F | 316-100 | $10 \Omega$ | 1/4 w |  |  |  |
| R263 | 315-510 | $51 \Omega$ | $1 / 4 \mathrm{w}$ |  |  | 5\% |
| R264 | 315-181 | $180 \Omega$ | 1/4 w |  |  | 5\% |
| R265 | 308-273 | 6.5 k | 5 w |  | WW | 3\% |
| R267 | 311-395 | 2.5 k |  | Var. |  | SWEEP CAL. |
| R270 | 316-101 | $100 \Omega$ | 1/4 w |  |  |  |
| R271 | 318-084 | 10 k | 1/8 w |  | Prec. | 1\% |
| R272 | 316-103 | 10 k | 1/4 w |  |  |  |
| R274 | 316-122 | 1.2 k | 1/4 w |  |  |  |
| R275 | 311-060 | 1 k |  | Var. |  | COMPARATOR LEVEL |
| R285 | 316-561 | $560 \Omega$ | 1/4 w |  |  |  |
| R286 | 316-152 | 1.5 k | 1/4 w |  |  |  |
| R287 | 316-332 | 3.3 k | 1/4 w |  |  |  |
| R288 | 307-057 | 5.10 | 1/2 w |  |  | 5\% |

RESISTORS (Cont'd.)

| R289 | 308-067 | $750 \Omega$ | 5 w | WW | 5\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R303 | 301-152 | 1.5 k | 1/2 w |  | 5\% - |
| R304 | 311-170 | 20 k |  | Var. | SAMPLES/CM CAL. |
| R305 | 302-270 | $27 \Omega$ | 1/2 w |  |  |
| R306 | 301-472 | 4.7 k | 1/2 w |  | 5\% |
| R308 | 316-223 | 22 k | $1 / 4$ w |  |  |
| R309 | 302-393 | 39 k | 1/2 w |  |  |
| R310 | 302-105 | 1 meg | 1/2 w |  |  |
| R312 | 317-910 | $91 \Omega$ | 1/10 w |  | 5\% |
| R314 | 317-910 | 91 』 | 1/10 w |  | 5\% |
| R315 | 301-102 | 1 k | 1/2 w |  | 5\% |
| R319 | 302-474 | 470 k | 1/2 w |  |  |
| R322 | 301-332 | 3.3 k | 1/2 w |  | 5\% |
| R323 | 302-101 | 100 @ | 1/2 w |  |  |
| R324 | 301-222 | 2.2 k | $1 / 2 \mathrm{w}$ |  | 5\% |
| R325 | 301-472 | 4.7 k | 1/2 w |  | 5\% |
| R330 | 301-274 | 270 k | 1/2 w |  | 5\% |
| R331 | 302-393 | 39 k | 1/2 w |  |  |
| R332 | 301-103 | 10 k | 1/2 w |  | 5\% |
| R333 | 301-272 | 2.7 k | 1/2 w |  | 5\% |
| R334 | 302-104 | 100 k | 1/2 w |  |  |
| R335 | 302-101 | $100 \Omega$ | 1/2 w |  |  |
| R336 | 301-472 | 4.7 k | 1/2 w |  | 5\% |
| R337 | 302-393 | 39 k | $1 / 2 \mathrm{~W}$ |  |  |
| R340 | 301-123 | 12 k | 1/2 w |  | 5\% |

RESISTORS (Cont'd.)

| R341 | 302-270 | 27 | $1 / 2 \mathrm{w}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R342 | 301-512 | 5.1 k | 1/2 w |  |  | 5\% |
| R343 | 301-332 | 3.3.k | 1/2 w |  |  | 5\% |
| R344 | 301-473 | 47 k | 1/2 w |  |  | 5\% |
| R345 | 311-170 | 20 k |  | Var. |  | SWP LENGTH |
| R346 | 302-101 | 100 | 1/2 w |  |  |  |
| R349 | 316-223 | 22 k | 1/4 w |  |  |  |
| R356 | 311-157 | 100 k |  | Var. |  | TIMED |
| R357 | 309-095 | 10 meg | 1/2 w |  | Prec. | 1\% |
| R358 | 301-102 | 1 k | $1 / 2 \mathrm{w}$ |  |  | 5\% |
| R362 | 303-223 | 22 k | 1 w |  |  | 5\% |
| R364 | 316-101 | 100 ת | 1/4 w |  |  |  |
| R365 | 302-101 | $100 \Omega$ | $1 / 2 \mathrm{w}$ |  |  |  |
| R370 | 316-101 | 1008 | 1/4 w |  |  |  |
| R371 | 301-393 | 39 k | 1/2 w |  |  | 5\% |
| R372 | 316-101 | $100 \Omega$ | 1/4 w |  |  |  |
| R373 | 316-101 | 100 | 1/4 w |  |  |  |
| R374 | 316-101 | 100 | 1/4 w |  |  |  |
| R375 | 303-273 | 27 k | 1 W |  |  | 5\% |
| R376 | 305-153 | 15 k | 2 w |  |  | 5\% |
| R377 | 301-124 | 120 k | $1 / 2 \mathrm{w}$ |  |  | 5\% |
| R381 | 311-125 | 50 k | . 2 w | Var. |  | STAIRCASE DC LEVEL |
| R382 | 309-090 | 50 k | 1/2 w |  | Prec. | 1\% |
| R383 | 309-090 | 50 k | 1/2 w |  | Prec. | 1\% |
| R384 | 309-115 | 1 k | 1/2 w |  | Prec. | 1\% |


|  |  | RESISTORS (Cont'd.) |  |
| ---: | ---: | ---: | ---: |
| R386 | $316-101$ | $100 \Omega$ | $1 / 4 \mathrm{w}$ |
| R393 | $306-330$ | $33 \Omega$ | 2 w |
| R394 | $306-330$ | $33 \Omega$ | 2 w |
| R395 | $304-101$ | $100 \Omega$ | 1 w |
| R420 | $302-275$ | 2.7 meg | $1 / 2 \mathrm{w}$ |

## SWITCHES

## Unwired Wired

| SWIOA ) | Rotary | TRIGGERING (Source) |  |  |
| :--- | ---: | :--- | :--- | :--- |
| SW1OB ) | $260-438$ | $* 262-452$ | Rotary | TRIGGERING (Polarity) |
| SW210 | $260-527$ | $* 262-552$ | Rotary | TIME EXPANDER |
| SW211t | $* 311-295$ |  |  |  |
| SW260 | $260-528$ | $* 262-553$ | Rotary | SWEEP TIME/CM |
| SW325 ) | $260-526$ | $* 262-554$ | Rotary | SWEEP MODE |
| SW358 ) |  |  | Rotary | SAMPLES/CM |

TRANSFORMERS
T2
T65
*120-262
Toroid $1 T$
Toroid 3T
T284
*120-263
Toroid 3T
T300 *120-265 Toroid TT

TRANSISTORS
Q4
151-027
2N700
Q73
151-068
2N636
Q84
151-065
2N1991
Q94
151-065
2N1991
Q104
151-031
2N1517
+Concentric with R21l. Furnished as a unit.

## TRANSISTORS (Cont'd.)

| Q115 | 151-072 | 2N1308 |
| :---: | :---: | :---: |
| Q125 | 151-072 | 2N1308 |
| Q144 | 151-072 | 2N1308 |
| Q154 | 151-071 | 2N1305 |
| Q165 | 151-072 | 2N1308 |
| Q175 | 151-072 | 2N1308 |
| Q223 | 151-103 | Planar Silicon |
| Q234 | 151-087 | J3138 |
| Q244 | 151-123 | 2N976 |
| Q254 | 151-123 | 2N976 |
| Q261 | 151-108 | Tek 151-108 |
| Q276 | 151-108 | Tek 151-108 |
| Q284 | 151-123 | 2N976 |
| Q300 | *153-511 | OC170 checked |
| Q314 | 151-054 | 2N1754 |
| Q324 | 151-068 | 2N636 |
| Q335 | 151-031 | 2 N 1517 |
| Q345 | 151-040 | 2N1302 |
|  |  | ELECTRON TUBES |
| V361 | 154-215 | 6688/E180F |
| V373 | 154-187 | 6DJ8/ECC88 |



FRONT

| Ref. | Part No. | Quan. | Description |
| :---: | :---: | :---: | :---: |
| 1. | 366-146 | 1 | Knob, Charcoal |
|  | 366-032 | 1 | Knob, Small Red |
|  | 210-413 | 1 | Nut |
|  | 210-840 | 1 | Washer |
|  | 210-012 | 1 | Lockwasher |
| 2. | 366-142 | 2 | Knob, Charcoal |
|  | 366-031 | 2 | Knob, Small Red |
|  | 210-413 | 2 | Nut |
|  | 210-840 | 2 | Washer |
|  | 210-012 | 2 | Lockwasher |
| 3. | 132-001 | 1 | Nut Coupling |
|  | 132-002 | 1 | Sleeve, Outer Conductor |
|  | 132-007 | 1 | Snap Ring |
|  | 132-016 | 1 | Retaining Nut |
|  | 132-026 | 1 | Outer Transition |
|  | 132-027 | 1 | Inner Transition |
|  | 132-028 | 1 | Insulator |
|  | 132-029 | 1 | Inner Conductor |
|  | 166-221 | 1 | Tube, Alum., Ferrule |
|  | 132-040 | 1 | Adapter, Pane1 |
|  | 211-038 | 4 | Screw, Adapter to Subpane 1 |
| 4. | 333-753 | 1 | Pane1, Front |
|  | 006-105 | 1 | Cover, Front Panel |
|  | 387-783 | 1 | Plate, Subpane 1 |
| 5. | 366-144 | 1 | Knob, Large Charcoal |
|  | 366-038 | 1 | Knob, Small Red |
|  | 210-413 | 1 | Nut |
|  | 210-840 | 1 | Washer |
|  | 210-012 | 1 | Lockwasher |
| 6. | 334-679 | 1 | Tag, Metal Serial |
| 7. | 366-175 | 1 | Knob, Charcoal |
|  | 366-140 | 1 | Knob, Small Red |
|  | 210-413 | 1 | Nut |
|  | 210-840 | 1 | Washer |
|  | 210-012 | 1 | Lockwasher |
| 8. | 358-054 | 1 | Bushing, Banana Jack |
|  | 210-011 | 1 | Lockwasher |
|  | 210-471 | 1 | Nut, Spacer |



## RIGHT SIDE

| Ref. | Part No. | Quan. | Description |
| :---: | :---: | :---: | :---: |
| 1. | 670-029 | 1 | Etched Circuit Board, Trigger |
|  |  | Include |  |
|  |  | 136-062 | Socket, Transistor |
|  |  | 352-041 | 1 Holder, Tunnel Diode |
|  | 211-008 | 4 | Screw, Circuit Board to Chassis |
| 2. | 426-121 | 1 | Mount, Toroid |
|  | 361-007 | 1 | Spacer |
| 3. | 348-003 | 1 | Grommet |
| 4. | 179-599 | 1 | Cable, Harness, Etched Board |
| 5. | 124-146 | 2 | Ceramic Strip, 16 Notch |
|  | 361-007 |  | Spacer |
| 6. | 210-413 | 2 | Nut, Pot Mounting |
|  | 210-840 | 2 | Washer |
| 7. | 348-031 | 3 | Grommet, Plastic Snap-in |
| 8. | 354-068 | 2 | Ring, Capacitor Securing |
| 9. | 210-204 | 1 | Solder Lug |
|  | 213-044 | 1 | Screw |
| 10. | 124-145 | 8 | Ceramic Strip, 20 Notch |
|  | 361-007 | 16 | Spacer |
| 11. | 348-005 | 2 | Grommet |
| 12. | 136-095 | 11 | Socket, Transistor |
|  | 213-113 | 22 | Screw, Socket to Chassis |
| 13. | 441-412 | 1 | Chassis, Ramp Amp |
|  | 211-538 | 3 | Screw, Chassis to Subpanel |
|  | 211-507 | 2 | Screw, Chassis to Rear Plate |
|  | 210-006 | 3 | Lockwasher |
|  | 210-407 | 3 | Nut |
| 14. | 210-201 | I | Solder Lug |
|  | 213-044 | 1 | Screw |
| 15. | 179-774 | 1 | Cable, Harness, Ramp Amp Chassis |
| 16. | 210-223 | 4 | Solder Lug, Mini. Pot (not shown) |
| 17. | 179-639 | 1 | Cable, Harness, Pot |

## RIGHT SIDE (Cont.)

| Ref. | Part No. | Quan. | Description |
| :---: | :---: | :---: | :---: |
| 18. | 670-030 |  | Etched Circuit Board, Fast Ramp |
|  |  | Include |  |
|  |  | 136-062 | Socket, Transistor |
|  |  | 352-041 | Holder, Tunnel Diode |
|  | 211-008 | 4 | Screw, Circuit Board to Chassis |
|  | 210-204 | 1 | Solder Lug |
| 19. | 124-147 | 1 | Ceramic Strip, 13 Notch |
|  | 361-007 | 2 | Spacer |
| 20. | 211-040 | 1 | Screw, Nylon |
|  | 210-810 | 1 | Washer, Fiber |
|  | 385-107 | 1 | Rod, Nylon, Core Mounting |
|  | 211-011 | 1 | Screw, Rod to Chassis |
| 21. | 124-149 | 1 | Ceramic Strip, 7 Notch |
|  | 361-007 | 2 | Spacer |



Ref. Part No. Quan. Description

1. | $131-149$ | 2 | Connector, Plug-in |
| :--- | :--- | :--- |
| $211-008$ | 4 | Screw |
| $210-004$ | 3 | Lockwasher |
| $210-201$ | 1 | Solder Lug |
| $210-406$ | 4 | Nut |
|  |  |  |
| 2. | $387-598$ | 1 |$\quad$ Plate, Rear Frame



LEFT SIDE

| Ref. | Part No. | Quan. | Description |
| :---: | :---: | :---: | :---: |
| 1. | 384-566 | 4 | Rod, Frame |
|  | 212-044 | 4 | Screw, Rod to Rear Plate |
| 2. | 179-772 | 1 | Cable, Harness, Stair-Step Chassis |
| 3. | 210-201 | 1 | Solder Lug |
|  | 213-044 | 1 | Screw |
| 4. | 136-014 | 1 | Socket, Tube |
|  | 213-044 | 2 | Screw |
| 5. | 348-003 | 3 | Grommet |
| 6. | 136-085 | 1 | Socket, Tube W/shield |
|  | 213-044 | 2 | Screw |
| 7. | 124-148 | 2 | Ceramic Strip, 9 Notch |
|  | 361-007 | 4 | Spacer |
| 8. | 352-008 | 1 | Holder, Neon |
|  | 211-031 | 1 | Screw, Holder to Subpane1 |
|  | 210-406 | 2 | Nut |
| 9. | 210-413 | 2 | Nut, Pot |
|  | 210-012 | 1 | Lockwasher |
| 10. | 348-002 | 2 | Grommet |
| 11. | 136-127 | 1 | Socket, Tunnel Diode Holder |
| 12. | 124-147 | 4 | Ceramic Strip, 13 Notch |
|  | 361-007 | 8 | Spacer |
| 13. | 348-005 | 1 | Grommet |
| 14. | 124-145 | 4 | Ceramic Strip, 20 Notch |
|  | 361-007 | 8 | Spacer |
| 15. | 136-095 | 5 | Socket, Transistor |
|  | 213-113 | 10 | Screw, Socket to Chassis |
| 16. | 441-489 | 1 | Chassis, Stairstep |
|  | 211-559 | 2 | Screw, Chassis to Subpanel |
|  | 211-507 | 2 | Screw, Chassis to Rear Plate |
|  | 210-006 | 4 | Lockwasher |
|  | 210-407 | 4 | Nut |



BOTTOM

| Ref. | Part No. | Quan. | Description |
| :---: | :---: | :---: | :---: |
| 1. | $\begin{aligned} & 166-204 \\ & 132-117 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | Tube, Coax. Adapter Ferrule |
| 2. | $\begin{aligned} & 166-240 \\ & 132-117 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | Tube, Coax. Adapter Ferrule |
| 3. | $\begin{aligned} & 406-747 \\ & 211-504 \end{aligned}$ | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ | Bracket, Sweep Speed Switch Screw, Bracket to Chassis |
| 4. | 348-031 | 1 | Grommet, Plastic Snap-in |
| 5. | 343-042 | 2 | Clamp, Cable |
|  | 211-507 | 2 | Screw, Clamp to Chassis |
|  | 210-803 | 2 | Washer |
|  | 210-006 | 2 | Lockwasher |
|  | 210-407 | 2 | Nut |
| 6. | 211-014 | 2 | Screw, Pot Mounting |
|  | 166-025 | 2 | Tube, Aluminum Spacer |
| 7. | 210-449 | 2 | Nut, Bracket to Switch |
|  | 210-006 | 2 | Lockwasher |
| 8. | 179-773 | 1 | Cable, Harness, Sweep Time/CM |
| 9. | 131-221 | 2 | Connector, Bulkhead Jack |
|  | 358-172 | 2 | Bushing, Connector |
| 10. | 426-150 | 1 | Mount, Connector |
|  | 211-511 | 2 | Screw, Mount to Bracket |
|  | 406-779 | 1 | Bracket, Mount Support (not shown) |
|  | 211-507 | 2 | Screw, Bracket to Chassis |
|  | 210-006 | 4 | Lockwasher |
|  | 210-407 | 4 | Nut |
| 11. | 214-222 | 1 | Spring Striker |
|  | 361-029 | 1 | Spacer, Spring Striker |
|  | 211-082 | 2 | Screw, Spring Striker to Subpane1 |
|  | 210-004 | 2 | Lockwas her |
|  | 210-406 | 2 | Nut |



| $\underline{\text { Ref. }}$ | Part No. | Quan. | Description |
| :---: | :---: | :---: | :---: |
| 1. | 406-748 | 1 | Bracket, Capacitor Mounting |
|  | 211-008 | 4 | Screw, Bracket to Switch |
|  | 210-004 | 4 | Lockwasher |
|  | 210-406 | 4 | Nut |
| 2. | 214-153 | 4 | Fastener, Capacitor |
| 3. | 406-914 | 1 | Bracket, Pot Mounting |
|  | 211-507 | 2 | Screw, Bracket to Chassis |
| 4. | 179-640 | 1 | Cable, Harness, Connecting |
| 5. | 343-042 | 1 | Clamp, Cable |
|  | 211-507 | 1 | Screw, Clamp to Chassis |
|  | 210-803 | 1 | Washer |
|  | 210-006 | 1 | Lockwasher |
|  | 210-407 | 1 | Nut |
| 6. | 384-135 | 1 | Rod, Spacer |
|  | 211-507 | 2 | Screw, Rod to Chassis |
| 7. | 131-180 | 2 | Connector, Stand-off |
|  | 358-135 | 2 | Bushing, Tefion |



Ref. Part No. Quan. Description

1. 017-044 2 Attenuator, $50 \Omega$, 10X
(see pub. no. 061-762 for parts breakdown)
2. 017-501
$1 \quad$ Cable, $50 \Omega, 10 \mathrm{~N} \mathrm{sec}$.
(see pub. no. 061-765 for parts breakdown)
