# OPERATOR'S, ORGANIZATIONAL, DIRECT SUPPORT GENERAL SUPPORT, AND DEPOT MAINTENANCE MANUAL 

## OSCILLOSCOPE AN/USM-273

(NSN 6625-00-930-6637)

This copy is a reprint which includes current pages from Changes 1.

THIS MANUAL IS AN AUTHENTICATION OF THE MANUFACTURER'S COMMERCIAL LITERATURE WHICH, THROUGH USAGE, HAS BEEN FOUND TO COVER THE DATA REQUIRED TO OPERATE AND MAINTAIN THIS EQUIPMENT. SINCE THE MANIJAL WAS NOT PREPARED IN ACCORDANCE WITH MILITARY SPECIFICATION, THE FORMAT HAS NOT BEEN STRUCTURED TO CONSIDER LEVEL OF MAINTENANCE NOR TO INCLUDE A FORMAL SECTION ON DEPOT MAINTENANCE STANDARDS.

WARNING<br>DANGEROUS VOLTAGES<br>EXIST IN THIS EQUIPMENT<br>DON'T TAKE CHANCES!

## CAUTION

Special 3\% silver solder is required on the ceramic terminal strips in this equipment. A 40 - to 75 -watt soldering iron should be used and it should be tinned with the same special solder. Additional quantities of the solder may be procured under FSN 3439-912-8698. Ordinary solder may be used only in dire emergency.
$\left.\begin{array}{l}\text { Technical Manual } \\ \text { no. } 11-6625-1722-15\end{array}\right\}$
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Fig. 1-1. Top; the Type 453 Oscilloscope. Bottom; the Type R453 Oscilloscope.

## SECTION 0

## INSTRUCTIONS

0-1. Scope
This manual describes Oscilloscope AN/USM-273 (fiq. 1-1 and provides maintenance instructions. Throughout this manual, the AN/USM-273 is referred to as the Tektronix Type 453 Oscilloscope. The maintenance allocation chart appears in appendix C. Repair parts and special tools lists are contained in TM-6625-1722-24P.
$0-2$. Indexes of Publications
a. DA Pam 310-4. Refer to the latest issue of DA Pam 310-4 to determine whether there are new editions, changes, or additional publications pertaining to the equipment.
b. DA Pam 310-7. Refer to DA Pam 310-7 to determine whether there are modification work orders ( $\mathrm{MWO}^{\prime}$ S) pertaining to the equipment. 0 -3. Maintenance Forms, Records, and Reports
a. Reports of Maintenance and Unsatisfactory Equipment. Department of the Army forms and procedures used for equipment maintenance will be those prescribed by TM 38-750, The Army Maintenance Management System.
b. Report of Packaging and Handling Deficiencies. Fill out and forward DD Form 6 (Packaging Improvement Report) as prescribed in AR 700-58/ NAVSUPINST 4030.29/AFR 71-13/MCO P4030.29A, and DLAR 4145.8.
c. Discrepancy in Shipment Report (DISREP) (SF 361). Fill out and forward Discrepancy in Shipment Report (DISREP) (SF 361) as prescribed in AR 55-38/NAVSUPINST 4610.33B/AFR 75-18/MCO P4610.19C and DLAR 4500.15.

0-4. Reporting Equipment Improvement Recommendations (EIR)

If your Oscilloscope AN/USM-273 needs improvement, let us know. Send us an EIR. You, the user, are the only one who can tell us what you don't like about your equipment. Let us know why you don't like the design. Tell us why a procedure is hard to perform. Put it on an SF 368 (Quality Deficiency Report). Mail it to Commander, US Army Communications and Electronics Materiel Readiness Command, ATTN: DRSEL-ME-MQ, Fort Monmouth, $N J$ 07703. We'll send you a reply.

0-5. Administrative Storage
Administrative storage of equipment issued to and used by Army activities shall be in accordance with TM 740-90-1.

0-6 Destruction of Army Electronics Materiel

Destruction of Army electronics materiel to prevent enemy use shall be in accordance with TM 750-244-2.

0-7. Reporting Errors and Recommending Improvements

You can help improve this manual. If you find any mistakes or if you know of a way to improve the procedures, please let us know. Mail your letter or DA Form 2028 (Recommended Changes to Publications and Blank Forms) to Commander, US Army Communications and Electronics Materiel Readiness Command, ATTN: DRSEL-ME-MQ, Fort Monmouth, NJ 07703. In either case, a reply will be furnished direct to you.

## SECTION

## CHARACTERISTICS

## Introduction

The Tektronix Type 453 Oscilloscope is a transistorized portable oscilloscope designed to operate in a wide range of environmental conditions. The light weight of the Type 453 allows it to be easily transported, while providing the performance necessary for accurate high-frequency measurements. The dual-channel DC-to- 50 MHz vertical system provides calibrated deflection factors from 5 millivolts to 10 volts/division. Channels 1 and 2 can be cascaded using an external cable to provide a one millivolt minimum defection factor (both VOLTS/DIV switches set to 5 mV ).

The trigger circuits provide stable triggering over the full range of vertical frequency response. Separate trigger controls are provided to select the desired triggering for the A and B sweeps. One of three sweep modes can be selected for the A sweep; automatic, normal or single sweep. The horizontal sweep provides a maximum sweep rate of 0.1 microsecond/division (10 nanosecond/division using 10X magnifier) along with a delayed sweep feature for accurate relative-time measurements. Accurate X-Y measurements can be made with Channel 2 providing the vertical deflection, and Channel 1 providing the horizontal [deflection. (TRIGGER switch set to CH 1 ONLY, HORIZ DISPLAY switch set to EXT HORIZ). The regulated DC power supplies maintain con-
stant output over a wide variation of line voltages and frequencies. Total power consumption of the instrument is approximately 90 watts.

Information given in this instruction monual applies to the Type R453 also unless otherwise noted. The Type R453 is electrically identical to the Type 453 but is mechanically adapted for mounting in a standard 19 -inch rack. Rackmounting instructions, a mechanical parts list and a dimensional drawing for the Type R453 are provided in Section 10 of this manual.

The electrical characteristics which follow are divided into two categories. Characteristics listed in the Performance Requirement column are checked in the Performance Check and Calibration sections of this manual. Items listed in the Operational Information column are provided for reference use and do not directly reflect the measurement capabilities of this instrument. The Performance Check procedure given in Section 5 of this manual provides a convenient method of checking the items listed in the Performance Requirement column. The following electrical characteristics apply over a calibration interval of 1000 hours at an ambient temperature range of $-15^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$, except as otherwise indicated. Warm-up time for given accuracy is 20 minutes.

## ELECTRICAL CHARACTERISTICS <br> VERTICAL DEFLECTION SYSTEM

| Characteristic | Performance Requirement | Operational Information |
| :---: | :---: | :---: |
| Deflection Factor | 5 millivolts/division to 10 volts/division in 11 calibrated steps for each channel. One millivolt/ division when Channel 1 and 2 are cascaded. | Steps in 1-2-5 sequence |
| Deflection Accuracy | Within $\pm 3 \mathrm{Y} \%$ of indicated deflection with VARIABLE control set to CAL. Cascaded deflection factor uncalibrated. | With gain correct at 20 mV |
| Variable Deflection Factor | Uncalibrated deflection factor at least 2.5 times the VOLTS/DIV switch indication. This provides a maximum uncalibrated deflection factor of 25 volts/division in the 10 volts position. |  |
| Bandwidth at Upper -3 dB point (with or without P6010 Probe) <br> 20 mV to 10 VOLTS/DIV | DC to 50 MHz or greater |  |
| $10 \mathrm{mV} / \mathrm{DIV}$ | DC to 45 MHz or greater | Driven from 25 -ohm source |
| $5 \mathrm{mV} / \mathrm{DIV}$ | DC to 40 MHz or greater |  |
| Channels land 2 cascaded | DC to 25 MHz or greater | Measured at one millivolt/division |
| Risetime (calculated). With or without P6010 Probe. 20 mV to 10 VOLTS/DIV | Less than 7 nanoseconds | Risetime calculated from bandwidth measurement using the formula: $350$ |
| $10 \mathrm{mV} / \mathrm{DIV}$ | Less than 7.8 nanoseconds |  |
| $5 \mathrm{mV} / \mathrm{DIV}$ | Less than 8.75 nanoseconds | Where: ${ }_{\mathrm{t}}=$ Risetime in nanoseconds. |
| Channels 1 and 2 cascaded | Less than 14 nanoseconds | BW = Bandwidth in megahertz. |

VERTICAL (cont)

| Characteristic | Performance Requirement | Operational Information |
| :---: | :---: | :---: |
| Input RC Characteristics |  | Typically 1 megohm ( $\pm 2 \%$ ), paralleled by 20 pF ( $\pm 3 \%$ ) |
| Maximum Input Voltage |  | 600 volts DC + peak AC (one kilohertz or less). Peak-to-peak AC not to exceed 600 volts. |
| Input Coupling Modes | AC or DC, selected by front-panel switch |  |
| AC Low-Frequency Response (lower -3 dB point) Without probe |  | Typicaily 1.6 Hz , Input Coupling switch set to AC |
| With P6010 Probe <br> Trace Shift Due to Input Gate Current (at $25^{\circ} \mathrm{C}$ ) | Negligible | Typically 0.16 Hz |
| Vertical Display Modes | Channel 1 only <br> Channel 2 only <br> Dual-troce, alternate between channels Dual-trace, chopped between channels Added algebraically |  |
| Chopped Repetition Rate | Approximately one-microsecond segments from each channel dispiayed at repetition rate of 500 $\mathrm{kHz}, \pm 20 \%$. |  |
| Attenuator Isolation | Greater than 10,000:1, DC to 20 MHz |  |
| Common Mode Rejection Ratio | Greater than $20: 1$ at 20 MHz for common-mode signals less than eight times VOLTS/DIV switch setting. | With optimum GAIN adjustment at low frequency |
| Linear Dynamic Range Useful for Common-Mode Relection in ADD Mode |  | Less than $10 \%$ incremental signal distortion for instantaneous input voltage of -10 or +10 times VOLTS/DIV switch setting |
| Polarity Inversion | Signal on Channel 2 can be inverted |  |
| Signal Delay Line |  | Approximately 140 nanoseconds |
| Low-Frequency Vertical Linearity | Less than 0.15 division compression or expansion of two division signal when positioned to vertical extremes of display area | Includes CRT linearity. Measured with one-kilohertz square wave. |
| Trace Drift (after 20 minute |  | Time Temperature |
| warm up) <br> 20 mV to 10 VOLTS/DIV |  | Typically less than Typically less than <br> 0.03 division/hour <br> 0.0075 <br> gree C division/de-  |
| $10 \mathrm{mV} / \mathrm{DIV}$ |  | Typically less than Typically less than <br> 0.05 division/hour <br> 0.0125 division/de- <br> gree C  |
| $5 \mathrm{mV} / \mathrm{DIV}$ |  | Typically less than Typically less than <br> 0.08 division/hour <br> 0.02 division/de- <br>  <br> gree C |

TRIGGERING (A AND B SWEEP)

| Source | Internal from displayed channel or from Channel <br> 1 only <br> Internal from AC power source <br>  <br> External <br> External divide by 10 |  |
| :--- | :--- | :--- |
| Coupling | AC low-frequency reject |  |
|  | AC low |  |
|  | AC high-frequency reject |  |
| DC | Sweep can be triggered from positive-going or <br> negative-going portion of trigger signal |  |

TRIGGERING (cont)

| Characteristic | Performance Requirement | Operational Information |
| :---: | :---: | :---: |
| Internal Trigger Sensitivity AC | 0.2 division of deflection, minimum, 30 Hz to 10 MHz ; increasing to 1 division at 50 MHz | Typical -3 dB point, 16 Hz |
| LF REJ | 0.2 division of deflection, minimum, 30 Hz to 10 0.2 division of deflection, minimum, 30 kHz to 10 | Typical -3 dB point, 16 kHz |
| HF REJ | 0.2 division of deflection, minimum, 30 Hz to 50 kHz | Typical -3 dB points, 16 Hz and 100 kHz |
| DC | 0.2 division of deflection, minimum, $D C$ to 10 MHz ; increasing to 1 division at 50 MHz |  |
| $\begin{aligned} & \text { External Trigger Sensitivity } \\ & \text { AC } \end{aligned}$ | 50 millivolts, minimum, 30 Hz to 10 MHz ; increasing to 200 millivolts at 50 MHz | Typical -3 dB point, 16 Hz |
| LF REJ | 50 millivolts, minimum, 30 kHz to 10 MHz ; increasing to 200 millivolts at 50 MHz | Typical -3 dB point, 16 kHz |
| HF REJ | 50 millivolts, minimum, 30 Hz to 50 kHz | Typical -3 dB points, 16 Hz and 100 kHz |
| DC | 50 millivolts, minimum, DC to 10 MHz ; increasing to 200 millivolts at 50 MHz |  |
| Auto Triggering (A sweep only) | Stable display presented with signal amplitudes given under Internal and External Trigger Sensitivity above 20 Hz . Presents a free-running sweep for lower frequencies or in absence of trigger signal. |  |
| Single Sweep (A sweep only) | A Sweep Generator produces only one sweep when triggered. Further sweeps are locked out until RESET button is pressed. Trigger sensitivity same as given above. |  |
| Display Jitter | Less than 1 nanosecond at 10 nanoseconds/division sweep rate (MAG switch set to X10) |  |
| Maximum Input Voltage |  | 600 volts $D C+$ peak AC (one kilohertz or less). Peak-to-peak AC not to exceed 600 volts. |
| External Trigger Characteristics (approximate) |  | 1 Megohm paralleled by 20 pF , except in LF REJ |
| LEVEL Control Range | At least $\pm 2$ volts, SOURCE switch in EXT position. At least $\pm 20$ volts, SOURCE switch in EXT $\div 10$ position |  |

## HORIZONTAL DEFLECTION SYSTEM

A and B Sweep Generator

| Sweep Rates A Sweep | 0.1 microsecond/division to 5 seconds/division in 24 calibrated stem | A sweep is main and delaying sweep |
| :---: | :---: | :---: |
| B sweep | 0.1 microsecond/division to 0.5 second/division in 21 calibrated steps | $B$ sweep is delayed sweep |
| Sweep Accuracy-A and B Sweep 5 s to $0.1 \mathrm{~s} /$ DIV | $0^{\circ} \mathrm{C}$ to $+40^{\circ} \mathrm{C}$ - $15^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$ | A VARIABLE and B TIME/DiV VARIABLE controls set to CAL |
|  | Within $\pm 3 \%$ of indi- Within $\pm 5 \%$ of indicated sweep rate cated sweep rate |  |
| 50 ms to $0.1 \mu \mathrm{~s} / \mathrm{DIV}$ | Within $\pm 3 \%$ of indi- Within $\pm 4 \%$ of indicated sweep rate cated sweep rate |  |
| Variable Sweep Rate | Uncalibrated sweep rate to at least 2.5 times the TIME/DIV indication, or a maximum of at least 12.5 seconds/division in the 5 s position (B sweep, maximum of 1.25 seconds/division in the .5 s position. |  |

## A and B Sweep Generotor

| Characteristic | Performance Requirement | Operational Information |
| :---: | :---: | :---: |
| Sweep Length <br> A sweep | Variable from less than 4 divisions to $11.0, \pm 0.5$ division | A TIME/DIV switch set to 1 ms |
| B sweep | 11.0 divisions, $\pm 0.5$ division | B TIME/DIV switch set to 1 ms |
| Sweep Hold-off-A sweep 5 s to $10 \mu \mathrm{~s} / \mathrm{DIV}$ | Less than one times the A TIME/DIV switch setting |  |
| $5 \mu \mathrm{~s}$ to $0.1 \mu \mathrm{~s} / \mathrm{DIV}$ | Less than 2.5 microseconds |  |

## Sweep Magnifier

| Sweep Magnification | Each sweep rate can be increased 10 times the Extends fastest sweep rate to 10 nano- <br> indicated sweep rate by horizontally expanding seconds/division <br> the center division of display |  |
| :--- | :--- | :--- | :--- |
| Magnified Sweep Accuracy | $1 \%$ tolerance added to speclfled sweep accuracy |  |
| Magnified Sweep Linearity | $\pm 1.5 \%$ for any eight division portion of the <br> total magnified sweep length (excluding first <br> and last 60 nanoseconds of magnified sweep) |  |
| Normal/Magnified Registration | $\pm 0.2$ division, or less, trace shift at graticuie <br> center when switching MAG switch from X10 <br> to OFF |  |

## Sweep Delay

| Calibrated Delay Time Range | Continuous from 50 seconds to 1 microsecond |  | A VARIABLE control set to CAL for indicated delay |
| :---: | :---: | :---: | :---: |
| DELAY-TIME MULTIPLIER  <br> Dial Range 0.20 to 10.20 |  |  |  |
| Delay Time Accuracy 5 s to $0.1 \mathrm{~s} / \mathrm{DIV}$ | $0^{\circ} \mathrm{C}$ to $+40^{\circ} \mathrm{C}$ | $-15^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$ | Includes incremental multiplier linearity |
|  | Within $\pm 2.5 \%$ of indicated delay | Within $\pm 3.5 \%$ of indicated delay |  |
| 50 ms to $1 \mu \mathrm{~s} /$ DIV | Within $\pm 1.5 \%$ of indicated delay | Within $\pm 2 \%$ of indicated delay |  |
| Incremental Multiplier Linearity | $\pm 0.2 \%$ | $\pm 0.3 \%$. |  |
| Delay Time Jitter | Less than 1 part in 20,0 DIV switch setting | 000 of 10 times A TIME/ | Equal to 0.5 division, or less, with the A TIME/DIV switch set to 1 ms and the B TIME/DIV switch set to $1 \mu \mathrm{~s}$. |

External Horizontal Amplifier

| Input to Channel 1 (TRIGGER switch in CH 1 ONLY) Deflection factor | 5 millivolts/division to 10 volts/division in 11 calibrated steps | Steps in 1-2-5 sequence. <br> Channel 1 VARIABLE control does not affect horizontal deflection |
| :---: | :---: | :---: |
| Accuracy | $0^{\circ} \mathrm{C}$ to $+40^{\circ} \mathrm{C} \quad-15^{\circ} \mathrm{V}$ to $+55^{\circ} \mathrm{C}$ |  |
|  | Within $\pm 5 \%$ of indi- Within $\pm 8 \%$ of indicated deflection cated deflection | With external horizontal gain correct at 20 mV |
| X Bandwidth at Upper -3 dB Point | 5 MHz or greater |  |
| Input RC characteristics |  | Typically 1 megohm ( $\pm 2 \%$ ), paralleled by 20 pF ( $\pm 3 \%$ ) |
| Phase difference between X and Y amplifiers at 50 kHz | Less than $3^{\circ}$ |  |
| Input to EXT HORIZ Connector Deflection factor | B SOURCE switch in EXT; 270 millivolts/division, $\pm 15 \%$. <br> B SOURCE switch in EXT $\div 10 ; 2.7$ volts/division, $\pm 20 \%$ |  |

External Horizontal Amplifier (cont)

| Characteristic | Performance Requirement | Operational Information |
| :---: | :---: | :---: |
| X Bandwidth at Upper -3 | 5 MHz or greater |  |
| Input RC characteristics (approximate] |  | 1 megohm, paralleled by 20 pF |
| Phase difference between $X$ and Y amplifiers at 50 kHz |  | Less than $3^{\circ}$ |

CALIBRATOR

| Waveshape | Square wave |  |  |
| :---: | :---: | :---: | :---: |
| Polarity | Positive going with baseline at zero volts |  |  |
| Output Voltage | 0.1 volt or 1 volt, peak to peak |  | Selected by CALBRATOR switch on side panel |
| Output Curent | 5-milliamperes through PROBE LOOP on side panel |  |  |
| Repetition Rate | 1 kHz |  |  |
|  | $0^{\circ} \mathrm{C}$ to $+40^{\circ} \mathrm{C}$ | $-15^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$ |  |
| Voltage Accuracy | $\pm 1 \%$ | $\pm 1.5 \%$ |  |
| Curent Accuracy | $\pm 1 \%$ | $\pm 1.5 \%$ |  |
| Repetition Rate Accuracy | $\pm 0.5 \%$ | $\pm 1 \%$ |  |
| Risetime | Less than 1 microsecond |  |  |
| Duty Cycle | 49\% to 51\% |  |  |
| Output Resistance |  |  | Approximately 200 ohms in 1 V position. Approximately 20 ohms in .1 V position. |

Z AXIS INPUT

| Sensitivity | 5 volt peak-to-peak signal produces noticeable modulation |  |
| :---: | :---: | :---: |
| Usable Frequency Range | DC to greater than 50 MHz |  |
| Input Resistance at DC |  | Approximately 47 kilohms |
| Input Coupling | DC coupled |  |
| Polarity of Operation |  | Positive-going input signal decreases trace intensity <br> Negative-going signal increases trace |
| Maximum Input Voltage |  | 200 volts combined DC and peak AC |

OUTPUT SIGNALS

| A and B Gate Waveshape | Rectangular pulse |  |
| :---: | :---: | :---: |
| Amplitude | 12 volts peak, $\pm 10 \%$ |  |
| Pola | Positlve-going with baseline at about -0.7 volts. |  |
| Duration | I Same duration as the respective sweep | A GATE duration variable between about 4 and 11 times the A TIME/DIV switch setting with the A SWEEP LENGTH control. |
| Output resistance |  | Approximately 1.5 kilohms |
| Vertical Signal Out (CH 1 only) Output voltage | 25 millivolts, or greater/division of CRT display into 1 megohm load. |  |
| Bandwidth | DC to 25 MHz or greater when cascaded with Channel 2 or into 50 -ohm load. |  |
| Output coupling | DC coupled |  |
| Output resistance |  | Approximately 50 ohms |

## POWER SUPPLY



CATHODE-RAY TUBE (CRT)

| Tube Type |  |  | Tektronix T4530-31-1 rectangular <br> Phosphor <br> Accelerating Potential |  |
| :--- | :--- | :--- | :--- | :--- |
| P31 standard. Others available on |  |  |  |  |
| special order. |  |  |  |  |

## ENVIRONMENTAL CHARACTERISTICS

The following environmental test limits apply when tested in accordance with the recommended test procedure. This instrument will meet the electrical characteristics given in this section following environmental test. Complete details on environmental test procedures, including failure criteria, etc., may be obtained from Tektronix, Inc. Contact your local Tektronix Field Office or representative.

| Characteristic | Performance Requirement | Supplemental Information |
| :---: | :---: | :---: |
| Temperature Operating | $-15^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$ | Fan at rear circulates air throughout instrument. Automatic resetting thermal cutout protects instrument from overheating. |
| Non-operating | $-55^{\circ}$ to $+75^{\circ} \mathrm{C}$ |  |
| Altitude Operating | 15,000 feet maximum | Derate maximum operating temperature by $1^{\circ} \mathrm{C} / 1000$ feet change in altitude above 5000 feet. |
| Non-operating | 50,000 feet maximum |  |
| Humidity Non-operating | Five cycles (120 hours) of Mil-Std-202C, Method 106B | Exclude freezing and vibration |
| Vibration Operating and non-operating | 15 minutes along each of the three major axes at a total displacement of 0.025 -inch peak to peak ( 4 g at $55 \mathrm{c} / \mathrm{s}$ ) with frequency varied from 10-55$10 \mathrm{c} / \mathrm{s}$ in one-minute cycles. Hold at $55 \mathrm{c} / \mathrm{s}$ for three minutes on each axis. | Instrument secured to vibration platform during test. Total vibration time, about 55 minutes. |
| Shock Operating and non-operating | Two shocks of 30 g , one-half sine, 11 millisecond duration each direction along each major axis. | Guillotine-type shocks. Total of 12 shocks |

ENVIRONMENTAL CHARACTERISTICS (cont)

| Characteristic | Performance Requirement | Operational Information |
| :---: | :---: | :---: |
| Transportation | Meets National Safe Transit type of test when <br> packaged as shipped from Tektronix, Inc. <br> One hour vibration slightly in excess of 1 g. | Package should just leave vibration sur- <br> Package vibration |
| Package drop <br> Type 453 | 30-inch drop on any comer, edge or flat surface. |  |$\quad$| Type R453 |
| :--- |

MECHANICAL CHARACTERISTICS

| Characteristic | Information |
| :--- | :--- |
| Construction <br> Chassis | Aluminum a lloy |
| Panel | Aluminum alloy with ano- <br> dized finish |
| Cabinet | Blue vinyl-coated aluminum |
| Circuit boards | Glass-epoxy laminate |
| Overall Dimensions, Type <br> 453 (measured ot maxi- <br> mum points) |  |
| Height | $\mathbf{7 1 / 4}$ inches |
| Width | $12 \frac{1}{2}$ inches |
| Length | $20 / 2$ inches (includes front <br> cover); 22 $\mathbf{3} / 8$ <br> handle positioned for camy- <br> ing. |
| Overall Dimensions, Type <br> R453 (measured at maxi- <br> mum points) <br> Height |  |

## STA NDARD ACCESSORIES

Standard accessories supplied with the Type 453 and R453 are listed on the last pullout page of the Mechanical Parts List illustrations.

## opERATING INSTRUCTIONS

## General

To effectively use the Type 453 , the operation and capabilities of the instrument must be known. This section describes the operation of the front-, side- and rear-panel controls and connectors, gives first time and general operating information and lists some basic applications for this instrument.

## Front Cover and Handle

The front cover furnished with the Type 453 provides a dust-tight seal around the front panel. Use the cover to protect the front panel when storing or transporting the instrument. The cover also provides storage space for probes and other accessories (see Fig. 2-1).


Fig. 2-1. Accessory storage provided in front cover.
The handle af the Type 453 can be positioned for carrying or as a tilt-stand for the instrument. To position the handle, press in at both pivot points (see Fig. 22) and turn the handle to the desired position. Several positions are provided for convenient carrying or viewing. The instrument may also be set an the rear-panel feet for operation or storage.

## Operating Voltage

The Type 453 can be operated from either a 115 -volt or a 230 -volt nominal line-voltage source. The Line Voltage


Fig. 2-2. Handle positioned to provide a stand for the instrument

Selector assembly on the rear panel converts the instrument from one operating range to the other. In addition, this assembly changes the primary connections of the power transformer to allow selection of one of three regulating ranges. The assembly also includes the two line fuses. When the instrument is converted from 115 -volt to 230 -volt nominal operation, or vice versa, the assembly connects or disconnects one of the fuses to provide the correct protection for the instrument. Use the following procedure to convert this instrument between nominal line voltages or regulating ranges.

1. Disconnect the instrument from the power source.
2. Loosen the two captive screws which hold the cover onto the voltage selector assembly; then pull to remove the cover.
3. To convert from 115 -volts nominal to 230 -volts nominal line voltage, pull out the Voltage Selector switch bar (see Fig. 2-3]; turn it around $180^{\circ}$ and plug it back into the remaining holes. Change the line-cord power plug to match the power-source receptacle or use a 115 - to 230 -volt adapter.
4. To change regulating ranges, pull out the Range Selector switch bar (see Fia. 2-3); slide it to the desired position and plug it back in. Select a range which is centered about the average line voltage to which the instrument is to be connected (se Table 2-1).
5. Re-install the cover and tighten the two captive screws.
6. Before applying power to the instrument, check that the indicating tabs on the switch bars are protruding through the correct holes for the desired nominal line voltage and regulating range.


Fig. 2-3. Line Voltage Selector assembly on the rear panel (shown with cover removed).

## CAUTION

The Type 453 should not be operated with the Voltage Selector or Range Selector switches in the wrong positions for the line voltage applied. Operation of the instrument with the switches in the wrong positions may either provide incorrect aperotion or damage the instrument.

TABLE 2-1
Regulating Ranges

| Range <br> Switch Pelector | Regulating115 -Volts <br> Nominal |  |
| :---: | :---: | :---: |
|  | 90 to 110 volts | 180 to 220 volts |
| Nominal |  |  |
| (switch bar in <br> middle holes) | 104 to 126 volts | 208 to 252 volts |
| HI (switch bar in <br> right holes) | 112 to 136 volts | 224 to 272 volts |

## Operating Temperature

The Type 453 is cooled by air drawn in at the rear and blown out through holes in the top and bottom covers. Adequate clearance on the top, bottom and rear must be provided to allow heat to be dissipated away from the instrument. The clearance provided by the feet at the bottom and rear should be maintained. If possible, allow about one inch of clearance on the top. Do not block or restrict the air flow from the air-escape holes in the cabinet.

A thermal cutout in this instrument provides thermal protection and disconnects the power to the instrument if the internal temperature exceeds a safe operating level. Operation of the instrument for extended periods without the covers may cause it to overheat and the thermal cutout to open
more frequently. The air filter should be cleaned occasionally to allow the maximum amount of cooling air to enter the instrument. Cleaning instructions are given in Section 4

The Type 453 can be operated where the ambient air temperature is between $-15^{\circ} \mathrm{C}$ and $+55^{\circ} \mathrm{C}$. Derate the maximum operating temperature $1^{\circ} \mathrm{C}$ for each additional 1000 feet of altitude above 5000 feet. This instrument can be stored in ambient temperatures between $-55^{\circ} \mathrm{C}$ and $+75^{\circ} \mathrm{C}$. After storage at temperatures beyond the operating limits, allow the chassis temperature to come within the operating limits before power is applied.

## Rackmounting

Complete information for mounting the Type R453 in a cabinet rack is given in Section 10 of this manual.

## CONTROLS AND CONNECTORS

A brief description of the function or operation of the front-, side- and rear-panel controls and connectors follows (see Fig. 2-4). More detailed information is given in this section under General Operating Information.

## Cathode-Ray Tube

INTENSITY Controls brightness of display.
FOCUS Provides adjustment for a well-defined display.

SCALE ILLUM Controls graticule illumination.
TRACE FINDER Compresses display within graticule area independent of display position or applied signals.

## Vertical (both channels except as noted)

VOLTS/DIV Selects vertical deflection factor (VARIABLE control must be in CAL position for indicated deflection factor).

VARIABLE Provides continuously variable deflection factor between the calibrated settings of the VOLTS/DIV switch.

Light indicates that the VARIABLE control is not in the CAL position.

Controls vertical position of trace.
Screwdriver adjustment to set gain of the Vertical Preamp. Line between adjustment and 20 mV VOLTS/DIV position indicates that gain should be set with VOLTS/DIV switch in this position.

Input Coupling Selects method of coupling input signal (AC GND DC) to Vertical Deflection System.

AC: DC component of input signal is blocked. Low frequency limit -3 dB point) is about 1.6 hertz.

GND: Input circuit is grounded (does not ground applied signal).


Fig. 2-4. Front-, side- and rear-panel controls and connectors.
 BAL

INPUT
MODE

TRIGGER Selects saurce of internal trigger signal from vertical system.

NORM: Sweep circuits triggered from displayed channel(s). Channel 1 signal available at CH 1 OUT connector.

CH 1 ONLY: Sweep circuits triggered only from signal applied to the Channel 1 INPUT connector. No signal available at CH 1 OUT connector. CH 1 lights, located beside A and B SOURCE switches indicate when the TRIGGER switch is in the CH 1 ONLY position.

INVERT (CH 2 Inverts the Channel 2 signal when pulled only) out.

## A and B Triggering (both where applicable)

EXT TRIG Input connector for external trigger signal. INPUT

SOURCE Selects source of trigger signal.
INT: Internal trigger signal obtained from Vertical Deflection System. When CH 1 light is on, trigger signal is obtained only from the Channel 1 input signal; when the light is off, the trigger signal is abtained from the displayed channel(s). Source of internal trigger signal is selected by the TRIGGER switch.

LINE: Trigger signal obtained from a sample of the line voltage applied to this instrument.

EXT: Trigger signal obtained from an external signal applied to the EXT TRIG INPUT connector.

EXT $\div 10$ : Attenuates external trigger signal approximately 10 times.

CH 1

OUPLING (A Triggering only)

SLOPE Selects portion of trigger signal which starts the sweep.
+: Sweep can be triggered from positivegoing portion of trigger signal.
-: Sweep can be triggered from negativegoing portion of trigger signal.
LEVEL Selects amplitude point on trigger signal at which sweep is triggered.

HF STAB Decreases display jitter for high-frequency
Light indicates that the internal trigger signal is abtained only from the signal connected to the Channel 1 INPUT connector (see TRIGGER switch).

Determines method of coupling trigger signal to trigger circuit.

AC: Rejects DC and attenuates signals below about 30 hertz. Accepts signals between abaut 30 hertz and 50 megahertz.

LF REJ: Rejects DC and attenuates signals below about 30 kilohertz. Accepts signals between about 30 kilohertz and 50 megahertz.

HF REJ: Accepts signals between about 30 hertz and 50 kilohertz; rejects DC and attenuates signals outside the above range.

DC: Accepts all trigger signals from DC to 50 megahertz or greater. signals. Has negligible effect at lower sweep rates.

## $A$ and $B$ Sweep

| DELAY-TIME | Provides variable sweep delay between <br> MULTIPLIER |
| :---: | :--- |
| 0.20 and 10.20 times the delay time indi- <br> cated by the A TIME/DIV switch. |  |
| A SWEEP | Light indicates that A sweep is triggered <br> and will produce a stable display with <br> correct INTENSITY and POSITION control <br> settings. |
| TRIG'D | Light indicates that either the A or B |
| ORCAL A | VARIABLE control is not in the CAL posi- <br> tion. |
| A AND B | A TIME/DIV switch (clear plastic flange) |
| TIME/DIV | selects the sweep rate of the A sweep <br> circuit for A sweep only operatian and |
| AND DELAY | selects the basic delay time (to be multi- <br> plied by DELAY-TIME MULTIPLIER dial <br> setting) for delayed sweep operation. |
|  | B TIME/DIV (DELAYED SWEEP) switch <br> selects sweep rate of the B sweep circuit |

A VARIABLE

B SWEEP
MODE

HORIZ DISPLAY MODE

MAG Increases sweep rate to ten times setting of A or B TIME/DIV switch by horizontally expanding the center division of the display. Light indicates when magnifier is on.

A SWEEP Determines the operating mode for A
for delayed sweep operation only. VARIABLE controls must be in CAL positions for calibrated sweep rates.

Provides continuously variable A sweep rate to at least 2.5 times setting of the A TIME/DIV switch. A sweep rate is calibrated when control is set fully clockwise to CAL.

Selects B sweep operation mode.
TRIGGERABLE AFTER DELAY TIME: B sweep circuit will not produce a sweep until a trigger pulse is received following the delay time selected by the DELAY TIME (A TIME/DIV) switch and the DELAY-TIME MULTIPLIER dial.

B STARTS AFTER DELAY TIME: B sweep circuit runs immediately following delay time selected by the DELAY TIME switch and DELAY-TIME MULTIPLIER dial.

Selects horizontal mode of operation.
A: Horizontal deflection provided by A sweep. B sweep inoperative.

A INTEN DURING B: Sweep rate determined by A TIME/DIV switch. An intensified portion appears on the sweep during the B sweep time. This position provides a check of the duration and position of the delayed sweep (B) with respect to the delaying sweep (A).

DELAYED SWEEP (B): Sweep rate determined by B TIME/DIV switch with the delay time determined by the setting of the DELAY TIME (A TIME/DIV) switch and the DELAY-TIME MULTIPLIER dial. Sweep mode determined by B SWEEP MODE switch.

EXT HORIZ: Horizontal deflection provided by an external signal. sweep.

AUTO TRIG: Sweep initiated by the applied trigger signal using the A Triggering controls when the trigger signal repetition rate is above about 20 hertz. For lower repetition rates or when there is no trigger signal, the sweep free runs at the sweep rate selected by the A TIME/DIV switch to produce a bright reference trace.

NORM TRIG: Sweep initiated by the applied trigger signal using the A Triggering controls. No trace is displayed when there is no trigger signal.

SINGLE SWEEP: After a sweep is displayed, further sweeps cannot be presented until the RESET button is pressed. Display is triggered as for NORM operation using the A Triggering controls.


Switch: Controls power to the instrument.

Side Panel

ASTIG

B TiME/DIVVARIABLE

PROBE LOOP

A GATE Output connector providing a rectangular pulse coincident with A sweep.

Output connector providing a rectangular pulse coincident with B sweep.

CH 1 OUT
Screwdriver adjustment used in conjunction with the FOCUS control to obtain a well-defined display. Does not require readjustment in normal use. continuously variable sweep rate to at least 2.5 times setting of B TIME/DIV switch. B sweep rate is calibrated when control is set fully clockwise to CAL.

Current loop providing five-milliampere square-wave current from calibrator circuit.

Output connector providing a sample of the signal applied to the Channel 1 IN PUT connector when the TRIGGER switch is in the NORM position.

| CALIBRATOR | Switch selects output voltoge of Calibrator. <br> 1 -volt or 0.1-volt square wave available. |
| :--- | :--- |
| TRACE | Screwdriver adjustment to align trace with <br> ROTATION |
| horizontal graticule lines. |  |

Rear Panel
Z AXIS INPUT Input connector for intensity modulation of the CRT display.

Line Voltage Switching assembly to select the nominal Selector

| HORIZ DISPLAY | A |
| :--- | :--- |
| MAG | OFF |
| POSITION | Midrange |
| A SWEEP LENGTH | FULL |
| A SWEEP MODE | AUTO TRIG |
| POWER | OFF |
| Side-Panel Controls |  |
| B TIME/DIV VARIABLE | CAL |
| CALIBRATOR | .1 V |

2. Connect the Type 453 to a power source that meets the voltage and frequency requirements of the instrument. If the available line voltage is outside the limits of the Line Voltage Selector assembly position (on rear panel), see Operating Voltage in this section.
3. Set the POWER switch to ON. Allow about five minutes warmup so the instrument reaches a normal operating temperature before proceeding.

## CRT Controls

4. Advance the INTENSITY control until the trace is at the desired viewing level (near midrange).
5. Connect the 1 kHz CAL connector to the Channel 1 INPUT connector with a BNC cable.
6. Turn the A LEVEL control toward 0 until the display becomes stable. Note that the A SWEEP TRIG'D light is on when the display is stable.
7. Adiust the FOCUS control for a sharp, well-defined display over the entire trace length. (If focused display cannot be obtained, see Astigmatism Adjustment in this section.)
8. Disconnect the input signal and move the trace with the Channel 1 POSITION control so it coincides with one of the horizontal graticule lines. If the trace is not parallel with the graticule line, see Trace Alignment Adjustment in this section.
9. Rotate the SCALE ILLUM control throughout its range and notice that the graticule lines are illuminated as the control is turned clockwise (most obvious with mesh or smokegray filter installed). Set control so graticule lines are illuminated as desired.

## Vertical Controls

10. Change the CH 1 VOLTS/DIV switch from 20 mV to 5 mV . If the vertical position of the trace shifts, see Step Attenuator Balance in this section.
11. Set the CH 1 VOLTS/DIV switch to 20 mV and set the Channel 1 Input Coupling switch to AC. Connect the 1 kHz CAL connector to both the Channel 1 and 2 INPUT connectors with two BNC cables and a BNC T connector.

## NOTE

If the BNC cables and BNC T connector are not available, make the following changes in the procedure. Place the BNC jack post (supplied accessory) on the 1 kHz CAL connector and connect the two $10 \times$ probes (supplied accessories) to
the Channel 1 and 2 INPUT connectors. Connect the probe tips to the BNC jack post. Set the CALIBRATOR switch (on side-panel) to 1 V .
12. Turn the Channel 1 POSITION control to center the display. The display is a square wave, five divisions in amplitude with about five cycles displayed on the screen. If the display is not five divisions in amplitude, see Vertical Gain Adjustment in this section.
13. Set the Channel 1 Input Coupling switch to GND ond position the trace to the center horizontal line.
14. Set the Channel 1 Input Coupling switch to DC. Note that the baseline of the waveform remains at the center horizontal line (ground reference).
15. Set the Channel 1 Input Coupling switch to AC. Note that the waveform is centered about the center horizontal line.
16. Turn the Channel 1 VARIABLE control throughout its range. Note that the UNCAL light comes on when the VARIABLE control is moved from the CAL position (fully clockwise). The deflection should be reduced to about two divisions. Return the VARIABLE control to CAL.

## 17. Set the MODE switch to CH 2.

18. Turn the Channel 2 POSITION control to center the display. The display will be similar to the previous display for Channel 1. Check Channel 2 step attenuator balance and gain as described in steps 10 through 12. The Channel 2 input Coupling switch and VARIABLE control operate as described in steps 13 through 16.
19. Set both VOLTS/DIV switches to 50 mV .
20. Set the MODE switch to ALT and position the Channel 1 waveform to the top of the graticule area and the Channel 2 waveform to the bottom of the graticule area. Turn the A TIME/DIV switch throughout its range. Note that the display alternates between channels at all sweep rates.
21. Set the MODE switch to CHOP and the A TIME/DIV switch to $10 \mu \mathrm{~s}$. Note the switching between channels as shown by the segmented trace. Set the TRIGGER switch to CH 1 ONLY; the trace should appear more solid, since it is no longer triggered on the between-channel switching transients. Turn the A TIME/DIV switch throughout its range. A dual-trace display is presented at all sweep rates, but unlike ALT, both channels are displayed on each trace on a timesharing basis. Return the A TIME/DIV switch to .5 ms .
22. Set the MODE switch to ADD. The display should be four divisions in amplitude. Note that either POSITION control moves the display.
23. Pull the INVERT switch. The display is a straight line indicating that the algebraic sum of the two signals is zero (if the Channel 1 and 2 gain is correct).
24. Set either VOLTS/DIV switch to 20 mV . The squarewave display indicates that the algebraic sum of the two signals is no longer zero. Return the MODE switch to CH 1 and both VOLTS/DIV switches to . 2 (if using 10X probes, set both VOLTS/DIV switches to 20 mV ). Push in the INVERT switch.

## Triggering

25. Set the CALIBRATOR switch to 1 V . Rotate the A LEVEL control throughout its range. The display free runs at the extremes of rotation. Note that the A SWEEP TRIG'D light is on only when the display is triggered.
26. Set the A SWEEP MODE switch to NORM TRIG. Again rotate the A LEVEL control throughout its range. A display is presented only when correctly triggered. The A SWEEP TRIG'D light operates as in AUTO TRIG. Return the A SWEEP MODE switch to AUTO TRIG.
27. Set the A SLOPE switch to -. The trace starts on the negative part of the square wave. Return the switch to +; the trace starts with the positive part of the square wave.
28. Set the A COUPLING switch to DC. Turn the Channel 1 POSITION control until the display becomes unstable (only part of square wave visible). Return the A COUPLING switch to AC; the display is again stable. Since changing trace position changes DC level, this shows how DC level changes affect DC trigger coupling. Return the display to the center of the screen.
29. Set the MODE switch to CH 2 ; the display should be stable. Remove the signal connected to Channel 1; the display free runs. Set the TRIGGER switch to NORM; the display is again stable. Note that the CH 1 lights in A and B Triggering go out when the TRIGGER switch is changed to NORM.
30. Connect the Calibrator signal to both the Channel 2 INPUT and A EXT TRIG INPUT connectors. Set the A SOURCE switch to EXT. Operation of the LEVEL, SLOPE and COUPLING controls for external triggering are the same as described in steps 25 through 28.
31. Set the A SOURCE switch to EXT $\div 10$. Operation is the same as for EXT. Note that the A LEVEL control has less range in this position, indicating trigger signal attenuation. Return the A SOURCE switch to INT.
32. Operation of the $B$ Triggering controls is similar to A Triggering.

## Normal and Magnified Sweep

33. Set the A TIME/DIV switch to 5 ms and the MAG switch to X10. The display should be similar to that obtained with the A TIME/DIV switch set to .5 ms and the MAG switch to OFF.
34. Turn the horizontal POSITION control throughout its range; it should be possible to position the display across the complete graticule area. Now turn the FINE control. The display moves a smaller amount and allows more precise positioning. Return the A TIME/DIV switch to .5 ms , the MAG switch to OFF and return the start of the trace to the left graticule line.

## Delayed Sweep

36. Pull the DELAYED SWEEP knob out and turn it to 50 $\mu \mathrm{s}$ ((DELAY TIME remains at .5 ms$)$. Set the HORIZ DISPLAY switch to A INTEN DURING B. An intensified portion, about one division in length, should be shown at the start of the trace. Rotate the DELAY-TIME MULTIPLIER dial throughout its range; the intensified portion should move along the display.
37. Set the B SWEEP MODE switch to TRIGGERABLE AFTER DELAY TIME. Again rolate the DELAY-TIME MULTIPLIER dial throughout its range and note that the intensified portion appears to jump between posltive slopes of the display. Set the B SLOPE switch to -; the intensified portion begins on the negative slope. Rotate the B LEVEL control; the intensified portion of the display disappears when the B LEVEL control is out of the trlggerable range. Return the B LEVEL control to 0 .
38. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B). Rotate the DELAY-TIME MULTIPLIER dial througout its range; about one-half cycle of the waveform should be displayed on the screen (leading edge visible only at high INTENSITY control setting). The display remains stable on the screen, indicating that the B sweep is triggered.
39. Set the B SWEEP MODE switch to B STARTS AFTER DELAY TIME. Rotate the DELAY-TIME MULTIPLIER dial throughout its range; the display moves continously across the screen as the control is rotated.
40. Rotate the DELAYTIME MIULTIPLIER dial fully counterclockwise and set the HORIZ DISPLAY switch to A INTEN DURING B. Rotate the A SWEEP LENGTH control counterclockwise; the length of the display decreases. Set the control to the B ENDS A position; now the display ends after the intensified portion. Rotate the DELAY-TIME MULTIPLIER dial ond note that the sweep length increases as the display moves across the screen. Return the A SWEEP LENGTH control to FULL and the HORIZ DISPLAY switch to A.

## Single Sweep

41. Set the A SWEEP MODE switch to SINGLE SWEEP. Remove the Calibrator signal from the Channel 2 INPUT connector. Press the RESET button; the RESET light should come on and remain on. Again apply the signal to the Channel 2 INPUT connector; a single trace should be presented and the RESET light should go out. Return the A SWEEP MODE switch to AUTO TRIG.

## External Horizontal

42. Connect the Calibrator signal to both the Channel 2 INPUT and EXT HORIZ (B EXT TRIG INPUT] connectors. Set the B SOURCE switch to EXT, B COUPLING switch to DC and the HORIZ DISPLAY switch to EXT HORIZ. Increase the INTENSITY control setting until the display is visible (two dots displayed diagonally). The display should be five divisions vertically and about 3.7 divisions horizontally. Set the B SOURCE switch to EXT $\div 10$. The display should be reduced ten times horizontally. The display can be positioned horizontally with the horizontal POSITION or FINE control and vertically with the Channel 2 POSITION control.
43. Connect the Calibrator signal to both the Channel 1 and 2 INPUT connectors. Set the TRIGGER switch to CH 1 ONLY and the B SOURCE switch to INT.
44. The display should be five divisions vertically and horizontally. The display can be postioned horizontally with the Channel 1 POSITION control and vertically with the Channel 2 POSITION control.
45. Change the CH1 VOLTS/DIV switch to 5 . The display play is reduced to two divisions horizontally. Now set the CH 2 VOLTS/DIV switch to 5 . The display is reduced to two divisions vertically.

## Trace Finder

46. Set the CH 1 and CH 2 VOLTS/DIV switches to 10 mv . The display is not visible since it exceeds the scan area of the CRT.
47. Press the TRACE FINDER button. Note that the display is returned to the display area. While holding the TRACE FINDER button depressed, increase the vertical and horizontal deflection factors until the display is reduced to about two divisions vertically ond horizontally. Adjust the Channel 1 and 2 POSITION controls to center the display about the center lines of the graticule. Release the TRACE FINDER and note that the display remains within the viewing area. Disconnect the applied signal.
48. Reduce the INTENSITY control setting to normal, B SOURCE switch to INT and set the HORIZ DISPLAY switch to A.

## Z-Axis Input

49. If an, External signal is available (five volts peak to peak minimum] the function of the Z AXIS INPUT circuit can be demonstrated. Connect the external signal to both the Channel 2 INPUT connector and the Z AXIS INPUT binding posts. Set the A TIME/DIV switch to display about five cycles of the waveform. The positive peaks of the waveform should be blanked and the negative peaks intensified, indicating intensify modulation.
50. This completes the basic operating procedure for the Type 453. Instrument operation not explained here, or operations which need further explanation are discussed under General Operating Information.

## CONTROL SETUP CHART

Fig. 2-5 shows the front, side and rear panels of the Type 453. This chart can, be reproduced and used as a test-setup record for special measurements, applications or procedures, or it may be used as a training aid for familiarization with this instrument.

## GENERAL OPERATING INFORMATION

## Intensify Control

The setting of the INTENSITY control may affect the correct focus of the display. Slight readjustment of the FOCUS control may be necessary when the intensity level is changed. To protect the CRT phosphor, do not turn the INTENSITY control higher than necessary to provide a satisfactory display. The light filters reduce the observed light output from the CRT. When using these filters, avoid odvancing the INTENSITY control to a setting that may bum the phosphor. When lhe highest intensity display is desired, remove the filters and use the clear faceplate protector. Also, be careful that the INTENSITY control is not set too high when changing the TIME/DIV switch front a fast to a slow sweep rate, or when changing the HORIZ DISPLAY switch from EXT HORIZ operation to the norrmal sweep mode.

## Astigmatism Adjustment

If a well-defined trace cannot be obtained with the FOCUS control, adjust the ASTIG adjustment (side panel) as follows.


Fig. 2-5. Control setup chart for the Type 453.

## NOTE

To check for proper setting of the ASTIG adjustment, slowly tum the FOCUS control through the optimum setting. If the ASTIG adjustment is correctly set, the vertical and horizontal portions of the trace will come into sharpest focus at the same position of the FOCUS control. This setting of the ASTIG adjustment should be correct for any display. However, it may be necessary to reset the FOCUS control slightly when the INTENSITY control is changed.

1. Connect a 1 V Calibrator signal to either channel and set the VOLTS/DIV switch of that channel to present a twodivision display. Set the MODE switch to display the channel selected.

## 2. Set the TIME/DIV switch to .2 ms

3. With the FOCUS control and ASTIG adjustment set to midrange, adjust the INTENSITY control so the rising portion of the display can be seen.
4. Set the ASTIG adjustment so the horizontal and vertical portions of the display are equally focused, but not necessarily well focused.
5. Set the FOCUS control so the vertical portion of the trace is as thin as possible.
6. Repeat steps 4 and 5 for best overall focus. Make final check at nomal intensity.

## Graticule

The graticule of the Type 453 is intemally marked on the faceplate of the CRT to provide accurate, no-parallax measurements. The graticule is marked with six vertical and 10 horizontal divisions. Each division is 0.8 centimeter square. In addition, each major division is divided inta five minor divisions at the center vertical and horizontal lines. The vertical gain and horizontal timing are calibrated to the graticule so accurate measurements can be made from the CRT. The illumination of the graticule lines can be varied with the SCALE IШUM control.

Fig. 2-6 shows the graticule of the Type 453 and defines the various measurement lines. The terminology defined here will be used in all discussions involving graticule measurements.

## Trace Alignment Adjustment

If a free-running trace is not parallel to the horizontal graticule lines, set the TRACE ROTATION adjustment as follows. Position the troce to the center horizontal line. Adjust the TRACE ROTATION adjustment (side panel) so the trace is parallel with the horizontal graticule lines.

## Light Filter

The mesh filter provided with the Type 453 provides shielding against radiated EMI (electro-magnetic interference) from the face of the CRT. It also serves as a light filter to make the trace more visible under ambient light conditions. To


Fig. 2-6. Definition of measurement lines on Type 453 graticule.
remove the filter, press down at the bottom of the frame and pull the top of the filter away from the CRT faceplate (se Fig. 2-7).

The tinted light filter minimizes light reflections from the face of the CRT to improve contrast when viewing the display under high ambient light conditions. A clear plastic faceplate protector is also provided with this instrument for use when neither the mesh nor the tinted filter is used. The clear faceplate protector provides the best display for waveform photographs. It is also preferable for viewing high writing rate displays.
A filter or the faceplate protector should be used at all timesta protect the CRTfaceplate from scratches. The faceplate protector and the tinted filter mount in the same holder.


Fig. 2-7. Removing the filter or faceplate protector.

To remove the light filter or faceplate protector from the holder, press it out to the rear. They can be replaced by snapping them back into the holder.

## Trace Finder

The TRACE FINDER provides a means af locating a display which overscans the viewing area either vertically or horizontally. When the TRACE FINDER button is pressed, the display is compressed within the graticule area. To locate and reposition an overscanned display, use the following procedure.

## 1. Press the TRACE FINDER button

2. While the TRACE FINDER button is held depressed, increase the vertical and horizontal deflection factors until the vertical deflection is reduced to about two divisions and the horizontal deflection is reduced to about four divisions (the horizontal deflection needs to be reduced only when in the extemal horizontal mode of operation).
3. Adjust the vertical and horizontal POSTION controls to center the display about the vertical and horizontal center lines.
4. Release the TRACE FINDER button; the display should remain within the viewing area.

## Vertical Channel Selection

Either of the input channels can be used for single-trace displays. Apply the signal to the desired INPUT connector and set the MODE switch to display the channel used. However, since CH 1 ONLY triggering is provided only in Channel 1 and the invert feature only in Channel 2, the correct channel must be selected to take advantage of these features. For dual-trace displays, connect the signals to both INPUT connectors and set the MODE switch to one of the dual-trace positions.

## Vertical Gain Adjustment

To check the gain of either channel, set the VOLTS/DIV switch to 20 mV . Set the CAUBRATOR switch to .1 V and connect the 1 kHz CAL connector to the INPUT of the channel used. The vertical deflection should be exactly five divisions. If not, adjust the front-panel GAIN adjustment for exactly five divisions of deflection.

## NOTE

If the gain of the two channels must be closely matched (such as for ADD mode operation), the ADJ USTMENT procedure given in the Calibration section should be used

The best measurement accuracy when using probes is provided if the GAIN adjustment is made with the probes installed (set the CAUBRATOR switch to 1 V ). Also, to provide the most accurate measurements, calibrate the vertical gain of the Type 453 at the temperature at which the measurement is to be made.

## Step Attenuator Balance

To check the step attenuator balance of either channel, set the Input Coupling switch to GND and set the A SWEEP

MODE swich to AUTO TRIG to provide a free-running trace. Change the VOLTS/DIV switch from 20 mV to 5 mV . If the trace moves vertically, adjust the front-panel STEP ATIEN BAL adjustment as follows (allow at least 10 minutes warm up before performing this adjustment].

1. With the Input Coupling switch set to GND and the VOLTS/DIV switch set to 20 mV , move the trace to the center horizontal line of the graticule with the vertical POSITION control.
2. Set the VOLTS/DIV switch to 5 mV and adjust the STEP ATIEN BAL adjustment to retum the trace to the center horizonal line.
3. Recheck step attenuator balance and repeat adjustment until no trace shift occurs as the VOLTS/DIV switch is changed from 20 mV to 5 mV .

## Signal Connections

In general, probes offer the most convenient means of connecting a signal to the input of the Type 453. The Tektronix probes are shielded to prevent pickup of electrostatic interference. A 10X attenuator probe offers a high input impedance and allows the circuit under test to perform very close to normal operating conditions. However, a 10X probe also attenuates the input signal 10 times. The Tektronix P6045 Field Effect Transistor probe and accessory power supply offer the same high-input impedance as the 10X probes. However, it is particularly useful since it provides wide-band operatian while presenting no attenuation (1X gain) and a low input capacitance. To obtain maximum bandwidth when using the probes, observe the grounding considerations given in the probe manual. The probe-toconnector adapters and the bayonet-ground tip provide the best frequency response. Remember that a ground strap only a few inches in length can produce several percent of ringing when operating at the higher frequency limit of this system. See your Tektronix, Inc. catalog for characteristics and compatibility of probes for use with this system.

In high-frequency applications requiring maximum overall bandwidth, use coaxial cables terminated at both ends in their characteristic impedance. See the discussion on coaxial cables in this section for more information.

High-level, low-frequency signals can be connected directly to the Type 453 INPUT connectors with short unshielded leads. This coupling method works best for signals below about one kilohertz and deflection foctors above one volt/ division. When this method is used, establish a common ground between the Type 453 and the equipment undertest. Attempt to position the leads away from any source of interference to avoid errors in the display. If interference is excessive with unshielded leads, use a coaxial cable or a probe.

## Loading Effect of the Type 453

As nearly as possible, simulate actual operating conditions in the equipment under test. Otherwise, the equipment under test may not produce a nomal signal. The 10X attenuator probe and field effect transistor probe mentioned previously offer the least circuit loading. See the probe instruction manual for loading characteristics of the individual probes.

When the signal is coupled directly to the input of the Type 453, the input impedance is about one megohm paralleled by about 20 pF . When the signal is coupled to the input through a coaxial cable, the effeclive input capacitance depends upon the type and length of cable used. See the following discussion for information on obtaining maximum frequency responspe with coaxial cables.

## Coaxial Cable Considerations

The signal cables used to connect the signal 10 the type 453 INPUT connectors have a large effect on the accuracy of the displayed high-frequency waveform. To maitain the high-frequency characteristics of the applied signal, highquality low-loss coaxial cable should be used. The cable should be temminated at the Type 453 INPUT connector in its characteristic impedonce. If it is necessary to use cables with differing characteristic impedances, use suitable imped-ance-matching devices to provide the correct transition, with minimum loss, from one impedance to the other.

The characteristic impedance, velocity of propagation and nature of signal lossesin a coaxial cable are detemmined by the physical and electrical characteristics of the cable. Losses caused by energy dissipation in the dielectric are proportional to the signal frequency. Therefore, much of the high-frequency information in a fast-rise pulse can be lost in only a few feet of interconnecting cable if it is not the correct type. To be sure of the high-frequency response of the system when using cables longer than about five feet, observe the transient response of the Type 453 and the interconnecting cable with a fast-rise pulse generator (generator risetime less than 0.5 na noseconds).

## Input Coupling

The Channel 1 and 2 Input Coupling switches allow a choice of input caupling. The type of display desired will detemmine the coupling used.

The DC position can be used for most applications. However, if the DC component of the signal is much larger than the AC component, the AC position vvill probably provide a better display. DC coupling should be used to display AC signals below about 16 heltz as they will be attenuated in the AC position.

In the AC position, the DC component of the signal is blocked by a capacitor in the input circuit. The low-frequency response in the $A C$ position is about 1.6 hertz ( -3 dB point). Therefore, some low-frequency distortion can be expected near this frequency limit. Distortion will also appear in square waves which have low-frequency components.

The GND position provides a ground reference at the input of the Type 453. The signal applied to the input connector is intemally disconnected but not grounded. The input circuit is held at ground potential, eliminating the need to extemally ground the input to establish a DC ground reference.

The GND position can also be used to pre-charge the coupling capacitor to the average voltage level of the signal applied to the INPUT connector. This allows measurement of only the AC component of signals having both AC and

DC components. The pre-charging network incorporated in this unit allows the input-coupling capacitor to charge to the DC source voltage level when the Input Coupling switch is set to GND. The procedure for using this feature is as follows:

1. Before connecting the signal containing a DC component to the Type 453 INPUTconnector, set the Input Coupling switch to GND. Then connect the signal to the INPUT connector.
2. Wait about one second for the coupling capacitor to charge.
3. Set the Input Coupling switch to AC. The trace (display) will remain on the screen and the AC component of the signal can be measured in the nomal manner.

## Deflection Factor

The amount of vertical deflection produced by a signal is determined by the signal amplitude, the attenuation factor of the probe (if used), the setting of the VOLTS/DIV switch and the setting of the VARIABLE VOLTS/DIV control. The calibrated deflection factors indicated by the VOLTS/DIV switches apply only when the VARIABLE control is set to the CAL position.

The VARIABLE VOLTS/DIV control provides variable (uncalibrated) vertical deflection between the calibrated settings of the VOLTS/DIV switch. The VARIABLE control extends the maximum vertical deflection factor of the Type 453 to at least 25 volts/division (10 volts position).

## Dual-Trace Operation

Alternate Mode. The ALT position of the MODE switch produces a disploy which altemates between Channel 1 and 2 with each sweep of the CRT. Although the ALT mode can be used at all sweep rates, the CHOP mode provides a more satisfactory display at sweep rates below about 50 microseconds/division. At these slower sweep rates, altemate mode switching becomes visually perceptible.

Proper intemal triggering in the ALT mode can be obtained in either the NORM or CH 1 ONLY positions of the TRIGGER switch. When in the NORM position, the sweep is triggered from the signal on each channel. This provides a stable display of two unrelated signals, but does not indicate the time relationship between the signals. In the CH 1 ONLY position, the two signals are displayed showing true time relationship. If the signals are not time related, the Channel 2 waveform will be unstable in the CH 1 ONLY position.

Chopped Mode. The CHOP position of the MODE switch produces a display which is electronic ally switched between channels. In general, the CHOP mode provides the best display at sweep rates slower than about 50 mic roseconds/ division, or whenever dual-trace, single-shot phenomena are to be displayed. At faster sweep rates the chopped switching becomes apparent and may interfere with the display.

Proper intemal triggering for the CHOP mode is provided with the TRIGGER switch set to CH 1 ONLY. If the NORM position is used, the sweep circuits are triggered from the between-channel switching signal and both waveforms will
be unstable. Extemal triggering provides the same result as CH 1 ONLY triggering.

Two signals which are time-related can be displayed in the chopped mode showing true time relationship. If the signals are not time-related, the Channel 2 display will appear unstable. Two single-shot, transient, or random signals which occur within the time interval determined by the TIME/DIV switch (10 times sweep rate) can be compared using the CHOP mode. To correctly trigger the sweep for maximum resolution, the Channel 1 signal must precede the Channel 2 signal. Since the signals show true time relationship, time-difference measurements can be made.

## Channel 1 Output and Cascaded Operation

If a lower deflection factor than provided by the VOLTS/ DIV switches is desired, Channel 1 can be used as a wideband preamplifier for Channel 2. Apply the input signal to the Channel 1 INPUT connector. Connect a 50 -ohm BNC cable ( 18 -inch or shorter cable for maximum cascaded frequency response) between the CH 1 OUT (side panel) and the Channel 2 INPUT connectors. Set the MODE switch to CH 2 and the TRIGGER switch to NORM. With both VOLTS/ DIV switches set to 5 mV , the deflection factor will be less than one millivolt/division.

To provide calibrated one millivolt/division deflection factor, connect the .1 volt Calibrator signal to the Channel 1 INPUT connector. Set the CH 1 VOLTS/DIV switch to . 1 and the CH 2 VOLTS/DIV switch to 5 mV . Adjust the Channel 2 VARIABLE VOLTS/DIV control to produce a display exactly five divisions in amplitude. The cascaded deflection factor is determined by dividing the CH 1 VOLTS/DIV switch setting by 5 (CH 2 VOLTS/DIV switch and VARIABLE control remain as set above). For example, with the CH 1 VOLTS/ DIV switch set to 5 mV the calibrated deflection factor will be 1 millivolt/division; CH 1 VOLTS/DIV switch set to 10 mV , 2 millivolts/division, etc.

The following operating considerations and basic applications may suggest other uses for this feature.

1. If AC coupling is desired, set the Channel 1 Input Coupling switch to AC and leave the Channel 2 Input Coupling switch set to DC. When both Input Coupling switches are set to DC, DC signal coupling is provided.
2. Keep both vertical POSITION controls set near midrange. If the input signal has a DC level which necessitates one of the POSITION controls being tumed away from midrange, correct operation can be obtained by keeping the Channel 2 POSITION control near midrange and using the Channel 1 POSITION control to position the trace near the desired locatian. Then, use the Channel 2 POSITION control far exact positioning. This method will keep both Input Preamps operating in their linear range.
3. The output voltage at the CH 1 OUT connectar is at least 25 millivolts/division of CRT display in all CH 1 VOLTS/ DIV switch positions.
4. The MODE switch and Channel 1 VARIABLE VOLTS/ DIV control have no effect on the signal available at the CH 1 OUT connector.
5. The Channel 1 Input Preamp can be used as an impedance matching stage with or without voltage gain. The
input resistance is one megohm and the output resistance is about 50 ohms.
6. The dynamic range of the Channel 1 Input Preamp is equal to about 20 times the CH 1 VOLTS/DIV setting. The CH 1 OUT signal is nominally at 0 volt DC for a 0 volt DC input level [Channel 1 POSTION control centered). The Chanel 1 POSITION control can be used to center the output signal within the dynamic range of the amplifier.
7. If dual-trace operation is used, the signal applied to the Channel 1 INPUT connector is displayed when Channel 1 is tumed on. When Channel 2 is tumed on, the amplified signal is displayed. Thus, Channel 1 trace can be used to monitor the input signal while the amplified signal is displayed by Channel 2.
8. In special applications where the flat frequency response of the Type 453 is not desired, a filter inserted between the CH 1 OUT and Channel 2 INPUT connector allows the oscilloscope to essentially take on the frequency response of the filter. Combined with method 7 , the input can be monitored by Channel 1 and the filtered signal displayed by Channel 2.
9. By using Channel 1 as a 5 X low-level voltage preamplifier ( 5 mV position), the Channel 1 signal available at the CH 1 OUT connector can be used for any application where a low-impedance preamplifier signal is needed. Remember that if a 50 -ohm load impedance is used, the signal amplitude will be about one-half.

## Algebraic Addition

General. The ADD position of the MODE switch can be used to display the sum or difference of two signals, for common-mode rejection to remove an undesired signal or for DC offset (applying a DC voltage to one channel to offset the DC component of a signal on the other channel).

The common-mode rejection ratio of the Type 453 is greater than 20:1 at 20 megahertz for signal a mplitudes up to eight times the VOLTS/DIV switch setting. Rejection ratios of 100:1 can typically be achieved between DC and 5 megahertz by careful adjustment of the gain of either channel while observing the displayed common-mode signal.

Deflection Factor. The overall deflection in the ADD position of the MODE switch when both VOLTS/DIV switches are set to the same position is the same as the deflection factor indicated by either VOLTS/DIV switch. The amplitude of an added mode display can be determined directly from the resultant CRT deflection multiplied by the deflection factor indicated by either VOLTS/DIV switch. However, if the CH 1 and CH 2 VOLTS/DIV switches are set to different deflection factors, resultant voltage is difficult to determine from the CRT display. In this case, the voltage amplitude of the resultant display can be detemined accurately only if the amplitude of the signal applied to either channel is known.

Precautions. The following general precautions should be observed when using the ADD mode.

1. Do not exceed the input voltage rating of the Type 453.
2. Do not apply signals that exceed on equivalent of about 20 times the VOLTS/DIV switch setting. For example, with a VOLTS/DIV switch setting of .5, the voltage applied to that channel should not exceed about 10 volts. Larger voltages may distort the display.
3. Use vertical POSITION control settings which most nearly position the signal of each channel to mid-screen when viewed in either the CH 1 or CH 2 positions of the MODE switch. This insures the greatest dynamic range for ADD mode operation.
4. For similiar response from each channel, set both Input Coupling switches to the same position.

## Trigger Source

INT. For most applications, the sweep can be triggered intemally. In the INT position of the Triggering SOURCE switch, the trigger signal is obtained from the Vertical Deflection System. The TRIGGER switch provides further selection of the intemal trigger signal; obtained from the Channel 1 signal in the CH 1 ONLY position, or from the displayed signal when in the NORM position. For singletrace displays of either channel, the NORM position provides the most convenient operation. However, for dualtrace displays special considerations must be made to provide the correct display. Set Dual-Trace Operation in this section for dual-trace triggering information.

UNE. The LINE position of the SOURCE switch connects a sample of the power-line frequency to the Trigger Generator circuit. Line triggering is useful when the input signal is time-related to the line frequency. It is also useful for providing a stable display of a line-frequency component in a complex waveform.

EXT. An extemal signal conected to the EXT TRIG INPUT connector can be used to trigger the sweep in the EXT position of the Triggering SOURCE switch. The extemal signal must be time-related to the displayed signal for a stable display. An extemal trigger signal can be used to provide a triggered display when the intemal signal is too low in amplitude for correct triggening, or contains signal components on which it is not desired to trigger. It is also useful when signal tracing in a mplifiers, phase-shift networks, waveshaping circuits, etc. The signal from a single point in the circuit under test can be connected to the EXT TRIG INPUT connector through a signal probe or cable. The sweep is then triggered by the same signal at all times and allows amplitude, time relationship or waveshape changes of signals at various points in the circuit to be examined without resetting the trigger controls.

EXT $\div 10$. Operation in the EXT $\div 10$ position is the same as described for EXT except that the extemal triggering signal is attenuated 10 times. Attenuation of high-a mplitude extemal triggering signals is desirable to broaden the range of the Triggering LEVEL control. When the COUPLING switch is set to LF REJ, attenuation is about 20:1.

## Trigger Coupling

Four methods of coupling the trigger signal to the trigger circuits can be selected with the Triggering COUPLING switches. Each position permits selection or rejection of the
frequency components of the trigger signal which can trigger the sweep.

AC. The AC position blocks the DC component of the trigger signal. Signals with low-frequency components below about 30 hertz are attenuated. In general, AC coupling can be used for most applications. However, if the trigger signal contains unwanted components or if the sweep is to be triggered at a low repetition rate or a DC level, one of the remaining COUPLING switch positions will provide a better display.

The triggering point in the AC position depends on the average voltage level of the trigger signal. If the trigger signals occur in a random fashion, the average voltage level will vary, causing the triggering point to vary also. This shift of the triggering point may be enough so it is impossible to maintain a stable display. In such cases, use DC coupling.

LFREJ. In the LF REJ position, DC is rejected and signals below about 30 kilohertz are attenuated. Therefore, the sweep will be triggered only by the higher-frequency components of the signal. This position is particularly useful for providing stable triggering if the trigger signal contains line-frequency components. Also, in the ALT position of the MODE switch, the LF REJ position provides the best display at high sweep rates when comparing two unrelated signals (TRIGGER switch set to NORM).

HF REJ. The HF REJ position passes all low-frequency signals between about 30 hertz and 50 kilohertz. DC is rejected and signals outside the given range are attenuated. When triggering from complex waveforms, this position is useful for providing stable display of low-frequency components.
DC. DC coupling can be used to provide stable triggering with low-frequency signals which would be attenuated in the AC position, or with low-repetition rate signals. The LEVEL control can be adjusted to provide triggering at the desired DC level on the waveform. When using intemal triggering, the setting of the Channel 1 and 2 POSITION controls affects the DC trigger level.

DC trigger coupling should not be used in the ALT dualtrace mode if the TRIGGER switch is set to NORM. If used, the sweep will trigger on the DC level of one trace and then either lock out completely or free run on the other trace. Correct DC triggening for this mode can be obtained with the TRIGGER switch set to CH 1 ONLY.

## Trigger Slope

The triggening SLOPE switch detemines whether the trigger circuit responds on the positive-going or negative-going portion of the trigger signal. When the SLOPE switch is in the + (positive-going) position, the display starts with the positive-going portion of the waveform; in the - (negativegoing) position, the display starts with the negative-going portion of the waveform (se Fiq. 2-8]. When several cycles of a signal appear in the display, the setting of the SLOPE switch is often unimportant. However, if only a certain portion of a cycle is to be displayed, correct setting of the SLOPE switch is important to provide a display which starts on the desired slope of the input signal.


Fig. 2-8. Effects of Triggering LEVEL control and SLOPE switch.

## Trigger Level

The Triggering LEVEL control determines the voltage level on the trigger signal at which the sweep is triggered. When the LEVEL control is set in the + region, the trigger circuit responds at a more positive point on the trigger signal. When the LEVEL control is set in the - region, the trigger circuit responds at a more negative point on the trigger signal. Fig. 2-8 illustrates this effect with different settings of the SLOPE switch.

To set the LEVEL control, first select the Triggering SOURCE, COUPLING and SLOPE. Then set the LEVEL control fully counterclockwise ond rotate it clockwise until the display starts at the desired point.

## High-Frequency Stability

The HF STAB control (A only) is used to provide a stable display of high-frequency signals. If a stable display cannot be obtained using the A LEVEL control (trigger signal must have adequate amplitude), adjust the HF STAB control for minimum horizontal jitter in the display. This control has little effect with low-frequency signals.

## A Sweep Triggered Light

The A SWEEP TRIG'D light provides a convenient indication of the condition of the A Triggering circuit. If the A Triggering controls are correctly adjusted with an adequate trigger signal applied, the light is on. However, if the A LEVEL control is misadjusted, the A COUPLING or A SOURCE switches incorrectly set or the trigger signal too low in omplitude, the A SWEEP TRIG'D light will be off. This feature can be used as a general indication of correct triggering. It is particularly useful when setting up the trigger circuits when a trigger signal is available without a trace displayed on the CRT and it also indicates that the A sweep is correctly triggered when operating in the DELAYED SWEEP (B) mode.

## A Sweep Mode

AUTO TRIG. The AUTO TRIG position of the A SWEEP MODE switch provides a stable display when the A LEVEL control is correctly set (see Trigger Level in this section] and a trigger signal is available. The A SWEEP TRIG'D light indicates when the A Sweep Generator is triggered.

When the trigger repetition rate is less then about 20 hertz, or in the absence of an adequate trigger signal, the A Sweep Generator free runs to produce a reference trace. When an adequate trigger signal is again applied, the free-running condition ends and the A Sweep Generator is triggered to produce a stable display (with correct A LEVEL control setting.)

NORM TRIG. Operation in the NORM TRIG position when a trigger signal is applied is the same as in the AUTO TRIG position. However, when a trigger signal is not present, the A Sweep Generator remains off and there is no display. The A SWEFP TRIG'D light indicates when the A sweep is triggered. The NORM TRIG mode can be used to display
signals with repetition rates below about 20 hertz. This mode provides an indication of an adequate trigger signal as well as the correctness of trigger control settings, since there is no display without proper triggering. Also, the A SWEEP TRIG'D light is off when the A sweep is not correctly triggered.

SINGLE SWEEP. When the signal to be displayed is not repetitive or varies in amplitude, shape or time, a conventional repetitive display may produce an unstable presentation. To avoid this, use the single-sweep feature of the Type 453. The SINGLE SWEEP mode can also be used to photograph a non-repetitive signal.

To use the SINGLE SWEEP mode, first make sure the trigger circuit will respond to the event to be displayed. Set the A SWEEP MODE switch to AUTO TRIG or NORM TRIG and obtain the best possible display in the normal manner (for random signals set the trigger circuit to trigger on a signal which is a pproximately the same omplitude and frequency as the random signal). Then, set the A SWEEP MODE switch to SINGLE SWEEP and press the RESET button. When the RESET button is pushed, the next trigger pulse initiates the sweep and a single trace will be presented on the screen. After this sweep is complete, the A Sweep Generator is "locked out" until reset. The RESET light located inside the RESET button lights when the A Sweep Generator circuit has been reset and is ready to produce a sweep; it goes out after the sweep is complete. To prepare the circuit for another single-sweep display, press the RESET button again.

## Selecting Sweep Rate

The A AND B TIME/DIV switches select calibrated sweep rates for the Sweep Generators. The A and B VARIABLE controls provide continuously variable sweep rates between the settings of the TIME/DIV switches. Whenever the UNCAL A OR B light is on, the sweep rate of either A or B Sweep Generator, or both, is uncalibrated. The light is off when the A VARIABLE (front panel) and B TIME/DIV VARIABLE (side panel) controls are both set to the CAL position.

The sweep rate of the A Sweep Generator is bracketed by the two black lines on the clear plastic flange of the TME/DIV switch (see Fiq. 2-9). The B Sweep Generator sweep rate is indicated by the dot on the DELAYED SWEEP knob. When the dot on the outer knob is set to the same position as the lines on the inner knob, the two knobs lock together and the sweep rate of both Sweep Generators is changed at the same time. However, when the DELAYED SWEEP knob is pulled outward, the clear plastic flange is disengaged and only the B Sweep Generator sweep rate is changed. This allows changing the delayed sweep rate wihout changing the delay time determined by the A Sweep Generator.

When making time measurements from the graticule, the area between the first-division and ninth-division vertical lines provides the most linear time measurement (se Fig. 2-10). Therefore, the first and last division of the display should not be used for making accurate time measurements. Position the start of the timing area to the first-division vertical line and set the TME/DIV switch so the end of the timing area falls between the first- and ninth-division vertical lines.


Fig. 2-9. A AND B TIME/DIV switch.

## Sweep Magnification

The sweep magnifier expands the sweep ten times. The center division of the unmagnified display is the portion visible on the screen in mognified form [see Fig. 2-11]. Equivalent length of the magnified sweep is about 100 divisions; any 10 division portion may be viewed by adjusting the horizontal POSITION control to bring the desired portion onto the viewing area. The FINE position control is particularly useful when the magnifier is on, as it provides positioning in small increments for more precise control.

To use the magnified sweep, first move the portion of the display which is to be expanded to the center of the graticule. Then set the MAG switch to X10. The FINE position control can be adjusted to position the magnified display


Fig. 2-10. Area of graticule used for accurate time measurements.


Fig. 2-11. Operation of sweep magnifier.
as desired. The light located below the MAG switch is on whenever the magnifier is on.

When the MAG switch is set to X10, the sweep rate is determined by dividing the TME/DIV switch setting by 10. For example, if the TME/DIV switch is set to $.5 \mu \mathrm{~s}$, the magnified sweep rate is 0.05 microsecond/division. The magnified sweep rate must be used for all time measurements when the MAG switch is set to X10. The magnified sweep rate is calibrated when the UNCAL A OR B light is off.

Delayed Sweep (B)
The delayed sweep ( $B$ sweep) is operable in the A INTEN DURING B and DELAYED SWEEP (B) positions of the HORIZ DISPLAY switch. The A sweep rate along with the DELAYTIME MULTIPLER dial setting determines the time that the B sweep is delayed. Sweep rate of the delayed portion is determined by the B TIME/DIV (DELAYED SWEEP) switch setting.

In the A INTEN DURING B position, the display will appear similar to Fig. 2-12A. The amount of delay time between the start of A sweep and the intensified portion is determined by the setting of the A TIME/DIV switch and the DELAY-TIME MULTIPLIER dial.

For example, the delay indicated by the DELAY-TIME MULTIPUER dial setting shown in Fig. 2-1 3 is 3.55; this corresponds to 3.55 CRT divisions of A sweep. This reading multiplied by the setting of the A TIME/DIV switch gives the calibrated delay time before the start of the B sweep (see B Sweep Mode which follows). The intensified portion of the display is produced by the B sweep. The length of


Fig. 2-12. (A) A INTEN DURING B display (DELAY-TIME MULTIPLIER, 2.95; A TME/DIV, . 5 ms ; B TME/DIV, $50 \mu \mathrm{~s}$ ), (B) DELAYED SWEEP (B) display.
this portion is about 10 times the setting of the $B$ TIME/DIV switch.

When the HORIZ DISPLAY switch is set to DELAYED SWEEP (B), only the intensified portion as viewed in the A INTEN DURING B position is displayed on the screen at the sweep rate indicated by the $B$ TIME/DIV switch (see Fiq. 2-12B).


Fig. 2-13. DELAY-TIME MULTIPLIER dial. Reading shown: 3.55 .

B SWEEP MODE. The B SWEEP MODE switch provides two modes of delayed sweep operatien. Fig. 2-14 illustrates the difference between these two modes. In the B STARTS AFIER DELAY TIME position, the B sweep is presented immediately after the delay time (se Fig. 2-14A]. The B sweep is triggered at a selected point on A sweep to provide the delay time ( $B$ sweep essentially free running]. Since the delay time is the same for each sweep, the display appears stable In the TRIGGERABLE AFIER DELAY TME position, the B sweep operates only when it is triggered (by Trigger Circ uits) after the selected delay time (see Fig. 2-IAB). The B Triggring controls operate as described in this section.

Delayed Sweep Operation. To obtain a delayed sweep display use the following procedure.

1. Obtain a stable display with the HORIZ DISPLAY switch set to A.
2. Set the HORIZ DISPLAY switch to A INTEN DURING B.
3. Set the B SWEEP MODE switch to the desired setting. If TRIGGERABLE AFIER DELAY TIME is selected, correct B Triggering is also necessary,
4. Set the delay time with the A TIME/DIV switch and the DELAY-TIME MULTIPUER dial.
5. Pull the DELAYED SWEEP (B TIME/DIV) knob out and set to the desired sweep rate.
6. If the TRIGGERABLE AFTER DELAY TMME position is used, check the display for an intensified portion. Absence of the intensified zone indicates that B sweep is not correctly triggered.
7. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B). The intensified zone shown in the A INTEN DURING B position is now displayed at the sweep rate selected by the $B$ TIME/DIV switch.

Several examples using the delayed sweep feature are given under Basic Applications in this section.

A Sweep Length. The A SWEEP LENGTH control is most useful when used with delayed sweep. As the control is rotated counterclockwise from the FUL position, the length of the A sweep decreases (sweep rate remains constant) until it is about four divisions iong in the counterclockwise position (not in B ENDS A detent). The B ENDS A position produces a display which ends immediately following $B$ sweep if the B sweep ends before the nomal end of A sweep. The A SWEEP LENGTH control is used to increase the repetition rate of delayed sweep displays.

To use the A SWEEP LENGTH control, set the HORIZ DISPLAY switch to A INTEN DURING B and set the delay time and delayed sweep rate in the normal manner. Tum the A SWEEP LENGTH control counterclockwise until the sweep ends immediately following the intensified portion on the display. Now set the HORIZ DISPLAY switch to DELAYED SWEEP (B). This method provides the maximum repetition rate for a given delayed sweep display. In the B ENDS A position, the maximum delayed sweep repetition rate is maintained automatically.


Fig. 2-14. Comparison of the delayed-sweep modes. (A) B STARTS AFTER DELAY TIME, [B) TRIGGERABLE AFTER DELAY TIME. In each display the $B$ sweep is delayed a selected amount of time by $A$ sweep.

## NOTE

Jitter can be introduced into the display and incorrect displays produced through the wrong usage of the A SWEEP LENGTH control. When using this control first obtain the best possible display in the FULL position. Then, set the control for the desired A sweep length. If jitter is evident in the display, readjust the Triggering controls or change the A SWEEP LENGTH control to a position that does not cause jitter.

## External Horizontal Deflection

In some applications, it is desirable to display one signal versus a nother ( $\mathrm{X}-\mathrm{Y}$ ] rather than a gainst time (intemal sweep).

The EXT HORIZ position of the HORIZ DISPLAY switch provides a means for applying an extemal signal to the horizontal amplifier for this type of display.

Two modes of extemal horizontal operation are provided. When the TRIGGER switch is set to CH 1 ONLY, the B SOURCE switch to INT and the B COUPLNG switch to DC, the horizontal deflection is provided by a signal applied to the Channel 1 INPUT connector. The CH 1 VOLTS/DIV switch setting indicates the calibrated horizontal deflection factor (Channel 1 VARIABLE control in-operative). Center the horizontal POSITION control and use the Channel 1 POSITION control for horizontal positioning.

In the EXT and EXT $\div 10$ positions of the B SOURCE switch, extemal horizontal deflection is provided by a signal
applied to the EXT HORIZ input connector (B EXT TRIG INPUT). The signal coupling provided by the B COUPUNG switch] can be used to select or reject components of the extemal horizontal signal (all components of extemal horizontal signal accepted (in DC position). Using this mode of operation, the horizontal deflection factor is uncalibrated. Extemal horizontal deflection factor is about 270 millivolts/ division in the EXT position of the B SOURCE switch and about 2.7 volts/division in the EXT $\div 10$ position.

## A and B Gate

The A and B Gate output connectors (on side panel) provide a rectangular output pulse which is coincident with the sweep time of the respective sweep generator. This rectangular pulse is about +12 volts in amplitude (into high-impedance loads) with pulse duration the same as the respective sweep.

## Intensity Modulation

Intensity (Z-axis) modulation can be used to relate a third item of electrical phenomena to the vertical ( $Y$-axis) and the horizontal (X-axis) coordinates without changing the wave shape. The $Z$-axis modulating signal applied to the CRT circuit changes the intensity of the displayed waveform to provide this display. "Gray scale" intensity modulation can be obtained by applying signals which do not completely blank the display. Large amplitude signals of the correct polarity will completely blank the display; the sharpest display is provided by signals with a fast rise and fall. The voltage amplitude required for visible trace modulation depends upon the setting of the INTENSITY control. At normal intensity level, a five-volt peak-to-peak signal produces a visible change in brightness. When the Z AXIS INPUT is not in use, keep the ground strap in place to prevent changes in trace intensity due to extraneous noise.

Time markers applied to the Z AXIS INPUT connector provide a direct time reference on the display. With uncalibrated horizontal sweep or extemal horizontal mode operation, the time markers provide a means of reading time directly from the display. However, if the markers are not time-related to the displayed waveform, a single-sweep display should be used (for intemal sweep only) to provide a stable display.

## Calibrator

The one-kilohertz square-wave Calibrator of the Type 453 provides a convenient signal source for checking basic vertical gain and sweep timing. However, to provide maximum measurement acuracy, the adjustment procedure given in the Calibration section of this manual should be used. The Calibrator output signal is also very useful for adjusting probe compensation as described in the probe instruction manual. In addition, the calibrator can be used as a convenient signal source for application to extemal equipment.

Voltage. The Calibrator provides accurate peak-to-peak square wave voltages of 0.1 and 1 volt into a high impedance load. Voltage range is selected by the CALBRATOR switch on the side panel. Output resistance is about 200 ohms in the 1 V position and about 20 ohms in the 0.1 V
position. The actual voltage across an extemal load resistor can be calculated in the same manner as with any series resistor combination (necessary only if the load resistance is less than about 50 kilohms).

Current. The current loop, located on the side panel, provides a five milliampere peak-to-peak square-wave current which can be used to check and calibrate currentmeasuring probe systems. This current signal is obtained by clipping the probe around the current loop. Current is constant through the loop in either position of the Calibrator switch. The arrow above the PROBE LOOP indicates conventional current flow; i.e., from + to -.

Frequency. The Calibrator circuit uses frequency-stable components to maintain accurate frequency and constant duty cycle. Thus the Calibrator can be used for checking the basic sweep timing of the horizontal system.

Wave shape. The square-wave output signal of the Calibrator can be used asa reference wave shape when checking or adjusting the compensation of passive, high-resistance probes. Since the square-wave output from the Calibrator has a flat top, any distortion in the displayed waveform is due to the probe compensation.

## BASIC APPLICATIONS

## General

The following information describes the procedure and technique for making basic measurements with a Type 453 Oscilloscope. These applications are not described in detail since each application must be adapted to the requirements of the individual measurements. Familiarity with the Type 453 will permit these basic techniques to be applied to a wide variety of uses.

## Peak-to-Peak Voltage Measurements-AC

To make a peak-to-peak voltage measurement, use the following procedure:

1. Connect the signal to either INPUT connector.
2. Set the MODE switch to display the channel used.
3. Set the VOLTS/DIV switch to display about five divisions of the waveform.
4. Set the Input Coupling switch to AC.

## NOTE

For low-frequency signals below about 16 hertz, use the DC position.
5. Set the A Triggering controls to obtain a stable display. Set the TMME/DIV switch to a position that displays several cycles of the waveform.
6. Tum the vertical POSITION control so the lower portion of the waveform coincides with one of the graticule lines below the center horizontal line, and the top of the waveform is an the viewing area. Move the display with the horizontal POSITION control so one of the upper peaks lies near the center vertical line (se Fig. 2-1b).
7. Measure the divisions of vertical deflection from peak to peak. Make sure the VARIABLE VOLTS/DIV control is in the CAL position.

## NOTE

This technique may also be used to make measurements between two points on the waveform rather than peak to peak.
8. Multiply the distance measured in step 7 by the VOLTS/ DIV switch setting. Also include the attenuation factor of the probe, if any.

Example. Assume a peak-to-peak vertical deflection of 4.6 divisions (see Fig. 2-15) using a 10X attenuator probe and a VOLTS/DIV switch setting of .5 .

Using the formula:

$$
\begin{gathered}
\text { Volts } \\
\text { ak to Peak } \\
\underset{\text { deflection }}{\text { (divisions) }}
\end{gathered} \times \underset{\text { setting }}{\text { voltical }} \times \underset{\text { attenuation }}{\text { factor }}
$$

Substituting the given values:

$$
\text { Volts Peak to Peak }=4.6 \times 0.5 \mathrm{~V} \times 10
$$

The peak-to-peak voltage is 23 volts.


Fig. 2-15. Measuring peak-to-peak voltage of a waveform.

Instantaneous Voltage Measurements-DC
To measure the DC level at a given point on a waveform, use the following procedure:

1. Connect the signal to either INPUT connector.
2. Set the MODE switch to display the channel used.
3. Set the VOLTS/DIV switch to display about five divisions of the waveform.
4. Set the Input Coupling switch to GND.
5. Set the A SWEEP MODE switch to AUTO TRIG.
6. Position the trace to the bottom line of the graticule or other reference line. If the voltage is negative with respect to ground, position the trace to the top line of the graticule.

Do not move the vertical POSTION control after this reference line has been established.

## NOTE

To measure a voltage level with respect to a voltage rather than ground, make the following changes in step 6. Set the Input Coupling switch to DC and apply the reference voltage to the $\mathbb{N}$ PUT connector. Then position the trace to the reference line.
7. Set the Input Coupling switch to DC. The ground reference line can be checked at any time by switching to the GND position (except when using a DC reference voltage).
8. Set the A Triggering controls to obtain a stable display. Set the TIME/DIV switch to a setting that displays several cycles of the signal.
9. Measure the distance in divisions between the reference line and the point on the waveform at which the DC level is to be measured. For example, in Fiq. 2-16 the measurement is made between the reference line and point $A$.
10. Establish the polarity of the signal. If the waveform is above the reference line, the voltage is positive; below the line, negative (when the INVERT switch is pushed in if using Channel 2 ).
11. Multiply the distance measured in step 9 by the VOLTS/ DIV switch setting. Include the attenuation factor of the probe, if any.

Example. Assume that the vertical distance measured is 4.6 divisions (se Fig. 216), the waveform is above the reference line, using a 10X attenuator probe and a VOLTS/ DIV setting of 2.

Using the formula:

## Instantaneous <br> Voltage

$\begin{gathered}\begin{array}{c}\text { vertical } \\ \text { distance } \\ \text { (divisions] }\end{array}\end{gathered} \times$ polarity $\times \underset{\text { setting }}{\text { VOLTS/DIV }} \times \begin{gathered}\text { probe } \\ \text { attenvation } \\ \text { factor }\end{gathered}$
Substituting the given values:

$$
\begin{gathered}
\text { Instantaneous } \\
\text { Voltage }
\end{gathered}=4.6 \times+1 \times 2 \mathrm{X} \times 10
$$

The instantaneous voltage is +92 volts.

## Voltage Comparison Measurements

In some applications it may be necessary to establish a set of deflection factors other than those indicated by the VOLTS/DIV switch. This is useful for comparing signals to a reference voltage amplitude. To establish a new set of deflection factors based upon a specific reference amplitude, proceed as follows:

1. Apply the reference signal of known amplitude to either INPUT conector. Set the MODE switch to display the channel used. Using the VOLTS/DIV switch and the VARIABLE control, adjust the display for an exact number of divisions. Do not move the VARIABLE VOLTS/DIV control after obtaining the desired deflection.


Fig. 2-16. Measuring instantaneous $D C$ voltage with respect to a reference.
2. Divide the amplitude of the reference signal (volts) by the product of the deflection in divisions (established in step 1] and the VOLTS/DIV switch setting. This is the Deflection Conversion Factor.
Deflection

Conversion $=$| reference signal amplitude (volts) |
| ---: |
| Factor | deflection (divisions) $\times$ VOLTS/DIV setting

3. To establish an Adjusted Deflection Factor at any setting of the VOLTS/DIV switch, multiply the VOLTS/DIV switch setting by the Deflection Conversion Factor established in step 2.

$$
\begin{aligned}
& \text { Adlusted } \\
& \text { Deflection }=\text { VOLTS/DIV } \\
& \text { Factor }
\end{aligned} \times \begin{gathered}
\text { Deflection } \\
\text { Conversion } \\
\text { Factor }
\end{gathered}
$$

This Adjusted Deflection Factor applies only to the channel used and is correct only if the VARIABLE VOLTS/DIV control is not moved from the position set in step 1.
4. To determine the peak to peak amplitude of a signal compared to a reference, disconnect the reference and apply the signal to the INPUT connector.
5. Set the VOLTS/ DIV switch to a setting that will provide sufficient deflection to make the measurement. Do not readiust the VARIABLE VOLTS/DIV control.
6. Measure the vertical deflection in divisions and determine the amplitude by the following formula:

$$
\underset{\text { Amplitude }}{\text { Signal }}=\underset{\substack{\text { Deflection } \\
\text { Fictor }}}{\text { Adisted }} \times \begin{gathered}
\text { deflection } \\
\text { (divisions) }
\end{gathered}
$$

Example. Assume a reference signal amplitude of 30 volts, a VOLTS/DIV setting of 5 and a deflection of 4 divisions. Substituting these values in the Deflection Conversion Factor formula (step 2):

$$
\begin{gathered}
\text { Deflection } \\
\text { Conversion } \\
\text { Factor }
\end{gathered}=\frac{30 \mathrm{~V}}{4 \times 5 \mathrm{~V}}=1.5
$$

Then, with a VOLTS/ DIV switch setting of 10, the Adjusted Deflection Factor (step 3) is:

Adjusted
Deflection $=10 \mathrm{~V}$ X $1.5=15$ volts/division
Factor
To determine the peak-to-peak amplitude of an applied signal which produces a vertical deflection of 5 divisions, use the Signal Amplitude formula (step 6):


## Time-Duration Measurements

To measure time between two points on a waveform, use the following procedure.

1. Connect the signal to either INPUT connector.
2. Set the MODE switch to display the channel used.
3. Set the VOLTS/DIV switch to display about five divisions of the waveform.
4. Set the A Triggering controls to obtain a stable display.
5. Set the TMME/DIV switch to the fastest sweep rate that displays less than eight divisions between the time measurement points (see Fia. 2-17). (See the topic entitled Selecting Sweep Rate in this section conceming non-linearity of first and last divisions of display.)
6. Adjust the vertical POSITION control to move the points between which the time measurement is made to the center horizontal line.
7. Adiust the horizontal POSITION control to center the display within the center eight divisions of the graticule.
8. Measure the horizontal distance between the time measurement points. Be sure the A VARIABLE control is set to CAL.
9. Multiply the distance measured in step 8 by the setting of the TME/DIV switch. If sweep magnification is used, divide this answer by 10.

Example. Assume that the distance between the time measurement points is 5 divisions (se Fig. 2-17) and the TIME/DIV switch is set to .1 ms with the magnifier off.

Using the formula:

$$
\text { Time Duration }=\frac{\begin{array}{c}
\text { horizontal } \\
\text { distance } \\
\text { (divisions) }
\end{array} \times \begin{array}{c}
\text { TIME/DIV } \\
\text { setting }
\end{array}}{\text { magnification }}
$$

Substituting the given values:

$$
\text { Time Duration }=\frac{5 \times 0.1 \mathrm{~ms}}{1}
$$

The time duration is 0.5 milliseconds.

## Frequency Measurements

The time measurement technique can also be used to measure the frequency of a signal. The frequency of a peri-odically-recurrent signal is the reciprocal of the time duration of one cycle.


Fig. 2-17. Measuring the time duration between points on a waveform.

1. Measure the time duration of one cycle of the waveform as described in the previous application.
2. Take the reciprocal of the time duration to determine the frequency.

Example. The frequency of the signal shown in Fig. 2-17 which has a time duration of 0.5 milliseconds is:

$$
\text { Frequency }=\frac{1}{\text { time duration }}=\frac{1}{0.5 \mathrm{~ms}}=2 \mathrm{kHz}
$$

## Risetime Measurements

Risetime measurements employ basically the same techniques as time-duration measurements. The main difference is the points between which the measurement is mode. The following procedure gives the basic method of measuring risetime between the $10 \%$ and $90 \%$ points of the waveform. Falltime can be measured in the same manner on the trailing edge of the waveform.

1. Connect the signal to either INPUT connector.
2. Set the MODE switch to display the channel used.
3. Set the VOLTS/DIV switch and the VARIABLE control to produce a display an exact number of divisions in amplitude.
4. Center the display about the center horizontal line.
5. Set the A Triggering controls to obtain a stable display.
6. Set the TMME/DIV switch to the fastest sweep rate that displays less than eight divisions between thel $10 \%$ and $90 \%$ points on the waveform.
7. Determine the $10 \%$ and $90 \%$ points on the rising portion of the waveform. The figures given in Table 2-2 are for the points $10 \%$ up from the start of the rising portion and $10 \%$ down from the top of the rising portion ( $90 \%$ point).
8. Adiust the horizontal POSTION control to move the $10 \%$ point of the waveform to the first graticule line. For

| Vertical <br> display <br> (divisions) | Divisions vertically <br> points |  <br> $90 \%$ points |
| :---: | :---: | :---: |
| 4 | 0.4 and 3.6 divisions | 3.2 |
| 5 | 0.5 and 3.5 divisions | 4.0 |
| 6 | 0.6 and 3.4 divisions | 4.8 |

example, with a five-division display as shown in_-ig. 2-18, the $10 \%$ point is 0.5 division up from the start of the rising portion.
9. Meosure the horizontal distance between the $10 \%$ and $90 \%$ points. Be sure the A VARIABLE control is set to CAL
10. Multiply the distance measured in step 8 by the setting of the TIME/DIV switch. If sweep magnification is used, divide this answer by 10.

Example. Assume that the horizontal distance between the $10 \%$ and $90 \%$ points is four divisions (see Fig. 2-18) and the TME/DIV switch is set to 1 us with the MAG switch set to X10.

Applying the time duration formula to risetime:

$\underset{\text { (Time Duration) }}{\text { Risetime }}=\frac{$|  horizontal  |
| :---: |
|  distance  |
|  (divisions)  |$\times$|  TIME/DIV  |
| :---: |
|  setting  |}{magnification}

Substituting the given values:
Risetime $=\frac{4 \times 1 \mu \mathrm{~s}}{10}$
The risetime is 0.4 mic rosecond.


Fig. 2-18. Measuring risetime.

## Time-Difference Measurements

The calibrated sweep rate and dual-trace features of the Type 453 allow measurement of time difference between two separate events. To meosure time difference, use the following procedure.

```
TM 11-6625-1722-15
```

1. Set the Input Coupling switches to the desired coupling positions.
2. Set the MODE switches to either CHOP or ALT. In general, CHOP is more suitable for low-frequency signals and the ALT position is more suitable for high-frequency signals. More information on determining the mode is given under Dual-Trace Operation in this section.
3. Set the TRIGGER switch to CH 1 ONLY
4. Connect the reference signal to Channel 1 INPUT and the comparison signal to Channel 2 INPUT. The reference signal should precede the comparison signal in time. Use coaxial cables or probes which have equal time delay to connect the signals to the INPUT connectors.
5. If the signals are of opposite polarity, pull out the INVERT switch to invert the Channel 2 display (signal may be of opposite polanty due to $180^{\circ}$ time difference; if so, take into account in final calculation).
6. Set the VOLTS/DIV switches to produce four-or fivedivision displays.
7. Set the A LEVEL control for a stable display
8. If possible, set the TIME/DIV switch for a sweep rate which shows three or more divisions between the two waveforms.
9. Adlust the vertical POSTION controls to center each waveform (or the points on the display between which the measurement is made) in relation to the center horizontal line.
10. Adjust the horizontal POSITION control so the Channel 1 (reference) waveform crosses the center horizontal line at a vertical graticule line.
11. Measure the horizontal difference between the Channel 1 wavefarm and the Channel 2 waveform (se Fig. 2-19).
12. Multiply the measured difference by the setting of the TME/DIV switch. If sweep magnification is used, divide this answer by 10 .

Example. Assume that the TMME/DIV switch is set to 50 $\mu s$, the MAG switch to X10 and the horizontal difference between waveforms is 4.5 divisions (se Fig. 2-1 3 ).
Using the formula:

$$
\text { Time Delay }=\frac{\begin{array}{c}
\text { TIME/DIV } \\
\text { setting }
\end{array} \times \begin{array}{c}
\text { horizontal } \\
\text { difference } \\
\text { (divisions) }
\end{array}}{\text { magnification }}
$$

Substituting the given values:

$$
\text { Time Delay }=\frac{50 \mu \mathrm{~s} \times 4.5}{10}
$$

The time delay is 22.5 microseconds.

## Delayed Sweep Time Measurements

The delayed sweep mode can be used to make accurate time measurements. The following measurement determines the time difference between two pulses displayed on the same trace. This application may also be used to measure


Fig. 2-19. Measuring time difference between two pulses.
time difference from two different sources (dual-trace) or to measure time duration of a single pulse. Se Section 11 for measurement accuracy.

1. Connect the signal to either INPUT connector. Set the MODE switch to display the channel used.
2. Set the VOLTS/DIV switch to produce a display about four divisions in amplitude.
3. Adjust the A Triggering controls for a stable display.
4. If possible, set the A TIME/DIV switch to a sweep rate which displays about eight divisions between the pulses.
5. Set the HORIZ DISPLAY switch to A INTEN DURING B and the B SWEEP MODE switch to B STARTS AFIER DELAY TME.
6. Set the B TME/DIV switch to a setting $1 / 100$ of the A TIME/DIV sweep rate. This produces an intensified portion about 0.1 division in length.

## NOTE

Do not change the A LEVEL control setting or the horizontal POSITION control setting in the following steps as the measurement accuracy will be affected.
7. Turn the DELAY-TIME MULTIPLIER dial to move the intensified portion to the first pulse.
8. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
9. Adiust the DELAY-TIME MULTIPLER dial to move the pulse (or the rising portion) to the center vertical line. Note the setting of the DELAY-TIME MULTIPLER dial.
10. Tum the DELAY-TIME MULTIPUER dial clockwise until the second pulse is positioned to this same point (if several pulses are displayed, retum to the A INTEN DURING B position to locate the correct pulse). Again note the dial setting.
11. Subtract the first dial setting from the second and multiply by the delay time shown by the A TIME/DIV switch. This is the time interval between the pulses.

Example. Assume the first dial setting is 1.31 and the second dial setting is 8.81 with the TIME/DIV switch set to 0.2 mic rosecond (se Fiq. 2-20].

Using the formula:

$$
\begin{aligned}
& \text { Time Difference } \\
& \text { (delayed sweep) }
\end{aligned}
$$

delay time
[second dial setting - first dial sefting] $\times$ (A TIME/DIV setting)

Substituting the given values:
Time Difference $=[8.81$ - 1.31] X $0.2 \mu \mathrm{~s}$
The time difference is 1.5 microseconds.


Fig. 2-20. Measuring time difference using delayed sweep.

## Delayed Sweep Magnification

The delayed sweep feature of the Type 453 can be used to provide higher apparent magnification than is provided by the MAG switch. The sweep rate of the DELAYED SWEEP (B sweep) is not actually increased; the apparent magnification is the result of delaying the B sweep an amount of time selected by the A TIME/DIV switch and the DELAY-TIME MULTIPUER dial before the display is presented at the sweep rate selected by the B TME/DIV switch. The following methods uses the B STARTS AFIER DELAY TMME position to allow the delayed portion to be positioned with the DELAYTIME MULTIPLER dial. If there is too much jitter in the delay-
ed display, use the Triggered Delayed Sweep Magnification procedure.

1. Connect the signal to either INPUT connector. Set the MODE switch to display the channel used.
2. Set the VOLTS/DIV switch to produce a display about 4 divisions in amplitude.
3. Adjust the A Triggering controls for a stable display.
4. Set the A TIME/DIV switch to a sweep rate which displays the complete waveform.
5. Set the HORIZ DISPLAY switch ta A INTEN DURING B and the B SWEEP MODE switch to B STARTS AFIER DELAY TMME.
6. Position the start of the intensified portion with the DELAY-TIME MULTIPUER dial to the part of the display ta be magnified.
7. Set the $B$ TME/DIV switch to a setting which intensifies the full portion to be magnified. The start of the intensified trace will remain as positioned above.
8. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B].
9. Time measurements can be made from the display in the conventional manner. Sweep rate is determined by the setting of the B TMME/DIV switch.
10. The apparent sweep magnification can be calculated by dividing the A TMME/DIV switch setting by the B TME/DIV switch setting.

Example: The apparent magnification of the display shown in Fiq. 2-21 with an A TIME/DIV switch setting of .1 ms and a B TIME/DIV switch setting of $1 \mu \mathrm{~s}$ is:

$$
\begin{gathered}
\text { Apparent Magnification } \\
\text { (delayed sweep) }
\end{gathered}=\frac{\text { A TIME/DIV setting }}{\text { B TIME/DIV setting }}
$$

Substituting the given values:
$\underset{\text { Magnification }}{\text { Apparent }}=\frac{1 \times 10^{-4}}{1 \times 10^{-6}}$
The apparent magnification is 100 times.
Triggered Delayed Sweep Magnification. The delayed sweep magnification method just described may produce too much jitter at high apparent magnification ranges. The TRIGGERABLE AFIER DELAY TIME position of the B SWEEP MODE switch provides a more stable display since the delayed display is triggered at the same point each time.

1. Set up the display as given in steps 1 through 7 described above.
2. Set the B SWEEP MODE switch to TRIGGERABLE AFIER DELAY TIME.
3. Adiust the B LEVEL control so the intensified portion on the trace is stable. (If an intensified portion cannot be obtained, see step 4.)
4. Inability to intensify the desired portion indicates that the B Triggering controls are incorrectly set or the signal does not meet the triggering requirements. If the condition cannot be remedied with the B Triggering controls or by


Fig. 2-21. Using delayed sweep for sweep magnification.
increasing the display amplitude (lower VOLTS/DIV setting), extemally trigger B sweep.
5. When the correct portion is intensified, set the HORIZ DISPLAY switch to DELAYED SWEEP (B). Slight readjustment of the B LEVEL control may be necessary for a stable display.
6. Measurement and magnification are as described above.

## Displaying Complex Signals Using Delayed

 SweepComplex signals often consist of a number of individual events of differing amplitudes. Since the trigger circuits are sensitive to changes in signal amplitude, a stable display can normally be obtained only when the sweep is triggered by the event(s) having the greatest amplitude. However, this may not produce the desired display of a lower amplitude event which follows the triggering event. The delayed sweep feature provides a means of delaying the start of the $B$ sweep by a selected amount following the event which triggers the A Sweep Generator. Then, the part of the waveform which contains the information of interest can be displayed.

Use the following procedure:

1. Connect the signal to either INPUT connector. Set the MODE switch to display the channel used.
2. Set the VOLTS/DIV switch to produce a display about four divisions in omplitude
3. Adjust the A Triggering controls for a stable display.
4. Set the A TIME/DIV switch to a sweep rate which displays the complete waveform.
5. Set the HORIZ DISPLAY switch to A INTEN DURING B and the B SWEEP MODE switch to B STARTS AFIER DELAY TME.
6. Position the start of the intensified portion with the DELAY-TIME MULTIPUER dial to the part of the display to be magnified.
7. Set the B TME/DIV switch to a setting which intensifies the full portion to be magnified. The start of the intensified trace will remain as positioned above.
8. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
9. Time measurements can be made from the display in the conventional manner. Sweep rate is determined by the setting of the B TIME/DIV switch.

Example. Fig. 2-22 shows a complex waveform as displayed on the CRT. The circled portion of the waveform cannot be viewed in any greater detail because the sweep is triggered by the larger amplitude pulses at the start of the display and a faster sweep rate moves this area of the waveform off the viewing area. The second waveform shows the area of interest magnified 10 times using Delayed Sweep. The DELAY-TMME MULTIPLER dial has been adjusted so the delayed sweep starts just before the area of interest.

## Pulse Jitter Measurements

In some applications it is necessary to measure the amount of jitter on the leading edge of a pulse, or jitter between pulses.

Use the following procedure:

1. Connect the signal to either INPUT connector. Set the MODE switch to display the channel used.
2. Set the VOLTS/DIV switch to display about four divisions of the waveform.
3. Set the A TIME/DIV switch to a sweep rate which displays the complete waveform.
4. Set the A Triggering controls to obtain as stable a display as possible,
5. Set the HORIZ DISPLAY switch to A INTEN DURING $B$ and the B SWEEP MODE switch to B STARTS AFIER DELAY TME.
6. Position the start of the intensified portion with the DELAY-TME MULTPLER dial so the pulse to be measured is intensified.
7. Set the B TME/DIV switch to a setting which intensifies the full portion of the pulse that shows jitter.
8. Set the B SWEEP MODE switch to TRIGGERABLE AFIER DELAY TME.

(A) This portion of display cannot be viewed adequately becouse $A$ sweep is triggered on larger amplitude signals af start of display.

(B) Area of inferest displayed by delaying B sweep (B STARTS AFTER DELAY TIME mode).

Fig. 2-22. Displaying a complex signal using delayed sweep.
9. Adiust the B LEVEL control so the intensified portion is as stable as possible.
10. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B). Slight readjustment of the B LEVEL control may be necessary to produce as stable a display as possible.
11. Pulse jitter is shown by horizontal movement of the pulse (take into account inherent jitter of Delayed Sweep). Measure the amount of horizontal movement. Be sure both VARIABLE controls are set to CAL
12. Multiply the distance measured in step 11 by the B TMME/DIV switch setting to obtain pulse iitter in time.

Example. Assume that the horizontal movement is 0.5 divisions (se Fig. 2-2.B), and the B TMME/DIV switch setting is $.5 \mu \mathrm{~s}$.

Using the formula:

$$
\text { Pulse Jitter }=\begin{gathered}
\text { horizontal } \\
\text { iitter } \\
\text { (divisions) }
\end{gathered} \times \times \begin{gathered}
\text { B TIME/DIV } \\
\text { setting }
\end{gathered}
$$

Substituting the given value:
Pulse Jitter $=0.5 \times 0.5 \mu \mathrm{~s}$
The pulse iitter is 0.25 microseconds.


Fig. 2-23. Measuring pulse jitter.

## Delayed Trigger Generator

The B GATE output signal can be used to trigger an external device at a selected delay time after the start of $A$ Sweep. The delay time of the B GATE output signal can be selected by the setting of the DELAY-TIME MULTIPUER dial and A TIME/DIV switch.

A Sweep Triggered Internally. When A sweep is triggered intemally to produce a nomal display, the delayed trigger may be obtained as follows.

1. Obtain a triggered display in the normal manner.
2. Set the HORIZ DISPLAY switch to A INTEN DURING B.
3. Select the amount of delay from the start of A Sweep with the DELAY-TIME MULTIPUER dial. Delay time can be calculated in the normol manner.
4. Set the B SWEEP MODE switch to B STARTS AFIER DELAY TME.
5. Connect the B GATE signal to the extemal equipment.
6. The duration of the B GATE signal is determined by the setting of the B TIME/DIV switch.
7. The extemal equipment will be triggered at the start of the intensified portion if it responds to positive-going triggers, or at the end of the intensified portion if it responds to negative-going triggers.

A Sweep Triggered Extemally. This mode of operation can be used to produce a delayed trigger with or without a corresponding display. Connect the extemal, trigger signal to the A EXT TRIG INPUT connector and set the A SOURCE switch to EXT. Follow the operation given above to obtain the delayed trigger.

## Normal Trigger Generator

Ordinarily, the signal to be displayed also provides the trigger signal for the oscilloscope. In some instances, it may be desirable to reverse this situation and have the oscilloscope trigger the signal source. This can be done by connecting the A GATE signal to the input of the signal source. Set the A LEVEL control fully clockwise, A SWEEP

MODE switch to AUTO TRIG and adjust the A TMME/DIV switch for the desired display. Since the signal source is triggered by a signal that has a fixed time relationship to the sweep, the output of the signal source can be displayed on the CRT as though the Type 453 were triggered in the normal manner (this method does not allow selection of trigger level or coupling).

## Multi-Trace Phase Difference Measurements

Phase comparison between two signals of the same frequency can be made using the dual-trace feature of the Type 453. This method of phase difference measurement can be used up to the frequency limit of the vertical system. To make the comparison, use the following procedure.

1. Set the Input Coupling switches to the same position, depending on the type of coupling desired.
2. Set the MODE switch to either CHOP or ALT. In general, CHOP is more suitable for low-frequency signals and the ALT position is more suitable for high-frequency signals. More information on determining the mode is given under Dual-Trace Operation in this section.
3. Set the TRIGGER switch to CH 1 ONLY.
4. Connect the reference signal to the Channel 1 INPUT connector and the comparison signal to the Channel 2 INPUT connector. The reference signal should precede the comparison signal in time. Use coaxial cables or probes which have equal time delay to connect the signals to the INPUT connectors.
5. If the signals are of opposite polarity, pull the INVERT switch out to invert the Channel 2 display. (Signals may be of opposite polarity due to $180^{\circ}$ phase difference; if so, take this into account in the final calculation.)
6. Set the CH 1 and CH 2 VOLTS/DIV switches and the VARIABLE VOLTS/DIV controls so the displays are equal and about five divisions in amplitude.
7. Set the triggering controls to obtain a stable display.
8. Set the TME/DIV switch to a sweep rate which displays about one cycle of the waveform.
9. Move the waveforms to the center of the graticule with the vertical POSITION controls.
10. Tum the A VARIABLE control until one cycle of the reference signal (Channel 1) occupies exactly eight divisions horizontally (see Fig. 2-24), Each division of the graticule represents $45^{\circ}$ of the cycle $\left[360^{\circ} \div 8\right.$ divisions $=45^{\circ}$ / division). The sweep rate con be stated in tems of degrees as $45^{\circ}$ /division.
11. Measure the horizontal difference between corresponding points on the waveforms.
12. Multip!y the measured distance (in divisions) by $45 \%$ division (sweep rate) to obtain the exact amount of phase difference,

Example. Assume a horizontal difference of 0.6 divisions with a sweep rate of $45 \%$ division as shown ir Fiq. 2-24

Using the formula:

$$
\text { Phase Difference }=\begin{aligned}
& \text { horizontal } \\
& \text { difference } \\
& \text { (divisions) }
\end{aligned} \times \begin{gathered}
\text { sweep rate } \\
\text { (degrees/div) }
\end{gathered}
$$

Substituting the given values:
Phase Difference $=0.6 \times 45^{\circ}$
The phase difference is $27^{\circ}$.

## High Resolution Phase Measurements

More accurate dual-trace phase measurements can be made by increasing the sweep rate (without changing the A VARIABLE control setting). One of the easiest ways to increase the sweep rate is with the MAG switch. Delayed sweep magnification may also be used. The magnified sweep rate is determined by dividing the sweep rate obtained previously by the amount of sweep magnification.


Fig. 2-24. Measuring phase difference.

Example. If the sweep rate were increased 10 times with the magnifier, the magnified sweep rate would be $45^{\circ} /$ division $\div 10=4.5^{\circ} /$ division. Fiq. $2-25$ hows the same signals as used in Fig. 2-24 but with the MAG switch set to X10. With a horizontal difference of six divisions, the phase difference is:

$$
\text { Phase Difference }=\begin{gathered}
\text { horizontal } \\
\text { difference } \\
\text { (divisions) }
\end{gathered} \quad \begin{gathered}
\text { magnified } \\
\text { sweep rate } \\
\text { (degrees/div) }
\end{gathered}
$$

Substituting the given values:
Phase Difference $=6 \times 4.5^{\circ}$.
The phase difference is $27^{\circ}$.

## X-Y Phase Measurements

The X-Y phase measurement method can be used to measure the phase difference between the two signals of the same frequency. This method provides an altemate method of measurement for signal frequencies up to about 100 kilohertz. However, above this frequency the inherent phase


Fig. 2-25. High resolution phase-difference measurement with increased sweep rate.
difference between the vertic al a nd horizontal systems makes accurate phase measurement difficult. In this mode, one of the sine-wave signals provides horizontal deflection (X) while the other signal provides the vertical deflection ( Y ). The phase angle between the two signalscan be determined from the lissajous pattem as follows.

1. Connect one of the sine-wave signals to both the Channel 1 INPUT and the Channel 2 INPUT connectors. (Note: steps 1 through 5 measure inherent phase difference between the $X$ and $Y$ amplifiers to provide a more accurate $X-Y$ phase measurement; not necessary below about 1 kHz ).
2. Set the HORIZ DISPLAY switch to EXT HORIZ Set the TRIGGER switch to CH 1 ONLY and the B SOURCE switch to $\operatorname{INT}$.


Fig. 2-26. Phase-difference measurement from an $X-Y$ display.
3. Position the display to the center of the screen and adjust the VOLTS/DIV switches to produce a display less than 6 divisions vertically ( Y ) and less than 10 divisians horizontally (X). The CH 1 VOLTS/DIV switch controls the horizontal deflection (X) and the CH 2 VOLTS/DIV switch controls the vertical deflection (Y).
4. Center the display in relation to the vertical graticule line. Measure the distances $A$ and $B$ as shown in Fig. 2-26 Distance $A$ is the horizontal measurement between the two points where the trace crosses the center horizontal line. Distance $B$ is the maximum horizontal width of the display.
5. Divide $A$ by $B$ to obtain the sine of the phase angle $(\phi)$ Ibetween the two signals. The angle can then be obtained from a trigonometric table. This is the inherent phase shift of the instrument.
6. Connect the $Y$ signal to Channel 2 INPUT connector. Repeat steps 2 through 5 to measure phase angle. If the dis-


[^0]play appears as a diaganal straight line, the two signals are either in phase (tilted upper right to lower left) or $180^{\circ}$ out of phase (tilted upper left to lower right). If the display is a circle, the signals are $90^{\circ}$ out of phase. Fiq. 2-27 shows the lissajous displays produced between $0^{\circ}$ and $360^{\circ}$. Notice that above $180^{\circ}$ phase shift, the resultant display is the same as at some lower angle.
7. Substract the inherent phase shift from the phase angle $\phi$ to obtain the actual phase difference.

Example. Assume an inherent phase difference of $2^{\circ}$ with a display as shown in Fig. 2-26 where A is 5 divisions and $B$ is 10 divisions.

Using the formula:

$$
\text { Sine } \phi=\frac{A}{B}
$$

Substituting the given values:

$$
\text { Sine } \phi=\frac{5}{10}=0.5
$$

From the trigonometric tables:

$$
\phi=30^{\circ}
$$

To adjust for the phase difference between X and Y amplifiers, subract the inherent phase shift.

$\underset{\text { Actual }}{\text { Phase }}$| Angle |
| :--- |$=\phi-$| inherent |
| :---: |
| phase |
| shift |

Substituting the given value:

> Actual
> Phase $=30^{\circ}-2^{\circ}=28^{\circ}$
> Angle

## Common-Mode Rejection

The ADD feature of the Type 453 can be used to display signals which contain undesirable components. These undesirable components can be eliminated through commonmode rejection. The precautions given under Algebraic Addition should be observed.

1. Connect the signal containing both the desired and undesired information to the Channel 1 INPUT connector.
2. Connect a signal similar to the unwanted portion of the Channel 1 signal to the Channel 2 INPUT connector. For example, in Fig. 2-28a line-frequency signal is connected to Channel 2 to cancel out the line-frequency component of the Channel 1 signal.
3. Set both Input Coupling switches to DC (AC if DC component of input signal is too large).
4. Set the MODE switch to ALT. Set the VOLTS/DIV switches so the signals are about equal in amplitude.
5. Set the TRIGGER switch to NORM
6. Set the MODE switch to ADD. Pull the INVERT switch so the common-mode signals are of opposite polanity.
7. Adjust the CH 2 VOLTS/DIV switch and VARIA8LE control for maximum cancellation of the common-mode signal.
8. The signal which remains should be only the desired portion of the Channel 1 signal. The undesired signal is cancelled out.

Example. An example of this mode of operation is shown in Fig. 2-28. The signal applied to Channel 1 contains unwanted line-frequency components (Fiq. 2-28A). A corresponding line-frequency signal is connected to Channel 2 (Fiq. 2-28B). Fiq. 2-28C shows the desired portion of the signal as displayed when common-mode rejection is used.


Fig. 2-28. Using the $A D D$ feature for common-mode rejection. (A) Channel 1 signal contains desired information along with line-frequency component, (B) Channel 2 signal contains line-frequency only, [C) CRT display using common-mode rejection.

## CIRCUIT DESCRIPTION

## Introduction

This section of the manual contains a description of the circuitry used in the Type 453 Oscilloscope. The description begins with a discussion of the instrument using the basic block diagram shown in Fig. 3-1. Then each circuit is described in detail using a detailed block diagram to show the interconnections between the stages in each major circuit and the relationship of the front-panel controls to the individual stages.

A complete block diagram is located in the Diagrams section at the rear of this manual. This block diagram shows the overall relationship between all of the circuits. Complete schematics of each circuit are also given in the Diagrams section. Refer to these diagrams throughout the following circuit description for electrical values and relationship.

## BLOCK DIAGRAM

## General

The following discussion is provided to aid in understanding the overall concept of the Type 453 before the individual circuits are discussed in detail. A basic block diagram of the Type 453 is show in Fily. 3-1. Only the basic interconnections between the individual blocks are shown on this diagram. Each block represents a major circuit within this instrument. The number on each block refers to the complete circuit diagram which is located at the rear of his manual.

Signals to be displayed on the CRT are applied to either the Channel 1 INPUT and/or the Channel 2 INPUT connectors. The input signals are then amplified by the Channel 1 Vertical Preamp and/or the Channel 2 Vertical Preamp circuits. The VOLTS/DIV switch in each Vertical Preamp circuit provides attenuation, or switches gain, to provide the indicated deflection factor. Each Vertical Preamp circuit also includes separate position, input coupling, gain, variable attenuation and balance controls. A trigger-pickoff stage in the Channel 1 Vertical preamp circuit supplies a sample of the Channel 1 signal to the Trigger Preamp circuit or the CH 1 OUT connector. The output of both Vertical Preamp circuits is connected to the Vertical Switching circuit. This circuit selects the channel(s) to be displayed. An output signal from this circuit is connected to the Z Axis Amplifier circ uit to blank out the between-channel switc hing transients when in the chopped mode af operation. A trigger-pickoff stage at the output of the Vertical Switching circuit provides a sample of the displayed signal(s) to the Trigger Preamp circuit.

The output of the Vertical Switching circuit is connected to the Vertical Output Amplifier through the Delay-Line

Driver stage and the Delay Line. The Vertical Output Amplifier circuit provides the final amplification for the signal before it is connected to the vertical deflection plates of the CRT. This circuit includes the TRACE FINDER switch which compresses the vertical and horizontal deflection within the viewing area to aid in locating an off-secreen display.
The Trigger Preamp circuit provides amplification for the intemal trigger signal selected by the TRIGGER switch. This intemal trigger signal is selected from either the Channel 1 Vertical Preamp circuit or the Vertical Switching circuit. Output from this circuit is connected to the A Trigger Generator circuit and the B Trigger Generator circuit.

The A and B Trigger Generator circuits produce an output pulse which initiates the sweep signal produced by the $A$ or B Sweep Generator circuits. The input signal to the A and B Trigger Generator circuits can be individually selected from the intemal trigger signal from the Trigger Preamp circuit, an extemal signal applied to the EXT TRIG INPUT connector, or a sample of the line voltage applied to the instrument. Each trigger circ uit contains level, slope, coupling and source controls.

The A Sweep Generator circuit produces a linear sawtooth output signal when initiated by the A Trigger Generator circuit. The slope of the sawtooth produced by the A Sweep Generator circuit is controlled by the A TIME/DIV switch. The operating mode of the A Sweep Generator circuit is controlled by the A SWEEP MODE switch. In the AUTO TRIG position, the absence of an adequate trigger signal causes the sweep to free run. In the NORM TRIG position, a horizontal sweep is presented only when correctly triggered by an adequate trigger signal. The SINGLE SWEEP position allows one (and only one) sweep to be initiated after the circuit is reset with the RESET button.

The B Sweep Generator circuit is basically the same as the A Sweep Generator circuit. However, this circuit only produces a sawtooth output signal after a delay time determined by the A TME/DIV switch and the DELAY-TME MULTIPLIER dial. If the B SWEEP MODE switch is set to the B STARTS AFIER DELAY TME position, the B Sweep Generator begins to produce the sweep immediately following the selected delay time. If this switch is in the TRIGGERABLE AFIER DELAY TIME position, the B Sweep Generator circuit does not produce a sweep until it receives a trigger pulse from the B Trigger Generator circuit after the selected delay time.

The output of either the A or B Sweep Generator circuit is amplified by the Horizontal Amplifier circuit to produce horizontal deflection for the CRT in all positions of the HORIZ DISPLAY switch except EXT HORIZ This circuit contains a 10 times magnifier to increase the sweep rate ten times in any A or B TME/DIV switch position. Other horizontal deflection signals can be connected to the Horizontal


Fig. 3-1. Basic block diagram of the Type 453.

Amplifier by using the EXT-HORIZ mode of operation. When the B SOURCE switch is set to INT, the $X$ signal is connected to the Horizontal Amplifier circuit through the CH 1 Vertical Preamp circuit, the Trigger Preamp circuit and the B Trigger Generator circuit (HORIZ DISPLAY switch set to EXT HORIZ, B SOURCE switch set to INT and the TRIGGER switch set to CH 1 ONLY). In the EXT or EXT $\div 10$ position of the B SOURCE switch, the $X$ signal is obtained from a signal connected to the B EXT TRIG INPUT or EXT HORIZ connector.

The Z Axis Amplifier circuit determines the CRT intensity and blanking. The Z Axis Amplifier circuit sums the current inputs from the INTENSTTY control, Vertical Switching circuit (chopped blanking), A and B Sweep Generator circuits (unblinking) and the extemal Z AXIS INPUT binding post. The output level of the Z Axis Amplifier circuit controls the trace intensity through the CRT Circuit. The CRT Circuit provides the voltages and contains the controls necessary for he operation of the cathode-ray tube.

The Power Supply circuit provides the low-voltage power necessary for operation of this instrument. This voltage is distributed to all of the circuits in the instrument as shown by the Power Distribution diagram. The Calibrator circuit produces a square-wave output with accurate amplitude and frequency which can be used to check the calibration of the instrument and the compensation of probes. The PROBE LOOP provides an accurate current source for calibration of current-measuring probe systems.

## CIRCUIT OPERATION

## General

The following circuit analysis is written around the detailed block diagrams which are given for each major circ uit. These detailed block diagrams give the names of the individual stages within the major circuits and show how they are connected together. The block diagrams also show the inputs and outputs for each major circuit and the relationship of the front-panel controls to the individual stages. The circuit diagrams from which the detailed block diagrams are derived are shown in the Diagrams section of this manual. The names assigned to the individual stages on the detailed block diagrams are used throughout the following discussion.

This section describes the electrical operation and relationship of the circuits in the Type 453. The theory of operation for circuits which are used only in this instrument are described in detail in this discussion. Circuits which are commonly used in the electronics industry are not described in detail. Instead, references are given to textbooks or other source material which describe the complete operation of these circuits.

CHANNEL 1 VERTICAL PREAMP

## General

Input signals for vertical deflection on the CRT can be connected to the channel 1 INPUT connector. In the EXT HORIZ mode of operation, this input signal provides the horizontal (X-axis] deflection [HORIZ DISPLAY switch set to

EXT HORIZ, B SOURCE switch set to INT and TRIGGER switch set to CH 1 ONLY). The Channel 1 Vertical Preamp circuit provides control of input coupling, vertical deflection factor, balance, vertical position and vertical gain. It also contains a stage to provide a sample of the Channel 1 input signal to the Trigger Preamp circuit to provide intemal triggering from the Channel 1 signal only. Fig. 3-2 shows a detailed block diagram of the Channel 1 Vertical Preamp circuit. A schematic of this circuit is shown on diagram 1 at the rear of this manual.

## Input Coupling

Input signals applied to the Channel 1 INPUT connector can be AC-coupled, DC-coupled or intemally disconnected. When the Input Coupling switch, SW1, is in the DC position, the input signal is coupled directly to the Input Attenuator stage. In the AC pasition, the input signal passes through capacitor C1. This capacitor prevents the DC component of the signal from passing to the amplifier. The GND position opens the signal path and the input to the amplifier is connected to ground. This provides a ground reference without the need to disconnect the applied signal from the INPUT connector. Resistor R2, connected across the Input Coupling switch, allows C1 to be precharged in the GND position so the trace remains on screen when switched to the AC position with a high DC level applied.

## Input Attenuator

The effective overall Channel 1 deflection factor of the Type 453 is detemined by the CH 1 VOLTS/DIV switch. In all positions of the CH 1 VOLTS/DIV switch above 20 mV , the basic deflection factor of the Vertical Deflection System is 20 millivolts per division of CRT deflection. To increase this basic deflection factor to the values indicated on the front panel, precision attenuators are switched into the circuit. In the 5 and 10 mV positions, input attenuation is not used. Instead, the gain of the Feedback Amplifier is changed to decrease the deflection factor (see Feedback Amplifier discussion).

For the CH 1 VOLTS/DIV switch positions above 20 mV , the attenuators are switched into the circuit singly or in pairs to produce the vertical deflection factor indicated on the front panel. These attenuators are frequency-compensated voltage dividers. For DC and low-frequency signals, they are primarily resistance dividers and the voltage attenuation is determined by the resistance ratio in the circuit. The reactance of the capacitors in the circuit is so high at low frequencies that their effect is negligible. However, at, higher frequencies, the reactance of the capacitors decreases and the attenuator becomes primarily a capacitance voltage divider.

In addition to providing constant attenuation at all frequencies within the bandwidth of the instrument, the Input Attenuators are designed to maintain the same input RC characteristics (one megohm $\times 20 \mathrm{pF}$ ) for each setting of the CH 1 VOLTS/DIV switch. Each attenuator contains an adjustable series capacitor to provide correct attenuation at high-frequencies and an adjustable shunt capacitor to provide correct input capacitance.

## Input Stage

The Channel 1 signal from the Input Attenuator is connected to the Input Stage through the network C17-C18-C20-R16-R17-R18-R19-R20-R21. R16, R17 and R20 provide the input resistance for this stage. These resistors are part of the attenuation network at all CH 1 VOLTS/DIV switch positions. Variable capacitor C17 adjusts the basic input time constant for a nominal value of one megohm $\times 20 \mathrm{pF}$. The divider action of R16-R17-R20 allows about 98\% of DC and low-frequency signals to pass to the gate of FET (fieldeffect transistor) Q23A. C18 with the stray capacitance in the circuit forms an AC divider which maintains this same voltage division for high-frequency signals. R18 limits the current drive to the gate of Q23A. Diode D18 protects the circuit by clamping the gate of Q23A at about -12.5 volts if a high-amplitude negative signal is applied to the Channel 1 INPUT connector. Over-voltage protection for high-amplitude positive signals is provided by forward conduction of Q23A. The current path is through R23, L23, D36 ond D37.

FET Q23B is a constant current source for Q23A and also provides temperature compensation for Q23A. The STEP ATIEN BAL adjustment, R30, varies the gate level of Q23B to provide a zero-volt level at the emitter of Q34 with no signal applied. With a zero-volt level at the emitter of Q34, the trace position will not change when switching between the 5,10 and 20 mV positions of the CH 1 VOLTS/DIV switch.

DC and low-frequency signals are connected from the source of Q23A to the Feedback Amplifier through R23, L23, Q33 ond R39.

L23 isolates the base of Q33 from the source of FET Q23A, Diodes D34-D35 and D36-D37 limit the dynamic range of the signal at the base of Q33 and prevent the following stages from being damaged by a large voltage swing at the source of Q23A. The signal path for high-frequency signals is through C23, Q43 and C39. High-frequency signals at the emitter of Q43 are connected to the base of Q33 through C38. This allows Q33 to be driven at high frequencies while preventing the base circuitry of Q33 from capacitively loading the input FET, Q23A. C 38 is selected to provide the same amplitude $A C$ and DC signal at the hose of Q33. C24 couples high-frequency information to the junction of R25-R26, thereby reducing the loading at the base of Q43.

## Feedback Amplifier

The Feedback Amplifier, Q34 and Q54, changes the overall gain of the Channel 1 Vertical Preamp to provide the correct deflection factor in the 5 and 10 mV positions of the CH 1 VOLTS/DIV switch. Gain of this stage is detemined by the ratio of R46-R50 to R43, R44 or R45. In the 5 mV position of the CH 1 VOLTS/DIV switch, the network C43A-C 43B-C43CC 43D-C 43E-L43A-R43A-R43C-R43E is connected into the emitter circuit of Q34. The ratio between R46-R50 and R43 provides a gain of obout 10. C43A, C43C, L43A and R43C are adjustable to provide high-frequency peaking for the network. In the 10 mV position, conditions are the same except that the network C44A-C 44B-C44C-L44A-R44A-R44BR44C is connected into the circuit in place of the previous network. The ratio between R46-R50 and R44 provides a gain of about 5 times in this CH 1 VOLTS/DIV switch position. C44A, C44C and R44C provide high frequency peaking for this network. In the 20 mV and higher CH 1 VOLTS/DIV switch
positions, the gain of the Feedback Amplifier is about 2.5 as established by the ratio between R46-R50 and R45. Adjustable capacitor C45A provides high-frequency peaking for the Feedback Amplifier stage. C49 and R49 provide high-frequency damping for the circuit. As mentioned previously, the STEP ATIEN BAL adjustment is set to provide zero volts at the emitter of Q34 when the input is at zero volts. Since there is no voltage difference across the emitter resistors, R43, R44 or R45, changing the value of the resistance does not change the current in the circuit. Therefore, the trace position does not change when switching between the $5 \mathrm{mV}, 10 \mathrm{mV}$ and 20 mV positions of the CH 1 VOLTS/DIV switch if the STEP ATIEN BAL control is correctly adjusted.

Vertical position of the trcce is determined by the setting of the POSITION control, R40. This control changes the current into the emitter of Q34, a low-Impedance point, which results in negligible voltage change at this point. However, the change in current from the POSTION control produces a resultant DC voltage at the output of the Feedback Amplifier stoge to change the vertical position of the trace. The CH 1 Position Center adjustment, R55, is adjusted to provide a centered display when the Channel 1 POSITION control is centered (with a zero-volt DC input level).
Zener diode D53 provides a low-impedance source for Q54. Variable capacitor C54 provides feedback from the collector to the base of Q54 for amplifier stabtllzation. The output signal from the Feedback Amplifler stage is connected to the Paraphrase Amplifier stage and the Channel 1 Trigger Pickoff stage.

## Channel 1 Trigger Pickoff

The signal at the collector of Q54 in the Feedback Amplifier stage is connected to the Channel 1 Trigger Pickoff stage through D58 and R59. This sample of the Channel 1 input signal provides intemal triggering from the Channel 1 signal or X-axis deflection for EXT HORIZ operation. Q63 is conneced as an emitter follower to provide isolation between the Trigger Preamp circuit and the Feedback Amplifier stage. It also provides a minimum load for the Feedback Amplifier stoge and a low output impedance to the Trigger Preamp circuit. D58 provides themal compensation for Q63. The CH 1 Trigger DC Level adjustment, R60, adjusts the DC level at the base of Q63 for a zero-volt DC output level from the Trigger Preamp circuit when the Channel 1 trace is centered vertic ally. Output from the Channel 1 Trigger Pickoff stage is connected to the Trigger Preamp circuit through the TRIGGER switch, SW230B.

## Paraphase Amplifier

The output signal from the Feedback Amplifier stage is connected to the Paraphase Amplifier stage through the VARIABLE control, R75. When the VARIABLE control is set to the CAL position (fully clockwise), R75 is effectively by-passed and maximum signal current reaches the base of Q84. Switch SW75, ganged with the VARIA8LE control, is open and the UNCAL neon bulb is disconnected. As the VARIABLE control is rotated counterclockwise from the CAL detent, SW75 is closed and the UNCAL light, B75, ignites to indicate that the vertical deflection is uncalibrated. The signal applied to the base of Q84 is continuously reduced as the VARIABLE control is rotated counterclockwise.


Fig. 3-2. Chennel 1 Vertical Preamp detailed block diagram.


Fig. 3-3. Channel 2 Verncal Preamp detailed block diagram.

Q84 and Q94 are connected as a common-emitter phase inverter (paraphase amplifier)I to convert the single-ended input signal to a push-pull output signal. Gain of this stage is determined by the emitter degeneration. As the resistance between the emitters of Q84 and Q94 increases, emitter degeneration increases also to result in less gain through the stage. The GAIN, adjustment, R90, varies the resistance between the emitters to control the overall gain of the Channel 1 Vertical Preamp.

## CHANNEL 2 VERTICAL PREAMP

## General

The Channel 2 Vertical Preamp circ uit is basic ally the same as the Channel 1 Vertical Preamp circuit. Only the differences between the two circuits are described here. Portions of this circ uit not described in the following description operate in the same manner as for the Channel 1 Vertical Preamp circuit [corresponding circuit numbers assigned in the 100-199 range]. Fiq. 3-3 \$hows a detailed block diagram of the Channel 2 Vertical Preamp circuit. A schematic of this circuit is shown in diagram 3 at the rear of this manual.

## Feedback Amplifier

Basically, the Channel 2 Feedback Amplifier operates as described for Channel 1. However, the Channel 2 Vertical
${ }^{3}$ Lloyd P. Hunter (ed.), "Handbook of Semiconductor Electronics", second edition, McGraw-Hill, New York, pp. 11-94.

Preamp circuit does not have a trigger pickoff stage. To provide a load at the collector of Q154 similar to the loc the Channel 1 Trigger Pickoff stage provides at the collect of Q54, C159 and R159 are connected into the circuit.

## Paraphase Amplifier

The basic Channel 2 Paraphase Amplifier configuratic and operation is the same as for Channel 1 . However, the INVERT switch, SW195, has been added in the Channel 2 circuit. This switch allows the displayed signal from Channel 2 to be inverted.

## VERTICAL SWITCHING

## General

The Vertical Switching circuit determines if the CH 1 and/ or the CH 2 Vertical Preamp output signal is connected to the Vertical Output Amplifier circuit (through the Delay Line Driver and Delay Line stages). In the ALT and CHOP positions of the MODE switch, both channels are altemately displayed on a shared-time basis. Fig. 3-4 shows a detailed block diagram of the Vertical Switching circuit. A schematic of this circuit is shown on diagram 5 at the rear of this manual.

## Diode Gates

The Diode Gates, consisting of four diodes each, can be thought of as switches which allow either of the Vertical


Fig. 3-4. Vertical 5 witching detailed block diagram.

Preamp output signals to be coupled to the Vertical Output Amplifier. D201 through D204 control the Channel 1 output and D206 through D209 control the Channel 2 output. These diodes are in tum controlled by the Switching Multivibrator for dual-trace displays, or by the MODE switch for singletrace displays.

CH 1. In the CH 1 position of the MODE switch, -12 volts is applied to the junction of D207-D208 in the Channel 2 Diode Gate through R227 (see simplified diagram in Fig. 3-5]. This forward biases D207-D208 and reverse biases D206-D209 since the input to the Delay-Line Driver stage is at about -5.8 volts. D206-D209 block the Channel 2 signal so it cannot pass to the Delay-Line Driver stage. At the same time, in the Channel 1 Diode Gate, D202-D203 are cannected to ground through R212. D202-D203 are held reverse biased while D201-D204 are forward biased. Therefore, the Channel 1 signal posses to the Delay-Line Driver stage.

CH 2. In the CH 2 position of the MODE switch, the above conditions are reversed. D202-D203 are connected to -12 volts through R217 and D207-D208 are connected to ground through R222. The Channel 1 Diode Gate blocks the signal and the Channel 2 Diode Gate allows it to pass.

## Switching Multivibrator

ALT. In this mode of operation, the Switching Multivibrator operates as a bistable multivibrator. ${ }^{2}$ In the ALT position of the MODE switch, -12 volts is applied to the emitter of the Altemate Trace Switching Amplifier stage, Q234 by the MODE switch. Q234 is forward biased to supply current to the "on" Switching-Multivibratar transistor through R235, D235 and R218 or R228. For example if Q225 is conducting, current is supplied to Q225 through R228. The current flow through collector resistors R212 and R222 drops the D207D208 cathode level negative so the Channel 2 Diode Gate is blocked as for Channel 1 only operation. The signal passes through the Channel 1 Diode Gate to the Delay-Line Driver stage.
The altemate trace sync pulse is applied to Q234 through D231 at the end of each sweep. This negative-going sync pulse momentarily intemupts the curent through Q234 and both Q215 and Q225 are tumed off. When Q234 tums on again after the altemate-trace sync pulse, the charge on C 218 determines whether Q215 or Q225 conducts. For example, when Q225 was conducting, C218 was charged negatively on the D228 side to the emitter level of Q225 and positively on the D218 side. This charge is stored while Q234 is off and when current flow through Q234 resumes, this stored charge holds the anode of D228 more negative than the anode of D218. D218 is forward biased and the emitter of Q215 is pulled more negative than the emitter of Q225 ta switch the multivibrator. The conditions described previously are reversed; now the Channel 1 Diode Gate is reverse biased and the Channel 2 signal passes through the Channel 2 Diode Gate.

The Reference Feedback stage, Q253, provides commonmode voltage feedback from the Delay-Line Driver stage to allow the diode gates to be switched with a minimum amplitude switching signal. The emitter level of Q253 is connetted to the junction of the Switching Multivibrator collector

[^1]resistors, R211-R212 and R221-R222 through D213 or D223. The collector level of the "on" Switching Multivibrator transistor is negative and either D213 or D223 is forward biased. This clamps the cathode level of the forward-biased shunt diodes in the applicable Diode Gate about 0.5 volts more negative than the emitter level of Q253. The shunt diodes are clamped near their switching level and therefore they can be switched very fast with a minimum amplitude switching signal. The level at the emitter of Q253 follows the average voltage level at the emitters of the Delay-Line Driver stage. This maintains about the same voltage difference across the Diode Gate shunt diodes so they can be switched with a minimum amplitude switching signal regardless of the deflection signal at the anodes of the shunt diodes.

CHOP. In the CHOP positian of the MODE switch, the Switching Multivibratar free runs as an astable multivibrator ${ }^{3}$ at about a $500-\mathrm{kHz}$ rate. The emitters of Q215 and Q225 are connected to -12 volts through R218 and R228. At the time of tum-on, one of the transistors begins to conduct; for example, Q225. Q225 conducts the Channel 2 current and prevents the Channel 2 signal from reaching the Delay-Line Driver stage. Meanwhile, the Channel 1 Diode Gate passes the Channel 1 signal to the Delay-Line Driver.

The frequency-determining components in the CHOP mode are C218-R218-R228. Switching action occurs as follows: When Q225 is on, C218 attempts to charge to -12 volts through R218. The emitter of Q215 slowly goes toward -12 volts as C218 charges. The base af Q215 is held at a negative point determined by voltage divider R215-R224 between -12 volts and the collector of Q225. When the emitter voltage of Q215 reaches a level slightly more negative than its base, Q215 conducts. The collector level of Q215 goes negative and pulls the base of Q225 negative also, through divider R214-R225, to cut Q225 off. When Q215 tums on, its emitter is pulled positive along with C218. This action switches the Diode Gate stage to connect the opposite half to the Delay-Line Driver stage. Again C218 begins to charge towards -12 volts but this time through R228. The emitter of Q225 slowly goes negative as C218 charges, until Q225 tums on. Q215 shuts off and the cycle begins again.

Diodes D218 and D228 have no effect in the CHOP mode. Q253 operates the same in CHOP as in ALT, to allow the Diode Gates to be switched with a minimum signal level.

The Chopped Blanking Amplifier stage, Q244, provides an output pulse to the Z Axis Amplifier which blanks out the transition between the Channel 1 trace and the Channel 2 trace. When the Switching Multivibrator changes states, the current through 7241 momentarily changes. A negative pulse is applied to the base of Q244, to tum it off. The width of the pulse at the base of Q244 is determined by R241 and C241. Q244 clips the signal applied to its base, and the positive-going output pulse, which is coincident with trace switching, is applied to the Z Axis Amplifier circuit through R245.

ADD. In the ADD position of the MODE switch, the Diode Gate stage allows both signals to pass to the Delay-Line Driver stage. The Diode Gates are both held on by -12 volts applied to their cathodes through R260 and R270. Since both signals are applied to the Delay-Line Driver stage, the output signal is the algebraic sum of the signals on both Channel 1 and 2.

[^2]

Fig. 3-5. Effect of Diode Gates on signal path (simplified Vertical Switching diagram). Conditions shown for CH 1 position of MODE switch.

## Delay-Line Driver

Output of the Diode Gate stage is applied to the DelayLine Driver stage, Q284 and Q294. Q284 and Q294 are connected as operational a mplifiers with feedback provided by R268-R269 and R278-R279 and the delay-line compensation network. The delay-line compensation network, C261-C262-C263-C 264-C 265-C 266-R261-R262-R264-R265, provides highfrequency compensation for the Delay Line. R289-C 289 in the collector circuit of Q284-Q294 improve the high-frequency reverse temination of the Delay Line. Output of the Delay-Line Driver stage is connected to the Vertical Output Amplifier through the Delay Line.

## Normal Trigger Pickoff Network

The trigger signal for NORM trigger operation is obtained from the collector of Q284. The Normal Trigger DC Level adjustment, R285, sets the DC level of the nomal trigger output signal so the sweep is triggered at the zero-level of the displayed signal when the Triggening LEVEL control is set to 0 . The nomal trigger signal is connected to the Trigger Preamp through SW230B. R294 and R295 provide the same DC load for Q294 as provided to Q284 by the Normal Trigger Pickoff Network.

VERTICAL OUTPUT AMPLIFIER

## General

The Vertical Output Amplifier circuit provides the final amplification for the vertical deflection signal. This circuit includes the Delay Line and the TRACE FINDER switch. The TRACE FINDER switch compresses an overscanned display within the viewing area when pressed in. Fig. 3-6]shows a detailed block diagram of the Vertical Output Amplifier circuit. A schematic of this circuit is shown on diagram 6 at the rear of this manual.

## Delay Line

The Delay Line provides approximately 140 nanoseconds delay for the vertical signal to allow the Sweep Generator circuits time to initiate a sweep before the vertical signal reaches the vertical deflection plates. This allows the instrument to display the leading edge of the signal originating the trigger pulse when using intemal triggering.

## Phase Equalizer Network

The Phase Equalizer Network is comprised of L301-L302-L311-C301-C302-C311-C312. This network compensates for


Fig. 3-6. Vertical Output Amplifier detailed block diagram.
the phase distortion of the Delay Line. C303-R303 and C313R313 in series with the base-emitter resistance of Q304 and Q314 provide the forward termination for the Delay Line.

## Output Amplifier

Q304 and Q314 are connected as common-base amplifiers to provide a low input impedance to properly terminate the Delay Line (along with the Phase Equalizer Network). It also provides isolation between the Delay Line and the following stages.

The output of Q304 and Q314 is connected to the bases of Q324 and Q334. The network C326-C327-C328-C336R328 provides high-frequency peaking to compensate for the capacitive loading of the deflection plates on the output stage. C328, C336 and R328 are adjustable to provide optimum response. The TRACE FINDER switch, SW330, reduces the quiescent current of Q324 and Q334, when pressed, to compress an off-screen display within the graticule area. Normally, the collector current for Q324 and Q334 is supplied through R321, R322 and the parallel combination of R323 and R333. When SW330 is pressed, -12-volts is connected to the collector circuit of Q324 and Q334 through R332. This limits the dynamic range of Q324 and Q334 to compress the display vertically within the graticule area. Although the display is nonlinear, it provides a method of locating a signal that is off screen vertically due to incorrect positioning or deflection factor.

Q344 and Q354 amplify the output of Q324 and Q334. The signal at the collectors of Q344 and Q354 is applied to the output transistors, Q364 and Q374, through R344, R354 and T357. D344 and D354 prevent saturation of Q344 and Q354 (to improve the recovery of the Vertical Output Amplifier circuit) when large signals deflect the display off screen. T357 provides high-frequency balance for the Output Amplifier stage. Q364 and Q374 provide the output signal voltage to drive the CRT vertical deflection plates. LR367 and LR377 provide damping for the leads connecting the output signal to the deflection plates.

## TRIGGER PREAMP

## General

The Trigger Preamp circuit amplifies the intemal trigger signal to the level necessary to drive the A and B Trigger

Generator circuits. Input signal for the Trigger Preamp circuit is either a sample of the signal applied to Channel 1 or a sample of the composite vertical signal from the Vertical Switching circuit. Fiq. 3-7 shows a detailed block diagram of the Trigger Preamp circuit. A schematic of this circuit is shown in diagram 7 at the rear of this manual.

## Input Circuitry

The intemal trigger signal from the Vertical Deflection System is connected to the Trigger Preamp through the TRIGGER switch, SW230B. When the TRIGGER switch is in the NORM position, the trigger signal is a sample of the composite vertical signal in the Vertical Switching circ uit. This signal is obtained from the collector of Q284 and is a sample of the displayed channel (or channels for dualtrace operation). Since the signal source follows the dualtrace switching stage, the NORM trigger signal also includes the chopped switching transients when operating in the CHOP mode. When the TRIGGER switch is in the NORM position, the CH 1 lights, B400 and B401, are disconnected. Also, the sample of the Channel 1 signal is connected to the CH 1 OUT connector. This output signal can be used to monitor Channel 1 or it can be used to cascade with Channel 2 to provide a one millivolt/division minimum deflection factor (with reduced bandwidth).

In the CH 1 ONLY position of the TRIGGER switch, the intemal trigger signal is obtained from the emitter of Q63 in the CH 1 Vertical Preamp circuit. Now, the intemal trigger signal is a sample of only the signal applied to the Channel 1 INPUT connector. The CH 1 lights are tumed on to indicate that the TRIGGER switch is in the CH 1 ONLY position and the CH 1 OUT connector is disconnected from the circuit.

R402, R403 and R404 terminate the coaxial cables from the trigger pickoff stages to provide a constant load for these stages. In the NORM position of the TRIGGER switch, the NORM trigger signal (from the Vertical Switching circuit) is teminated at the input to the amplifier by R404. The CH 1 ONLY trigger signal (from the CH 1 Vertic al Preamp circuit) is terminated at the CH 1 OUT connector by R402. In the CH 1 ONLY position, the CH 1 ONLY trigger signal is terminated at the input to the amplifier by R404 and the NORM trigger signal is terminated by R403.


Fig. 3-7. Trigger Preamp detailed diagram

## Amplifier Circuitry

The intemal trigger signal selected by the TRIG GER switch is connected to the base of Q404. Transistor Q404 converts the trigger voltage signal at its base to a current drive for the remainder of the Trigger Preamp. D408 in the emitter circuit of Q404 provides themal compensation for the amplifier.

The signal current at the collector of Q404 is connected to the base of Q414, Q413, Q414 and Q423 are connected as a current driven, voltage output operational amplifier. The amplified signal at the collector of Q414 is connected directly to the base of Q413, and to the base of Q423 through zener diode D421 This zener diode provides a DC voltage drop while the signal is connected to the base of Q423 with minimum attenuation. Q413 and Q423 are connected as emitter followers in the complementary symmetry amplifier ${ }^{\text {con }}$ configuration. This configuration overcomes the basic limitation of emitter followers; inability to provide equal response to

[^3]both positive- and negative-going portions of a signal. This is remedied in this configuration by using an NPN transistor for one emitter follower, Q413, and a PNP transistor for the other emitter follower, Q423. Since Q413 is an NPN transistor, it responds best to positive-going signals and Q423, being a PNP transistor responds best to negative-going signals. The result is a circuit which has equally fast response to both positive- and negative-going trigger signals while maintaining a low output impedance. Feedback from the output of the Trigger Preamp circuit is connected to the base of Q414 through R419. This feedback provides more linear operation. Total overall gain of the Trigger Preamp is about 10 . The amplified intemal trigger signal is connected to the A and B SOURCE switches through R427 and R429.

## A TRIGGER GENERATOR

## General

The A Trigger Generator circuit produces trigger pulses to start the A Sweep Generator circuit. These trigger pulses


Fig. 3-8. A Trigger Generator detailed block diagram.
are derived either from the intemal trigger signal from the Vertical Deflection System, an extemal signal connected to the EXT TRIG INPUT connector, or a sample of the line voltage applied to the instrument. Controls are provided in this circuit to select trigger level, slope, coupling and source. Fig. 3-8, shows a detailed block diagram of the A Trigger Generator circuit. A schematic of this circuit is shown on diagram 8 at the rear of this manual.

## Trigger Source

The A SOURCE switch, SW430, selects the source of the A trigger signal. Three trigger sources are ovailable; intemal, line and extemal. A fourth position of the A SOURCE switch provides 10 times attenuation for the extemal trigger signal.

The intemal trigger signal is abtained from the Vertical Deflection System through the Trigger Preamp circuit. This signal is a sample of the signal(s) applied to the Channel 1 and/or Channel 2 INPUT connectors. Further selection of the intemal trigger source is provided by the TRIGGER switch to provide the intemal trigger signal from both channels or from Channel 1 only (see Trigger Preamp discussion for details).

The line trigger is obtained from voltage divider R1104R1105 in the Power Supply circuit. This sample of the line frequency, about 1.5 volts RMS, is coupled to the A Trigger Generator in, the LINE position of the A SOURCE switch. The

A COUPLNG switch should not be in the LF REJ position when using this trigger source.

Extemal trigger signals applied to the A EXT TRIG INPUT connector can be used to produce a trigger in the EXT and EXT $\div 10$ positions of the A SOURCE switch. Input resistance (DC) is about one megohm in both extemal positions. However, in the LF REJ position of the A COUPUNG switch, the medium and high-frequency resistance drops to about 90 kilohms due to the addition of C436-R436 in the circuit. In the EXT $\div 10$ position, a 10 times frequency compensated attenuator is connected into the input circuit. This attenuator reduces the input signal amplitude 10 times to provide more A LEVEL control range while maintaining the one-megohm X 20 pF input RC characteristics.

## Trigger Coupling

The A COUPUNG switch offers a means of accepting or reiecting certain frequency components of the trigger signal. In the AC and LF REJ positions, the DC component of the trigger signal is blocked by coupling capacitors C435 or C436. In the AC position, frequency components below about 30 hertz are attenuated. In the LF REJ position, frequency components below about 30 kilohertz are attenuated.

The HF REJ position attenuates high-frequency components of the triggering signal. The trigger signal is AC coupled to the input, attenuating signals below about 30 hertz and above about 50 kilohertz. The DC position provides equal coupling for all signals from DC to 50 megahertz.

## Input Stage

The trigger signal from the A COUPUNG switch is connected to the Input Stage through the network C440-R438-R439-R440-R441. R438-R439 provide the input resistance for this stage. The voltage-divider action of R438-R439 allows about $98 \%$ of DC or low frequency signals applied to R438 to be available at the junction of R438 and R439. C440 along with the stray capacitance in the circuit forms an AC divider which maintains about this same voltage division for high-frequency signals. R440 limits the current drive to the gate of FET Q443. Diode D441 protects the circuit by clamping the gate of Q443 at about - 12.5 volts if a highamplitude negative signal is applied to the EXT TRIG INPUT connector. Over-voltage protection for high-amplitude positive signals is provided by the forward conduction of FET Q443.

Q443 is connected as a source follower to provide a high input impedance and a low output impedance. As a result, this stage provides isolation between the A Trigger Generator circuit and the trigger signal source. The output signal from Q443 is connected to the Slope Comparator stage through emitter follower Q453. Diodes D449 and D459 provide protection for the Slope Comparator stage transistors, Q454 and Q464.

## Slope Comparator

Q454 and Q464 are connected as a difference amplifier (comparator) ${ }^{\text {s }}$ to provide selection of the slope and level at which the sweep is triggered. The reference voltage for the comparator is provided by the A LEVEL control, R460, and the A Trigger Level Center adjustment, R462. The A Trigger Level Center adjustment sets the level at the base of Q464 so the display is triggered at the zero-volt DC level of the incoming trigger signal when the A LEVEL control is centered. The A LEVEL control varies the base level of Q464 to select the point on the trigger signal where triggering occurs.

R458 establishes the emitter current of Q454 and Q464. The transistor with the most positive base controls conduction of the comparator. For example, assume that the trigger signal from the Input Stage is positive going and Q454 is forward biased. The increased curent flow through R458 produces a larger voltage drop and the emitters of both Q454 and Q464 go more positive. A more positive voltage at the emitter of Q464 reverse biases this transistor, since its base is held at the voltage set by the A LEVEL control, and its collector curent decreases. At the same time, Q454 is forward biased and its collector curent increases. Notice that the signal currents at the collectors of Q454 and Q464 are oppos-te in phase, The sweep can be triggered from either the negative-going or positive-going slope of the input trigger signal by producing the trigger pulse from either the signal at the collector of Q464 for - slope operation or the signal at the collector of Q454 for + slope operation. This selection is made by the SLOPE switch, SW455.

When the A LEVEL control is set to 0 (midrange], the base of Q464 is at about one volt positive which corresponds to a zero-volt level at the input to this circuit (with correct calibration]. The base-emitter drop af Q464 sets the common emitter level of Q454-Q464 to about +0.3 volts. Since the

[^4]base of Q454 must be about 0.65 volts more positive than the emitter before it can conduct, the comparator switches around the zero-volt level of the trigger signal (zero-volt level an the trigger signal corresponds to about one volt positive at this point). As the A LEVEL control is tumed clockwise toward + , the voltage at the base of Q464 becomes more positive. This increases the current flow through R458 to produce a more positive voltage on the emitters of both Q454 and Q464. Now the trigger signal must rise more positive before Q454 is biased on. The resultant CRT display starts at a more positive point on the displayed signal. When the A LEVEL control is in the - region, the effect is the opposite to produce a resultant CRT display which starts at a more negative point on the trigger signal.

The slope of the input signal which triggers the A sweep is determined by the A SLOPE switch, SW455. When the A SLOPE switch is set to the - position, the collector of Q454 is connected to the +12 -volt supply through D456 and R467. The anode of D466 is grounded and it is reverse biased. Now the collector current af Q464 must flow through D465, R459, the parallel combination D475 and R468-R469L469 and R467 to the +12 -volt supply (see Fig. 3-9). Since the output pulse from the A Trigger Generator circuit is derived from the negative-going portion af the signal applied to the Trigger TD stage, the sweep is triggered on the nega-tive-going portion of the input trigger signal (signal applied to Trigger TD stage is in phase with the input signal for slope triggering). When the A SLOPE switch is set to + , conditions are reversed (se Fig. 3-1g). Q464 is connected to the +12 -volt supply through D466 and R467. The anode of D456 is grounded to divert the collector current of Q454 through the Trigger TD stage. The signal applied to the Trigger TD stage is now $180^{\circ}$ out of phase with the input trigger signal so the sweep is triggered on the positive-going portion of the input signal.

## Trigger TD

The Trigger TD stage shapes the output of the Slope Comparator to provide a trigger pulse with a fast leading edge. Tunnel diode D475 ${ }^{6}$ is quiescently biased so it operates in its low-voltage state. The current from one of the transistors in the Slope Comparator stage is diverted through the Trigger TD stage by the A SLOPE switch. As this current inc reases due to a change in the trigger signal, tunnel diode D475 switches to its high-voltage state. L469 opposes the sudden change in current which allows more current to pass through D475 and switch it more quickly. As the curent flow stabilizes, L469 again conducts the major part of the current. However, the current through D475 remains high enough to hold it in its high-voltage state. The circuit remains in this condition until the current from the Slope Comparator stage decreases due to a change in the trigger signal applied to the input. Then, the current through D475 decreases and it reverts to its low-voltage state.

## Pulse Amplifier

The trigger signal from the Trigger TD stage is connected to the base of the Pulse Amplifier, Q473, through R472. The trigger pulse at this point is basically a negative-going pulse with a fast rise. The width of the pulse depends upon the
${ }^{6}$ Millman and Taub, pp. 452-455.


Fig. 3-9. Trigger path for negative-slope triggering (simplified A Trigger Generator diagram).
waveshape of the input signal and the setting of the A LEVEL control. Q473 is connected as an amplifier with the primary of pulse transformer T474 providing the major collector load. The negative-going pulse at the base of Q473 drives it into heavy conduction and the resulting current increase of Q473 flows through T474, R474, Q473, C473 and C467. Due to the short time constant of the RC network involving C473, the curent of Q473 quickly retums to the level detemined by R473. The resultant signal at the collector of Q473 is a positive-going fast-rise pulse with the width determined by the time constants of the RC network in the circuit. T474 inverts the output pulse to produce a negativegoing trigger pulse which is coincident with the rise of the output signal from the Trigger TD stage. This negative-going trigger pulse is connected to the A Sweep Generator circuit through C476-R476. D474 limits the collector of Q473 from going more positive than about +0.5 volts. A simulaneous negative-going pulse with the same width as the trigger pulse is available at the emitter of Q473. This pulse is connected to the Auto Pulse Amplifier stage.

## Auto Pulse Amplifier

The negative-going trigger pulse from the emitter of Q473 is connected to the base of Q484 through R481. This stage is similar to the Pulse Amplifier stage. Inductor L484 provides the collector load for this stage. The positive-going portion of the trigger pulse is coupled to the Auto Multivibrator stage through D484. D483 clamps the collector of Q484 at about -0.5 volts to eliminate negative transients.

## Auto Multivibrator

The basic configuration of the Auto Multivibrator stage is a monostoble multivibrator made up of Q485 and Q495. This stage produces the control gate for the auto trigger circuits located in the A Sweep Generator circuit. Under quiescent conditions (no trigger signal), the base of Q495 is

[^5]

Fig. 3-10. Trigger path for positive-slope triggering (simplified A Trigger Generator diagram)
near zero volts. The base of Q485 is held at about -0.65 volts by the forward voltage drop of D484. Since the base of Q495 is the most positive, it conducts and raises the emitter level of Q485 positive enough to hold it off. C 485 charges to about +13 volts where it is clamped by D486 and D493. The base of Q494 is clamped at about +12.6 volts by D493 which reverse biases it. Since there is no curent flow through Q494, its collector level goes negative.

When a trigger signal is present, the positive-going pulses from the Auto Pulse Amplifier stage tum Q485 on through D484. The collector of Q485 goes negative and C485 discharges rapidly through Q485, R490 and R485. As C 485 discharges, the current flow through R490 biases Q495 off. When C485 is fully discharged, the current flow through R490 ceases and Q495 comes back on to reset the multivibrator. Now C 485 begins to charge towards +75 volts through R486. Current also flows through R494 and the base of Q494 goes negative to bias it on. The collector level of Q494 rises positive to produce the auto gate output for the A Sweep Generator circuit.

For low-frequency signals (below about 30 hertz), C485 recharges to about +13 volts in about 85 milliseconds. Then Q494 is biased off to end the auto gate (display free runs or is unstable). However, if a repetitive trigger signal tums Q485 on again before C 485 has charged to +13 volts, C 485 is discharged completely again and once more starts to charge towards +75 volts. Since the base of Q494 remains negative enough with a repetitive trigger signal to hold it in conduction, the auto output level is continuous for a stable display (with correct A LEVEL control setting).

## A SWEEP GENERATOR

## General

The A Sweep Generator circuit produces a sawtooth voltage which is amplified by the Horizontal Amplifier circuit to provide horizontal sweep deflection on the CRT. This output signal is generated on command (trigger pulse) from the A Sweep Generator circuit. The A Sweep Generator cir-


Fig. 3-11. A Sweep Generator defailed block diagram.
cuit also produces on unblanking gate to unblank the CRT during A sweep time. In addition-this circ uit produces several control signals for other circuits within this instrument and several output signals to the side-panel connectors Fig. 3-11 shows a detailed block diagram of the A Sweep Generotor circuit. A schematic of this circuit is shown on diagram 9 at the rear of this manual.

The A SWEEP MODE switch allows three modes of operation. In the NORM TRIG position, a sweep is produced only when a trigger pulse is received from the A Trigger Generator circuit. Operation in the AUTO TRIG position is much the same as NORM TRIG except that a free-running trace is disployed when a trigger pulse is not present. In the SINGLE SWEEP position, operation is also similar to NORM TRIG except that the sweep is not recurent. The following circuit description is given with the A SWEEP MODE switch set to NORM TRIG. Differences in operation for the other two modes are then discussed later.

Normal Trigger Mode Operation
Sweep Gate. The negative-going trigger pulse generated by the A Trigger Generator circuit is applied to the Sweep

Gate stage through D501. Tunnel diode D505 is quiescently biased on in its low-voltage state. When the negative-going trigger pulse is applied to its cathode, the current through D505 increases and it rapidly switches to its high-voltage state where it remains until reset by the Sweep Reset Multivibrator stage at the end of the sweep. The negative-going level at the cathode of D505 is connected to the base of Q504 through C503 and R503. Q504 is tumed on and its collector goes positive. This positive-going step is connected to the Disconnect Diode through C509-R509 and to the Output Signal Amplifier through C506-R506.

Output Signal Amplifier. The positive-going gate pulse from the Sweep Gate stage applied to the base of Q514 produces a negative-going pulse at its collector. This pulse is connected to the Z Axis Amplifier circuit through R519 to unblank the CRT during sweep time. It is also connected to the Holdoff Capacitor through R517 and D517 to discharge it completely at the beginning of each sweep.

The positive-going gate pulse at the base of Q514 is also coupled from the emitter of Q514 to the emitter of Q524. The resulting positive-going signal at the collector of Q524 is coupled to the Vertical Switching circuit through C526 to
provide an altemate-trace sync pulse for dual-trace operation. It is also coupled to the A GATE output connector on the side panel through R529. D528 and D-529 clamp the gate signal so it does not go more than about 0.5 volts negative and 12.5 volts positive.

Disconnect Diode. The Disconnect Diode, D533, is quiescently conducting curent through R506, R508, R509, R530 and R531. The positive-going gate signal from Q504 reverse biases D533 and intemupts the quiescent current flow. Now the timing current through the Timing Resistor begins to charge the Timing Capacitor, C530, so the Sawtaoth Sweep Generator stage can produce a sawtooth output signal. The pasitive-going gate signal also reverse biases D547 to disconnect the Sweep Start Amplifier. The Disconnect Diode is a fast tum-off diode with low reverse leakage to reduce switching time and improve timing linearity at the sfart of the sweep,

Sawtooth Sweep Generator. The basic generator circuit is a Miller Integrator circuit. ${ }^{8}$ When the current flow through D533 is intemupted by the Sweep Gate signal, the Timing Capacitor, C530, begins to charge through the Timing Resistor, R530, ond the A Sweep Cal Adjustment, R531. The Timing Capacitor and Resistor are selected by the A TIME/DIV switch to change sweep rate. The A Sweep Cal adjustment allows calibration for accurate sweep timing. The A VARIABLE control, R530Y (see Timing Switch diagram), pravides variable sweep rates by changing the charge time of C530.

The pasitive-going voltage at the R530 side of C530 as it charges toward +75 volts is connected to the gate of FET Q533. This produces a positive-going output voltage which is connected to the base of Q531 through R536. Q531 amplifies and inverts the voltage change at its base to produce a negative-going sawtooth output. To provide a linear charging rate for the Timing Capacitor, the sweep output signal is connected to the negative side of C530. This feedback provides a constant charging current for C530 which maintains o constant charge rate to produce a lineor sawtooth output signal. The output voltage continues to go negative until the circuit is reset through the Sweep Reset Multivibrator stage. The output signal from the collector of Q531 is connected to the Horizontal Amplifier circuit through R538 and the Delay Pickoff Comparator stage in the B Sweep Generator circuit through R532.

Sweep Reset Emitter Follower. The negative-going sawtooth voltage at the collector of Q531 is connected to the base of the Sweep Reset Emitter Fallower stage, Q543. The negative-going signal at the emitter of Q543 is coupled to the Sweep Reset Multivibrator stage to determine sweep length and to the Sweep Start Amplifier stage to set the starting point for the sweep. D542 connected to the base of Q543 protects this stage during instrument warmup,

Sweep Start Amplifier. The signal at the emitter of Q543 goes negative along with the applied sawtooth signal. This increases the forward bias on D543 which in tum decreases the forward bias on D545 as the sawtooth goes negative, When the anode of D543 reaches a level about one volt more positive than the level on the base of Q544, it is reverse biased to intemupt the current flow through Q544.

[^6]The circuit remains in this condition until after the sweep retrace is complete. As the voltage at the emitter of Q543 retums to its original DC level at the end of the sweep, D545 is again forward biased and Q544 conducts through D547 to set the quiescent current through the Disconnect Diode, D533. This establishes the correct starting point for the sweep. D546 clamps the collector of Q544 at about +0.5 volt. This reduces the voltage swing at the collector of Q544 and improves the response time. The Sweep Start adjustment, R758 (in the B Sweep Generator circuit), sets the base voltage level of Q544. The collector of Q531 is held at this same voltage level through the feedback loop comprised of Q533 ond Q531, thereby setting the starting point of the sawtooth output signal. The level established by the Sweep Start adjustment is also connected to the B Sweep Start Amplifier so the B sweep starts at the same voltage level as the A sweep.

Sweep Reset Multivibrator. The negative-going sawtooth signal at the emitter of Q543 is coupled to the cathodes of D555 and D556. These diodes are quiescently reverse biased at the start of the sweep. As the sawtooth voltage at the cathode of D555 goes negative, D555 is forward biased at a level about 0.5 volts more negative than the base level of Q575 (A SWEEP LENGTH cantrol in FULL position). Then the negative-going sawtooth signal from the Sweep Reset Emitter Follower stage is connected to the base of Q575. Q575 and Q585 are connected as a Schmitt bistable multivibratar ${ }^{9}$. Quiescently, at the start of the sweep, Q585 is conducting and Q575 is biased off to produce a negative level at its collector. This negative level allows the Sweep Gate tunnel diode, D505, to be switched to produce a sweep as discussd previously. When the negative-going sweep signal is connected to the base of Q575 through D555, Q575 is eventually biased on and Q585 is biased off by the emitter coupling between Q575 and Q585. The collector of Q575 rises positive and D505 is switched back to its low-voltage state through R502. D505 is held in its low-voltage state so it cannot accept incoming trigger pulses until after the Sweep Reset Multivibratar stage is reset. This ends the Sweep Gate stage output and the Disconnect Amplifier stage is tumed on to rapidly discharge the Timing Capacitor and pull the gate of Q533 rapidly negative to its original level to produce the retrace portion af the sawtooth signal. The Sawtooth Sweep Generator stage is now ready to produce another sweep as soon as the Sweep Reset Multivibrator stage is reset and another trigger pulse is received.

When Q575 is tumed on to end the sweep, it remains in conduction for a period of time to establish a holdoff period and allow all circuits to retum to their original conditions before the next sweep is produced. The holdoff time is determined by the charge rate of the Holdoff Capacitor, C550. At the start of the sweep, C550 is completely discharged by the unblinking gate at the collector af Q514. It is held at this level throughout the sweep time. When the Sweep Gate output ends, Q514 is cut off and C550 begins to charge toward +75 volts through R552 and R551. The positive-going voltage across he Holdoff Capacitor as it charges is connected to the base of Q575 through D552 and D559. When the base of Q 575 rises positive enaugh so it is reverse biased, its collector level drops negative and Q585 comes back into conduction. The bias on the Sweep Gate tunnel diode, D505, retums to a level that allows it to accept the next trigger pulse (D505 is enabled). The Holdoff Capacitor, C550, is

[^7]changed by the A TIME/DIV switch for the various sweep rates to provide the correct holdoff time. Diagram 12 shows a complete diagram of the A TIME/DIV switch.

As the A SWEEP LENGTH control is rotated counterclockwise from the FULL position, R555 place as more positive Level on the anode af D556 than is on the anode of D555 so D555 remains reverse biased. The Sweep Reset Multivibrator is reset as described for FUL sweep length operation at the point where D556 (instead of D555) is forward biased. Since this occurs at a more positive level on the negative-going sawtooth, the displayed sweep is shorter. Thus, R555 provides a variable sweep length for the A Sweep (from about 11 divisions in the FULL position to about four divisions in the fully clockwise position-not in B ENDS A detent). In the B ENDS A position (fully counterclockwise), o negative-going pulse from the B Sweep Generator circuit is connected to the base of Q575 through D575 at the end of the $B$ sweep time. If the A sweep is still running, this nega-tive-going pulse tums Q575 on to end the A sweep also. Since the A sweep ends immediately following the end of the B sweep, this position provides the maximum repetition rate (brightest trace) for Delayed Sweep mode operation.

The HF STAB control, R551, varies the charging rate af the Holdoff Capacitor to provide a stable display at fast sweep rates. This change in holdoff allows sweep synchronization for less display jitter at the faster sweep rates. The HF STAB control has little effect at slow sweep rates.

Lamp Driver. The auto gate level from the Auto Multivibrator stage in the A Trigger Generatar circuit is connected to the Lamp Driver stage, Q594, through D591 and D594. This gate level is coincident with the trigger pulse generated by the A Trigger Generator circuit and is present only when the instrument is correctly triggered. The positivegoing auto-gate level saturates Q594 and its collector goes negative to about zero volts. This applies about 12 volts across B596, A SWEEP TRIG'D light, and it comes on. This light remains on as long as the auto-gate level is present. When the auto-gate level goes negative because the instrument is no longer triggered, D595 clamps the base level of Q594 at about -0.5 volt and Q594 is reverse biased. The collector of Q594 rises positive and B596 goes off.

## Auto Trigger Mode Operation

Operation of the A Sweep Generator circuit in the AUTO TRIG position of the A SWEEP MODE switch, is the same as for the NORM TRIG position iust described when a trigger pulse is applied. However, when a trigger pulse is not present, a free-running reference trace is produced in the AUTO TRIG mode. This occurs as follows:
The auto-gate level from the Auto Multivibrator stage in the A Trigger Generator circuit is also connected to D592. When the auto-gate level is positive (triggered), the current flowing through D592 and R593 reverse biases D593 and the Sweep Gate tunnel diode, D505, operates as previously described for NORM TRIG operation. However, when the instrument is not triggered, the auto-gate level drops negative and the reduction in current through D592 and R593 allow D593 to become forward biased. Now, when the Sweep Reset Multivibratar stage resets at the end of the holdoff period, the additional current from R593-D593 flows through D505 and is sufficient to automatically switch
the Sweep Gate tunnel diode back into its high-voltoge state. The result is that the A Sweep Generator circuit is automatically retriggered at the end of each holdoff period and a free-running sweep is produced. Since the sweep free runs at the sweep rate of the A Sweep Generator circ uit (as selected by the A TIME/DIV switch), a bright reference trace is produced even at fast sweep rates.

## Single Sweep Operation

General. Operation of the Sweep Generator in the SINGLE SWEEP position of the A SWEEP MODE switch is similar to operation in the other modes. However, after one sweep has been produced, the Sweep Reset Multivibrator stage does not reset. All succeeding trigger pulses are locked out until the RESET button is pressed.

In the SINGLE SWEEP position, the A SWEEP MODE switch disconnects the charging curent for the Holdoff Capacitor. Now, Q575 remains on when it is forward biased through D555 or D556 at the end of the sweep. With Q575 on, D505 is held in its low-voltage state to lock out any incoming trigger pulses. The circuit remains in this condition until reset by the Single-Sweep Reset Amplifier stage.

Single-Sweep Reset Amplifier. The Single-Sweep Reset Amplifier, Q564, produces a pulse to reset the Sweep Reset Multivibrator stage so another sweep can be produced in the SINGLE SWEEP mode of operation. Quiescently, Q564 is biased off and the RESET switch is open. When the RESET button is pressed, B568 ignites and the voltage at the base of Q564 goes negative. Q564 saturates and produces a positive-going output pulse. This pulse has sufficient amplitude to shut off Q575 and allow Q585 to conduct and enable the Sweep Gate tunnel diode, D505. Now the A Sweep Generator circuit can be triggered when the next trigger pulse is received.

Lamp Driver. In the SINGLE SWEEP mode, the cathode of D591 is connected to ground to block the incoming auto-gate level. The A SWEEP TRIG'D light, B596 is disconnected from the collector of Q594 and the RESET light, B597, is connected into the circuit. The anode of D595 is also disconnected from ground. Now the condition of Q594 is determined by the Sweep Reset Multivibratar stage. When Q585 is off before the RESET button is pressed, the collector level of Q585 is negative. The current through R594-D595-R587-R588 sets the base level of Q594 negative enough to bias it off. However, when the RESET button is pressed and Q585 tums on, its collector goes positive. This positive level allows the base of Q594 to go positive also and it is biased on. The collector of Q594 goes negative and the RESET light comes on. Q594 and the RESET light remain on until Q585 tums off again at the end of the next sweep.

## B TRIGGER GENERATOR

## General

The B Trigger Generatar circuit is basically the same as the A Trigger Generator circuit. Only the differences between the two circuits are discussed here. Portions of the circuit not described in the following discussion operate in the same manner as for the A Trigger Generator circuit


Fig. 3-12. B Trigger Generator detailed block diagram
(corresponding circuit numbers are assigned in the 600-699 range). Fig. 3-12 shows a detailed block diagram of the B Trigger Generator circuit. A schematic of this circuit is shown on diagram 10 at the rear of this manual.

## Input Stage

The B Input Stoge operotes in basically the same manner as described for the A Trigger Generatar circuit. However, in the B Trigger Generator circuit, the HORIZ DISPLAY switch, SW801A and D638, block the B Trigger Generator input signal in the modes where B triggering is not desired. In the A position of the HORIZ DISPLAY switch, -12 volts is connected to the cathode af D635 and it is forward biased. Since the cathode of D638 is connected to +12 volts through R638, D638 is reverse biased and it blocks the trigger signal. In the A INTEN DURING B and DELAYED SWEEP (B) posiions, a second switch, B SWEEP MODE SW635 determines whether the $B$ trigger signal is blocked or passed to the Slope Comparator stage. If the B SWEEP MODE switch is in the B STARTS AFIER DELAY TMME position, the trigger signal is blocked as in the A position. However, the B Sweep Generator essentially free runs in this position as controlled by another portion of the B SWEEP MODE switch located in the B Sweep Generator circuit (see B Sweep Generator discussion). In the TRIGGERABLE AFIER DELAY TIME position, -12 volts is connected to the cathode of D638 through R639 rather than to D635. This forward biases D638 and allows the $B$ trigger signal to pass to the $B$ Slope Comparator stage.

In all positions of the HORIZ DISPLAY switch except EXT HORIZ, D641 is back biased since it is connected to +12 volts through R641. In the EXT HORIZ position, D638 is reverse biased because its cathode rises positive toward +12 volts applied through R638. Therefore, the trigger signal can not pass through D638. D641 is forward biased by -12 volts connected to its cathode through R642 by SW801A. The signal from the Input Stage is connected to the Horizontal Amplifier through D641 and the Extemal Horizontal Gain Network, R644-R645-R646. Gain of the Extemal Horizontal circuit is set by R645, Ext Horiz Gain, so a signal applied to the Channel 1 INPUT connector produces the indicated horizontal deflection.

The extemal horizontal signal can be obtained either extemally from the B EXT TRIG INPUT or EXT HORIZ connector when the B SOURCE switch is set to EXT or EXT $\div$ 10, or intemally from Channel 1 when the TRIGGER switch is in the CH 1 ONLY position and the B SOURCE switch is set to INT.

## Pulse Amplifier

The Pulse Amplifier in the B Trigger Generator operates much the same as in the A Tigger Generator. However, since there is no Auto circuit in the B Trigger Generator, a pulse is available only at the collector of Q684. The output pulse is applied to the B Sweep Generator through T686 and R688-C688.

## B SWEEP GENERATOR

## General

The B Sweep Generator circuit is basically the same as the A Sweep Generator circuit. Only the differences between the two circuits are discusssd here. The following circuits operate as described for the A Sweep Generator corresponding circuit numbers assigned in the 700-799 range): Sweep Gate [D705, Q704), Disconnect Diode (D742), Sawtooth Sweep Generator (Q743 and Q741), Sweep Reset Emitter Follower (Q753) and the Sweep Start Amplifier (Q754). Fig. 3-13 shows a detailed block diagram of the B Sweep Generator circuit. A schematic of this circuit is shown on diagram 11 at the rear of this manual.

## Output Signal Amplifier

Basically, the B Output Signal Amplifier is the same as the corresponding circuit in the A Sweep Generator circuit. Two unblanking gates are available from the collector of Q714. An unblanking gate is connected to the $Z$ Axis Amp-
lifier circuit through R717 and the HORIZ DISPLAY switch to unblank the CRT to display the B sweep. For A INTEN DURING B operation, additional unblinking current is added to the $A$ unblinking gate during the $B$ sweep time. This produces a display which is partially unblanked during $A$ sweep time and further unblanked during B sweep time to produce a display which has an intensified portion coincident with the B sweep time.

## Delay-Pickoff Comparator

The Delay-Pickoff Comparator stage allows selection of the amount of delay from the start of the A sweep before the B Sweep Generator is tumed on. This stage allows the start of B sweep to be delayed between 0.20 and 10.20 times the setting of the A TIME/DIV switch. Then, the B Sweep Generatar is tumed on and operates at a sweep rate independent of the A Sweep Generator (detemmined by setting of B TIME/DIV switch).

Q764A and B are connected as a voltage comparator. In this configuration, the transistor with the most positive


Fig. 3-13. B Sweep Generator detailed block diagram.
base controls conduction. A dual transistor, Q764, and a dual diode, D764, provide temperature stability for the comparatorcircuit. Q769 maintains a constant current through the conducting transistor. Reference voltage for the comparator circuit is provided by the DELAY-TME MULTPLIER control, R760. The voltage to this control is filtered by R759-C 759 to hold it constant and allow precise delay pickoff. The instrument is calibrated so that the major dial markings of R760 correspond to the major divisions of horizontal deflection on the graticule. For example, if the DELAY-TIME MULTIPLIER dial is set to 5.00 , the B Sweep Generator is delayed five divisions of the A sweep time before it can produce a sweep ( B sweep delay time equals five times setting of A TIME/DIV switch).

The output sawtooth from the A Sawtooth Sweep Generator stage is connected to the base of Q764A. The quiescent level of the A sawtooth biases Q764A on and its collector is negative enaugh to hold Q772 in the Delay Multivibrator stage in conduction. As the A sweep output sawtooth begins to run down, the base of Q764A also goes negative. When it goes more negative than lhe level at the base of Q764B (established by the DELAY-TIME Multiplier control), Q764B takes over conduction of the comparator and Q764A shuts off. This also switches the Delay Multivibratar stage to produce a negative-going reset pulse to the B Sweep Reset Multivibrator.

When the A sweep resets, Q764A is again retumed to conduction and Q764B is tumed off. This also resets the Delay Multivibrator to produce a positive-going output pulse. If the $B$ sweep is still running, this positive-going pulse forces the B Sweep Reset Multivibrator to reset and end the B sweep also.

## Delay Multivibrator

The Delay Multivibrator, Q768 and Q772, provides a lockout for the B Sweep Generator circuit during the A Sweep Generator reset and holdoff time to allow accurate delayed-sweep measurements when the DELAY-TIME Multiplier dial is set near 0 . This stage prevents the B Sweep Generator from being triggered before the A Sweep Generator is triggered ( $B$ Sweep Generator must always be triggered after the A Sweep Generator is triggered). This circuit also produces a pulse which resets the $B$ Sweep Reset Multivibrator stage after the delay period so the B Sweep Gate tunnel diode can be enabled to produce a sweep.

Transistors Q768 and Q772 are connected as a Schmitt bistable multivibrator. Quiescently, Q772 is held on by the negative level at the collector of Q764A and Q768 remains off. The circuit remains in this condition until the incoming A Sweep switc hes the Delay-Pickoff Comparator (see DelayPickoff Comparator discussion). Then, the base of Q772 goes positive and it tums off. At the same time, the base of Q768 is pulled negative by the collector level of Q764B and it tums on. The collector of Q772 goes negative and a negative-going output pulse is coupled to the B Sweep Reset Multivibrator stage through C774. This pulse resets the B Sweep Reset Multivibrator which in tum enables the B Sweep Gate stage.

## Sweep Reset Multivibrator

The basic B Sweep Reset Multivibra!or configuration and operation is the same as for the A Sweep Generator. How-
ever, several differences do exist. The B Sweep Reset Multivibrator dos not have a sweep length network for variable sweep length or a Holdoff Capacitor and associated circuit to reset the B Sweep Reset Multivibrator after the retrace. Instead, the negative-going sweep from the B Sweep Reset Emitter Follower, Q753, is connected to the base of Q785 through D748. Diode D748 is forward biased when the sweep voltage at the emitter of Q753 drops about 0.5 volts, more negative than the level at the base of Q 785 established by voltage divider R784-R785 between +12 volts and the collector of Q775. This negative-going sawtooth tums on Q785 and its collector goes positive to switch the B Sweep Gate tunnel diode, D705 to its low-voltage state, which resets the B Sweep. Q785 remains on and holds the B Sweep Gate tunnel diode locked out until the B Sweep Reset Multivibrator is reset by the Delay Multivibrator.

When the B Sweep Reset Multivibrator is reset by the Delay Multivibrator, Q775 comes on and Q785 turns off. The collector of Q785 goes negative and the B Sweep Gate tunnel diode, D705, is enabled. The state in which D705 remains depends upon the B SWEEP MODE switch and the HORIZ DISPLAY switch. When the B SWEEP MODE switch, SW635, is set to the TRIGGERABLE AFIER DELAY TMME position, D705 is biased so it can be switched to its highvoltage state by the next trigger pulse from the B Trigger Generatar. However, if the B SWEEP MODE switch is set to the B STARTS AFIER DELAY TIME position, the setting of the HORIZ DISPLAY switch, SW801A, determines operation of the B Sweep Gate tunnel diode. In the A position, the $B$ trigger pulses are blocked in the B Trigger Generator circuit so the B Sweep Generator cannot be triggered and does not produce a sweep. In the A INTEN DURING B and DELAYED SWEEP (B) position, -12 volts is connected to the cathode of D705 through R786 and R789. This voltage pulls the cathode of D705 negative enough so that it automatic ally switches to its high-voltage state after it is enabled by the B Sweep Reset Multivibrator stage. This produces a free-running B sweep Reset similar to the no trigger AUTO TRIG mode in the A Sweep Generator. However, since the B Sweep is reset (and automatically retriggered) at a fixed point on the A sweep sawtooth, the display is relatively stable. The best delayed sweep stability is provided in the TRIGGERABLE AFIER DELAY TME position, since the $B$ sweep is triggered by the trigger signal in this mode.

## B Ends A Pulse Amplifier

The positive-going voltage as the B unblanking gate ends is coupled to the B Ends A Pulse Amplifier, Q734, through C731 and D731. When the A SWEEP LENGTH control is in the B ENDS A position, this pulse saturates Q734 to produce a negative-going ouput pulse at its collector. This negative-going pulse is connected to the A Sweep Reset Multivibrator stage to reset the A sweep at the end of the $B$ sweep for maximum delayed sweep repetition rate.

## HORIZONTAL AMPLIFIER

## General

The Horizontal Amplifier circuit provides the output signal to the CRT horizontal deflection plates. In all positions of the HORIZ DISPLAY switch except EXT HORIZ the horizontal deflection signal is a sawtooth from either the A Sweep Generator circuit or the B Sweep Generator circuit.


Fig. 3-14. Herizontal Amplifier detailed block dlagram.

In the EXT HORIZ position, the horizontal deflection signal is obtained from the input Stage of the B Trigger Generator. In addition, this circuit contains the horizontal magnifier circuit and the horizontal positioning network. Fiq. 3-14 shows a detailed block diagram of the Horizontal Amplifier circuit. A schematic of this circuit is shown on diagram 13 at the rear of this manual.

## Input Amplifiers

The input signal for the Horizontal Amplifier is selected by the HORIZ DISPLAY switch, SW801A. In the A and A INTEN DURING B positions of the HORIZ DISPLAY switch, the sawtooth from the A Sweep Generator is connected to the base of the - Input Amplifier, Q814, through R803. In the DELAYED SWEEP (B) position, the B sawtooth is connected to the base of Q814. Whichever sawtooth signal is connected to the base of Q814 produces a current change which is amplified to produce a positive-going sawtooth voltage at the collector. This positive-going sawtooth signal is connected ta the base af Q834 in the Paraphase Amplifier stage.

In the EXT HORIZ position of the HORIZ DISPLAY switch, the extemal horizontal signal from the B Trigger Generator
circuit is connected to the base of the + Input Amplifier, Q824, through R821 The A and B sawtooth signals are grounded by the HORIZ DISPLAY switch. The B SOURCE switch selects either the intemal signal from Channel 1 (TRIGGER switch set to CH 1 ONLY) or an extemal signal connected to the EXT HORIZ connector. When the intemal signal is selected, the Channel 1 deflection factor as indicated by the CH 1 VOLTS/DIV switch applies as Horizontal Volts/Division. More information on the extemal horizontal circuitry is contained in the B Trigger Generator circuit discussion.

Horizontal positioning is provided by the POSITION control, R805A, and the FINE control, R805B, connected to the base of Q814. These controls vary the quiescent DC level at the base of Q814 which in tum sets the DC level at the horizontal deflection plates to determine the horizontal position of the trace. C804-RB04 eliminate common-mode noise from the position controls.

## Paraphase Amplifier

The output of the + and - Input Amplifier stages is connected to the Paraphase Amplifier stage, Q834 and Q844. This stage converts the single-ended input signal from either

Input Amplifier stage to a push-pull output signal which is necessary to drive the horizontal deflection plates of the CRT. In all positions of the HORIZ DISPLAY switch except EXT HORIZ, a positive-going sawtooth signal is connected to the base of Q834 through Q814. This produces a nega-tive-going sawtooth valtage at the collector of Q834. At the same time, the emitter of Q834 goes positive and this change is connected to the emitter of Q844 through the gain-setting network, R835-R836-R845-R846. In all positions of the HORIZ DISPLAY switch except EXT HORIZ, no signal is connected to the base of Q844 thraugh Q824 so that Q844 operates as the emitter-driven section of a paraphase amplifier. Then, the positive-going change at its emitter is amplified to produce a positive-gaing sawtooth signal at the collector. Thus the single-ended input sawtooth signal has been amplified and is available as a push-pull signal at the collectors of Q834 and Q844.

In the EXT HORIZ position of the HORIZ DISPLAY switch, the extemal horizontal deflection signal is connected to the base of Q844 through Q824 and the sawtooth signal at the base of Q814 is disconnected. Now, the circuit operates much the same as just described with the sawtooth input. A positive-going extemal horizontal deflection signal produces a negative-going change at the base of Q844 which decreases the current flow through this transitor. The collector of Q844 goes positive while the emitter-coupled signal to Q834 produces a negative-going change at the collector of Q834.

This stage also provides adjustment to set the nomal and magnified gain of the Horizontal Amplifier circuit, and the MAG switch to provide a horizontal sweep which is magnified 10 times. For normal sweep operation [MAG switch set to OFF), R835 and R836 cantrol the emitter degeneration between Q834 and Q844 to set the gain of the stage. R835, Normal Gain, is adjusted to provide calibrated sweep rates. When the MAG switch, SW801B, is set to the X10 position, R845 and R846 are connected in parallel with R835 and R836. This additional resistance dec reases the emitter degeneration of this stage and increases the gain of the circuit 10 times. R845, Mag Gain, is adjusted to provide calibrated magnified sweep rates. When the MAG switch is set to X10, the MAG ON light, B849, is connected to the $+150-$ volt supply through R849. B849 ignites to indicate that the sweep is magnified. In the EXT HORIZ position of the HORIZ DISPLAY switch, the magnifier is connected into the circuit so the horizontal gain is correct far extemal horizontal operation regardless of the setting of the MAG switch. However, both sides of B1049 are connected to ground so it does not ignite.

## Output Amplifier

The push-pull output of the Paraphase Amplifier is connected to the Output Amplifier. Each half of the Output Amplifier can be considered as a single-ended, feedback amplifier which amplifies the signal current at the input to produce a voltage output to drive the horizontal deflection plates of the CRT. The amplifiers have a low input impedance and require very little voltage change at the input to produce the desired output change. Diodes D851-D852 and D861-D871 protect the amplifier from being overdriven by excessive current swing at the collectors of Q834 and Q844. Negative feedback is provided from the collectors of the final transistors, Q884 and Q894, to the bases of the input
transistors through C882-R882 and C892-R892. C882 and C892 adjust the transient response of the amplifier so it has good linearity at fast sweep rates.

The Mag Register adjustment, R855, balances the quiescent DC curent to the base of Q863 and Q873 so a center-screen display does not change position when the MAG switch is changed from X10 to OFF.

The TRACE FINDER switch, SW330, reduces horizontal scan by limiting the current available to Q884 and Q894. Nomally the collectors of these transistors are retumed to +150 volts. However, when the TRACE FINDER switch is pressed in, the power from the unregulated +150 -volt supply is intemupted and the collector voltage for Q884 and Q894 is supplied from +75 volts through D884. Since the collectors are retumed to a lower potential, the output voltage swing is reduced to limit the horizontal deflection within the graticule area.

## Z AXIS AMPLIFIER

## General

The Z Axis Amplifier circuit controls the CRT intensity level from several inputs. The effect of these input signals is to either increase or decrease the trace intensity, or to completely blank portions of the display. Fiq. 3-15 shows a detailed block diagram of the Z Axis Amplifier circuit. A schematic of this circuit is shown on diagram 16 at the rear of this manual.

## Input Amplifier

The input transistor, Q1014, in the Input Amplifier stage is a current-driven, low-input impedance amplifier. It provides temination for the input signals as well as isolation between the input signals and the following stages. The current signals from the various central sources are connected to the emitter of Q1014 and the sum or difference of the signals determines the collector conduction level. D1015 and D1016 in the collector provide limiting protection at minimum intensity. When the INTENSITY control is set fully counterclockwise (minimum), the collector current of Q1014 is reduced and its collector rises positive. D1015 is reverse biased to block the control current at the base of Q1023, and Q1016 is forward biased to protect the circuit by clamping the collector af Q1014 about 0.5 volts more positive than the emitter level of Q1023. This limiting action also takes place when a blanking signal is applied. The clamping of D1016 allows Q1014 to recover faster to produce a sharper display with sudden changes in blanking level. At nomal intensity levels, D1016 is reverse biased and the signal from Q1014 is coupled to emitter follower Q1023 through D1015.

The input signals vary the current drive to the emitter of Q1014, which produces a collector level that detemines the brilliance of the display. The INTENSITY control sets the quiescent level at the emitter of Q1014. When R1005 is tumed in the clockwise direction, more current from the INTENSITY control is added to the emitter circuit of Q1014 which results in an increase in collector current to provide a brighter trace. However, the vertical chopped blanking, Z Axis Input and $A$ and $B$ unblanking signals determine whether the trace is visible. The vertical chopped blanking signal blanks the trace during dual-trace switching. This signal


Fig. 3-15. Z Axis Amplifier detailed block diagram.
decreases the current through Q101 4 during the trace switching time to blank the CRT display. The extemal blanking input allows an extemal signal connected to the Z AXIS INPUT connector to change the trace intensity. A positivegoing signal connected to the Z AXIS INPUT connector decreases trace intensity and a negative-going signal increases trace intensity. The A and B unblanking gate signals from the A and B Sweep Generator circuits blank the CRT during sweep retrace and recovery time so there is no display on the screen. When the Sweep Generator circuits are reset and recovered, (see A and B Sweep Generator discussion for more information) the next trigger initiates the sweep and an unblanking gate signal is generated in the A ar B Sweep Generator circuit that goes negative to allow the emitter current to reach the level established by the INTENSITY control and the other blanking inputs.

## Output Amplifier

The resultant signal produced from the various inputs by the Input Amplifier stage is connected to the base of Q1024 through C1029 and to the base of Q1034 through R1024. These transistors are connected as a collector-coupled complementary amplifier. This configuration provides a linear, fast output signal with minimum quiescent power.

The ZAxis Amplifier circ uit is a shunt-feedback operational amplifier with feedback from the Output Amplifier stage to the Input Amplifier stage through C1036-C 1037-R1036. The output voltage is determined by the input curent times the feedback resistor and is shown by the formula; $\mathrm{E}_{\text {out }}=\mathrm{i}_{\text {in }} \times$ $\mathbf{R}_{\mathrm{fb}}$ where $\mathrm{R}_{\mathrm{fb}}$ is R1036. The unblanking input curent change is approximately two milliamperes. Therefore, the output voltage change is about 60 volts ( $2 \mathrm{~mA} \times 30.1 \mathrm{k} \Omega$ ). Cl036
adjusts the feedback circuit for optimum high-frequency response.

Zener diode D1043 connected between +75 volts and +150 volts through D1044, R1044 and R1043 produces a +90 -volt level at the cathode of D1043. This voltage establishes the correct operating level for the Geometry adjustment in the CRT Circuit ond establishes the comect collector level for Q1043. D1045 connected from base to emitter of Q1043 improves the response of Q1043 to negative-going signals. When the base of Q1043 is driven negative to cutoff, D1045 is forward biased and conducts the negative-going portion of the unblanking signal. This provides a fast falling edge on the unblanking gate to quickly tum the display off. The output unblanking gate at the emitter of Q1043 is connected to the CRT circ uit through R1046.

## CRT CIRCUIT

## General

The CRT Circuit provides the high voltoge and control circuits necessory for operation of the cathode-ray tube (CRT). Fig. 3-16 Shows a detailed block diagram of the CRT Circuit. A schematic, of this circuit is shown on diagram 16 at the rear of this manual.

## High-Voltage Oscillator

Q930 and associated circuitry comprise a class C oscillator ${ }^{20}$ to produce the drive for the high-voltage transformer, 1930. When the instrument is tumed on, the current through R925 charges C913 positive and Q930 is forward biased.

[^8]

Fig. 3-16. CRT Circuit detailed block diagram.

The collector current of Q930 increoses and a voltage is developed across the collector winding of T930. This produces a corresponding voltage increase in the feedback winding of 1930 which is connected to the base of Q930, and it conducts even harder. While Q930 is on, its base current exceeds the current through R925 and C913 charges negatively. Eventually the rate of collector curent increase in Q930 becomes less than that required to maintain the voltage across the collector winding and the output voltage drops. This tums off Q930 by way of the feedback voltage to the base. The voltage waveform at the collector of Q930 is a sine wave at the resonant frequency of T930. Q930 remains off until a little less than one cycle later when C913 discharges sufficiently to raise the voltage at the base of Q930 positive enough to bias Q930 into conduction again. The cycle repeats at a frequency of 40 to 50 kilohertz. The amplitude of sustained oscillation depends upon the average current delivered to the base of Q930.

Fuse $F 937$ protects the +12 -volt Supply if the High-Voltage Oscillator stage is shorted. C937 and L937 prevent the current changes at the collector of Q930 from affecting the +12 -volt regulator circuit.

## High-Voltage Regulator

Feedback from the secondary of 1930 is connected to the base of Q914 through the voltage divider network R901R910. This sample of the output voltage is compared to the -12 -volt level at the emitter of Q 914 . It is then amplified by Q914 and Q913 and applied to the base of Q923. Amplitude of the oscillations at the collector of Q930
is determined by the average DC level at the emitter of Q923.

Regulation takes place as follows: If the output voltage at the -1950V test point starts to go positive (less negative), a sample of this positive-going voltage is applied to the base of Q914. Q914 is forward biased and it, in tum, forward biases Q913 to increase the conduction of Q923. An increase in current through Q923 raises the average voltage level of its emitter which is connected to the base of Q930 through the feedback winding of T930. A more positive level at the base of Q930 increases the collector current to produce a larger induced voltage in the secondary of 1930. This increased voltage appears as a more negative voltage at the -1950 V test point to correct the original positivegoing change. By sampling the output from the cathode supply in this manner, the total output of the high-voltage supply is held constant.

Output voltage level of the high-voltage supply is controlled by the High Voltage adjustment, R900, in the base circuit of Q914. This adjustment sets the conduction level of Q914 which controls the quiescent conduction of Q913, Q923 and Q930 similar to the manner just described for a change in output voltage.

## High Voltage Rectifiers and Output

The high-voltage transformer, T930, has five output windings. Two of these windings provide filament voltage for the rectifier tubes V952 and V962. A third low-voltage winding provides filament voltage for the cathode-ray tube. The
filament voltage can be supplied from the high-voltage supply since the cathode-ray tube has a very low filament current drain. Two high-voltage windings provide the negative and positive accelerating voltage and the CRT grid bias voltage. All of these outputs are regulated by the HighVoltage Regulator stage in the primary of 1930 to hold the output voltage constant.

Positive accelerating potential is supplied by voltage doubler V952 and V962. Regulated voltage output is about +8 kilovolts. Ground retum for this supply is through the resistive helix inside the cathode-ray tube to pin 7 and then to ground through R972.

The negative accelerating potential for the CRT cathode is supplied by the half-wave rectifier D952. Voltage output is about -1.95 kilovolts. A sample of this output voltage is connected to the High-Voltage Regulator stage to provide a regulated high-voltage output.

The half-wave rectifier D940 provides a negative voltage for the control grid of the CRT. Output level is adjustable by R940, CRT Grid Bias adjustment. The neon bulbs B973, B974 and B975 provide protection if the voltage difference between the control grid and cathode exceeds about 165 volts. The unblanking gate from the Z Axis Amplifier is applied to the positive side of this circuit to produce a change in output voltage to control CRT intensity, unblanking, dual-trace blanking and intensity modulation.

## CRT Control Circuits

Focus of the CRT display is controlled by the FOCUS control, R967. Divider R963-R968 is connected between the CRT cathode supply and ground. The voltage applied to the focus grid is more positive (closer to ground level) than the voltage on either the control grid or the CRT cathode. The ASTIG adjustment, R985, which is used in conjunction with the FOCUS control to provide a well-defined display, varies the positive level on the astigmatism grid. The +90 -volt source for this control is provided by zener diode D1043 in the $Z$ Axis Amplifier circuit.

Geometry adjustment, R982, varies the positive level on the horizontal deflection plate shields to control the overall geometry of the display. Two adjustments control the trace alignment by varying the magnetic fields around the CRT. The Y Axis Align adjustment, R989, controls the current through L989 which affects the CRT beam after vertical deflection but before horizontal deflection. The TRACE ROTATION adjustment, R980, controls the curent through L980 and affects both vertic al and horizontal rotation of the beam.

## External Z Axis Input

A signal applied to the Z AXIS INPUT connector (see Z Axis Amplifier schematic) is applied to the CRT cathode through C979-C976-R976. DC and low frequency Z-axis signals are blocked from the CRT circuit by C979. They are connected to the Z Axis Amplifier circuit to produce an increase or decrease in intensity, depending upon polarity. C976 and C979 couple high-frequency signals directly to the CRT cathode to produce the same resultant display as the Z Axis Amplifier circuit produces for low-frequency signals.

This configuration operates as a crossover network to provide nearly constant intensity modulation from DC to 50 megahertz.

LOW - V OLTA G P POWER SUPPLY

## General

The low-voltage Power Supply circuit provides the operating power for this instrument from three regulated supplies and one unregulated supply. Electronic regulation ${ }^{11}$ is used to provide stable, low-nipple output voltages. Each regulated supply contains a short-protection circuit to prevent instrument damage if a supply is inadvertently shorted to ground. The Power Input stage includes the Line Voltage Selector assembly. This assembly allows selection of the nominal operating voltage and regulating rcmge for the instrument. Fig. 3-17 shows a detailed block diagram of the Power Supply circuit. A schematic of this circuit is shown on diagram 17 at the rear of this manual.

## Power Input

Power is applied to the primary of transformer T1101 through the 115 -volt line fuse F1101, POWER switch SW1101, themal cutout TK1101, Voltage Selector switch SW1102 and Range Selector switch SW1103. The Voltage Selector switch SW1102 connects the split primaries of 71101 in parallel for 115 -volt nominal operation, or in series for 230 -volt nominal operation. A second line fuse, F1102, is connected into the circuit when the Voltage Selector switch is set to the 230 V position to provide the correct protection for 230 -volt operation (F1102 current rating is one-half of F1101). The fan is connected across one half of the split primary winding so it always has about 115 volts applied to it.

The Range Selector switch, SW1103, allows the instrument to regulate correctly on higher or lower than nomal line voltages. Each half of the primary has taps above and below the 115 -volt ( 230 ) nominal point. As the Range Selector switch, SW1103, is switched from LO to M to HI, more tums are effectively added to the primary winding and the tums ratio is decreased. This provides a fairly constant voltage in the secondary of 71101 even through the primary voltage has increased.

Themal cutout TK1101 provides themal protection for this instrument. If the intemal temperature of the instrument exceeds a safe operating level, TK1101 opens to intemupt the applied power. When the temperature retums to a safe level, TK1101 automatically closes to reapply the power.

## -12-volt Supply

The -12-Volt Supply provides the reference voltage for the remaining supplies. The output from the secondary of T1101 is rectified by bridge rectifier D112A-D. This voltage is filtered by C1112 and then applied to the -12-Volt Series Regulator stage to provide a stable output voltage. The Series Regulator can be compared to a variable resistance which is changed to control the output current. The curent through the Series Regulator stage is controlled by the Error Amplifier to provide the correct regulated output voltage.

[^9]

Fig. 3-17. Power Supply detailed block diagram.

The Error Amplifier is connected as a comparator. Reference voltage for the comparator is provided by zener diode D1114 which sets the base of Q1114 at about -9 volts. The base level of Q1124 is determined by voltage divider R1121-R1122-R1123 between the output of this supply and ground. R1122 is adjustable to set the output voltage of this supply to -12 volts. R1119 is the emitter resistor for both comparator transistors and the current through it divides between Q1114 and Q1124. The output current of the Error Amplifier stage controls the conduction of the Series Regulator stage (through Q1133). This output current changes to provide a canstant, low-ripple -12-volt output level. This occurs as follows: The -12-volt regulatar maintains equal voltage at the bases of the Error Amplifier transistors Q1114 and Q1124. If the -12 Volts adjustment R1122, is tumed clockwise, the current through Q1124 increases (Q1124 base tends to go more positive than the base of Q1114) and the current through Q1114 decreases. Decreased current through Q1114 produces less voltage drop across R1117 and the base of Q1133 goes positive. The emitter of Q1133 pulls the base of Q1137 positive to increase the current through the load, thereby increasing the output voltage of the supply. This places more voltage across divider R1121-R1122-R1123 and the divider action retums the base of Q1124 to about -9 volts. A similar, but opposite, action takes place when R1122 is tumed counterclockwise so the base of Q1124 is more negative than the base of Q1114. The - 12 Volts adjustment R1122, is set to provide a -12-volt level at the output of this supply.

The output voltage is regulated to provide a constant voltage to the load by feeding a sample of the output back to the Series Regulator, Q1137. For example, assume that the output voltage increases (more negative) because of a change in load or an increase in line voltage. This negative-going level at the output is applied across the voltage divider R1121-R1122-R1123 and the base of Q1124 goes negative also. This reduces the current flow through Q1124 which allows Q1114 to conduct more and its collector goes negative. When the collector of Q1114 goes negative, the bias on Q1133 is reduced, resulting in reduced current through the Series Regulator, Q1137. Reduced curent through Q1137 also means that there is less current through the load and the output voltage decreases (less negative). In a similar manner the Series Regulator and Error Amplifier stages compensate for output changes due to ripple.

The Short-Protection Amplifier stage, Q1129, protects the -12-Volt Supply if the output is shorted. For nomal operation, the emitter-base voltage of Q1129 is not enough to bias it on. However, when the output is shorted, high curent is demanded from the -12-Volt Supply, and this curent flows through R1129. The voltage drop across R1129 becomes sufficient to forward bias Q1129 and its collector current produces an increased voltage drop across R1117. The increased voltage drop across R1117 reduces the current flow of both Q1133 and Q1137 to limit the output current.

## +12 -Volt Supply

Rectified voltage for operation of the +12 -Volt Supply is provided by D1142 A-D. This voltage is filtered by C1142 and connected to the +12 -Volt Supply Series Regulator and to the High-Voltage Oscillator stage in the CRT Circuit. Reference voltage for this supply is provided by voltage divider

R1151-R1152-R1153 between the regulated -12 volts and the output of this supply. The -12 volts is held stable by the -12 -Volt Supply as discussed previously. If the +12 -volt output changes, a sample of this change appears at the base of Q1154 as an error signal. Regulation of the output voltage is controlled by the +12 -Volt Series Regulator stage, Q1167, in a similar manner to that described for the -12Volt Supply. The +12 Volts adjustment, R1152, sets the output level to +12 volts. D1152 provides themal compensation for the Error Amplifier. C1164 improves response of the regulator circuit to AC changes at the output.

Shorting protection is provided by Q1159 and R1159. If the output of this supply is shorted, Q1159 is biased on to limit the conduction of the Series Regulator in the same manner as described for the -12-Volt Short-Protection Amplifier. D1164 protects Q1154 when the output of this supply is shorted.

## +75-Volt Supply

D1172 A-D provides the rectified voltage for the +75 Volt Supply. C1172 filters the rectified voltage which is connected to the +75 -Volt Series Regulator. Reference voltage for this supply is provided by voltage-divider R1181-R1182R1183 between the regulated -12 volts and the output of this supply. Since the -12 volts is held stable by the -12Volt Regulator circuit, any change at the base of Error Amplifier Q1184 is due to change at the output of the $+75-$ Volt Supply. Regulation of the output voltage is controlled by Error Amplifier Q1184-Q1193 and Series Regulator, Q1197, in a manner similar to that described for the $+12-$ Volt Supply. The +75 Volts adjustment R1182, sets the quiescent conduction level of the Error Amplifier stage to provide an output level of +75 volts. The output of the $+150-$ Volt Supply (unregulated) is connected to the Error Amplifier to provide the required collector supply for stable operation. Zener diode D1209 establishes a volage at its cathode of about +108 volts. Then, R1186, zener diode D1185 and R1185 drop this voltage to the correct level for the operation of Q1184. D1182 provides themal compensation for the Error Amplifier.

Q1189 provides current limiting for this supply through D1188. Quiescently, Q1189 is off and under nomal operating conditions, D1189 is conducting and D1188 is reverse biased. However, when the output is shorted, the increased curent flow thraugh R1187 biases Q1189 on and its collector goes negative. This forward biases D1188 and reverse biases D1189. Now Q1189 limits the collector current of Q1197 through Q1193. F1172 also provides overload protection. D1198 protects the +75 -volt supply from damage if it is shorted to the -12-volt output.

## +150-Volt Unregulated Supply

Rectifiers D1202 and D1212 provide the unregulated output for the +150 -Volt Supply. The output of the +75 -Volt Supply is connected to the negative side of the +150 -Volt Supply to elevate the output level to +150 volts. Diodes D1202 and D1212 are connected as a full-wave center-tapped rectifier and the output is filtered by C1202-C1204-R1204 to hold the output level at about +150 volts. Fuse F1204 protects this supply if the output is shorted.

## 6.3-Volt RMS AC Source

The 6.3 -volt RMS secondary winding of Tl 101 provides power for the POWER ON light, B1107, and the scale illumination lights, B1108 and B1109. The current through the scale illumination lights is controlled by the SCALE IШUM control, R1108, to change the illumination of the graticule line voltage to the A and B Trigger Generatar circuits for line voltage to the A and B Trigger Generaar circuits for intemal triggering at the line frequency. C1105 reduces noise on the line frequency signal.

## VOLTAGE DISTRIBUTION

Diagram 17 also shows the distribution of the output voltages from the Power Supply circuit to the circuit boards in this instrument. The decoupling networks which provide decoupled operating voltages are shown on this Diagram and are not repeated on the individual circuit diagrams.

## C A LIBRATOR

## General

The Calibrator circuit produces a square-wave output with accurate amplitude and frequency. This output is available as a square-wave voltage at the 1 kHz CAL connector or as a square-wave current through the side-panel PROBE LOO P. Fig. 3-18 shows a detailed block diagram of the Calibratar circuit. A schematic of this circuit is shown on diagram 18 at the rear of this manual.

## Oscillator

Q1255 and its associated circuitry comprise a tuned-collector oscillator. ${ }^{12}$ Frequency of oscillation is determined by the LC circuit comprised of the primary of variable transformer T1255 in parallel with C1255. The accuracy and sta-
${ }^{12}$ Lloyd P. Hunter, Pp. 14-3-1 4-7.
bility required to provide an accurate time and frequency reference is obtained by using a capacitor and transformer which have equal but opposite temperature coefficients.

The oscillations of the LC circuit, T1255-C 1255, are sustained by the feedback winding of T1255 connected to the base of Q1255. C 1266 connects a sample of the output of the LC circuit to the base of Q 1265 . The regenerative feedback from the emitter of Q1265 to the emitter of Q1255 produces fast changeover between Q1255 and Q1265 to provide a fast risetime on the output square wave. Frequency of the output square wave can be adjusted by varying the coupling to the feedback winding of T1255. The squarewave signal at the collector of Q 1265 is connected to the Output Amplifier.

## Output Amplifier

The output signal from the oscillator stage saturates Q 1274 to produce the accurate square wave at the output. When the base of Q1274 goes positive, Q1274 is cut off and the output signal drops negative to ground. When its base goes negative, Q1274 is driven into saturation and the output signal rises positive to about +12 volts. The output of the +12 -Volt Supply is adjusted for an accurate one-volt output signal at the 1 kHz CAL connector when the Calibrator switch is set to 1 V .

## Output Divider

The Output Divider, R1275-R1276-R1277, provides two output voltages from the Calibrator circuit. In the 1 V CALBRATOR switch position, voltage is obtained from the callector of Q1274 through R1274. In the . 1 V CALBRATOR switch position, the output is obtained at the junction of voltage divider R1275 and R1276-R1277 to provide one-tenth of the previous output voltage.

Collector current of Q1274 flows through the PROBE LOOP on the side panel. Output curent is a five-millampere square wave.


Fig. 3-18. Calibrator detailed block diagram.

## SECTION 4

## MAINTENANCE

## Introduction

This section of the manual contains maintenance information for use in preventive maintenance, corrective maintenance or troubleshooting of the Type 453.

## Cover Removal

The top and bottom covers of the instrument are held in place by thumb screws located on each side of the instrument. To remove the covers, loosen the thumb screws and slide the covers off the instrument. The covers protect the instrument from dust in the interior. The covers also direct the flow of cooling air and reduce the EMI radiation from the instrument.

## PREVENTIVE MAINTENANCE

## General

Preventive maintenance consists of cleaning, visual inspecon, lubrication, etc. Preventive maintenance performed on a regulor basis may prevent instrument breakdown and will improve the reliability of this instrument. The severity of the environment to which the Type 453 is subjected determines the frequency of maintenance.

## Cleaning

General. The Type 453 should be cleaned as aften os operating conditions require. Accumulation of dirt in the instrument can cause overheating and component breakdown. Dirt on components acts as an insulating blanket and prevents efficient heat dissipation. It also provides an electrical conduction path.

## CAUTION

Avoid the use of chemical cleaning agents which might damage the plastics used in this instrument. Avoid chemicals which contain benzene, toluene, xylene, acetone or similar solvents.

The top and bottom covers provide protection against dust n the interior of the instrument. Operation without the covers in place necessitates more frequent cleaning. The front cover provides dust protection for the front panel and the CRT face. The front cover should be installed for storage or transportation. The plastic cover supplied with the Type 453 provides protection for the outside of the instrument during transportation or storage. The pocket on the side also provides a convenient place to camy this instruction manual.

Air Filter. The air filter should be visually checked every few weeks and cleaned or replaced if dirty. More frequent inspections are required under severe operating conditions. The following procedure is suggested for cleaning the filter.

1. Remove the filter by pulling it out of the retaining frame on the rear panel. Be careful not to drop any of the accumulated dirt into the instrument.
2. Flush the loose dirt from the filter with a stream of hot water.
3. Place the filter in a solution of mild detergent and hot water and let it soak for several minutes.
4. Squeeze the filter to wash out any dirt which remains.
5. Rinse the filter in clear water and allow it to dry .
6. Coat the dry filter with an air-filter adhesive,
7. Let the adhesive dry thoroughly.
8. Re-install the filter in the retaining frame.

Exterior. Loose dust accumulated on the outside of the Type 453 can be removed with a soft cloth or small paint brush. The paint brush is particularly useful for dislodging dirt on and around the front-panel controls. Dirt which remains can be removed with a soft cloth dampened in a mild detergent and water solution. Abrasive cleaners should not be used.

CRT. Clean the plastic light filter, faceplate protector and the CRT face with a soft, lint-free cloth dampened with denatured alcohol. The CRT mesh fiter can be cieaned in the following manner.

1. Hold the filter in a vertical position and brush lightly with a soft \#7 water-color brush to remove light coatings of dust or lint.
2. Greasy residues or dried-on dirt can be removed with a solution of warm water and a neutral-pH liquid detergent. Use the brush to lightly scrub the filter.
3. Rinse the filter thoroughly in clean water and allow to air dry.
4. If any lint or dirt remains, use clean low-pressure air to remove. Do not use tweezers or other hard cleaning tools on the filter, as the special finish may be damaged.
5. When not in use, store the mesh fiiter in a lint-free, dust-proof container such as a plastic bag.

Interior. Dust in the interior of the instrument should be removed occasionally due to its electrical conductivity under high-humidity conditions. The best way to clean the interior it to blow off the accumulated dust with dry, low-velocity air. Remove any dirt which remains with a soft paint brush or a cloth dompened with a mild detergent and water solution. A cotton-tipped applicator is useful for cleaning in narrow spaces or for cleaning ceramic terminal strips and circuit boards.

The high-voltage circuits, particularly parts located in the high-voltage compartment and the area surrounding the post-deflection anode connector, should receive special attention. Excessive dirt in these areas may cause highvoltage arcing and result in improper instrument operation.

## Lubrication

General. The reliability of potentiometers, rotary switches and other moving parts can be maintained if they are kept properly lubricated. Use a cleaning-type lubricant (e.g., Tektronix Part No. 006-0218-00) on switch contacts. Lubricate switch detents with a heavier grease (e.g., Tektronix Part No. 006-0219-00). Potentiometers which are not permanently sealed should be lubricated with a lubricant which does not affect electrical characteristics (e.g., Tektronix Part No. 006-0220-00). The pot lubricant can also be used on shaft bushings. Do not over-lubricate. A lubrication kit containing the necessary lubricants and instructions is available from Tektronix, Inc. Order Tektronix Part No. 003-0342-00.

Fan. The fan-motor bearings are sealed and do not require lubrication.

## Visual Inspection

The Type 453 should be inspected ossasionally for such defects as broken connections, broken or damaged ceramic strips, improperly seated transistors, damaged circuit boards and heat-damaged parts.

The corrective precedure for most visible defects is obvious; however, particular care must be taken if heat-damaged components are found. Overheating usually indicates other trouble in the instrument; therefore, it is important that the cause of over-heating be corrected to prevent recurrence of the damage.

## Transistor Checks

Periodic checks of the transistors in the Type 453 are not recommended. The best check of transistor performance is its actual operation in the instrument. More details on checking transistor operation is given under Troubleshooting.

## Recalibration

To assure accurate measurements, check the calibration of this instrument after each 1000 hours of operation or every six months if used infrequently. In addition, replacement of components may necessitate recalibration of the affected circuits. Complete calibration instructions are given in the Calibration section.

The calibration procedure can also be helpful in localizing cerain troubles in the instrument. In some cases, minor
troubles may be revealed and/or corrected by recalibration.

## TROUBLESHOOTING

## Introduction

The following information is provided to facilitate troubleshooting of the Type 453. Information contained in other sections of this manual should be used along with the following information to aid in locating the defective component. An understanding of the circuit operation is very helpful in locating troubles. See the Circuit Description section for complete information.

## Troubleshooting Aids

Diagrams. Circuit diagrams are given on foldout pages in Section 9. The component number and electrical value of each component in this instrument are shown on the diagrams. Each main circuit is assigned a series of component numbers Table 4-1 lists the main circuits in the Type 453 and the series of component numbers assigned to each. Important voltages and waveforms are also shown on the diagrams. The portions of the circuit mounted on circuit boards are enclosed with a blue line.

TABLE 4-1
Component Numbers

| Component <br> Numbers on <br> Diagrams | Diagram <br> Number | Circuit |
| :---: | :---: | :--- |
| $1-99$ | 1 | Channel 1 Vertical Preamp |
| $100-199$ | 3 | Channel 2 Vertical Preamp |
| $200-299$ | 5 | Vertical Switching |
| $300-399$ | 6 | Vertical Output Amplifier |
| $400-429$ | 7 | Trigger Preamp |
| $430-499$ | 8 | A Trigger Generator |
| $500-599$ | 9 | A Sweep Generator |
| $600-699$ | 10 | B Trigger Generator |
| $700-799$ | 11 | B Sweep Generator |
| $800-899$ | 13 | Horizontal Amplifier |
| $900-999$ | 16 | CRT Circuit |
| $1000-1099$ | 15 | Z Axis Amplifier |
| $1100-1199$ | 17 | Power Supply and Distribution |
| $1250-1299$ | 18 | Calibrator |

Switch Wafer Identification. Switch wafers shown on the diagrams are coded to indicate the position of the wafer in the complete switch assembly. The numbered portion of the code refers to the wafer number counting from the front, or mounting end of the switch, toward the rear. The letters F and R indicate whether the front or rear of the wafer performs the particular switching function. For example, a wafer designated 2 R indicates that the rear of the second wafer from the front is used for this particular switching function.

Circuit Boards Fig. 4-6 through 4-14 show the circuit boards used in the Type 453 . Fig. 4-5 shows the location of each board within the instrument. Each electrical component on the boards is identified by its circuit number.

The circuit boards are also outlined on the diagrams with a blue line. These pictures, used along with the diagrams, aid in locating the components mounted on the circuit boards.

Wiring Color-Code. All insulated wire and cable used in the Type 453 is color-coded to facilitate circuit tracing. Signal camying leads are identified with one or two colored stripes. Voltage supply leads are identified with three stripes to indicate the approximate voltage using the EIA resistor color code. A white background color indicates a positive voltage and a tan background indicates a negative voltage. The widest color stripe identifies the first color of the code. Table 4-2 gives the wiring color-code for the power-supply voltages used in the Type 453.

TABLE 4-2
Power Supply Wiring Color Code

| Supply | Back- <br> ground <br> Color | First <br> Stripe | Second <br> Stripe | Third <br> Stripe |
| :---: | :--- | :--- | :--- | :--- |
| -12 volt | Tan | Brown | Red | Black |
| +12 volt | White | Brown | Red | Black |
| +75 volt | White | Violet | Green | Black |
| +150 volt | White | Brown | Green | Brown |

Resistor Color-Code. In addition to the brown composition resistors, some metal-film resistors and some wirewound resistors are used in the Type 453. The resistance values of wire-wound resistors are printed on the body of the component. The resistance values of composition resistors and metal-film resistors are color-coded on the components with EIA color-code (some metal-film resistors may have the value printed on the body). The color-code is read starting with the stripe nearest the end of the resistor. Composition resistors have four stripes which consist of two significant figures, a multiplier and a tolerance value (see Fiq. $4-1)$. Metal-film resistors have five stripes consisting of three significant figures, a multiplier and a tolerance value.

Capacitor Marking. The capacitance values of common disc capacitors and small elecrolytics are marked in microfarads on the side of the component body. The white ceramic capacitors used in the Type 453 are color coded in picofarads using modified EIA code (se Fia. 4-1).

Diode Color Code. The cathode end of each glass-encased diode is indicated by a stripe, a series of stripes or a dot. For most silicon or germanium diodes with a series of stripes, the color-code also indicates the type of diode and identifies the Tektronix Part Number using the resistor colorcode system (e.g., a diode color-coded blue-brown-graygreen indicates diode type 6185 with Tektronix Part Number


Fig. 4-1. Color code for resistors and ceramic capacitors.


Fig. 4-2. Electrode configuration for semiconductors in this instrument.

152-0185-00). The cathode and anode end of metal-encased diodescan be identified by the diode symbol marked on the body.

Transistor Lead Configuration. Fig. 4-2 shows the lead configurations of the transistors used in this instrument. This view is as seen from the bottom of the transistors.

## Troubleshooting Equipment

The following equipment is useful for troubleshooting the Type 453.

## 1. Transistor Tester

Description: Tektronix Type 575 Transistor-Curve Tracer or equivalent.

Purpose: To test the semiconductors used in this instrument.

## 2. Multimeter

Description: VTVM, 10 megohm input impedance and 0 to 500 volts range; ohmmeter, 0 to 50 megohms. Accuracy, within $3 \%$. Test prods must be insulated to prevent accidental shorting.

Purpose: To check voltages and for general troubleshooting in this instrument.

NOTE
A 20,000 ohms/volt VOM can be used to check the voltages in this instrument if allowances are made for the circuit loading of the VOM at highimpedance points.
3. Test Oscilloscope

Description: DC to 20 MHz frequency response. 5 millivolts to 10 volts/division deflection factor. Use a 10X probe.

Purpose: To check waveforms in this instrument.

## Troubleshooting Techniques

This troubleshooting procedure is arranged in an order which checks the simple possibilities before proceeding with extensive troubleshooting. The first few checks assure proper connection, operation and calibration. If the trouble is not located by these checks, the remaining steps aid in locating the defective component. When the defective component is located, it should be replaced following the replacement procedures given under Corrective Maintenance.

1. Check Control Settings. Incorrect control settings can indicate a trouble that does not exist. If there is any question about the correct functian or operation of any control, see the Operating Instructions section of this manual.
2. Check Associated Equipment. Before proceeding with troubleshooting of the Type 453, check that the equipment used with this instrument is operating correctly. Check that the signal is properly connected and that the interconnecting cables are not defective. Also, check the power source.
3. Visual Check. Visually check the portion of the instrument in which the trouble is located. Many troubles can be located by visual indications such as unsoldered connections, broken wires, damaged circuit boards, damaged components, etc.
4. Check Instrument Calibration. Check the calibration of this instrument, or the affected circuit if the trouble exists in one circuit. The apparent trouble may only be a result of misadjustment or may be corrected by calibration. Complete calibration instructions are given in the Calibration section of this manual.
5. Isolate Trouble to a Circuit. To isolate trouble to a circuit, note the trouble symptom. The sympton often identifies the circuit in which the trouble is located. For example, poor focus indicates that the CRT (includes high voltage) circuit is probably at fault. When trouble symptoms appear in more than one circuit, check affected circuits by taking voltage and waveform readings. Also check for the correct output signals at the side-panel output connectors with a test oscilloscope. If the signal is correct, the circuit is working correctly up to that point. For example, correct amplitude and time of the A Gate out waveform indicates that the A Trigger Generatar and A Sweep Gate circuits are operating corectly.

Incorrect operation of all circuits often indic ates trouble in the power supply. Check first for corect voltage of the individual supplies. However, a defective component elsewhere in the instrument can appear as a power-supply trouble and may also affect the operation of other circuits. Table 4-3 lists the tolerances of the power supplies in this instrument. [f a power-supply voltage is within the listed tolerance, the supply can be assumed to be working correctly. If outside the tolerance, the supply may be misadjusted or operating incorrectly. Use the procedure given in the Calibration section to adjust the power supplies.

TABLE 4-3
Power Supply Tolerance

| Power Supply | Tolerance |
| :---: | :---: |
| -12 volt | $\pm 0.12$ volt |
| +12 voit | 12.1 volts, $\pm 0.21$ volt ${ }^{1}$ |
| +75 volt | $\pm 0.75$ volt |
| -1950 volt | $\pm 58.5$ volts |

## ${ }^{1}$ Adjusted for correct output from the Calibrator circuit; see Calibration procedure.

Fiq. 4-3 provides a guide to aid in locating a defective circuit. This chart may not include checks for all possible defects; use steps 6-8 in such cases. Start from the top of the chart and perform the given checks on the left side of
the page until a step is found which is not corect. Further checks and/or the circuit in which the trouble is prabably located are listed to the right of this step.

After the defective circuit-has been located, proceed with steps 6 through 8 to locate the defective component(s).
6. Check Circuit Board Interconnections. After the trouble has been isolated to a particular circuit, check the pin connectors on the circuit board for correct connection. Figs. 4-8 through 4-16 show the correct connections for each board.

The pin connectors used in this instrument also provide a convenient means of circuit isolation. Far example, a short in a power supply can be isolated to the power supply itself by disconnecting the pin connectors for that voltage at the remaining boards.
7. Check Voltage and Waveforms. Often the defective component can be located by checking for the correct voltage or waveform in the circuit. Typical voltages and waveforms are given on the diagrams.

## NOTE

Voltages and wavefarms given on the diagrams are not absolute and may vary slightly between instruments. To obtain operating conditions similar to those used to take these readings, see the first diagram page.
8. Check Individual Components. The following procedures describe methods of checking individual components in the Type 453. Components which are soldered in place are best checked by disconnecting one end. This isolates the measurement from the effects of surrounding circuitry.
A. TRANSISTORS. The best check of transistor operation is actual performance under aperating conditions. If a transistor is suspected of being defective, it can best be checked by substituting a new component or one which has been checked previously. However, be sure that circuit conditions are not such that a replacement transistor might also be damaged. If substitute transistors are not available, use a dynamic tester (such as Tektronix Type 575). Statictype testers are not recommended, since they do not check operation under simulated operating conditions.
B. DIODES. A diode can be checked for an open or shorted condition by measuring the resistance between terminals. With an ohmmeter scale having an intemal source of between 800 millivolts and 3 volts, the resistance should be very high in one direction and very low when the leads are reversed.

## CAUTION

Do not use an ohmmeter scale that has a high internal current. High currents may damage the diode. Do not measure tunnel diodes with an ohmmeter; use a dynamic tester (such as a Tektronix Type 575 Transistor-Curve Tracer).
C. RESISTORS. Check the resistors with an ohmmeter. Check the Electrical Parts List for the tolerance of the resistors used in this instrument. Resistors normally do not need to be replaced unless the measured value varies widely from the specified value.


D. INDUCTORS. Check for open inductors by checking continuity with an ohmmeter. Shorted or partially shorted inductors can usually be found by checking the waveform response when high-frequency signals are passed through the circuit. Partial shorting often reduces high-frequency response (roll-off).
E. CAPACITORS. A leaky or shorted capacitor can best be detected by checking resistance with an ohmmeter on the highest scale. Do not exceed the voltage rating of the capacitor. The resistance reading should be high after initial charge of the capacitor. An open capacitor can best be detected with a capacitance meter or by checking whether the capacitor passes AC signals.
9. Repair and Readjust the Circuit. If any defective parts are located, follow the replacement procedures given in this section. Be sure to check the performance of any circuit that has been repaired or that has had any electrical components replaced.

## CORRECTIVE MAINTENANCE

## General

Corrective maintenance consists of component replacement and instrument repair. Special techniques required to replace components in this instrument are given here.

## Soldering Techniques

## WARNING

Disconnect the instrument from the power source before soldering.

Circuit Boards. Use ordinary $60 / 40$ solder and a 35 - to 40 -watt pencil type soldering iron on the circuit boards. The tip of the iron should be clean and properly tinned for best heat transfer to the solder joint. A higher wattage soldering iron may separate the wiring from the base material.

The following technique should be used to replace a component on a circuit board. Most components can be replaced without removing the boards from the instrument.

1. Grip the component lead with long-nose pliers. Touch the soldering iron to the lead at the solder connection. Do not lay the iron directly on the board.
2. When the solder begins to melt, pull the lead out gently. This should leave a clean hole in the board. If not, the hole can be cleaned by reheating the solder and placing a sham object such as a toothpick into the hole to clean it out. A vacuum-type resoldering tool can also be used for this purpose.
3. Bend the leads of the new component to fit the holes in the board. If the component is replaced while the board is mounted in the instrument, cut the leads so they will just protrude through the board. Insert the leads into the holes in the board so the component is firmly seated against the board (or as positioned originally). If it does not seat properly, heat the solder and gently press the component into place.
4. Touch the iron to the connection and apply a small amount of solder to make a firm solder joint; do not apply too much solder. To protect heat-sensitive components, hold the lead between the component body and the solder joint with a pair of long nose pliers or other heat sink.
5. Clip the excess lead that protrudes through the board.
6. Clean the area around the solder connection with a flux-remover solvent. Be careful not to remove information printed on the board.

Ceramic Terminal Strips. Solder used on the ceramic terminal strips should contain about $3 \%$ silver. Use a 40to 75 -watt soldening iron with a $1 / 8$-inch wide wedge-shaped tip. Ordinary solder should not be used
on the ceramic teminal strips. If ordinary solder is used repeatedly or if excessive heat is applied, the solder-to-ceramic bond may be broken.

A sample roll of solder containing about $3 \%$ silver is mounted on the rear subpanel of this instrument. Additional solder of the same type should be available locally, or it can be procured under FSN 3439-912-8698.

Observe the following precautions when soldering to ceramic terminal strips

1. Use a hot iron for a shorT time. Apply only enough heat to make the solder flow freely.
2. Maintain a clean, properly tinned tip.
3. Avoid putting pressure on the ceramic teminal strip.
4. Do not attempt to fill the terminal-strip notch with solder, use only enough solder to cover the wires adequately.
5. Clean the flux from the terminal strip with a fluxremover solvent.

Metal Terminals. When soldering metal terminals (e.g., switch terminals, potentiometers, etc), ordinary $60 / 40$ solder can be used. Use a soldering iron with a 40- to 75 -watt rating and a $1 / 8$-inch wide wedge-shaped tip.

Observe the following precautions when soldering metal teminals:

1. Apply only enough heat to make the solder flow freely.
2. Apply only enough solder to form a solid connection. Excess solder may impair the function of the part.
3. If a wire extends beyond the solder joint, clip off the excess.
4. Clean the flux from the solder joint with a flux-remover solvent.

## Component Replacement

## WARNING

Disconnect the instrument from the power source before replacing components.

Removing the Rear Panel. The rear panel must be removed for access to the rear subpanel. This panel can be removed by removing the Z Axis ground strap and the four screws located near the rear feet.

Swing-Out Chassis. Some of the controls and connectors are mounted on a swing-out chassis on the right side of this instrument. To reach the rear of this chassis or the components mounted behind it, first remove the top cover from the instrument. Then, loosen the captive securing screw so the chassis can swing outward.

Ceramic Terminal Strip Replacement. A complete ceramic terminal strip assembly is shown in Fiq. 4-4. Replacement strips (including studs) and spacers are supplied under separate part numbers. However, the old spacers may be re-used if they are not damaged. The applicable Tektronix Part Numbers for the ceramic strips and spacers used in this instrument are given in the Mechanical Parts List.

To replace a ceramic teminal strip, use the following pracedure:

## REMOVAL:

1. Unsolder all components and connections on the strip. To aid ih replacing the strip, it may be advisable to mark


Fig. 4-4. Troubleshooting chart for Type 453.
each lead or draw a sketch to show location of the components and connections.
2. Pry or pull the damaged strip from the chassis. Be careful not to damage the chassis.
3. If the spacers come out with the strip, remove them from the stud pins for use on the new strip (spacers should be replaced if they are damaged).

## REPLACEMENT:

1. Place the spacers in the chassis holes.
2. Carefully press the studs of the strip into the spacers until they are completely seated. If necessary, use a soft mallet and tap lightly, directly over the stud, to seat the strip completely.
3. If the stud extends through the spacers, cut off the excess.
4. Replace all components and connections. Observe the soldering precautions given under Soldering Techniques in this section.

Circuit Board Replacement. If a circuit board is damaged beyond repair, either the entire assembly including all soldered-on components, or the board only, can be replaced. Part numbers are given in the Mechanic al Parts List for either the completely wired or the unwired board. Most of the components mounted or, the circuit boardscan be replaced without removing the boards from the instrument. Observe the soldering precautions given under Soldering Techniques in this section. However, if the bottom side of the board must be reached orif the board must be moved to gain access to other areas of the instrument, only the mounting screws need to be removed. The interconnecting wires on most of the boards are long enough to allow the board to be moved out of the way or tumed over without disconnecting the pin connectors.

## G ENERAL:

Most of the connections to the circuit boards are made with pin connectors. However, several connections are soldered between the attenuators and Vertical Preamp board. See the special removal instructions to remove these as a unit.

Use the following procedure to remove a circuit board.

1. Disconnect all pin connectors which come through holes in the board.
2. Remove all screws holding the board to the chassis.
3. The board may now be lifted for maintenance oraccess to areas beneath the board.
4. To completely remove the board, disconnect the remaining pin connectors.
5. Lift the circuit board out of the instrument. Do not force or bend the board.
6. To replace the board, reverse the order of removal. Correct location of the pin connectors is shown ir Fig. 4-8 through 4-16. Replace the pin connectors (carefully so they mate correctly with the pins. If forced into place incorrectly positioned, the pin connectors may be damaged.
VERTICAL PREAMP UNIT REMOVAL:
Use the following procedure to remove the Vertical Preamp board and the attenuators as a unit.
7. Remove the screw (mounted with a washer) which holds the MODE-TRIGGER switch (rear of board) to the chassis. The other screw may be left in place.
8. Remove the screw (with fiber washer) from the center of the board.
9. Unsolder the connections on he MODE TRIGGER switch which do not go to the Vertical Preamp board.
10. Disconnect all pin connectors which lead off of the Vertical Preamp board.
11. Remove the attenuator shield and remove the nuts (four) located under this shield at each side of the INPUT connectors.
12. Remove the VARIABLE, CH 1 and CH 2 VOLTS/DIV, POSITION, Input Coupling, TRIGGER and MODE knobs.
13. Remove the securing nuts on the VOLTS/DIV switches and the STEP ATIEN BAL controls.
14. Remove the three screws at the rear of the board.
15. Lift up on the rear of the assembly and slide it out of the instrument.
16. The board may now be removed from the Vertical Preamp unit as follows:
a. Disconnect all pin connectors remaining on the board.
b. Unsolder all connections on the rear side of the board which connect between the attenuators and the board. Observe the soldering precautions given in this section.
c. Remove the remaining screw whichi holds the MODETRIGGER switch to the board.
d. Remove the four screws holding the board to the attenuators.
17. To replace the unit, reverse the order of removal. Be sure the GAIN and INVERT extensions are positioned correctly in the corresponding front-panel holes.

Cathode-Ray Tube Replacement. Use care when handling a CRT. Protective clothing and safety glasses should
be wom. Avoid striking it on any object which might cause it to crock or implode. When storing a CRT, place it face down on a smooth surface with a protective cover or soft mat under the faceplate to protect it from scratches.

The CRT shield should also be handled carefully. This shield protects the CRT display from distortion due to magnetic interference. If the shield is dropped or struck sharply, it may lose its shielding ability.

The following procedure outlines the removal and replacement of the cathode-ray tube:

## A. REMOVAL:

1. Remove the top and bottom covers and rear panel as described previously.
2. Remove the light filter or faceplate protector.
3. Disconnect the CRTanode connector. Ground this lead and the anode conection to discharge any stored charge.
4. Unsolder the trace-rotation leads at the CRT shield.
5. Unsolder the $y$-axis rotation leads at the $Y$ Axis Align control.
6. Disconnect the deflection-plate connectors. Be careful not to bend the deflection-plate pins.

## 7. Remove the CRT socket.

8. Remove the two nuts (by the graticule iights) which hold the front of the CRT shield to the subpanel.
9. Remove the graticule lights from the studs and position them away from the shield.
10. Loosen the two hex-head screws inside the rear of the CRT shield. Remove the shield angle clamps and mounting screws.
11. Slide the CRT assembly to the rear of the instrument until the faceplate clears the mounting studs. Then, lift the front of the CRT assembly up and slide it out of the instrument.
12. Loosen the three screws on the CRT clamp inside the CRT shield. Do not remove the screws.
13. Hold the left hand on the CRT faceplate and push forward on the CRT base with the right hand. As the CRT starts out of the shield, grasp it firmly with the left hand. When the CRT is free of the clamp, slide the shield completely off the CRT. Be careful not to bend the neck pins.

## B. REPLACEMENT:

1. Insert the CRT into the shield. Be careful not to bend the neck pins. Seat the CRT firmly against the shield.
2. Tighten the bottom clamp screw-inside the CRT shield. Recommended tightening torque: 4 to 7 inch-lbs. Do not tighten the screws on the sides.
3. Place the light mask over the CRT faceplate.
4. Using a method similar to that for removal (step 11) re-insert the CRT assembly into the instrument. Be sure the CRT faceplate seats properly in the subpanel.
5. Tighten the two remaining screws on the inside of the CRT shield.
6. Replace the shield angle clamps and mounting screws on the rear subpanel. Tighten the two hex-head screws inside the rear of the CRT shield.
7. Replace the graticule lights and securing nuts.
8. Replace the CRT socket.
9. Reconnect the anode connector. Align the jack on the CRT and then plug in the connector and press fimlly on the insulated cover to snap the plug into place.
10. Reconnect the trace-rotation and $y$-axis leads.
11. Reconnect the deflection-plate connectors. Correct location is indicated on the CRT shield.
12. Adiust the High Voltage, TRACE ROTATION, ASTIG, Y-Axis Align and Geometry adjustment. Adjustment procedure is given in the Calibration sectian. Also check the basic vertical and horizontal gain.

Transistor Replacement. Transistors should not be replaced unless actually defective. If removed from their sockets during routine maintenance, retum them to their original sockets. Unnecessary replacement of transistors may affect the calibration of this instrument. When transistors are replaced, check the operation of that part of the instrument which may be affected.

## CAUTION

POWER switch must be tumed off before removing or replacing transistors.

Replacement transistors should be of the original type or a direct replacement. Fig. 4-2 shows the lead configuration of the transistors used in this instrument. Some plastic case transistors have lead configurations which do not agree with those shown here. If a transistor is replaced by a transistor which is made by a different manufacturer than the original, check the manufacturer's basing diagram for correct basing. All transistor sockets in this instrument are wired for the basing used for metal-case transistors. Transistors which have heat radiators or are mounted on the chassis use silicone grease to increase heat transfer. Replace the silicone grease when replacing these transistors.

## WARNING

Handle silicone grease with care. Avoid getting silicone grease in the mouth or eyes. Wash hands thoroughly after use.

Two transistors in both the Channel 1 and Channel 2 Preamp circuit (Vertical Preamp circuit board) are permanently mounted in special temperature compensation blocks. These transistors (along with the temperature compensation block) must be replaced as a unit. When replacing the unit, place it so the reference information faces the left side of the instrument and the PNP transistor (labeled on side of unit) is toward the front of the instrument.

Fuse Replacement. Table 4-4 gives the rating, location, and function of the fuses used in this instrument.

Rotary Switches. Individual wafers or mechanical parts of rotary switches are nomally not replaceable. If a switch is defective, replace the entire assembly. Replacement switch-
es can be ordered either wired or unwired; refer to the Parts List for the applicable part numbers.

When replacing a switch, tag the leads and switch teminals with corresponding identification tags as the leads are disconnected. Then, use the old switch as a guide for installing the new one. An altemative method is to draw a sketch of the switch layout and record the wire colorat each terminal. When soldering to the new switch be careful that

TABLE 4-4
Fuse Ratings

| Circuit <br> Number | Rating | Location | Function |
| :---: | :---: | :--- | :--- |
| F937 | 2A Fast | Rear subpanel | High voltage |
| F1101 | 2A Fast | Line Voltage <br> Selector assembly | 115-volt line |
| F1102 | 1A Fast | Line Voltage <br> Selector assembly | 230-volt line |
| F1172 | $0.5 A$ Fast | By power <br> transformer | +75 volts |
| F1204 | $0.25 A$ Fast | By power <br> transformer | +150 volts |

the solder does not flow beyond the rivets on the switch terminals. Spring tension of the switch contact can be destroyed by excessive solder.

The swing-out chassis on the right side of the instrument provides access to the side of the TIME/DIV and HORIZ DISPLAY switches. The top and bottom of these switches can be reached for easier repair or removal by removing the B Sweep board (top) or the A Sweep board (bottom).

Power Transformer Replacement. The power transformer in this instrument is warranted for the life of the instrument. If the power transformer becomes defective, contact your local Tektronix Field Office or representative for a warranty replacement (see the Waranty note in the front of this manual). Be sure to replace only with a direct replacement Tektronix transformer.

When removing the transformer, tag the leads with the corresponding terminal numbers to aid in connecting the new transformer. After the transformer is replaced, check the performance of the complete instrument using the Performance Check procedure.

Power Chassis. The power transistors and other heat dissipating power-supply components are mounted below the Low-Voltage Regulator board. Remove the Low-Voltage Regulator board to reach these components. To reach the underside of the chassis, remove the fan through the rear subpanel.

High-Voltage Compartment. The components located in the high-voltage compartment can be reached for maintenance or replacement by using the following procedure.

1. Remove the bottom cover of the instrument as described in this section.
2. Remove the high-voltage shield.
3. Remove the three screws which hold the cover on the high-voltage compartment.
4. To remove the complete wining assembly from the highvoltage compartment, unsolder the post-deflection anode lead (heavily insulated lead at side of compartment). The other leads are long enough to allow the ossembly to be lifted out of the compartment to reach the parts on the under side.
5. To replace the high-voltage compartment, reverse the order of removal.

## NOTE

All solder joints in the high-voltage compartment should have smooth surfaces. Any protrusions may cause high-voltoge arcing at high altitudes.

## Recalibration After Repair

After any electrical component has been replaced, the calibratian of that particular circuit should be checked, as
well as the calibration of other closely related circuits. Since the low-voltage supply affects all circuits, calibration of the entire instrument should be checked if work has been done in the low-voltage supply or if the power transformer has been replaced. The Performance Check procedure in Section 5 provides a quick and convenient means of checking instrument operation.

## Instrument Repackaging

If the Type 453 is to be shipped for long distances by commercial means of transportation, it is recommended that the instrument be repackaged in the original manner for maximum protection. The original shipping carton can be saved and used for this purpose Fig. 4-5 illustrates how to repackage the Type 453 and gives the part number for the packaging components if new items are needed Fig. 4-6 illustrates how to repackage the Type R453 and the applicable part numbers.

Complete carton assembly; Tektronix Part No. 065-0076-00.

## Includes:

1 - Outer box; 004-0679-00

2 - Case halves (2); 004-0222-00

3 - Plastic bag;, 006-0342-00

4 - Accessory box and pad; 004-0685-00


Instrument placed in plastic bag, item 3 (not shown), before packaging

## Complete carton assembly; Tektronix Part

Ne. 065-0101-00.

## Includes:

1 - Inner box; 004-0460-00

2 - Inner pad sef; 004-0359-00

3 - Side pad set; 004-0360-00
4 - Bottom pad; 004-0357-00

5 - Rear pad (2); 004-0556-00

6 - Outer box; 004-0461-00

7 - Accessories bex; 004-0462-00

8 - Outer pad sel; 004-0361-00


Fig. 4-6. Repackaging the Type R453 for shipment.


Fig. 4-7. Location of circuit boards in Type 453.


Fig. 4-8. Vertical Output Amplifier circuit board.


Fig. 4-9. Partial Vertical Preamp circuit board. Vertical Switching and partial Vertical Preamp circuit shown.


Fig. 4-10. Partial Vertical Preamp circuit board. Partial Vertical Preamp circuit shown.


Fig. 4-11. Partial A Sweep circuil board. A Sweep Generator and Calibrator circuits shown.

fig. 4-12. Partial A Sweep circuit board. Trigger Preamp and A Trigger Generator circuits shown.


Fig. 4-13. Partial B Sweep circuit board. Horizontal Amplifier and partial B Sweep Generator circuils shown.


Fig. 4-14. Partial B Sweep circuit board. B Trigger Generator and B Sweap Generator circuits shown.


Fig. 4-15. Z Axis Amplifier and High-Voltage Regulator circuif board.


Fig. 4-16. Low Voltage Regulator eireuit board.

# SECTION 

## PERFORMANCE CHECK

## Introduction

This section of the manual provides a procedure for rapidly checking the performance of the Type 453. This procedure checks the operation of the instrument without removing the covers or making intemal adjustments. However, screwdriver adjustments which are located on the front panel are adjusted in this procedure.

If the instrument does not meet the performance requirements given in this procedure, intemal checks and/or adjustments are required. See the Calibration section of this manual. All performance requirements given in this section correspond to those given in Section 1] of this manual.

## NOTE

All waveforms shown in this section are actual waveform photographs taken with a Tektronix Oscilloscope Camera System unless noted otherwise. Graticule lines have been photographically retouched.

## Recommended Equipment

The following equipment is recommended for a complete performance check. Specifications given are the minimum necessary to perform this procedure. All equipment is assumed to be calibrated and operating within the given specifications of the recommended equipment.
For the most accurate and convenient performance check, special Tektronix calibration fixtures are used in this procedure. These special calibration fixtures are available from Tektronix, Inc. Order by part number through your local Tektronix Field Office or representative.

1. Time-mark generator. Marker outputs, five seconds to 10 nanoseconds; marker accuracy, within $0.1 \%$. Tektronix Type 184 Time-Mark Generator recommended.
2. Standard amplitude calibrator. Amplitude accuracy, within $0.25 \%$; signal amplitude, five millivolts to 50 volts; output signal, one-kilohertz square wave and positive DC voltage; must have mixed display feature. Tektronix calibration fixture 067-0502-00.
3. Square-wave generator. Frequency, one and 100 kilohertz; risetime, 12 nanoseconds or less from high-amplitude output and one nanosecond or less from fast-rise output; output amplitude, about 120 volts unterminated or 12 volts into 50 ohms from high-amplitude output-50 to 500 millivolts from fast-rise output. Tektronix Type 106 Square-Wave Generator recommended.
4. Constant-amplitude sine-wave generator. Frequency, 350 kilohertz to above 50 megahertz; reference frequency, 50 kilohertz; output amplitude, variable from five millivolts
to five volts into 50 ohms or 10 volts maximum unterminated; amplitude accuracy, within $3 \%$ at 50 kilohertz and from 350 kilohertz to above 50 megahertz. Tektronix Type 191 Constant Amplitude Signal Generator recommended.
5. Low-frequency sine-wave generator. Frequency 60 hertz to one megahertz; output amplitude, variable from 0.5 volts to 40 volts peak to peak; amplitude accuracy, within $3 \%$ from 60 hertz to one megahertz. For example, General Radio 1310-A Oscillator (use a General Radio Type 274QBJ Adaptor to provide BNC output).
6. 10X probe with BNC connector. Tektronix P6010 Probe recommended.
7. Test oscilloscope. Bandwidth, DC to 50 megahertz; minimum deflection factor, five millivolts/division; accuracy, within 3\%. Tektronix Type 453 Oscilloscope recommended.
8. Curent-measuring probe with passive termination. Sensitivity, two milliamperes/millivolt; accuracy, within 3\%. Tektronix P6019 Current Probe with 011-0078-00 passive termination recommended.
9. Cable (two). Impedance, 50 ohms; type, RG-58/U; length, 42 inches; connectors, BNC. Tektronix Part No. 012-0057-01.
10. BNC T connector. Tektronix Part No. 103-0030-00.
11. Cable. Impedance, 50 ohms; type, RG-58/U; length, 18 inches; connectors, BNC. Tektronix Part No. 012-0076-00.
12. Cable. Impedance, 50 ohms; type, RG-213/U; electrical length, five nanoseconds; connectors, GR874. Tektronix Part No. 017-0502-00.
13. In-1ine temination. Impedance, 50 ohms; wattage rating, two watts; accuracy, $\pm 3 \%$; connectors, GR874 input with BNC male output. Tektronix Part No. 017-0083-00.
14. Input RC normalizer. Time constant, 1 megohm $\times 20$ pF ; attenuation, 2 X ; connectors, BNC. Tektronix calibration fixture 067-0538-00.
15. 5 X attenuator. Impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, GR874. Tektronix Part No. 017-0079-00.
16. Dual-input coupler. Matched signal transfer to each input. Tektronix calibration fixture 067-0525-00.
17. Adapter. Adapts GR874 connector to BNC female connector. Tektronix Part No. 017-0064-00.
18. Termination. Impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, BNC. Tektronix Part No. 011-0049-00.
19. Adapter. Connectors, BNC female and two alligator clips. Tektronix Part No. 013-0076-00.
20. Screwdriver. Three-inch shaft, $3 / 32$-inch bit for slotted screws. Tektronix Part No. 003-0192-00.

## PERFORMANCE CHECK PROCEDURE

## General

In the following procedure, control settings or test equipment connections should not be changed except as noted. If only a partial check is desired, refer to the preceding step(s). for setup information. Type 453 front-panel control titles referred to in this procedure are capitalized (e.g., VOLTS/DIV).

The following procedure uses the equipment listed under Recommended Equipment. If equipment is substituted, control settings or setup may need to be altered to meet the requirements of the equipment used.

## Preliminary Procedure

1. Connect the Type 453 to a power source which meets the voltage and frequency requirements of this instrument.
2. Set the Type 453 controls as follows:

## CRT controls

| INTENSITY | Counterclockwise |
| :---: | :---: |
| FOCUS | Midrange |
| SCALE ILLUM | As desired |
| Vertical controls (both channels if applicable) |  |
| VOLTS/DIV | 20 mV |
| VARIABLE | CAL |
| POSITIO N | Midrange |
| Input Coupling | DC |
| MODE | CH 1 |
| TRIG G ER | NORM |
| INVERT | Pushed in |
| Triggering controls (both $A$ and $B$ if applicable) |  |
| LEVEL | 0 |
| S L O P E | + |
| COUPLING | AC |
| SOURCE | INT |
| Sweep controls |  |
| DELAY-TIME MULTIPLIER | Fully counterclockwise |
| $A$ and $B$ TIME/DIV | 1 ms |
| A VARIABLE | CAL |
| A SWEEP MODE | AUTO TRIG |
| B SWEEP MODE | TRIG GERABLE AFIER DELAY TME |
| HORIZ DISPLAY | A |
| MAG | OFF |
| A SWEEP LENGTH | FULL |
| POSITIO N | Midrange |
| POWER | off |

Side-panel controls
B TIME/DIV VARIABLE
CAL
CALBRATOR
1V
3. Set the POWER switch to ON. Allow at least 20 minutes warm up before proceeding,

## 1. Check Trace Alignment

REQ UIREMENT-Trace parallel to horizontal graticule lines.
a. Advance the INTENSITY control until the trace is visible.
b. Tum the Channel 1 POSITION control to move the trace to the center horizontal line.
c. Adiust the FOCUS control for as sharp a display as possible.
d. CHECK-The trace should be parallel with the center horizontal line.
e. If necessary, adiust the TRACE ROTATION adjustment (on side panel) so the trace is parallel to the horizontal graticule lines.

## 2. Check Astigmatism

REQUIREMENT-Sharp, well-defined display.
a. Connect the time-mark generator (Type 184) to the Channel 1 INPUT connector with the 42-inch BNC cable.
b. Set the time-mark generator for output markers of 1 and 0.1 millisecond.
c. Set the CH 1 VOLTS/DIV switch so the large markers extend beyond the bottom and top of the graticule area.
d. Set the A LEVEL control for a stable display.
e. CHECK-Markers should be well defined with optimum setting of FOCUS control.
f. If necessary, adjust the FOCUS control and ASTIG adjustment (on side panel) for best definition of markers.

## 3. Check $Y$ Axis Alignment and Geometry

REQUIREMENT-Y axis alignment, markers parallel to center vertical line within 0.1 division; geometry, bowing or tilt of markers at left and right extremes of display 0.1 division or less.
a. Set the horizontal POSITION control to move a large marker to the center vertical line.
b. CHECK-Markers parallel to the center vertical line within 0.1 division (see Fig. 5-1).
C. Set the horizontal POSITION and A VARIABLE controls so a large marker coincides with each vertical graticule line.
d. CHECK-Bowing and tilt of markers over entire display area 0.1 division or less (see Fig. 5-1).
e. Disconnect all test equipment.


Fig. 5-1. Typical CRT display showing good geometry and Y-axis alignment.

## 4. Check Channel 1 and 2 Step Attenuator Balance

REQUIREMENT-NO trace shift as the VOLTS/DIV switch is changed between 20 mV and 5 mV .
a. Position the trace to the center horizontal line with the Channel 1 POSITION control.
b. Change the following control settings:

```
CH I VOLTS/DIV
20 mV
Input Coupling (CH 1 GND
```

    and 2)
    c. CHECK-Change the CH 1 VOLTS/DIV switch from 20 mV to 5 mV . Trace should not move vertically.

NOTE
Use the TRACE FINDER switch to locate the trace if it is deflected off screen when switching to 10 or 5 mV .
d. If there is trace shift, adjust the Channel 1 STEP ATIEN BAL adjustment (on front panel) for no trace shift as the CH 1 VOLTS/DIV switch is changed from 20 mV to 5 mV .
e. Set the MODE switch to CH 2.
f. Position the trace to the center horizontal line with the Channel 2 POSITION control.
g. CHECK-Change the CH 2 VOLTS/DIV switch from 20 mV to 5 mV . Trace should not move vertically.
$h$. If there is trace shift, adjust the Channel 2 STEP ATIEN BAL adjustment (on front panel] for no trace shift as the CH 2 VOLTS/DIV switch is changed from 20 mV to 5 mV .

## 5. Check Channel 1 and 2 Position Center

REQUIREMENT-Trace positioned beyond graticule limits at both extremes of POSITION control rotation.
a. Set the Channel 1 and 2 VARIABLE controls for minimum ga in (fully counterclockwise).
b. Set the CH 1 and CH 2 VOLTS/DIV switches to .1.
c. CHECK-Tum the Channel 2 POSITION control to each extreme of rotation; trace should be positioned beyond the graticule limits at each extreme of rotation.
d. Set the MODE switch to CH 1 .
e. CHECK-Turn the Channel 1 POSITION control to each extreme of rotation; trace should be positioned beyond the graticule limits at each extreme of rotation.

## 6. Check Channel 1 and 2 Gain

REQUIREMENT-Correct vertical deflection in the 20 mV position of the CH 1 and CH 2 VOLTS/DIV switches.
a. Change the following control settings:

| VOLTS/DIV (CH 1 and 2) | 20 mV |
| :--- | :--- |
| VARIABLE (CH 1 and 2) | CAL |
| POSITION (CH $\& \mathrm{CH} 2)$ | Midrange |
| Input Coupling (CH 1 <br> and 2) | DC |
| A and B TME/DIV | .5 ms |

b. Connect the standard amplitude calibrator (067-0502-00) cutput connector to the Channel 1 and 2 INPUT connectors through a BNC Tconnector and two BNC cables.
c. Set the standard amplitude calibrator for a 0.1-volt square-wave output.
d. CHECK-CRT display for five divisions of deflection (se Fiq. 5-2).


Fig. 5-2. Typical CRT display showing correct vertical gain.
e. If necessary, adjust the Channel 1 GAIN adjustment (on front panel) for exactly five divisions of deflection.
f. Set the MODE switch to ADD.
g. Pull the INVERT switch.
h. Center the display with the Channel 2 POSITION control.
i. CHECK-CRT display for straight line.
i. If necessary, adjust the Channel 2 GAIN adjustment (on front panel) for straight line.

## 7. Check Added Mode Operation

REQUIREMENT-C orrect signal addition.
a. Push the INVERT switch in.
b. Set the standard amplitude calibrator far a 50-millivolt square-wave autput.
c. CHECK-CRT display five divisions in amplitude,

## 8. Check Channel 1 and 2 Deflection Accuracy

REQUIREMENT-Vertical deflection factor within 3\% of CH 1 and CH 2 VOLTS/DIV switch indication.
a. Set the MODE switch to CH 1.
b. Set the Channel 1 Input Coupling switch to GND.
c. CHECK-Using the CH 1 VOLTS/DIV switch and standard amplitude calibrator settings given ir Table 5-1, check vertical deflection factor within $3 \%$ in each position of the CH 1 VOLTS/DIV switch.
d. Set the MODE switch to CH 2.
e. Set the Channel 1 Input Coupling switch to GND and the Channel 2 Input Coupling switch to DC.
f. CHECK-Using the CH 2 VOLTS/DIV switch and standard amplitude calibrator settings given in Table 5-1] check the vertical deflection factar within $3 \%$ in each position of the CH 2 VOLTS/DIV switch.

TABLE 5-1
Vertical Deflection Accuracy

| VOLTS/DIV <br> Switch <br> Setting | Standard <br> Amplitude <br> Calibrator <br> Output | Vertical <br> Deflection <br> In <br> Divisions | Maximum <br> Error For <br> $\mathbf{3 \%}$ Accuracy <br> (divisions) |
| :---: | :---: | :---: | :---: |
| 5 mV | 20 millivolts | 4 | $\pm 0.12$ |
| 10 mV | 50 millivolts | 5 | $\pm 0.15$ |
| 20 mV | 0.1 volt | 5 | Previously set <br> in step 6 |
| 50 mV | 0.2 volt | 4 | $\pm 0.12$ |
| 1 | 0.5 volt | 5 | $\pm 0.15$ |
| 2 | 1 volt | 5 | $\pm 0.15$ |
| .5 | 2 volts | 4 | $\pm 0.12$ |
| 1 | 5 volts | 5 | $\pm 0.15$ |
| 2 | 10 volts | 5 | $\pm 0.15$ |
| 5 | 20 volts | 4 | $\pm 0.12$ |
| 10 | 50 volts | 5 | $\pm 0.15$ |

## 9. Check Channel 1 and 2 Variable Volts/ Division Range

REQUIREMENT-Continuously variable deflection factor between the calibrated steps.
a. Set the standard amplitude calibrator for a 0.1-volt square-wave output.
b. Change the following central settings:

| VOLTS/DIV (CH 1 and 2) | 20 mV |
| :--- | :--- |
| Input Coupling (CH 1 <br> and 2) |  |
| MODE | AC |
|  | CH 1 |

c. CHECK-Tum the Channel 1 VARIABLE control fully counterclockwise (minimum gain). Display should be reduced to two divisions or less (indicates adequate range for continuously variable deflection factors between the calibrated steps; se Fig. 5-3); Channel 1 UNCAL light must be on when the Channel 1 VARIABLE control is not in CAL position.


Fig. 5-3. Typical CRT display showing correct Channel I and 2 VARIABLE control range (double exposure)
d. Set the MODE switch to CH 2.
e. CHECK-Tum the Channel 2 VARIABLE control fully counterclockwise (minimum gain). Display should be reduced to two divisions or less (indicates adequate range for continuously variable deflection factors between the calibrated steps; se Fig. 5-3). Channel 2 UNCAL light must be on when Channel 2 VARIABLE control is not in CAL position.
f. Disconnect the cable from the Channel 2 INPUT connector.

## 10. Check Channel 1 and 2 Cascaded Deflection Factor

REQUIREMENT-One millivolt/division or less.
a. Cannect the CH 1 OUT connector to the Channel 2 INPUT connector with the 18 -inch 50 -ohm BNC cable.
b. Change the following control settings:

| VOLTS/DIV (CH 1 and 2) | 5 mV |
| :--- | :--- |
| VARIABLE (CH 1 and 2) | CAL |
| Input Coupling (CH 1 <br> and 2) | DC |

c. Set the standard amplitude calibrator for a five-millivolt square-wave output.
d. CHECK-CRT display five divisions or greater in amplitude (one millivolt/division, or less, minimum deflection factor).

## 11. Check Channel 1 and 2 Input Coupling Switch Operation

REQUIREMENT-Correct signal coupling in each position of the Channel 1 and 2 Input Coupling switches.
a. Set the CH 1 and CH 2 VOLTS/DIV switches to 20 mV .
b. Disconnect the 18 -inch BNC cable and reconnect the standard amplitude calibrator to the Channel 2 INPUT connector.
c. Set the standard amplitude calibrator for a 50-millivolt square-wave output.
d. Position the display with the Channel 2 POSITION control so the bottom of the square-wave is at the center horizontal line.
e. Set the Channel 2 Input Coupling switch to GND.
f. CHECK-CRT display for straight line near the center horizontal line.
g. Set the Channel 2 Input Coupling switch to AC.
h. CHECK-CRT display centered about center horizontal line.
i. Set the MODE switch to CH 1 .
j. Position the display with the Channel 1 POSITION control so the bottom of the square wave is at the center horizontal line.
k. Set the Channel 1 Input Coupling switch to GND.
I. CHECK-CRT display for straight line near the center horizontal line.
m . Set the Channel 1 Input Coupling switch to $A C$.
n. CHECK-CRT display centered about center horizontal line.

## 12. Check Low-Frequency Vertical Linearity

REQUIREMENT-0.15 division, or less, compression or expansion of a two-division signal (at center screen) when positioned to the vertical extremes of the graticule area.
a. Set the Channel 1 and 2 Input Coupling switches to DC.
b. Position the display to the center of the graticule with the Channel 1 POSITION control.
c. Adiust the Channel 1 VARIABLE control far exactly two divisions of deflection.
d. Position the top of the display to the top horizontal line.
e. CHECK-Compression or expansion 0.15 division or less (see Fiq. 5-14).
f. Position the bottom of the display to the bottom horizontal line.


Fig. 5-4. Typical CRT display showing acceptable compression and expansion. (A) Expansion, (B) correct deflection af cenfer of graticule, (C) compression.
g. CHECK-Compression or expansion 0.15 divisions or less (se Fiq. 5-4).
h. Set the MODE switch to CH 2.
i. Position the display to the center of the graticule with the Channel 2 POSITION control.
j. Adiust the Channel 2 VARIABLE control for exactly two divisions of deflection.
k. Position the top of the display to the top horizontal line.
I. CHECK-Compression or expansion 0.15 division or less (see Fig. 5-4).
m . Position the bottom of the display to the bottom horizontal line.
n. CHECK-Compression or expansion 0.15 division or less (see Fig. 5-4).
o. Disconnect all test equipment.

## 13. Check Trace Shift Due to Input Gate Current

REQUIREMENT-Negligible trace shift at $5 \mathrm{mV} / \mathrm{DIV}$.
a. Change the following control settings:

| VOLTS/DIV (CH 1 and 2) | 5 mV |
| :--- | :--- |
| VARIABLE (CH 1 and 2) | CAL |
| Input Coupling (CH 1 | GND |
| and 2 ) |  |

b. Position the trace to the center horizontal line with the Channel 2 POSITION control.
c. CHECK-Set the Channel 2 Input Coupling switch to DC. Trace shift should be negligible.
d. Set the MODE switch to CH 1.
e. Position the trace to the center horizontal line with the Channel 1 POSITION control.
f. CHECK-Set the Channel 1 Input Coupling switch to DC. Trace shift should be negligible.

## 14. Check Alternate Operation

REQUIREMENT-Trace altemation at all sweep rates.
a. Set the MODE switch to ALT.
b. Position the traces about two divisions apart
c. Tum the $A$ TIME/DIV switch throughout its range.
d. CHECK-Trace altemation between Channel 1 and 2 at all sweep rates. At faster sweep rates, altemation will not be apparent; instead display appears as two traces on the screen.

## 15. Check Channel 1 Volts/Division Switch Compensation

REQUIREMENT-370 or less overshoot, rounding or tilt in all positions of the CH 1 VOLTS/DIV switch.
a. Change the following control settings:

| VOLTS/DIV (CH 1 and 2) | 20 mV |
| :--- | :--- |
| MODE | CH 1 |
| A and B TME/DIV | .2 ms |

$A$ and B TIME/DIV . 2 ms
b. Connect the square-wave generator (Type 106) highamplitude output connector to the Channel 1 INPUT connector through the five-nanosecond GR cable, 50-ohm inline temmination and 20 pF input RC nomalizer, in given order.
c. Set the square-wave generator for four divisions of one-kilohertz signal.
d. CHECK-CRT display at each CH 1 VOLTS/DIV switch position for $3 \%$ or less overshoot, rolloff or tilt (se屯 Fig. 5-\$). Adjust the square-wave generator output amplitude as


Fig. 5-5. (A) Typical CRT display showing correct compensation, (B) and (C) incorrect compensation.
needed to maintain a four-division display (except in 2, 5 and 10 positions where display will be less than four divisions).

## 16. Check Channel 2 Volts/Division Switch Compensation

REQ UIREMENT-3\% or less overshoot, rounding or tilt in all positions of the CH 2 VOLTS/DIV switch,
a. Set the MODE switch to CH 2.
b. Connect the square-wave generator high-amplitude output connector to the Channel 2 INPUT connector through the five-nanosecond GR cable, 50-ohm in-line temination and 20 pF input RC nomalizer, in given order.
c. Set the square-wave generator for four divisions of one-kilohertz signal.
d. CHECK-CRT display at each CH 2 VOLTS/DIV switch position for $3 \%$ or less overshoot, rolloff or tilt (se Fiq. 5-\$). Adjust the square-wave generatar output amplitude as needed to maintain a four-division display (except in 2,5 and 10 positions where display will be less than four divisions).
e. Disconnect all test equipment.

## 17. Check High-Frequency Compensation

REQUIREMENT-Optimum square-wave response at high frequencies.
a. Change the following control settings:

| CH 1 VOLTS/DIV | 20 mV |
| :--- | :--- |
| MODE | CH 1 |
| A and B TME/DIV | $0.2 \mu \mathrm{~s}$ |
| MAG | $\mathrm{X10}$ |

b. Connect the square-wave generator fast-rise + output to the Channel 1 INPUT connector through the five-nanosecond GR cable, 5 X GR attenuator and the 50 -ohm in-line temination, in given order.
c. Set the square-wave generator for fast-rise operation and a four-division display at 100 kilohertz.
d. CHECK-CRT display for optimum square-wave response (see Fiq. 5-j).
e. Set the CH 1 VOLTS/DIV switch to 10 mV .
f. Set the square-wave generator output amplitude for four-division display.
g. CHECK-CRT display for optimum square-wave response (se Fig. 5-6).
h. Set the CH 2 VOLTS/DIV switch to 5 mV .
i. Set the square-wave generator output amplitude for four-division display.
j. CHECK-CRT display for optimum square-wave response (se Fig. 5-6).


Fig. 5-6. Typical CRT display showing correct high-frequency cominsation.

## k. Set the MODE switch to CH 2 .

I. Disconnect the 50 -ohm in-line termination from the Channel 1 INPUT connector and connect it to the Channel 2 INPUT connector.
m . Set the CH 2 VOLTS/DIV switch to 5 mV .
n. CHECK-CRT display for optimum square-wave response (see Fig. 5-6).
o. Set the CH 2 VOLTS/DIV switch to 10 mV .
p. Set the square-wave generator output amplitude for a four-division display.
q. CHECK-CRT display for optimum square-wave response (see Fig. 5-6).
r. Set the CH 2 VOLTS/DIV switch to 20 mV .
s. Set the square-wave generator output amplitude for a four-division display.
t. CHECK-CRT display for optimum square-wave response (se Fiq. 5-6).
u. Disconnect all test equipment.

## 18. Check Upper Vertical Bandwidth Limit of Channels 1 and 2

REQUIREMENT-20 mV, not more than -3 dB at 50 megahertz; 10 mV , not more than -3 dB at 45 megahertz; 5 mV , not more than -3 dB at 40 megahertz.
a. Change the following control settings:

| CH 1 VOLTS/DIV | 20 mV |
| :--- | :--- |
| MODE | CH 1 |
| A and B TME/DIV | $20 \mu \mathrm{~s}$ |
| MAG | OFF |

b. Connect the constant-amplitude sine-wave generator (Type 191) to the Channel 1 INPUT connector through the five-nanosecond GR cable, 5X GR attenuator and the 50ohm in-line termination.
c. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
d. Without changing the output amplitude, increase the output frequency of the generator until the display is reduced to 2.8 divisions ( -3 dB point; se Fig. 5-7).
e. CHECK-Output frequency of generator must be 50 megahertz or higher. Actual frequency, $\qquad$ megahertz.
f. Set the CH 1 VOLTS/DIV switch to 10 mV .
g. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
h. Without changing the output amplitude, increase the output frequency of the generator until the display is reduced to 2.8 divisions ( -3 dB point).
i. CHECK-Output frequency of generator must be 45 megahertz or higher. Actual frequency, ..... megahertz.
j. Set the CH 1 VOLTS/DIV switch to 5 mV .
k. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).


Fig. 5-7. Typical CRT display when checking vertical frequency response (simulated waveform)
I. Without changing the output amplitude, increase the output frequency of the generator until the display is reduced to 2.8 divisions ( -3 dB point).
m . CHECK-Output frequency of generator must be 40 megahertz or higher, Actual frequency, megahertz.
n. Set the MODE switch to CH 2.
o. Disconnect the output of the in-line termination from the Channel 1 INPUT connector and connect it to the Channel 2 INPUT connector.
p. Set the constant amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
q. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point).
r. CHECK-Output frequency of generator must be 50 megahertz or higher. Actual frequency, megahertz.
s. Set the CH 2 VOLTS/DIV switch to 10 mV .
t. Set the constant-amplitude generator far a four-division display at its reference frequency ( 50 kHz ).
u. Without changing the output amplitude, increase the output frequency of the generator until the display is reduced ta 2.8 divisions ( -3 dB point).
v. CHECK-Output frequency of generator must be 45 megahertz or higher. Actual frequency, megahertz.
w. Set the CH 2 VOLTS/DIV switch to 5 mV .
x. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
$y$. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point).
z. CHECK-Output frequency of generator must be 40 megahertz or higher. Actual frequency,
megahertz.
19. Check Added Mode Upper Bandwidth Limit

REQUIREMENT-Not more than -3 dB at 50 megahertz.
a. Change the following control settings:
VOLTS/DIV (CH 1 and 2) 20 mV
CH 1 POSITION Midrange

CH 1 Input Coupling GND MODE

ADD
b. Set the constant-amplitude generatar for a four-division display at its reference frequency ( 50 kHz ).
c. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point; se Fig. 5-7).
d. CHECK-Output frequency of generator must be 50 megahertz or higher. Actual frequency,
megahertz.
e. Change the following control settings:

CH 2 POSITION Midrange
CH 1 Input Coupling
CH 2 Input Coupling

DC
GND
f. Disconnect the output of the in-line termination from the Channel 2 INPUT connector and connect it to the Channel 1 INPUT connector.
g. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
h. Without changing the output amplitude, increase the output frequency af the generator until the deflection is reduced to 2.8 divisions ( -3 dB point),
i. CHECK-Output frequency of generator must be 50 megahertz or higher. Actual frequency,___ megahertz.

## 20. Check Channel 1 and 2 Cascaded Upper Bandwidth Limit

REQUIREMENT-Not more than -3 dB at 25 megahertz.
a. Connect the CH 1 OUT connector to the Channel 2 INPUT connector with the 18 -inch $50-\mathrm{ohm}$ BNC cable.
b. Set the MODE switch to CH 2.
c. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
d. Withaut changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point; see Fig. 5-7).
e. CHECK-Output frequency of generator must be 25 megahertz or higher. Actual frequency, megahertz.
f. Disconnect the cable from between the CH 1 OUT and Channel 2 INPUT connectors.

## 21. Check Common-Mode Rejection Ratio

REQUIREMENT-20:1 or greater at 20 megahertz.
a. Change the following control settings:

## VOLTS/DIV (CH 1 and 2) 50 mV Input Coupling (CH 1 DC

 and 2)A and B TME/DIV . 1 ms
b. Connect the constant-amplitude generator to the Channel 1 and 2 INPUT connectors through the five-nanosecond GR cable, 50 -ohm in-line termination and the duel-input coupler.
c. Set the constant-amplitude generator for a 3.2-division display at 20 megahertz.
d. Change the following control settings:

| VOLTS/DIV (CH 1 and 2) | 20 mV |
| :--- | :--- |
| MODE | ADD |
| INVERT | Pulled out |

e. CHECK-CRT display for 0.4-division deflection, or less (common-mode reiection ratio 20:1 or better, se Fiq. 5-8).

## NOTE

This check applies only when the Channel 1 and 2 gain is correct as given in step 6. If the com-mon-mode reiection ratio is lower than 20:1, check and readjust the gain. Then recheck this step.
f. Disconnect the dual-input coupler.

## 22. Check Attenuator Isolation Ratio

REQUIREMENT-10,000:1 or greater at 20 megahertz.
a. Change the following control settings:

```
CH 1 VOLTS/DIV
1
CH 2 VOLTS/DIV 5mV
CH2 Input Coupling GND
MODE CH1
INVERT Pushed in
```

b. Connect the constant-amplitude generator to the Channel 1 INPUT connector through the five-nanosecond GR cable and the 50 -ohm in-line termination.


Fig. 5-8. Typical CRT display showing correct common-mode rejection ratio.
c. Set the constant-amplitude generator for a five-division display at 20 megahertz (use the variable control of the generator, if necessary, to obtain a five-division display.
d. Set the MODE switch to CH 2.
e. CHECK-CRT display for 0.1-division deflection, or less (attenuator isolation ratio 10,000:1 or better, see Fig. 5-9).
f. Change the following control settings:
CH 1 VOLTS/DIV
5 mV

CH 2 VOLTS/DIV
1
CH 1 Input Coupling GND
CH 2 Input Coupling DC


Fig. 5-9. Typical CRT display when checking altenuator isolation ratio and amplifier crosstalk ratio.
g. Disconnect the 50 -ohm in-line termination from the Channel 1 INPUT connector and reconnect it to the Channel 2 INPUT connector.
h. Set the constant-amplitude generator for a five-division display at 50 megahertz [use the variable control of the generator, if necessary, to obtain a five-division display).
i. Set the MODE switch to CH 1.
j. CHECK-CRT display for a 0.1-division deflection or less (attenuator isolation ratio 10,000:1 or better, see■Fig. 5-9).
k. Disconnect all test equipment.

## 23. Check A and B Trigger Level Centering

REQUIREMENT-Stable display in accordance with the following procedure.
a. Change the following control settings:

| VOLTS/DIV (CH 1 and 2$)$ |  | 50 mV |
| :--- | :--- | :--- |
| CH 1 POSITION |  | Midrange |
| INPUT COUPLING (CH 1 | DC |  |
| and 2) |  | 0 |
| LEVEL (A and B) |  | 0 |
| A and B TIME/DIV |  | $20 \mu \mathrm{~s}$ |

b. Connect the constant-amplitude generator to the $A$ EXT TRIG INPUT connector through the five-nanosecond GR cable, GR to BNC adapter and BNC T connector. Connect the output of the BNC T connector to the Channel I INPUT connector through the 18 -inch 50 -ohm BNC cable and a 50-ohm BNC termination.
c. Set the canstant-amplitude generator for a 0.2 -division display at 50 kilohertz.
d. Slowly rotate the A LEVEL control until a stable display is presented (A SWEEP TRIG'D light on).
e. CHECK-A LEVEL control must be near 0 . This check indicates that the A Trigger Level Center adjustment is set comectly.
f. Change the following control settings:

| TRIGGER | CH 1 ONLY |
| :--- | :--- |
| A LEVEL | 0 |
| COUPLNG (A and B] | DC |

g. Slowly rotate the Channel 1 POSITION control until a stable display is presented (A SWEEP TRIG'D light on).
h. CHECK-CRT display must be within one division of the center horizontal line (see Fig. 5-10). CH 1 light in both A and B Triggering must be on. This check indicates that the Channel 1 Trigger DC Level adjustment is set correctly.
i. Set the TRIGGER switch to NORM.
j. Slowly rotate the Channel 1 POSITION control until a stable display is presented (A SWEEP TRIG'D light on).
k. CHECK-CRT display must be within two divisions of the center horizontal line (see Fig. 5-10). This check indicates that the Normal Trigger DC Level adjustment is set correctly.
l. Set the HORIZ DISPLAY switch to DELAYED SWEEP ( (B).
m . Set the CH 1 POSITION control to midrange.
$n$. Slowly rotate the B LEVEL control until a stable display is presented.
o. CHECK-B LEVEL control must be near 0 . This check indicates that the B Trigger Level Center adjustment is set correctly.


Fig. 5-10. Typical CRT display when checking trigger level centering.

## 24. Check $A$ and $B$ Internal Triggering Operation

REQUIREMENT-Stable display in AC, LF REJ and DC positions of the A and B COUPUNG switches with a 0.2division display at 10 megahertz and a one-division display at 50 megahertz.
a. Set the constant-amplitude generator for a 0.2-division display at 10 megahertz.
b. Change the fallowing control settings:

| TME/DIV | $.1 \mu \mathrm{~s}$ |
| :--- | :--- |
| A SWEEP MODE | NORM TRIG |
| HORIZ DISPLAY | A |

c. CHECK-Stable CRT display (see Fiq. 5-11A) can be obtained with the A COUPUNG switch set to AC, LF REJ and DC (A LEVEL control may be adjusted as necessary to obtain stable display). The A SWEEP TRIG'D light must be on when the display is stable.
d. Set the canstant-amplitude generator for a one-division display at 50 megahertz.
e. Set the MAG switch to X10.
f. CHECK-Stable CRT display (see Fig. 5-11B) can be obtained with the A COUPUNG switch set to AC, LF REJ and DC (A LEVEL and HF STAB controls may be adiusted as necessary to obtain a stable display). Display jitter should not exceed 0.1 division (one nanosecond).
g. Change the following control settings:
A LEVEL
Set for a stable A display HORIZ DISPLAY
DELAYED SWEEP
(B)
h. Set the constant-amplitude generator for a one-division display at 50 megahertz (as set in part d above).
i. CHECK-Stable CRT display (see Fig. 5-11B) can be obtained wwith the B COUPLNG switch set to AC, LF REJ and DC (B LEVEL control may be adjusted as necessary to obta in stable display).
j. Set the constant-amplitude generator for a 0.2-division display at 10 megahertz.
k. Set the MAG switch to OFF.
I. CHECK-stable CRT display (see Fiq. 5-11A) can be obtained with the B COUPUNG switch set to AC, LF REJ and DC (B LEVEL control may be adjusted as necessary to obtain a stable display).

## 25. Check $A$ and $B$ External Triggering Operation

REQ UIREMENT-Stable display in AC, LF REJ and DC positions of A and B COUPUNG switches with a 50 -millivolt signal at 10 megahertz and a 200-millivolt signal at 50 megahertz.
a. Change the following control settings:

| SOURCE (A and B) | EXT |
| :--- | :--- |
| HORIZ DISPLAY | A |
| MAG | OFF |



Fig. 5-11. (A) Typical CRT display when checking internal 10-megaintz triggering, (B) typical CRT display when checking internal J-megahertz triggering.
b. Set the constant-amplitude generator for a one-division display ( 50 millivolts) at 10 megahertz.
c. CHECK-Stable CRT display (see Fiq. 5-12A) can be obtained with the A COUPLNG switch set to AC, LF REJ and DC (A LEVEL control may be adjusted as necessary to obtain stable display).
d. Set the MAG switch to X10.
e. Set the constant-amplitude generator for a 2.8 -division display at 50 megahertz (2.8-division display takes into account typical rolloff in vertical response at 50 MHz ).
f. CHECK-Stable CRT display (see Fig. 5-12B) can be obtained with the A COUPUNG switch set to AC, LF RE and DC (A LEVEL and HF STAB controls may be adjusted as necessary to obtain stable display).
g. Disconnect the constant-amplitude generator signal from the A EXT TRIG INPUT connector and reconnect it to the B EXT TRIG INPUT connector.
h. Change the following control settings:

$$
\begin{aligned}
& \text { A SOURCE } \\
& \text { A LEVEL } \\
& \text { HORIZ DISPLAY }
\end{aligned}
$$

INT
Set for a stable A display DELAYED SWEEP (B)
i. CHECK-Stable CRT display (see Fig. 5-12B) can be obtained with the B COUPLNG switch set to AC, LF RE and DC (B LEVEL control may be adjusted as necessary to obtain stable display).
j. Set the MAG switch to OFF.
k. Set the constant-amplitude generator for a one-division display at 10 megahertz.
I. CHECK-Stable CRT display (see Fiq. 5-12A) can be obtained with the B COUPLING switch set to AC, LF REJ and DC (B LEVEL control may be adjusted as necessary to obtain stable display; A LEVEL control must also be correctly adjusted).
m . Disconnect all test equipment.


Fig. 5-12. (A) Typical CRT display when checking external 10megahertz triggering, (B) typical CRT display when checking external 50 -megahertz triggering.

## 26. Check A and B Low-Frequency Triggering Operation

REQUIREMENT-Intemal, stable display in AC, HF REJ and DC positions of the A and B COUPUNG switches with a 0.2 -division display; extemal, stable display in AC, HF REJ and DC positions of A and B COUPLING switches with a 50-millivolt signal.
a. Connect the low-frequency constant-amplitude generator to the A EXT TRIG INPUT connector through a 42inch 50 -ohm BNC cable and the BNC T connector. Connect the output of the BNC T connector to the Channel 1 INPUT connector through an 18 -inch 50 -ohm BNC cable and a 50 -ohm BNC termination.
b. Change the following control settings:
$A$ and B TIME/DIV
5 ms
HORIZ DISPLAY
A
c. Set the low-frequency generator for a 0.2-division display at 60 hertz.
d. CHECK-Stable CRT display (see Fiq. 5-13A) can be obtained with the A COUPUNG switch set to AC, HF REJ and DC (A LEVEL control may be adjusted as necessary to obtain a stable display).
e. Set the A and B SOURCE switches to EXT.
f. Set the low-frequency generator for a one-division display at 60 hertz ( 50 millivolts).
g. CHECK-Stable CRT display (see Fiq. 5-13B) can be obtained with the A COUPUNG switch set to AC, HF REJ and DC (A LEVEL control may be adjusted as necessary to obta in stable display).
h. Change the following control settings:
A SOURCE
INT
A LeVEl
Set for a stable A display
HORIZ DISPLAY
DELAYED SWEEP
(B)
i. Disconnect the low-frequency generator from the $A$ EXT TRIG INPUT connector and reconnect it to the B EXT TRIG INPUT connector.
j. CHECK-Stable CRT display (see Fiq. 5-13B) can be obtained with the B COUPUNG switch set to AC, HF REJ and DC (B LEVEL control may be adjusted as necessary to obta in stable display).
k. Set the B SOURCE switch to INT.
I. Set the low-frequency generator for a 0.2-division display at 60 hertz.


Fig. 5-13. (A) Typical CRT displaay when checking internal Jowfrequency triggering at 60 hertz. (B) Typical CRT display when checking external low-frequency triggering at 60 hertz.
m. CHECK--Stable CRT display (see Fig, 5-13A) can be obtained with the B COUPLING switch set to AC, HF REJ and DC (B LEVEL control may be adjusted as necessary to obtain stable display; A LEVEL control must also be correctly adiusted).

## 27. Check $A$ and $B$ High-Frequency Reject Operation

REQ UIREMENT-Stable triggering with 0.2-division display at 50 kilohertz; does not trigger at one megahertz.
a. Change the following control settings:

| COUPLING (A and B) | HF REJ |
| :--- | :--- |
| SOURCE (A and B) | INT |
| A and B TME/DIV | $20 \mu \mathrm{~s}$ |
| A SWEEP MODE | AUTO TRIG |

b. Set the low-frequency constant-amplitude generator for a 0.2 -division display at 50 kilohertz.
c. CHECK-Stable CRT display (see Fig. 5-14) can be obtained with the B LEVEL control,
d. Without changing the output amplitude, set the lowfrequency generatar to one megahertz,
e. Set the MAG switch to X10,
f. CHECK-Stable CRT display cannot be obtained at any setting of the B LEVEL control.
g. Change the following control settings:
A SWEEP MODE NORM TRIG
HORIZ DISPLAY
MAG
A
OFF
h. Set the low-frequency generator for a 0.2-divisian display at 50 kilohertz.
i. CHECK-Stable CRT display (see Fiq. 5-14 can be obtained with the A LEVEL control.
j. Without changing the output amplitude, set the con-stant-amplitude generator to one megahertz.
k. Set the MAG switch to X10.
I. CHECK-Stable display cannot be obtained at any setting of the A LEVEL control.

## 28. Check $A$ and $B$ Low-Frequency Reject Operation

REQUIREMENT-Stable display with 0.2 -division disploy at 30 kilohertz; does not trigger at 60 hertz.
a. Set the low-frequency generator for a 0,2-division display at 30 kilohertz.
b. Change the following control settings:

| COUPLNG (A and B) | LF REJ |
| :--- | :--- |
| A and B TME/DIV | .1 ms |
| MAG | OFF |

c. CHECK-Stable CRT display (see Fiq. 5-15) can be obtained with the A LEVEL control.


Fig. 5-14. Typical CRT display when checking high-frequency reject operation af 50 kilohortz.
d. Without changing the output amplitude, set the lowfrequency generator to 60 hertz.
e. Set the A and B TME/DIV switch to 2 ms .
f. CHECK-Stable CRT display cannot be obtained at any setting of the A LEVEL control.
g. Change the following control settings:
$A$ and $B$ TIME/DIV
.1 ms
HORIZ DISPLAY
DELAYED SWEEP (B)
(B)
h. Set the low-frequency generator for a 0.2-divisian display at 30 kilohertz.
i. CHECK-Stable CRT display (see Fig. 5-15) can be obtained with the B LEVEL control.
j. Without changing the output amplitude, set the lowfrequency generator to 60 hertz.
k. Set the $A$ and $B$ TIME/DIV switch to 2 ms .
I. CHECK-Stable CRT display cannot be obtained at a ny setting of the B LEVEL control.


Fig. 5-15. Typical CRT display when checking low-frequency reject eperation of 30 kilohertz.

## 29. Check Single Sweep Operation

REQUIREMENT-Sweep triggers at same A LEVEL control setting as in AUTO TRIG; after each sweep, further displays are locked out until the RESET button is pressed.
a. Change the following control settings:

$$
\begin{array}{ll}
\text { COUPUNG (A and B) } & \text { AC } \\
\text { A and B TIME/DIV } & 5 \mathrm{~ms} \\
\text { HORIZ DISPLAY } & \text { A }
\end{array}
$$

b. Set the low-frequency generator for a five-division display at one kilohertz.
c. Set the A LEVEL control fully clockwise.
d. Set the A SWEEP MODE switch to SINGLE SWEEP.
e. Push the RESET button.
f. CHECK-RESET light must come on when button is pressed and remain on until sweep is triggered.
g. Slowly rotate the A LEVEL control counterclockwise.
h. CHECK-A single-sweep display (one sweep only) is presented when the A LEVEL control is in the triggerable region. RESET light must go off at the end of the sweep and remain off until the RESET button is pressed again.

## 30. Check A and B Slope Switch Operation

REQUIREMENT-Stable triggering on correct slope of trigger signal.
o. Change the following control settings:
A LEVEL
0
A SWEEP MODE
AUTO TRIG
b. Set the low-frequency generator for a four-division display at one kilohertz.
c. CHECK-CRT display starts on positive slope of the waveform (se Fig. 5-15A).
d. Set the A SLOPE switch to -.
e. CHECK-CRT display starts on negative slope of the waveform (se Fig. 5-16B).
f. Change the following control settings:
HORIZ DISPLAY
DELAYED SWEEP (B)
A SWEEP MODE
AUTO TRIG
g. CHECK-CRT display starts on positive slope of the waveform (see Fig. 5-16A).
h. Set the B SLOPE switch to -.
i. CHECK-CRT display starts on negative slope of the waveform (se Fig. 5-15B).
j. Disconnect all test equipment.

## 31. Check A and B Triggering Level Control Range

REQUIREMENT-EXT, at least + and - 2 volts; EXT 10, at least + and - 20 volts.


Fig. 5-16. Typical CRT display when checking slope switch operation. (A) SLOPE switch set to + , (B) SLOPE switch set to -.
a. Connect the low-frequency generator to the B EXT TRIG INPUT connector through a 42 -inch BNC cable and the BNC T connector. Connect the output of the BNC T connector to the Channel 1 INPUT connector through an 18inch BNC cable.
b. Change the following control settings:

| CH 1 VOLTS/DIV | 1 |
| :--- | :--- |
| LEVEL (A and B) | Midrange |
| COUPLNG (A and B) | DC |
| SOURCE (A and B) | EXT |

c. Set the low-frequency generator for a four-division display (four volts peak to peak) at one kilohertz.
d. CHECK-Rotate the B LEVEL control throughout its range and check that display can be triggered at any point along the negative slope of the waveform (indicates B LEVEL control range of at least + and - two volts). Display is not triggered at either extreme of rotation.
e. Set the B SLOPE switch to + .
f. CHECK-Rotate the B LEVEL control throughout its range and check that display can be triggered at any point along the positive slope of the waveform. Display is not triggered at either extreme of rotation.
g. Set the CH 1 VOLTS/DIV switch to 10.
h. Set the B SOURCE switch to EXT +10 .
i. Set the low-frequency generator for a four-division display ( 40 volts peak to peak) at one kilohertz.
j. CHECK-Rotate the B LEVEL control throughout its range and check that display can be triggered at any point along the positive slope of the waveform (indicates B LEVEL control range of at least + and -20 volts). Display is not triggered at either extreme of rotation.
k. Set the B SLOPE switch to -
I. CHECK-Rotate the B LEVEL control throughout its range and check that display can be triggered at any point along the negative slope of the waveform. Display is not triggered at either extreme of rotation.
m . Change the following control settings:

| A SOURCE | EXT $\div 10$ |
| :--- | :--- |
| A SWEEP MODE | NORM TRIG |
| HORIZ DISPLAY | A |

$n$. Disconnect the low-frequency generator from the $B$ EXT TRIG INPUT connector and reconnect it to the A EXT TRIG INPUT connector.
o. CHECK-Rotate the A LEVEL control throughout its range and check that display can be triggered at any point along the negative slope af the waveform (indicates $A$ LEVEL control range of at least + and - 20 volts). Display is not triggered at either extreme of rotation.
p. Set the A SLOPE switch to +.
q. CHECK-Rotate the A LEVEL control throughout its range and check that display can be triggered at any point along the positive slope of the waveform. Display is not triggered at either extreme of ratation.
r. Change the following control settings:

CH 1 VOLTS/DIV
A SOURCE
s. Set the low-frequency generator for a four-division display (four volts peak to peak) at one kilohertz.
t. CHECK-Rotate the A LEVEL control throughout its range and check that display can be triggered at any point along the positive slope of the waveform (indicates A LEVEL control range of at least + and - two volts). Display is not triggered at either extreme of rotation.
u. Set the A SLOPE switch to -.
v. CHECK-Rotate the A LEVEL control throughout its range and check that display can be triggered at any point along the negative slope of the waveform. Display is not triggered at either extreme of rotation.
w. Disc onnect all test equipment.

## 32. Check $A$ and $B$ line Triggering Operation

REQUIREMENT-Stable display of line-frequency signal, triggered on the correct polarity.
a. Connect the 10X probe to the Channel 1 INPUT connector.
b. Change the following control settings:

CH 1 VOLT5/DIV 10
SOURCE (A and B) LINE
$A$ and $B$ TIME/DIV 2 ms
c. Connect the probe tip to the same line-voltage source which is connected to this instrument.
d. CHECK-Stable CRT display triggered on the corect slope.
e. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
f. CHECK-Stable CRT display triggered on the correct slope.
g. Disconnect all test equipment.

## 33. Check Auto Recovery Time and Operation

REQUIREMENT-Stable display with 50 -millisecond markers (20 hertz); free-running display with 0.1 -second markers (10 hertz).
a. Change the following control settings:

| VOLTS/DIV (CH 1 and 2$)$ | .2 |
| :--- | :--- |
| SLOPE (A and B) | + |
| COUPUNG (A and B) | AC |
| SOURCE (A and B) | INT |
| DELAY-TME MULTPLIER | 1.00 |
| A and B TME/DIV | $50 \mu \mathrm{~s}$ |
| BSWEEP MODE | B STARTS AFIER DELAY |
|  | TIME |
| HORIZ DISPLAY | A |

b. Connect the time-mark generator to the Channel 1 INPUT connector through a 42 -inch 50 -ohm BNC cable and a 50 -ohm BNC termination.
c. Set the time-mark generator for 50 -millisecond markers.

## CAUTION

To avoid possible buming of the CRT phospor at slow sweep rates, position the baseline of the marker display below the viewing area.
d. CHECK-Stable CRT display can be obtained with the A LEVEL control. Marker must be at the start of the sweep.
e. Set the time-mark generator for 0.1-second markers.
f. CHECK-Sweep free runs and stable display cannot be obtained. If stable display is obtained, marker must not be at the start of the sweep.

## 34. Check A Sweep Timing Accuracy

REQUIREMENT-Within $3 \%$ over middle eight divisions of the display.
a. CHECK-Using the A TIME/DIV switch and time-mark generator settings given in Table 5-2, Fheck A sweep timing within 0.24 division, over the middle eight divisions of the display (within 3\%). Fia. 5-17 shows a typical CRT display when checking sweep timing.


Fig. 5-17. Typical CRT display showing correct A sweep timing.

NOTE
Unless otherwise noted, use the middle eight horizontal divisions when checking timing.

TABLE 5-2
A and B Timing Accuracy

| A and B <br> TIME/DIV <br> Switch Setting | Time-Mark <br> Generator Output | CRT Display <br> (markers/ <br> division) |
| :---: | :---: | :---: |
| $.1 \mu \mathrm{~s}$ | 0.1 microsecond | 1 |
| $.2 \mu \mathrm{~s}$ | 0.1 microsecond | 2 |
| $.5 \mu \mathrm{~s}$ | 0.5 microsecond | 1 |
| $1 \mu \mathrm{~s}$ | 1 microsecond | 1 |
| $2 \mu \mathrm{~s}$ | 1 microsecond | 2 |
| $5 \mu \mathrm{~s}$ | 5 microsecond | 1 |
| $10 \mu \mathrm{~s}$ | 10 microsecond | 1 |
| $20 \mu \mathrm{~s}$ | 10 microsecond | 2 |
| $50 \mu \mathrm{~s}$ | 50 microsecond | 1 |
| .1 ms | 0.1 millisecond | 1 |
| .2 ms | 0.1 millisecond | 2 |
| .5 ms | 0.5 millisecond | 1 |
| 1 ms | 1 millisecond | 1 |
| 2 ms | 1 millisecond | 2 |
| 5 ms | 5 millisecond | 1 |
| 10 ms | 10 millisecond | 1 |
| 20 ms | 10 millisecond | 2 |
| 50 ms | 50 millisecond | 1 |
| .1 s | 0.1 second | 1 |
| .2 s | 0.1 second | 2 |
| .5 s | 0.5 second | 1 |
|  | A Sweep Only |  |
| 1 1 s | 1 second | 1 |
| 2 s | 1 second | 2 |
| 5 s | 5 second | 1 |
| 2 |  |  |

## 35. Check A Magnified Sweep Accuracy

REQUIREMENT-Within $4 \%$ over middle eight divisions of the CRT display with the MAG switch set to X10. Magnifier light must be on.
a. Set the MAG switch to X10.
b. CHECK-Using the A TIME/DIV switch and time-mark generator settings given in Table 5-3. check A magnified sweep timing within 0.32 division over the middle eight divisions of the magnified display (within 4\%]. Note the portions of the total magnified sweep length to be excluded from the measurement. Magnifier light must be on.

TABLE 5-3
A and B Magnified Accuracy
$\left.\begin{array}{c|c|c|c}\hline \begin{array}{c}\text { A and B } \\ \text { TIME/ } \\ \text { DIV } \\ \text { Switch } \\ \text { Setting }\end{array} & \begin{array}{c}\text { Time- } \\ \text { Mark } \\ \text { Output }\end{array} & \begin{array}{c}\text { CRT } \\ \text { Display } \\ \text { (Mark- } \\ \text { ers/ } \\ \text { Division) }\end{array} & \begin{array}{c}\text { Portions of } \\ \text { total magnified } \\ \text { sweep length } \\ \text { to exclude } \\ \text { from }\end{array} \\ \hline \hline .1 \mu \mathrm{~s} & 10 \text { nanosecond } & 1 & \begin{array}{c}\text { First and last } \\ \text { measurement }\end{array} \\ \hline \text { three divisions }\end{array}\right\}$
c. Set the time-mark generatar for 0.1-millisecond markers.
d. Set the A TME/DIV switch to 1 ms .
e. Position the first eight-division portion of the total magnified sweep onto the viewing area.
f. CHECK-One marker each division between the firstand ninth-division vertical graticule lines; marker at ninthdivision vertical line must be within 0.32 division [within 4\%) of the line when the marker at the first-division vertical line is positioned exactly.
g. Repeat this check for each eight-division portion of the total magnified sweep length.

## 36. Check B Sweep Timing Accuracy

REQUIREMENT-Within $3 \%$ over middle eight divisions of the display.
a. Set the MAG switch to OFF.
b. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
c. CHECK-Using the $A$ and $B$ TME/DIV switch and time-mark generator settings given in Table 5-2 check B sweep timing within 0.24 division over the middle eight divisions of the display [within 3\%).

## 37. Check B Magnified Sweep Accuracy

REQUIREMENT-Within $4 \%$ over middle eight divisions of the CRT display with the MAG switch set to X10.
a. Set the MAG switch to X10.
b. CHECK-Using the A and B TME/DIV switch and timemark generator settings given Tin Table $5-3$, check $B$ magnified sweep timing within 0.32 division over the middle eight divisions of the magnified display (within 4\%). Note the portions of the total magnified sweep length to be excluded from the measurement.

## 38. Check Delay Time Accuracy

REQUIREMENT-DELAY TIME switch (A TIME/DIV) posifions of $1 \mu \mathrm{~s}$ to 20 ms , within $1.5 \%$; 1 s to 5 s , within $2.5 \%$.
a. Set the MAG switch to OFF.
b. CHECK-Using the A TME/DIV switch, B TME/DIV switch and time-mark generator settings given in Table 5-4, check delayed sweep accuracy within the given tolerance. First set the DELAY-TIME MULTIPLER dial to 1.00 and rotate the dial until the sweep starts at the top of the second marker (see Fiq. 5-18). Note the dial reading and then set the dial to 9.00 and rotate slightly until the sweep starts at the top of the tenth marker. DELAY-TIME MULTIPLIER dial setting must be 8.00 divisions higher, + or - the allowable error given in Table 5-4

## NOTE

Sweep will start at top of third marker at 1.00 and nineteenth marker at 9.00 for sweep rates which are multiples of 2 (e.g., $2 \mu \mathrm{~s}, 20 \mu \mathrm{~s}, .2 \mathrm{~ms}$, etc.). If in doubt as to the correct setting of the DELAY-TIME MULTIPLIER dial, set the HORIZ DISPLAY switch to A INTEN DURING B and check which marker is intensified.


FIg. 5-18. Typical CRT display when checking delayed-sweep acaracy.

TABLE 5-4
Delayed Sweep Accuracy

| A TIME/ DIV switch setting | B TIME/ DIV switch setting | TimeMark Generator Output | Allowable Error for Given Accuracy |
| :---: | :---: | :---: | :---: |
| $1 \mu \mathrm{~s}$ | . 1 ¢ | 1 microsecond | $\pm 12$ minor dial divisions ( $\pm 1.5 \%$ ) |
| $2 \mu s$ | . $1 \mu \mathrm{~s}$ | 1 microsecond |  |
| $5 \mu \mathrm{~s}$ | . $5 \mu \mathrm{~s}$ | 5 microsecond |  |
| $10 \mu \mathrm{~s}$ | $1 \mu \mathrm{~s}$ | 10 microsecond |  |
| $20 \mu \mathrm{~s}$ | $1 \mu \mathrm{~s}$ | 10 microsecond |  |
| $50 \mu \mathrm{~s}$ | $5 \mu \mathrm{~s}$ | 50 microsecond |  |
| . 1 ms | $10 \mu \mathrm{~s}$ | 0.1 millisecond |  |
| . 2 ms | $10 \mu \mathrm{~s}$ | 0.1 millisecond |  |
| . 5 ms | $50 \mu \mathrm{~s}$ | 0.5 millisecond |  |
| 1 ms | .1 ms | 1 millisecond |  |
| 2 ms | . 1 ms | 1 millisecond |  |
| 5 ms | . 5 ms | 5 millisecond |  |
| 10 ms | 1 ms | 10 millisecond |  |
| 20 ms | 1 ms | 10 millisecond |  |
| 50 ms | 5 ms | 50 millisecond |  |
| 1 s | 10 ms | 0.1 second | $\pm 20$ minor dial divisions ( $\pm 2.5 \%$ ) |
| 2 s | 10 ms | 0.1 second |  |
| . 5 s | 50 ms | 0.5 second |  |
| 1 s | . 1 s | 1 second |  |
| 2 s | . 1 s | 1 second |  |
| 5 s | . 5 s | 5 second |  |

## 39. Check Delay-Time Multiplier Incremental Linearity

## REQUIREMENT-Within 0.2\%.

a. Change the following control settings:

```
A TME/DIV 1 ms
B TMME/DIV 10 \mus
```

b. Set the time-mark generator for one-millisecond markers.

## NOTE

If the display is not exactly 8.00 dial divisions between 1.00 and 9.00 with the A TMME/DIV switch set to 1 ms as measured in step 37, use parts c through k to compensate for this error. Then the incremental linearity of the DELAY-TMME MULTIPLIER dial can be read directly from the dial. If the difference is exactly eight divisions, proceed to part m.
c. Set the A TIME/DIV switch to .5 ms ; then retum the B TIME/DIV switch to $10 \mu \mathrm{~s}$.


Fig. 5-19. Typical CRT display when checking DELAY-TIME MULTIPLIER dial incremental linearity.
d. Set the HORIZ DISPLAY switch to A.
e. Set the A VARIABLE control for one marker each division between the first- and ninth-division vertical lines.
f. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
g. Set the DELAY-TMME MULTPUER dial to 1.00 and rotate slightly until a marker is displayed at the start af the sweep. Note the dial reading.
h. Set the DELAY-TMME MULTIPUER dial exactly 8.00 dial divisions higher than the reading in part $g$.
i. Turn the A VARIABLE control slightly so a marker is displayed at the start of the sweep.
j. Set the HORIZ DISPLAY switch to A INTEN DURING $B$ and check for nine markers between the DELAY-TIME MULTIPLER dial positions of 1.00 and 9.00 .
k. Retum the HORIZ DISPLAY switch to DELAYED SWEEP (B) and repeat parts g through j until the difference between the markers at about 1.00 and 9.00 is exactly 8.00 dial divisions.
I. Set the DELAY-TIME MULTIPUER dial to 9.00 .
m . Rotate the DELAY-TIME MULTIPLER dial slightly so a marker is displayed at the start of the sweep (se Fig. 5-19).
$n$. Note the exact DELAY-TIME MULTIPUER dial reading.
o. Set the DELAY-TIME MULTIPLIER dial to 8.00.
p. CHECK-Dial reading should be $8.00 \pm 2$ minor dial divisions (within $0.2 \%$ ). Take into account the basic dial error at 9.00.
q. Repeat check at each major dial division between 8.00 and 1.00 .

## 40. Check Delay-Time Jitter

REQUIREMENT-One part or less in 20,000.
a. Change the following control settings:

| DELAY TMME MULTIPLIER | 1.00 |
| :--- | :--- |
| A TME/DIV | 1 ms |
| B TME/DIV | $1 \mu \mathrm{~s}$ |
| A VARIABLE | CAL |

b. Position the pulse near the center of the display a rea with the DELAY-TIME MULTIPLIER dial.
c. CHECKJJitter on the leading edge of the pulse should not exceed 0.5 division ( 1 part in 20,000 see Fig. 5-20). Disregard slow drift.
d. Turn the DELAY-TMME MULTIPLIER dial to 9.00 and adjust so the pulse is displayed near the center af the display area.
e. CHECK-Jitter on leading edge of the pulse should not exceed 0.5 division; se Fig. 5-2b. Disregard slow drift.

## 41. Check Magnifier Register

REQUIREMENT-Less than 0.2 -division shift when switching MAG switch from X10 to OFF.
a. Set the time-mark generator for five-millisecond markers.
b. Change the following control settings:

$$
\begin{array}{ll}
\text { HORIZ DISPLAY } & \text { A } \\
\text { MAG } & \times 10
\end{array}
$$

C. Position the middle marker (three markers on total sweep) to the center vertical line with the horizontal POSITION and FINE controls (se Fia. 5-21A ).
d. Set the MAG switch to OFF.
e. CHECK-Trace shift less than 0.2 division (see Fig $5-21 \mathrm{~B}$ ).

## 42. Check A Sweep Length

REQUIREMENT-Variable from four divisions or less to 11.0 divisions, $\pm 0.5$ division.
a. Set the time-mark generator for 1- and 0.1-millisecond markers.
b. Set the A LEVEL control for a stable display.
c. Move the eleventh marker to the center vertical line with the horizontal POSITION control (see Fig. 5-22). Large markers indicate divisions and small markers indicate 0.1 division.

Check leading edge of delayed sweep display for jitter


Fig. 5-20. Typical CRT display when checking delay-time jitter.
d. CHECK-A sweep length must be between 10.5 and 11.5 divisions as shown by 0.5 to 1.5 divisions of display to the right of the center vertical line (se Fig. 5-22).
e. Reposition the first marker to the left graticule line.
f. Tum the A SWEEP LENGTH control to 4 DIV (not in $B$ ENDS A detent).
g. CHECK-A sweep length must be four divisions or less.

## 43. Check B Sweep Length

REQUIREMENT-11.0 divisions, $\pm 0.5$ division.
a. Change the following control settings:

| DELAY-TIME MULTPLIER | Fully counterclockwise |
| :--- | :--- |
| A TIME/DIV | 2 ms |
| B TMME/DIV | 1 ms |
| B SWEEP MODE | TRIGGERABLE AFIER |
|  | DELAY TMME |
| HORIZ DISPLAY | DELAYED SWEEP (B) |
| A SWEEP LENGTH | FULL |

b. Adjust the B LEVEL control for a stable display.
q. Move the eleventh large marker to the center vertical line with the horizontal POSITION control (see Fiq. 5-22).
d. CHECK-B sweep length must be between 10.5 and 11.5 divisions as shown by 0.5 to 1.5 divisions of display to the right of the center vertical line (se Fig. 5-2k).

## 44. Check B Ends A Operation

REQUIREMENT-A sweep ends immediately after the end of the B sweep when the A SWEEP LENGTH control is set to $B$ ENDS A.
a. Change the following control settings:

| A TME/DIV | 1 ms |
| :--- | :--- |
| B TME/DIV | .1 ms |
| B SWEEP MODE | B STARTS AFIER |
|  | DELAY TME |
| HORIZ DISPLAY | A INTEN DURING B |
| A SWEEP LENGTH | B ENDS A |



Fig. 5-21. Typical CRT display showing correct magnifier registration. (A) MAG switch set to XI O, (B) MAG switch set to OFF.
b. Rotate the DELAY-TMME MULTIPLIER dial throughout its range.
c. CHECK-CRT display ends after the intensified portion at all DELAY-TME MULTPLIER dial settings.

## 45. Check A Variable Control Range

REQUIREMENT-Continuously variable sweep rate between calibrated A TIME/DIV switch settings.


Fig. 5-22. Typical CRT display when checking A and Bweep length.
a. Change the following control settings:

| DELAY-TIME MULTIPLIER | Fully counterclockwise |
| :--- | :--- |
| B TME/DIV | 1 ms |
| HORIZ DISPLAY | A |
| A SWEEP LENGTH | FULL |

b. Set the time-mark generator for 10-millisec ond markers.
c. Set the A LEVEL control for a stable display.
d. Position the markers to the far left and right graticule lines with the horizontal POSITION control.
e. Tum the A VARIABLE control fully counterclockwise.
f. CHECK-CRT display for four-divisions maximum spacing between markers (indicates adequate range for continuously variable sweep rate between the calibrated steps; se Fig. 5-23) UNCAL A OR B light must be on when A VARIABLE control is not in CAL position.

Spacing between markers must be four divisions or less for correct VARIABLE control range.


Fig. 5-23. Typical CRT display when checking A and BARIABLE control range.

## 46. Check B Variable Control Range

REQUIREMENT-Continuously variable sweep rate between calibrated B TIME/DIV switch settings.
a. Change the following control settings:

| A TME/DIV | 5 ms |
| :--- | :--- |
| B TMME/DIV | 1 ms |
| A VARIABLE | CAL |
| B SWEEP MODE | TRIG GERABLE AFIER |
|  | DELAY TIME |
| HORIZ DISPLAY | DELAYED SWEEP (B) |

b. Position the markers to the far left and right graticule lines with the horizontal POSITION control.
C. Tum the $B$ TIME/DIV VARIABLE control (on side panel) fully counterclockwise.
d. CHECK-CRT display for four-division maximum spacing between markers (indicates adequate range for continuously variable sweep rate between the calibrated steps; see Fig.

5-23). UNCAL A OR B light must be on when B VARIABLE control is not in CAL position.

## 47. Check X Gain

REQUIREMENT-Correct horizontal deflection for EXT HORIZ mode operation in the 20 mV CH 1 VOLTS/DIV switch position.
a. Chonge the following control settings:

| VOLTS/DIV | 20 mV |
| :--- | :--- |
| MODE | CH 2 |
| TRIGGER | CH 1 ONLY |
| B COUPLING | DC |
| HORIZ DISPLAY | EXT HORIZ |

b. Connect the standard amplitude calibrator to the Channel 1 INPUT connector with the 42 -inch BNC cable.
c. Set the standard amplitude calibrator for a 0.1 -volt square-wave output.
d. Increase the INTENSTTY control setting until the display (two dots about five divisions apart] is visible.
e. Move the display to the center of the graticule with the Channel 1 POSITION control.
f. CHECK-CRT display for five divisions horizontal deflection (se Fig. 5-24).


Fig. 5-24. Typical CRT display showing correct $X$ Gain.

## 48. Check External Horizontal Operation

a. Set the B SOURCE switch to EXT.
b. Connect the standard amplitude calibrator to the EXT HORIZ input connector (B EXT TRIG INPUT).
c. Set the standard amplitude calibrator for a two-volt square-wave output.
d. CHECK-CRT display for horizontal deflection between 6.5 and 8.7 divisions ( 270 millivolts/division, $\pm 15 \%$ ).
e. Set the standard amplitude calibrator for a 20 -volt square-wave output.
f. Set the B SOURCE switch to EXT $\div 10$.
g. CHECK-CRT display for horizontal deflection between 6.2 and 9.2 divisions ( 2.7 volts/division, $\pm 20 \%$ ).
h. Disconnect all test equipment.

## 49. Check X-Y Phasing

REQUIREMENT-3ºr less phase shift up to two megahertz.
a. Connect the constant-amplitude sine-wave generator to the Channel 1 and 2 INPUT connectors through the fivenanosecond GR cable, 50 -ohm in-line temination and the dual-input coupler.
b. Change the following control settings:

| CH 1 VOLTS/DIV | 10 mV |
| :--- | :--- |
| CH 2 VOLTS/DIV | 50 mV |
| B SOURCE | INT |

c. Set the constant-amplitude generator for a 10 -division horizontal display at 50 kilohertz.
d. Center the display vertically and horizontally with the Channel 1 and 2 POSITION controls.
e. CHECK-CRT display for an opening at the center horizontal line of 0.52 division ar less ( $3^{\circ}$ or less phase shift; se Fig. 5-25).

0.52 division or less

Fig. 5-25. Typical CRT display when checking X-Y phasing.

## 50. Check $X$ Bandwidth in $X-Y$ Mode

REQUIREMENT-Not more than -3 dB at five megahertz.
a. Disconnect the dual-input coupler from the Channel 2 INPUT connector.
b. Set the constant-amplitude generator for a six-division horizontal display at its reference frequency ( 50 kHz ).
c. Without changing the output amplitude, increase the output frequency of the generator until the horizontal deflection is reduced to 4.2 divisions ( -3 dB point; se Fig. 5-26).


Fig. 5-26. Typleal CRT display when checking external horizonial bondwidth (double exposure).
d. CHECK-Output frequency of generator must be five megahertz or higher.

## 51. Check Trace Finder Operation

REQUIREMENT-Display remains within graticule area when TRACE FINDER button is depressed regardless of the deflection factor or POSITION control settings.
a. Reconnect the dual-input coupler to the Channel 2 INPUT connector.
b. While holding the TRACE FINDER button depressed, rotate the Channel 1 and 2 POSITION controls and CH 1 and CH 2 VOLTS/DIV switches throughout their range.
c. CHECK-CRT display remains within the graticule area.
d. While holding the TRACE FINDER button depressed, adjust the positioning controls until the display is centered about the graticule center lines. Then, increase the $X$ and $Y$ deflection factors until the display is reduced to about two divisions vertically and about four divisions horizontally.
e. Release the TRACE FINDER button.
f. CHECK-CRT display must remain within the graticule area.
g. Reduce the INTENSITY control to a nomal setting.
h. Disconnect all test equipment.

## 52. Check Chopped Operation

REQUIREMENT-Chopped repetition rate, 500 kilohertz, $\pm 20 \%$; switching transients blanked out.
a. Change the following control settings:

| MODE | CHOP |
| :--- | :--- |
| TRIGGER | NORM |
| A and B TIME/DIV | $.5 \mu \mathrm{~s}$ |
| HORIZ DISPLAY | A |
| B TMME/DIV VARIABLE | CAL |

b. Position the traces about four divisions apart.
c. Set the A LEVEL control for a stable display.
d. CHECK-Each cycle for duration of 3.4 to 5 divisions ( 500 kilohertz, $\pm 20 \%$; see Fig. 5-27).
e. CHECK-CRT display for complete blanking of switching transients between chopped segments (se Fig. 5-27).


Fig. 5-27. Typical CRT display when checking chopped repetition rate and blanking.

## 53. Check Calibrator Repetition Rate

REQ UIREMENT-One kilohertz, $\pm 0.5 \%$.
a. Change the following control settings:

| CH 1 VOLTS/DIV | .5 |
| :--- | :--- |
| CH 2 VOLTS/DIV | .2 |
| MODE | ALT |
| B COUPLING | AC |
| A and B TMME/DIV | .1 ms |

b. Connect the 1 kHz CAL connector to the Channel 1 INPUT connector with an 18 -inch 50 -ohm BNC cable.
c. Connect the time-mark generator to the Channel 2 INPUT connector through a 42 -inch 50 -ohm BNC cable and a 50 -ohm BNC termination.
d. Set the time-mark generator for one-millisecond markers.
e. Position the display vertically so the tips of the markers fall just below the rising portions of the square wave.
f. Set the A LEVEL control so both waveforms start at the same point.
g. Position the rising portion of the second calibrator cycle to the center vertical line.
h. Set the MAG switch to X10.
i. CHECK-Separation between Calibrator waveform leading edge and the marker leading edge not to exceed 0.5 division ( $0.5 \%$ accuracy; se $\square$ Fig. 5-28).
j. Disconnect the time-mark generator.


Fig. 5-28. Typical CRT display showing correct calibrator repetition rate.

## 54. Check Calibrator Duty Cycle

REQ UIREM ENT-49\% to $51 \%$.
a. Change the following control settings:

| CH 1 VOLTS/DIV | .2 |
| :--- | :--- |
| MODE | CH 1 |
| MAG | OFF |

b. Center the display vertically with the Channel 1 POSITION control.
c. Set the A LEVEL control so the display starts at the $50 \%$ point on the rising portion of the waveform (the INTENSITY control may need to be advanced slightly to see the rising portion of the waveform).
d. Set the MAG switch to X10.
e. Position the $50 \%$ point on the falling edge of the Calibrator waveform to the center vertical line.
f. Set the A SLOPE switch to -.
g. CHECK-50\% point on rising edge now displayed not displaced more than two divisions from the center vertical line (duty cycle $49 \%$ to $51 \%$; see Fig. 5-29).

## 55. Check Calibrator Risetime

REQUIREMENT-One microsecond or less.
a. Change the following control settings:

A SLOPE
$A$ and $B$ TMME/DIV

$$
\begin{aligned}
& + \\
& .2 \mu s \\
& \text { OFF }
\end{aligned}
$$

M A G
b. Set the A LEVEL control so all of the rising portion of the Calibrator waveform is visible.
c. Position the $10 \%$ point of the leading edge to a vertical graticule line.


Fig. 5-29. Typical CRT display when checking calibrator duty cycle.
d. CHECK-CRT display for five divisions or less between the $10 \%$ and $90 \%$ points on the leading edge of the calibrator waveform (one microsecond or less risetime; see Fig. 5-30),


Fig. 5-30. Typical CRT display when checking calibrator risetime.

## 56. Check Calibrator Voltage Output

REQ UIREMENT-O ne volt, $\pm 1 \%$.
a. Change the following control settings:

| CH 1 VOLTS/DIV | .1 |
| :--- | :--- |
| A SOURCE | LINE |
| A and B TMME/DIV | 5 ms |
| CAUBRATOR | 1 V |

b. Connect the 1 kHz CAL connector to the unknown input connector of the standard amplitude calibrator with a 42-inch BNC cable.
c. Set the standard amplitude calibrator for a positive one-volt DC output in the mixed mode.
d. Connect the standord amplitude calibrator output to the Channel 1 INPUT connector.
e. Set the A LEVEL control for a stable display.
f. Position the top of the waveform onto the display area with the Channel 1 POSITION control.
g. CHECK-Difference between the standard amplitude calibrator output level and the TYpe 453 Calibrator output is 0.1 division or less (one volt output, $\pm 1 \%$; se $\square$ Fig. 5-31).
h. Set the CALBRATOR switch (side panel) to .1 V .
i. Set the standard amplitude calibrator for a positive, 0.1 -volt DC output in the mixed mode.
j. Position the top of the waveform onto the display area with the Channel 1 POSTIION control.
k. CHECK-Difference between the standard amplitude calibrator output level and the Type 453 Calibrator output is 0.1 division or less ( 0.1 volt output, $\pm 1 \%$; see Fig. 5-31).


Fig. 5-31. Typical CRT display when checking voltage output of calibrator.

## 57. Check Current Through Probe Loop REQUIREMENT-Five milliamperes.

a. Connect the current-measuring probe and passive termination to the Channel 1 INPUT connector.
b. Set the passive termination for a sensitivity of $2 \mathrm{~mA} / \mathrm{mV}$.
c. Clip the current-measuring probe around the PROBE LOOP on the side panel.
d. Change the following control settings:
CH 1 VOLTS/DIV 5 mV
A SOURCE
INT
e. CHECK-CRT display 0.5 division in amplitude (five millia mperes; se Fig. 5-32).

## NOTE

This step checks far the presence of current in the PROBE LOOP. This current will remain within the


Fig. 5-32. Typical CRT display when checking calibrator current.
stated $1 \%$ accuracy due to the tolerance of the divider resistors and tolerance of the Calibrator output voltage. If it is necessary to verify the accuracy of the Calibrator current, use a current-measuring meter with an accuracy of at least $0.25 \%$.
f. Disconnect all test equipment.

## 58. Check External Z Axis Operation

REQUIREMENT-Noticeable trace modulation with fivevolt signal from DC to 50 megahertz or greater.
a. Change the following control settings:
A SOURCE
EXT
$A$ and $B$ TIME/DIV
$20 \mu \mathrm{~s}$
b. Set the INTENSITY control to a nomal setting.
c. Connect the constant-amplitude generatar to the A EXT TRIG INPUT connector through the five-nanosecond GR cable, 50 -ohm in-line temination ond BNC T connector. Connect the output of the BNC T connector to the ZAXIS INPUT binding posts through a 42 -inch BNC cable and the BNC to alligator clip adapter (connect black lead of alligator clip adapter to ground post).
d. Remove the ground strap from between the binding posts.
e. Set the constant-amplitude generator for five volts output at 50 kilohertz (use calibrated position of generator amplitude control).
f. CHECK-CRT display for noticeable intensity modulation (se Fig. 5-3BA). The INTENSITY control setting may need to be reduced to view trace modulation.
g. Set the constant-amplitude generator for five volts output at 50 megahertz (use calibrated position of generator amplitude control).
h. Set the A and B TIME/DIV switch to .1.
i. CHECK-CRT display for noticeable intensity modulation (see Fig. 5-33B). The INTENSITY control setting may need to be reduced to view trace modulation.


Fig. 5-33. (A) Typical CRT display when checking Z-axis operation et 50 kilohertz, (B) typical CRT display when checking Z-axis op-- retion e 50 megahertz.
i. Disconnect all test equipment and replace ground strap.

## 59. Check A Gate Output Signal

REQ UIREMENT-Polarity, positive going; amplitude, 12 volts $\pm 10 \%$; duration, about 11 times the A TIME/DIV switch setting.
a. Set the $A$ and $B$ TMME/DIV switch to 1 ms . Be sure the A SWEEP LENGTH control is set to FULL.
b. Connect the A GATE connector (on side panel) to the test oscilloscope input connector with the 42-inch BNC cable.
c. Set the test oscilloscope for a vertical deflection factor of five volts/division at a sweep rate of two milliseconds/ division.
d. CHECK-Test oscilloscope display for 2.4 divisions $\pm 0.24$ division, vertical deflection with the bottom of the waveform near the zero-volt level ( 12 volts $\pm 10 \%$; see Fig. 5-34) Gate duration should be about 5.5 divisions (about 11 times the A TME/DIV switch setting).


Fig. 5-34. Typical test oscilloscope display when checking $A$ and B GATE output amplitude and duration (vertical deflection factor, five volts/division; sweep rate, two millseconds/division).

## 60. Check B Gate Output Signal

REQ UIREMENT-Polarity, positive going; amplitude, 12 volts $\pm 10 \%$; duration, about 11 times the B TIME/DIV switch setting.
a. Connect the B GATE connector (on side panel) to the test oscilloscope input connector with the 42-inch BNC cable.
b. Change the following control settings:

| A TIME/DIV | 2 ms |
| :--- | :--- |
| B TIME/DIV | 1 ms |
| HO RIZ DISPLAY | DELAYED SWEEP (B) |

C. CHECK-Test oscilloscope display for 2.4 divisions $\pm 0.24$ division vertical deflection with the bottom of the waveform near the zero-volt level ( 12 volts $\pm 10 \%$; see Fig. 5-34. Gate duration should be about 5.5 divisions (about 11 times the B TME/DIV switch setting).

This completes the performance check procedure for the Type 453. If the instrument has met all performance requirements given in this procedure, it is correctly calibrated and within the specified tolerances.

## CALIBRATION

## Introduction

Complete calibration information for the Type 453 is given in this section. This procedure calibrates the instrument to the performance requirements listed in the Characteristics section. The Type 453 can be retumed to original performance standards by completion of each step in this procedure. If it is desired to merely touch up the calibration, perform only those steps entitled "Adiust . . .". A short-form calibration procedure is also provided in this section for the convenience of the experienced calibrator.

The Type 453 should be checked, and recalibrated if necessary, after each 1000 hours of operation, or every six months if used infrequently, to assure correct operation and accuracy. The Performance Check section of this manual provides a complete check of instrument performance without making intemal adjustments. Use the performance check procedure to verify the calibration of the Type 453 and determine if recalibration is required.

## TEST EQUIPMENT REQUIRED

## General

The following test equipment, or its equivalent, is required for complete calibration of the Type 453 (see Figs. 6-1] and $6-2$ ). Specifications given are the minimum necessary for accurate calibration of this instrument. All test equipment is assumed to be correctly calibrated and operating within the given specifications. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

For the quickest and most accurate calibration, special Tektronix calibration fixtures are used where necessary. These special calibration fixtures are available from Tektronix, Inc. Order by part number through your local Tektronix Field Office or representative.

1. Variable autotransformer. Must be capable of supplying 200 volt-amperes over a range of 90 to 137 volts ( 180 to 274 volts for 230 -volt nominal line). (If autotransformer does not have an AC voltmeter to indicate output voltage, monitor the output with an AC voltmeter with range of at least 137 or 274 volts, RMS.) For example, General Radio W10MT3W Metered Variac Autotransformer (note that the full current capabilities of this unit are not required).
2. Precision DC voltmeter. Accuracy, within $\pm 0.057 \%$; meter resolution, 50 microvolt; range, zero to two kilovolts. For example, Fluke Model 825A Differential DC Voltmeter [use Fluke Model 80E-2 Voltage Divider to measure voltages above 500 volts).
3. Test Oscilloscope. Bandwidth, DC to 50 megahertz; minimum deflection factor, five millivolts/division; accuracy, within $3 \%$. Tektronix Type 453 Oscilloscope recommended.
4. $1 \times$ Probe with BNC connector. Tektronix P6011 Probe recommended.
5. 10X Probe with BNC connector. Tektronix P6010 Probe recommended.
6. Time-mark generator. Marker outputs, five seconds to 10 nanoseconds; marker accuracy, within $0.1 \%$. Tektronix Type 184 Time-Mark Generator recommended.
7. Standard amplitude calibrator. Amplitude accuracy, within $0.25 \%$; signal amplitude, five millivolts to 50 volts; output signal, one-kilohertz square wave and positive DC voltage. Tektronix calibration fixture 067-0502-00 recommended.
8. Square-wave generator. Frequency, one and 100 kilohertz; risetime, 12 nanoseconds or less from high-amplitude output and one nanosecond or less from fast-rise output (into 50 ohms); output amplitude, about 120 volts unterminated or 12 volts into 50 ohms from high-a mplitude output- 50 to 500 millivolts into 50 ohms from fast-rise output. Tektronix Type 106 Square-Wave Generator recommended.
9. Constant-amplitude sine-wave generator. Frequency, 350 kilohertz to above 50 megahertz; reference frequency, 50 kilohertz; output amplitude, variable from five millivolts to five volts into 50 ohms or 10 volts unterminated; a mplitude accuracy, within $3 \%$ at 50 kilohertz and from 350 kilohertz to above 50 megahertz. Tektronix Type 191 Constant Amplitude Signal Generator recommended.
10. Low-frequency sine-wave generator. Frequency, 60 hertz to one megahertz; output amplitude, variable from 0.5 volts to 40 volts peak to peak; amplitude accuracy, within $3 \%$ from 60 hertz to one megahertz. For example, General Radio 1310-A Oscillator (use a General Radio Type 274 QBJ Adaptor to provide BNC output).
11. Current-measuring probe with passive termination. Sensitivity, two milliamperes/millivolt accuracy, within $3 \%$. Tektronix P6019 Curent Probe with 011-0078-00 passive termination recommended.
12. Cable (two). Impedance, 50 ohms; type, RG-58/U; length, 42 inches; connectors, BNC. Tektronix Part No. 012-0057-01.
13. BNC T connector. Tektronix Part No. 103-0030-00.
14. Cable. Impedance, 50 ohms; type, RG-58/U; length, 18 inches; connectors, BNC. Tektronix Part No. 012-00764-00.
15. Cable. Impedance, 50 ohms; type, RG-213/U; electrical length, five nanoseconds; connectors, GR874. Tektronix Part No. 017-0502-00.
16. In-1ine termination. Impedance, 50 ohms; wattage rating, two watts; accuracy, $\pm 3 \%$; connectors, GR874 input with BNC male output. Tektronix Part No. 017-0083-00.

(5)

(6)


4
(9)


30

(1)


Fig. 6-1. Recommended test equipment. Ifems 1 through 12.


Fig. 6-2. Recommended test equipment. Items 13 through 26.
17. Input $R C$ normalizer. Time constant, 1 megohm $X 20$ pF; attenuation, 2X; connectors, BNC. Tektronix calibration fixture 067-0538-00.
18. 5X attenuator. Impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, GR874. Tektronix Part No. 017-0079-00.
19. Dual-input coupler. Matched signal transfer to each input. Tektronix calibration fixture 067-0525-00.
20. Adapter. Adapts GR874 connector to BNC female connector. Tektronix Part No. 017-0064-00.
21. Termination. Impedance, 50 ohms; accuracy, $\pm 3 \%$; connectors, BNC. Tektronix Part No. 011-0049-00.
22. Adapter. Connectors, BNC female and two alligator clips. Tektronix Part No. 013-0076-00.
23. Screwdriver. Three-inch shaft, $3 / 32$-inch bit for slotted screws. Tektronix Part No. 003-0192-00.
24. Low-capacitance screwdriver. 1 $1 / 2$-inch shaft. Tektronix Part No. 003-0000-00.
25. Tuning rod. Five-inch, for 0.100 -inch (ID) hex slugs. Tektronix Part No. 003-0301-00.
26. Tuning tool. Handle and insert for $5 / 64$-inch (ID) hex cores. Tektronix Part Nos. 003-0307-00 and 033-0310-00.

## SHORT-FORM CAUBRATION PROCEDURE

This short-form calibration procedure is provided to aid in checking the operation of the Type 453. It may be used as a calibration guide by the experienced calibrator, or it may be used as a record of calibration. Since the step numbers and titles used here correspond to those used in the complete procedure, this procedure also serves as an index to locate a step in the complete Calibration Procedure. Performance requirements correspond to those given in Section 1] of this manual.

Type 453, Serial No.

## Calibration Date

## Calibrated by

1. Adiust -12-Volt Power Supply (R1122). Page 6-8 -12 volts, $\pm 0.02$ volt.
2. Adiust +12-Volt Power Supply (R1152).

Page 6-8 Adiust for +1 volt, $\pm 0.002$ volt, at 1 kHz CAL connector with Q 1255 removed. Check for +12.1 volts, $\pm 0.12$ volt, output from supply.
$\square$ 3. Adjust +75 -Volt Power Supply (R1182).
Paqe 6-9 +75 volts, $\pm 0.2$ volt.
$\square$ 4. Adiust High-Voltage Supply and Check Page 6-10 Regulation (R900).
-1950 volts, $\pm 20$ volts. Must maintain this output level over input line voltage range and INTENSITY control changes.
$\square$ 5. Adjust CRT Grid Bias (R940).
Page 6-10
See procedure.6. Check-Low-Voltage Power-Supply Ripple Page 6-11

Two millivolt peak-to-peak maximum ripple on the 12-, $\quad+12-\quad$ and +75 -volt supplies.7. Adjust Trace Alignment [R980).

Page 6-12
Trace parallel to horizontal graticule lines.8. Adjust Astigmatism (R985).

Page 6-13
Sharp, well-defined display.9. Adjust $Y$ Axis Alignment (R989).

Page 6-14
Markers parallel to the center vertical line.
$\square$ 10. Adjust CRT Geometry (R982).
Page 6-14
Minimum bowing or tilt of markers at left and right extremes of display.11. Adiust Channel 1 and 2 Step Atten- Page 6-14 uator Balance (R30, R130).

No trace shift as CH 1 or CH 2 VOLTS/DIV switch is changed from 20 mV to 5 mV .
12. Adjust Channel 1 and 2 Position Center Page 6-15 (R55, R155).

Trace at center horizontal line with Channel 1 and 2 POSITION controls centered.13. Adjust Channel 1 and 2 Gain (R90, R190). Page 6-17

Correct vertical deflection in the 20 mV positions of the CH 1 and CH 2 VOLTS/DIV switches.14. Check Added Mode Operation.

Page 6-18
Correct signal addition.15. Check Channel 1 and 2 Deflection

Page 6-18 Accuracy.

Vertical deflection within $3 \%$ of CH 1 and CH 2 VOLTS/DiV switch indication.16. Check Channel 1 and 2 Variable

Page 6-18 Volts/Division Range.

Continuously variable deflection factor between the calibrated steps.17. Check Channel 1 and 2 Cascaded Page 6-19 Deflection Factor.

One millivolt/division or less.18. Check Channel 1 and 2 Input Coupling Page 6-19 Switch Operation.

Correct signal coupling in each position of the Channel 1 and 2 Input Coupling switches.
19. Check Low-Frequency Vertical Linearity. Page 6-19 0.15 division, or less compression or expansion of a two-division signal (at center screen) when positioned to the vertical extremes of the graticule area.
20. Check Trace Shift Due to Input Gate Page 6-20 Current.

Trace shift negligible.
21. Check Altemate Operation.

Page 6-20
Trace altemation at all sweep rates.
22. Adjust Channel 1 Volts/Division Switch Page 6-21 Compensation (C6B, C6C, C7B, C7C, C8B, C8C, C9B, C9C, C11, C17).

Optimum Channel 1 square-wave response.
23. Adjust Channel 2 Volts/Division Switch $\square$ Page 6-22 Compensation (C 106B, C106C, C 107B, C107C, C108B, C108C, C109B, C109C, C111, C117).

Optimum Channel 2 square-wave response.
24. Adjust High-Frequency Compensation Page 6-23 C 43A, C $43 \mathrm{C}, \mathrm{C} 44 \mathrm{~A}, \mathrm{C} 44 \mathrm{C}, \mathrm{C} 45 \mathrm{~A}, \mathrm{C} 49, \mathrm{C} 54, \mathrm{C} 143 \mathrm{~A}$, C143C, C144A, C144C, C145A, C149, C154, C263, C265, C328, C336, L43A, L143A, R43C, R49, R44C, R143C, R144C, R149, R328).

Optimum square-wave response.25. Check Upper Vertical Bandwidth Limit Page 6-26 of Channel 1 and 2.

20 mV , not more than -3 dB at 50 megahertz; 10 mV , not more than -3 dB at 45 megahertz; 5 mV , not more than -3 dB at 40 megahertz.
26. Check Upper Added Mode Bandwidth Page 6-27 Limit.

Not more than -3 dB at 50 megahertz.
27. Check Upper Channel 1 and 2 CascadedPage 6-27 Bandwidth Limit.

Not more than -3 dB at 25 megahertz.
28. Check Common-Mode Rejection Ratio. Page 6-28

20:1 or greater at 20 megahertz.29. Check Attenuator Isolation Ratio.

Page 6-29
$10,000: 1$ or greater at 20 megahertz.
30. Adjust A and B Trigger Level Centering Page 6-30 [R462, R662).

Correct operation of trigger circuits; see procedure.
31. Adjust Channel 1 Trigger DC Level Page 6-31 and Normal Trigger DC Level (R60, R285).

Correct operatian of trigger circuits; see procedure.32. Check A and B Intemal Triggering

Page 6-31 Operation.
Stable display in AC, LF REJ and DC positions of A and B COUPUNG switches with 0.2-division display at 10 megahertz and one-division display at 50 megahertz.

## 33. Check A and B Extemal Triggering <br> Page 6-32

 Operation.Stable display in AC, LF REJ and DC positions of A and B COUPLING switches with a 50 -millivolt signal at 10 megahertz and a 200 -millivolt signal at 50 megahertz.
34. Check A and B Low Frequency Triggerin Page 6-33 Operation.
Intemal, stable display in AC, HF REJ and DC positions of A and B COUPLING switches with 0.2division display at 60 hertz; extemal, stable display in $A C, H F$ REJ and $D C$ positions of $A$ and $B$ COUPUNG switches with a 50 -millivolt signal at 60 hertz.
35. Check A and B High-Frequency Reject

Page 6-33 Operation.

Stable display with 0.2 -division display at 50 kilohertz; does not trigger at one megahertz.
36. Check A and B Low-Frequency Reject Page 6-34 Operation.

Stable display with 0.2 -division display at 30 kilohertz; does not trigger at 60 hertz.
37. Check Single Sweep Operation.

Page 6-34
Sweep triggers at same A LEVEL control setting as in AUTO TRIG; after each sweep, further displays are locked out until the RESET button is pressed.
38. Check A and B Slope Switch Operation. Page 6-34

Stable triggering on correct slope of trigger signal.
39. Check $A$ and $B$ Level Control Range. Page 6-35

EXT, at least + and - 2 volts; EXT $\pm 10$, at least + and - 20 volts.
40. Check Line Triggering Operatian.

Page 6-35
Stable display of line-frequency signal, triggered on the correct polarity.
$\square$ 41. Check Auto Recovery Time and Operatior. Page 6-37
Stable display with 50 -millisecond markers ( 20 hertz); free-running display with 0.1 -second markers.
42. Adiust Sweep Start and A Sweep Cali- Page 6-37 bration (R531, R758).
Correct operation of sweep circuits; see procedure.
43. Adjust Normal Gain (R835).

Page 6-38
Correct A sweep timing at $1 \mathrm{~ms} /$ DIV.44. Adjust Magnified Gain (R845).

Page 6-38
Correct A sweep timing at $1 \mathrm{~ms} /$ DIV with the MAG switch set to X 10 .45. Adjust Magnifier Register (R855).

Paqe 6-39
Less than 0.2-division shift when switching MAG switch from X10 to OFF.
46. Adjust B Sweep Calibration (R741].

Page 6-39
Correct B sweep timing at $1 \mathrm{~ms} / \mathrm{DIV}$.47. Check B Sweep Length.

Page 6-39
11.0 divisions, $\pm 0.5$ division.48. Check A Sweep Length.

Page 6-39
Variable from four divisions, or less, to 11.0 divisions, $\pm 0.5$ division.
49. Check B Ends A Operation.

Page 6-40
A sweep ends immediately after the end of B sweep when the A SWEEP LENGTH control is set to $B$ ENDS A.50. Check A Variable Control Range. Page 6-40

Continuously variable sweep rates between the calibrated A TIME/DIV switch settings.
51. Check B Variable Control Range.

Page 6-41
Continuously variable sweep rates between the calibrated B TME/DIV switch settings.
52. Adjust $A$ and $B$ One Microsecond Timing Page 6-41 (C530A, C 740A).

Correct A and B sweep timing atl $\mu s / D I V$.53. Adjust High-Speed Linearity (C882, C 892). Page 6-42

Optimum linearity over the center eight divisions.
54. Check A Sweep Timing Accuracy.

Page 6-42
Wthin $3 \%$ over middle eight divisions of the display.
55. Check A Magnified Sweep Accuracy. Paqe 6-42

Within $4 \%$ over middle eight divisions of the CRT display with the MAG switch set to X10. Magnifier light must be on.
56. Check B Sweep Timing Accuracy.

Page 6-43
Within $3 \%$ over middle eight divisions of the display.
57. Check B Magnified Sweep Accuracy.

Page 6-43
Within 4\% over middle eight divisions of the CRT display with the MAG switch set to X10.
58. Check Delay-Time Accuracy.

Page 6-43
DELAY TIME switch (A TIME/DIV) settings of $1 \mu \mathrm{~s}$ to 50 ms , within $1.5 \%$; 1 s to 5 s , within $2.5 \%$.
59. Check Delay-Time Multiplier Incremental Page 6-44 Linearity.

Within $0.2 \%$.60. Check Delay-Time Jitter. $\quad$ Page 6-44

One part, or less, in 20,000.
61. Adjust Extemal Horizontal Gain (R645). Page 6-46

Correct horizontal deflection for extemal horizontal mode operation in the 20 mV CH 1 VOLTS/DIV switch position.62. Check Extemal Horizontal Operation.

Page 6-47
B SOURCE switch set to EXT, 270 millivolts/division, $+15 \%$; B SOURCE switch set to EXT $\div 10,2.7$ volts/ division, $\pm 20 \%$.63. Check X-Y Phasing.

Paqe 6-47
$3^{\circ}$ or less phase shift up to 50 kilohertz.64. Check X Bandwidth in Extemal Hori- Page 6-47 zontal Mode.

Not more than -3 dB at five megahertz.65. Check Beam Finder Operation. Page 6-47

Display remains within graticule area when TRACE FINDER button is depressed regardless of the deflection factor or POSITION control settings.66. Check Chopped Operation.

Page 6-48
Chopped repetition rate, 500 kilohertz $\pm 20 \%$; time segment displayed from each channel, about one microsecond; switching transients blanked out.67. Adjust Calibrator Repetition Rate (T1255). Page 6-49 One kilohertz, $\pm 0.57 \%$.68. Check Calibrator Duty Cycle.

Page 6-50
$49 \%$ to $51 \%$.
69. Check Calibrator Risetime.

Page 6-50
One microsecond or less.
70. Check Curent Through Probe Loop.

Page 6-51
Five milliamperes.
71. Adjust $Z$ Axis Compensation (C1036).

Page 6-52
Optimum square comer on blanking pulse.72. Check Extemal Z Axis Operation. Page 6-53

Noticeable trace modulation with five-volt signal from DC to 50 megahertz.
73. Check A Gate Output Signal.

Paqe 6-53
Polarity, positive going; amplitude, 12 volts $\pm 10 \%$; duration, about 11 times the A TIME/DIV switch setting.74. Check B + Gate Output Signal.

Page 6-54
Polarity, positive going; amplitude, 12 volts, $\pm 10 \%$; duratiom about 11 times the B TME/DIV switch setting.

## CALIBRATION PROCEDURE

## General

The following procedure is a rranged in a sequence which allows the Type 453 to be calibrated with the least interaction of adjustments and reconnection of equipment. However, some adjustments affect the calibration of other circuits within the instrument. In this case, it will be necessary to check the operation of other parts of the instrument. When a step interacts with others, the steps which need to be checked are noted under "INTERACTION-. . .".

Any needed maintenance should be performed before proceeding with calibration. Troubles which become apparent during calibration should be corrected using the techniques given in the Maintenance section.

The steps titled "Adjust . . (1)" in the following procedure provide a check of instrument performance, whenever possible, before the adjustment is made. The symbol (1) is used to identify the steps in which an adjustment is made. To prevent recalibration of other circuits when performing a partial calibration, readiust only if the listed tolerance is not met. However, when performing a complete calibration, best overall performance will be provided if each adjustment is made to the exact setting, even if the "CHECK- . . ." is within the allowable tolerance.
in the following procedure, a test equipment setup picture is shown for each major group of adjustments and checks. Beneath each setup picture is a complete list of front-panel
control settings for the Type 453. To aid in locating individual controls which have been changed during complete calibration, these control names are printed in bold type. If only a partial calibration is performed, start with the nearest setup preceding the desired portion. Type 453 front-panel control titles referred to in this procedure are capita lized (e.g., HO RIZ DISPLAY). Intemal adjustment titles are initial capitalized only (e.g., Normal Gain).

The following procedure uses the equipment listed under Equipment Required. If equipment is substituted, control settings or test equipment setup may need to be altered to meet the requirements of the equipment used.

## N O TE

All wavefarms shown in this procedure are actual waveforms photographs taken with a Tektronix Oscilloscope Camera System unless otherwise noted. Graticule lines have been photographically retouched.

## Preliminary Procedure

1. Remove the top and bottom covers from the Type 453.
2. Connect the autotransformer to a suitable power source.
3. Connect the Type 453 to the autotransformer output.
4. Set the autotransformer output voltage to the center voltage of the range selected by the line Voltage Selelctor assembly on the rear panel.
5. Set the Type 453 POWER switch to ON (set INTENSTTY control fully counterclockwise). Allow at least 20 minutes warmup at $25^{\circ} \mathrm{C}, \pm 5^{\circ} \mathrm{C}$, for checking the instrument to the given accuracy.

NOTES


Fig. 6-3. Initial test equipment setup for steps 1 through 5.

CRT controls

| INTEN SITY | Counterclockwise |
| :--- | :--- |
| FOCUS | Midronge |
| SC ALE ILLUM | As desired |

Vertical controls [both chonnels if applicable)

| VOLTS/DIV | 20 mV |
| :--- | :--- |
| VARIABLE | CAL |
| POSITION | Midrange |
| Input Coupling | DC |
| MODE | CH 1 |
| TRIGGER | NORM |
| INVERT | Pushed in |

Triggering controls [both A and B if applicable)
LEVEL
Fully clockwise
SLOPE +

COUPLING
SO URCE

Sweep controls
DELAY-TIME MULTIPLIER
$A$ and B TIME/DIV
A VARIABLE
A SWEEP MODE
B SWEEP MODE

HORIZ DISPLAY

| MAG | OFF |
| :--- | :--- |
| A SWEEP LENGTH | FULL |
| POSITION | Midrange |
| POWER | O N |

Side-panel controls

| B TIME/DIV VARIABLE | CAL |
| :--- | :--- |
| CALIBRATOR | 1 V |

## 1. Adjust - 12-Volt Power Supply

a. Test equipment setup is shown in Fig. 6-3,
b, Connect the precision DC voltmeter from the -12 -volt test point (pin connector 'H', Low-Voltage Regulator board; see Fig. 6-4) to chassis ground.
c. CHECK-Meter reading; -12 volts, $\pm 0.02$ volt.
d. ADJ UST- -12 Volts adjustment, R1122 (see Fig, 6-4) for -12 volts.
e. INTERACTION-May affect operation of all circuits within the Type 453.
2. Adjust +12-Volt Power Supply
a. Connect the precision DC voltmeter from the center contact of the 1 kHz CAL connector to chassis ground.


Fig. 6-4. Low-valtage power supply test points and adjustments (Low-Voltage Regulator circuit board).
b. Remove Q1255 [see Fiq. 6-5) from the Calibrator section of the A Sweep circuit board.
c. CHECK-Meter reading; +1 volt, $\pm 0.002$ volt.
d. ADJ UST- +12 Volts adjustment, R1152 (see Fiq. 6-4), fora +1 volt meter reading.
e. Set the CALBRATOR switch (on side panel) to 1 V .
f. CHECK-Meter reading; +0.1 volt, $\pm 0.001$ volt.
g. Replace Q1255.
h. Connect the precision DC voltmeter from the +12 -volt test point (pin connector 'D', Low-Voltage Regulator board; se Fig. 6-4) to chassis ground.
i. CHECK-Meter reading; +12.1 volts, $\pm 0.12$ volt.
j. INTERACTION-May affect operation of all circuits within the Type 453.

## 3. Adjust +75 -Volt Power Supply

a. Connect the precision $D C$ voltmeter from the +75 -volt test point (pin connector 'B', Low-Voltage Regulator circuit board; see Fiq. 6-4) to chassis ground.
b. CHECK-Meter reading; +75 volts, $\pm 0.2$ volt
c. ADJ UST- +75 Volts adjustment, R1182 (see Fig. 6-4], for +75 volts.
d. Recheck all supplies and readjust if necessary.
e. INTERACTION-May affect operation of all circuits within the Type 453
f. Disconnect all test equipment.


Fig. 6-5. Location of Q1255 (Calibrator section of A Sweep circuit beard).


Fig. 6-6. Location of high-valtage adjustments and test points (bottom).

## 4. Adjust High-Voltage supply and Check Regulation

a. Connect the DC voltmeter (use the precision 2 kV divider) from the -1950 V test point (see Fig. 6-6) to chassis ground.
b. CHECK-Meter reading; -1950 volts, $\pm 20$ volts.
c. ADJUST-High-Voltage adjustment, R900 (see Fig. 6-6), for -1950 volts.
d. INTERACTION-May affect operation of all circuits within the Type 453.
e. CHECK-Change the autotransformer output voltage throughout the regulating range selected by the Line Voltage Selector assembly on the rear panel and check for less than $\pm 20$ volts change in the high-voltage output level. Also vary the INTENSITY control throughout its range at the maximum and minimum line voltage; check that regulation remains within given limits.

## NOTE

If the high-voltage supply is out of regulation, check the regulation of the low-voltage supplies
(step 6) before troubleshooting in the high-voltage supply.
f. Return the autotransformer output voltage to the center of the regulating range selected by the Line Voltage Selector assembly.

## 5. Adjust CRT Grid Bias

a. Connect the precision DC voltmeter from TP1047 (Z Axis Amplifier board; see Fig. 6-6] to chassis ground.
b. Set the A SWEEP MODE switch to SINGLE SWEEP.
c. Set the INTENSITY control for a meter reading of +12 volts.
d. ADJUST-CRT Grid Bias adjustment, R940 (se\& Fiq. 6-6), so the spot just disappears (it may be necessary to turn the horizontal POSITION control clockwise to bring the spot onto the viewing area).

## CAUTION

Do not allow a bright spot to remain stationary for an extended period, as it may burn the CRT phosphor.
e. INTERACTION-Check steps 65, 71 and 72.
f. Disconnect the precision DC voltmeter.


Fig. 6-7. Test equipment setup for steps $\mathbf{6}$ and 7 .

CRT controls

```
INTENSITY
FOCUS
SCALE ILLUM
```

Counterclockwise
Midrange
As desired
HORIZ DISPLAY
MAG
A SWEEP LENGTH
POSITION
POWER

A
OFF
FULL
Midrange
ON

Vertical controls (both channels if applicable)

| VOLTS/DIV | 20 mV |
| :--- | :--- |
| VARIABLE | CAL |
| POSITION | Midrange |
| Input Coupling | DC |
| MODE | CH 1 |
| TRIGGER | NORM |
| INVERT | Pushed in |

Triggering controls (both A and B if applicable)

| LEVEL | Fully clockwise |
| :--- | :--- |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | INT |

Sweep controls

| DELAY-TIME MULTPLIER | Fully counterclockwise |
| :--- | :--- |
| A and B TMME/DIV | 1 ms |
| A VARIABLE | CAL |
| A SWEEP MODE | NORM TRIG |
| B SWEEP MODE | TRIGGERABLE AFIER |
|  | DELAY TIME |

Side-panel controls

| B TMME/DIV VARIABLE | CAL |
| :--- | :--- |
| CALIBRATOR | .1 V |

## 6. Check Low-Voltage Power Supply Ripple

NOTE
This step also checks regulation of the low-voltage supplies.
a. Test equipment setup is shown in Fig. 6-7
b. Connect the $1 X$ probe to the test oscilloscope input.
c. Set the test oscilloscope for a vertical deflection of 0.005 volts/division, AC coupled, at a sweep rate of five milliseconds/division. Use line-frequency triggering to produce a stable display.
d. CHECK-Two millivolts ( 0.4 division) peak-to-peak maximum line frequency ripple on the -12 -volt, +12 -volt and +75 -volt supplies while changing the autotransformer output voltage throughout the regulating range selected by the Line


Fig. 6-8. Typical test oscilloscope display of power-supply sipple ( 60 -cycle line). Vertical 0.005 volt/division; sweep rate, five milliseconds/division.

Voltage Selector assembly on the rear panel. Power-supply test points are shown in Fiq. 6-4. Fiq. 6-8 shows a typical test oscilloscope display of ripple.
e. Return autotransformer output voltage to the center of the regulating range selected by the Line Voltage Selector assembly. (If the line voltage is near the center of the regulating range, the Type 453 may be connected directly to the line; otherwise, leave the instrument connected to the autotransformer for the remainder of this procedure.)
f. Disconnect all test equipment.

## 7. Adjust Trace Alignment

a. Set the A SWEEP MODE switch to AUTO TRIG.


Fig. 6-9. Location of TRACE ROTATION adjustment ( side panel).
b. Advance the INTENSITY control until the troce is visible.
c. Tum the Channel 1 POSITION control to move the trace to the center horizontal line.
d. Set the FOCUS control for as sharp a display as possible.
e. CHECK-The trace should be parallel with the center horizontal line.
f. ADJ UST-TRACE ROTATION adjustment, R980 (see Fig 6-9), so the trace is parallel to the horizontal graticule lines.

## NOTES



Fig. 6-10. Initial test equipment setup for steps 8 through 12.

| CRT controls |  |
| :--- | :--- |
| INTENSITY | Midrange |
| FOCUS | Adjust for focused dis- |
|  | play |
| SCALE ILLUM | As desired |

Vertical controls [both channels if applicable)

| VOLTS/DIV | 20 mV |
| :--- | :--- |
| VARIABLE | CAL |
| POSITION | Midrange |
| Input Coupling | DC |
| MODE | CH 1 |
| TRIGGER | NORM |
| INVERT | Pushed in |

Triggering controls (bath A and B if a pplicable)

| LEVEL | 0 |
| :--- | :--- |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | INT |

Sweep controls

| DELAY-TIME MULTIPLIER | Fully counterclockwise |
| :--- | :--- |
| A and B TIME/DIV | 1 ms |
| A VARIABLE | CAL |
| A SWEEP MODE | AUTO TRIG |
| B SWEEP MODE | TRIG GERABLE AFIER |
|  | DELAY TIME |



Fig. 6-11. Location of ASTIG adiustment (side panel)

## 9. Adjust $Y$ Axis Alignment

a. CHECK-The markers should be parallel to the center vertical line (se屯 Fig. 6-12A).
b. ADJ UST-Y Axis Align adjustment, R989 [see Fig. 6-12B), to align the markers with the center vertical line.

## 10. Adiust CRT Geometry

a. Set the horizontal POSITION and the A VARIABLE controls so a large marker coincides with each vertical graticule line.
b. CHECK-Bowing and tilt of markers at left and right edges of the graticule. Fig. 6-13 shows a typical display of good geometry as well as examples of poor geometry.
c. ADJ UST-Geometry adjustment, R982 (see Fig. 6-1BD), for minimum bowing of the trace at the left and right edges of the graticule.
d. INTERACTION-Recheck step 9.
e. Disconnect the time-mark generator.
f. Position the trace to the top of the graticule area.
g. CHECK-Deviation from straight line should not exceed 0.1 division.
h. Position the trace to the bottom of the graticule area.
i. CHECK-Deviation from straight line should not exceed 0.1 division.

## 11. Adjust Channel 1 and 2 Step Attenuator Balance

a. Position the trace to the center horizontal line with the Channel 1 POSITION control.


Fig. 6-12. (A) Typical CRT display showing correct Y-axis alignment, ( $B$ ) location of $Y$ Axis Align adjustment (left side).

```
b. Change the following control settings:
VOLTS/DIV
        (CH 1 and 2) }20\textrm{mV
        Input Coupling
        (CH 1 and 2)
        GND
```

c. CHECK-Change the CH 1 VOLTS/DIV switch from 20 mV to 5 mV . Trace should not move vertically.

## NOTE

Use the TRACE FINDER switch to locate the trace if it is deflected off screen when switching to 10 or 5 mV .
d. ADJUST-Channel 1 STEP ATTEN BAL adjustment, R30 (see Fig. 6-14), for no trace shift as the CH 1 VOLTS/DIV switch is changed from 20 mV to 5 mV .
e. Set the MODE switch to CH 2 .
f. Position the trace to the center horizontal line with the Channel 2 POSITION control.
g. CHECK-Change the CH 2 VOLTS/DIV switch from 20 mV to 5 mV . Trace should not move vertically.

$6-13$. (A) Typical CRT display showing good geometry; (B) and (C) poor geometry; (D) Location of Geometry adjustment (Z Axis Amplifier circuit board).
h. ADJUST-Channel 2 STEP ATIEN BAL adjustment, R130 (see Fig. 6-14), for no trace shift as the CH 2 VOLTS/DIV switch is changed from 20 mV to 5 mV .

## 12. Adjust Channel 1 and 2 Position Center

a. Connect the precision DC voltmeter between the Channel 2 position center test point (pin connector 'Z) on the Vertical Preamp board (se Fig. 6-15) and chassis ground.
b. Set the Channel 2 POSITION control for a meter reading of zero volts. (The dot on the POSTION control should be centered mechanically. If not, loosen the set screw and reposition the knob.)
c. CHECK-Trace should be at the center horizontal line.
d. ADJUST-CH 2 Position Center adjustment, R155 (see (Fig. 6-1\$), to position the trace to the center line.
e. Set the MODE switch to CH 1.
f. Connect the precision DC voltmeter between the Channel 1 position center test point ( p in connector ' $W$ ') on the Vertical Preamp board (se Fiq. 6-15) and chassis ground.
g. Set the Channel 1 POSTION control for a meter reading of zero volts. (The dot on the POSTION control should be centered mechanically. If not, loosen the set screw and reposition the knob.)
h. CHECK-Trace should be at the center horizontal line.
i. ADJ UST-CH 1 Position Center adjustment, R55 (see Fig. 6-15), to position the trace to the center line.
j. INTERACTION-Recheck step 11.
k. Disconnect all test equipment.


Fig. 6-1 4. Location of Channel 1 and 2 STEP ATTEN BAL adjustments (front panel).


Fig. 6-1 5. Location of Channel 1 and 2 position center test points and adjustments (Vertical Preamp circuit board).

NOTES


Fig. 6-16. Initial test equipment setup for steps 13 through 21.

CRT controls
INTENSITY
FOCUS
SCALE ILLUM
Vertical controls (both channels if applic able]

| VOLTS/ DIV | 20 mV |
| :--- | :--- |
| VARIABLE | CAL |
| POSITON | Midrange |
| Input Coupling | DC |
| MODE | CH 1 |
| TRIGGER | NORM |
| INVERT | Pushed in |

Triggering controls (both A and B if applicable)

| LEVEL | 0 |
| :--- | :--- |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | INT |

## Sweep controls

| DELAY-TME MULTIPLIER | Fully counterclockwise |
| :--- | :--- |
| A and B TIME/DIV | .5 ms |
| A VARIABLE | CAL |
| A SWEEP MODE | AUTO TRIG |
| B SWEEP MODE | TRIG GERABLE AFIER |
|  | DELAY TME |


| HORIZ DISPLAY | A |
| :--- | :--- |
| MAG | OFF |
| A SWEEP LENGTH | FULL |
| POSITON | Midrange |
| POWER | ON |

Side-panel controls

| B TMME/DN VARIABLE | CAL |
| :--- | :--- |
| CALIBRATOR | .1 V |

## 13. Adjust Channel 1 and 2 Gain

a. Test equipment setup is shown ir Fiq. 6-16
b. Connect the standard amplitude calibrator (067-0502-00) output connector to the Channel 1 and 2 INPUT connectors through a BNC Tconnector and two 42 -inch BNC cables.
c. Set the standard amplitude calibrator for a 0.1 -volt square-wave output.
d. Position the display to the center of the graticule with the Channel 1 POSITION control.
e. CHECK-CRT display exactly five divisions in amplitude (se Fig. 6-17A).
f. ADJ UST-Channel 1 GAIN adjustment, R90 (see Fig. $6-17 B]$, for exactly five divisions of deflection.
g. Set the MODE switch to ADD.


Fig. 6-17. (A) Typical CRT display showing correct gain adjustments; (B) location of Channel 1 and 2 GAI $N$ adjustments (front panel).
h. Pull the INVERT switch.
i. CHECK-CRT display for straight line.
j. ADJ UST-Channel 2 GAIN adjustment, R190 (see Fig $6-17 B)$, for straight line display.

## 14. Check Added Mode Operation

a. Push the INVERT switch in.
b. Set the standard amplitude calibrator for a 50-millivolt square-wave output.
c. CHECK-CRT display five divisions in amplitude.

## 15. Check Chanel 1 and 2 Deflection Accuracy

a. Set the MODE switch to CH 1.
b. Set the Channel 2 Input Coupling switch to GND.
c. CHECK-Using the CH 1 VOLTS/DIV switch and standard amplitude calibrator settings given in Table 6-1, check vertical deflection within $3 \%$ in each position of the CH 1 VOLTS/DIV switch.
d. Set the MODE switch to CH 2 .
e. Set the Channel 1 Input Coupling switch to GND and Channel 2 Input Coupling switch to DC.
f. CHECK-Using the CH 2 VOLTS/DIV switch and standard amplitude calibrator settings given in Table 6-1, check vertical deflection within $3 \%$ in each position of the CH 2 VOLTS/DIV switch.

TABLE 6-1

| VOLTS/DIV <br> Switch <br> Setting | Standard <br> Amplitude <br> Calibrator <br> Output | Vertical <br> Deflection <br> In Divisions | Maximum <br> Error for <br> $\pm \mathbf{~} \%$ <br> Accuracy <br> (divisions) |
| :---: | :---: | :---: | :---: |
| 5 mV | 20 millivolts | 4 | $\pm 0.12$ |
| 10 mV | 50 millivolts | 5 | $\pm 0.15$ |
| 20 mV | 0.1 volt | 5 | Previously <br> set in step 13 |
| 50 mV | 0.2 volt | 4 | $\pm 0.12$ |
| .1 | 0.5 volt | 5 | $\pm 0.15$ |
| .2 | 1 volt | 5 | $\pm 0.15$ |
| .5 | 2 volts | 4 | $\pm 0.12$ |
| 1 | 5 volts | 5 | $\pm 0.15$ |
| 2 | 10 volts | 5 | $\pm 0.15$ |
| 5 | 20 volts | 4 | $\pm 0.12$ |
| 10 | 50 volts | 5 | $\pm 0.15$ |

## 16. Check Channel 1 and 2 Variable Volts/ Division Range

a. Set the standard amplitude calibrator for a 0.1 -volt square-wave output.
b. Change the following control settings:

```
VOLTS/DIV
    (CH 1 and 2) }20\textrm{mV
Input Coupling
    (CH 1 and 2)
MODE
AC
CH }
```

c. CHECK-Turn the Channel 1 VARIABLE VOLTS/DIV control fully counterclockwise. Display should be reduced to two divisions or less (se Fiq. 6-1 8 ). Channel 1 UNCAL light must be on when Channel 1 VARIABLE control is not in CAL position.
d. Set the MODE switch to CH 2
e. CHECK-Turn the Channel 2 VARIABLE VOLTS/DIV control fully counterclockwise. Display should be reduced to two divisions or less (se Fiq. 6-18). Channel 2 UNCAL light must be on when Channel 2 VARIABLE control is not in CAL position.
f. Disconnect the cable from the Channel 2 INPUT connector.

## 17. Check Channel 1 and 2 Cascaded Deflection Factor

a. Connect the CH 1 OUT connector to the Channel 1 INPUT connector with the 18 -inch 50 -ohm BNC cable.


Fig. 6-1 8 . Typieal CRT display showing adequate Channel 1 and 2 VARIABLE centrol range (double exposure).
b. Change the following control settings:

| VOLTS/DIV |  |
| :--- | :--- |
| (CH 1 and 2) | 5 mV |
| VARIABLE (CH 1 and 2) |  |
| Input Coupling |  |
| (CH 1 and 2) |  |$\quad$ CAL

c. Set the standard amplitude calibrator for a five-millivolt square-wave output.
d. CHECK-CRT display five divisions or greater in amplitude (one millivolt/division, or less, minimum deflection factor).

## 18. Check Channel 1 and 2 Input Coupling

 Switch Operationa. Set the CH 1 and CH 2 VOLTS/DIV switches to 20 mV .
b. Disconnect the 18 -inch BNC cable from the Channel 2 INPUTconnector and reconnect the standard amplitude calibrator to the Chonnel 2 INPUT connector.
c. Set the standard amplitude calibrator for a 50 -millivolt square-wave output.
d. Position the display with the Channel 2 POSITION control so the bottom of the square wave is at the center horizontal line.
e. Set the Channel 2 Input Coupling switch to GND.
f. CHECK-CRT display for straight line near the center horizontal line.
g. Set the Channel 2 Input Coupling switch to AC.
h. CHECK-CRT display centered about center horizontal line.
i. Set the MODE switch to CH 1 .
j. Position the display with the Channel 1 POSITION control so the bottom of the square wave is at the center horizontal line.
k. Set the Channel 1 Input Coupling switch to GND.
I. CHECK-CRT display for straight line near the center horizontal line.
m . Set the Channel 1 Input Coupling switch to AC.
n. CHECK-CRT display centered about center horizontal line.
19. Check Low-Frequency Vertical Linearity
a. Set the Channel 1 and 2 Input Coupling switches to DC.
b. Position the display to the center of the graticule with the Channel 1 POSTION control.


Fig. 6-19. Typical CRT display showing acceptable compression and expansion. (A) Expansion, (B) correct deflection at center of graticule, (C) compression.
C. Adjust the Channel 1 VARIABLE control for exactly two divisions of deflection.
d. Position the top of the display to the top horizonal line.
e. CHECK-Compression or expansion 0.15 division or less (se Fig. 6-19).
f. Position the bottom of the display to the bottom horizonal line.
g. CHECK-Compression or expansion 0.15 division or less (se@ Fiq. 6-19).
h. Set the MODE switch to CH 2.
i. Position the display to the center of the graticule with the Channel 2 POSITION control.
j. Set the Channel 2 VARIABLE control for exactly two divisions of deflection.
k. Position the top of the display to the top horizontal line.
I. CHECK-Compression or expansion 0.15 division or less (see Fig. 6-19).
m. Position the bottom of the display to the bottom horizontal line.
n. CHECK-Compression or expansion 0.15 division or less (see Fig. 6-19].
o. Disconnect all test equipment.

## 20. Check Trace Shift Due to Input Gate Current

a. Change the following control settings:

| VOLTS/DIV |  |
| :--- | :--- |
| (CH 1 and 2) | 5 mV |
| VARIABLE (CH 1 and 2) | CAL |
| Input Coupling |  |
| (CH 1 and 2) GND |  |

b. Position the trace to the center horizontal line with the Channel 2 POSITION, control.
C. CHECK-Set the Channel 2 Input Coupling switch to DC. Trace shift should be negligible.
d. Set the MODE switch to CH 1.
e. Position the trace to the center horizontal line with the Channel 1 POSTION control.
f. CHECK-Set the Channel 1 Input Coupling switch to DC. Trace shift should be negligible.

## 21. Check Alternate, Operation

a. Set the MODE switch to ALT.
b. Position the traces about two divisions apart.
c. Tum the A TIME/DIV switch throughout its range.
d. CHECK-Trace altemation between Channel 1 and 2 at all sweep rates. At faster sweep rates, altemation is not apparent; instead display appears as two traces on the screen.

## NOTES



Fig. 6-20. Initial test equipment sefup for sfeps 22 through 24.

| CRT controls |  |
| :--- | :--- |
| INTENSITY | Midrange |
| FOCUS | Adjust for f |
| SCALE ILLUM | As desired |
|  |  |
| Vertical controls (both channels | if applicable) |
| VOLTS/DIV | $\mathbf{2 0 ~ m V}$ |
| VARIABLE | CAL |
| POSITION | Midrange |
| Input Coupling | DC |
| MODE | CH 1 |
| TRIGGER | NORM |
| INVERT | Pushed in |

Triggering controls (both $A$ and $B$ if applicable)

| LEVEL | Clockwise |
| :--- | :--- |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | INT |

Sweep controls

| DELAY-TIME MULTIPLIER | Fully counterclockwise |
| :--- | :--- |
| A and B TIME/DIV | .2 ms |
| A VARIABLE | CAL |
| A SWEEP MODE | AUTO TRIG |
| B SWEEP MODE | TRIGGERABLE AFTER |
|  | DELAY TIME |


| HORIZ DISPLAY | A |
| :--- | :--- |
| MAG | OFF |
| A SWEEP LENGTH | FULL |
| POSITION | Midrange |
| POWER | ON |

Side-panel controls

| B TIME/DIV VARIABLE | CAL |
| :--- | :--- |
| CALIBRATOR | .1 V |

22. Adjust Channel 1 and 2 Volts/ Division Switch Series Compensation
a. Test equipment setup is shown in Fig. 6-20
b. Connect the square-wave generator (Type 106) highamplitude output connector to the Channel 1 INPUT connector through the five-nanosecond GR cable, 5 X GR attenuator and 50 -ohm in-line termination in given order.
c. Set the square-wave generator for four divisions of onekilohertz signal.
d. Set the A LEVEL control for a stable display.
e. CHECK-CRT display at each CH 1 VOLTS/DIV switch setting listed in Table 6-2 for optimum square corner (see Fig 6-21A, B and C).


Fig. 6-21. (A) Typical CRT display showing correct compensation; (B) and (C) incorrect compensation; (D) location of variable capacitors (bottom view).
f. ADJUST-CH 1 VOLTS/DIV switch series compensation as given i Table 6-2 for optimum square comer on the display. Readjust the generator output with each setting of the CH 1 VOLTS/DIV switch (remove $5 X$ attenuator as required) to provide four divisions of deflection Fig. 6-2]D shows the location of the variable capacitors.
g. Disconnect the signal from the Channel 1 INPUT connector and reconnect it to the Channel 2 INPUT connector through the five-nanosecond GR cable, 5X GR attenuator and 50 -ohm in-line termination.
h. Set the MODE switch to CH 2.
i. CHECK-CRT display at each CH 2 VOLTS/DIV switch setting listed ir Table 6-2 for optimum square comer (see Fig 6-21A, B and C).

TABLE 6-2
Channel 1 and 2 VOLTS/DIV Series Compensation

| CH 1 <br> VOLTS/DIV <br> Switch Setting | Channel 1 <br> Series <br> Compensation | Channel 2 <br> Series <br> Compensation |
| :---: | :---: | :---: |
| 50 mV | C 6 C | $\mathrm{Cl06C}$ |
| .1 | $\mathrm{C7C}$ | $\mathrm{Cl07C}$ |
| .2 | C 8 C | Cl 08 C |
| 2 | C 9 C | $\mathrm{Cl09C}$ |

j. ADJUST-CH 2 VOLTS/DIV switch series compensation as given in Table 6-2 for optimum square corner on the display. Readjust the generator output with each setting of the CH 2 VOLTS/DIV switch (remove 5 X attenuator as required) to provide four divisions of deflection Fig. 6-2ll shows the location of the variable capacitors.
k. Disconnect the test equipment from the Channel 2 INPUT connectar.

## 23. Adjust Channel 1 and 2 Volts/ Division Shunt Compensation

a. Connect the square-wave generator high-amplitude output connector to the Channel 2 INPUT connector through the five-nanosecond GR cable, $5 X G R$ attenuator, 50-ohm in-line termination and 20 pF input $R C$ normalizer, in given order.
b. Set the CH 2 VOLTS/DIV switch to 20 mV .
c. Set the square-wave generator for four divisions of one-kilohertz signal.
d. CHECK-CRT display at each CH 2 VOLTS/DIV switch setting listed in Table 6-3 for optimum flat top (se Fig. 6-21A, $B$ and $C$ ).
e. ADJUST-CH 2 VOLTS/DIV switch shunt compensation as given in Table 6-3 for optimum flat top on the display.

Readjust the generator output with each setting of the CH 2 VOLTS/DIV switch [remove the 5X attenuator as required) to provide four divisions of deflection (only about three divisions obtainable in 2 position]. Fig. 6-21D shows the location of the variable capacitors.
f. Disconnect the signal from the Channel 2 INPUT connector and reconnect it to the Channel 1 INPUT connector through the five-nanosecond GR cable, 5X GR attenuator, 50 -ohm in-line termination and 20 pF input RC normalizer, in given order.
g. Set the MODE switch to CH 1.
h. CHECK-CRT display at each CH 1 VOLTS/DIV switch setting listed in Toble 6-3 for optimum square comer (see Fig. 6-21A, $B$ and C).
i. ADJUST-CH 1 VOLTS/DIV switch shunt compensation as given in Table 6-3 for optimum flat top on the display. Readjust the generator output with each setting of the CH 1 VOLTS/DIV switch (remove 5X attenuator as required) to provide four divisions of deflection (only about three divisions obtainable in 2 position). Fiq. 6-211 shows the location of the variable capacitors.
j. Disconnect all test equipment.

TABLE 6-3
Channel 2 VOLTS/DIV Shunt Compensation

| CH 2 <br> VOLTS/DIV <br> Switch Setting | Channel 1 <br> shunt <br> compensation | Channel 2 <br> shunt <br> compensation |
| :---: | :---: | :---: |
| 20 mV | C17 | C117 |
| 50 mV | C6B | C106B |
| .1 | C7B | C107B |
| .2 | C8B | C108B |
| .5 | Adiust C11 for <br> best compromise | Adjust C111 for <br> best compromise |
| 2 | C9B | C109B |

## 24. Adjust High-Frequency Compensation

## SELECTED COMPONENTS

The Vertical Preamp circuit board has four selected components which provide high-frequency compensation for various devices within the Vertical Deflection System. It should not be necessary to re-select these components unless the devices for which they compensate have been changed. Use Table 6-4 to select these components. If more than one component needs to be selected, select the components in the order given in this table. All of the selected components except R195 are mounted in sockets in the circuit board to facilitate selection. The locatian of each selected component is shown on Fig. 6-22 Table 6-4 lists the range of camponent values which provide correct compensation.

C38 and C138 are selected from among the following capacitors.

| $.001 \mu \mathrm{~F}$ | $283-0067-00$ | 200 V | $\pm 10 \%$ |
| :--- | :--- | :--- | :--- |
| .0015 | $283-0114-00$ | 200 V | $\pm 20 \%$ |
| .0022 | $283-0119-00$ | 200 V | $\pm 5 \%$ |
| .0027 | $283-0142-00$ | 200 V | $\pm 5 \%$ |
| .0033 | $283-0041-00$ | 500 V | $\pm 5 \%$ |
| .0047 | $283-0083-00$ | 500 V | $\pm 5 \%$ |
| .01 | $283-0079-00$ | 250 V | $\pm 20 \%$ |

C264 is selected from among the following capacitors.

| 14 pF | $281-0577-00$ | 500 V | $\pm 5 \%$ |
| :--- | :--- | :--- | :--- |
| 18 pF | $281-0578-00$ | 500 V | $+5 \%$ |
| 22 pF | $281-0511-00$ | 500 V | $\pm 2.2 \mathrm{pF}$ |
| 27 pF | $281-0512-00$ | 500 V | $\pm 2.7 \mathrm{pF}$ |
| 33 pF | $281-0629-00$ | 600 V | $+5 \%$ |
| 39 pF | $281-0603-00$ | 500 V | $\pm 5 \%$ |
| 47 pF | $281-0519-00$ | 500 V | $\pm 4.7 \mathrm{pF}$ |

TABLE 6-4

| Selected Component | Range of Values (to provide a 2 to $3 \%$ total compensating effect) | Device(s) for which this provides a compensating effect | Conditions for selecting ( $20 \mathrm{mV} / \mathrm{DIV}$, fourdivision 100 kHz, signal applied) | Selection procedure |
| :---: | :---: | :---: | :---: | :---: |
| 1. C38 | . 001 to .01 pF | Q23, Q33 | MODE CH 1 $10 \mu \mathrm{~S} / \mathrm{DIV}$ MAG OFF | Select for best flat top over first 2 to 5 microseconds |
| 2. C264 | 14 to 47 pF | Delay line | MODE CH 1 $2 \mu s / D I V$ MAG OFF | Select far best flat top over first 0.2 to 0.6 microsecond |
| 3. C138 | . 001 to $.01 \mu \mathrm{~F}$ | Q123, Q133 | MODE CH 2 $10 \mu \mathrm{~S} / \mathrm{DIV}$ MAG OFF | Select for best flat top over first 2 to 5 microseconds |
| 4. R195 | 24 k to 300 k , | Q84, Q94, Q184, Q194 | MODE CH 2 $2 \mu \mathrm{~s} / \mathrm{DIV}$ MAG OFF | Select for best match of Channel 2 to Channel 1 over first 0.5 mic rosecond |



Fig. 6-22. (A) Typical CRT display showing correct high-frequency compensation ( 0.5 microseconds/division) ; (B) typical CRT display showing correct high-frequency compensation ( 10 nanoseconds/division); (C) Jocation of high-frequency compensation adjustments and selected components (Vertical Preamp circuit board) ; (D) location of R328, C328 and C336 (Vertical Output Amplifier circuit board).
a. Change the following control settings:

| VOLTS/DIV(CH 1 and 2) | 20 mV |
| :--- | :--- |
| MODE | CH 1 |
| A and B TIME/DIV | $.5 \mu \mathrm{~s}$ |

b. Connect the square-wave generator fast-rise + output to the Channel 1 INPUT connector through the five-nanosecond GR cable, 5X GR attenuator and 50 -ohm in-line termination, in given order.
c. Set the square-wave generator for fast-rise operation and four-division display at 100 kilohertz.
d. CHECK-CRT display for optimum flat top (see Fig, 6-22A.
e. ADJUST-C263 and C265 (see Fig. 6-2 2 C ) for optimum flat top.
f. Change the following control settings:

$$
\begin{array}{ll}
\text { A and B TIME/DIV } & .2 \mu \mathrm{~s} \\
\text { MAG } & \times 10
\end{array}
$$

g. CHECK-CRT display for optimum square corner and flat top (see Fiq. 6-22B).
NOTE

In the following steps, change the MAG switch from X10 to OFF and compare the response at both sweep rates. Then adjust for the best overall response.
h. ADJUST-R49, C49, R328, C336, C328, C54 and C45A, in given order, (see Fig. 6-22C and D) for optimum square corner and flat top. Repeat this adjustment until optimum high-frequency response is obtained (similar to Fig. 6-2pB).

## i. Set the MODE switch to CH 2.

j. Disconnect the 50 -ohm in-line termination from the Channel 1 INPUT connector and connect it to the Channel 2 INPUT connector.
k. CHECK-CRT display for optimum square-wave response similar to Channel 1 response (se Fig. 6-22B).
I. ADJUST-R149, C149, C154 and C145A (see Fiq. 6-22C) for optimum square-wave response similar to Channel 1 response. Repeat this adjustment until optimum response is obtained.

## NOTE

If response of Channel 1 and 2 cannot be correctly matched using this adjustment procedure, see the procedure for reselecting R195 given in Table 6-4
m . Set the CH 2 VOLTS/DIV switch to 10 mV .
$n$. Set the square-wave generator for a four-division display.
o. CHECK-CRT display for optimum square-wave response (se Fig. 6-2ねB).
p. ADJUST-R144C, C144C and C144A, in given order, (see Fiq. 6-22C for optimum square-wave response. Repeat this adjustment until optimum response is obtained.
q. Set the CH 2 VOLTS/DIV switch to 5 mV .
r. Set the square-wave generator for a four-division display.
s. CHECK-CRT display for optimum square-wave response (se Fig. 6-2\$B).
t. ADJUST-R143C, C143C, C143A and L143A (see Fig. $6-22 C$ ) for optimum square-wave response. Repeat this adjustment until optimum response is obtained.
u. Change the following control settings:

```
MODE
    CH 1
CH 1 VOLTS/DIV 5 mV
```

v. Disconnect the 50 -ohm in-line termination from the Channel 2 INPUT connector and connect it to the Channel 1 INPUT connector.
w. CHECK-CRT display for optimum square-wave response (see Fia. 6-22 B).
x. ADJUST-R43C, C43C, C43A and L43A (see Fig. 6-2 ${ }^{\circ} \mathrm{C}$ ) for optimum square-wave response. Repeat this adjustment until optimum response is obtained.
y. Set the CH 1 VOLTS/DIV switch to 10 mV .
z. Set the square-wave generator for a four-division display.
aa. CHECK-CRT display for optimum square-wave response (see Fig. 6-22 B).
ab. ADJUST-R44C, C44C, and C44A (see Fiq. 6-2C) for optimum square-wave response. Repeat this adjustment until optimum response is obtained.
ac. Disconnect all test equipment.


Fig. 6-23. Inlfial test equipment setup for steps $\mathbf{2 5}$ through 27.

CRT controls
INTENSITY
FOCUS
SCALE ILLUM

Vertical controls (both channels if applicable)

| VOLTS/DIV | $\mathbf{2 0} \mathbf{~ m V}$ |
| :--- | :--- |
| VARIABLE | CAL |
| POSITION | Midrange |
| Input Coupling | DC |
| MODE | CH 1 |
| TRIGGER | NORM |
| INVERT | Pushed in |

Triggering controls (both A and B if applicable)
LEVEL
SLOPE
COUPLING
SOURCE

Sweep Controls

| DELAY-TIME MULTIPLIER | Fully counterclockwise |
| :--- | :--- |
| A and B TIME/DIV | $20 \mu$ s |
| A VARIABLE | CAL |
| A SWEEP MODE | AUTO TRIG |
| B SWEEP MODE | TRIG GERABLE AFIER |
| HORIZ DISPLAY | DELAY TIME |
| MAG | A |


| A SWEEP LENGTH | FULL |
| :--- | :--- |
| POSITION | Midrange |
| POWER | ON |

Side-panel controls

| B TIME/DIV VARIABLE | CAL |
| :--- | :--- |
| CALIBRATOR | .1 V |

## 25. Check Upper Vertical Bandwidth Limit of Channel 1 and 2

a. Test equipment setup is shown in Fia. 6-23
b. Connect the constant-amplitude sine-wave generator (Type 191) to the Channel 1 INPUT connector through the five-nanosecond GR cable, 5X GR attenuator and the 50ohm in-line termination.
c. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
d. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point; se Fiq. 6-24).
e. CHECK-Output frequency of generator must be 50 megahertz or higher.
f. Set the CH 1 VOLTS/DIV switch to 10 mV .
g. Set the constant-amplitude generator for a four division display at its reference frequency ( 50 kHz ).


Fig. 6-24. Typical CRT display when checking vertical bandwidth (simulated waveform).
h. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point; se Fig. 6-24).
i. CHECK-Output frequency of generator must be 45 megahertz or higher.
j. Set the CH 1 VOLTS/DIV switch to 5 mV .
k. Set the constant-amplitude generator for a four division display at its reference frequency ( 50 kHz ).
l. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point; se Fiq. 6-24).
m. CHECK-Output frequency of generator must be 40 megahertz or higher.
n. Set the MODE switch to CH 2.
o. Disconnect the output of the in-line termination from the Channel 1 INPUT connector and connect it to the Channel 2 INPUT connector.
p. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
q. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions (-3 dB point; see Fig. 6-24).
r. CHECK-Output frequency of generator must be 50 megahertz or higher.
s. Set the CH 2 VOLTS/DIV switch to 10 mV .
t. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
u. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point; se Fig. 6-24).
v. CHECK-Output frequency of generator must be 45 megahertz or higher.
w. Set the CH 2 VOLTS/DIV switch to 5 mV .
$x$. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
y. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions (-3 dB point; se $e$ Fiq. 6-24).
z. CHECK-Output frequency of generator must be 40 megahertz or higher.

## 26. Check Added Mode Upper Bandwith Limit

a. Change the following control settings:

| VOLTS/DIV (CH 1 and 2) | 20 mV |
| :--- | :--- |
| CH 1 POSITION | Midrange |
| CH 1 Input Coupling | GND |
| MODE | ADD |

b. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
c. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point; se Fiq. 6-24).
d. CHECK-Output frequency of generator must be 50 megahertz or higher.
e. Change the following control settings:

| CH 2 POSITION | Midrange |
| :--- | :--- |
| Ch 1 Input Coupling | DC |
| CH 2 Input Coupling | GND |

f. Disconnect the output of the in-line temmination from the Channel 2 INPUT connector and connect it to the Channel 1 INPUT connector.
g. Set the constant-amplitude generator for a four division display at its reference frequency ( 50 kHz ).
h. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point; se Fig. 6-24).
i. CHECK-Output frequency of generatar must be 50 megahertz or higher.

## 27. Check Channel 1 and 2 Cascaded Upper Bandwidth limit

o. Connect the CH 1 OUT connector to the Channel 2 INPUT connector with an 18-inch, 50-ohm BNC cable.
b. Change the following control settings:

| VOLTS/DIV | 5 mV |
| :--- | :--- |
| MODE | CH 2 |

c. Set the constant-amplitude generator for a four-division display at its reference frequency ( 50 kHz ).
d. Without changing the output amplitude, increase the output frequency of the generator until the deflection is reduced to 2.8 divisions ( -3 dB point; se Fig. 6-24).
e. CHECK-Output frequency of generator must be 25 megahertz or higher.
f. Disconnect the cable from between the CH 1 OUT and Channel 2 INPUT connectors.


Fig. 6-25. Test equipment setup for steps $\mathbf{2 8}$ and 29.

## CRT c ontrols

| INTENSITY | Midrange |
| :--- | :--- |
| FOCUS | Adjust for focused display |
| SCALE ILLUM | As desired |

Vertical controls (both channels if applic able)

| VOLTS/ DIV | 50 mV |
| :--- | :--- |
| VARIABLE | CAL |
| POSITION | Midrange |
| Input Coupling | DC |
| MODE | CH 1 |
| TRIGGER | NORM |
| INVERT | Pushed in |

Triggering controls (both A and B if applicable)

| LEVEL | Any position |
| :--- | :--- |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | INT |

Sweep controls

| DELAY-TME MULTIPLIER | Fully counterclockwise |
| :--- | :--- |
| A and B TME/DIV | .1 ms |
| A VARIABLE | CAL |
| A SWEEP MODE | AUTO TRIG |
| B SWEEP MODE | TRIGGERABLE AFTER |
| HORIZ DISPLAY | AELAY TME |


| MAG | OFF |
| :--- | :--- |
| A SWEEP LENGTH | FULL |
| POSITON | Midrange |
| POWER | ON |

Side-panel controls

| B TME/DIV VARIABLE | CAL |
| :--- | :--- |
| CALBRATOR | .1 V |

28. Check Common-Mode Rejection Ratio
a. Test equipment setup is shown ir Fig. 6-25
b. Connect the constant-amplitude generator to the Channel 1 and 2 INPUT connectors through the five-nanosecond GR cable, 50 -ohm in-line temination and the dual-input coupler.
c. Set the constant-amplitude generator for a 3.2-division display at 20 megahertz.
d. Change the following control settings:

| VOLTS/DIV (CH 1 and 2) | 20 mV |
| :--- | :--- |
| MODE | ADD |
| INVERT | Pulled out |

e. CHECK-CRT display for 0.4 division deflection, or less (common-mode rejection ratio 20:1 or better see Fig. 6-26).


Fig. 6-26. Typleal CRT display when checking common-mode rejection ratio.

NOTE
This check applies anly when the Channel 1 and 2 gain is correctly adjusted as given in step 13. If the common-mode rejection ratio is lower than 20:1, check and readjust the gain. Then recheck this step. (Transistors Q43, Q54, Q143, Q154 have the largest effect on common-mode rejection ratio.)
f. Disconnect the dual-input coupler.

## 29. Check Attenuator Isolation Ratio

a. Change the following control settings:

| CH 1 VOLTS/DIV | 1 |
| :--- | :--- |
| CH 2 VOLTS/DIV | 5 mV |
| CH 2 Input Coupling | GND |
| MODE | CH 1 |
| INVERT | Pushed in |

b. Connect the constant-amplitude generator to the Channel 1 INPUT connector through the five-nanosecond GR cable and the 50 -ohm in-line termination.
c. Set the constant-amplitude generator for a five-division


Fig. 6-27. Typleal CRT display when checking attenuator isolation rafie.
display at 20 megahert (use the variable control of the generator, if necessary, to obtain a five-division display).
d. Set the MODE switch to CH 2.
e. CHECK-CRT display for 0.1-division deflection, or less (attenuator isolation ratio 10,000:1 or better, see Fig. 6-27).
f. Change the following control settings:

| CH | 1 | VOLTS/DIV |
| :--- | :--- | :--- |
| CH | 2 VOLTS/DIV | 1 |
| CH | 1 Input Coupling | GND |
| CH 2 Input Caupling | DC |  |

g. Connect the constant-amplitude generator to the Channel 2 INPUT connector through the five-nanosecond GR cable and the 50 -ohm in-line termination.
h. Set the constant-amplitude generator for a five-division display at 20 megahert (use the variable control of the generator, if necessary, to obtain a five-division display).
i. Set the MODE switch to CH 1 .
j. CHECK-CRT display far 0.1-division deflection or less (attenuator isolation 10,000:1 or better; see Fig. 6-27).
k. Disconnect all test equipment.

NOTES


Fig. 6-28. Initial test equipment setup for steps 30 through 40.

CRT controls
INTENSITY FOCUS SCALE ILLUM

Midrange
Adjust for focused display
As desired

Vertical controls (both channels if applicable)

| VOLTS/DIV | 50 mV |
| :--- | :--- |
| VARIABLE | CAL |
| POSITION | Midrange |
| Input Coupling | DC |
| MODE | CH 1 |
| TRIGGER | NORM |
| INVERT | Pushed in |

Triggering controls (both A and B if applicable]

| LEVEL |  | 0 |
| :--- | :--- | :--- |
| SLOPE |  | + |
| COUPLNG |  | AC |
| SOURCE |  | INT |

Sweep controls

| DELAY-TME MULTIPLIER | Fully counterclockwise |
| :--- | :--- |
| A and B TME/DIV | 20 HS |
| A VARIABLE | CAL |
| A SWEEP MODE | NORM TRIG |
| B SWEEP MODE | TRIGGERABLE AFIER |
|  | DELAY TIME |
| HORIZ DISPLAY | A |


| MAG | OFF |
| :--- | :--- |
| A SWEEP LENGTH | FULL |
| POSITON | Midrange |
| POWER | O N |

Side-panel controls

| B TMME/DIV VARIABLE | CAL |
| :--- | :--- |
| CALBRATOR | .1 V |

30. Adjust $A$ and $B$ Trigger Level Centering
a. Test equipment setup is shown in Fig. 6-28
b. Connect the constant-amplitude generator to the A EXT TRIG INPUT connector through the five-nanosecond GR cable, GR to BNC adapter and BNC Tconnector. Connect the output of the BNC Tconnector to the Channel 1 INPUT connector through an 18 -inch 50 -ohm BNC cable and a $50-$ ohm BNC termination.
c. Set the constant-amplitude generator for a 0.2 -division display at 50 kilohertz (if necessary, use AUTO TRIG position to obtain 0.2-division display).
d. Be sure the $A$ LEVEL control is set to 0 .
e. CHECK-Stable CRT display (se Fiq. 6-29A).
f. ADJ UST-A Trigger Level Center adjustment, R462 (see Fiq. 6-29B), for a stable display.


6-2 9. (A) Typical CRT display when checkina trigaar level centering, (B) location of the A Trigger Level Center adjustment (A Sweep circuit board), (C) location of B Trigger Level Center edjushments of (B Sweep circuit board).
g. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
h. Be sure the $B$ LEVEL control is set to 0 .
i. CHECK-Stable CRT display (se Fiq. 6-29A).
i. ADJ UST-B Trigger Level Center adjustment, R662 (see Fiq. 6-29(), for a stable display.

## 31. Adjust Channel 1 Trigger DC Level and Normal Trigger DC Level

a. Change the following control settings:


Fig. 6-30. Location of Channel 1 Trigger and Normal Trigger DC level (Vertical Preamp circuit board).

TRIG G ER
A COUPLING
A SWEEP MODE HORIZ DISPLAY

CH 1 ONLY
DC
AUTO TRIG
A
b. Move the trace to the center horizontal line with the CH 1 POSITION control.
C. CHECK-Stable CRT display. CH 1 light in both $A$ and $B$ Triggering must be on.
d. ADJUST-Channel 1 Trigger DC Level adjustment, R60 (see Fiq. 6-30), for a stable display.
e. CHECK-Stable CRT display.
f. ADJ UST-Normal Trigger DC Level adjustment, R285 (see Fig. 6-30), for a stable display.

## 32. Check A and B Internal Triggering Operation

a. Set the constant-amplitude generator for a 0.2-division display at 10 megahertz (use AUTO TRIG position, if neces sary, to obtain display).
b. Set the $A$ and $B$ TMME/DIV switch to $.1 \mu \mathrm{~s}$.
c. CHECK-Stable CRT display (see Fig. 6-31A) can be obtained with the A COUPUNG switch set to AC, LF REJ and DC (A LEVEL control may be adjusted as necessary to obtain stable display). The A SWEEP TRIG'D light must be on when the display is stable.
d. Set the constant-amplitude generator for a one-division display at 50 megahertz.
e. Set the MAG switch to X10.
f. CHECK-Stable CRT display (see Fig. 6-31.B) can be obtained with the A COUPUNG switch set to AC, LF REJ and DC (A LEVEL and HF STAB controls may be adjusted as necessary to obtain stable display). Display jitter should not exceed 0.1 division (one na nosecond).
g. Change the following control settings:
A LEVEL
Set for stable A display
HORIZ DISPLAY
DELAYED SWEEP (B)


Fig. 6-31. : A) Typical CRT display when checking internal 10 megahertz triggering, (B) typical CRT display when checking internal 50 megahertz triggering.
h. Set the constant-amplitude generator for one-division display at 50 megahertz (as set in part $d$ above).
i. CHECK-Stable CRT display (see Fig. 6-31B) can be obtained with the B COUPLING switch set to AC, LF REJ and DC ( $B$ LEVEL control may be adjusted as necessary to obtain stable display).
j. Set the constant-amplitude generator for a 0.2-division display at 10 megahertz.
k. Set the MAG switch to OFF.
I. CHECK-Stable CRT display (see Fig. 6-31A) can be obtained with the B COUPLNG switch set to AC, LF REJ and DC (B LEVEL control may be adjusted as necessary to obtain a stable display).

## 33. Check A and B External Triggering Operation

a. Change the following control settings:

| SOURCE (A and B) | EXT |
| :--- | :--- |
| HORIZ DISPLAY | A |
| MAG | OFF |

b. Set the constant-amplitude generator for a one-division display ( 50 millivolts) at 10 megahertz.
c. CHECK-Stable CRT display (see Fig. 6-32A) can be obtained with the A COUPLING switch set to AC, LF REJ and DC (A LEVEL control may be adjusted as necessary to obtain stable display).


Fig. 6-32. (A) Typical CRT display when checking external 10 megahertz triggering, (B) typical CRT display when checking external 50 megahertz triggering.
d. Set the MAG switch to X10.
e. Set the constant-amplitude generator for a 2.8-division display at 50 megahertz (2.8-division display takes into occount typical rolloff in vertical response at 50 mHz ).
f. CHECK-Stable CRT display (see Fig. 6-32B) can be obtained with the A COUPLING switch set to AC, LF REJ and DC (A LEVEL and HF STAB controls may be adjusted as necessary to obtain stable display).
g. Disconnect the constant-amplitude generator signal from the A EXT TRIG INPUT connector and reconnect it to the B EXT TRIG INPUT connector.
h. Change the following control settings:
A SOURCE
INT
A LEVEL
HORIZ DISPLAY
Set for stable A display DELAYED SWEEP (B)
i. CHECK-Stable CRT display (see Fia. 6-32B) can be obtained with the B COUPLING switch set to AC, LF REJ and DC (B LEVEL control may be adjusted as necessary to obtain stable display).
j. Set the MAG switch to OFF.
k. Set the constant-amplitude generator for a one-division display at 10 megahertz.
I. CHECK-Stable CRT display (see Fig. 6-32A) can be obtained with the $B$ COUPLING switch set to AC, LF REJ and DC (B LEVEL control may be adjusted as necessary to obtain stable display).
m. Disconnect all test equipment.

## 34. Check A and B Low-Frequency Triggering Operation

a. Connect the low-frequency constant-amplitude generator to the A EXT TRIG INPUT connector through a 50 -ohm BNC cable and the BNC Tconnector. Connect the output of the BNC Tconnector to the Channel 1 INPUT connector through an 18 -inch 50 -ohm BNC cable and a 50 -ohm BNC termination.
b. Change the following control settings:
$A$ and $B$ TIME/DIV
5 ms
HORIZ DISPLAY
A
c. Set the low-frequency generator for a 0.2-division display at 60 hertz.
d. CHECK-Stable CRT display (see Fiq. 6-33A) can be obtained with the A COUPUNG switch set to AC, HF REJ and DC (A LEVEL control may be adjusted as necessary to obtain stable display).
e. Set the A and B SOURCE switches to EXT.
f. Set the low-frequency generatar far a one-division display at 60 hertz ( 50 millivolts).
g. CHECK-Stable CRT display (see Fig. 6-33B) can be obtained with the A COUPUNG switch set to AC, HF REJ and DC (A LEVEL control may be adjusted as necessary to obtain stable display).
h. Change the following control settings:

> A SOURCE

INT


Fig. 6-3 3. (A) Typical CRT display when checking internal lowrequency triggering af 60 hertz, (B) typical CRT display when hacking external low-frequency triggering at 60 hertz.

A LEVEL HORIZ DISPLAY
i. Disconnect the low-frequency generator from the A EXT TRIG INPUT connector and reconnect it to the B EXT TRIG INPUT connector.
j. CHECK-Stable CRT display (see Fig. 6-33B) can be obtained with the B COUPUNG switch set to AC, HF REJ and DC (B LEVEL control may be adjusted as necessary to obta in stable display).
k. Set the B SOURCE switch to INT.
I. Set the low-frequency generator for a 0.2 -division display at 60 hertz.
m. CHECK-Stable CRT display (see Fiq. 6-33A) can be obtained with the B COUPUNG switch set to AC, HF REJ and DC (B LEVEL control may be adjusted as necessary to obtain stable display).

## 35. Check A and B High-Frequency Reject Operation

a. Change the following control settings:

| COUPLNG (A and B) | HF REJ |
| :--- | :--- |
| A and B TMME/DIV | $20 \mu \mathrm{~s}$ |
| A SWEEP MODE | AUTO TRIG |

b. Set the low-frequency constant-amplitude generator for a 0.2 -division display at 50 kilohertz.
c. CHECK-Stable CRT display (see Fig. 6-34 can be obtained with the B LEVEL control.
d. Without changing the output amplitude, set the lowfrequency generatar to one megahertz.
e. Set the MAG switch to X10.
f. CHECK-Stable display cannot be obtained at any setting of the $B$ LEVEL control.


Fig. 6-34. Typical CRT display when checking high-frequency reject operation at 50 kilohertz.
g. Change the following control settings:

| A SWEEP MODE | NORM TRIG |
| :--- | :--- |
| HORIZ DISPLAY | A |
| MAG | OFF |

h. Set the low-frequency generator for a 0.2-division display at 50 kilohertz.
i. CHECK-Stable CRT display (see Fig. 6-34) can be obtained with the A LEVEL control.
j. Without changing the output amplitude, set the con-stant-amplitude generator to one megahertz.
k. Set the MAG switch to X 10 .
I. CHECK-Stable display cannot be obtained at any setting of the A LEVEL control.

## 36. Check A and B Low-Frequency Reiect Operation

a. Set the low-frequency generator for a 0.2-division display at 30 kilohertz.
b. Change the following control settings:

| COUPLING (A and B) | LF REJ |
| :--- | :--- |
| $A$ and $B$ TME/DIV | .1 ms |

c. CHECK-Stable CRT display (see Fig. 6-35 can be obtained with the A LEVEL control.
d. Without changing the output amplitude, set the lowfrequency generator to 60 hertz.
e. Set the $A$ and $B$ TME/DIV switch to 2 ms .
f. CHECK-Stable CRT display cannot be obtained at any setting of the A LEVEL control.
g. Change the following control settings:

| A and B TME/DIV | .1 ms |
| :--- | :--- |
| A SWEEP MODE | AUTO TRIG |
| HO RIZ DISPLAY | DELAYED SWEEP [B) |

h. Set the low-frequency generator for a 0.2-divisian display at 30 kilohertz (as set in part a of this step).
i. CHECK-Stable CRT display (see Fiq. 6-35 can be obtained with the B LEVEL control.
j. Without changing the output amplitude, set the lowfrequency generatar to 60 hertz.
k. Set the $A$ and $B$ TIME/DIV switch to 2 ms .
I. CHECK-Stable CRT display cannot be obtained at any setting of the $B$ LEVEL control.

## 37. Check Single Sweep Operation

a. Change the following control settings:

| COUPLING (A and B) | $A C$ |
| :--- | :--- |
| $A$ and B TME/DIV | 5 ms |
| HO RIZ DISPLAY | $A$ |

b. Set the low-frequency generator for a five-division display at one kilohertz.


Fig. 6-35. Typical CRT display when checking low-frequency reiect operation at 30 kilohertz.
c. Set the A LEVEL control fully clockwise.
d. Set the A SWEEP MODE switch to SINGLE SWEEP.
e. Push the RESET button.
f. CHECK-RESET light must come on when button is pressed and remain on until sweep is triggered.
g. Slowly rotate the A LEVEL control counterclockwise.
h. CHECK-A single-sweep display (one sweep only) is presented when the $A$ LEVEL control is in the triggerable region. RESET light must go off at the end of the sweep and remain off until the RESET button is pressed again.

## 38. Check A and B Slope Switch Operation

a. Change the following control settings:
A LEVEL
0
A SWEEP MODE
NORM TRIG
b. Set the low-frequency generator for a four-division display at one kilohertz.
c. CHECK-CRT display starts on the positive slope of the waveform (se€ Fiq. 6-36A].
d. Set the A SLOPE switch to -.
e. CHECK-CRT display starts on the negative slope of the waveform (se Fiq. 6-36B).
f. Set the A SWEEP MODE switch to AUTO TRIG.
g. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
h. CHECK-CRT display starts on the positive slope of the waveform (se Fig. 6-36A).
i. Set the B SLOPE switch to -.
j. CHECK-CRT display starts on the negative slope of the waveform (se Fid. 6-36B).
k. Disconnect all test equipment.


Fig. 6-36. Typical CRT display when ehecking slope switch operstien. (A) SLOPE switch set to + , (B) SLOPE switth sel to -.

## 39. Check $A$ and $B$ Level Control Range

a. Connect the law-frdquency generator to the B EXT TRIG INPUT connector through a 42-inch BNC cable and the BNC T connector. Connect the output of the BNC T connector to the Channel 1 INPUT connector through an 18inch BNC cable.
b. Change the following control settings:

```
Cl-f 1 VOLTS/DIV
COUPLING (A and B) DC
LEVEL (A and B)
B SOURCE EXT
1
```

c. Set the low-frequency generator for a four-division display [four volts peak to peak) at one kilohertz.
d. CHECK-Rotate the B LEVEL control throughout its range and check that display can be triggered (stable display) at any point along the negative slope of the waveform (indicates B LEVEL cantrol range of at least + and - twa vabs). Display is not triggered at either extreme of ratation.
e. Set the B SLOPE switch to +.
f. CI-IECK-Rotate the B LEVEL control throughout its range and check that display can be triggered at any point along the positive slope of the waveform. Display is not triggered at either extreme of rotation.
g. Set the CH 1 VOLTS/DIV switch to 10.
h. Set the B SOURCE switch to EXT + 10.
i. Set the low-frequency generator for a four-division display (40 volts peak to peak) at one kilohertz.
j. CHECK-Rotate the B LEVEL control throughout its range and check that display can be triggered at any point along the positive slope of the waveform (indicates B LEVEL control range of at least + and -20 volts). Display is not triggered at either extreme of rotation.
k. Set the B SLOPE switch to -.
I. CHECK-Rotate the B LEVEL control throughout its range and check that display can be triggered at any point along the negative slope of the waveform. Display is not triggered at either extreme of rotation.
m. Change the following central settings:
A SOURCE
EXT $\div 10$
A SWEEP MODE HORIZ DISPLAY
NORM TRIG
A
n. Disconnect the low-frequency generator from the $B$ EXT TRIG INPUT connector and reconnect it to the A EXT TRIG INPUT connector.
a. CHECK-Rotate the A LEVEL control throughout its range and check that display can be triggered at any point along the negative slope af the waveform (indicates A LEVEL control range af at least + and - 20 volts). Display is not triggered at either extreme of rotation.
p. Set the A SLOPE switch to +.
q. CHECK-Rotate the A LEVEL control throughout its range and check that display can be triggered at any point along the positive slope of the waveform. Display is not triggered at either extreme of rotation.
r. Change the following control settings:

```
CH 1 VOLTS/DIV
A SOURCE
1
EXT
```

s. Set the low-frequency generator for a four-division display (four volts peak to peak) at one kilohertz.
t. CHECK-Rotate the A LEVEL control throughout its range and check that display can be triggered at any point along the positive slope of the waveform (indicates A LEVEL control range of at least + and - two volts). Display is not triggered at either extreme of rotation.
u. Set the A SLOPE switch to -.
v. CHECK-Rotate the A LEVEL control throughout its range and check that display can be triggered at any point along the negative slope of the waveform. Display is not triggered at either extreme of rotation.
w. Disconnect all test equipment.

## 40. Check $A$ and $B$ line Triggering Operation

a. Connect the 10X probe to the Channel 1 INPUT connector.
b. Change the following control settings:

| CH 1 VOLTS/DIV | 10 |
| :--- | :--- |
| SOURCE (A and B) | LINE |
| A and B TIME/DIV | 2 ms |

c. Connect the probe tip to the same line-voltage source which is connected to this instrument.
d. CHECK-Stable CRT display triggered on the correct slope.
e. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
f. CHECK-Stable CRT display triggered on the correct slope.
g. Disconnect all test equipment.


Fig. 6-37. Initial test equipment setup for steps 41 through 60

| CRT controls |  | COUPLING | AC |
| :---: | :---: | :---: | :---: |
|  |  | SOURCE | INT |
| INTENSITY | Midrange |  |  |
| FOCUS | Adjust far focused display | Sweep controls |  |
| SCALE ILLUM | As desired |  |  |
|  |  | DELAY-TIME MULTIPLIER | Fully counterclockwise |
| Vertical controls (both channels if applicable) |  | $A$ and $B$ TME/DIV A VARIABLE | $50 \mu \mathrm{~s}$ CAL |
| VOLTS/DIV | . 2 | A SWEEP MODE | AUTO TRIG |
| VARIABLE | CAL | B SWEEP MODE | B STARTS AFTER |
| POSITIO | Midrange | HORIZ DISPLAY | ME |
| Input Coupling | DC | MAG |  |
| MODE | CH 1 |  |  |
| TRIG GER | NORM | A SWEEP LENGTH | Midrange |
| INVERT | Pushed in | POWER | ON |
| Triggering controls (both A and | B if applicable) | Side-panel controls |  |
| LEVEL | Stable display | B TIME/DIV VARIABLE | CAL |
| SLOPE | + | CALIBRATOR | . 1 V |

41. Check Auto Recovery Time and Operation
a. Test equipment setup is shown in Fig. 6-37
b. Connect the time-mark generator to the Channel 1 INPUT connector through the 42 -inch 50 -ohm BNC cable and 50 -ohm BNC termination.
c. Set the time-mark generator for 50-millisecond markers.

## CAUTION

To prevent permanent damage to the CRT phosphor at slow sweep rates, position the baseline of the marker display below the viewing area.
d. CHECK-Stable display can be obtained with the A LEVEL control. Marker must be at the start af the sweep.
e. Set the time-mark generator for 0.1-second markers.
f. CHECK-Sweep free runs and stable display cannot be obtained. If stable display is obtained, marker must not be at the start of the sweep.
42. Adjust Sweep Start and A Sweep

Calibration
a. Change the following control settings:

| A TME/DIV | 1 ms |
| :--- | :--- |
| B TMME/DIV | $5 \mu \mathrm{~s}$ |
| HORIZ DISPLAY | A INTEN DURING B |

b. Tum the DELAY-TIME MULTIPLIER dial fully counterclockwise.
c. CHECK-DELAY-TIME MULTIPLIER dial setting 0.20 .
d. ADJUST-If the DELAY-TMME MULTPLIER dial is not correctly positioned when fully counterclockwise, loosen the set screw and reposition the dial to 0.20 .
e. Repeat parts b through d until the DELAY-TIME Multiplier dial is correctly positioned at 0.20 .
f. Set the time-mark generator for one-millisecond markers.
g. Set the DELAY-TIME MULTIPUER dial to 1.00 .
h. CHECK-Intensified portion of display starts at secand marker (se Fig. 6-38A).
i. ADJ UST-Sweep Start adjustment, R758 (se屯 Fig. 6-38C), so intensified portion starts at second marker (preliminary adjustment).
j. Set DELAY-TMME MULTIPLIER dial to 9.00.
k. CHECK-Intensified portion of display starts at tenth marker (se Fig. 6-38B).


Fig. 6-38. (A) Typical CRT display showing intensified portion correctly located at the second marker, (E) typical CRT display showing intensified portion correctly located at the tenth marker, (C) location of Sweep Start and A Sweep Cal adjustments (B Sweep board), (D) trpical CRT display showing correct final adjustment of Sweep Start and A Sweep Cal dajustments.

1. ADJ UST-A Sweep Cal adjustment, R531 Isee Fig. 6 . 38C), so intensified portion starts at tenth marker (preliminary adjustment].
$m$. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
$n$. Set the DELAY-TIME MULTIPLER dial to 1.00 .
o. CHECK-Displayed pulse starts at the beginning of the sweep (se Fig. 6-38 D).
p. ADJ UST-Sweep Start adjustment, R758 (se Fig. 6-3\$C), so displayed pulse starts at the beginning of the sweep.
q. Set DELAY-TMME MULTIPLER dial to 9.00.
r. CHECK-Displayed pulse starts at the beginning of the sweep (see Fig. 6-38D).
s. ADJUST-A Sweep Cal adjustment, R531 (see Fig. 6-38C), so displayed pulse starts at the beginning of the sweep.
t. Recheck parts $n$ through $s$ and readjust if necessary.
2. Adjust Normal Gain
a. Set the HORIZ DISPLAY switch to A.


Fig. 6-39. (A) Typical CRT display showing correct normal gain; (B) location of Normal Gain adjustment (B Sweep circuit board).
b. CHECK-CRT display for one marker each division between the first-and ninth-division vertical lines (see fig. 6-39A).

## NOTE

Unless otherwise noted, use the middle eight horizontal divisions when checking or adjusting timing.
c. ADJ UST-Normal Gain adjustment, R835 (see Fig. 639B), for one marker each division. The second and tenth markers must coincide exactly with their respective graticule lines (repositian the display slightly with the horizontal POSITION control if necessary).
d. iNTERACTION-Check steps 44-59.
44. Adjust Magnified Gain
a. Set the time-mark generator for 0.1 millisec ond markers.
b. Set the MAG switch to X10.
c. CHECK-CRT display for one marker each division between the first and ninth graticule lines (se Fig. 6-40A).


Fig. 6-40. (A) Typical CRT display showing correct magnified gain; (B) location of Mag Gain adjustment (B Sweep circuit board).
d. ADJ UST-Mag Gain adjustment, R845 (se Fig. 6-40B), for one marker each division. The second and tenth markers must coincide exactly with their respective graticule lines (reposition the display slightly with the horizontal FINE control if necessary).
e. Position the first eight-division portion of the total magnified sweep onto the viewing area.
f. CHECK-One marker each division between the firstand ninth-division vertical lines; marker at ninth-division vertical line must be within 0.12 division (within $1.5 \%$ ) of the line when the marker at the first-division vertical line is positioned exactly.
g. Repeat this check for each eight division portion of the total magnified sweep length.
h. INTERACTION-Check steps 45, 53, 55 and 57.
45. Adjust Magnifier Register
a. Set the time-mark generator for five-millisecond markers.
b. Position the middle marker (three markers on total magnified sweep) to the center vertical line (see Fig. 6-41A).
c. Set the MAG switch to OFF.
d. CHECK-Middle marker should remain at the center vertical line (se屯 Fig. 6-41B).
e. ADJ UST-Mag Register adjustment, R855 (see Fig. 641C ], to position the middle marker to the center vertic al line.
f. Set the MAG switch to X10.
g. Repeat parts b through e until no shift occurs when MAG switch is set to OFF.
46. Adjust B Sweep Calibration
a. Change the following control settings:

| DELAY-TME MULTPLIER | Fully counterclockwise |
| :--- | :--- |
| A TME/DIV | 2 ms |
| B TME/DIV | 1 ms |
| B SWEEP MODE | TRIGGERABLE AFTER |
|  | DELAY TME |
| HORIZ DISPLAY | DELAYED SWEEP (B) |
| MAG | OFF |

b. Set the time-mark generator for one-millisecond markers.
c. Set the B LEVEL control for a stable display.
d. CHECK-CRT display for one marker each division. between the first- and ninth-division vertical lines (see-Fig. [6-42A].
e. ADJ UST-B Sweep Cal adjustment, R741 (se Fiq. 6-42B), for one marker each division.
f. INTERACTION-Check steps 51 and 56.

## 47. Check B Sweep Length

a. Set the time-mark generator for 1- and 0.1-millisecond markers.
b. Move the eleventh large marker to the center vertical line with the horizontal POSITION control (see Fiq. 6-43).


Fig. 6-41. Typical CRT display showing correct magnif ier register. (A) MAG switch to $X 10$, (B) MAG switch set to OFF, (C) locs. tion of Mag Register adjustment (B Sweep circuit board).
c. CHECK-B Sweep length must be between 10.5 and 11.5 divisions, as shown by 0.5 to 1.5 divisions of display to the right of the center vertical line (se Fig. 6-43). Large markers indicate divisions and small markers indicate 0.1 division.
48. Check A Sweep Length
a. Set the HORIZ DISPLAY switch to A.
b. Set the $A$ TMME/DIV switch to 1 ms .


Fig. 6-42. (A) Typical CRT display showing correct B Sweep calibration, (B) location of the B Sweep Cal adjustment of (B Sweep circuit board).
c. Move the eleventh marker to the center vertical line with the horizontal POSITION control (see Fiq. 6-4 B].
d. CHECK-A Sweep length must be between 10.5 and 11.5 divisions as shown by 0.5 to 1.5 divisions of display to the right of the center vertical line.
e. Reposition the first marker to the left graticule line.
f. Tum the A SWEEP LENGTH control to 4 DIV (not in B ENDS A detent).
g. CHECK-A Sweep length must be four divisions or less.

## 49. Check B Ends A Operation

a. Change the following control settings:
B TIME/DIV
.1 ms
B SWEEP MODE
B STARTS AFIER DELAY TME
HORIZ DISPLAY
A INTEN DURING B
B ENDS A
b. Rotate the DELAY-TIME MULTIPUER dial throughout its range.
c. CHECK-CRT display ends after the intensified portion at 011 DELAY-TIME MULTIPLER dial settings.


Fig. 6-43. Typical CRT display when checking A and sweep lengih.

## 50. Check A Variable Control Range

a. Change the following control settings:

| DELAY-TIME MULTIPLIER | Fully counterclockwise |
| :--- | :--- |
| B TIME/DIV | 1 ms |
| HORIZ DISPLAY | A |
| A SWEEP LENGTH | FULL |

b. Set the time-mark generator for 10 -millisecond markers.
c. Position the markers to the far left and right graticule lines with the horizontal POSITION control.
d. Tum the A VARIABLE control fully counterclockwise.
e. CHECK-CRT display for four-division maximum spacing between markers (indicates adequate range for continuously variable sweep rates between the calibrated steps; se Fiq. 6-44] UNCAL A OR B light must be on when A VARIABLE control is not in CAL position.

Spacing between markers must be four divisions or less for correct VARIABLE control range.


Fig. 6-44. Typical CRT display when checking $A$ and B VARIABLE control range.
51. Check B Variable Control Range
a. Change the following control settings:

| A TIME/DIV | 5 ms |
| :--- | :--- |
| B TME/DIV | 1 ms |
| A VARIABLE | CAL |
| B SWEEP MODE | TRIGGERABLE AFTER |
|  | DELAY TME |
| HORIZ DISPLAY | DELAYED SWEEP (B) |

b. Position markers to the far left and right vertical lines of the graticule with the horizontal POSTION control.
c. Tum the B TIME/DIV VARIABLE control fully counterclockwise.
d. CHECK-CRT display for four-division maximum spacing between markers (indicates adequate range for continuously variable sweep rate between the calibrated steps; se Fig. 6-44) UNCAL A OR B light must be on when B TME/DIV VARIABLE control is not in CAL position.
52. Adjust One-Microsecond Timing
a. Change the following control settings:

| A and B TMME/DIV | $1 \mu s$ |
| :--- | :--- |
| HORIZ DISPLAY | A |
| B TMME/DIV VARIABLE | CAL |

b. Set the time-mark generator for one-mic rosecond markers.
c. CHECK-CRT display for one marker each division between the first- and ninth-division vertical lines (see Fig. 6-45A).
d. ADJ UST-C530A (see Fig. 6-45B) for one marker each division.
e. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B].


Fia. 6-45. Troical CRT display showing correct one-microsecond timing, (B) location of C530A and C740A (behind swing-out side panell.
f. CHECK-CRT display for one marker each division between the first- and ninth-division vertical lines (see Fig. $6-45 \mathrm{~A}$ ).
g. ADJ UST-C 740A (see Fig. 6-45B) for one marker each division.

NOTES


Fig. 6-4 6. (A) Typical CRT. display showina correct hiah epand linearity, (B) location of C882 and C892 (B Sweep circuif board).

## 53. Adjust High-Speed Linearity

a. Change the following control settings:

| CH 1 VOLTS/DIV | 20 mV |
| :--- | :--- |
| A ond B TMME/DIV | $.1 \mu \mathrm{~s}$ |
| HORIZ DISPLAY | A |

b. Set the time-mark generator for 10 -na nosecond markers.
c. Position the display horizontally so the sweep starts at the left edge of the graticule.
d. Set the MAG switch to $X 10$.
e. CHECK-CRT display for optimum linearity over the center eight divisions of the graticule (see Fig. 6-4б A ).
f. ADJ UST-C882 and C892 (see Fig. 6-46B) for optimum linearity over the center eight divisions of the graticule (attempt to keep C882 and C892 nearly equal in capacitance by adjusting each capacitor about the same amount).

## 54. Check A Sweep liming Accuracy <br> a. Change the following control settings:

## CH 1 VOLTS/DIV MAG <br> . 2 <br> OFF

b. CHECK-Using the A TIME/DIV switch and time-mark generator settings given in Table 6-5, check A sweep timing within 0.24 division, over the middle eight divisions of the display (within 3\%).

## CAUTION

To prevent possible buming of the CRT phosphor at slow sweep rates, position the baseline of the marker display below the viewing area.

TABLE 6-5
A and B Timing Accuracy

| A and B <br> TIME/DIV <br> Switch Setting | Time-Mark <br> Generator Output | CRT Display <br> (markers/ <br> division) |
| :---: | :---: | :---: |
| $.1 \mu \mathrm{~s}$ | 0.1 microsecond | 1 |
| $.2 \mu \mathrm{~s}$ | 0.1 microsecond | 2 |
| $.5 \mu \mathrm{~s}$ | 0.5 microsecond | 1 |
| $1 \mu \mathrm{~s}$ | 1 microsecond | 1 |
| $2 \mu \mathrm{~s}$ | 1 microsecond | 2 |
| $5 \mu \mathrm{~s}$ | 5 microsecond | 1 |
| $10 \mu \mathrm{~s}$ | 10 microsecond | 1 |
| $20 \mu \mathrm{~s}$ | 10 microsecond | 2 |
| $50 \mu \mathrm{~s}$ | 50 microsecond | 1 |
| .1 ms | 0.1 millisecond | 1 |
| .2 ms | 0.1 millisecond | 2 |
| .5 ms | 0.5 millisecond | 1 |
| 1 ms | 1 millisecond | 1 |
| 2 ms | 1 millisecond | 2 |
| 5 ms | 5 millisecond | 1 |
| 10 ms | 10 millisecond | 1 |
| 20 ms | 10 millisecond | 2 |
| 50 ms | 50 millisecond | 1 |
| .1 s | 0.1 second | 1 |
| .2 s | 0.1 second | 2 |
| .5 s | 0.5 second | 1 |
|  | A Sweep Only |  |
| 1 l | 1 second | 1 |
| 2 s | 1 second | 2 |
| 5 s | 5 second | 1 |
|  |  |  |

55. Check A Magnified Sweep Accuracy
a. Set the MAG switch to X 10 .
b. CHECK-Using the A TIME/DIV switch and time-mark generator settings given in Table 6-6, check A magnified sweep timing within 0.32 divisions over the middle eight divisions of the magnified display (within 4\%). Note the portion of the total magnified sweep length to be excluded from the measurement. Magnifier light must be on.

TABLE 6-6

A and B Magnified Accuracy

| A and B <br> TIM E/DIV <br> Switch Setting | Time-Mark <br> Generator Output | CRT Display <br> (markers/ <br> division) | Portions of total magnified <br> sweep length to exclude <br> from measurement |
| :---: | :---: | :---: | :---: |
| $.1 \mu \mathrm{~s}$ | 10 nanosecond | 1 | First and last three divisions. |

56. Check B Sweep Timing Accuracy
a. Set the MAG switch to OFF.
b. Set the HORIZ DISPLAY switch to DELAYED SWEEP (B).
c. CHECK-Using the A and B TME/DIV switch and timemark generator settings given in Table 6-5. check B sweep timing within 0.24 division over the middle eight divisions of the display (within 3\%).

## 57. Check B Magnified Sweep Accuracy

a. Set the MAG switch to X10.
b. CHECK-Using the A and B TME/DIV switch and timemark generator settings given in Table 6-6, check B magnified sweep timing within 0.32 division over the middle eight divisions of the magnified display (within 4\%). Note the portions of the total magnified sweep length to be excluded from the measurement.
58. Check Delay-Time Accuracy
a. Set the MAG switch to OFF.
b. Set the B SWEEP MODE switch to B STARTS AFTER DELAY TME.
c. CHECK-Using the A TMME/DIV switch, B TME/DIV switch and time-mark generator settings given in Table 6-7, check delayed sweep accuracy within the given tolerance. First set the DELAY-TIME MULTIPUER dial to 1.00 and rotate the dial until the sweep starts at the top of the second marker (see Fig. 6-47). Note the dial reading and then set the dial to 9.00 and rotate until the sweep starts at the top of the tenth marker. DELAY-TME MULTIPLIER dial setting must be 8.00 divisions higher, + or - the allowable error given in Table 6-7.

## NOTE

Sweep will start at top of third marker at 1.00 , and nineteenth marker at 9.00 for sweep rates which are multiples of 2 (e.g., $2 \mu \mathrm{~s}, 20 \mu \mathrm{~s}, .2 \mathrm{~ms}$, etc.). If in doubt as to the correct setting af the DELAYTME MULTPLIER dial, set the HORIZ DISPLAY switch to A INTEN DURING B and check which marker is intensified.

TABLE 6-7
Delayed Sweep Accuracy

| A TIME/DIV Switch Setting | B TME/DIV Switch Setting | Time-Mark Generator Output | Allowable error for given accuracy |
| :---: | :---: | :---: | :---: |
| $1 \mu \mathrm{~s}$ | . $1 \mu \mathrm{~s}$ | $1 \mathrm{mic}^{\text {rosec ond }}$ | $\pm 12$ minor dial divisions ( $\pm 1.5 \%$ over center eight divisions) |
| $2 \mu \mathrm{~s}$ | . $1 \mu \mathrm{~s}$ | 1 microsecond |  |
| $5 \mu \mathrm{~s}$ | . $5 \mu \mathrm{~s}$ | 5 mic rosecond |  |
| $10 \mu \mathrm{~s}$ | $1 \mu \mathrm{~s}$ | 10 microsecond |  |
| $20 \mu \mathrm{~s}$ | $1 \mu \mathrm{~s}$ | 10 microsecond |  |
| $50 \mu \mathrm{~s}$ | $5 \mu \mathrm{~s}$ | 50 microsecond |  |
| . 1 ms | $10 \mu \mathrm{~s}$ | 0.1 millisec ond |  |
| . 2 ms | $10 \mu \mathrm{~s}$ | 0.1 millisec ond |  |
| . 5 ms | $50 \mu \mathrm{~s}$ | 0.5 millisec ond |  |
| 1 ms | . 1 ms | 1 millisec ond |  |
| 2 ms | . 1 ms | 1 millisecond |  |
| 5 ms | . 5 ms | 5 millisecond |  |
| 10 ms | 1 ms | 10 millisec ond |  |
| 20 ms | 1 ms | 10 millisec ond |  |
| 50 ms | 5 ms | 50 millisec ond |  |
| . 1 s | 10 ms | 0.1 second | $\pm 20$ minor dial divisions ( $+2.5 \%$ over center eight divisions] |
| . 2 s | 10 ms | 0.1 second |  |
| . 5 s | 50 ms | 0.5 second |  |
| 1 s | . 1 s | 1 second |  |
| 2 s | . 1 s | 1 second |  |
| 5 s | . 5 s | 5 second |  |

59. Check Delay-Time Multiplier Incremental Linearity
a. Change the following control settings:

| DELAY-TIME MULTIPLIER | 9.00 |
| :--- | :--- |
| A TMME/DIV | 1 ms |
| B TME/DIV | $5 \mu \mathrm{~s}$ |

b. Set the time-mark generator for one-millisecond markers.

Fig. 6-47. Typical CRT display when checking delayed-sweep accuracy.

c. Rotate the dial as necessary to position the start of the pulse to the beginning of the sweep (see Fiq. 6-48).
d. CHECK-Deviation of dial reading from 9.00 should be within two minor dial divisions ( $\pm 0.2 \%$ ).

NOTE
A sweep must be correctly calibrated to check this step to the given accuracy.
e. Repeat check at each major dial division between 9.00 and 1.00.


Fig. 6-48. Typical CRT display when checking DELAY-TIME MULTIPLIER incremental linearity.
60. Check Delay-Time Jitter
a. Change the following control settings:

DELAY-TIME MULTIPLIER $\quad 1.00$ B TIME/DIV
$1 \mu \mathrm{~s}$
b. Position the pulse near the center of the display area with the DELAY-TMME MULTIPLIER dial.
c. CHECK-Jitter on the leading edge of the pulse should not exceed 0.5 division (one part in 20,000; see Fig. 6-49). Disregard slow drift.
d. Tum the DELAY-TIME MULTPUER dial to 9.00 and adjust so the pulse is displayed near the center of the display area.
e. CHECK-Jitter on leading edge of the pulse should not exceed 0.5 division (sce Fig. 6-49]. Disregard slow drift.
f. Disconnect all test equipment.

Chock leading edge of delayed swoep display for filter


Fig. 6-49. Typical CRT display when checking delay-fime jitter.


Fig. 6-50. Initial test equipment setup for steps 61 through 66.

CRT controls
INTENSITY
FOCUS
SCALE ILLUM

Midrange
Adjust for focused display As desired

Vertical controls (both channels if a pplic able)

| VOLTS/DIV | 20 mV |
| :--- | :--- |
| VARIABLE | CAL |
| POSITON | Midrange |
| INPUT COUPLING | DC |
| MODE | CH 2 |
| TRIGGER | CH 1 ONLY |
| INVERT | Pushed in |

Triggering controls (both A ond B if applicable)

| LEVEL | Any position |
| :--- | :--- |
| SLOPE | + |
| COUPLING | DC |
| SOURCE | INT |

Sweep controls

| DELAY-TIME MULTIPLIER | 9.00 |
| :--- | :--- |
| A TMME/DIV | 1 ms |
| B TMME/DIV | 1 ms |
| A VARIABLE | CAL |
| A SWEEP MODE | AUTO TRIG |
| B SWEEP MODE | B STARTS AFIER |
|  |  |
|  | DELAY TIME |

HORIZ DISPLAY
MAG
A SWEEP LENGTH
POSITION
POWER

Side-panel controls

| B TMME/DIV VARIABLE | CAL |
| :--- | :--- |
| CALIBRATOR | .1 v |

61. Adjust Extemal Horizontal Gain
a. Test setup is shown in Fig. 6-50
b. Connect the standard amplitude calibrator to the Channel 1 INPUT connector through the 42-inch BNC cable.
c. Set the standard amplitude calibrator for a 0.1 -volt squore-wave output.
d. Increase the INTENSITY control setting until the display is visible (two dots about five divisions apart).
e. Move the display to the center of the graticule with the Channel 1 POSITION control.
f. CHECK-CRT display for five divisions horizontal deflection. (See Fiq. 6-5)A).
g. ADJ UST-Ext Horiz Gain adjustment, R645 (see Fig $6-51 B)$, for five divisions horizontal deflection.


Fig. 6-51. (A) Typical CRT display showing correct external horizental gain, (B) location of Ext Horiz Gain adjustment (B Sweep circuit board).
62. Check External Horizontal Operation
a. Set the B SOURCE switch to EXT.
b. Connect the standard amplitude calibrator to the EXT HORIZ input connector (B EXT TRIG INPUT).
c. Set the standard amplitude calibrator for a two-volt square-wave output.
d. CHECK-CRT display for horizontal deflection between 6.5 and 8.7 divisions ( 270 millivolts/division, $+15 \%$ ).
e. Set the standard amplitude calibrator for a 20 -volt square-wave output.
f. Set the 8 SOURCE switch to EXT $\div 10$.
g. CHECK-CRT display for horizontal deflection between 6.2 and 9.2 divisions ( 2.7 volts/division, $\div 20 \%$ ).
h. Disconnect all test equipment.

## 63. Check X-Y Phasing

a. Connect the constant-amplitude sine wave generator to the Channel 1 and 2 INPUT connectors through the fivenanosceond GR cable, 50 -ohm in-line termination and the dual-input coupler.


Fig. 6-52. Typical CRT display when checking X-Y phasing.
b. Change the following control settings:

| CH 1 VOLTS/DIV | 10 mV |
| :--- | :--- |
| CH 2 VOLTS/DIV | 50 mV |
| B SOURCE | INT |

c. Set the medium-frequency generator for a 10-division horizontal display at 50 kilohertz.
d. Center the display vertically and horizontally with the Channel 1 and 2 POSITION controls.
e. CHECK-CRT display for an opening at the center horizontal line of 0.52 division or less ( $3^{\circ}$ or less phase shift; see Fig. 6-52).
64. Check X Bandwidth in External Horizontal Mode
a. Disconnect the dual-input coupler from the Channel 2 INPUT connector.
b. Set the medium-frequency generator for a six-division horizontal display at its reference frequency ( 50 kHz ).
c. Without changing the output amplitude, increase the output frequency of the generator until the horizontal deflection is reduced to 4.2 divisions ( -3 dB point; se Fiq. 6-53).
d. CHECK-Output frequency of generator must be five megahertz or higher.

## 65. Check Trace Finder Operation

a. Reconnect the dual-input coupler to the Channel 2 INPUT connector.
b. While holding the TRACE FINDER button depressed, rotate the Channel 1, Channel 2 and horizontal POSITION controls and the CH 1 and CH 2 VOLTS/DIV switches throughout their ranges.
c. CHECK-CRT display remains within the graticule area.
d. While holding the TRACE FINDER button depressed, adjust the positioning controls until the display is centered about the graticule center lines. Then, increase the $X$ and $Y$


Fig. 6-53. Typical CRT display when checking external horizontal bandwidth (double exposure).
deflection factors until the display is reduced to about two divisions vertically and abaut four divisions horizontally.
e. Release the TRACE FINDER button.
f. CHECK-CRT display must remain within the graticule area.
g. Reduce the INTENSITY control to a normal setting (about midrange).
h. Disconnect all test equipment.
66. Check Chopped Operation
a. Change the following control settings:


Fig. 6-54. Typical CRT display when checking chopped repetition rate and blanking.

| MODE | CHOP |
| :--- | :--- |
| TRIG GER | NORM |
| A and B TME/DIV | $.5 \mu \mathrm{~S}$ |
| HORIZ DISPLAY | A |

b. Position the traces about four divisions apart.
c. Set the A LEVEL control for a stable display.
d. CHECK-Each cycle for duration of 3.4 to 5 divisio ( 500 kilohertz, $\pm 20 \%$; see Fig. 6-54).
e. CHECK-CRT display for complete blanking of switching transients between chopped segments (sele Fig. 6-54).

NOTES


Fig. 6-55. Initial test equipment setup for steps $\mathbf{6 7}$ through $\mathbf{7 0}$.

CRT controls
INTENSITY
Focus SCALE ILLUM

Midrange
Adjust for focused display As desired

Vertical controls (both channels if applicable)

| CH 1 VOLTS/DIV | 50 mV |
| :--- | :--- |
| CH 2 VOLTS/DIV | .2 |
| VAARIABE | CAL |
| POSITION | Midrange |
| Input Coupling | DC |
| MODE | ALT |
| TRIGGER | NORM |
| INVERT | Pushed in |

Triggering controls (both A and B if applicable)

| LEVEL | Stable display |
| :--- | :--- |
| SLOPE | + |
| COUPLING | AC |
| SOURCE | INT |

## Sweep controls

DELAY-TIME MULTIPLIER 9.00
$A$ and $B$ TME/DIV 1 ms
A VARIABLE CAL
A SWEEP MODE AUTO TRIG
B SWEEP MODE
B STARTS AFIER DELAY TME

| HORIZ DISPLAY | A |
| :--- | :--- |
| MAG | OFF |
| A SWEEP LENGTH | FULL |
| POSITION | Midrange |
| POWER | ON |

Side-panel controls

| B TIME/DIV VARIABLE | CAL |
| :--- | :--- |
| CALIBRATOR | .1 V |

67. Adjust Calibrator Repetition Rate
a. Test equipment setup is shown ir Fiq. 6-55
b. Connect the 1 kHz CAL connector to the Channel 1 INPUT connector with an 18 -inch BNC cable.
c. Connect the time-mark generator to the Channel 2 INPUT connector with a 42 -inch BNC cable.
d. Set the time-mark generator for one-millisec ond markers.
e. Position the display so the tips of the markers fall iust below the rising portions of the square wave (se Fig. 6-5\%A).
f. CHECK-For one cycle of calibrator waveform for each marker (se Fia. 6-56A).
g. ADJ UST-C a librator Frequency adjustment, T1255 (see Fig. 6-56|B), for one cycle of calibrator waveform for each marker (preliminary adjustment).


Fig. 6-56. (A) Typical CRT display showing correct calibrator repetition rate, (B) location of Calibrator Frequency adjustment.
h. Set the TRIGGER switch to CH 1 ONLY.
i. CHECK-CRT display for slow drift or no drift of the time markers.
j. ADJ UST-T1255 for minimum drift of time markers. (final adjustment).
k. Disconnect the time-mark generator.

## 68. Check Calibrator Duty Cycle

a. Change the following control settings:

| CH 1 VOLTS/DIV | 20 mV |
| :--- | :--- |
| MODE | CH 1 |
| A and B TME/DIV | .1 ms |

b. Center the display vertically with the Channel 1 POSITION control.
c. Set the A LEVEL control so the display starts at the $50 \%$ point on the rising portion of the waveform (the INTENSITY control may need to be advanced slightly to see the rising portion of the waveform).
d. Set the MAG switch to $\times 10$.


Fig. 6-57. Typieal CRT display when checking calibrator duty cycle.
e. Position the $50 \%$ point on the falling edge of the Calibrator waveform to the center vertical line.
f. Set the A SLOPE switch to -.
g. CHECK-50\% point on rising edge now displayed not displaced more than two divisions from the center vertical line (duty cycle $49 \%$ to $51 \%$; see Fig. 6-57).
69. Check Calibrator Risetime
a. Change the following control settings:

```
A SLOPE
A and B TMME/DIV
MAG
```



```
OFF
```

b. Set the A LEVEL control so all of the rising portion of the Calibrator waveform is visible.
c. Position the $10 \%$ point on the leading edge to a vertical graticule line.
d. CHECK-CRT display for five divisions or less between the $10 \%$ and $90 \%$ points an the leading edge of the cali-


Fig. 6-58. Typical CRT display when checking Calibrator risetime.

0.5 division

Fig. 6-59. Typical CRT display when checking calibrator current.
brator waveform (one microsecond or less, risetime, see Fig. 6-58).
e. Disconnect the 18 -inch BNC cable.
70. Check Current through Probe Loop
a. Connect the current-measuring probe and passive termination to the Channel 1 INPUT connector.
b. Set the passive temmination for a sensitivity of $2 \mathrm{~mA} /$ mV .
c. Clip the current probe around the PROBE LOOP on the side panel.
d. Set the CH 1 VOLTS/DIV switch to 5 mV .
e. Set the $A$ and $B$ TIME/DIV switch to .5 ms .
f. CHECK-CRT display 0.5 division in amplitude (five millisec onds; see Fig. 6-59).

## NOTE

This step checks for the presence of current in the PROBE LOOP. This current will remain within the stated $1 \%$ accuracy due to the tolerance of the divider resistors and tolerance of the calibrator output voltage (adjusted in step 2). If it is necessary to verify the accuracy of the calibrator current, use a current measuring meter with an accuracy of at least 0.25\%.
g. Disc onnect all test equipment.

N O TES


Fig. 6-60. Initial test equipment sefup for steps 71 through 74.

CRT controls
INTENSITY
FOCUS
SCALE ILLUM

Midrange
Adjust for focused display As desired

HORIZ DISPLAY
MAG
A SWEEP LENGTH
POSITION Midrange
POWER ON

Side-panel controls

| B TIME/DIV VARIABLE | CAL |
| :--- | :--- |
| CALIBRATOR | .1 V |

71. Adjust $Z$ Axis Compensation
a. Test equipment setup is shown ir Fig. 6-60
b. Connect the 10X probe to the input connector of the test oscilloscope.
c. Connect the 10X probe to TP1047 (se Fig. 6-61A).
d. Set the test oscilloscope for a vertical deflection factor of 0.5 volts/division ( 5 volts/division total with probe) at a sweep rate of 0.1 microsecond/division.
e. Set the INTENSITY control so the test oscilloscope display is three divisions in amplitude.
f. CHECK-Test oscilloscope display for optimum square comer (slightly rounded) on blanking gate (se Fig. 6-61B).
g. ADJ UST-C1036 (see Fig. 6-61A) for optimum square comer on the unblanking gate.


Fig. 6-61. (A) Location of TP 1047 and C1 036, (B) typical fes oscilloscope display showing correct adjustment of C1 036 (vertical deflection, 5 volts/division, sweep rate, 0.1 microsecond/division)
h. Disconnect all test equipment.

## 72. Check Extemal Z Axis Operation

a. Set the INTENSITY control to a nomal setting.
b. Set the $A$ and B TIME/DIV switch to 20 Ks .
c. Connect the constant-amplitude generator to the A EXT TRIG INPUT connector through the five-nanosecond GR cable, $50-0 h m$ in-line termination and BNC Tconnector. Connect the output of the BNC T connector to the Z AXIS INPUT binding posts through a 42-inch BNC cable and the BNC to alligator clips adapter. (Connect black lead af alligator clips adapter to ground post.)
d. Set the A SOURCE switch to EXT.
e. Remove the ground strap from between the binding posts.
f. Set the constant-amplitude generator for five volts output at 50 kilohertz (use calibrated position of generator amplitude control).
g. CHECK-CRT display for noticeable intensity modulation [se Fig. 6-6RA). The INTENSITY control setting may need to be reduced to view trace modulation.


Fig. 6.62. (A) Typical CRT display when checking Z-axis operation at 50 kilohertz, (B) typical CRT display when checking Z-axis operation at 50 megahertz.
h. Set the constant-amplitude generator for five volts output at 50 megahertz [use calibrated position of generator amplitude control).
i. Set the $A$ and $B$ TIME/DIV switch to $.1 \mu \mathrm{~s}$.
j. CHECK-CRT display for noticeable intensity modulation (see Fig, 6-62B). The INTENSITY control setting may need to be reduced to view trace modulation.
k. Disconnect all test equipment and replace ground strap.

## 73. Check A Gate Output Signal

a. Set the $A$ and $B$ TIME/DIV switch to 1 ms.
b. Connect the A GATE cannector (on side panel) to the test-oscilloscope input connector with the 42-inch BNC cable.
c. Set the test oscilloscope for a vertical deflection factor of five volts/division at a sweep rate of twa milliseconds/ division.
d. CHECK-Test oscilloscope display for 2.4 divisions; $\pm 0.24$ division, vertical deflection with the bottom of the waveform near the zero-volt level ( 12 volts, $\pm 10 \%$; see Fiq. 6-63. Gate duration should be about 5.5 divisions (about 11 times the A TIME/DIV switch setting).


Fig. 6-63. Typical CRT display when checking gate amplitude and duration (vertical deflection, five volts/division; sweep rate, iwo milliseconds/divisionl.

## 74. Check B Gate Output Signal

a. Cannect the B GATE connector (on side panel) to the test-oscilloscope input connector with the 42-inch BNC cable.
b. Change the following control settings:

| A TME/DIV | 2 ms |
| :--- | :--- |
| B TME/DIV | 1 ms |
| HORIZ DISPLAY | DELAYED SWEEP (B) |

c. CHECK-Test oscilloscope display for 2.4 divisions, $\pm 0.24$ division, vertical deflection with the bottom of the waveform near the zero-volt level ( 12 volts $\pm 10 \%$; see Fig. 6-63), Gate duration should be about 5.5 divisions (about 11 times the B TIME/DIV switch setting).
This completes the calibration procedure for the Type 453. Disconnect all test equipment and replace the top and bottom covers. If the instrument has been completely checked and calibrated to the tolerances given in this procedure, it will meet the electrical characteristics listed in the Performance Requirement column of the Characteristics section of this manual.

## NOTES

## PREVENTIVE MAINTENANCE INSTRUCTIONS

## 7-1. Scope of Maintenance

The maintenance duties assigned to operator and organizational categories are listed below, together with a reference to the paragraphs covering the specific maintenance functions.
a. Daily preventive maintenance checks and services para 7-4).
b. Weekly preventive maintenance checks and services (para 7-5).
c. Monthly preventive maintenance checks and services (para 7-6).
d. Quarterly preventive maintenance checks and services (para 7-7).
e. Cleaning (para 7-8).
f. Touchup painting (para 7-9).

## 7-2. Preventive Maintenance

Preventive maintenance is the systematic care, servicing, and inspection of equipment to prevent the occurrence of trouble, to reduce downtime, and to assure that the equipment is serviceable.
a. Systematic Care. The procedures given in paragraphs 7-3 through 7-9 cover routine systematic care and cleaning essential to proper upkeep and operation of the equipment.
b. Preventive Maintenance Checks and Services. The preventive maintenance checks and services charts (paras $7 \exists 4$ through 7-7) outline functions to be performed at specific intervals. These checks and services are to maintain Army electronic equipment in a combat-serviceable condition; that is, in good general (physical) condition and in good operating condition. To aisist operators in maintaining combat serviceability, the charts indicate what to check, how to check, and what the normal conditions are; the References column lists the illustrations, paragraphs, or manuals that contain detailed repair or replacement procedures. If the defect cannot be remedied by the corrective actions listed, higher category of maintenance repair is required. Records and reports of these checks and services must be made in accordance with the requirements set forth in TM 38-750.

## 7-3. Preventive Maintenance Checks and Services Periods

Preventive maintenance checks and services of the equipment are required daily, weekly, monthly, and quarterly.
a. Paragraph 7-4 pecifies the checks and services that must be accomplished daily (or at least once each week if the equipment is maintained in standby condition).
b. Paragraphs 7-5, 7-6, snd 7-7 specify additional checks and services that must be performed weekly, monthly, and quarterly.

7-4. Daily Preventive Maintenance Checks and Services Chart

| Sequence no. | Item to be inspected | Procedure | References |
| :---: | :---: | :---: | :---: |
| 1 | Completeness | See that the equipment is complete (app. B). | None. |
| 2 | Exterior surfaces. | Clean the exterior surfaces (para 7- ${ }^{\text {P }}$ |  |
| 3 | Connectors | Check the tightness of all connectors. |  |
| 4 | Controls | While makhg the operating check (sequence No. 5), check to see that the mechanical action of each knob, dial, and switch is smooth and free of extemal or internal binding, and that there is no excessive looseness. |  |
| 5 | Operation | Operate the equipment according th section 2 |  |

7-5. Weekly Preventive Maintenance Checks and Services Chart

| Sequence no. . | Item to be inspected | Procedure | References |
| :---: | :---: | :---: | :---: |
| 1 | Cables and probes . | Inspect cords, cables, probes, and wires for chafed, cracked, or frayed insulation. Replace connectors that are broken, arced, stripped, or wom excessively. |  |
| 2 | Handles and latches. | Inspect handles for looseness. Replace or tighten as necessary. |  |
| 3 | Metal surfaces . | Inspect exposed metal surfaces for rust and corrosion. Clean and touch up paint as required. | Paras 7-8 and 7-9. |

7-6. Monthly Preventive Maintenance Checks and Services Chart

| Sequence no. | Item to be inspected | Procedure | References |
| :---: | :---: | :---: | :---: |
| 1 | Pluckout items | Inspect seating of pluckout items. | None. |
| 2 | Jacks | Inspect jacks for snug fit and good contact. |  |
| 3 | Transformer terminals. | Inspect terminals on the transformers. There should be no evidence of dirt or corrosion. |  |
| 4 | Terminal blocks | Inspect terminal blocks for loose connections and cracked or broken insulation. |  |
| 5 | Resistors and capacitors | Inspect resistors and capacitors for cracks, blistering, or other defects. |  |
| 6 | Variable capacitors | Inspect variable capacitors for dirt, comosion, and deformed plates. |  |
| 7 | Interior | Clean interior of chassis and cabinet. |  |

7-7. Quarterly Preventive Maintenance Checks and Services Chart

| Sequence no. | Item to be inspected | Procedure | References |
| :---: | :---: | :---: | :---: |
| 1 | Public ations | See that all publications are complete, serviceable, and current. | DA Pam 310-4. |
| 2 | Modifications | Check DA Pam 310-7 to determine whether new applicable MWO's have been published. All URGENT MWO'S must be applied immediately. All NORMAL MWO'S must be scheduled. | TM 38-750 and DA Pam 310-7. |
| 3 | Spare parts | Check all spare parts (operator and organizational) for general condition and method of storage. No overstock should be evident, and all shortages must be on valid requisitions. |  |

7-2

## 7-8. Cleaning

Inspect the exterior of the equipment. The exterior surfaces should be free of dirt, grease, and fungus.
a. Remove dust and other loose dirt with a clean soft cloth.

## WARNING

Adequate ventilation should be provided while using TRICHLOROTRIFLUOROETHANE. Prolonged breathing of vapor should be avoided. The solvent should not be used near heat or open flame; the products of decomposition are toxic and irritating. Since TRICHLOROTRIFLUOROETHANE dissolves natural oils, prolonged contact with skin should be avoided. When necessary, use gloves which the solvent cannot penetrate. If the solvent is taken internally, consult a physician immediately.
b. Remove grease, fungus, and ground-in dirt from the cases; use a cloth dampened (not wet) with cleaning compound.
c. Remove dust or dirt from plugs and jacks with a brush.
d. Clean the front panel and control knobs; use a soft, clean cloth. If dirt is difficult to remove, dampen the cloth with water; mild soap may be used for more effective cleaning.

## 7-9. Touchup Painting Instructions

Remove rust and corrosion from metal surfaces by lightly sanding them with fine sandpaper. Brush two thin coats of paint on the bare metal to protect it from further corrosion. Refer to the applicable cleaning and refinishing practices specified in TB 43-0118.

# SECTION 8 <br> MECHANICAL PARTS LIST 

FIGURE FO-1 FRONT


| Index No. | Tektronix Part No. | Serial/Model No. Disc | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 20 | 331-0092-00 |  | 1 | DIAL, window knob-A TIME/DIV |
|  | - . . . |  | - | dial includes: |
|  | 213-0022-00 |  | 1 | SCREW, set, $4-40 \times 3 / 16$ inch, HSS |
| 21 | 262-0724-01 |  | 1 | SWITCH, wired-A AND B TIME/DIV |
|  | - . - |  | - | switch includes: |
|  | 260-0694-00 |  | 1 | SWITCH, unwired |
| 22 | 131-0371-00 |  | 9 | CONNECTOR, single contact, female |
| 23 | 131-0181-00 |  | 2 | CONNECTOR, "erminal standoff |
|  | - |  |  | mounting harclware for each: (not included w/connector) |
| 24 | 358-0136-00 |  | 1 | BUSHING, plastic |
| 25 | 179-1122-00 |  | 1 | CABLE HARNESS |
| 26 | 384-0262-00 |  | 1 | ROD, extension |
| 27 | - - - |  | 1 | RESISTOR, variable |
|  | - |  | - | mounting hard'ware: (not included w/resistor) |
| 28 | 210-04 13-00 |  | 2 | NUT, hex., $3 / 8.32 \times 1 / 2$ inch |
| 29 | 210-0012-00 |  | 1 | LOCKWASHEER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
| 30 | 407-0148-00 |  | 1 | BRACKET |
|  | - . - |  |  | mounting hordware: (not included w/bracket) |
|  | 210-0006-00 |  | 1 | LOCKWASH ER, internal, \#6 (not shown) |
| 3132 | 210-0202-00 |  | 1 | LUG, solder, SE \#6 |
|  | 210-0449-00 |  | 2 | NUT, hex., 5-40 $\times 1 / 4$ inch |
| 33 | -•••• |  | 2 | CAPACITOR |
|  | - 21 - - |  |  | mounting hardware for each: (not included w/capacitor) |
| 34 | $210-0018.00$ |  | 1 | LOCKWASHER, internal, $5 / 16$ inch |
|  | $210-0524-00$ |  | 1 | NUT, hex., $5 / 16-24 \times 1 / 2$ inch |
| 3637 | 376-0014-00 |  | 1 | COUPLING |
|  | . - . - |  | 1 | CAPACITOR |
|  | $\cdot$ |  | - | mounting hardware: (not included w/capacitor) |
| 38 | 210-0457-00 |  | 2 | NUT, keps, $6-32 \times 5 / 16$ inch |
| 39 | 348-0055-00 |  | 1 | GROMMET, plastic, $1 / 4$ inch |
|  | - --. |  | I | mounting hardware: (not included w/switch) |
|  | 211-0507-00 |  | 2 | SCREW, $6-32 \times 5 / 16$ inch, PHS (not shown) |
| 40 | 210-0049-00 |  | 1 | LOCKWASHER, internal, $5 / 8$ inch |
| 41 | 210-0579-00 |  | 1 | NUT, hex., $5 / 8-24 \times 3 / 4$ inch |
| 42 | 331-0139-00 |  | 1 | DIAL-DELAY TIME MULTIPLIER |
|  | - . . - |  | - | dial includes: |
|  | 213-0048-00 |  | 1 | SCREW, set, $4-40 \times 1 / 8$ inch, HSS |
| 43 | - . . - |  | 1 | RESISTOR, variable |
|  | - -- - |  | - | mounting hardware: (not included w/resistor) |
| 44 | 210.0012-00 |  | 1 | LOCKW ASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
| 45 | 366-0220-00 |  | 1 | KNOEs, charcoal-LEVEL (B TRIGGERING) |
|  | - . . - |  | - | knob includes: |
|  | 213-0020-00 |  | 1 | SCREW, set, $6-32 \times 1 / 8$ inch, HSS |


| Index No. | Tekłronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Disc | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 46 | - - - - |  | 2 | RESISTOR, variable |
|  | - . . . - |  | - | mounting hardware for each: (not included w/resistor) |
| 47 | 210-0012-00 |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 1 / 2$ inch OD |
| 48 | 210-0978-00 |  | 1 | WASHER, flat, $3 / 8$ ID $\times 1 / 2$ inch OD |
| 49 | 210-0590-00 |  | 1 | NUT, hex., $3 / 8 \cdot 32 \times 7 / 16$ inch |
| 50 | 366-0148-00 |  | 1 | KNOB, charcoal-A SWEEP LENGTH |
|  | - - - |  | I | knob includes: |
|  | $213-0004-00$ |  | 1 | SCREW, set, 6-32 $\times 3 / 16$ inch, HSS |
| 51 | $262-0726-02$ |  | 1 | SWITCH, wired-A SWEEP LENGTH |
|  | - . . - |  | - | switch includes: |
|  | 260-0697-01 |  | 1 | SWITCH, Unwired |
|  | - - - |  | 1 | RESISTOR, variable |
|  |  |  | i | mounting hardware: (not included w/resistor) |
|  | 210-0012-00 |  | $1$ | LOCKWASHER, internal, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0590-00 |  | 2 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
|  | 376-0014-00 |  | 1 | COUPLING |
| $\begin{aligned} & 52 \\ & 53 \end{aligned}$ | 210-0978-00 |  | 1 | mounting hardware: WASHER, flat, $3 / 8 \mathrm{ID} \times 1 / 2$ inch OD |
|  | 210-0590-00 |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| 54 | 366-0189-00 |  | 1 | KNOB, red-MAG |
|  | $213-0020-00$ |  | 1 | knob includes: SCREW, set, $6-32 \times 1 / 8$ inch, HSS |
| 55 | 366-0322-00 |  | 1 | KNOB, charcoal-HORIZ DISPLAY |
|  | - . - - |  | - | knob includes: |
|  | 213-0004-00 |  | 1 | SCREW, set, $6.32 \times 3 / 16$ inch, HSS |
| 56 | 262-0725-02 |  | 1 | SWITCH, wired-HORIZ DISPLAY |
|  | - - - - |  | - | switch includes: |
|  | 260-0696-00 |  | 1 | SWITCH, Unwired |
|  | --..- |  | - | mounting hardware: (not included w/switch) |
| 57 | 210.0978-00 |  | 1 | WASHER, flat, $3 / 1$ ID $\times 1 / 2$ inch OD |
| 58 | 210-0590-00 |  | 1 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| 59 | 366-0319-00 |  | 1 | KNOB, red-_FINE knob includes: |
|  | 213-0020-00 |  | 1 | SCREW, set, $6-32 \times 1 / 8$ inch, HSS |
| 60 | 366-0138-00 |  | 1 | KNOB, charcoal-POSITION |
|  | 213-0004-00 |  | 1 | knob includes: SCREW, set, $6.32 \times 3 / 16$ inch, HSS |


| Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Nisc }}{\text { No. }}$ | $\begin{aligned} & \mathbf{Q} \\ & \dagger \\ & \mathbf{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | - . - |  |  | 1 | RESISTOR, variable |
|  | - - . . - |  |  |  | mounting hardware: (not included w/resistor) |
| 62 | 210-00 12-00 |  |  | 1 | LOCKWASHER, internal, $3 / 8-32 \times 1 / 2$ inch OD |
|  | 210.0494-00 | 20000 | 26129 | 1 | NUT, hex., $3 / 8-32 \times 1 / 2 \times 1 / 16$ inch OD |
|  | 129-0167-00 | 26130 |  | 1 | POST, metallic |
|  | 210.0013.00 | 20000 | 22039 | 1 | LOCKWASHER, internal, $3 / 8 \mathrm{ID} \times 1 / 16$ inch OD |
| $\begin{aligned} & 64 \\ & 65 \end{aligned}$ | 210-0012-00 | 22040 | 26129X | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 1 / 2$ inch OD |
|  | 210-0840-00 |  |  | 1 | WASHER, flat, 0.390 ID $\times 9 / 16$ inch OD |
| 66 | 358-0029-05 |  |  | 1 | BUSHING, hex., $1 / 2$ inch long |
| 67 | 366-0319.00 |  |  | 1 | KNOB, red-HF STAB |
|  | - - . |  |  |  | knob includes: |
|  | 213-0020-00 |  |  | 1 | SCREW, set, $6.32 \times 1 / 8$ inch, HSS |
| 68 | 366-0138-00 |  |  | 1 | KNOB, charcoal-LEVEL (A TRIGGERING) |
|  | - - - |  |  | - | knob includes: |
|  | 213-0004-00 |  |  | 1 | SCREW, set, $6-32 \times 3 / 16$ inch, HSS |
| 69 | 366-0215-01 |  |  | 1 | KNOB, charcoal-SLOPE (A TRIGGERING) |
| 70 | 260-0472-00 |  |  | 1 | SWITCH, lever-SLOPE |
|  | - - . . - |  |  | - | mounting hardware: (not included w/switch) |
| 71 | 220.0413-00 |  |  | 2 | NUT, switch, $4.40 \times 3 / 16 \times 0.562$ inch |
| 72 | 366-0215-01 |  |  | 1 | KNOB, charcoal-COUPLING (A TRIGGERING) |
| 73 | 366-0215-01 |  |  | 1 | KNOB, charcoal-SOURCE (A TRIGGERING) |
|  | 262-0723-00 |  |  | 1 | SWITCH, wired-COUPLING \& SOURCE |
|  | - - - - |  |  | - | switch includes: |
| 74 | 260-0700-00 |  |  | 1 | SWITCH, lever-COUPLING |
| 75 | 260-0698-01 |  |  | 1 | SWITCH, lever-SOURCE |
| 76 | 131.0371.00 |  |  | 2 | CONNECTOR, single contact, female |
|  | - . . . - |  |  |  | mounting hardware: (not included w/switch) |
| 77 | 220-0413-00 |  |  | 4 | NUT, switch, $4.40 \times 3 / 16 \times 0.562$ inch |
| 78 | 366-0215-01 |  |  | 1 | KNOB, charcoal-A SWEEP MODE |
|  | 260-0699-00 |  |  | 1 | SWITCH, lever-A SWEEP MODE |
|  | - - . . - |  |  | - | mounting hardware: (not included w/switch) |
| 80 | 220.0413-00 |  |  | 2 | NUT, switch, $4.40 \times 3 / 16 \times 0.562$ inch |
| $\begin{aligned} & 81 \\ & 82 \end{aligned}$ | 366-0215-01 |  |  | 1 | KNOB, charcoal-B SWEEP MODE |
|  | 260-0587-00 |  |  | 1 | SWITCH, lever-B SWEEP MODE |
|  | - . - |  |  |  | mounting hardware: (not included w/switch) |
| 83 | 220-041 3-00 |  |  | 2 | NUT, switch, $4-40 \times 3 / 16 \times 0.562$ inch |
| $\begin{aligned} & 84 \\ & 85 \end{aligned}$ | 366-0215-01 |  |  | 1 | KNOB, charcoal-SLOPE (B TRIGGERING) |
|  | 260-0472-00 |  |  | 1 | SWITCH, lever-SLOPE |
|  | --- - - |  |  |  | mounting hardware: (not included $\mathrm{w} / \mathrm{switch}$ ) |
| 86 | $220.0413-00$ |  |  | 2 | NUT, switch, $4-40 \times 3 / 16 \times 0.562$ inch |


| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | Q t y | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 87 | 366-0215-01 |  | 1 | KNOB, charcoal-COUPLING (B TRIGGERING) KNOB, charcoal-SOURCE (B TRIGGERING) SWITCH, wired-COUPLING \& SOURCE |
| 88 | 366-0215-01 |  | 1 |  |
|  | 262-0723-00 |  | 1 |  |
|  | - - - . - |  | - |  |
| 89 | 260-0700-00 |  | 1 | SWITCH, lever-COUPLING |
| 90 | 260-0698-01 |  | 1 | SWITCH, lever-SOURCE |
| 91 | 131-0371-00 |  | 2 | mounting hardware: (not included w/switch) |
|  | --- |  |  |  |
| 92 | 220-0413-00 |  | 4 | NUT, switch, 4-40 $\times 3 / 16 \times 0.562$ inch |
| 93 | 260-0834-00 |  | 1111 | SWITCH, toggle-POWER ON mounting hardware: (not included w/switch) |
|  | - ... |  |  |  |
| 94 | 210-0046-00 |  |  | LOCKWASHER, internal, $1 / 4 \mathrm{ID} \times 0.400$ inch ODWASHER, flat, $1 / 4 \mathrm{ID} \times 3 / 8$ inch OD |
| 95 | 210.0940-00 |  |  |  |
| 96 | 210-0562-00 |  |  | NUT, hex., $1 / 4-40 \times 5 / 16$ inch |
| 97 | 131-0352-01 |  | 3 | CONNECTOR, coaxial, 1 confact BNC, (w/hardware) FILTER, lens, clear |
| 98 | 378-0541-00 |  | 4 |  |
| 99 | $378-0541-01$ |  | 1 | FILTER, lens, clear FILTER, lens, green |
| 100 | 352-0084-00 |  | 2 | HOLDER, neon, black |
| 101 | 352-0084-01 |  | 3 | HOLDER, neon, white |
| 102 | 200-0609-00 |  | 5 | COVER, neon holder |
| 103 | 129-0103-00 |  | 1 | ASSEMBLY, binding post |
|  | $\cdots$ |  |  | assembly includes: |
|  | $200-01 \quad 03-00$ |  | 1 | CAP |
|  | 129-0077-00 |  | 1 | POST |
|  | . ... . - |  |  | mounting hardware: (not included w/assembly) |
|  | 210-0046-00 |  | 1 | LOCKWASHER, internal, $1 / 4 \mathrm{ID} \times 0.400$ inch OD |
|  | 210-0455-00 |  | 1 | NUT, hex., $1 / 4-28 \times 3 / 8$ inch |
| 104 | 358-0216-00 |  | 2 | BUSHING, gray |
| 105 | 260-0717-00 |  | 1 | SWITCH, push-RESET |
|  | - - - |  | - | mounting hardware: (not included w/switch) |
| 106 | 210-0012-00 |  | 1 | LOCKWASHER, internal, $3 / 8$ ID $\times 1 / 2$ inch OD |
| 107 | 210-0978-00 |  | 1 | WASHER, flat, $3 / 8$ ID $\times 1 / 2$ inch OD |
| 108 | 210-0590-00 |  | 1 | NUT, hex., 3/8-32 $\times 7 / 16$ inch |
| 109 260-0688-00 |  |  | 1 | SWITCH, push-TRACE FINDER mounting hardware: (not included w/switch) LOCKWASHER, internal, $1 / 4$ ID $\times 15 / 32$ inch OD WASHER, flat, $1 / 4$ ID $\times 3 / 8$ inch OD NUT, hex., $1 / 4-32 \times 5 / 16$ inch |
|  | - |  | - |  |
| 110 | 210-0011-00 |  | 1 |  |
| 111 | 210-0940-00 |  | 1 |  |
| 112 | 210-0583-00 |  | 2 |  |
| 113 | 200-0608-00 |  | 1 | COVER, variable resistor FILTER, mesh (See Standard Accessories Page) |



| Index No. | Tektronix Part No. | Serial/Madel Eff No. Disc | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \\ & \hline \end{aligned}$ | $22345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 141 | 211-0598-00 |  | 1 | SCREW, captive, $6-32 \times 3 / 8$ inch, FHS |
| 142 | 210-0869-00 |  | 1 | WASHER, plastic, $5 / 32$ ID $\times 3 / 8$ inch OD |
| 143 | 354-0163-00 |  | 1 | RING, retaining |
| 144 | 214-0573-00 |  | 1 | PIN, hinge |
| 145 | 210-0805-00 |  | 1 | WASHER, flat, 0.204 ID $\times 0.438$ inch OD |
| 146 | 354-0165-00 |  | 1 | RING, retaining |
| 147 | 179-0996-01 |  | 1 | CABLE HARNESS, main |
| 148 | 131-0371-00 |  | 12 | cable harness includes: CONNECTOR, single contact, female |


| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { No. }}{\text { No }}$ | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 644-0413-01 |  | 1 | ASSEMBLY, attenuator preamplifier assembly includes: CONNECTOR, coaxial, 1 contact, BNC, female w/mounting hardware mounting hardware for each: (not included w/connector) SPACER, BNC connector |
|  | . . . - |  | - |  |
|  | 131-0352-00 |  | 2 |  |
|  |  |  |  |  |
| 2 | -- - |  |  |  |
|  | 166-0402-00 |  | 1 |  |
| 3 | 644-0412-01 |  | 2 | ASSEMBLY, attenuator switch and chassis (CH $1 \& \mathrm{CH}$ 2) each assembly includes: |
|  | - . - |  |  |  |
|  | 262-0728-01 |  | 1 | SWITCH, wired-VOLTS/DIV |
|  | - - - - |  |  | switch includes: |
|  | 260-0720-01 |  | 1 | SWITCH, unwired |
| 4 | 214.0599-00 |  | 2 | SPRING, switch shaft ground |
| 5 | ...... |  | 2 | RESISTOR, variable forl |
|  | - |  |  | mounting hardware for each: (not included w/resistor) |
| 6 | 210-0223-00 |  | 1 | LUG, solder, $1 / 4 \mathrm{ID} \times 7 / 16$ inch OD, SE |
| 7 | 210-0046-00 |  | 1 | LOCKWASHER, internal, $1 / 4 \mathrm{ID} \times 0.400$ inch OD |
| 8 | 210-0583-00 |  | 1 | NUT, hex., $1 / 4-32 \times 5 / 16$ inch |
| 9 | 386-1284-00 |  | 1 | PLATE, mounting, plastic |
|  | - -. - . |  |  | mounting hardware: (not included w/plate) |
|  | 210-0053-00 |  | 2 | LOCKWASHER, split, \#2 (not shown) |
|  | 210-0405-00 |  | 2 | NUT, hex., $2-56 \times 3 / 16$ inch (not shown) |
| 10 | $131-0157-00$ |  | 1 |  |
|  | 610-0473-01 |  | 1 | ASSEMBLY, attenuator chassis |
|  | - - - - |  |  | assembly includes: |
| 11 | 131-0180-00 |  | 1 | CONNECTOR, terminal |
|  | - - - |  |  | mounting hardware: (not included w/connector) |
|  | 358-0135-00 |  | 1 | BUSHING, plastic (not shown) |
| 12. | 260-0621-00 |  | 1 | SWITCH, lever-AC GND DC |
|  | $\because-\cdot$ |  | - | mounting hardware: (not included w/switch) |
|  | 211-0105-00 |  | 2 | SCREW, 4-40 $\times 3 / 16$ inch, $100^{\circ}$ csk, FHS (not shown) |
|  | 210-0004-00 |  | 2 | LOCKWASHER, internal, \#4 (not shown) |
|  | 210-0406-00 |  | 2 | NUT, hex., 4-40 $\times 3 / 16$ inch (not shown) |
| 13 | 214-0456-00 |  | 5 | FASTENER, press, plastic CHASSIS, attenuator |
| 14 | 441-0639-00 |  | 1 |  |
| 15 | 378-0541-00 |  | 2 | FILTER, lens, clear |
| 16. | 352-0067-00 |  | 2 | HOLDER, neon, single |
|  | - --- |  |  | mounting harware for each: (not included w/holder) |
| 17 | 211 -0109-00 |  | 1 | SCREW, 4-40 $\times 7 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
|  | 210-0406-00 |  | 2 | NUT, hex., 4-40 $3 / 16$ inch (not shown) |
| 18 | $\cdots$ |  | 2 | RESISTOR, variable mounting hardware: (not included w/resistor) NUT, hex., $1 / 4-32 \times 5 / 16$ inch |
|  | 210-0583-00 |  |  |  |
| 19 | 210-0583-00 |  | 1 |  |

FIGURE FO-2. ATIENUATOR PREAMPUFIER ASSEMBLY (cont)


| Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Nisc }}{\text { No. }}$ | Q t y | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 43 | 131-0235-00 |  |  | 2 | CONNECTOR, terminal mounting hardware for each: (not included w/connector) BUSHING, plastic (not shown) |
|  | - . . |  |  |  |  |
|  | 358.0135.00 |  |  | 1 |  |
| 44 | 136.0235.01 |  |  | 2 | SOCKET, diode, 6 contact, plastic SOCKET, diode, 6 contact |
| 45 | 136.0235.00 |  |  | 2 |  |
| 46 | 136-0183-00 |  |  | 2 | SOCKET, transistor, 3 pin |
| 47 | 136-0220-00 |  |  | 14 | SOCKET, transistor, 3 pin |
| 48 | 136-0261-00 |  |  | 6 | SOCKET, connector pin |
| 49 | 200-0642-00 |  |  | 1 | CAP |
|  | - - - |  |  |  | mounting hardware: (not included w/assembly) |
| 50211.0116 .00 |  |  |  | 5 | SCREW, sems, $4-40 \times 5 / 16$ inch, PHB |
| 5152 | 343-0088-00 |  |  | 1 | CLAMP, cable |
|  | 179.0992-01 |  |  | 1 | CABLE HARNESS, vertical preamp |
|  | - --- |  |  |  | cable harness includes: |
| 53131-0371-00 |  |  |  | 11 | CONNECTOR, single contact, female |
| 54 | 210-0012-00 |  |  | 2 |  |
| 55 | 210-0590-00 |  |  | 2 | NUT, hex., $3 / 8-32 \times 7 / 16$ inch |
| 56. |  |  |  | 2 | RESISTOR, variable mounting hardware for each: (not included w/resistor) |
|  | 21 -0-0223-00 |  |  |  |  |
| 57 | 210-0016-00 |  |  | 1 | LOCKWASHER, split, $1 / 4$ inch ID |
| 58 | 220-0440-00 |  |  | 1 | NUT, hex., $1 / 4-32 \times 13 / 32$ inch |
|  | - - - - |  |  |  | mounting hardware: (not included w/atten preamp assembly) |
|  | 211-0116-00 |  |  | 3 | SCREW, sems, $4-40 \times 5 / 16$ inch, PHB (not shown) |
|  | 210-1001-00 |  |  | 3 | WASHER, flat, 0.119 ID $\times 3 / 8$ inch OD (not shown) |
|  | 210-0457-00 |  |  | 4 | NUT, keps, 6-32 $5 / 16$ inch (not shown) |
| 59 | 337-0767.00 | 20000 | 23849 | 1 |  |
|  | 337-0767.04 | 23850 |  | 1 | SHIELD, attenuator |
|  | ---.-- |  |  | 5 | mounting hardware: (not included w/shield) SCREW $4-40 \times 3 / 16$ inch, PHS (not shown) |

FIGURE FO-3 CRT SHIELD

| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Dise | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 337-0754-00 |  | 1 | SHIELD, CRT |
| 2 | 337-0954-01 |  | 1 | SHIELD, CRT (outer) |
| 3 | 348-0070-01 |  | 4 | CUSHION, CRT |
| 4 | 331.0141-00 |  | 1 | MASK, graticule |
| 5 | -•••• |  | 1 | COIL mounting hardware: (not included w/coil) |
| 6 | 211-0590-00 |  | 2 | SCREW, $6-32 \times 1 / 4$ inch, PHS |
| 7 | 211.0589 .00 |  | 1 | SCREW, $6.32 \times 0.312$ inch, PHS |
| 8 | 210-0863-00 |  | 1 | WASHER, D shape, 0.191 ID $\times 33 / 64 \times 33 / 64$ inch long |
| 9 | 343-0042-00 |  | 1 | CLAMP, cable, plastic, 5/16 inch (half) |
| 10 | 343-0131-00 |  | 1 | CLAMP, coil form mounting hardware: (not |
| 11 | 211-0590-00 |  | 2 | SCREW, 6-32 $\times 1 / 4$ inch, PHS |
| 12 | 210.0006-00 |  | 2 | LOCKWASHER, internal, \#6 |
| 13 | 210-0407-00 |  | 2 | NUT, hex., $6.32 \times 1 / 4$ inch |
| 14 | 358-0281-00 |  | 1 | BUSHING |
| 15 | 343-0124-00 |  | 1 | CLAMP, retainer |
|  | -..-. |  | - | mounting hardware: (not included w/clamp) |
| 16 | 211.0599.00 |  | 2 | SCREW, $6.32 \times 3 / 4$ inch, FIL HS |
| 17 | 220-0444-00 |  | 2 | NUT, square, $6.32 \times 1 / 4$ inch |
| 18 | 352-0091.01 |  | 2 | HOLDER, CRT retainer |
|  | -- |  | - | mounting hardware for each: (not included w/holder) |
| 19 | 211-0590-00 |  | 2 | SCREW, $6.32 \times 1 / 4$ inch, PHS |
| 20 | 343-0123-01 |  | 2 | CLAMP, CRT retainer |
| 21 | 220-0444-00 |  | 1 | NUT, square, $6-32 \times 1 / 4$ inch |
| 22 | $211-0600-00$ |  | 1 | SCREW, 6-32 $\times 2$ inches. FIL HS |
| 23 | 343-0122-01 |  | 2 | CLAMP |
|  | 213-0049-00 |  | 2 | SCREW, 6-32 $\times 5 / 16$ inch HHS (not shown) |
| 24 | 210-0949-00 |  | 2 | WASHER, flat, $9 / 64$ ID $\times 1 / 2$ inch OD |
| 25 | 211-0510-00 |  | 2 | SCREW, 6-32 $\times 3 / 8$ inch, PHS |
| 26 | 136-0205-00 |  | 2 |  |
| 27 | 210-0586-00 |  | 1 | mounting hardware for each: (not included w/socket) NUT, keps, $4-40 \times 1 / 4$ inch |
| 28 | 175-0582-00 |  | 1 | WIRE, CRT lead |
|  | 175-0583-00 |  | 1 | WIRE, CRT lead |
|  | 175.0584-00 |  | 1 | WIRE, CRT lead |
|  | 175-0596-00 |  | 1 | WIRE, CRT lead |
|  | ---- |  |  | each wire includes: |
| 29 | 131-0049-00 |  | 1 | CONNECTOR, single contact, female |
| 30 | 179-1001-00 |  | 1 | CABLE HARNESS, graticule lights |
| 31 | 179-0997-02 |  | 1 | CABLE HARNESS, anode |
| 32 | 131-0371-00 |  | 9 | cable harness includes: CONNECTOR, single contact, female |



FIGURE FO-4. A \& B SWEEPS

| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { No. }}{\text { Nisc }}$ | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 386-1268-00 |  | 1 | SUPPORT, chassis |
| 2 | 214-0317-00 |  | 2 | HEAT SINK |
| 3 | 210-0627-00 |  | 2 | RIVET, heat sink |
| 4 | 343-0097-00 |  | 2 | CLAMP, heat sink |
| 5 | 352-0062-00 |  | 2 | HOLDER, heat sink |
|  | -. - |  | - | mounting hardware for each: (not included w/holder) |
| 6 | 211-0033-00 |  | 2 | SCREW, sems, $4-40 \times 5 / 16$ inch, PHS |
| 7 | 211-0012-00 |  | 2 | SCREW, $4-40 \times 3 / 8$ inch, PHS |
| 8 | 210-0004-00 |  | 4 | LOCKKWASHER, internal, \#4 |
| 9 | 214-0368-00 |  | 1 | SPRING, heat sink |
| 10 | 210-0599-00 |  | 2 | NUT, sleeve |
| 11 | 670-0418-02 |  | 1 | ASSEMBLY, circuit board-B Sweep assembly includes: <br> BOARD, circuit |
|  | - - - |  |  |  |
|  | 388-0645-02 |  | 1 |  |
| 12 | 136-0220-00 |  | 24 | SOCKET, transistor, 3 pin |
| 13 | 136-0235-00 |  | 1 | SOCKET, transistor, 6 pin |
| 14 | 214-0506-00 |  | 49 | PIN, connector |
| 15 | 214-0579-00 |  | 7 | PIN, test point |
| 16 | 214-0565-00 |  | 1 | FASTENER, pin dress |
| 17 | 344-0119-00 |  | 6 | CLIP, electrical |
| 18 | 210-1014-00 |  | 1 | WASHER, plastic, 0.094 ID $\times 5 / 16$ inch, PHB |
| 19 | 337-0763-00 |  | 1 | SHIELD |
|  | - . . . - |  |  | mounting hardware: (not included w/assembly) SCREW, sems, $4-40 \times 5 / 16$ inch, PHB |
| 20 | 211-0116-00 |  | 6 |  |
| 212223 | 343-0089-00 |  | 7 | CLAMP, cable, plastic, large CLAMP, cable, plastic, small BRACKET capacitor mounting mounting hardware: (not included w/bracket) SCREW, 6-32 $\times 1 / 4$ inch, PHS |
|  | 343-0088-00 |  | 2 |  |
|  | 407-0144-00 |  | 1 |  |
|  | $\cdots{ }^{-}$ |  | - |  |
| 24 | 211-0504-00 |  | 4 |  |
| 25 | 344-0116-00 |  | 1 | CLIP, capacitor mounting mounting hardware: (not included w/clip) SCREW, $4-40 \times 3 / 16$ inch, PHS NUT, keps, $4-40 \times 1 / 4$ inch (not shown) |
|  | - - - - |  | - |  |
| 26 | 211-0007-00 |  | 1 |  |
|  | 210-0586-00 |  | 1 |  |
| 27 | 200-0255-00 |  | 2 | COVER, capacitor, 1 inch diameter $\times 31 / 32$ inches long COVER, capacitor, 1 inch diameter $\times 21 / 32$ inches long CAPACITOR mounting hardware for each: (not included w/capacitor) |
| 28 | 200-0257-00 |  | 2 |  |
| 29 | . . - |  | 4 |  |
|  | - - - |  |  |  |
| 30 | 211-0534-00 |  | 2 | SCREW, sems, $6.32 \times 5 / 16$ inch, PHS |
| 31 | 386-0252-00 |  | 1 | PLATE, fiber, small |
| . 32 | 210-0006-00 |  | 2 | LOCKKWASHER, internal, \#6 |
|  | 210-0407-00 |  | 2 | NUT, hex., $6.32 \times 1 / 4$ inch |



FIGURE FO-5. HIGH VOLTAGE ASSEMBLY

| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Dise | Q t y | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
|  | 621-0424-01 |  | 1 | ASSEMBLY, high voltage assembly includes: |
|  | - . . |  | - |  |
| 1 | 380-0077-00 |  | 1 | HOUSING, plastic |
| 2 | 179-0988-01 |  | 1 | CABLE HARNESS |
| 3 | 381-0243-00 |  | 1 | BAR, heat sink |
| 4 | 392-0169-00 |  | 1 | BOARD, high voltage, plastic board includes: |
|  | - - - - |  |  |  |
| 5 | 124-0176-00 |  | 1 |  |
|  | 124.0175-00 |  | 1 | STRIP, ceramic, $7 / 16$ inch $h$, w/2 notches mounting hardware: (not included w/board) |
|  | - - - |  |  |  |
| 7 | 211-0036-00 |  | 1 | SCREW, 4-40 $41 / 2$ inch, BH plastic |
| 8 | 392-0170-00 |  | 1 BOARD, high voltage, plastic board includes: | BOARD, high voltage, plastic board includes: |
|  | - - - |  |  |  |
| 9 | 124-0163-00 |  | 8 | STRIP, ceramic, 2 notches |
| 10 | 124.0164-00 |  | 4 | STRIP, ceramic, 4 notches |
| 11 | 131-0227-00 |  | 1 | CONNECTOR, terminal stand off |
|  | 131-0359-00 |  | 1 | CONNECTOR, terminal feed thru |
| 12 | 358-0176-00 |  | 2 | BUSHING, plastic (not shown) |
| $13$ | 210-0966-00 |  | 3 |  |
|  | - - - - - |  | 1 | RESISTOR, variable |
| 14 | $\cdots$ |  | 1 | mounting hardware: (not included w/resistor) |
|  | 210-0046-00 |  | 1 | LOCKWASHER, internal, $1 / 41 D \times 0.400$ inch OD |
| 15 | 210-0583-00 |  | 1 | NUT, hex., $1 / 4.32 \times 5 / 16$ inch $\times 0.400$ inch |
| 16 | 346-0032-00 |  | 4 | STRAP, rubber TRANSFORMER |
|  | -•• |  | 1 |  |
|  | - - . - |  | - | mounting hardware: (not included w/transformer) |
| 18 | 211-0552-00 |  | 2 | SCREW, 6-32 2 2 inches, PHS |
| 19 | 210.0869-00 |  | 2 | WASHER, plastic, $5 / 32$ ID $\times 3 / 8$ inch OD |
| 20 | 358-0231-00 |  | 4 | BUSHING, rubber |
| 21 | 200-0620-00 |  | 1 | COVER, plastic, high voltage supply mounting hardware: (not included (w/cover) SCREW, 6-32 $\times 2$ inches, PHS |
|  | - . . . |  | - |  |
| 22 | 211-0552-00 |  | 2 |  |
| 23 | $\begin{gathered} 337-0752-00 \\ 211-0503-00 \end{gathered}$ |  | $\begin{aligned} & 1 \\ & 3 \end{aligned}$ | SHIELD, high voltage supply mounting hardware: (not included $w /$ shield) SCREW, 6-32 $\times 3 / 16$ inch, PHS (not shown) |
|  |  |  |  |  |
|  |  |  |  |  |


| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\substack{\text { Serial/Model } \\ \text { No. } \\ \text { Disc }}}$ | $\begin{aligned} & Q \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 441-0719-00 |  | 1 | CHASSIS, rear |
| 2 | $\begin{aligned} & 211-0504-00 \\ & 635-0433-00 \end{aligned}$ |  | 2 | SCREW, $6-32 \times 1 / 4$ inch, PHS ASSEMBLY, fan |
| 3 | - ---- |  | 1 | assembly includes: IMPELLER, fan, axial |
|  | 213-0126-00 |  | 1 | impeller includes: <br> SCREW, set, $6.32 \times 0.250$ inch, HSS |
| 4 | 407-0308-01 |  | 1 | BRACKET, fan motor |
| 5 | 147-0027-00 |  | 1 | MOTOR, fan mounting hardware: (not included w/motor) |
| 6 | 211-0008-00 |  | 3 | SCREW, $4-40 \times 1 / 4$ inch, PHS |
| 7 | 210-0054-00 |  | 3 | LOCKWASHER, \#4 split |
|  | - - . |  |  | mounting hardware: (not included w/assembly) |
| 8 | 211-0012-00 |  | 3 | SCREW, $4-40 \times 3 / 8$ inch, PHS |
| 9 | 210-0851-00 |  | 6 | WASHER, flat, 0.119 ID $\times 3 / 8$ inch OD |
| 10 | 348-0093-00 |  | 3 | GROMMET, rubber, shock mount, $0.140 \mathrm{ID} \times 0.375$ inch OD |
| 11 | 220-0471-00 |  | 3 | NUT, stepped, round, $4-40 \times 0.217$ inch long |
| 12 | 380-0114-00 |  | 1 | HOUSING, air flow |
| 13 | - . . |  | 1 | SWITCH, thermostatic |
|  | --- - |  |  | mounting hardware: not included w/switch] |
| 14 | 213-0044-00 |  | 2 | SCREW, thread cutting, 5-32 $\times 3 / 16$ inch, PHS |
| 15 | -••••• |  | 3 | TRANSISTOR |
|  | - - - |  | - | mounting hardware for each: (not included w/transistor) |
| 16 | 211-0510-00 |  | 2 | SCREW, $6.32 \times 3 / 8$ inch, PHS |
| 17 | 387-0345-00 |  | 1 | PLATE, insulator |
| 19 | 210-0802-00 |  | 2 | WASHER, fiber, shouldered, \#6 |
| 18 | 210-0811-00 |  | 2 | WASHER, flat, 0.150 ID $\times 5 / 16$ inch OD |
| 20 | 210-0202-00 |  | 1 | LUG, solder, SE \#6 |
| 21 | 210-0006-00 |  | 1 | LOCKWASHER, internal, \#6 |
| 22 | 210-0407-00 |  | 2 | NUT, hex., $6-32 \times 1 / 4$ inch |
| 23 | - |  | 1 | RESISTOR, variable |
|  | - |  | - | mounting hardware: (not included w/resistor) |
|  | $210.0223-00$ |  | 1 | LUG, solder, $1 / 4$ ID $\times 7 / 16$ inch OD, SE |
| 24 | 210-0940-00 |  | 1 | WASHER, flat, $1 / 4$ ID $\times 3 / 8$ inch OD |
| 25 | 210-0583-00 |  | 1 | NUT, hex., $1 / 4-32 \times 5 / 16$ inch |
| 26 | 352-0031-00 |  | 1 | HOLDER, fuse single |
|  | . . . . . - |  |  | mounting hardware: (not included w/holder) |
| 27 | 211-0507-00 |  | 1 | SCREW, $6-32 \times 5 / 16$ inch, PHS |
| 28 | 358-0215-00 |  | 2 | BUSHING, plastic |

FIGURE FO-6. REAR CHASSIS (cont)

| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \quad$No. <br> Disc | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 29 | 214-0210.00 |  | 1 | ASSEMBLY, solder spool <br> assembly includes: <br> SPOOL, solder <br> mounting hardware: (not included w/assembly) <br> SPACER, plastic, 0.156 inch long |
|  | - . . . |  | - |  |
|  | 214-0209-00 |  | 1 |  |
|  | . . . . - |  |  |  |
|  | 361.0007-00 |  | 1 |  |
| 30 | 124-0147-00 |  | 1 | STRIP, ceramic, $7 / 16$ inch $h, w / 13$ notches strip includes: <br> STUD, plastic <br> mounting hardware: (not included w/strip) SPACER, plastic, 0.156 inch long |
|  | - - - |  | 2 |  |
|  | 355-0046-00 |  | 2 |  |
|  | - - . - |  | $\dot{\square}$ |  |
|  | 361-0007-00 |  |  |  |
| 31 | 124-0145-00 |  |  | STRIP, ceramic, $7 / 16$ inch $h, w / 20$ notches each strip includes: <br> STUD, plastic mounting hardware for each: (not included w/strip) SPACER, plastic, 0.156 inch long |
|  | .-. - |  | - |  |
|  | 355-0046-00 |  | 2 |  |
|  |  |  | - |  |
|  | 361-0007-00 |  |  |  |
| 32 | 210-0202-00 |  | 1 | LUG, solder, SE \#6 mounting hardware: (not included w/lug) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
|  | . - . . - |  | , |  |
| 33 | 213-0044-00 |  | 1 |  |
| 34 | 348-0063-00 |  |  | GROMMET, plastic, $1 / 2$ inch GROMMET, plastic, $5 / 8$ inch BRACKET, regulator mounting hardware: (not included w/bracket) SCREW, 6-32 $\times 1 / 4$ inch, PHS - |
| 35 | 348-0064-00 |  | 2 |  |
| 36 |  |  | 1 |  |
|  | $\ldots$ |  | - |  |
|  | 211-0504-00 |  | 4 |  |
| 37 | 348-0056-00 |  | 1 | GROMMET, plastic, 0.354 ID $\times 0.406$ inch OD RESISTOR <br> mounting hardware for each: (not included w/resistor) |
| 38 | ...... |  | 2 |  |
|  | - - . - |  |  |  |
| $\begin{aligned} & 39 \\ & 40 \end{aligned}$ | 211-0507-00 |  | 1 | mounting hardware for each: (not included w/resistor) SCREW, $6-32 \times 5 / 18$ inch, PHS <br> NUT, hex., $5 / 16 \times 21 / 32$ inch long <br> EYELET <br> SCREW, $6.32 \times 1 \frac{1}{2}$ inch, RHS |
|  | 210-0478-00 |  | 1 |  |
|  | 210-0601-00 |  | 1 |  |
|  | 211-0553-00 |  | 1 |  |
| 41 | 214-0289-00 |  | 2 | HEAT SINK, transistor mounting hardware for each: (not included w/heat sink) NUT, keps, $10-32 \times 3 / 8$ inch |
|  | $220-0410-00$ |  | 1 |  |
| 42 | 179-0991-01 |  | 1 | CABLE HARNESS, regulator bracket |
| 43 | 124-0147-00 |  | 1 | STRIP, ceramic, $7 / 16$ inch $h, w / 13$ notches |
|  | - - - |  | 2 | strip includes: |
|  | 355-0046-00 |  | 2 | STUD, plastic |
|  | - $361-0009.00$ |  | 2 | mounting hardware: (not included w/strip) SPACER, plastic, 0.406 inch long |
|  | 361-0009.00 |  | 2 | SPACER, plastic, 0.406 inch long |

FIGURE FO-6. REAR CHASSIS (cont)

| Index No. | Tektronix Part No. |  | $\underset{\text { Eff }}{\text { Serial/Model }} \quad$No. <br> Disc | $\begin{aligned} & Q \\ & t \\ & y \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 44 | 124-0119-00 |  |  | 1 | STRIP, ceramic, $7 / 16$ inch $h, w / 2$ notches strip includes: <br> STUD, plastic <br> mounting hardware: (not included w/strip) SPACER, plastic, 0.188 inch long |
|  | -. - . |  |  |  |  |
|  | 355-0046-00 |  |  | 1 |  |
|  | . . . . - |  |  |  |  |
|  | 316-0007-00 |  |  | 1 |  |
| 45 | -•- |  |  | 1 | TRANSISTOR <br> mounting hardware: (not included w/transistor) |
|  | - . . . - |  |  |  |  |
| 46 | 211-0510.00 |  |  | 2 | SCREW, $6.32 \times 3 / 8$ inch, PHSPLATE, mica insulator |
| 47 | 386-0143-00 |  |  | 1 |  |
|  | 210-0983-00 |  |  | 2 | PLATE, mica insulator WASHER, shouldered |
|  | 210-0802-00 |  |  | 2 | WASHER, flat, 0.150 ID $\times 5 / 16$ inch ODLUG, solder, SE \#6 |
| 49 | 210-0202-00 |  |  | 1 |  |
|  | 210-0006-00 |  |  | 1 | LOCKWASHER, internal, \#6 |
| 50 | 21 0-0407-00 |  |  | 2 | NUT, hex., $6.32 \times 1 / 4$ inch |
| 51 | 670-0415-00 |  |  |  | ASSEMBLY, circuit board-LLOW VOLTAGE REGULATOR assembly includes: |
|  | 388-0642-00 |  |  | 1 |  |
|  | -..... |  |  | - | BOARD, circuit |
|  | 388-0642.01 |  |  | 1 | board includes: <br> BOARD, circuit, w/o pins |
| 52 | 214-0506-00 |  |  | 21 | PIN, connector |
| 54. | 136-0183-00 |  |  | 4 | SOCKET, transistor, 3 pinSOCKET, transistor, 3 pin |
|  | 136-0220-00 |  |  | 4 |  |
|  | - --- |  |  | 3 | mounting hardware: (not included w/board) |
| $\begin{aligned} & 55 \\ & 56 \end{aligned}$ | 211 -0040-00 |  |  | 33 | SCREW, $4-40 \times 1 / 4$ inch, BH plastic INSULATOR, plastic |
|  | 214-0781-00 |  |  |  |  |
| 57 | 343-0088-00 |  |  | 6 CLAMP, cable, small CABLE HARNESS, low voltage regulator BRACKET, upper, vertical preamp board BRACKET, upper, vertical preamp board |  |
| 58 | 179-0987-02 |  |  |  |  |  |
| 59 | 407-0146-00 |  |  |  |  |  |
|  | 407-0147-00 |  |  |  |  |  |
| 61 | 670-0416-00 |  |  | 1 | CABLE HARNESS, low voltage regulator BRACKET, upper, vertical preamp board BRACKET, upper, vertical preamp board ASSEMBLY, circuit board-VERT OUTPUT AMP |
|  | -388-0643-01 |  |  |  |  |
|  |  |  |  | 1 | assembly includes: <br> BOARD, circuit |
| 62 | 214-0506-00 |  |  | 1 | PIN, connector |
| 63 <br> 64 | 136-0220-00 |  |  | 6 | SOCKET, transistor, 3 pin |
|  | 344-0119-00 |  |  | 4 | CLIP, electrical |
|  | ----- |  |  | 4 | mounting hardware: (not included w/assembly) SCREW, 4-40 $\times 5 / 16$ inch, PHS w/lockwasher |
| $65211-0116.00$ |  |  |  |  |  |
| 66 | . . . . . |  |  | 1 | TRANSFORMER mounting hardware: (not included w/transformer) |
|  |  |  |  |  |  |
| 67 | 212-0576-00 | $\begin{aligned} & 20000 \\ & 25610 \end{aligned}$ | 25609 | 4 | SCREW, $10.32 \times 13 / 8$ inches, HHS SCREW, $10-32 \times 1 \frac{1}{2}$ inches, RHS |
|  | 212-0553-00 |  |  |  |  |
| 68 | 220-0410.00 |  |  | 4 | NUT, keps, $10-32 \times 3 / \mathrm{s}$ inch |
| 69 | 407-0323-00 |  |  | 1 | BRACKET, transformer |
| 70 | 212-0004-00 |  |  | 4 | mounting hardware: (not included w/bracket) SCREW, 8 - $32 \times 5 / 16$ inch, PHS |


| .ndex No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Disc | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | 12345 Description |
| :---: | :---: | :---: | :---: | :---: |
| 71 | 352-0031-00 |  | 2 | HOLDER, fuse, single mounting hardware for each: (not included w/holder) |
|  | . . . . - |  | - |  |
| 72 | 211-0538-00 |  | 2 | SCREW, $6-32 \times 5 / 1{ }^{\text {a }}$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| 73 | 210-0006-00 |  | 2 | LOCKWASHER, internal, \#6 |
| 74 | 210-0407-00 |  | 2 | NUT, hex., $6.32 \times 1 / 4$ inch |
| 75 | $670-0414-04$ |  |  |  |
|  | $388-0641-02$ |  |  |  |
|  |  |  | $j$ | ASSEMBLY, circuit board-Z AXIS assembly includes: BOARD, circuit |
| 76 | 214-0506-00 |  | $2{ }^{1}$ | PIN, connector |
| 77 | 214-0579-00 |  | 34 | PIN, test point |
| 78 | 136-0183-00 |  |  | SOCKET, transistor, 3 pin |
| 79 | 136-0220-00 |  | 44- | SOCKET, transisior, 3 pin mounting hardware: (not included w/socket) |
|  | $211-0116-00$ |  |  |  |
| 80 |  |  | 3 | SCREW, sems, 4-40 $\times 5 / 16$ inch, PHB |
| 81 | $\begin{aligned} & 179-0995-02 \\ & ---0 \\ & 131-0371-00 \end{aligned}$ |  | 1 | CABLE HARNESS, A sweep cable harness includes: CONNECTOR, single contact, female |
|  |  |  | 37 |  |
| 8283848586 | 386-0202-01 |  | 1 | PLATE, center bulk head GROMMET, plastic, $5 / 8$ inch GROMMET, plastic, 0.354 ID $\times 0.406$ inch OD GROMMET, plastic, $1 / 4$ inch CONNECTOR, terminal, standoff mounting hardware: (not included w/connector) BUSHING, plastic |
|  | 348-0064-00 |  | 2 |  |
|  | 348-0056-00 |  | 2 |  |
|  | 348-0055-00 |  | 1 |  |
|  | 131-0181-00 |  |  |  |
|  | 358-0136-00 |  |  |  |
| 87 | $343-0002-00$ |  | 1111 | CLAMP, cable, $3 / 16$ inch mounting hardware: (not included w/clamp) SCREW, $6-32 \times 5 / 16$ inch, PHS WASHER, "D" type, 0.191 ID $\times 33 / 64 \times 33 / 64$ inch long NUT, keps, $6.32 \times 5 / 16$ inch |
|  |  |  |  |  |
| $\begin{aligned} & 88 \\ & 89 \\ & 90 \end{aligned}$ | 211-0507-00 |  |  |  |
|  | 210-0863-00 |  |  |  |
|  | 210-0457-00 |  |  |  |
| 91 | $\begin{gathered} 129-0069-00 \\ -361-0007-00 \end{gathered}$ |  | 31 | POST, terminal, tie off mounting hardware for each: (not included w/post) SPACER, plastic, 0.188 inch long |
|  |  |  |  |  |
|  |  |  |  |  |
| 92 | $\begin{aligned} & 210-0201-00 \\ & 213-0044-00 \end{aligned}$ |  | 1 | LUG, solder, SE \#4 mounting hardware: (not included w/lug) SCREW, thread forming, $5-32 \times 3 / 16$ inch, PHS |
|  |  |  |  |  |
| $\begin{aligned} & 93 \\ & 94 \end{aligned}$ | $\begin{aligned} & 214-0317-00 \\ & 352-0062-00 \\ & ---\cdots- \\ & 211-0033-00 \\ & 211-0012-00 \\ & 210-0004-00 \\ & 210-0406-00 \end{aligned}$ |  | 22-2244 | HEAT SINK <br> HOLDER, heat sink mounting hardware for each: (not included w/holder) SCREW, sems, $4-40 \times 5 / 16$ inch, PHS SCREW, $4-40 \times 3 / 8$ inch, PHS LOCKWASHER, internal, \#4 NUT, hex., 4-40 $\times 3 / 16$ inch |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |

## FIGURE FO-6. REAR CHASSIS (cont)

| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { Disc }}{\text { No. }}$ | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 95 | 343-0097-00 |  | 2 | CLAMP, heat sink |
| 96 | 214-0368-00 |  | 4 | SPRING, heat sink |
|  | 210-0627-00 |  | 2 | RIVET, heat sink (not shown) |
| 97 | 210-0599-00 |  | 4 | NUT, sleeve |
| 98 | 202-0142-01 |  | 1 | BOX, high voltage |
|  | - . |  |  | mounting hardware: (not included w/box) |
| 99 | 210-0504-00 |  | 6 | SCREW, $6.32 \times 1 / 4$ inch, PHS |
| 100 | 343-0013-00 |  | 3 | CLAMP, cable, $3 / 8$ inch |
|  | - - - - |  |  | mounting hardware for each: (not included w/clamp) |
| 101 | 211-0507-00 |  | 1 | SCREW, $6.32 \times 5 / 16$ inch, PHS |
| 102 | 210-0863-00 |  | 1 | WASHER, "D' type, $0.191 \times 33 / 64 \times 33 / 64$ inch long |
| 103 | 210-0473-00 |  | 1 | NUT, keps, 12 sided, $15 / 32-32 \times 0.634$ inch |
| 104 | -••••• |  | 1 | CAPACITOR |
|  | - . - |  | - | mounting hardware: (not included w/capacitor) |
|  | 211-0504-00 |  | 2 | SCREW, 6-32 $\times 1 / 4$ inch, PHS |
|  | 210-0006-00 |  | 2 | LOCKWASHER, internal, \#6 |
|  | 210-0407-00 |  | 2 | NUT, hex., $6.32 \times 1 / 4$ inch |
| 105 | 407-0145-00 |  | 1 | BRACKET, delay line |
|  | - - - - |  |  | bracket includes: |
| 106 | 358-0282-00 |  | 1 | BUSHING, insulating |
|  | - . - - |  | - | mounting hardware: (not included w/bracket) |
|  | 211-0097-00 |  | 3 | SCREW, 4-40 $\times 5 / 16$ inch |
|  | 210-0851.00 |  | 1 | WASHER, flat, $0.119 \mathrm{ID} \times 3 / 8$ inch OD |
|  | 210-0935-00 |  | 1 | WASHER, fiber, 0.140 ID $\times 0.375$ inch OD |
|  | 211-0507-00 |  | 1 | SCREW, $6.32 \times 5 / 16$ inch, PHS |
|  | 213-0049-00 |  | 1 | SCREW, $6.32 \times 5 / 16$ inch, HHS |
| 107 | 348-0055-00 |  | 2 | GROMMET, plastic, $1 / 4$ inch |


| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\substack{\text { Serial/Model } \\ \text { No. } \\ \text { Disc }}}$ | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| $)^{-1} 119-0029-00$, ASSEMBLY delay line |  |  |  |  |
|  |  |  | 1 | assembly includes: |
| 108 | 380-0049-00 |  | 1 | HOUSING, delay line |
| 109 | 200-0482-00 |  | 1 | COVER, delay line |
|  | -. - . - |  | - | mounting hardware: (not included w/cover) |
| 110 | 211-0513.00 |  | 4 | SCREW, $6-32 \times 5 / 8$ inch, PHS |
|  | 210-0407-00 |  | 4 | NUT, hex., $6.32 \times 1 / 4$ inch |
| 111 | 131-0272-00 |  | 1 | CONNECTOR, left hand mounting |
|  | - . . . - |  | - | mounting hardware: (not included w/connector) |
|  | $211-0097-00$ |  | 1 | SCREW, 4-40 5 5/16 inch, PHS |
|  | 210-0004-00 |  | 1 | LOCKWASHER, internal, \#4 |
| 112 | 21 0-0406-00 |  | 1 | NUT, hex., $4-40 \times 3 / 16$ inch |
| 113 | 131-0271-00 |  | 1 | CONNECTOR, right hand mounting |
|  | - . . . - |  | - | mounting hardware: (not included w/connector) |
|  | 211-0097-00 |  | 1 | SCREW, 4-40 x 5/16 inch, PHS |
|  | 210-0004-00 |  | 1 | LOCKWASHER, internal, \#4 |
|  | 210-0406-00 |  | 1 | NUT, hex., 4-40 $3 / 16$ inch |
| 114 |  |  | 2 |  |
|  | $131-0158-00$ |  | 2 | CONNECTOR, terminal, feed-thru |
| 115 | 211-0517-00 |  | 1 | SCREW, 6-32 $\times 1$ inch, PHS |
|  | 210-0407-00 |  | 1 | NUT, hex., $6-32 \times 1 / 4$ inch |
|  | - - . |  | , | mounting hardware: (not included w/assembly) |
|  | 210-0457-00 |  | 1 | NUT, keps, 6-32 5 5/16 inch |



FIGURE FO-7. CABINET \& FRAME

| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\text { Serial/Model }}$No. <br> Disc | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 31 | 129-0064-00 |  | 1 | POST, binding |
|  | - . - |  | - | mounting hardware: (not included w/post) |
| 32 | 358-0181-00 |  | 1 | BUSHING, plastic |
|  | 210-0203-00 |  | 1 | LUG, solder, SE \#6 long |
| 33 | 210-0457-00 |  | 1 | NUT, keps, $6.32 \times 5 / 16$ inch |
| 3435 | 346-0043-00 |  | 1 | STRAP, ground |
|  | 386-1187-00 |  | 1 | PLATE, rear panel |
|  | -... |  | - | mounting hardware: (not included w/plate) |
| 36 | 211-0565-00 |  | 4 | SCREW, $6.32 \times 1 / 4$ inch, THS |
| 37 | 386-1122-00 |  | 1 | PLATE |
|  | - -- - |  | - | mounting hardware: (not included w/plate) |
| 38 | 211.0504-00 |  | 2 | SCREW, 6-32 $\times 1 / 4$ inch, PHS |
| 394041 | 358-0323-00 |  | 1 | FASTENER, power cord |
|  | 161-0033-00 |  | 1 | CORD, power, 3 conductor |
|  | 204-0279-00 |  | 1 | BODY, line voltage selector |
|  | - - - |  |  | mounting hardware: (not included w/body) |
|  | 210-0006-00 |  | 2 | LOCKWASHER, internal, \#6 (not shown) |
|  | 210-0407-00 |  | 2 | NUT, hex., 6-32 $\times 1 / 4$ inch (not shown) |
| 42 | 200-0704-00 |  | 1 | COVER, line voltage selector |
|  | - - - - |  | 2 | cover includes: |
| 43 | 352-0102-00 |  | 2 | HOLDER, fuse, plastic <br> mounting hardware for each: (not included w/holder) |
| 44 | 213-0035-00 |  | 2 | SCREW, thread cutting, 4-40 $\times 1 / 4$ inch (not shown) |
| 45 | 378-0036-01 |  | 1 | FILTER, air |
| 46 | 380-0082-00 |  | 1 | HOUSING, fan filter |
|  | --.- |  | - | mounting hardware: (not included w/housing) |
| 47 | 213-0107-00 |  | 4 | SCREW, thread forming, 4-40 $\times 1 / 4$ inch, FHS |
| 48 | 179.1140-00 |  | 1 | CABLE HARNESS, w/connector, line voltage selector |
|  | 343-0004-00 |  | 1 | CLAMP, cable, plastic, $5 / 16$ inch diameter |
|  | -... |  | - | mounting hardware: (not included w/clamp) |
|  | 211-0510-00 |  | 1 | SCREW, $6.32 \times 3 / 8$ inch, PHS |
|  | 210-0863-00 |  | 1 | WASHER, "D" shape, 0.191 ID $\times 33 / 64 \times 33 / 64$ inch long |
| 50 | 210-0457-00 |  | 1 | NUT, keps, $6-32 \times 5 / 16$ inch |


| Index No. | Tektronix Pari No. | $\underset{\text { Eff }}{\text { Serial/Model }} \underset{\text { No. }}{\text { Nisc }}$ | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \\ & \hline \end{aligned}$ | $12345 \quad$ Description |
| :---: | :---: | :---: | :---: | :---: |
| 1 | - . - - |  | 1 | TYPE 453 OSCILLOSCOPE |
| 2 | 426-0297-00 |  | 1 | FRAME, front |
| 3 | 386-1059-00 |  | 1 | PLATE, shield |
|  | - . . |  |  | mounting hardware: (not included w/plate) |
| 4 | 211-0503-00 |  | 3 | SCREW, 6-32 $\times 3 / 16$ inch, PHS |
| 5 | 386-1063-00 |  | 1 | PLATE, front frame backing, top |
|  | -- |  |  | mounting hardware: (not included w/plate) |
| 6 | 212-0002-00 |  | 1 | SCREW, $8.32 \times 1 / 4$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| 7 | 386-1062-00 |  | 1 |  |
|  | --- |  |  | mounting hardware: (not included w/plate) |
| 8 | 212-0002-00 |  | 1 | SCREW, $8-32 \times 1 / 4$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| 9 | 200-0668-00 |  | 1 | COVER, bottom |
|  |  |  |  | mounting hardware: (not included w/cover) |
| 10 | $\begin{aligned} & 212-0001-00 \\ & 211-0502-00 \end{aligned}$ |  | 2 | SCREW, $8-32 \times 1 / 4$ inch, PHS <br> SCREW, $6.32 \times 3 / 16$ inch $100^{\circ}$ csk FHS (not shown) |
| 11 | 200-0667-00 |  | 1 | COVER, top |
|  | - - - |  | - | mounting hardware: (not included w/cover) |
| 1213 | 212.0001-00 |  | 2 | SCREW, $8.32 \times 1 / 4$ inch, PHS |
|  | 211-0502-00 |  | 1 | SCREW, 6-32 $\times 3 / 16$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| 14 | 386-1064-00 |  | 1 | PLATE, side |
|  | --- - |  |  | mounting hardware: (not included w/plate) |
| 15 | 212-0043-00 |  | 4 | SCREW, $8-32 \times 1 / 2$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| 16 | 212-0040-00 |  | 1 | SCREW, $8-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| 17 | 212-0023-00 |  | 1 | SCREW, $8-32 \times 3 / 8$ inch, PHS |
| 18 | 210-0458-00 |  | 6 | NUT, keps, $8-32 \times 11 / 32$ inch |
| 1920 | 351-0104-00 |  | 1 | GUIDE, w/mounting hardware (pair) |
|  | 426-0291-02 |  | 1 | FRAME, support, right |
|  | 212-0040-00 |  | 4 | mounting hardware: (not included w/frame) SCREW, $8-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |
| 22. | 426-0291-01 |  | 1 | FRAME, support, left |
|  | ---- |  |  | mounting hardware: (not included w/frame) |
| 23 | 21 2-0040-00 |  | 4 | SCREW, $8-32 \times 3 / 8$ inch, $100^{\circ} \mathrm{csk}$, FHS |


| Index No. | Tektronix Part No. | $\underset{\text { Eff }}{\substack{\text { Serial/ Model } \\ \text { No. } \\ \text { Dise }}}$ | $\begin{aligned} & \mathbf{Q} \\ & \mathbf{t} \\ & \mathbf{y} \end{aligned}$ | 12345 Description |
| :---: | :---: | :---: | :---: | :---: |
| 24 | 213-0129-00 |  | 4 | SCREW, $1 / 4-20 \times 3 / 4$ inch, HSS |
| 25 | 361-0120-00 |  | 2 | SPACER, stepped |
| 26 | 386-1061-00 |  | 1 | PLATE, hinge |
|  | - - - - |  |  | mounting hardware: (not included w/plate) |
| 27 | 211 -0503-00 |  | 3 | SCREW, 6-32 $\times 3 / 16$ inch, PHS |
| 28 | 358-0215-00 |  | 1 | BUSHING, black plastic |
| 29 | 211-0507-00 |  | 1 | SCREW, 6-32 $\times 5 / 16$ inch, PHS |
| 30 | 134-0067-00 |  | 4 | PLUG, gray plastic |
| 31 | 386-1261-00 |  | 1 | PLATE, rear |
| 32 | 212-0010-00 |  | 4 | SCREW, $8.32 \times 5 / 8 \mathrm{inch}$, PHS |
| 33 | 210-0808-00 |  | 1 | WASHER, centering |
|  | - - - . |  | - | mounting hardware: (not included w/washer) |
|  | 211 -0507-00 |  | 1 | SCREW, $6-32 \times 5 / 16$ inch, PHS |
| 35 | 210-0457-00 |  | 1 | NUT, keps, $6.32 \times 5 / 16$ inch |
| 36 | 386-1066-00 |  | 2 | PLATE, pin retaining |
|  | - . . - |  | - | mounting hardware for each: (not included w/plate) |
| 37 | 212-0008-00 |  | 2 | SCREW, 8-32 $\times 1 / 2$ inch, PHS |
| 38 | 367-0022-00 |  | 2 | HANDLE |
|  | - . . . |  | - | mounting hardware for each: (not included w/handle) |
| 39 | 213-0090-00 |  | 2 | SCREW, 10-32 $\times 1 / 4$ inch, HHS |

## SECTION <br> 9

## DIAGRAMS

This section consists of the following fold-out diagrams fapplicable to equipments serial-numbered 20,000 and $u p)$ located at the back of the text.


## RACKMOUNTING

## Introduction

The Tektronix Type R453 Oscilloscope is designed to mount in a standard 19-inch rack. When mounted in accordance with the following mounting procedure this instrument will meet all electrical and environmental characteristics given in Section 1] of this manual.

## Rack Dimensions

Height. At least seven inches of vertical space is required to mount this instrument in a rack.

Width. Minimum width of the opening between the left and right front rails of the rack must be $175 / 8$ inches. This allows room on each side of the instrument for the slide-out tracks to operate freely, permitting the instrument to move smoothly in and out of the rack.

Depth. Total depth necessary to mount the Type R453 in a cabinet rack is 18 inches. This allows room for air circulation, power cord connections and the necessary mounting hardware.

## Slide-out Tracks

Fig. 10-1 shows the Type R453 installed in a cabinet-type rack. The slide-out tracks provided with the Type R453 permit it to be extended out of the rack for maintenance or calibration without removing the instrument from the rack. In the fully extended position, the Type R453 can be tilted up so the bottom of the instrument can be reached for maintenance or calibration. To operate the Type R453 in the extended position, be sure the power cord and any interconnecting cables are long enough for this purpase. When not extended, the instrument is held in the rack with four sec uring screws (se Fiq. 10-1A).

The slide-out tracks consist of two assemblies-one for the left side of the instrument and one for the right side Fig. 10-2 shows the complete slide-out track assemblies. The stationary section of each assembly attaches to the front and rear rails of the rack, and the chassis section is attached to the instrument. The intermediate sectian slides between the stationary and chassis sections and allows the Type R453 to be extended out of the rack. When the instrument is shipped, the stationary and intermediate sections of the tracks are packaged as matched sets and should not be separated. Ta identify the left or right assembly, note the position of the automatic latch (sele Fig. 10-2). When mounted in the rack, the automatic latch should be at the top of both assemblies. The chassis sections are installed on the instrument at the factory.

The hardware needed to mount the slide-out tracks is shown in Fig. 10-3. Since the hardware supplied is intended to make the tracks compatible with a variety of cabinet racks and installation methods, not all of it will be needed for this
installation. Use only the hardware that is required for the mounting method used.

## Mounting Procedure

The following mounting procedure uses the rear support kit (se Fig. 10-4 and 10-7] to meet the environmental characteristics of the instrument (shock and vibration). Two alternative mounting methods are described at the end of this procedure. However, when mounted according to these altemative methods, the instrument may not meet the given environmental characteristics for shock and vibration.

The mounting flanges of the stationary sections may be mounted in front of or behind the front rails of the rack, depending on the type of rack. If the front rails of the rack are tapped for 10-32 screws, the mounting flanges are placed in front of the rails. If the front rails of the rack are not tapped for 10-32 screws, the mounting flanges are placed behind the front rail and a bar nut is used Fig. 10-5 shows these methods of mounting the stationary sections.
The rear of the stationary sections must be firmly supported to provide a shock-mounted installation. This rear support must be located 17.471 inches, $\pm 0.031$ inches, from the outside surface of the front rail when the mounting flange is mounted outside of the rail, or 17.531 inches, $\pm 0.031$ inches, from the rear surface of the front rail when the mounting flange is mounted behind the front rail. If the cabinet rack does not have a strong supporting member located the correct distance from the front rail, an additional support must be added. The instrument will not meet the environmental specifications unless firmly supported at this point. Fig. 10-4 illustrates a typical rear installation using the rear support kit and gives the necessary dimensions.

Use the following procedure to install the Type R453 in a rack:

1. Select the proper front-rail mounting holes for the stationary sections using the measurements shown ir Fig. 10-6

2a. If the mounting flanges of the stationary sections are to be mounted in front of the front rails (rails tapped for 10-32 screws), mount each stationary section as shown in Fig. 10-5A.

2b. If the mounting flanges of the stationary sections are to be mounted behind the front rails (rails not tapped for 10-32 screws), mount each stationary section as shown in Fiq. 10-\$B.
3. Attach an angle bracket to both rear rails of the rack through the spacerblock, stationary section and into the rear rail of the rack. Note that the holes in the spacer block are not centered. Be sure to mount the block with the narrow edge toward the front of the rack; otherwise, the instrument may not slide all the way into the rack. Do not tighten the mounting screws. Fig. 10-7]shows the parts in the rear support kit and the order in which they are assembled.
4. Assemble the support pin to the angle bracket in the order shown in Fiq. 10-7. Leave the spacer (washer) off, but install the neoprene washer.
5. Install a support block on each side of the instrumental shown in Fig. 10-8
6. Refer to Fig. 10-9 to insert the instrument into the rack. Do not connect the power cord or install the securing screws until all adjustments have been made.
7. With the instrument pushed all the way into the rack, adjust the angle brackets so the neoprene washers on the support pins are seated firmly against the rear of the instrument and the support pins are correctly positioned in the support block on the rear of the instrument. Tighten all screws.
8. Pull the instrument partially out of the rack.
9. Remove the neoprene washers from the support pins and place the spacers on the pins. Replace the neoprene washers.
10. Position the instrument so the pivot screws (widest part of instrument) are approximately even with the front rails.
11. Adjust the alignment of the stationary sections according to the procedure outlined in Fiq. 10-10. (If the rear alignment is changed, recheck the rear support pins for correct alignment.)
12. After the tracks operate smoothly, connect the power cord to the power source.
13. Push the instrument all the way into the rack and secure it to the rack with the securing screws and washers as shown in Fig. 10-9C.

## NOTE

The securing screws are an important part of the shock-mounted installation. If the front rails are not tapped for the 10-32 securing screws, other means must be provided for securing the instrument to the rack.

Alternative Rear Mounting Methods

## CAUTION

Although the following methods provide satisfactory mounting under normal conditions, they do not provide solid support at the rear of the instrument. If the instrument is subjected to severe shock or vibration when mounted using the following methods, it may be damaged.

An altemative method of supporting the rear of the instrument is shown in Fig. 10-11. The rear support brackets supplied with the instrument allow it to be mounted in a rack which has a spacing between the front and rear rails of 11 to 24 inches. Fiq. 10-11A illustrates the mounting method if the rear rails are tapped for $10-32$ screws, and Fig. 1011 B illustrates the mounting method if the rear rails are not tapped for $10-32$ screws. The rear support kit is not used for this installation.

If the rack does not have a rear rail, of if the distance between the front and rear rails is too large, the instrument may be mounted without the use of the slide-out tracks. Fasten the instrument to the front rails of the rack with the securing screws and washers. This mountina method should be used only if the instrument will not be subjected to shock or vibration and if it is installed in a stationary location.

## Removing or Installing the Instrument

After initial installation and adjustment of the slide-out tracks, the Type R453 can be removed or installed by following the instructions give in Fig 10-9. No further adjustments are required under nomal conditions.

## Slide-out Track Lubrication

The slide-out tracks normally require no lubrication. The special finish on the sliding surfaces provides permanent lubrication. However, if the tracks do not slide smoothly even after proper adjustment, a thin coating of paraffin rubbed onto the sliding surfaces may improve operation.


Fig. 10-1. The Type $\mathbf{R 4 5 3}$ installed in a cabinet rack (sides removed): (A) Held into rack with securing screws; (B) extended on slideout



Fig. 10-3. Hardware needed to mount the instrument in the cabinet rack.


[^10]

Fig. 10-5. Methods of mounting the stationary section to the front rails.


Fig. 10-6. Locating the mounting holes for the left stationary section. Same dimensions apply to right stationary section.


Fig. 10-8. Installing the support black on the Instrument.


Fig. 10-9. Procedure for inserting or removing the instrument after the slideout tracks have been installed.

## TO ADJUST ALIGNMENT:

1. Position the instrument with the pivot screws approximately even with the front rails.
2. Loosen the mounting screws af the front of both stationary sections (left side shown).
3. Allow the tracks to seek their normal positions with the instrument centered in the rack.
4. Tighten the mounting screws.
5. Push the instrument all the way into the rack. If tracks do not slide smoothly, check for correcl spacing between the rear supports.
6. Check the vertical positioning of the Type R453 front panal with respact to adjacent instruments or panels. If not correct, reposition as necessary.


Fig. 10-10. Alignment adjustments for correct operation.


Fig. 10-11. Alternative method of installing the instrument using rear support brackets.

Pigure 10-12. REAR VIEW


Figure 10-13. Pivoting Dimensions.



section detall "A"
recommended mounting


## APPENDIX A

## REFERENCES

DA Pam 310-4
DA Pam 310-7
SB 38-100
TB SIG 355-1
TB SIG 355-2
TB SIG 355-3
TB 43-0118

TB 43-180
TM 11-6625-938-15

TM 11-6625-1549-15
TM 11-6625-1615-15
TM 11-6625-2376-15

TM 11-6625-2381-15

TM 11-6625-2383-15
TM 11-6625-2384-15

TM 11-6625-2385-15

TM 11-6625-2386-15
TM 11-6625-2399-15

TM 11-6625-2400-15

TM 38-750
TM 740-90-1
TM 750-244-2

Index of Technical Manuals, Technical Bulletins, Supply Manuals (Types 7, 8, and 9), Supply Bulletins, and Lubrication Orders.
Military Publications: US Army Equipment Index of Modification Work Orders.
Preservation, Packaging, Packing and Marking Materials, Supplies and Equipment Used by the Army.
Depot Inspection Standard for Repaired Signal Equipment.
Depot Inspection Standard for Refinishing Repaired Signal Equipment.
Depot Inspection Standard for Moisture and Fungus Resistant Treatment.
Field Instructions for Painting and Preserving Electronics Command Equipment Including Camouflage Pattern Painting of Electrical Equipment Shelters.
Calibration Requirements for the Maintenance of Army Materiel
Operator, Organizational, Direct Support, General Support, and Depot Maintenance Manual: Transportable Maintenance Calibration Facility, AN/TSM-55A.
Operator's, Organizational, Direct Support, General Support, and Depot Maintenance Manual: Test Set, Radio Frequency Power AN/USM-260.
Organizational, DS, GS, and Depot Maintenance Manual: HewlettPackard Oscilloscope Model 130C.
Operator's, Organizational, DS, GS, and Depot Maintenance Manual, Including Repair Parts and Special Tools Lists: Signal Generator AN/USM-256.
Operator's, Organizational, DS, GS, and Depot Maintenance Manual, Including Repair Parts and Special Tools Lists: Signal Generator AN/USM-269.
Operator's, Organizational, DS, GS, and Depot Maintenance Manual: Electronic Marker Generator AN/USM-271.
Operator's, Organizational, DS, GS, and Depot Maintenance Manual, Including Repair Parts and Special Tools Lists: Signal Generator AN/USM-272.
Operator's, Organizational, Direct Support, General Support, and Depot Maintenance Manual: Multimeter, ME-333/U (NSN 6625-00-935-1425) and J-Omega Volt-Ohmmeter, Types 213A, 215A, and 219A.
Operator's, Organizational, Direct Support, General Support, and Depot Maintenance Manual: Multimeter ME-338/U (NSN 6625-00-054-3486).
Operator's, Organizational, Direct Support, General Support, and Depot Maintenance Manual (Including Repair Parts and Special Tool Lists): Electrical Meter Test Set, TS-2734/U.
Operator's, Organizational, Direct Support, General Support, and Depot Maintenance Manual (Including Repair Parts and Special Tools Lists): Voltmeter TS-2843/U.
The Army Maintenance Management System (TAMMS).
Administrative Storage of Equipment.
Procedures for Destruction of Electronics Materiel to Prevent Enemy Use (Electronics Command).

## APPENDIX B

ITEMS COMPRISING AN OPERABLE EQUIPMENT

```
Oscilloscope AN/USM-273
    1 ea Oscilloscope OS-188/U
    2 ea Adapter, Connector UG-1825/U
    1 e a Adapter, Connector UG-1826/U
    1 ~ e a ~ A d a p t e r , ~ C o n n e c t o r ~ U G - 1 8 6 7 / U ~
    1 ea Cable Assembly, (SP) Electrical CX-10551/U
    2 e a Lead, Test CX-10552/U
    1 ea Cable Assembly, RF CG-3363/U
    1 ea Cover, Oscilloscope CU-931/U
```

Tektronix Model 453
Major equipment less accessories
TEK 103-0033-00
TEK 012-0092-00
TEK 103-0013-00
TEK 161-0024-00
TEK 010-0188-00
TEK 012-0076-00
TEK 016-0074-01

The followlng additional items were furnished with the equipments supplied in Transportable Maintenance Calibration Facility AN/TSM-55 (V).

1 ea CRT Ring
1 ea Mesh Filter
1 ea Light Filter
1 ea CRT Protector Plate
2 ea Fuse, fast-blo, 2 amp, 3 A(3
1 ea Fuse, fast-blo, 1 amp, 3 AG
1 ea Fuse, fast-blo, $\frac{1}{2}$ amp, 3 AG
1 ea Fuse, fast-blo, $\frac{1}{4}$ amp, 3 AG

TEK 354-0269-00
TEK 378-0573-00
TEK 376-0576-00
TEK 386-0218-00
TEK 159-0021-00
TEK 159-0022-00
TEK 159-0025-00
TEK 159-0026-00

APPENDIX C
MAINTENANCE ALLOCATION

## Section I. INTRODUCTION

## C-1. General

This appendix provides a summary of the maintenance operations for Oscilloscope AN/USM-273 (Tektronix 453). It authorizes categories of maintenance for specific maintenance functions on repairable items and components and the tools and equipment required to perform each function.This appendix may be used as an aid in planning maintenance operations.

## $\mathbf{C - 2}$. Maintenance Function

Maintenance functions will be limited to and defined as follows:
a. Inspect. To determine the serviceability of an item by comparing its physical, mechanical, and/or electrical characteristics with established standards through examination.
b. Test. To verify serviceability and to detect incipient failure by measuring the mechanical or electrical characteristics of an item and comparing those characteristics with prescribed standards.
c. Service. Operations required periodically to keep an item in proper operating condition; i.e., to clean (decontaminate), to preserve, to drain, to paint, or to replenish fuel, lubricants, hydraulic fluids, or compressed air supplies.
d. Adjust. To maintain, within prescribed limits, by bringing into proper or exact position, or by setting the operating characteristics to the specified parameters.
e. Align. To adjust specified variable elements of an item to bring about optimum or desired performance.
f. Calibrate To determine and cause corrections to be made or to be adjusted on instruments or test measuring and diagnostic equipments used in precision measurement. Consists of comparisons of two instruments, one of which is a certified standard of known accuracy, to detect and adjust any discrepancy in the accuracy of the instrument being compared.
g. Install. The act of emplacing, seating, or fixing into position an item, part, module (component or assembly) in a manner to allow the proper functioning of the equipment or system.
h. Replace The act of substituting a serviceable like type part, subassembly, or module (component or assembly) for an unserviceable counterpart.
i. Repair. The application of maintenance serv-
ices (inspect, test, service, adjust, align, calibrate, replace) or other maintenance actions (welding, grinding, riveting, straightening, facing, remachining, or resurfacing) to restore serviceability to an item by correcting specific damage, fault, malfunction, or failure in a part, subassembly, module (component or assembly), end item, or system.
j. Overhaul. That maintenance effort (service/ action) necessary to restore an item to a completely serviceable/operational condition as prescribed by maintenance standards (i.e., DMWR) in appropriate technical publications. Overhaul is normally the highest degree of maintenance performed by the Army. Overhaul does not normally return an item to like new condition.
k. Rebuild. Consists of those services/actions necessary for the restoration of unserviceable equipment to a like new condition in accordance with original manufacturing standards. Rebuild is the highest degree of materiel maintenance applied to Army equipment. The rebuild operation includes the act of returning to zero those age measurements (hours, miles, etc.) considered in classifying Army equipments/components.

## C-3. Column Entries

a. Column 1, Group Number. Column 1 lists group numbers, the purpose of which is to identify components, assemblies, subassemblies, and modules with the next higher assembly.
b. Column 2, Component/ Assembly. Column 2 contains the noun names of components, assemblies, subassemblies, and modules for which maintenance is authorized.
c. Column 3, Maintenance Functions. Column 3 lists the functions to be performed on the item listed in column 2. When items are listed without maintenance functions, it is solely for purpose of having the group numbers in the MAC and RPSTL coincide.
d. Column 4, Maintenance Category. Column 4 specifies, by the listing of a "work time" figure in the appropriate subcolumn(s), the lowest level of maintenance authorized to perform the function listed in column 3. This figure represents the active time required to perform that maintenance function at the indicated category of maintenance. If the number or complexity of the tasks within the
listed maintenance function vary at different maintenance categories, appropriate "work time" figures will be shown for each category. The number of task-hours specified by the "work time" figure represents the average time required to restore an item (assembly, subassembly, component, module, end item or system) to a serviceable condition under typical field operating conditions. This time includes preparation time, troubleshooting time, and quality assurance/quality control time in addition to the time required to perform the specific tasks identified for the maintenance functions authorized in the maintenance allocation chart. Subcolumns of column 4 are as follows:

C - Operator/Crew
O - Organizational
F - Direct Support
H - General Support
D - Depot
e. Column 5, Tools and Equipment. Column 5 specifies by code, those common tool sets (not individual tools) and special tools, test, and support equipment required to perform the designated function.
f. Column 6, Remarks. Column 6 contains an al phabetic code which leads to the remark in section IV, Remarks, which is pertinent to the item opposite the particular code.

## C-4 Tool and Test Equipment Requirements (Sec III)

a. Tool or Test Equipment Reference Code. The numbers in this column coincide with the numbers used in the tools and equipment column of the MAC. The numbers indicate the applicable tool or test equipment for the maintenance functions.
b. Maintenance Category. The codes in this column indicate the maintenance category allocated the tool or test equipment.
c. Nomenclature. This column lists the noun name and nomenclature of the tools and test equipment required to perform the maintenance functions.
d. National/ NATO Stock Number. This column lists the National/NATO stock number of the specific tool or test equipment.
e Tool Number. This column lists the manufacturer's part number of the tool followed by the Federal Supply Code for manufacturers (5-digit) in parentheses.

## C-5. Remarks (Sec IV)

a. Reference Code. This code refers to the appropriate item in section II, column 6.
b. Remarks. This column provides the required explanatory information necessary to clarify items appearing in section II.

## SECTION II MAINTENANCE ALLOCATION CHART

FOR
OSCILLOS E AN/USM-273 (TEKTRONIX 453)
SN 6625-00-930-6637)


OSCILLOSCOPE AN/USM-273 (TEKTRONIX 453)
NSN 6625-00-930-6637

| OOL OR TEST EQUIPMENT REF CODE | MAINTENANCE CATEGORY | NOMENCLATURE | NATI ONA L/NATO STOCK NUMBER | TOOL NUMBER |
| :---: | :---: | :---: | :---: | :---: |
| 1 | H, D | TRANSFORMER, VARIABLE POWER TF-510/U (GR WLOMT3A) OR EQUAL | 6120-00-054-7794 |  |
| 2 | H, O | GENERAIOR, ELECTRONIC MARKER AN/USM-271 (TEKTRONIX 184) OR EQUAL | 6625-00-982-1543 |  |
| 3 | H, O | TRANSFORMER, RATIO DECADE TF-515U (S INGER-GERTSCH RT60) OR EQUAL | 5950-00-087-5433 |  |
| 4 | H, 0 | GENERATOR, SIGNAL AN/USM-272 (TEKTRONIX 191) OR EQUAL | 6625-00-957-0421 |  |
| 5 | H, D | GENERATOR, SIGNAL AN/USM-269 (GR-1310A) | 6625-00-054-3476 |  |
| 6 | H, D | COUNTER, ELECTRONIC READOUT AN/ USM-257A (SYSTEM DONNER 1037) | 6625-00-935-1457 |  |
| 7 | H, D | OSCILLOSCOPE AN/USM-254 (HP 130C) OR EQUAL | 6625-00-069-5477 |  |
| 8 | H, D | MUL.ti METER ME-333/U OR Equal | 6625-00-935-1425 |  |
| 9 | H, D | GENERATOR, SIGNAL AN/USM-264 (HP 652A) OR EQUAL | 6625-00-935-4214 |  |
| 10 | H, D | TEST SET ELECTRICAL METER TS-2734 (FLUKE 760A) OR EQUAL | 6625-00-054-4976 |  |
| 11 | H, D | VOLTMETER TS-2843 (FLUKE 883AB OR 887AB) OR EQUAL | 6625-00-965-8304 |  |
| 12 | H, ${ }^{\text {d }}$ | GENERATOR, SIGNAL AN/USM-358 (TEKTRONI $\times$ 106) OR EQUAL | 6625-00-455-7302 |  |
| 13 | H, O | CALIBRATOR, AMPLITUDE-COMPARATOR AN/USM-360 (TEKTRONIX 067-0502-01) OR EQUAL | 6625-00-192-0866 |  |
| 14 | H, O | TEST SET, ELECTRON TUBE TV-7D/U OR Equal | 6625-00-820-0064 |  |
| 15 | H, ${ }^{\text {d }}$ | TEST SET, TRANSISTOR TS-18360/U OR EQUAL | 6625-00-13 8-7320 |  |
| 16 | 0,H, D | T00L KIT, TK-100/G | 5180-00-605-0079 |  |
| 17 | 0,H, D | tOOLS AND TEST EQUipment available to the repairman in his ASSIGNED MISSION. |  |  |



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LOGCOMD (2) except
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9th Log Comd (5)
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USATECOM (2)
USASTRATCOM (5)
USASTRATCOM-SIG-GP-T (2)
USASTRATCOM-EUR (5)
USASTRATCOM-PAC (5)
USASTRATCOM-SO (5)
USASTRATCOM-A (2)
USARV (5)
USAESC (40)
MDW (1)
USASCS (10)
USASESS (10)
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USAFAS (2)
USAARMS (2)
USAIS (2)
USAES (2)
USAOC\&S (2)
USAMCC (3)
Fort Huachuca (5)
WSMR (3)
Fort Carson (7)
Army Dep (2) except
LBAD (14)
SAAD (30)
TOAD (14)
LEAD (7)
ATAD (10)
USACDCEC (10)
Gen Dep (2)
Sig Sec Gen Dep (5)
Sig Dep (5)
USACRREL (2)
WRAMC (1)
Sig FLDMS (1)
ATS (1)
USAERDAA (2)
USAERDAW (5)
Units org under fol TOE:
(2 cys each unit)
9-550
Armies (2)
11-158
Corps (2)
29-134
Corps (2) 29.227
1st Cav Div (2)
Svc Colleges (2)
NG. State AG (3)
USAR: None.
For explanation of abbreviations used see AR 310-50.








## FIC. po-9 $453 /$ /443 Standard Accessores \& Other parts funished with ras3

Index. Tektronix Serial/Model No.


(3)
(as)

## DIAGRAMS



| Typical voltage measurements and waveform photographs wore obtained under the following conditions unless noted otherwise on the individual diagram |  | Vertical Controls (both c volts/ilv | nnels if applicables 20 mv |
| :---: | :---: | :---: | :---: |
|  |  |  | Cat |
| est Oscilloscope (with $10 \times$ |  | position | Midange |
| Frequency response Deflection factor (with probe) Input impedance | Dc to 20 MHz 50 millivolts to 10 volts/ division <br> 10 Megohms, 735 pico <br> farads | Input Coupling | DC |
|  |  | mode | CH 1 |
|  |  | trig Ger | norm |
|  |  | invert | i |
| Probe ground | Type 453 chasis ground |  |  |
| Trigger Source | Extemal from A GATE connector to indicate true time relationship between signals | Triggering Controls (both Level <br> SLOPE | A and B If applicable) <br> 0 |
| Recommended type <br> veforms <br> on diagrams) | Tektronix Type 545B with Type 1A1 plug-in unit | coupling | ac |
|  |  | source | int |
| veltmeter |  | Sweep Controls |  |
| type | Non-loading AC (RMS)DC VTVM | delar-TMe multiler | 0.20 |
|  |  | A TMEIDV | 1 ms |
| Senstivity | 20,000 ohmsivolt | в TME/div | 1 m |
| RangeReference voltage | O to 300 volts | a varable | cal |
|  | General Radio Type 1006 A | A SWEEP MODE | Auto trig |
| Recommended type (as used for voltages on diagrams) |  | ${ }_{\text {B S SWEEP MODE }}$ | TRIG G ERABLE AFIER DELAY TIME |
| Type 453 Conditions |  | Horiz ilsplay | A |
|  |  | mag | off |
| $\underset{\text { Line voltage }}{\text { Sigal aplied }}$ | 115 volts | A sweep length | FUL |
|  | Calibrator output signal connected tochannel1 and 2 INPUT Connectors for wavefoms Ont | pos | Midrange |
|  |  | fine |  |
|  |  | power | ON |
|  | No connections <br> (except as above) | Side-Panel Controls |  |
| Tace postion |  | в tmediv varialie | cal |
| Control setting | AS fallows except as noted otherwise on in dividual diagrams: | calbeator |  |
|  |  |  |  |
|  |  | All voltages given on the diagrams are in volts. Waveforms hown are actual waveform photographs taken with a Tek |  |
| CRT Controls |  | Voltages and waveforms on the diagrams (shown in blue) |  |
| ENSIT | Midrange |  |  |
| SCALE IUUM | Adiust for focused displayAsdesied | of differing component tolerances, intemal calibration or front-panel control settings. |  |
|  |  |  |  |




| $\div 10$ | $\div 2.5$ |
| :---: | :---: |
|  |  |
| $\div 100$ | * 5 |
|  |  |
| (1) ChanNeL vertical preamp |  |
| TYPE 453 OSCILLOSCOPE |  ( $5 / \mathrm{N} 20,000$ \& UF) |




 (3)CHANNEL I VERTICAL PREAMP

TYPE 453 OSCILLOSCOPE















TYPE 453 OSCILLOSCOPE


FIG. FO-27. DOWER SUPPLY E DISTRIBUTION


EARTS LIST FOR SEMICONDUCTOR TYPES



[^0]:    Fig. 2-27. Phase of lissajous display. (A) $0^{\circ}$ or $360^{\circ}$, (B) $30^{\circ}$ or $330^{\circ}$, (C) $90^{\circ}$ or $270^{\circ}$, (D) $150^{\circ}$ or $210^{\circ}$ and (E) $180^{\circ}$.

[^1]:    ${ }^{2}$ Jacob Millman and Herbert Taub, "Pulse, Digital and Switching Waveforms" McGraw-Hill, New York, 1965, pp. 362-389.

[^2]:    ${ }^{3}$ lbid., pp. 438-451.

[^3]:    ${ }^{4}$ Lloyd P. Hunter, pp. 11-57--11-62.

[^4]:    ${ }^{5 P h}$ illip Cutler, "Semiconductor Circuit Analysis", McGraw-Hill, New York, pp. 365-372.

[^5]:    ${ }^{7}$ Ibid., Pp. 405-438.

[^6]:    I bid., pp 540-548.

[^7]:    ${ }^{9}$ lbid., pp. 389-394.

[^8]:    ${ }^{10}$ Lloyd P. Hunter, pp. 14-1 9-1 4-21.

[^9]:    ${ }^{11}$ Cutler, pp. 559-625.

[^10]:    Fig. 10-4. Supporting the rear of the stationary sections:
    (A) Dimensions necessary; (B) completed installation.

