

## CHAPTER 1

## GENERAL DESCRIPTION, SPECIFICATION,

FIRST TIME OPERATION

## 1. GENERAL DESCRIPTION

The D56 is a double-beam instrument, with two identical timebases, "A" and " B ". A versatile switching arrangement enables either timebase to be coupled to either beam, or alternatively enables both beams to be coupled to one timebase. Alternatively, timebase " B " can be switched to trigger timebase " A ". The point at which timebase " A " is triggered can be varied by a delay pick-off control, calibrated from 0-100.

Thus the instrument has a unique facility whereby a signal displayed on the lower beam has a bright-up marker superimposed on it. This marker may be moved over the entire length of the trace by the delaying sweep control; the portion of the signal covered by the marker is determined by the setting of the main sweepand is simultaneously displayed across the entire length of the upper trace.

A special 5" Spiral PDA C.R. tube, with a double-gun assembly, ensures that both traces are completely independent. This enables both a completed waveform and a selected and magnified part of it to be displayed simultaneously. The double-gun assembly also eliminates the need for "chopper circuits", whichare normally used when the phase relationship between waveforms is being examined.

In addition, the instrument is ideally suitable for use as a general purpose oscilloscope where a large display is required.

## Twin High Gain D.C. Coupled Amplifiers

Each has a total of four stages, including interstage and output cathodefollowers. The amplifiers are compensated for optimum pulse response.

## Accurate Calibrated Input Attenuators

Give direct reading of input voltages A.C. and D.C. from $100 \mathrm{mV} / \mathrm{cm}$ to $50 \mathrm{~V} / \mathrm{cm}$. D.C. to $15 \mathrm{Mc} / \mathrm{s}$. $10 \mathrm{mV} / \mathrm{cm}$ to $5 \mathrm{~V} / \mathrm{cm}$. D.C. to $500 \mathrm{Kc} / \mathrm{s}$.

A $10 \mathrm{Mc} / \mathrm{s}$ triggered marker is provided for accurate measurement of rise times to $1 / 10$ th of a microsecond. This is available when using the upper beam, and the trace is displayed by Timebase "A".

## High Quality Components

"C" core mains transformer and latest high efficiency valves ensure complete reliability and long periods of service between maintenance.

Unique System of Construction
Ensures adequate cooling under continuous operating conditions in addition to ensuring maximum accessibility for easy maintenance.

## 2. SPECIFICATION

### 2.1 Timebases

Two identical Timebases, " A " and " B " are provided, each with:
22 Pre-set calibrated Sweep Speeds.
5, 2 and 1 seconds per cm .
$500,200,100,50,20,10,5,2$ and 1 milliseconds per cm .
$500,200,100,50,20,10,5,2,1$ and 0.5 microseconds per cm.

Variable control covering intermediate speeds.
Time measurement accuracy $\pm 5 \%$.

Timebase "A" may be switched to both traces or to the upper one only. In the latter case, the lower tiace is coupled to Timebase "B".

Similarly, Timebase "B" may be switched to both traces, or to the lower one only.

## 2.2 "X" Expansion

Continuously variable up to 10 screen diameters ( 100 cms .) approx. Trace expands symmetrically about centre of screen. "X" - Shift - Control positions any portion of expanded trace on screen. Both these facilities are available for Timebases " A " and " B ".

### 2.3 D.C. Coupled Trace Bright Up

Ensures uniform trace brightness at slow sweep speeds.

### 2.4 Triggering

Two modes of triggering are provided.
(1) Auto. On this setting the sweep free runs at a slow speed in the absence of an input signal, but is triggered automatically as soon as an input signal is applied.
(2) Trigger Level Selection. With the AUTO switch off, the TRIG LEVEL control allows the sweep to be triggered from any part of the slope of the input waveform.

### 2.5 Trigger Selection

Selector switches enable the timebases to be triggered from the output of either Vertical Deflection Amplifier, positive or negative; or from an EXTERNAL input, positive or negative.
2.5.1 H.F. Triggering

A special H.F. switch position gives good synchronization from

- high frequency input signals between $1 \mathrm{Mc} / \mathrm{s}$ and $15 \mathrm{Mc} / \mathrm{s}$.


### 2.5.2 TV Sync.

D.C. restoration enables the sweep to be triggered from the LINE or FRAME pulses of a composite TV waveform without a change of picture content affecting the triggering point.

$$
\begin{aligned}
& \text { 2.5.3 } \frac{\text { Delay }}{\text { The DISPLAY switch, when set to }} \\
& \begin{array}{l}
\text { "A" DLD by "B" } \\
\text { Y1 by "A" } \\
\text { Y2 by "B" }
\end{array}
\end{aligned}
$$

allows timebase " A " to be triggered by timebase " B ". Under these conditions, the " $A$ " timebase produces a brightening pulse which is added to the " $B$ " timebase trace, so that the position of the delayed sweep can be seen.

### 2.6 Trigger Level Control

Allows any point on the synchronizing waveform, (repetitive, random or single shot) to be selected for triggering the timebase. A similar control is available for either timebase " A " or " B ".

### 2.7 Cathode Ray Tube

$5^{\prime \prime}$ flat-faced, double-gun, tube, operated at 6KV overall. Screen phosphor P31 fitted as standard, removable filters are fitted to improve contrast at high ambient illumination.
$10 \times 6 \mathrm{cms}$ " X " and " Y " deflection with 4 cms of overlap.

### 2.8 Illuminated Graticule

Edge-lit Illuminated Graticule facilitates accurate measurements. A front panel control varies illumination intensity.

X1 Position
D.C. to $15 \mathrm{Mc} / \mathrm{s}$ (approx. $-3 d B$ ) adjusted for optimum pulse response.
$100 \mathrm{mV} / \mathrm{cm}$ at all frequencies.
$0.023 u S e c$ (less than $2 \%$ overshoot).

Maximum Sensitivity

Rise Time
Frequency Response

Maximum " $Y$ " Deflection

X 10 Position
D.C. to $500 \mathrm{Kc} / \mathrm{s}$ (approx. -3dBs).
$10 \mathrm{mV} / \mathrm{cm}$ at all frequencies.
0.7 uS 6 cms at all frequencies.

### 2.10 Input Attenuators

Nine position, frequency compensated.
Direct reading in Volts/cm:-
$100 \mathrm{mV}, 200 \mathrm{mV}, 500 \mathrm{mV}, 1 \mathrm{~V}, 2 \mathrm{~V}, 5 \mathrm{~V}, 10 \mathrm{~V}, 20 \mathrm{~V}, 50 \mathrm{~V} / \mathrm{cm}$ on X 1 position.
$10 \mathrm{mV}, 20 \mathrm{mV}, 50 \mathrm{mV}, 100 \mathrm{mV}, 200 \mathrm{mV}, 500 \mathrm{mV}, 1 \mathrm{~V}, 2 \mathrm{~V}, 5 \mathrm{~V}$ on X 10 position.
Input Impedance 1 Megohm +40 pf (approx.).
Voltage Measuring Accuracy $\pm 5 \%$.
A variable control provides continuous gain variation between the fixed steps.

### 2.11 Marker

A $10 \mathrm{Mc} / \mathrm{s}$ marker may be switched in to give Z-modulation at 0.1 us intervals, for the purpose of accurate measurements of rise times, etc. This is available on the upper beam, and using timebase " A ".
2.12 Supply Voltage \& Current

$$
\begin{aligned}
&90-130 v) \\
&200-240 v) 50 c / s
\end{aligned} \quad V A=375
$$

### 2.13 Valve Content



## Transistor Content

| $\frac{\text { Qty }}{}$ | $\frac{\text { Type }}{}$ |  |
| :--- | :--- | :--- |
| 6 | - | A1668 |
| 2 | SGS Fairchild |  |
| 1 | - | ACY22 |
| MUllard |  |  |
| NKT452 | Newmarket |  |

2.14 Cooling

Convected air thermo-syphon cooling.
2.15 Dimensions
9.7/8" wide $\times 17^{\prime \prime}$ high $\times 19^{\prime \prime}$ long. ( $24 \mathrm{cms} \times 43 \mathrm{cms} \times 48 \mathrm{cms}$ )
Weight: 58 lbs.

## 3. FIRST TIME OPERATION

### 3.1 Introduction

The following detailed instructions are intended for those unfamiliar with this type of oscilloscope. It is suggested that the user should carefully carry out this procedure several times, in order to become thoroughly familiar with the instrument before putting it into use.

Throughout this handbook all front panel controls and sockets are shown in CAPITALS UNDERLINED; preset (internal) controls are shown in CAPITALS only.

### 3.2 Operation

Set the front panel controls for both Amplifiers and both Timebases as follows:

INPUT SWITCH
VOLTS/CM
Y GAIN
VARIABLE
FOCUS
ASTIG
Y SHIFT
BRILLIANCE
X GAIN
X SHIFT
STABILITY
TRIG LEVEL

TIME/CM
VARIABLE
TRIG SELECTOR
DISPLAY
-SINGLE SHOT/NORMAL
SWITCH
"DC"
"0.2"
X1
Fully clockwise
Mid-position
Mid-position
Mid-position
Fully anticlockwise
Fully anticlockwise
Mid-position
Fully clockwise
Anticlockwise to position just before switch operation
"10MS"
Fully clockwise
"NORMAL" (all out), "+" in, "Yl" in.
Y1 by "A" Y2 by "B"

Normal
3.2.1 Set the links on the Voltage Selector Panel, at the rear of the instrument, according to the mains supply voltage to be used. Plug in, rotate the POWER switch clockwise, to the "ON" position, and allow a few minutes for the instrument to warm up. (Further clockwise rotation of the POWER switch will simply increase the graticule illumination).
3.2.2 Advance each BRILLIANCE control until a trace appears; position the trace in the centre of the screen by means of the $X$ SHIFT (Horizontal) and Y SHIFT (Vertical) controls. Adjust the ASTIG and FOCUS controls, in conjuncfion with one another, for a well-defined frace.
3.2.3 Now back-off each STABILITY control unit the sweep just fails to free run. This is the normal position of this control, and, once set, it should not require any readjustment except at the very highest sweep speeds. The instrument is now ready for use.

### 3.3 Triggering

If the TRIG LEVEL controls are turned fully anticlockwise to operate the AUTO switch, the traces will reappear. In this condition the instrument is ready to accept almost any input waveform and will automatically be triggered by it. The only adjustments required are the selection of the appropriate sweep speeds and " $Y$ " sensitivity (VOLTS/CM). However, in order to use the instrument to best advantage, the functions of the controls should be fully understood. The following procedure will demonstrate their use:
3.3.1 Return the TRIG LEVEL control anticlockwise to the position just before the switch operates. There should now be no trace visible on the screen.

Joint a short connector between the CAL terminal and each INPUT socket and rotate the TRIG LEVEL controls clockwise, Until the traces just appear. (If the sweep is not triggered, the STABILITY control has been backed off too far).

The oscilloscope is now displaying the CALIBRATION VOLTAGE waveform (see Chapter 4, Section 2.4), which should be a square wave of $2 \frac{1}{2} \mathrm{cms}$ amplitude, with one cycle occurring every 2 cms . This is a very convenient waveform for demonstrating the functions of the controls.

### 3.4 Focus and Astigmatism

By adjusting the FOCUS control, either the horizontal or vertical edges of the squarewave can be brought into focus, but only if the ASTIG control is correctly adjusted will it be possible to focus the whole of the waveform simultaneously. Once the ASTIG control is set, it should require no further adjustment and a welldefined trace will be obtained over the whole of the screen.

### 3.5 Speed Calibration

The calibration waveform is at supply-line frequency, so that when the instrument is operated on $50 \mathrm{c} / \mathrm{s}$ mains, 1 cycle occupies 20 milliseconds. With the TIME/CM switch set to " 10 milliseconds" and the VARIABLE control fully clockwise, the timebase speed is 10 milliseconds per centimetre, so that one cycle should occupy two centimetres. The SET SPEED control, adjacent to the TIME/CM switch, is used to adjust the sweep speed on this calibration waveform to give precisely 1 cycle per 2 cms . This standardizes the whole of the time calibration of the instrument, all other ranges being direct multiples of this. Speed calibrations only apply when the VARIABLE control is in the fully clockwise position. On $60 \mathrm{c} / \mathrm{s}$ mains the SET SPEED should be adjusted on $10 \mathrm{mS} / \mathrm{cm}$ so that 3 cycles occupy 5 cms .

For most purposes, when accurate time calibration is not required, the above controls are used to produce a picture of convenient size, with the TIME/CM switch as the "coarse" control and the VARIABLE control for "fine" adjustments.

## 4. SWEEP CONTROLS

### 4.1 Trig Level

The Trigger Level control is used to set the precise part of the slope of the input waveform at which the sweep is triggered. The use of this control may be demonstrated as follows:

Set the TIME/CM switch to $5 \mathrm{~m} / \mathrm{s}$, as described in Chapter 2, to give one cycle of the squarewave, 4 cm long. Now rotate the TRIG LEVEL control. It will be found that the starting point of the trace can be moved up and down the sloping edge of the squarewave. If the control is turned too far clockwise, this point rises above the top of the squarewave and the sweep stops. Similarly, rotation too far anticlockwise produces the same effect.

This facility is useful for displaying complex waveforms, when a normal type of sweep generator will either fail to trigger the sweep or cause double trigger action, producing a multiple pattern. It may also be used as an amplitude discriminator, so that signals of small amplitude are ignored and the sweep is triggered only when the input voltage reaches a predetermined value. Positive or negative going edges may be selected by using the TRIG SELECTOR switch.

Adjustment of the sweep speed controls does not shift the starting point of the sweep but expands the trace from this point. Thus it is possible to examine a section of the waveform in detail by setting the TRIG LEVEL control so that the sweep is triggered just in advance of the portion to be examined and then expanding this portion as required by means of the sweep speed control(s).

### 4.2 Auto

On this setting no control over the trigger level is available; the sweep automatically adjusts itself to trigger at the mean level of the input waveform. This setting may be used for almost all applications involving repetitive waveforms of a simple nature. The sweep generator will be automatically triggered by signals between about $50 \mathrm{c} / \mathrm{s}$ and $1 \mathrm{Mc} / \mathrm{s}$. In the H.F. position the sweep generator will synchronize to incoming signals up to at least $15 \mathrm{Mc} / \mathrm{s}$ provided their amplitude gives about 2 centimetres vertical deflection. Correct synchronization can be achieved by adjusting the level control.

In the "AUTO" position with no input signals the trace will become progressively fainter as the sweep speed is increased. This is due to the sweep running free at about $40 \mathrm{c} / \mathrm{s}$ in the absence of a trigger signal, regardless of the setting of the speed controls. As soon as an input signal is applied, the sweep is immediately synchronized by it and the trace reverts to its full brightness.

### 4.3 Trig Selector

The Trigger Selector switch is divided into two sets of three push buttons. One position, used for most purposes, selects "NORMAL" triggering. The top two buttons bring the D.C. restoration into circuit. This enables the sweep to be triggered from the Line or Frame pulses of a TV waveform (normally negative going) independent of the picture content (positive going). The third button selects H.F. operation. In this latter position the sweep is synchronized by the incoming signals. The lower three buttons select positive or negative, $\mathrm{Y} 1, \mathrm{Y} 2$, or external triggering waveforms as required.

A differentiating circuit of $22 u S$ is used in the Sync. Separator to permit triggering from the Frame pulse, effectively removing the line pulse.

For triggering from an external signal, set the switch to EXT, both buttons out, and connect the signal to the EXT TRIG terminal socket.

### 4.4 X Gainand Shift

The $X$ GAIN control expands the length of the trace from approximately one screen diameter in the anticlockwise position to approx. 10 screen diameters when rotated fully clockwise.

The X SHIFT control is used to centre the trace symmetrically about the ruled graticule or to display any portion of the expanded trace on the screen for examination.

The time calibration holds good only at the minimum setting of the XGAIN control. It is possible to measure time intervals at other settings, however, by using the internal calibration waveform as a standard. For instance, if the X GAIN control is adjusted so that one cycle of the calibration waveform occupies 5 centimetres on the $20 \mathrm{Ms} / \mathrm{cm}$ range, then the gain is exactly five times on all ranges and, provided the $X$ GAIN control is not touched, all sweep speeds will be multiplied by a factor of 5. Any multiplication factor between 1 and 10 is possible.

### 4.5 Display Switch

4.5.1 The DISPLAY switch, switches the output sawtooth waveforms from timebases "A" and "B" to the appropriate pair of C.R.T. "X" plates.

In the "Y1, Y2 by $A$ " position, both Y1 and Y2 amplifier signals are displayed by the "A" timebase only.

Similarly, in the "Y1, Y2 by B" position, both Y1 and Y2 amplifier signals are displayed by the "B" timebase only.

$$
\text { In the }\binom{(Y 1 \text { by } A)}{(Y 2 \text { by } B)} \text { position, }
$$

the Y 1 amplifier signal is displayed on the " A " timebase and the Y 2 amplifier signal is displayed on the " $B$ " timebase. Under these conditions, the timebase trigger selector buttons should be switched to the appropriate amplifier and trigger conditions.
$(A$ DLD by $B)$
In the $(Y 1$ by $A)$
$(Y 2$ by $B)$
the " $B$ " timebase is triggered from any selected source, "Y1 or $Y 2$ or EXT" and a pulse is produced, part of the way along the sweep, which is automatically used to arm timebase " A ".

If the "Stability" control on timebase " $A$ " is fully clockwise, it will trigger on receipt of the arming pulse.

The displayed waveform will show the "B" sweep with a brightened portion. The length of the brightened portion is the time duration of sweep " $A$ ", and its position can be varied along the trace using the DELAY control.

If now, the same signal is connected to both $Y 1$ and $Y 2$ inputs, then the " $B$ " trace will show the waveform with a brightened portion, and the " $A$ " trace will show the brightened portion only. Hence, an expanded portion of the "B" trace may be viewed simultaneously with the unexpanded wave train.

If the "Stability" control on timebase "A" is set to its normal triggering position, it will trigger from the first trigger pulse which occurs after the arming pulse. This is the gated condition and jitter in the delay circuit will not affect the displayed trace.

To set up the correct conditions, switch to
( Y 1 by A ) (Y2 by B) position
and trigger both timebases from the appropriate trigger sources. These can, of course, be two independent but time related sources.

Then switch to
$\left.\begin{array}{l}(\mathrm{ADLD} \text { by } \mathrm{B}) \\ (\mathrm{Y} 1 \text { by } \mathrm{A}) \\ (\mathrm{Y} 2 \text { by } \mathrm{B}\end{array}\right)$
and adjusting the delay control will vary the position of the bright up portion of the " $B$ " timebase waveform in a series of discrete jumps instead of a smooth variation as when the "Stability" control of the "A" timebase is in the fully clockwise position. If gated operation is not required no trigger waveform should be fed to timebase $A$.

### 4.6 Single Shot Operation

With the switch in the Single Shot position the timebase will trigger from the first trigger pulse received after release of the "Reset" button. A neon indicator lights when the timebase is ready for triggering. After the timebase has fired it is insensitive to further triggering pulses until reset.

## 5. VERTICAL DEFLECTION AMPLIFIER CONTROLS

### 5.1 VOLTS/CM Switch

This nine-position switch inserts a series of frequency compensated attenuators between the coaxial INPUT socket and the Vertical Deflection Amplifier. If the gain of the amplifier is calibrated, direct readings of input voltages may be obtained. The $\frac{1}{2}$ volt calibration squarewave should measure 5 centimetres vertically with the VOLT/CM switch set to $0.1 \mathrm{~V} / \mathrm{cm}$. It is most important that the amplitude of the calibration squarewave should be measured between the horizontal flat portions.

### 5.2 Variable Gain Control

The Variable Gain Control is mounted concentric with the VOLTS/CM switch and varies the gain of the amplifier to cover the range between the VOLTS/ CM switch positions. The amplifier gain is only calibrated when the Variable Gain Control is in the fully clockwise position.

### 5.3 DC/AC Switch

This switch will normally be used in the "AC" position, in which a blocking capacitor removes the DC component of the input signal to the Vertical Deflection Amplifier. The time constant of the input circuit in this position is such that the response is 3 dB down at $2 \mathrm{c} / \mathrm{s}$, which, whilst adequate for most normal purposes, may prove critical in some applications. (For example, in the "AC" position, the $50 \mathrm{c} / \mathrm{s}$ calibration waveform acquires a pronounced tilt). If a longer time constant is required, an external blocking capacitor must be used, with a value suitably greater than 0.1 microfarad and the input switch set to "DC".

The "DC" position is also used if it is specifically desired to include the DC component of the input waveform to be measured.

### 5.4 XI/X10 Y Gain. Switch

This switch changes the gain of the Y amplifier, the normal X 1 sensitivity being multiplied by 10 when the X 10 position is selected. The calibration of the attenuator (VOLTS/CM) switch applies only in the XI position and should be divided by ten in the X 10 position.

## 6. ADDITIONAL FACILITIES

### 6.1 Sweep Output

The terminal marked Sweep Output on the timebase front panel provides an A.C. coupled positive going sawtooth waveform of approximately 50 v amplitude.

### 6.2 X Input

The terminal marked $X$ Input on the timebase front panel is normally linked to earth. Removing the link and turning the Variable control to the Off position enables external signals to be fed to the X amplifier. The sensitivity is approx. 0.1 to $\mathrm{IV} / \mathrm{cm}$ and the bandwidth D.C. to $500 \mathrm{Kc} / \mathrm{s}$ (approx. -3 dBs ). Input impedance is $1 M+30 \mathrm{pF}$ (approx.).

### 6.3 Z Mod

This connector, at the rear of the instrument, is taken, via a blocking capacitor, to the upper gun grid. A positive pulse applied here will brighten the trace. The bandwidth is $20 \mathrm{c} / \mathrm{s}$ to $30 \mathrm{Kc} / \mathrm{s}(-3 \mathrm{dBs})$ and a $10 \mathrm{v} \mathrm{P} / \mathrm{P}$ signal will give a clearly visible modulation of the trace.

## CHAPTER 2

## TIMEBASES \& ASSOCIATED CIRCUITS

In the D56 two similar Timebases "A" and "B" are incorporated. The circuit description refers to either timebase unless specifically stated otherwise.

## 1. THE TRIGGER CIRCUIT

### 1.1 General

Figure 2.1 shows the trigger and TV sync. selection. The operation of the push button switches is described and a detailed summary of the switch positions is also given in this chapter.

### 1.2 Circuit Description

The trigger amplifier consists of a longtailed pair followed by a cathode follower. The trigger signal from Y1, Y2 or External is fed to either grid of the longtailed pair depending on the setting of SIOIA (+,-), the other grid being earthed. The output from the pentode anode (V101B) is taken via cathode follower (V101A) to the input of the Schmitt trigger circuit (V103 ECC88). The output D.C. level of the trigger amplifier is varied by RV115, the Trig Level control which varies the D.C. level of both input grids symmetrically, allowing the triggering point to be set to any desired point on the waveform. On the Auto position the Level control is switched out of circuit and the output of the trigger amplifier is $\overline{\text { A.C. }}$ coupled to the Schmitt trigger circuit. The input grid resister R125 is returned to the opposite grid causing the circuit to free run at approx. $40 \mathrm{c} / \mathrm{s}$ in the absence of triggering signal. As soon as a trigger signal is applied the circuit is synchronised and the time base will trigger from a point near the mean level of the trigger waveform. This setting may be used for almost all applications involving repetitive waveforms with approximately equal excursions about the mean level and repetition frequencies between $50 \mathrm{c} / \mathrm{s}$ and $1 \mathrm{Mc} / \mathrm{s}$.

### 1.3 H.F. Operation

On H.F. operation S102C removes the D.C. coupling between the cathodes of the Schmitt trigger converting it into a multivibrator running at approx. $0.5 \mathrm{Mc} / \mathrm{s}$. The circuit will then synchronise to high frequencies from approx. 1 to $15 \mathrm{Mc} / \mathrm{s}$.

### 1.4 TV Sync. Pulse Selection

On these positions + and - refer to the picture content not the sync. pulse.
On TV Frame and TV Line positions the gain of the trigger amplifier is increased 3 fimes and a D. C. restoring circuit C106, R123 and MR101 introduced into the Schmitt trigger circuit input. The Trig Level control is set to trigger off the synchronising pulses. The D.C. restoration prevents change of triggering point with picture content variations. On TV Line the output of the Schmitt trigger circuit is differentiated by a short time constant C111 and R136 and fed to the time base. On TV Frame the time constant is increased by the addition of R137. This gives a greater output from the wider frame pulses than from the line pulses and the time base can be adjusted to trigger off the frame pulses by means of the Stability control.

### 1.5 Trigger Sensitivity

The trigger sensitivity control RV127 is a preset resistor between the cathodes of V 103 and is set to give the maximum trigger sensitivity on the 'Cal' waveform without multi-triggering.

### 1.6 Facilities

The trigger selector switch is divided into two sections, each of which is operated by three push buttons. The functions of the sections are as follows:

Upper Section:

Lower Section
selects NORMAL operation, H.F. operation, or TV sync., line or frame.
selects the polarity of the triggering signal (positive or negative) and selects the source of the triggering signal (internal Yl or Y2: external).

In order to clarify the operation of the selector switches, their positions are summarized below:

| Switch | Positions of <br> Buttons | Function |
| :---: | :---: | :---: |
| Upper Section | All Out |  |
|  | Top In | Normal |
|  | Middle In | TV Frame |
| Lower Section | Lower In | TV Line |
|  | Top In | H.F. |
|  | Top Out | - ve |
|  | Middle In | + ve |
|  | Lower In | Y1 |
|  | Both Out | Y2 |
|  |  | EXT |

## 2. THE TIMEBASE AND HORIZONTAL DEFLECTION AMPLIFIER

Fig. 2.4 shows the Timebase and Horizontal Amplifier and Fig. 2.5 the Time/Cm switch.

### 2.1 Timebase - Technical Description

V102B and V107A form a grid triggered Miller circuit, the timing components comprising C276, 277, 278, 279, 280 and R285, 287, 288, 289, 290. The Miller is driven by a bistable circuit V104 via diodes MR 104 and V105A. MR 105 clamps the starting point of the sweep at approx. 97.5 v .

The bistable circuit is triggered by a positive pulse from the trigger circuit via V106A. This cuts off diode V105A and the Miller action produces a positive going linear waveform at V107A cathode. A fraction of this voltage is fed via diodes MR 107 and V105B to the timebase bistable resetting it at an amplitude determined by RV148 the T.B. Length control. When the bistable resets MR104 is cut off and V105A conducts starting the flyback. The flyback continues until MR 105 conducts and clamps the cathode potential of V107A to that of V102B grid. During the flyback V105B is cut off and its cathode falls on a time constant R275, R277 and C275, 277, 278, 279, 280 until MR106 conducts. During this hold off
period the timebase can not be retriggered. If the Stability control RV152 is turned clockwise the potential at which MR106 conducts is reduced and eventually the potential of V105B cathode will fall low enough to retrigger the timebase bistable. The timebase will then free-run.

V106B amplifies the timebase bistable waveform to drive the bright-up circuits.

The timing and hold-off capacitors are switched in $10: 1$ steps the intermediate 1,2 and 5 steps being obtained by switching the timing resistor. RV291 is the Variable control giving a continuous variation of $2.5: 1$ and the calibration is correct in the fully clockwise position only. C276 is set up on the highest time base speed to give $0.5 \mathrm{~J} / \mathrm{cm}$ sweep speed. The output from V107A cathode, approx. 50 v of sawtooth, is taken via C118 to the Sweep Output terminal and to the $X$ amplifier.

When switched to Single Shot transistor bistable TR 101 and TR 102 is triggered at the end of the sweep and holds the anode of V105B sufficiently positive to prevent the timebase being retriggered. The transistor bistable is reset by S105 the Reset button and a neon N101 lights to indicate that the timebase is ready for friggering.

### 2.2 X Amplifier Technical Description

The sawtooth from the timebase and the X shift voltage from RV182 are mixed in a capacity compensated mixing circuit C116, R163, R164, R165 and applied to the grid of V107B which together with V108B form a longtailed pair. The X Gain control RV171 is connected between the cathodes and gives approx. 10:1 variation. RV172 Set Speed is set up with the X Gain in the fully anticlockwise (minimum gain) position. The push-pull output from the anodes is directly coupled via cathode followers V303 (Timebase A), V302 (Timebase B), to the X plates of the C.R.T. Trace equalising potentiometers RV311, 315, 319 and 324 are provided to set the traces to exactly the same length and position on both timebases. The grid of V108B is D.C. coupled to the anode of V109A the ' $X$ ' Input amplifier. The grid of V109A is D.C. coupled to the ' X ' Input terminal which is normally linked to earth. V109B is a cathode follower supplying the H.T. for V109A and RV195 is adjusted to give the correct D.C. level at V109A anode.

V108A is a cathode follower giving a low impedance 100 v supply for the timebase.

## 3. TIME BASE CONTROLS

### 3.1 The Stepped Sweep Control

Fig. 2.5 shows the stepped sweep control which consists of a 3 wafer 24 way rotary switch ( $\mathrm{Time} / \mathrm{cm}$ ) to which are connected the resistor-capacitor networks for obtaining the required time base speeds. These speeds range from 5 seconds to 0.5 microsecond per cm ascending in $5,2,1$ steps.

### 3.2 Variable Sweep Control

This control (RV291) is concentric with the Time/cm switch and the calibration is correct in the fully clockwise position. Turning the Variable anticlockwise decreases the speed by greater than 2.5:1 ensuring continuous coverage over a range of 0.5 microsecond per cms to 12.5 seconds per cm . In the fully anticlockwise position a switch turns the timebase off.

### 3.3 Preset Speed Adjustment

This is formed by the combination of a preset panel control (RV172) Set Speed (Fig. 2.4) and a small preset capacitor (C276 Fig. 2.5) which is mounted on the Time/cm switch assembly. The Set Speed control is adjusted at relatively low timebase speeds and the preset capacitor on the highest speed ( 0.5 microsecond $/ \mathrm{cm}$ ).

Details of these adjustments are given in the setting-up instructions (Chapter 5). The calibration is correct when the Variable is set fully clockwise and the $X$ Gain fully anticlockwise (i.e. minimum $X$ expansion).

### 3.4 X Gain and X Shift

The X Gain control (RV171) connected between the cathodes of V107B and $V 108 B$ varies the gain of the $X$ amplifier and allows the trace to be expanded approx. 10 times.

The $X$ Shift control RV182 is concentric with the $X$ Gain and provides a variable voltage which is mixed with the sweep voltage and fed to the grid of V107B. By this means the trace, with or without expansion, may be moved laterally across the screen to centralise any portion of it.

### 3.5 Stability Control

This control (RV152) varies the grid potential of V104A and is normally set to a point just above the free-running condition. The control adjusts the sensitivity of the sweep circuit to trigger pulses.

### 3.6 Internal Preset Controls

RV148 (T/B Length) controls the amplitude of the sawtooth from the Miller circuit and is set with the $X$ Gain fully anticlockwise.

RV195 is a preset X Shift and is set so that the X Shift control moves the trace symmetrically about the screen centre.

RV201 is a preset control on the transistor bistable which is set for correct operation on Single Shot.

C116 is the capacity compensation on the shift mixing circuit and is set to give no overshoot after the flyback on the 10 microseconds per cm range.

RV319 and RV324 (Trace Equalising) are set up so that both traces are identical in length and position on the screen when displaying Timebase A.

RV311 and RV315 (Trace Equalising) are set up so that both traces are identical in length and position on the screen when displaying Timebase B.

## 4. DELAY CIRCUIT

Fig. 2.6 shows the Delay Circuit which enables Timebase $A$ to be triggered from any portion of the sawtooth voltage produced by Timebase B.

Any waveform occurring during the period of one sweep of the lower trace (Y2) may be examined on the upper trace (Y1) at a faster timebase speed selected on Timebase A. The duration of the upper trace (YI) appears on the lower trace $(\mathrm{Y} 2)$ as a brightened portion allowing the delaying time to be determined.

### 4.1 Operation

The Timebase B sweep voltage is mixed with a variable D.C. voltage from the Delay potentiometer RV251 and applied to the base of TR251. TR251 and TR252 of a transistor bistable circuit which produces a fast positive edge at the collector of TR252 when the base of TR251 reaches a high enough potential for TR251 to conduct. The point on the incoming sawtooth at which the bistable circuit produces an output edge can be varied by means of the 10 turn Delay potentiometer.

In the "A" delayed by "B" position of the Display switch Timebase A is automatically switched to Single Shot as the single shot and display switches are in series. The positive edge from the Delay circuit resets the Single Shot bistable and if the Stability control of Timebase $A$ is in the free-running position Timebase A will fire. If Delayed gating operation is required Timebase A Stability control is set for normal triggered operation and the timebase will fire from the first triggered pulse occurring after the Single Shot bistable has been reset by the Delay circuit.

A portion of the bright-up pulse from Timebase $A$ is fed to the grid of the lower trace gun of the C.R.T. on the 'A delayed by B ' position of the Display switch S302. A 0.5 v positive going bright-up pulse is also available at a front panel socket marked B.U. Out.

## 5. BRIGHT-UP CIRCUITS

These are shown in Fig. 4.1.
Each gun of the C.R.T. has its own bright-up bistable V305 for the upper gun and V304 for the lower gun. Triggering waveforms from the appropriate timebases are switched by S302b (F) the Display switch.

### 5.1 Operation

The bright-up bistables V304 and V305 have the ir own 150v D.C. supply at the C.R.T. cathode potential -1200 v . The cathodes of the C.R.T. guns are D.C. coupled to the anodes of their appropriate bistable circuit. A positive triggering edge at the start of the sweep is fed to the input grid of the bistable circuit from
the timebase. This triggers the bistable and drives the C.R.T. cathode negative thus brightening the trace. At the end of the sweep a negative edge from the timebase resets the bistable blanking the trace. Presets RV347 and RV356 set the D.C. level of the unused grid to a suitable potential for correct operation of the bistable circuit.

## $5.2 \mathrm{l} 10 \mathrm{Mc} / \mathrm{s}$ Markers

V301A is a cathode coupled L.C. oscillator whose output is fed to the grid of the upper gun of the C.R.T. The tuned circuit is normally heavily damped by V301B which is conducting. When Timebase A is triggered a portion of the brightup pulse is fed to the grid of V301B cutting it off. The circuit then oscillates at $10 \mathrm{Mc} / \mathrm{s}$ until V301B again conducts and damps out the oscillation. RV305 adjusts the amplitude of oscillation and L301 the frequency.

## 6. TRACE SWITCHING

The Display switch 5302 has four positions:-

| Y1 Y2 | A DLD by B | Y1 by $A$ | Y1 Y2 |
| :--- | :--- | :--- | :--- |
| by B | Y1 by A | Y2 by B | by B |
|  | Y2 by B |  |  |

S302A switches the sweep outputs leads to the appropriate pairs of $X$ plates. S302B switches the timebase bright-up pulses to the appropriate bright-up bistable circuit and also switches Timebase A to Single Shot operation on position 2.

## CHAPTER 3

## VERTICAL DEFLECTION CIRCUITS

## 1. INTRODUCTION

The oscilloscope contains two identical " $Y$ " amplifiers, each with its own switched attenuator network; this network may be varied in 1, 2, 5 steps up to a division ratio of 1:500.

A switch provides facilities for alternating or direct voltage inputs and is connected directly in the input circuit.

The amplifiers employ D.C. -coupling and are frequency- compensated throughout, thus giving substantially uniform application from D.C. to $15 \mathrm{Mc} / \mathrm{s}$ with a sensitivity of $100 \mathrm{mV} / \mathrm{cm}$ and from D.C. to $500 \mathrm{Kc} / \mathrm{s}$ with a sensitivity of $10 \mathrm{mV} /$ cm.

Maximum visible " $Y$ " deflection is 6 cms at all frequencies. Rise time of 0.023 microsecond, with less than $2 \%$ overshoot on X1 position. Rise time of 0.7 microsecond, with less than $2 \%$ overshoot on $\times 10$ position.

## 2. INPUT ATTENUATORS (Fig. 3.2)

These are identical for the upper and lower trace amplifiers.
An A.C.D.C. switch S1, brings a capacitor (C1) in series with the INPUT coaxial socket (Amphenol Type 83-1R) and the attenuator, in the "A.C." position.

The VOLTS/CM stepped switch S2, may be set to one of nine positions marked .1, .2,.5, 1, 2, 5, 10, 20 and 50 read in a counter-clockwise direction; these figures indicate volts per centimeter. Four frequency-compensated resistance-divider networks are used; these will be obvious from the appropriate figure.

They may, however, be used singly or in cascade, as will be seen by the various positions of the ganged switch (S2).

The first attenuator section has ratios of 1,10 , and 100 and the second section 1, 2 and 5.

The attenuated output from R11 is taken to the grid of V26 (Fig. 3.2).
Input impedance to the attenuator is one megohm +40 picofarads (approx.) with a voltage measuring accuracy of $\pm 5 \%$.

## 3. VERTICAL DEFLECTION AMPLIFIERS (Fig. 3.1)

Apart from HT supplies, these amplifiers are identical for upper and lower trace in each case; both HT supplies, however, are taken from the same winding on T402 through a voltage-doubling network (Fig. 5.1).

### 3.1 Input Circuit

A signal (A.C. or D.C.) is fed into the control grid of V21 from the associated attenuator.

V21 and V22 form a cathode-coupled pair. The cathodes are coupled through RV22, a variable gain control, and RV23, a preset gain control, and the cathode currents are supplied through cathode resistors R26, R28 and RV27. RV27 is a DC BALANCE control and is adjusted so that there is no trace shift as the VARIABLE gain control is rotated.

A negative supply of -10 volts is available to provide the valve current, and also the shift voltage. This is applied to the grid of V22 via RV42.

The peaking inductors L21 and L22 in the anode circuits of V21 and V22 respectively are compensation for high-frequency inputs.

### 3.2 Anode Supply to Input Valves

The supply to the anodes and screens of V 21 and V 22 is somewhat unusual and is obtained from the common-cathode resistor V 26 (a) and (b) cathode-followers;
hence the cathode current of the input stages flows through these two output cathode-followers.

This is done to reduce the total current consumption of the amplifier.

### 3.3 Y Shift

This is obtained from a potentiometer network connected between the minus 10 volt supply and the output stage H.T. supply. The negative line is obtained by rectifying the 12.6 volt heater and smoothing with R416, C413 in Y1 and R417, C414 in Y2.

### 3.4 Pre-stage Cathode-followers and Final Amplifiers

V21 and V22 are D.C. -coupled to the grids of their respective cathode followers, the outputs of which are fed to the grids of the output amplifying valves V 24 and V 25 respectively. The output amplifier is a cathode compensated stage, C 23 being set for optimum pulse response. The diode between grid and cathode prevent high grid cathode voltages being applied when switching on and the valves are non-conducting. The diodes are automatically cut off when the valves have warmed up.

### 3.5 Output Cathode-followers

V24 and V25 are D.C. -coupled to the grids of the cathode-followers V26 (a) and (b).

The outputs from both cathode-followers are then fed to the " Y " plates and also fed via attenuator R56, R57 to the TRIGGER SELECTOR switches. See Chapter 2, Section 1.7.

### 3.6 Y Gain X $1 / 10$

With the $Y$ Gain switch in the ' XI ' position, the maximum sensitivity of the amplifier is $100 \mathrm{~m} \overline{\mathrm{~V} / \mathrm{cm} \text {. The gain is set up by the Set Gain control RV23 with the }}$ Variable control RV22 in the fully clockwise position.

When the $Y$ Gain switch $S 21$ is in the ' X 10 ' position, higher value load resistors are switched into the anode circuits of the input stage V21, V22. The
amount of $Y$ Shift is also reduced by a factor of 10. The D.C. Bal control RV44 is adjusted to give no trace movement when switching from ' $\overline{X 11^{\prime} \text { to }}$ ' $\times 10^{\prime}$ '.

### 3.7 Gain Stability

Due to the large amount of feedback on both amplifier stages the gain is unaffected by mains variations and the measurement accuracy of $\mp 5 \%$ is maintained with mains variations of $\mp 10 \%$.

## CHAPTER 4

## POWER SUPPLIES

## 1. INTRODUCTION

The Power Supply schematic is shown in Figure 5.1. All the rectifiers used are semiconductor diodes, thus ensuring maximum reliability.

## 2. CIRCUITRY

Two mains transformers provide all the required secondary voltages. The primary may be adjusted, by means of a double-link input voltage selector panel, for operation on alternating voltages from $90-130 \mathrm{~V}$ and $200-240 \mathrm{~V}, 50-60$ cycles.

### 2.1 H.T. Supplies

2.1.1 Time Base H.T.'s

A voltage doubler circuit MR403, MR404, C404, C405 supplies all the timebase H.T. voltages. Both X amplifiers and their associated cathode followers are fed from separately smoothed unstabilised supplies whilst both sweep and trigger circuits are stabilised. The stabiliser consists of series valve V401 which is controlled by a long-tailed pair amplifier V402 with a constant current transistor TR403 as the anode load. This arrangement gives a very high gain and therefore good stabilisation against both mains variations and load variations. The reference is a neon N401. The output voltage of the stabiliser is approx. 250 v for the timebases and dropping resistors R432, 433, 434, 435 provide separate 120 v supplies for the trigger circuits.

### 2.1.2 Y Amplifier H.T.'s

A voltage doubler circuit MR407, MR408, C406, C407 supplies both Y amplifiers via separate smoothing and decoupling circuits. The values of the H.T. voltages are shown against the appropriate outputs in Fig. 5.1.

### 2.1.3 Bright-Up H.T.

A half wave rectifier circuit MR419, C431, R436 provides the H.T. supply for both Bright-Up circuits and also the supply for the Brightness potentiometers RV331 and RV337. The positive side of this floating supply is connected to the $-1200 v$ E.H.T. supply.

### 2.2 E.H.T. Supplies

The positive P.D.A. supply of +4.7 Kv is obtained by voltage doubling a 750 v winding with MR411, MR412, C415 and C419 and then adding a further doubler from a 1000 y winding MR413, MR414, C417 and C418.

The negative supply of -1200 v is obtained from a voltage doubler circuit MR415, MR416, MR417, MR418, C421, C422, C423 and C424. The output from the doubler is stabilised by series valve $\vee 403$ the reference being the +250 v stabilised line. In order to compensate for changes in C.R.T. sensitivity due to the unstabilised A3 and P.D.A. supplies the -1200 v supply is arranged to change in the opposite direction to the mains variations by taking resistor R441 from the reference network to -16 v unstabilised across C409. MR410 protects V403 against high anode voltages on switch on.

### 2.3 L.T. Supplies

The transformer secondary windings supply 6.3 v and 12.6 v A.C. for valve heaters, pilot light and graticule illumination. A separate 6.3 v winding is provided for the C.R.T. and bright-up circuit heaters.

A stabilised 6.3v D, C. supply for Timebase B heaters is provided by a full wave rectifier circuit MR401, MR402, C403 feeding a transistor stabiliserTR401 and TR402. Zener diode MR409 is the reference.

Half wave rectifier MR405 and C409 rectify the 12.6 v heater voltage to give -16 v which is smoothed by R416, C413 and R417, C414 to give -10 v supplies for each $Y$ amplifier.

### 2.4 Calibration Voltage

A square wave of 0.5 v peak to peak is provided for calibrating purposes. This is obtained from a Zener diode clipping circuit fed from the 150 v tap on T402.

The square wave of approx. 11.5 v across the Zener diode MR406 is attenuated by a network of resistors having an opposite temperature coefficient to that of the Zener to $0.5 \mathrm{v} \mathrm{p} / \mathrm{p}$ and fed to a socket on the front panel. RV406 allows the amplitude to be set to exactly 0.5 v .

### 2.5 General

A fuse (F401) in the primary circuit, in series with the POWER switch (S401), protects the transformers against overload. The SCALE ILLUM control is coupled mechanically to the mains switch; it varies the brightness of the lamps illuminating the graticule and consists of a potentiometer (RV403) across the 6.5 V winding (see Chapter 1).

## CHAPTER 5

## MAINTENANCE, SERVICING AND SETTING-UP PROCEDURE

## 1. GENERAL

The simplicity of the circuitry of the D56 makes it an extremely reliable instrument. For the most part, servicing will be limited to the replacement of defective valves, but should a less common fault occur no difficulty should be experienced in detecting the source, if the circuit diagrams are used, in conjunction with normal test procedure. Test voltages at critical points are shown on the circuit diagrams, and the location of major components is given on Plates 2-4.

## 2. DISMANTLING FOR SERVICING

The "unit" method of construction used for the D56 ensures that all components are easily accessible for testing and servicing. The Timebases and Delay Circuit are built as a detachable unit and may be withdrawn as follows:

### 2.1 Removing the Timebases and Delay Circuit

To remove this unit the cover plates of the oscilloscope must be removed, by loosening the Philips type screws securing the carrying handle (the handle need not be removed). Then proceed as follows:
(1) Remove the four fixing screws at the centre top and bottom of the timebase chassis.
(2) Disconnect the four noval plugs on the leads from the timebase unit to the main chassis.
(3) Withdraw the unit by sliding it forward out of the front of the instrument.

### 2.2 Access to the Power Supply and CRT Circuitry

Access to the Power Supply and C.R.T. circuitry is by removal of the rear cover plate of the oscilloscope. This is secured by the two screws at either side of the voltage selector panel. The components in these circuits are easily identified from the circuit diagrams. The voltage tappings on the transformer are marked.

## 3. REPLACEMENT OF DEFECTIVE VALVES

When replacing valves in the Vertical Deflection Amplifier it is necessary to reset the DC Bal, RV27 and the Set Gain controls. Apart from this, little effect on the performance of the Vertical Deflection Amplifier should be experienced when valves are replaced, and no further readjustments should be necessary.

In the Sweep Generator and associated Amplifier the valve characteristics are not critical, and valves may be replaced without readjusting the preset controls.

If the internal preset controls should require readjustment, the following. detailed instructions should be followed.

## 4. SETTING-UP PROCEDURE

### 4.1 Input Attenuator

The eight trimmer capacitors of the Input Attenuator Switch (C12, C13, C4, C8, C9, C5, C2 and C3) are accessible for adjustment from underneath the instrument.

### 4.2 Apparatus and Procedure

In order to carry out this adjustment a square wave generator is required, giving a frequency of approximately $1 \mathrm{Kc} / \mathrm{s}$; its output must be variable between 0.5 V and 100 V . The rise time of the square wave need not be particularly fast, but it must have good, flat tops and bottoms. The adjustment procedure is as follows:
(1) Connect the square wave generator to the INPUT socket and adjust its output to approximately 0.5 V .
(2) Set the input attenuator to $0.1 \mathrm{volt} / \mathrm{cm}$. Adjust the sweep controls to display three cycles of the square wave on the screen.
(3) Adjust each capacitor in turn, to give square corners to the waveform. The input attenuator switch should be turned to the appropriate setting as shown in the table below. At the same time, adjust the output of the square wave generator to give a trace of 5 cm amplitude in each case.

| Input Attenuator Setting | Capacitor to be adjusted |
| :---: | :---: |
| $0.2 \mathrm{volt} / \mathrm{cm}$ | C 12 |
| 0.5 " | C13 |
| 1.0 " | C4 |
| 2.0 " | C8 |
| 5.0 " | C9 |
| 10.0 " | C5 |

When this procedure is correctly carried out, the 20 volts $/ \mathrm{cm}$ and 50 volts/ cm ranges are automatically correct.

### 4.3 Adjustments for Using Probe

The capacitors C2 and C3 affect compensation only when the High Impedance probe is in use. To adjust them proceed as follows:
(1) Remove the square wave generator from the input socket and plug in the High Impedance probe. Connect the output of the generator to the probe tip.
(2) Set the input attenuator to $0.1 \mathrm{volt} / \mathrm{cm}$ and the square wave generator output to give approximately 5 cm vertical deflection.
(3) Adjust the probe trimmer, which is accessible through a hole in the probe body, to give a flat top to the square wave.
(4) Switch the input attenuator to the 1 volt/cm range. Readjust the square wave generator output as before, and adjust C2. Set the input attenuator to the 10 volts $/ \mathrm{cm}$ range and adjust C3. All other ranges will automatically be correct.

### 4.4 Adjustment of High Impedance Probe Compensation Trimmer

This adjustment is best carried out with a square wave generator at an output frequency of $1 \mathrm{Kc} / \mathrm{s}$. Connect the probe to the INPUT socket and apply it to the signal generator output. The compensation trimmer is accessible through the hole in the body of the probe and should be adjusted to give square wave corners to a few cycles of the $1 \mathrm{Kc} / \mathrm{s}$ square wave displayed on the screen.

## 5. VERTICAL AMPLIFIER ADJUSTMENT

### 5.1 General

The preset controls on the Vertical Amplifier are the high frequency compensation and the Set Gain and Balance controls. The Set Gain controls should be set before adjusting the high frequency compensation.

### 5.2 Set Gain and Balance controls

(1) Set Variable control fully clockwise, Volts/cm switch to 0.1 and $Y$ Gain control to $X 1$. Set Y 1 trace to +1.2 cms and $Y 2$ trace to -1.2 cms with $\bar{Y}$ Shift. Switch Y Gain to X 10 and reset trace with DC Bal. Repeat until switch$\overline{\text { ing from }} \mathbf{X 1}$ to $\times 1 \overline{0}$ gives no shift of the trace.
(2) On $\times 10$ rotate Variable control anticlockwise and reset trace with RV27. Repeat until rotation of the Variable control gives no shift of trace.

Repeat (1) and (2) until there is no shift of the trace with either Variable or Y Gain switch.

### 5.3 High Frequency Compensation

This should not be attempted unless a square wave generator capable of producing an accurate square wave at $100 \mathrm{Kc} / \mathrm{s}$ to $1 \mathrm{Mc} / \mathrm{s}$, with a rise time of less than 5 millimicroseconds, is available. It must also be absolutely free from ring or overshoot.

The H.F. compensation circuits are extremely stable, and unless such a generator is available, it is best not to attempt any readjustment. Suitable square wave generators are the Tektronix Type 107 and Cossor Type 1090 or Telequipment Calibrator Type C1.

If such a generator is available, the following procedure should be adopted.
(1) Connect the square wave generator to the input socket. Set the attenuator switch to 0.1 volt $/ \mathrm{cm}$.
(2) Adjust the output of the generator to give a vertical deflection of 2-3 cm 。
(3) Set L21 and L22 to minimum (fully in). Adjust C23 for best square wave. Adjust L21 and L22 by equal amounts to obtain a flat topped square wave with a fast rise time, square corners and no overshoot rechecking C23 if necessary. The inductor affects the extreme corners of the square wave while the trimmer adjusts the flatness at the start of the flat top.

## 6. THE TRIGGER CIRCUIT

RV127 is adjusted to give maximum trig sensitivity and RV138 is adjusted so that the Level control operates symmetrically about its mid-position.

## Procedure

The internal calibration signal may be used to make this adjustment.
(1) Connect the CAL 0.5 V P - P and INPUT sockets and set the TIME/CM switch to $500 \mathrm{us} / \mathrm{cm}$.
(2) Set the input attenuator to the $2 \mathrm{~V} / \mathrm{cm}$ range. This gives a trace 2.5 mm high .
(3) Adjust RV127 to give maximum trigger sensitivity without multi-triggering on AUTO, tve or -ve.
(4) Set the $\mathrm{V} / \mathrm{cm}$ switch to $0.1 \mathrm{~V} / \mathrm{cm}$ range and set RV135 so that the LEVEL control operates symmetrically about its mid-position.
(5) Re-check RV127 setting.

## 7. THE SWEEP GENERATOR AND AMPLIFIER

### 7.1 Trace Length Control (RV148)

Set TIME/CM to $1 \mathrm{Ms} / \mathrm{cm}$ and STABILITY control fully clockwise, adjust Trace Length (RV148) control to give approx. 50 v at the sweep output terminal. Turn STABILITY fully anti-clockwise and if the time base does not stop, turn Trace Length (RV148) anti-clockwise until it does.

### 7.2 Frequency Compensation Trimmer Cill

Short together pins 7 and 8 on TB power socket. On 10uS/cm range with X GAIN at minimum increasing C116 will produce a small 'tail' to the left of the spot at the start of the time base. The correct setting of C116 is that at which the 'tail' just disappears into the spot. With X GAIN at maximum adjust neutralizing by bending wire connected to anode of V108B until the 'tail' just disappears. Check setting of C116 at minimum gain and repeat until rotating the $X$ GAIN from maximum to minimum produces no 'tail' on the spot in either direction.

### 7.3 Preset Speed Adjustments (RV172, C276)

Set $X$ GAIN to minimum and TIME/CM to $1 M s / c m$. Remove the short between pins 7 and 8 and display a $1 \overline{\mathrm{Kc} / \mathrm{s} \text { crystal controlled waveform. Set RV172 }}$ SET SPEED control to give one cycle per cm. Turn STABILITY control fully clockwise. Set trace length (RV148) to give slightly more than 10 cms of trace. Set TIME/CM to $0.5 \mathrm{uS} / \mathrm{cm}$ and display $1 \mathrm{Mc} / \mathrm{s}$ crystal controlled waveform. Adjust C276 to give one cycle per two cms.

Set RV195 so that X Shift control moves the trace by equal amounts to the left and right.

### 7.4 Single Shot Adjustment (RV201)

Display CAL waveform, switch to Single Shot and set RV201 to centre of range over which timebase triggers correctly when Reset button is pressed.

### 7.5 Bright-Up Circuits

Display 0.5 v Cal on both traces with Display switch on Y1 by A, Y2 by B. Adjust RV347 and RV356 to centre of region where the flyback is blanked. Check on all Display switch positions.

### 7.6 Trace Equalization

(1) Timebase "A"

$$
\begin{gathered}
\text { Set DISPLAY Switch to } \begin{array}{c}
\text { Y1 Y2 } \\
\text { by A }
\end{array}
\end{gathered}
$$

Display 1 mS markers on $1 \mathrm{mS} / \mathrm{cm}$ range of Timebase $A$ on both traces.
Using both Y SHIFT controls, bring the two traces so that they are almost touching each other.

Adjust both upper TRACE EQUALIZATION potentiometers, RV319, 324, together to make the start and finish of both traces coincident. RV3 19 affects mostly the start of the traces and RV324 the finish.
(2) Timebase "B"

Set DISPLAY Switch to (Y1 by B)

Display 1 mS markers on $1 \mathrm{mS} / \mathrm{cm}$ range of Timebase $B$ on both traces.
Adjust both lower TRACE EQUALISATION potentiometers together to make the start and finish of both traces coincident. RV311 affects mostly the start of the traces and RV315 the finish.

## 8. ADJUSTMENTS IN THE POWER SUPPLY CIRCUIT

### 8.1 The Calibration Voltage

The preset variable resistor (RV406) in the calibration voltage supply circuit (Power Supply Circuit, Fig. 5.1) is provided so that the output voltage can be set to precisely 0.5 volt peak to peak. This adjustment can only be made by comparing the calibration voltage with a known, accurate 0.5 volt peak to peak signal.

In practice RV416 should not require adjustment, unless the Zener diode MR406 has been replaced. If MR406 is replaced an equivalent type must be used.

### 8.2 The E.H.T. Stabiliser

Set mains voltage to exactly 240 v on 240 v tap. Adjust RV439 to give 250 v at anode of V403.

## 9. CRT CIRCUIT ADJUSTMENTS (Fig. 4.1)

## 9.1 $10 \mathrm{Mc} / \mathrm{s}$ Markers

Switch the MARKERS on, and switch the DISPLAY switch to
Y1 Y2
by A
Set Timebase "A" T/cm switch to $0.5 \mathrm{Sec} / \mathrm{cm}$, and display $1 \mathrm{Mc} / \mathrm{s}$ square wave with X expansion. Adjust L301, available through the printed circuit board PC23, mounted on the side of the H.T. chassis so that 10 markers occupy luS. The amplitude of markers is adjusted by RV329. There should be approximately 15 V at the CRT grid.

## CHAPTER 6

## COMPONENTS LIST

## ABBREVIATIONS

## Capacitors

SM
CER
ELEC
P
PC
PE
PS

Silver Mica
Ceramic
Electrolytic
Paper
Polycarbonate
Polyester
Polystyrene

Resistors
C
HS
WW
MO
MF

Carbon Composition
High Stability Carbon
Wire Wound
Metal Oxide
Metal Film

In the following component lists, no manufacturers' names have been included. When replacing components, locally available alternatives may be used if exact replacements are not to hand, provided the physical size is the same.

It is, however, preferable to use exact replacements whenever possible and these should be ordered direct from:

TELEQUIPMENT LIMITED 313 Chase Road Southgate, LONDON, N. 14.

Telephone: FOX Lane 1166 Telegraph: Telequipt. London. N. 14.
or from our Agents.

## INPUT ATTENUATOR TYPE D56

| Part No. | C.C.T. Ref。 | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 H 90401 | R 1 | 900K | HS | 1\% | $\frac{1}{4} \mathrm{~W}$ |
| 2H99401 | R 2 | 990K | HS | 1\% | $\frac{1}{4} \mathrm{w}$ |
| 18M | R 3 | 111 K | HS | 1\% | $\frac{1}{4} \mathrm{w}$ |
| 20M | R 4 | 10.1K | HS | 1\% | $\frac{1}{4} w$ |
| 2H50401 | R 5 | 500K | HS | 1\% | $\frac{1}{4} \mathrm{w}$ |
| 2 H 80401 | R 6 | 800K | HS | 1\% | $\frac{1}{4} \mathrm{w}$ |
| 2H10501 | R 7 | 1 M | HS | 1\% | $\frac{1}{4} \mathrm{w}$ |
| 2 H 25401 | R 8 | 250K | HS | 1\% | $\frac{1}{4} w$ |
| 2H10501 | R 9 | 1 M | HS | 1\% | $\frac{1}{4} \mathrm{w}$ |
| S 10410 | R10 | 100K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S82010 | R11 | 82 OHM | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| 16K | C 1 | 0.1 l | POL | 10\% | 400v |
| 16J | C 2 | 6-30pf | CER TRIMMER |  | 250 v |
| 16J | C 3 | 6-30pf | CER TRIMMER |  | $250 v$ |
| 16J | C 4 | 6-30pf | CER TRIMMER |  | $250 v$ |
| 16 J | C 5 | 6-30pf | CER TRIMMER |  | 250 v |
| 59 K | C 6 | 100pf | SM | 10\% | 350 v |
| 61K | C 7 | 1000pf | SM | 10\% | 350 v |
| 16J | C 8 | 6-30pf | CER TRIMMER |  | 250 v |
| 16J | C 9 | 6-30pf | CER TRIMMER |  | $250 v$ |
| 63X | C10 | 15pf | SM | 5\% | 350 v |
| 64X | C11 | 20pf | SM | 5\% | 350 v |
| 16 J | C12 | 6-30pf | CER TRIMMER |  | 250 v |
| 16J | C13 | 6-30pf | CER TRIMMER |  | 250 v |
| 65X | C14 | 30pf | SM | 5\% | 350 v |
| 63 X | C15 | 15pf | SM | 5\% | 350 v |
| 67 J | C16 | 0.0luf | MP | 10\% | 500 v |
| 36P | S 2 |  | SWITCH (Drg. |  |  |

NOTE: 2 Per Instrument

## VERTICAL AMPLIFIER TYPE D56

| Part No. | $\underset{\text { C.C.T. }}{\text { Ref. }}$ | Value | Description | Tolerance | $\begin{aligned} & \text { Rating } \\ & @ 70^{\circ} \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S10110 | R21 | 100 | C | 10\% | $\frac{1}{4} w$ |
| 82C | RV22 | 500 | Potentiometer 'Variable Gain' |  |  |
| 119C | RV23 | 500 | Potentiometer 'Preset Gain' | ${ }^{\text {' Drg. No. Pl05 }}$ |  |
| 2 H 82201 | R24 | 8.2K | HS | 1\% | $\frac{1}{4} w$ |
| 2H75101 | R25 | 750 | HS | 1\% | $\frac{1}{4} w$ |
| S15210 | R26 | 1.5K | C | 10\% | $\frac{1}{4} w$ |
| 16C | RV27 | 470 | Potentiometer (MP Plessey) |  |  |
| S15210 | R28 | 1.5K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| 2H75101 | R29 | 750 | HS | 1\% | $\frac{1}{4} w$ |
| 539210 | R30 | 3.9K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 2H82201 | R31 | 8.2K | HS | 1\% | $\frac{1}{4}$ W |
| S10110 | R32 | 100 | C | 10\% | $\frac{1}{4} w$ |
| S10110 | R33 | 100 | C | 10\% | $\frac{1}{4} w$ |
| S10110 | R34 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| Y27310 | R35 | 27K | C | 10\% | $\frac{1}{2} w$ |
| S12410 | R37 | 1.2 M | C | 10\% | $\frac{1}{4} w$ |
| S 10110 | R38 | 100 | C | 10\% | $\frac{1}{4} w$ |
| S12510 | R39 | 1.2 M | C | 10\% | $\frac{1}{4} w$ |
| S18210 | R40 | 1.8K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 910610 | R41 | 10M | C | 10\% | $\frac{1}{4} w$ |
| 62 C | RV42 | 100K | Potentiometer 'Shift' |  |  |
| S68410 | R43 | 680K | C | 10\% | $\frac{1}{4} w$ |
| 125C | RV44 | 100K | Potentiometer 'D.C. BAL' | (Drg. No. Pllo) |  |
| S18010 | R45 | 18 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| Y27310 | R46 | 27K | C | 10\% | $\frac{1}{2} w$ |
| S10110 | R47 | 100 | C | 10\% | $\frac{1}{4} w$ |
| S18010 | R48 | 18 | C | 10\% | $\frac{1}{4} w$ |
| S10110 | R49 | 100 | C | 10\% | $\frac{1}{4} w$ |
| S47410 | R50 | 470K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 82M | R51 | 2.2K | MO | 5\% | 3.25w |
| 131L | R52 | 5.1K | MO | 5\% | 3.25w |
| 131L | R53 | 5.1K | MO | 5\% | 3.25w |
| 82M | R54 | 2.2K | MO | 5\% | 3.25w |
| S10310 | R55 | 10K | C | 10\% | $\frac{1}{4} w$ |

40. 

## VERTICAL AMPLIFIER TYPE D56 (continued)

| Part <br> No. | C.C.T. <br> Ref. | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S56110 | R56 | 560 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 111L | R57 | 6.2K | MO | 5\% | 3.25 w |
| S 10110 | R58 | 100 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S 10310 | R59 | 10K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S47410 | R60 | 470K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S 10110 | R61 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 112L | R62 | 6.8K | MO | 5\% | 3.25 w |
| Y10210 | R63 | 1K | C | 10\% | $\frac{1}{2} \mathrm{w}$ |
| 113 L | R64 | 7.5K | MO | 5\% | 1.5 w |
| S 18210 | R65 | 1.8K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S 18210 | R66 | 1.8K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 65M | R67 | 1K | WW | 5\% | 4.5 w |
| 43K | C21 | 2.2 PF | CER |  |  |
| 29K | C22 | 0.47 | PE | 10\% | $125 v$ |
| 15J | C23 | 450 PF | CER TRIMMER |  |  |
| 96J | C24 | 32+32 | ELEC |  | 275v |
| 16K | C25 | 0.1 | PE | 10\% | 400 v |
| 29K | C26 | 0.47 | PE | 10\% | 125v |
| 59J | C27 | $32+32$ |  |  | 450 v |
| 39D | S21 | Switch X1 - X 103 Pole 2 Way |  |  |  |
| 34E | MR21 |  | Diode OA. 81 |  |  |
| 34E | MR22 |  | Diode OA81 |  |  |
|  | $\begin{aligned} & \mathrm{L} 21 \\ & \text { L22 } \end{aligned}$ |  | Variable Coil <br> Variable Coil |  |  |

## VERTICAL AMPLIFIER TYPE D56 (continued)

| Part No. | $\underset{\text { C.C.T. }}{\text { Ref. }}$ | Value | Description |  | Tolerance | $\begin{aligned} & \text { Rating } \\ & @ 70^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26 T | V21 |  | Valve Mullard | EF184 |  |  |
| 26 T | V22 |  | Valve Mullard | EF184 |  |  |
| 18 T | V23 |  | Valve Mullard | ECC88 |  |  |
| 27 T | V24 |  | Valve Mullard | E801F |  |  |
| 27 T | V25 |  | Valve Mullard | E801F |  |  |
| 18 T | V26 |  | Valve Mullard | ECC88 |  |  |

## TRIGGER CIRCUIT \& TIME BASE

| Part <br> No. | $\begin{gathered} \text { C.C.T. } \\ \text { Ref. } \\ \hline \end{gathered}$ | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 968510 | R101 | 6.8 M | C | 10\% | $\frac{1}{4} w$ |
| 968510 | R102 | 6.8 M | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S10110 | R103 | 100 | C | 10\% | $\frac{1}{4} w$ |
| S10510 | R104 | 1 M | C | 10\% | $\frac{1}{4} w$ |
| S18010 | R105 | 18 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S15210 | R106 | 1.5K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S68210 | R107 | 6.8K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S33210 | R108 | 3.3K | C | 10\% | $\frac{1}{4} w$ |
| S 10110 | R109 | 100 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S10110 | R110 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S 10510 | R111 | 1 M | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S22410 | R112 | 220K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S 15310 | R113 | 15K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| 933510 | R114 | 3.3M | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
|  | RV115 |  | See RV152 |  |  |
| 933510 | R116 | 3.3 M | C | 10\% | $\frac{1}{4} w$ |
| S 10110 | R117 | 100 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S18010 | R118 | 18 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S 10310 | R119 | 10K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| Y22310 | R120 | 22K | C | 10\% | $\frac{1}{2} \mathrm{w}$ |
| S33410 | R121 | 330K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S68410 | R122 | 680K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S 10410 | R123 | 100K | C | 10\% | $\frac{1}{4} w$ |
| S 10110 | R124 | 100 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S47410 | R125 | 470K | C | 10\% | $\frac{1}{4} w$ |
| S68310 | R126 | 68K | C | 10\% | $\frac{1}{4} w$ |
| 16C | RV127 | 470 | C Potentiometer Preset | 20\% | $\frac{1}{4} w$ |
| S22210 | R128 | 2.2K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S 10210 | R129 | 1K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S33310 | R130 | 33K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S 10410 | R131 | 100K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S10110 | R 132 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| Y22310 | R133 | 22K | C | 10\% | $\frac{1}{2} w$ |
| S68310 | R134 | 68K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 112C | RV135 | 47K | Potentiometer Preset | 20\% | $\frac{1}{4} w$ |

## TRIGGER CIRCUIT \& TIME BASE (continued)

| Part No. | $\begin{gathered} \text { C.C.T. } \\ \text { Ref. } \\ \hline \end{gathered}$ | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S 10310 | R136 | 10K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S22410 | R137 | 220K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| Y68310 | R138 | 68K | C | 10\% | $\frac{1}{2} w$ |
| S 10110 | R139 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S10110 | R140 | 100 | C | 10\% | $\frac{1}{4} W$ |
| S56310 | R141 | 56K | C | 10\% | $\frac{1}{4} w$ |
| S33205 | R 142 | 3.3K | C | 5\% | $\frac{1}{4} w$ |
| S15305 | R143 | 15K | C | 5\% | $\frac{1}{4} w$ |
| S82310 | R144 | 82K | C | 10\% | $\frac{1}{4} w$ |
| S 10110 | R145 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S18410 | R 146 | 180K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S68310 | R147 | 68K | C | 10\% | $\frac{1}{4} w$ |
| 104C | RV148 | 100K | Potentiometer Preset 'T/B Length' |  |  |
|  |  |  |  | 20\% | $\frac{1}{4} \mathrm{~W}$ |
| S15410 | R149 | 150K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S 10110 | R150 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S22310 | R151 | 22 K | C | 10\% | $\frac{1}{4} w$ |
|  | RV115 ) | 100K | Potentiometer 'Level' |  |  |
| 115C | RV152 ) | 10K | Potentiometer 'Stab' | 20\% | 2 w |
|  | S104) |  | Switch Auto On/Off |  |  |
| S12310 | R153 | 12K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S10110 | R154 | 100 | C (Positioned on copper side) | ) $10 \%$ | $\frac{1}{4} w$ |
| 556310 | R155 | 56K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S33410 | R156 | 330K | C | 10\% | $\frac{1}{4} W$ |
| S 10110 | R157 | 100 | C | 10\% | $\frac{1}{4} w$ |
| S 10510 | R158 | 1 M | C | 10\% | $\frac{1}{4} w$ |
| S 18010 | R159 | 18 | C | 10\% | $\frac{1}{4} w$ |
| Y 10305 | R161 | 10K | C | 5\% | $\frac{1}{2} w$ |
| Y56205 | R162 | 5.6K | C | 5\% | $\frac{1}{2} w$ |
| S33405 | R163 | 330K | C | 5\% | $\frac{1}{4} \mathrm{~W}$ |
| S56405 | R164 | 560K | C | 5\% | $\frac{1}{4} \mathrm{w}$ |
| S51405 | R165 | 510K | C | 5\% | $\frac{1}{4} w$ |
| S10110 | R166 | 100 | C | 10\% | $\frac{1}{4} w$ |
| 102M | R167 | 22K | MO | 5\% | 3 w |
| S10110 | R168 | 100 | C | 10\% | $\frac{1}{4} w$ |

## TRIGGER CIRCUIT \& TIME BASE (continued)

| Part <br> No. | C.C.T. Ref. | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 010310 | R169 | 10K | C | 10\% | lw |
|  | RV171 |  | See RV182 |  |  |
| 106C | RV172 | 25K | Potentiometer Preset 'Set Speed' |  |  |
|  |  |  |  | 20\% | $\frac{1}{4} w$ |
| S10110 | R173 | 100 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S10110 | R174 | 100 | C | 10\% | $\frac{1}{4} W$ |
| 010310 | R175 | 10K | C | 10\% | lw |
| 102M | R176 | 22K | MO | 5\% | 3 w |
| 2 H 15401 | R179 | 150K | HS | 1\% | $\frac{1}{4} w$ |
| S 10810 | R180 | 18 | C | 10\% | $\frac{1}{4} w$ |
| 2 H 82301 | R181 | 82K | HS | 1\% | $\frac{1}{4} w$ |
| 107C | RV182 | 50K ) | Potentiometer 'X Shift' " 'X Gain' | 20\% | 2 w |
| 107 C | RV171 | 10K ) |  |  |  |
| S 10310 | R183 | 10K | C , | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 015310 | R184 | 15K | C | 10\% | 1w |
| S82410 | R185 | 820K | C | 10\% | $\frac{1}{4} w$ |
| S10510 | R190 | 1 M | C | 10\% | $\frac{1}{4} w$ |
| S10110 | R191 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S33210 | R192 | 3.3K | C | 10\% | $\frac{1}{4} w$ |
| S15310 | R193 | 15K | C | 10\% | $\frac{1}{4} w$ |
| S10110 | R194 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 18C | RV195 | 1M | Potentiometer Preset | 20\% | $\frac{1}{4} \mathrm{w}$ |
| S 15510 | R196 | 1.5M | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S47310 | R197 | 47K | C | 10\% | $\frac{1}{4} w$ |
| S 10610 | R198 | 10M | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S39310 | R199 | 39 K | C | 10\% | $\frac{1}{4} w$ |
| 17C | RV201 | 10K | Potentiometer Preset | 20\% | $\frac{1}{4} w$ |
| S12310 | R202 | 12K | C | 10\% | $\frac{1}{4} w$ |
| S22410 | R203 | 220K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 922510 | R204 | 2.2M | C | 10\% | $\frac{1}{4} w$ |
| S18310 | R205 | 18K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S56310 | R206 | 56K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S 10310 | R207 | 10K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S68210 | R208 | 6.8K | C | 10\% | $\frac{1}{4} w$ |
| S 10410 | R209 | 100K | C | 10\% | $\frac{1}{4} w$ |

TRIGGER CIRCUIT \& TIME BASE (continued)

| Part No. | $\underset{\text { Ref. }}{\text { C.C. }}$ | Value | Description | Tolerance | $\begin{array}{r} \text { Rating } \\ @ 70^{\circ} \mathrm{C} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S56310 | R211 | 56 K | C | 10\% | $\frac{1}{4} w$ |
| S10410 | R212 | 100K | C | 10\% | $\frac{1}{4} w$ |
| 74J | C101 | 3.9pf | CER | $\pm \frac{1}{4} \mathrm{pf}$ | 750v |
| 74. | C102 | 3.9pf | CER | $7 \frac{1}{4} \mathrm{pf}$ | 750 v |
| 67 J | C103 | 0.01 | POL | 20\% | 400 v |
| 67J | C104 | 0.01 | POL | 20\% | 400 v |
| 66 J | C105 | 0.1 | POL | 20\% | 250 v |
| 66 J | C106 | 0.1 | POL | 20\% | 250v |
| 33K | C107 | 0.1 | POL | 20\% | 125 v |
| 66 J | C108 | 0.1 | POL | 20\% | 250 v |
| 76 J | C109 | 470pf | CER | 10\% | 500 v |
| 66 J | C110 | 0.1 | POL | 20\% | 250 v |
| 69 J | C111 | 100pf | POLY | 10\% | $350 v$ |
| 39 K | C112 | 15pf | CER | 5\% | 750v |
| 39 K | C113 | 15pf | CER | 5\% | 750v |
| 45K | C114 | 10pf | CER | 10\% | 750v |
| 41K | C115 | 30pf | CER | 10\% | 750v |
| 17J | C116 | 4-20pf | TRIMMER |  |  |
| 16K | C118 | 0.1 | POL | 20\% | 400v |
| 71J | C119 | 50 | ELEC |  | 150v |
| 45K | C122 | 10pf | CER | 20\% | 750 v |
| 72 J | C123 | 2200pf | P.E. | 20\% | 400 v |
| 100J | C124 | 100pf | CER | 10\% | 500 v |
| 67 J | C125 | 0.01 | POL | 20\% | 400 v |
| 100J | C126 | 100pf | CER | 10\% | 500 v |
| 101J | C127 | 150pf | CER | 10\% | 500 v |
| 90J | C128 | 0.033 | POL | 20\% | 250 v |
| 66 J | C129 | 0.1 | POL | 20\% | $250 v$ |


| 34 E | MR141 | Diode OA 81 |
| :--- | :--- | :--- |
| 34 E | MR102 | Diode OA 81 |
| 34 E | MR103 | Diode OA 81 |
| 34E | MR104 | Diode OA 81 |

## TRIGGER CIRCUIT \& TIME BASE (continued)

| Part <br> No. | $\begin{aligned} & \text { C.C.T. } \\ & \text { Ref. } \\ & \hline \end{aligned}$ | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 34E | MR 105 |  | Diode OA 81 |  |  |
| 34E | MR 106 |  | Diode OA 81 |  |  |
| 34E | MR107 |  | Diode OA 81 |  |  |
| 34E | MR108 |  | Diode OA 81 |  |  |
| 34D | S101) |  | Trig Selector Switches |  |  |
| 25D | S102) |  |  |  |  |
|  | S103 |  | Switch See RV284 |  |  |
|  | S104 |  | Switch See RV115 \& RV152 |  |  |
| 94 C | S105 |  | Reset |  |  |
| 560 | S106 |  | Single Shot/Normal |  |  |
| 36Y | N101 |  | Neon Type 3L |  |  |
| 119 T | TR101 |  | Transistor LB293 motorola |  |  |
| 119 T | TR102 |  | Transistor LB293 motorola |  |  |
| $10 T$ | V101 |  | Valve ECF80 |  |  |
| 10 T | V102 |  | Valve ECF80 |  |  |
| 18T | V103 |  | Valve ECC88 |  |  |
| 18 T | V104 |  | Valve ECC88 |  |  |
| 117 | V105 |  | Valve EB91 |  |  |
| 10T | V106 |  | Valve ECF80 |  |  |
| 10 T | V107 |  | Valve ECF80 |  |  |
| 10 T | V108 |  | Valve ECF80 |  |  |
| 10 T | V109 |  | Valve ECF80 |  |  |

## TIME/CM SWITCH CIRCUIT D56

| Part <br> No. | С.С.т. <br> Ref. | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S47510 | R276 | 4.7M | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S47410 | R277 | 470K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S33410 | R278 | 330K | C | 10\% | $\frac{1}{4} w$ |
| S39410 | R279 | 390K | C | 10\% | $\frac{1}{4} w$ |
| S68310 | R280 | 68K | C | 10\% | $\frac{1}{4} w$ |
| S30305 | R281 | 30K | C | 5\% | $\frac{1}{4} w$ |
| S15310 | R282 | 15K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S51405 | R283 | 510K | C | 5\% | $\frac{1}{4} w$ |
| S 10410 | R284 | 100K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| 3 H 15506 | R285 | 15M | HS 2HS3 | 2\% | $\frac{1}{2} w$ |
| 2H50501 | R286 | 5M | HS 2HS2 | 1\% | $\frac{1}{4} \mathrm{~W}$ |
| 2H25501 | R287 | 2.5M | HS 2HS2 | 1\% | $\frac{1}{4} \mathrm{w}$ |
| 159L | R288 | 1.5M | M.F. | 1\% | $\frac{1}{4} \mathrm{~W}$ |
| 160L | R289 | 500K | M.F. | 1\% | $\frac{1}{4} \mathrm{~W}$ |
| 14M | R290 | 500K | HS 2HS2 | 1\% | $\frac{1}{4} w$ |
| 103C | RV291 | 1M | C Potentiometer 'Variable' Drg. P1 |  |  |
| 912510 | R292 | 1.2M | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 42K | C275 | 39pf | CER | 5\% | 750 v |
| 16J | C276 | 6/30pf | CER TRIMMER Stentite |  | 250 v |
| 102J | C277 | 20pf | CER Lemco 310 NPO Erie BD NPO | Fo. $25 p$ | 750v |
| 103J | C278 | 380pf | P.S. Lemco G.E.C. Suflex or Lemco | 1\% | 125v |
| 104」 | C279 | 4000pf | P.S. Lemco G.E.C. Suflex or Lemco | 1\% | $125 v$ |
| 105J | C280 | 0.04 | P.S. Lemco G.E.C. Suflex or Lemco | 1\% | $125 v$ |
| 106 J | C281 | 0.4 | P.E. (0.33 $1 \%+.068$ 3\%) |  |  |
|  |  |  | Wima M | 2\% | 125v |
| 107J | C282 | 4 | P.E. Wima MKB2 | 2\% | 250 v |
|  | S 103 |  | Switch 'T/B ON OFF' see Drg. P101 <br> Switch 24 POS 'TM/CM' Drg. SW1350 |  |  |
| 55D | S275 |  |  |  |  |

## DELAY CIRCUIT

| Part <br> No. | $\begin{aligned} & \text { C.C.T. } \\ & \text { Ref. } \\ & \hline \end{aligned}$ | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 86C | RV251 | 100K | Potentiometer 'Knobpot' | 5\% |  |
| 168L | R252 | 47K | M.F. | 5\% | $\frac{1}{4} w$ |
| 118L | R253 | 27K | M.F. | 5\% | $\frac{1}{4} w$ |
| S68110 | R254 | 680 | C | 10\% | $\frac{1}{4} w$ |
| S22210 | R255 | 2.2 K | C | 10\% | $\frac{1}{4} w$ |
| S18210 | R256 | 1.8K | C | 10\% | $\frac{1}{4} w$ |
| Y47310 | R257 | 47K | C | 10\% | $\frac{1}{2} w$ |
| Y33310 | R258 | 33K | C | 10\% | $\frac{1}{2} w$ |
| S33410 | R259 | 330 K | C | 10\% | $\frac{1}{4} w$ |
| 54 K | C251 | 200P | CER | 10\% | 750 v |
| 53K | C252 | 100P | CER | 10\% | 750 v |
| 34E | MR251 |  | Diode OA 81 |  |  |
| 1197 | TR251 |  | Transistor LB293 Motorola |  |  |
| 1197 | TR252 |  | Transistor LB293 Motorola |  |  |

## C!R.T. CIRCUIT

| Part No. | C.C.T. <br> Ref. | Value | Description | Tolerance | $\begin{aligned} & \text { Rating } \\ & \text { @ } 700 \mathrm{C} \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S 10410 | R301 | 100K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| Y15310 | R302 | 15K | C | 10\% | $\frac{1}{2} \mathrm{w}$ |
| S56110 | R303 | 560 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 117L | R304 | 6.8 K | MO | 5\% | 3.25 w |
| 55C | RV305 | 4.7K | Potentiometer |  |  |
| S10310 | R306 | 10K | C | 10\% | $\frac{1}{4} w$ |
| 114L | R307 | 56K | MO | 5\% | 1.5w |
| S 10110 | R308 | 100 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| 114L | R309 | 56K | MO | 5\% | 1.5 w |
| 55C | RV311 | 4.7K | Potentiometer |  |  |
| 114L | R312 | 56K | MO | 5\% | 1.5w |
| S 10110 | R313 | 100 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| 114L | R314 | 56 K | MO | 5\% | 1.5w |
| 55C | RV315 | 4.7K | Potentiometer |  |  |
| 114 L | R316 | 56K | MO | 5\% | 1.5w |
| S 10110 | R317 | 100 | C | 10\% | $\frac{1}{4}$ W |
| 114L | R318 | 56K | MO | 5\% | 1.5 w |
| 55C | RV319 | 4.7K | Potentiometer |  |  |
| 114 L | R321 | 56K | MO | 5\% | 1.5w |
| S10110 | R322 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 114L | R323 | 56K | MO | 5\% | 1.5w |
| 55C | RV324 | 4.7K | Potentiometer |  |  |
| 98C | RV325 | 250K | Potentiometer 'Astig' |  |  |
| S56310 | R326 | 56K | C | 10\% | 1 |
| 922510 | R327 | 2.2 M | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 46 C | RV328 | 1 M | Potentiometer 'Focus' |  |  |
| S56410 | R329 | 560K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 46C | RV331 | 500K | Potentiometer 'Brilliance' |  |  |
| 98C | RV332 | 250K | Potentiometer 'Astig' |  |  |
| S56310 | R333 | 56K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 922510 | R334 | 2.2M | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| 46C | RV335 | 1 M | C Potentiometer 'Focus'; |  |  |
| S56410 | R336 | 560K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| 46C | RV337 | 500K | Potentiometer 'Brilliance' |  |  |
| S 10510 | R338 | 1M | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |

## C.R.T. CIRCUIT (continued)

| Part No. | C.C.T. <br> Ref. | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S 10510 | R339 | 1 M | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S18310 | R341 | 18K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S18310 | R342 | 18K | C | 10\% | $\frac{1}{4} w$ |
| S18310 | R343 | 18K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S18310 | R344 | 18K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| Y39210 | R345 | 3.9K | C | 10\% | $\frac{1}{2} w$ |
| 2H40401 | R346 | 400K | H.S. | 1\% | $\frac{1}{4} w$ |
| 57C | RV347 | 22K | Potentiometer |  |  |
| 2 H 82301 | R348 | 82K | H.S. | 1\% | $\frac{1}{4} \mathrm{~W}$ |
| 2H33401 | R349 | 330K | H.S. | 1\% | $\frac{1}{4} \mathrm{w}$ |
| S 10210 | R350 | 1K | C | 10\% | $\frac{1}{4} w$ |
| 2 H 10401 | R351 | 100K | H.S. | 1\% | $\frac{1}{4} \mathrm{w}$ |
| Y47210 | R352 | 4.7K | C | 10\% | $\frac{1}{2} w$ |
| Y75205 | R353 | 7.5K | C | 5\% | $\frac{1}{2} \mathrm{w}$ |
| Y39210 | R354 | 3.9K | C | 10\% | $\frac{1}{2} w$ |
| 2 H 40401 | R355 | 400K | H.S. | 1\% | $\frac{1}{4} W$ |
| 57C | RV356 | 22K | Potentiometer |  |  |
| 2 H 82301 | R357 | 82K | H.S. | 1\% | $\frac{1}{4} \mathrm{~W}$ |
| 2 H 33401 | R358 | 330K | H.S. | 1\% | $\frac{1}{4} \mathrm{w}$ |
| 2H10401 | R359 | 100K | H.S. | 1\% | $\frac{1}{4} \mathrm{~W}$ |
| Y56210 | R361 | 5.6K | C | 10\% | $\frac{1}{2} \mathrm{w}$ |
| Y75205 | R362 | 7.5K | C | 5\% | $\frac{1}{2} \mathrm{w}$ |
| S39210 | R363 | 3.9K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S 15210 | R364 | 1.5K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S22110 | R365 | 220 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S56210 | R366 | 5.6K | C | 10\% | $\frac{1}{4} w$ |
| S 10110 | R367 | 100 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S10110 | R368 | 100 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S 10110 | R369 | 100 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S10110 | R371 | 100 | C | 10\% | $\frac{1}{4} w$ |
| 20X | C301 | 0.01 | CER | 20\% | 1.5 KV |
| 18K | C302 | 1000P | PE | 10\% | 400v |
| 46K | C303 | 5P | SM | 10\% | 250 v |

## C.R.T. CIRCUIT (continued)

| Part No. | С.С.т. Ref. | Value | Description | Tolerance | $\begin{aligned} & \text { Rating } \\ & @ 70^{\circ} \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 65 J | C304 | 0.1 | PE | 10\% | 400v |
| 6 J | C305 | 470P | CER | 20\% | 1.5 KV |
| 20x | C306 | 0.01 | CER | 20\% | 1.5 KV |
| 98J | C307 | 0.02 | CER | $-20 \%$ | 2KV |
| 49K | C309 | 30P | CER |  | 500 v |
| 67J | C311 | 0.01 | PE | 20\% | 400 v |
| 49 K | C312 | 30P | CER |  | $500 v$ |
| 67J | C313 | 0.01 | PE | 20\% | 400 v |
| 16K | C314 | 0.1 | PE | 10\% | 400 v |
| 78C | S301 |  | Switch 'Markers On/Off' |  |  |
| 42D | S302 |  |  |  |  |
|  | L301 |  | Coil Variable set $10 \mathrm{mc} / \mathrm{s}$ Markers Drg. 41114 |  |  |
| 18 T | V301 |  | Valve ECC88 |  |  |
| 18 T | V302 |  | Valve ECC88 |  |  |
| 18 T | V303 |  | Valve ECC88 |  |  |
| 189 | V304 |  | Valve ECC88 |  |  |
| 18 T | V305 |  | Valve ECC88 |  |  |
| $50 Y$ | CRT |  | M.O. Valv |  |  |

## POWER SUPPLY

| Part <br> No. | $\begin{aligned} & \text { C.C.T. } \\ & \text { Ref. } \\ & \hline \end{aligned}$ | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S22410 | R401 | 220K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| 69L | R402 | 100K | M.F. | 5\% | $\frac{1}{4}$ |
| 99 C | RV403 | 25 | Potentiometer Scale Illum ganged to S401 |  |  |
| S22110 | R404 | 220 | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| Y33210 | R405 | 3.3K | C | 10\% | $\frac{1}{2} \mathrm{w}$ |
| 56 C | RV406 | 2.2K | C Potentiometer |  |  |
| 2 H 36201 | R407 | 3.6K | H.S. | 1\% | $\frac{1}{4} w$ |
| 65 M | R408 | 1 K | W/W | 5\% | 4.5 w |
| Y82110 | R409 | 820 | C |  | $\frac{1}{2} w$ |
| 65M | R411 | 1 K | W/W | 5\% | 4.5 w |
| Y82110 | R412 | 820 | C | 10\% | $\frac{1}{2} w$ |
| S27210 | R413 | 2.7K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S22110 | R414 | 220 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| Y33210 | R415 | 3.3K | C | 10\% | $\frac{1}{2} \mathrm{w}$ |
| S68110 | R416 | 680 | C | 10\% | $\frac{1}{4} w$ |
| S68110 | R417 | 680 | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| 116L | R418 | 2.2K | W/W | 10\% | 10 w |
| 2H18401 | R419 | 180K | H.S. | 1\% | $\frac{1}{4} w$ |
| 2 H 35401 | R421 | 350K | H.S. | 1\% | $\frac{1}{4} \mathrm{w}$ |
| S10110 | R422 | 100 | C | 10\% | $\frac{1}{4} w$ |
| S10110 | R423 | 100 | C | 10\% | $\frac{1}{4} w$ |
| 556210 | R424 | 5.6K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S 10510 | R425 | 1 M | C | 10\% | $\frac{1}{4} w$ |
| S47210 | R426 | 4.7K | C | 10\% | $\frac{1}{4} \mathrm{w}$ |
| S33310 | R427 | 33K | C | 10\% | $\frac{1}{4} \mathrm{~W}$ |
| S 10110 | R428 | 100 | C | 10\% | $\frac{1}{4} w$ |
| S 10510 | R429 | 1 M | C | 10\% | $\frac{1}{4} w$ |
| S18410 | R431 | 180K | C | 10\% | $\frac{1}{4} w$ |
| Y27310 | R432 | 27K | C | 10\% | $\frac{1}{2} w$ |
| Y27310 | R433 | 27K | C | 10\% | $\frac{1}{2} \mathrm{w}$ |
| Y27310 | R434 | 27K | C | 10\% | $\frac{1}{2} w$ |
| Y27310 | R435 | 27K | C | 10\% | $\frac{1}{2} w$ |
| Y15210 | R436 | 1.5K | C | 10\% | $\frac{1}{2} w$ |
| S 10510 | R437 | 1 M | C | 10\% | $\frac{1}{4} w$ |

POWER SUPPLY (continued)

| Part <br> No. | $\begin{gathered} \text { C.C.T. } \\ \text { Ref. } \\ \hline \end{gathered}$ | Value | Description | Tolerance | Rating <br> @ $70^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| S27410 | R438 | 270K | C | 10\% | $\frac{1}{4}$ w |
| 58 C | RV439 | 220K | Potentiometer |  |  |
| S68310 | R441 | 68K | C | 10\% | $\frac{1}{4} w$ |
| S10110 | R442 | 100 | C | 10\% | $\frac{1}{4} w$ |
| 65 J | C401 | 0.1 | PE | 10\% | $400 \sim$ |
| 65J | C402 | 0.1 | PE | 10\% | $400 v$ |
| 995 | C403 | 16000 | ELEC |  | 10 |
| 915 | C404 | 120 | ELEC |  | 200 v |
| 915 | C405 | 120 | ELEC |  | $200 \%$ |
| 915 | C406 | 120 | ELEC |  | 200 , |
| 915 | C407 | 120 | ELEC |  | $200 \%$ |
| 42X | C408 | 32+32 | ELEC |  | 450 v |
| 93J | C409 | $\begin{aligned} & 1000 \\ & 1000 \end{aligned}$ | ELEC |  | 18 v |
| 20K | C411 | 4700P | PE | 10\% | 125 v |
| 42X | C412 | $32+32$ | ELEC |  | 450 |
| 33X | C413 | 250 | ELEC |  | 18 v |
| 33X | C414 | 250 | ELEC |  | 18 v |
| 39J | C415 | 0.05 | P |  | 2 Kv |
| 66 J | C416 | 0.1 | PE | 10\% | 250 |
| 37X | C417 | 0.05 | P |  | 3.5 Kv |
| 37X | C418 | 0.05 | P |  | 3.5 KV |
| 13K | C419 | 0.05 | P |  | 2.5 KV |
| 92J | C421 | 16 | ELEC |  | 450 v |
| 92J | C422 | 16 | ELEC |  | 450 v |
| 92J | C423 | 16 | ELEC |  | 450 v |
| 92J | C424 | 16 | ELEC |  | 450 v |
| 66J | C425 | 0.1 | PE | 10\% | 250 v |
| 94 J | C426 | $32+32+32$ | ELEC |  | 350 v |
| 65J | C427 | 0.1 | PE | 10\% | 400 v |
| 42X | C428 | 32+32 | ELEC |  | 450 v |
| 42X | C429 | 32+32 | ELEC |  | 450 v |

## POWER SUPPLY (continued)

| Part No. | $\begin{aligned} & \text { C.C.T. } \\ & \text { Ref. } \\ & \hline \end{aligned}$ | Value | Description | Tolerance | $\begin{aligned} & \text { Rating } \\ & @ 70^{\circ} \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 97J | C431 | 50+50 | ELEC | $\begin{aligned} & -20 \% \\ & +50 \% \end{aligned}$ | $200 v$ |
| 98J | C432 | 0.02 | CER |  | 2 Kv |
| 98J | C433 | 0.02 | CER |  | 2 Kv |


| 55F | MR401 | Rectifier Type | 15020 Texas |
| :---: | :---: | :---: | :---: |
| 55F | MR402 | " " | 15020 Texas |
| 180 | MR403 | " " | ZS75 |
| 180 | MR404 | " " | ZS75 |
| 10E | MR405 | " " | ZS70 |
| 68 T | MR406 | Zener Diode | $11 V 15 \%$ |
| 180 | MR407 | Rectifier Type | ZS75 |
| 180 | MR408 | " | ZS75 |
| 72 T | MR409 | Zener Diode | ZB7.5 Brush |
| 180 | MR410 | Rectifier | ZS75 or DDO58 |
| 60 | MR411 | " | K8/50 |
| 60 | MR412 | " | K8/50 |
| 60 | MR413 | " | K8/50 |
| 60 | MR414 | " | K8/50 |
| 70 | MR415 | " | ZS78 or DDO58 |
| 70 | MR416 | " | ZS78 or DDO58 |
| 70 | MR417 | " | ZS78 or DDO58 |
| 70 | MR418 | " | ZS78 or DDO58 |
| 180 | MR419 | " | ZS75 |
| 120 T | TR401 | Transistor Mullard Type ACY22 <br> " Newmarket Type NKT452 <br> " Mullard Type ACY22 |  |
| 118 T | TR402 |  |  |
| 120 T | TR403 |  |  |
| 38 T | V401 | Valve Mullard EL86  <br> $"$ $"$ ECF80 <br> $"$ $"$ EF184 |  |
| 10 T | V402 |  |  |
| 26 T | V403 |  |  |

## POWER SUPPLY (continued)

| Part No. | $\begin{aligned} & \text { C.C.T. } \\ & \text { Ref. } \\ & \hline \end{aligned}$ | Value | Description | Tolerance | $\begin{aligned} & \text { Rating } \\ & @ \quad 70^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 48 Y | N401 |  | Neon XC 12 |  |  |
| 4 Y | LP401 |  | Power Supply Lamp 6.5v |  |  |
| 4 Y | LP402 |  | Scale Illum 6.5v |  |  |
| 4 Y | LP403 |  | $\begin{array}{ll} " & 6.5 v \end{array}$ |  |  |
| 615 | T401 |  | Primary$\begin{aligned} & 0-110 v A C \\ & 0-110 v A C \\ & 0-5-10-20 v A C \end{aligned}$ | $\begin{aligned} & \text { Secondary } \\ & 0-6.5 \mathrm{v} \\ & 8.1 \mathrm{lv}-0-8.1 \mathrm{lv} \\ & 0-153 \mathrm{v} \\ & 0-510 \mathrm{v} \end{aligned}$ |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| 625 | T402 |  | $\begin{aligned} & \text { Primary } \\ & 0-110 v A C \\ & 0-110 v A C \\ & 0-5-10-20 v A C \end{aligned}$ | Secondary$\begin{aligned} & 0-6.3 v 0-6.3 v \\ & 0-6.3 v \\ & 150 v \\ & 0-150-350-750-1000 \end{aligned}$ |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  | P401 |  | Fuse 1.5 A at 250 v 3 A at 110 v |  |  |
|  |  |  |  | \% |  |
|  | S401 |  | Mains On/Off o | le lllum 'Pot |  |



PLATE. 2.


PLATE. 3.


VIEWED AT REAR.
PLATE. 4.



TRIG SELECTOR SWIICH
TRIGGER CIRCUIT
FIG.2.I.
TYPE TS4I,TD4I, TS42 \& TD42

Milles generator


TIMEBASE \& HORIZONTAL AMPLIFIER TYPE TD42 \& TS42

TB (B) Pin $6-6.3$ volt. $A C$


notes
1 * denotes components not mounted on pcr
2 (N) oenotes terminals on pC 26
DELAY CIRCUIT TYPE D56 FIG 2.6


VERTICAL AMPLIFIERS TYPE D56
FIG 3.1


INPUT ATTENUATOR
TYPE.D 56
FIG.3.2.

TELEQUIPEMENT D56 TID-BAS PC 8


